

CITY OF ALBUQUERQUE

PLANNING DEPARTMENT – Development Review Services



May 5, 2016

Ron Bohannan, PE
Tierra West, LLC
5571 Midway Park Pl NE
Albuquerque, NM 87109

Richard J. Berry, Mayor

**RE: Skilled Nursing Facility, Renaissance Center (File: F16D017)
Drainage Report, Engineer's Stamp Date 4-25-2016
Grading Plan, Engineer's Stamp Date 5-5-2016**

Dear Mr. Bohannan:

Based upon the information provided in your submittal received 4-26-16, the above referenced plan is approved for ESC Permit (Building Permit). Please attach a copy of this approved plan in the construction sets when submitting for a building permit.

Prior to Certificate of Occupancy release, Engineer Certification per the DPM checklist will be required.

PO Box 1293

If you have any questions, you can contact me at 924-3695.

Albuquerque

New Mexico 87103

www.cabq.gov

Sincerely,

A handwritten signature in black ink, appearing to read "Rita L. H."

Rita Harmon, P.E.
Senior Engineer, Planning Dept.
Development Review Services

Orig: Drainage file
c.pdf recipient , Joel Hernandez



City of Albuquerque

Planning Department
Development & Building Services Division

DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 09/2015)

Project Title: Skilled Nursing Facility	Building Permit #: _____	City Drainage #: F16/D017
DRB#:	EPC#:	Work Order#:
Legal Description: TR 8-A Plat of Tracts 8-A and 8-B Renaissance Center		
City Address: 1610 Renaissance Blvd NE Albuquerque NM 87107		
Engineering Firm: Tierra West, LLC	Contact: Joel Hernandez	
Address: 5571 Midway Park Place NE Albuquerque NM 87109		
Phone#: 505-858-3100	Fax#: 505-858-1118	E-mail: jdherandez@tierrawestllc.com
Owner: AS Realty Investors	Contact: Adam Schlesinger	
Address: 3701 S. Robertson Blvd., Suite 201 Culver City, California 90232		
Phone#: 310-202-6204	Fax#: 310-202-0831	E-mail: adam@asrealtyinvestors.com
Architect: Bixler Management	Contact: Mark Bixler	
Address:		
Phone#: 870-653-3382	Fax#:	E-mail: mbixler@bixlermanagement.com
Other Contact: Surveyor- Precision Surveys, Inc.	Contact: Larry Medrano	
Address: P.O. Box 90636 Albuquerque NM 87199		
Phone#: 505-858-5700	Fax#:	E-mail: larry@presurv.com

Check all that Apply:

DEPARTMENT:

- HYDROLOGY/ DRAINAGE
 TRAFFIC/ TRANSPORTATION
 MS4/ EROSION & SEDIMENT CONTROL

TYPE OF SUBMITTAL:

- ENGINEER/ ARCHITECT CERTIFICATION

 CONCEPTUAL G & D PLAN
 GRADING PLAN
 DRAINAGE MASTER PLAN
 DRAINAGE REPORT
 CLOMR/LOMR

 TRAFFIC CIRCULATION LAYOUT (TCL)
 TRAFFIC IMPACT STUDY (TIS)
 EROSION & SEDIMENT CONTROL PLAN (ESC)

OTHER (SPECIFY) _____

CHECK TYPE OF APPROVAL/ACCEPTANCE SOUGHT:

- BUILDING PERMIT APPROVAL
 CERTIFICATE OF OCCUPANCY

 PRELIMINARY PLAT APPROVAL
 SITE PLAN FOR SUB'D APPROVAL
 SITE PLAN FOR BLDG. PERMIT APPROVAL
 FINAL PLAT APPROVAL
 SIA/ RELEASE OF FINANCIAL GUARANTEE
 FOUNDATION PERMIT APPROVAL
 GRADING PERMIT APPROVAL
 SO-19 APPROVAL
 PAVING PERMIT APPROVAL
 GRADING/ PAD CERTIFICATION
 WORK ORDER APPROVAL
 CLOMR/LOMR

 PRE-DESIGN MEETING
 OTHER (SPECIFY) _____

IS THIS A RESUBMITTAL?: Yes _____ No _____

DATE SUBMITTED: 4/25/16 By: Joel Hernandez

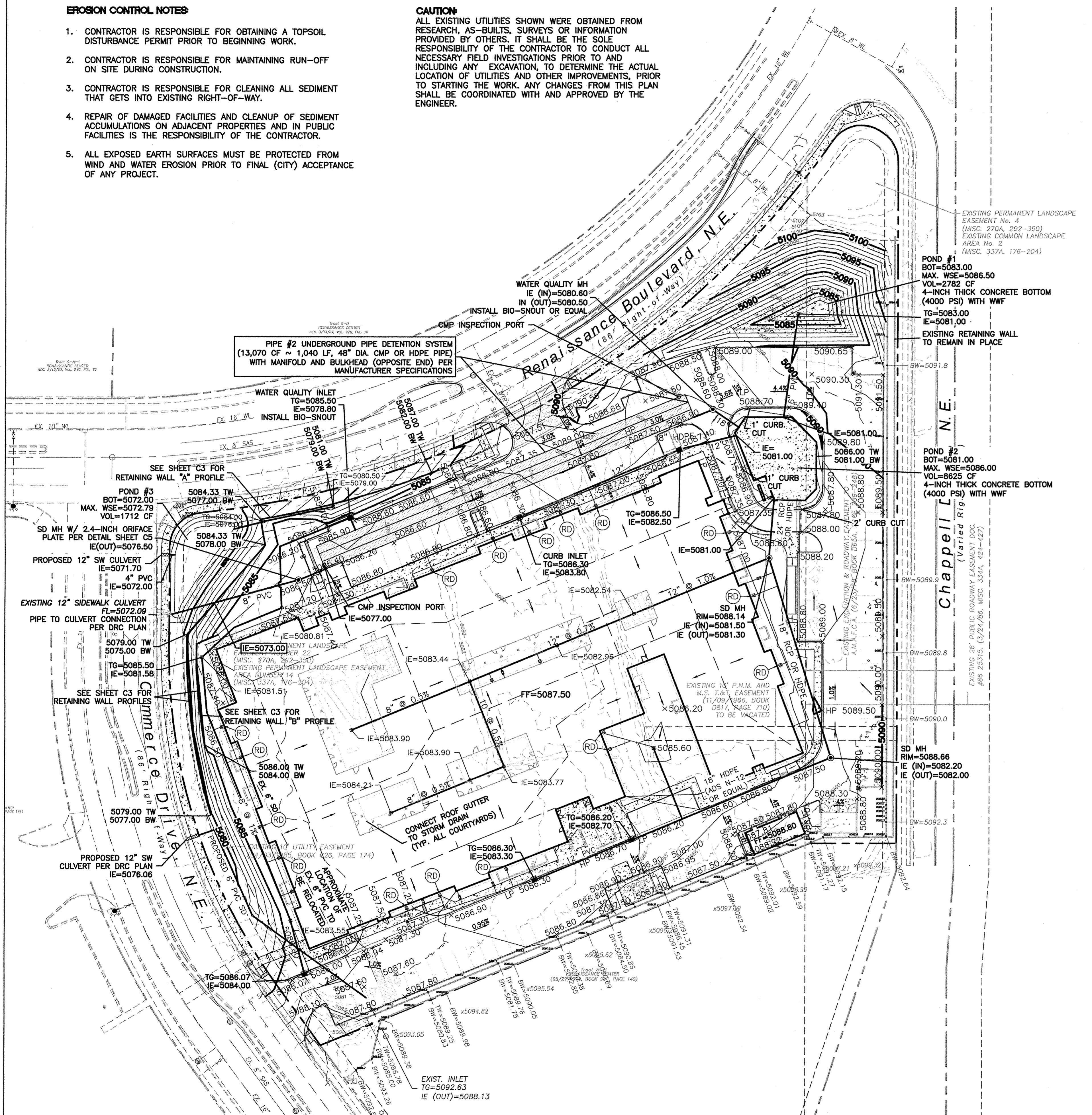
COA STAFF: ELECTRONIC SUBMITTAL RECEIVED: _____

EROSION CONTROL NOTES:

1. CONTRACTOR IS RESPONSIBLE FOR OBTAINING A TOPSOIL DISTURBANCE PERMIT PRIOR TO BEGINNING WORK.
 2. CONTRACTOR IS RESPONSIBLE FOR MAINTAINING RUN-OFF ON SITE DURING CONSTRUCTION.
 3. CONTRACTOR IS RESPONSIBLE FOR CLEANING ALL SEDIMENT THAT GETS INTO EXISTING RIGHT-OF-WAY.
 4. REPAIR OF DAMAGED FACILITIES AND CLEANUP OF SEDIMENT ACCUMULATIONS ON ADJACENT PROPERTIES AND IN PUBLIC FACILITIES IS THE RESPONSIBILITY OF THE CONTRACTOR.
 5. ALL EXPOSED EARTH SURFACES MUST BE PROTECTED FROM WIND AND WATER EROSION PRIOR TO FINAL (CITY) ACCEPTANCE OF ANY PROJECT.

CAUTION

ALL EXISTING UTILITIES SHOWN WERE OBTAINED FROM RESEARCH, AS-BUILTS, SURVEYS OR INFORMATION PROVIDED BY OTHERS. IT SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR TO CONDUCT ALL NECESSARY FIELD INVESTIGATIONS PRIOR TO AND INCLUDING ANY EXCAVATION, TO DETERMINE THE ACTUAL LOCATION OF UTILITIES AND OTHER IMPROVEMENTS, PRIOR TO STARTING THE WORK. ANY CHANGES FROM THIS PLAN SHALL BE COORDINATED WITH AND APPROVED BY THE ENGINEER.

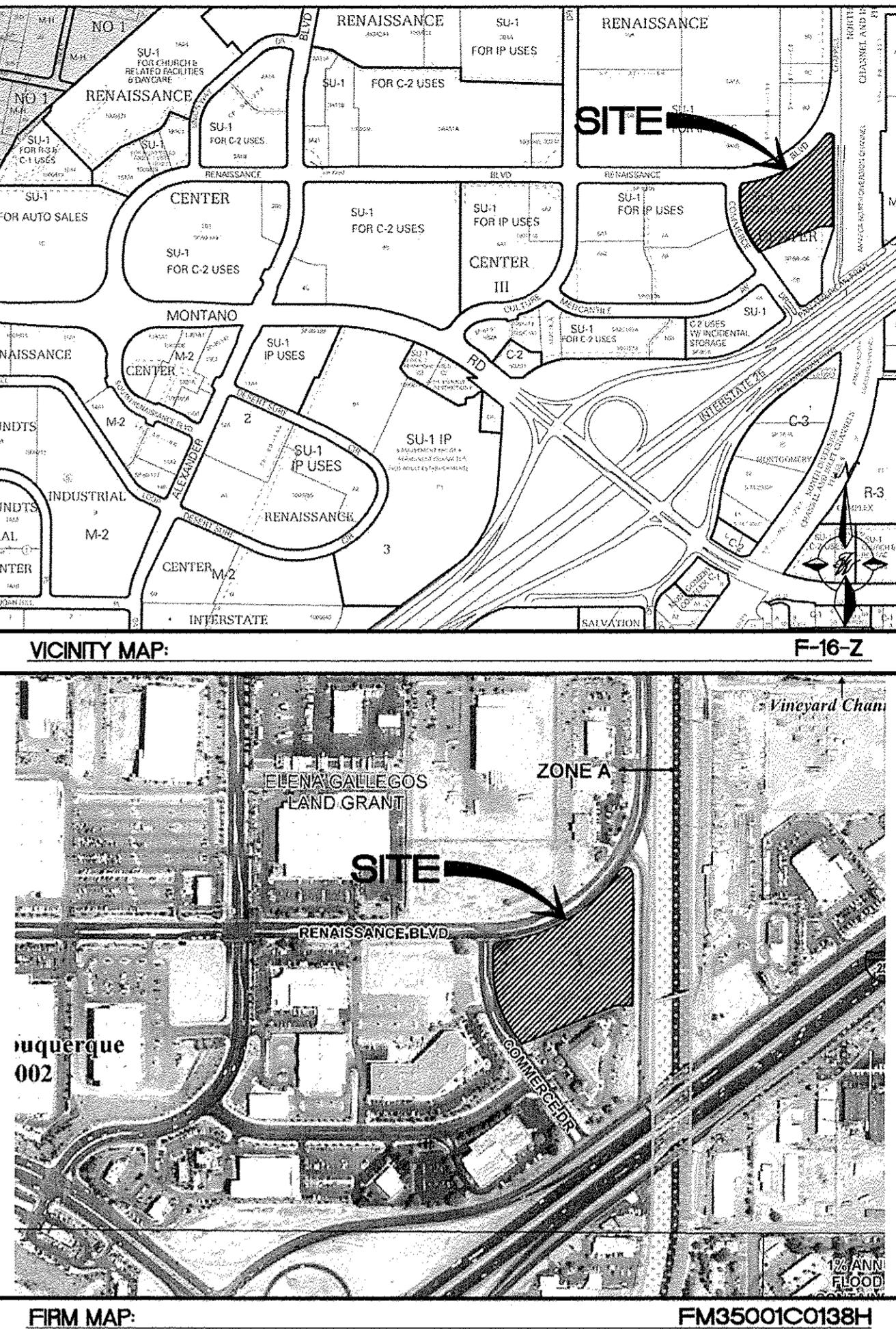


LEGEND

— — — — —	CURB & GUTTER
— — — — —	BOUNDARY LINE
— — — — —	EASEMENT
— — — — —	CENTERLINE
— — — — —	RIGHT-OF-WAY
— — — — —	BUILDING
— — — — —	SIDEWALK
— — — — —	SCREEN WALL
— — — — —	RETAINING WALL
5010 — — — —	CONTOUR MAJOR
5011 — — — —	CONTOUR MINOR
x 5048.25	SPOT ELEVATION
— — — — —	FLOW ARROW
— — — — —	EXISTING CURB & GUTTER
— — — — —	EXISTING BOUNDARY LINE
— — — — —	EXISTING CONTOUR MAJOR
— — — — —	EXISTING CONTOUR MINOR
x 5048.25	EXISTING SPOT ELEVATION

KEYED NOTE:

ROOF DRAIN CONNECTED TO 9"X9" AREA INLET, NDS
OR EQUAL

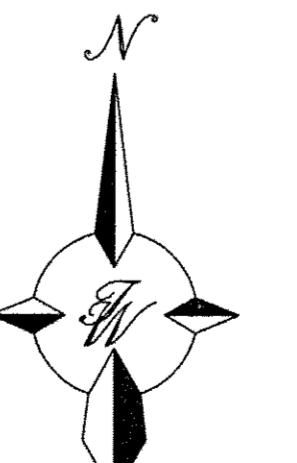


NOTICE TO CONTRACTORS

1. AN EXCAVATION/CONSTRUCTION PERMIT WILL BE REQUIRED BEFORE BEGINNING ANY WORK WITHIN CITY RIGHT-OF-WAY.
 2. ALL WORK DETAILED ON THESE PLANS TO BE PERFORMED, EXCEPT AS OTHERWISE STATED OR PROVIDED HERON, SHALL BE CONSTRUCTED IN ACCORDANCE WITH CITY OF ALBUQUERQUE INTERIM STANDARD SPECIFICATIONS FOR PUBLIC WORKS CONSTRUCTION, 1985.
 3. TWO WORKING DAYS PRIOR TO ANY EXCAVATION, CONTRACTOR MUST CONTACT LINE LOCATING SERVICE, 765-1234, FOR LOCATION OF EXISTING UTILITIES.
 4. PRIOR TO CONSTRUCTION, THE CONTRACTOR SHALL EXCAVATE AND VERIFY THE HORIZONTAL AND VERTICAL LOCATIONS OF ALL CONNECTIONS. SHOULD A CONFLICT EXIST, THE CONTRACTOR SHALL NOTIFY THE ENGINEER SO THAT THE CONFLICT CAN BE RESOLVED WITH A MINIMUM AMOUNT OF DELAY.
 5. BACKFILL COMPACTION SHALL BE ACCORDING TO TRAFFIC/STREET USE.
 6. MAINTENANCE OF THESE FACILITIES SHALL BE THE RESPONSIBILITY OF THE OWNER OF THE PROPERTY SERVED. 7. WORK ON ARTERIAL STREETS SHALL BE PERFORMED ON A 24-HOUR BASIS.

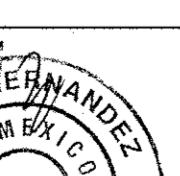
APPROVAL	NAME	DATE
INSPECTOR		

ROUGH GRADING APPROVAL



GRAPHIC SCALE

SCALE: 1" = 40'

ENGINEER'S SEAL	SKILLED NURSING FACILITY RENAISSANCE CENTER	DRAWN BY DY
	GRADING AND DRAINAGE PLAN	DATE 5/05/16
		2014088-GRE
		SHEET #
		C2
JOEL D. HERNANDEZ P.E. #17893	TIERRA WEST, LLC <hr/>  5571 MIDWAY PARK PLACE NE ALBUQUERQUE, NM 87109 (505) 858-3100 www(tierrawestllc.com	JOB # 2014088

EROSION CONTROL NOTES:

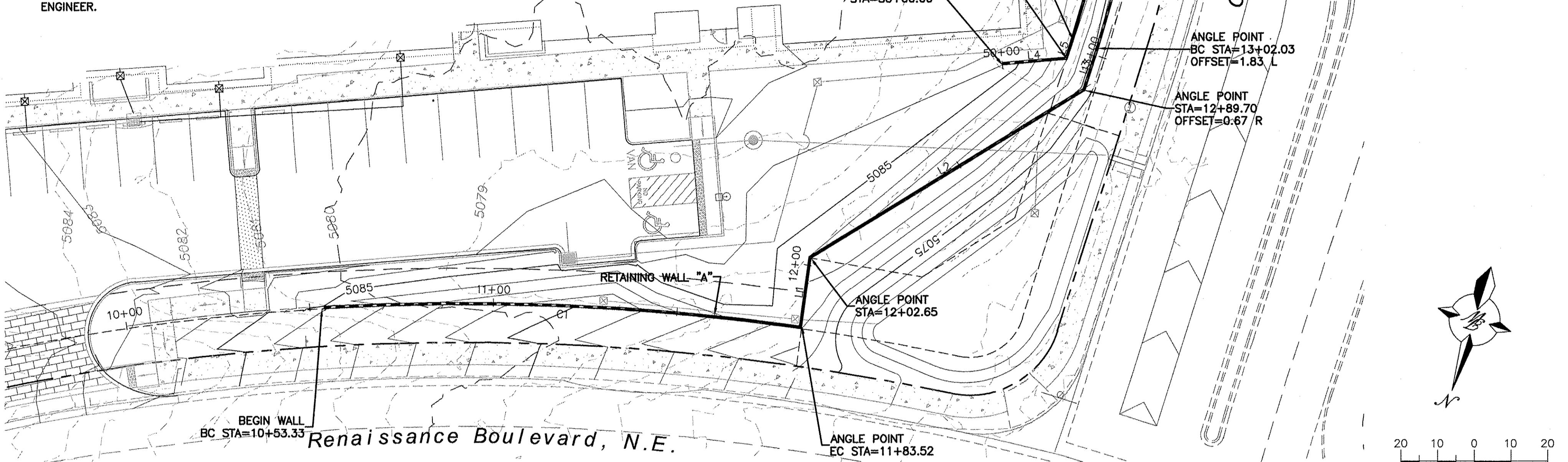
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LINE TABLE

LINE	BEARING	LENGTH
L1	S9°50'02"E	19.16
L2	S41°19'13"W	87.05
L3	S0°12'08"W	11.90
L4	S67°47'37"W	17.68
L5	S0°12'08"W	5.38

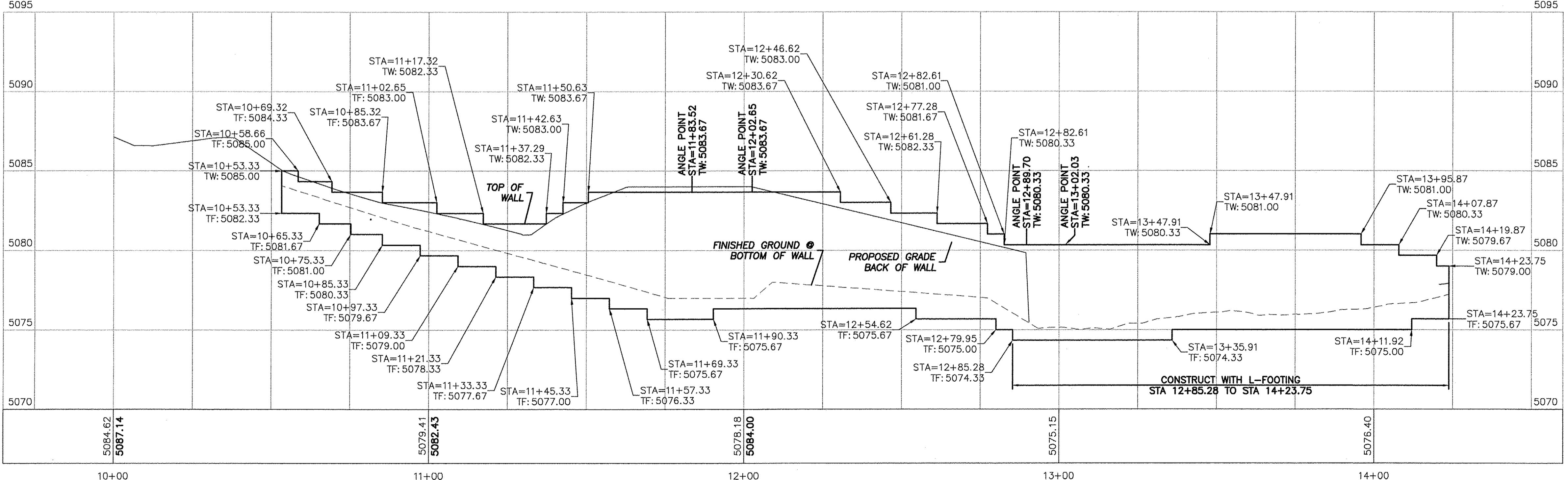
CURVE TABLE			
CURVE	DELTA	RADIUS	LENGTH
C1	11°28'16"	653.00	130.74
C2	16°53'06"	411.14	121.16
C3	9°47'25"	403.97	69.03

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LOCATION OF UTILITIES AND OTHER IMPROVEMENTS, PRIOR
TO STARTING THE WORK. ANY CHANGES FROM THIS PLAN
SHALL BE COORDINATED WITH AND APPROVED BY THE
ENGINEER.



SCALE: HORIZ. 1"=20'
 VERT. 1"=4'

RETAINING WALL "A"



LEGEND

- | | |
|------------|------------------------|
| ===== | CURB & GUTTER |
| ----- | BOUNDARY LINE |
| ----- | EASEMENT |
| ----- | BUILDING |
| [REDACTED] | SIDEWALK |
| ===== | RETAINING WALL |
| ----- | 5010 CONTOUR MAJOR |
| ----- | 5011 CONTOUR MINOR |
| ----- | EXISTING CURB & GUTTER |
| ----- | EXISTING BOUNDARY LINE |
| ----- | EXISTING CONTOUR MAJOR |
| ----- | EXISTING CONTOUR MINOR |

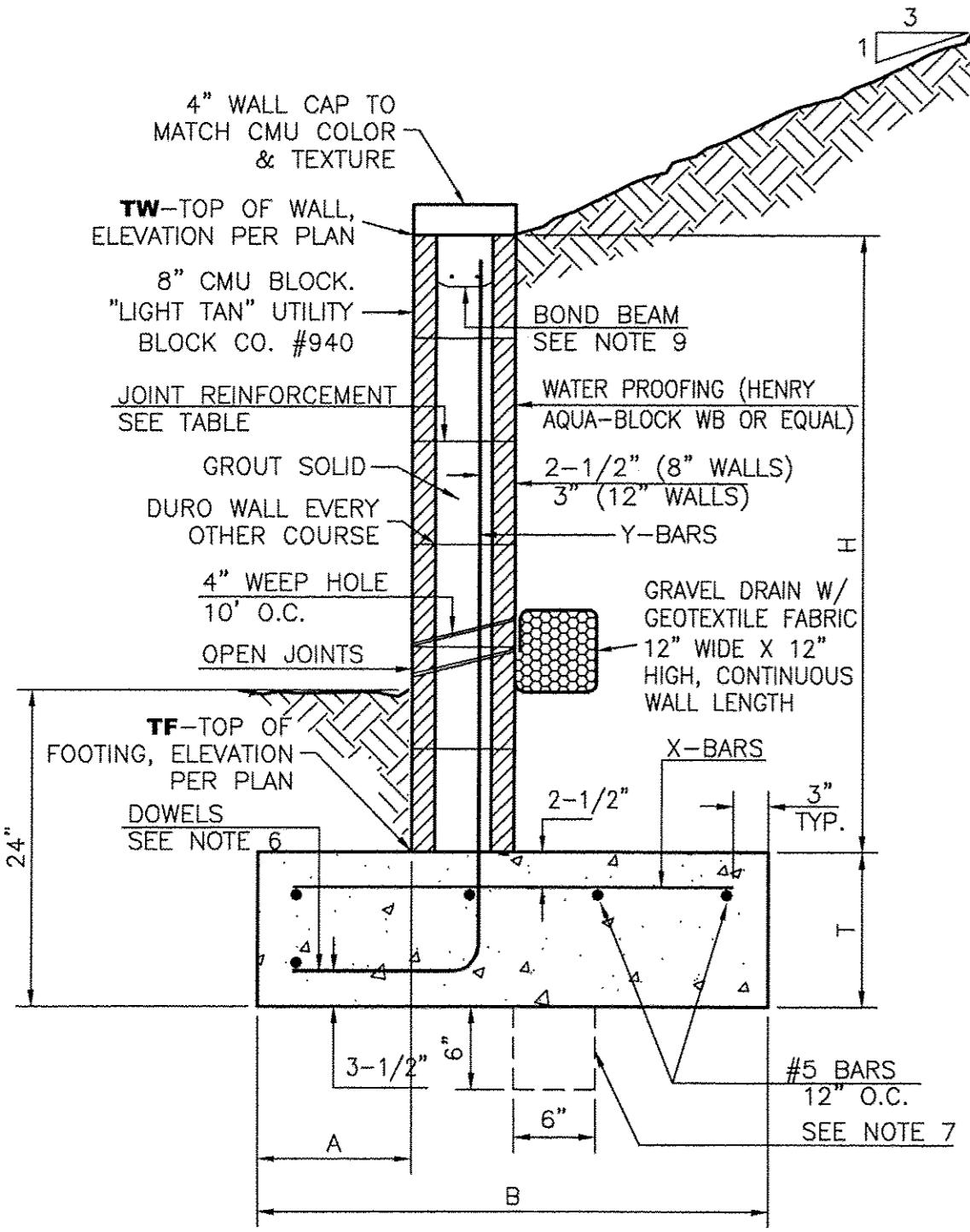
**SKILLED NURSING FACILITY
RENAISSANCE CENTER**

**RETAINING WALL
PLAN AND PROFILE**

DRAWN BY
DY
DATE
4/25/16

TIERRA WEST, LLC
5571 MIDWAY PARK PLACE NE
ALBUQUERQUE, NM 87109
(505) 858-3100
www.tierrawestllc.com

SHEET #
C3
JOB #
2014088



8 INCH REINFORCED CONCRETE MASONRY WALL					
H	A	B	T	Y-BARS	X-BARS
ft.-in.	in.	ft.-in.	in.		
2'-0"	8"	2'-0"	9"	#4 @ 32" O.C.	
3'-4"	8"	2'-0"	9"	#4 @ 32" O.C.	#4 @ 24" O.C.
4'-0"	10"	2'-8"	9"	#4 @ 32" O.C.	#4 @ 24" O.C.
4'-4"	12"	3'-4"	10"	#5 @ 32" O.C.	#4 @ 18" O.C.
5'-4"	14"	3'-10"	10"	#6 @ 16" O.C.	#4 @ 18" O.C.
6'-0"	16"	4'-8"	12"	#6 @ 8" O.C.	#4 @ 12" O.C.

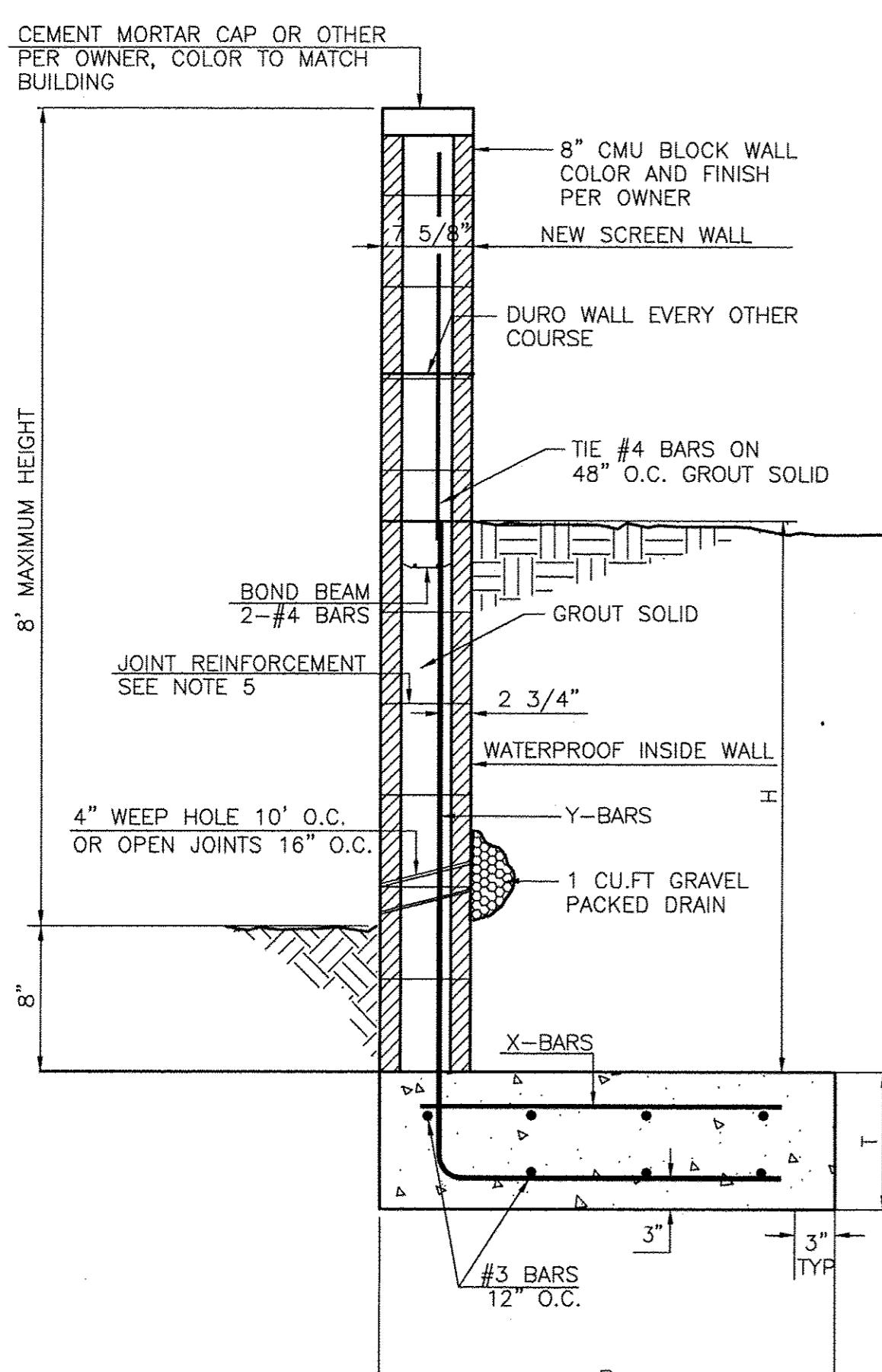
12 INCH REINFORCED CONCRETE MASONRY WALL					
H	A	B	T	Y-BARS	X-BARS
ft.-in.	in.	ft.-in.	in.		
5'-4"	14"	3'-8"	10"	#6 @ 18" O.C.	#4 @ 24" O.C.
6'-0"	15"	4'-2"	12"	#4 @ 16" O.C.	#4 @ 18" O.C.
6'-8"	16"	4'-6"	12"	#6 @ 24" O.C.	#5 @ 18" O.C.
7'-4"	18"	4'-10"	12"	#6 @ 16" O.C.	#5 @ 18" O.C.
8'-0"	20"	5'-4"	12"	#7 @ 18" O.C.	#6 @ 12" O.C.
8'-8"	20"	5'-8"	12"	#7 @ 16" O.C.	#6 @ 12" O.C.

GENERAL NOTES:

- ALL CONCRETE IS TO BE 4000 PSI @ 28 DAYS.
- MINIMUM COMPACTION UNDER FOOTINGS IS TO BE 95% PER ASTM D 1557 FOR A DEPTH OF 12" MOISTURE CONTENT IS TO BE \pm 2.0%.
- BACK FILL AGAINST WALLS IS TO BE HAND-PLACED AND COMPAKTED.
- ALL BARS ARE TO BE GRADE 60, ASTM 615.
- TRUSS TYPE DUR-O-WALL EVERY OTHER COURSE.
- DOWELS SHALL BE AT LEAST EQUAL IN SIZE AND SPACING TO V-BARS, SHALL PROJECT A MINIMUM OF 30 BAR DIAMETER INTO THE FILLED BLOCK CORES, AND SHALL EXTEND TO THE TOE OF THE FOOTING.
- PROVIDE KEY FOR 8" AND 12" WALLS WHERE H EXCEEDS 6'-0".
- USE EITHER EXPANSION JOINTS ON 20' CENTERS OR PILASTERS EVERY 12'.
- BOND BEAM, 1-#4 BARS FOR WALLS UNDER 3'-4", 2-#4 BARS FOR WALLS UNDER 5'-4", 2-#5 BARS FOR WALLS OVER 5'-4".

RETAINING WALL DETAIL

NTS

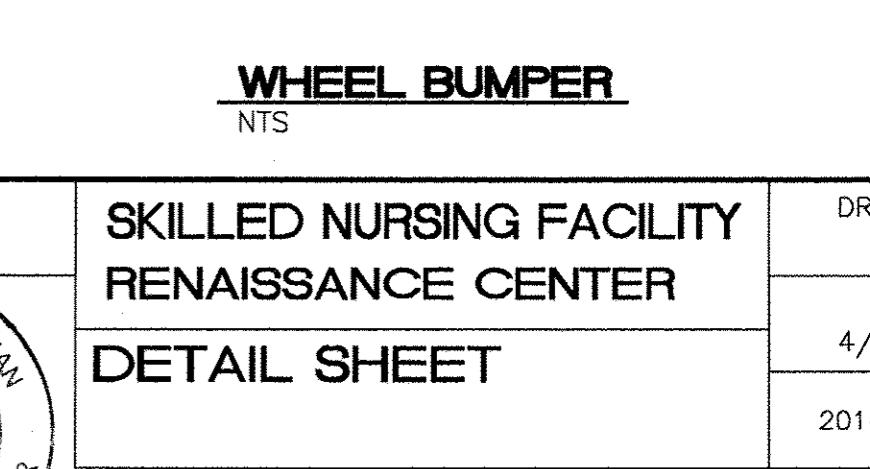
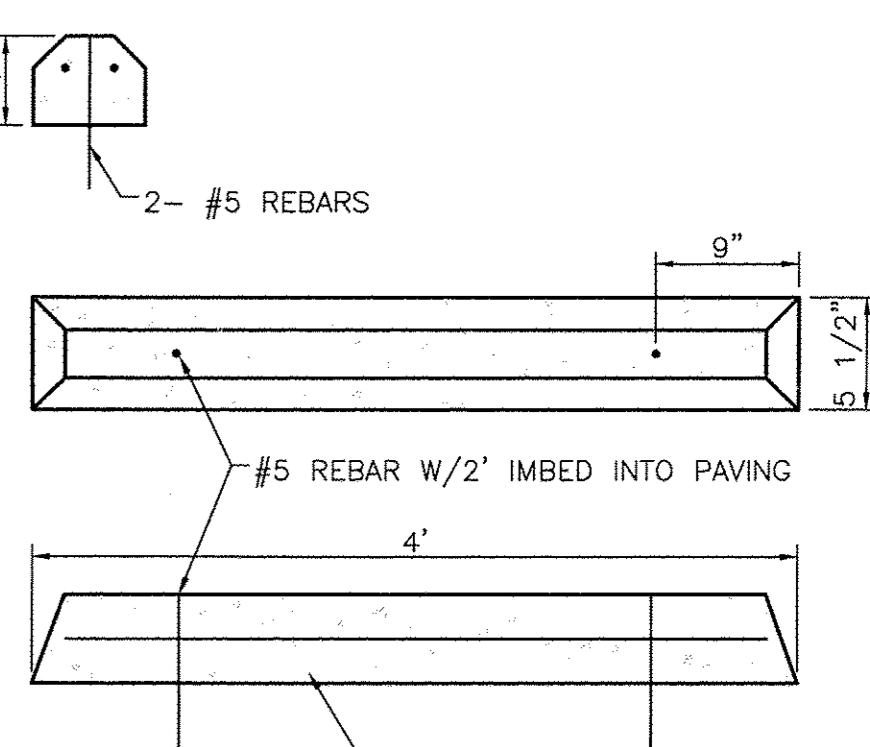
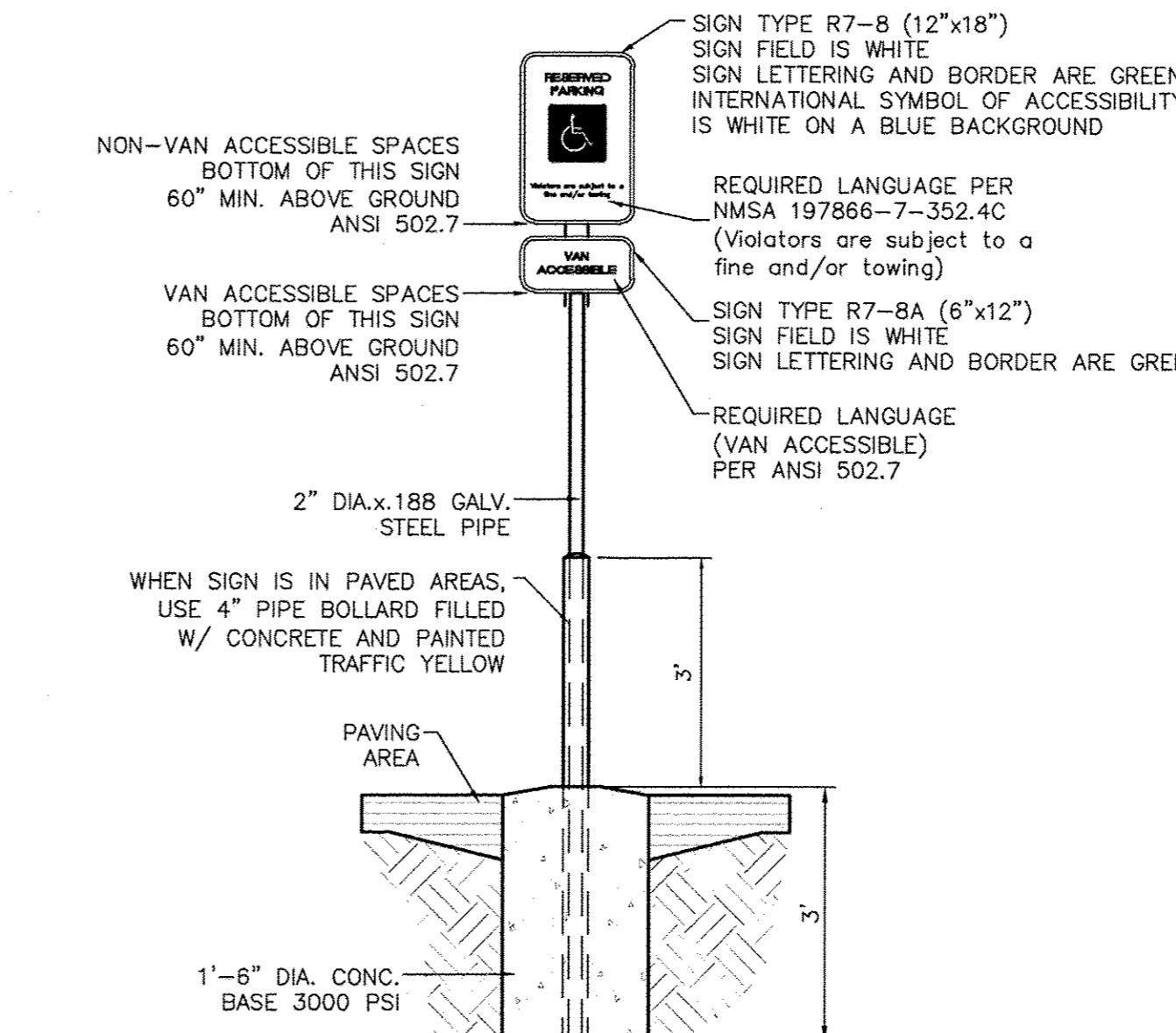
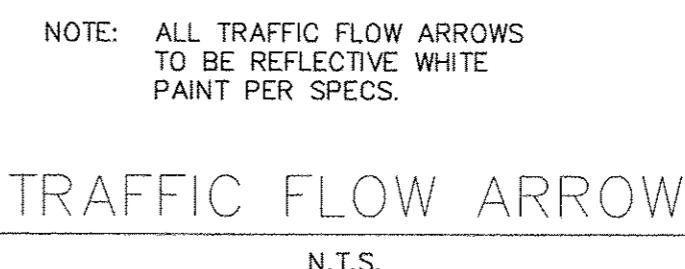
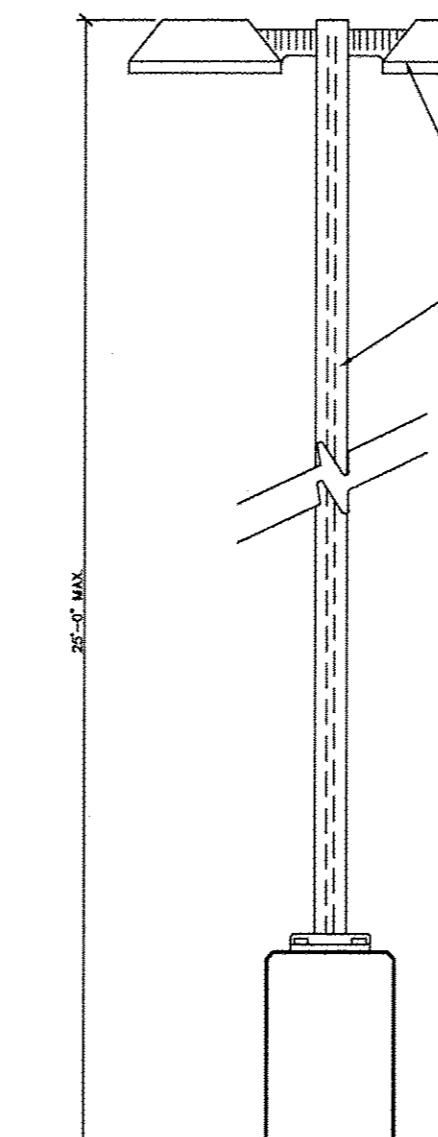
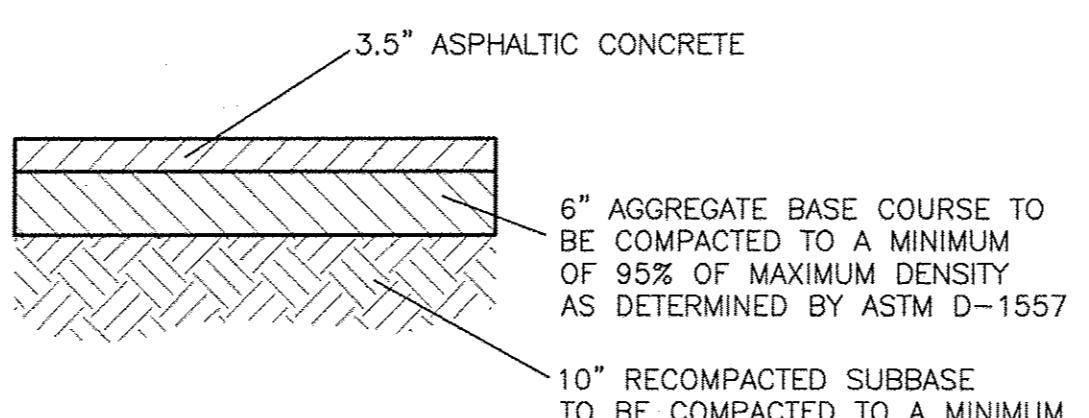
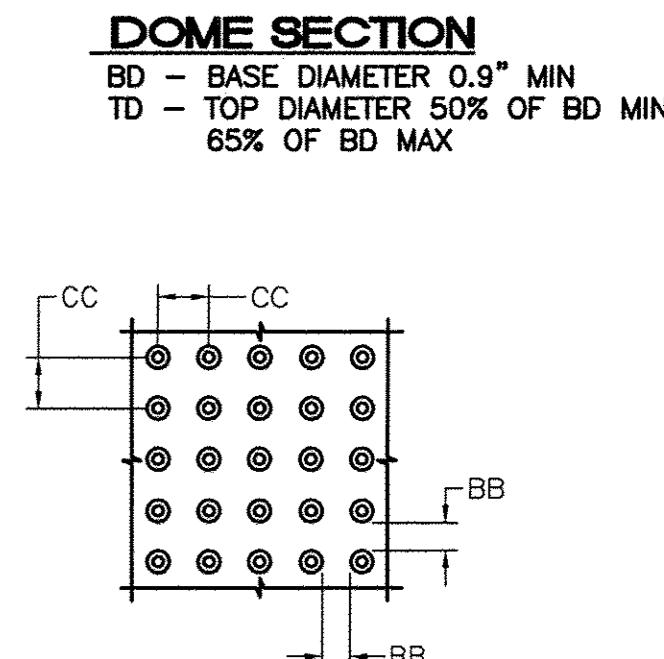
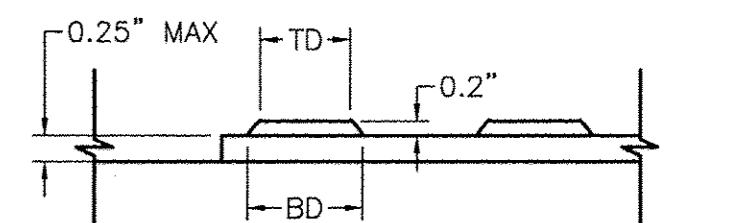
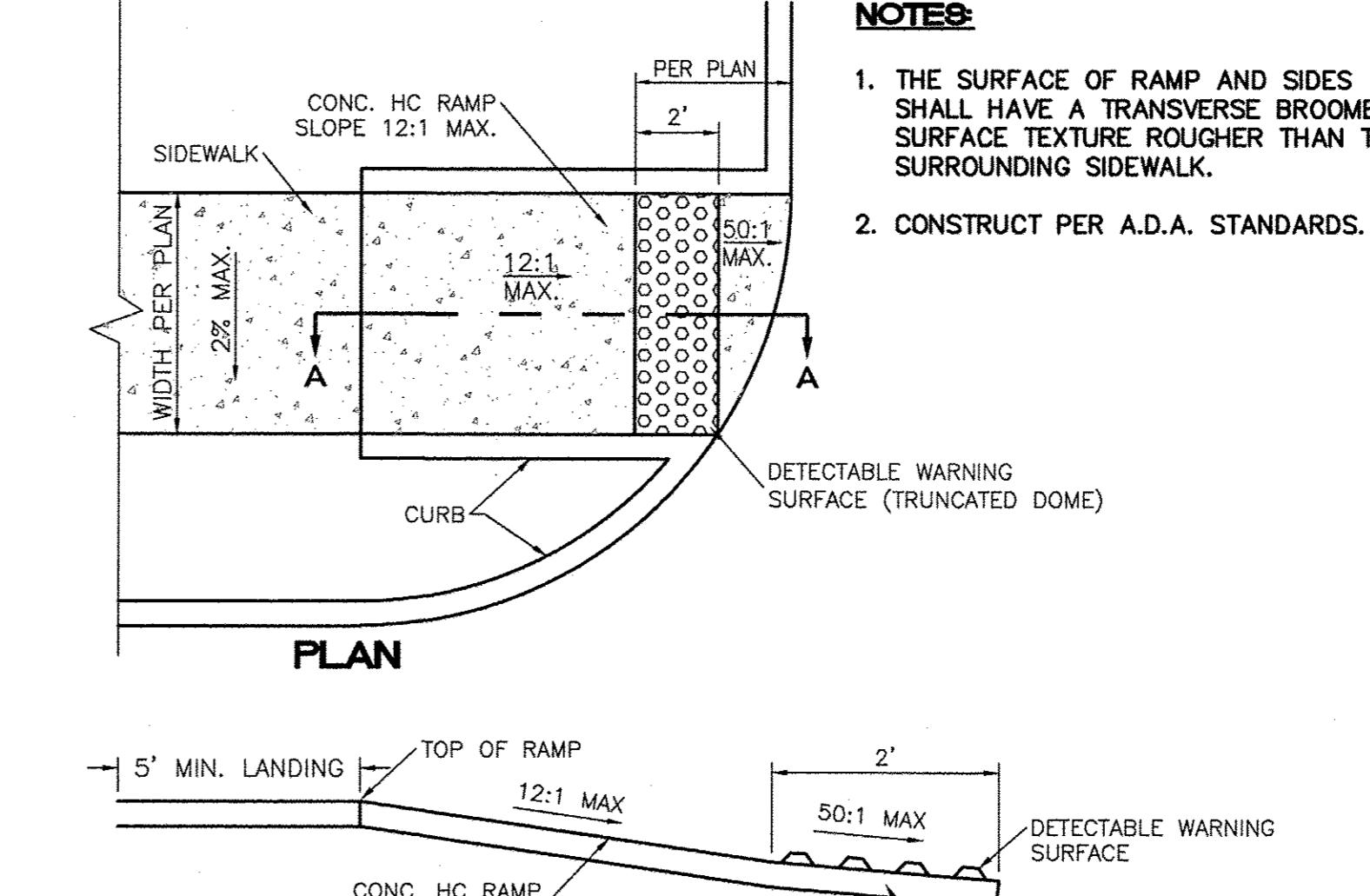
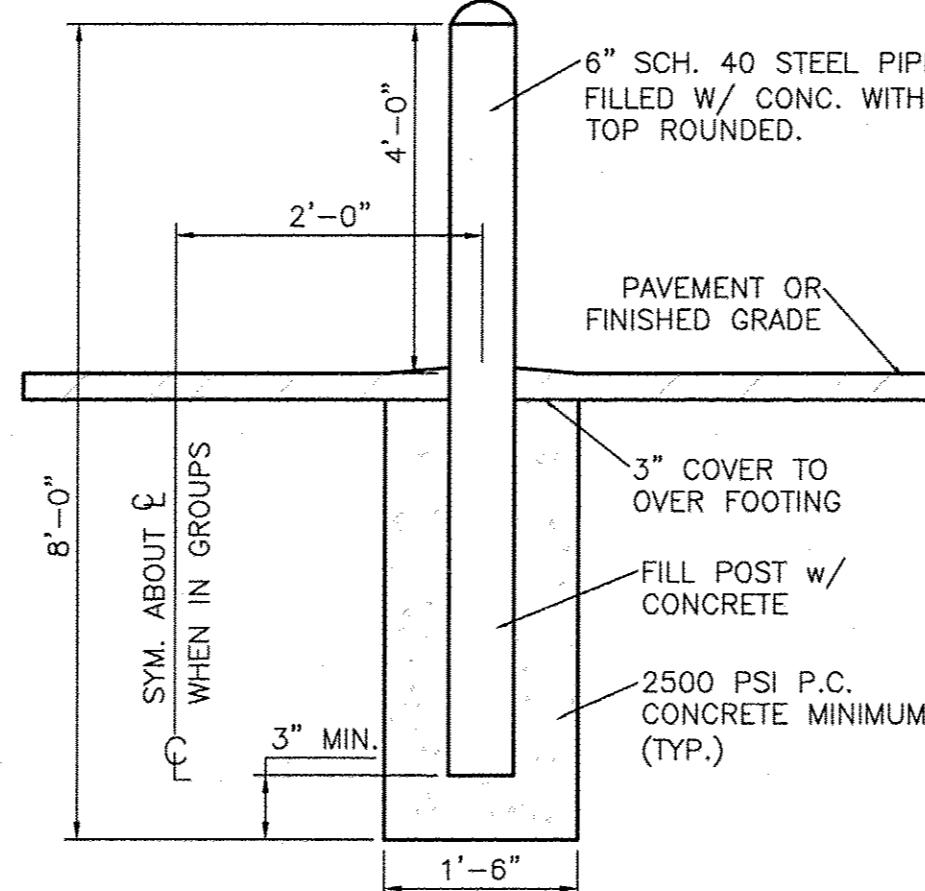


8 INCH REINFORCED CONCRETE MASONRY WALL (FOR RETAINING PORTION ONLY)

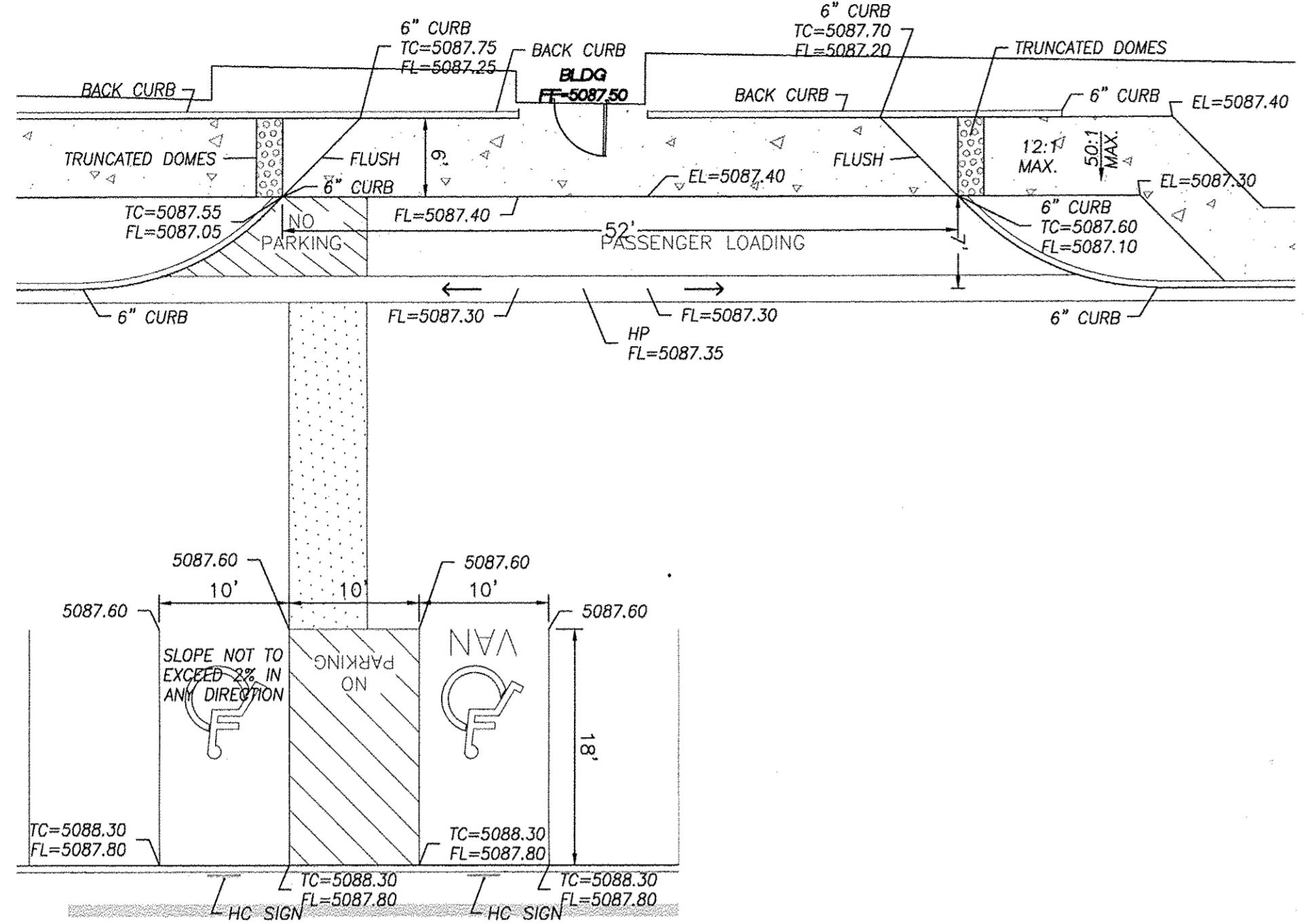
H	B	T	Y-BARS	X-BARS
ft.-in.	ft.-in.	in.		
1'-4"	1'-9"	9"	#4 @ 24" O.C.	
2'-0"	2'-0"	9"	#4 @ 24" O.C.	
2'-8"	2'-6"	9"	#4 @ 24" O.C.	
3'-4"	2'-9"	12"	#4 @ 16" O.C.	#4 @ 16" O.C.
4'-0"	3'-3"	12"	#4 @ 16" O.C.	#4 @ 16" O.C.
4'-8"	4'-0"	12"	#4 @ 16" O.C.	#4 @ 16" O.C.
5'-4"	5'-0"	12"	#4 @ 8" O.C.	#4 @ 8" O.C.
6'-0"	5'-6"	12"	#4 @ 8" O.C.	#4 @ 8" O.C.

'L' FOOTING RETAINING WALL DETAIL

NTS

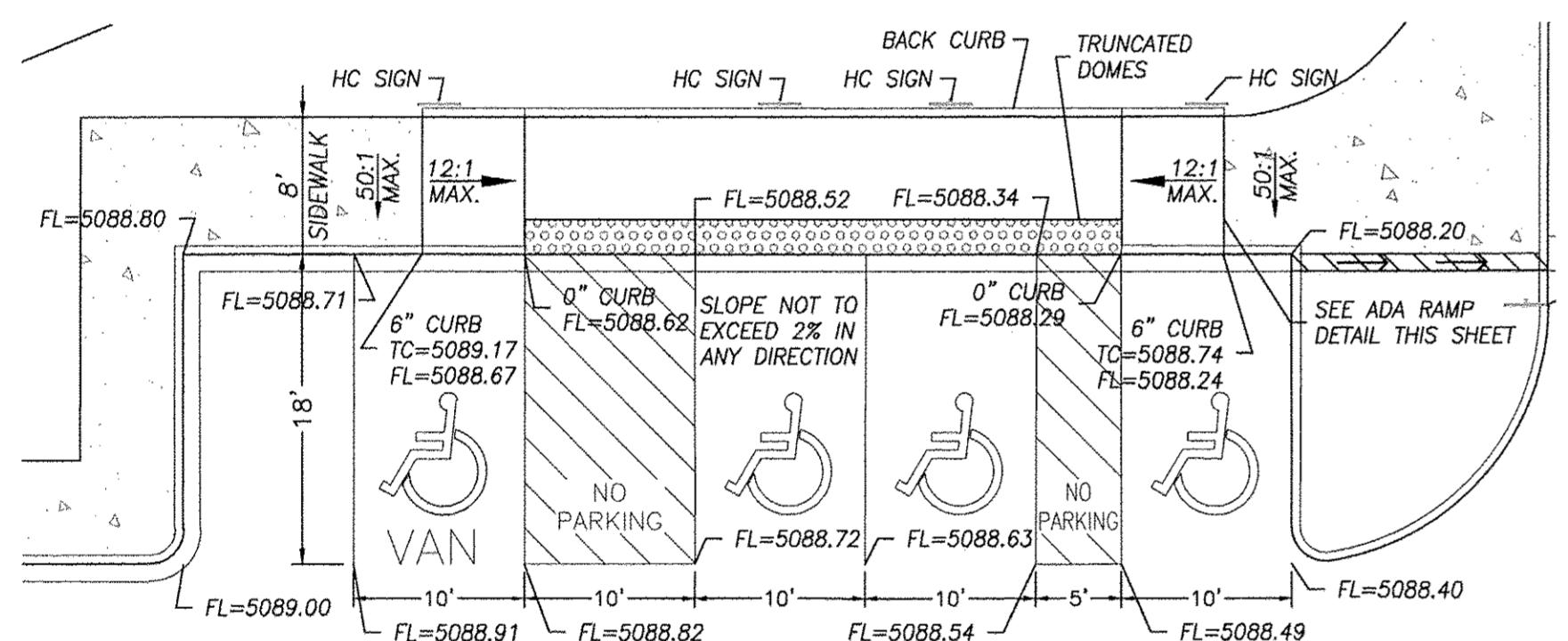


SKILLED NURSING FACILITY RENAISSANCE CENTER DETAIL SHEET		DRAWN BY DY
		DATE 4/15/16
		2014088-DTE
		SHEET #
		C5
		JOB # 2014088
		JOEL D. HERNANDEZ P.E. #17893
TERRA WEST, LLC 5571 MIDWAY PARK PLACE NE ALBUQUERQUE, NM 87109 (505) 858-3100 www.tierrawestllc.com		



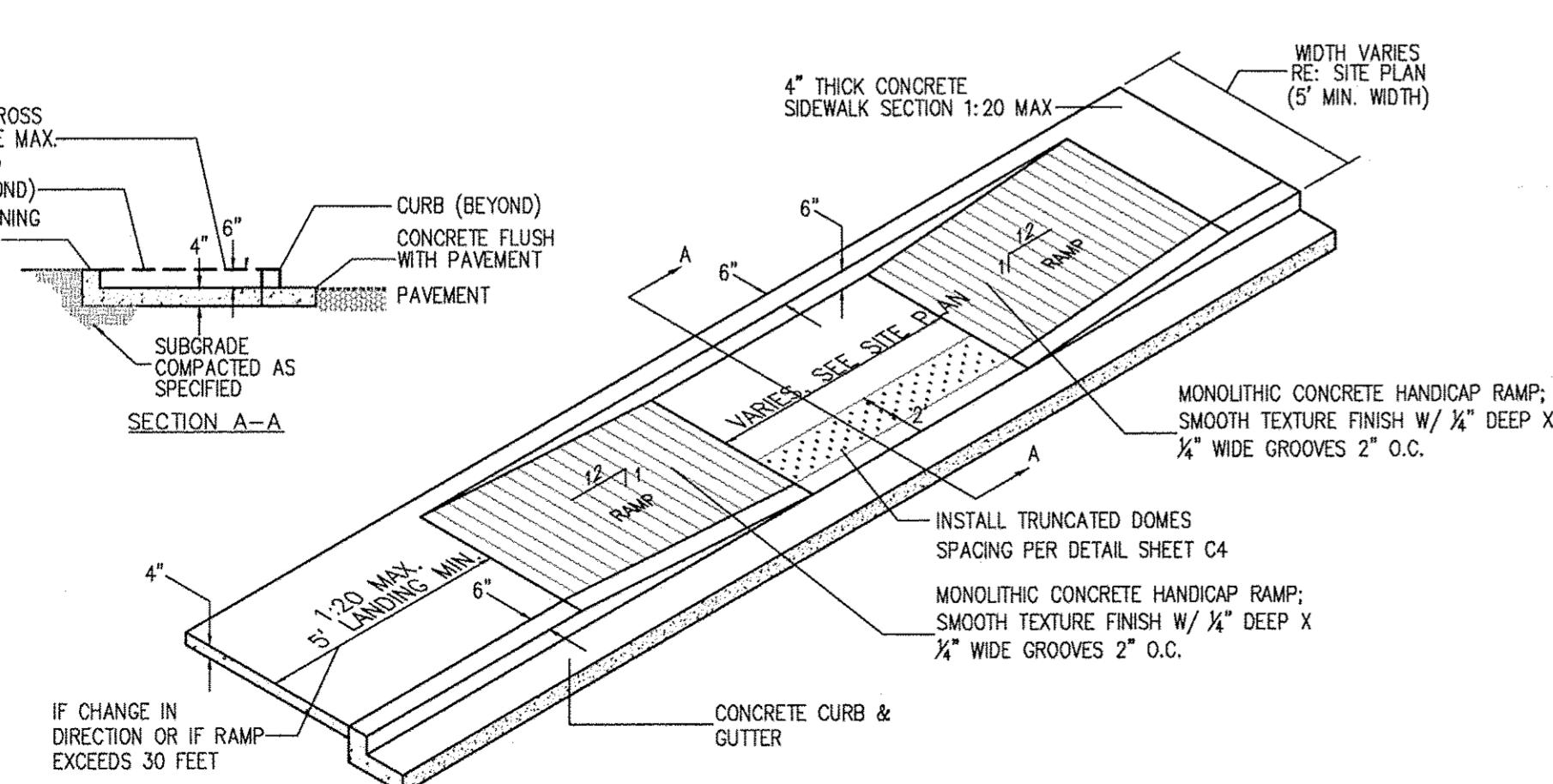
DETAIL "A"

SCALE: 1"=10'



DETAIL "C"

SCALE: 1"=10'

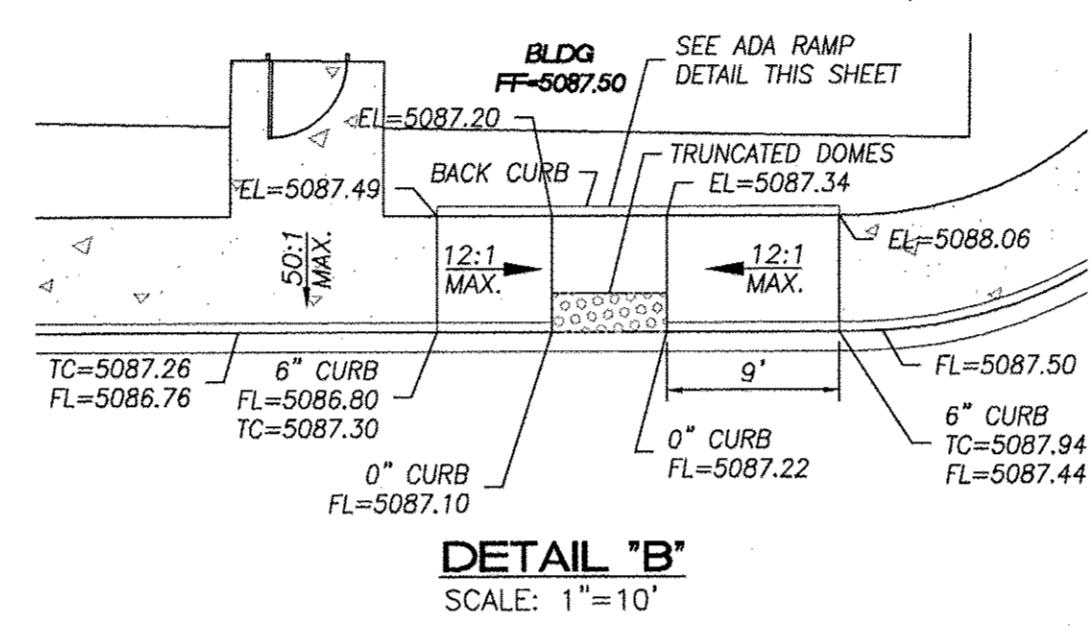


ADA RAMP DETAIL - SEE DETAIL "C" THIS SHEET
SCALE: 1"=10'

SCALE: 1" =

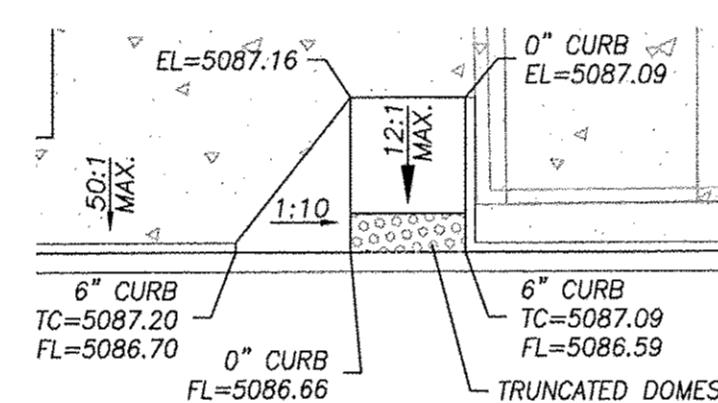
NOTES:

- 1) International Symbol of Accessibility shall be painted on the pavement at rear of space, white symbol on blue background.
- 2) Parking space lines and diagonal striping to be painted blue.
- 3) Access aisle shall have the words "NO PARKING" in capital letters, each of which shall be at least one foot high and at least two inches wide, placed at the rear of the parking space so as to be close to where an adjacent vehicle's rear tires would be placed.
- 4) See sheet C5 for HC Parking Sign Detail.



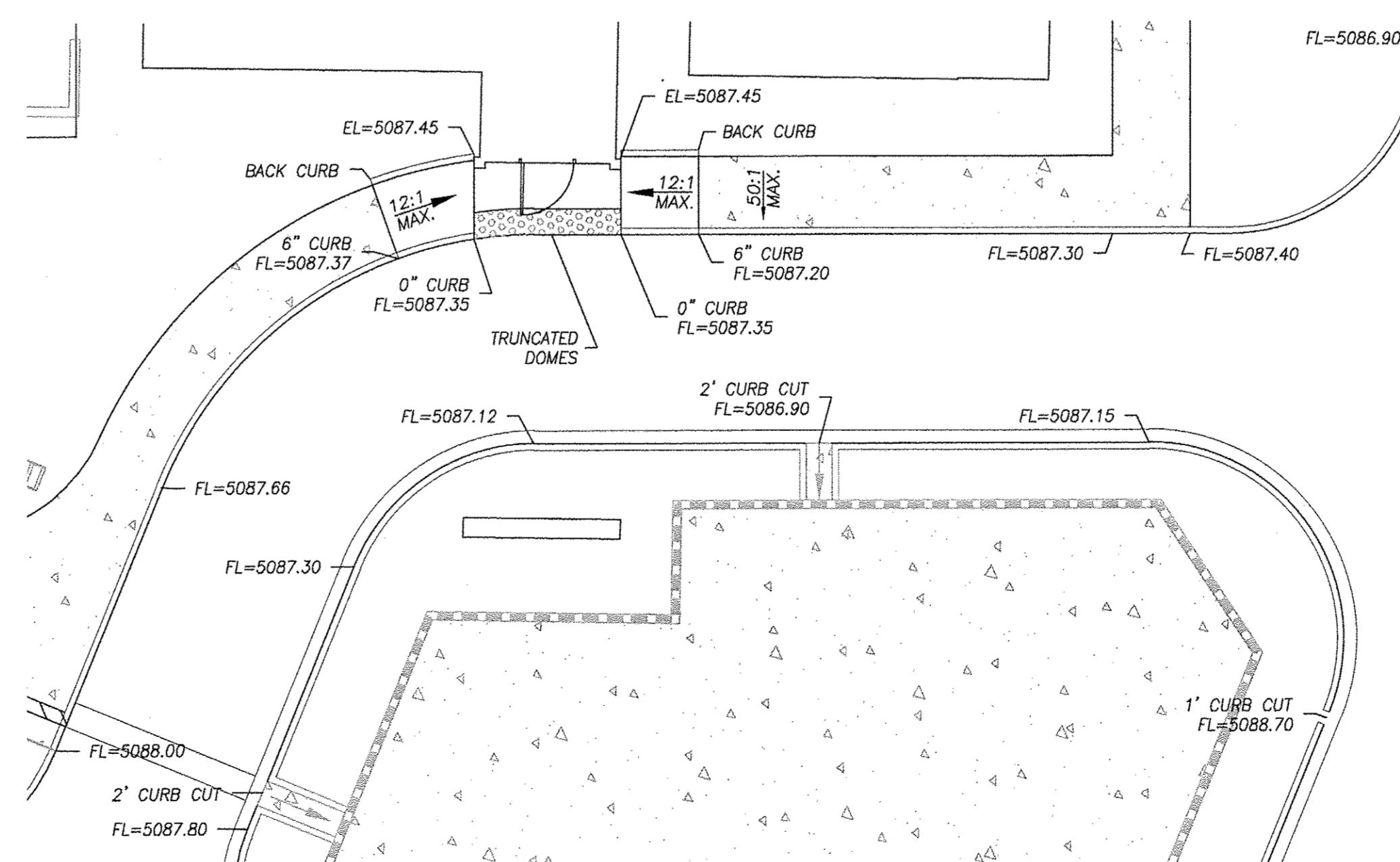
DETAIL "B"

SCALE: 1"=10'

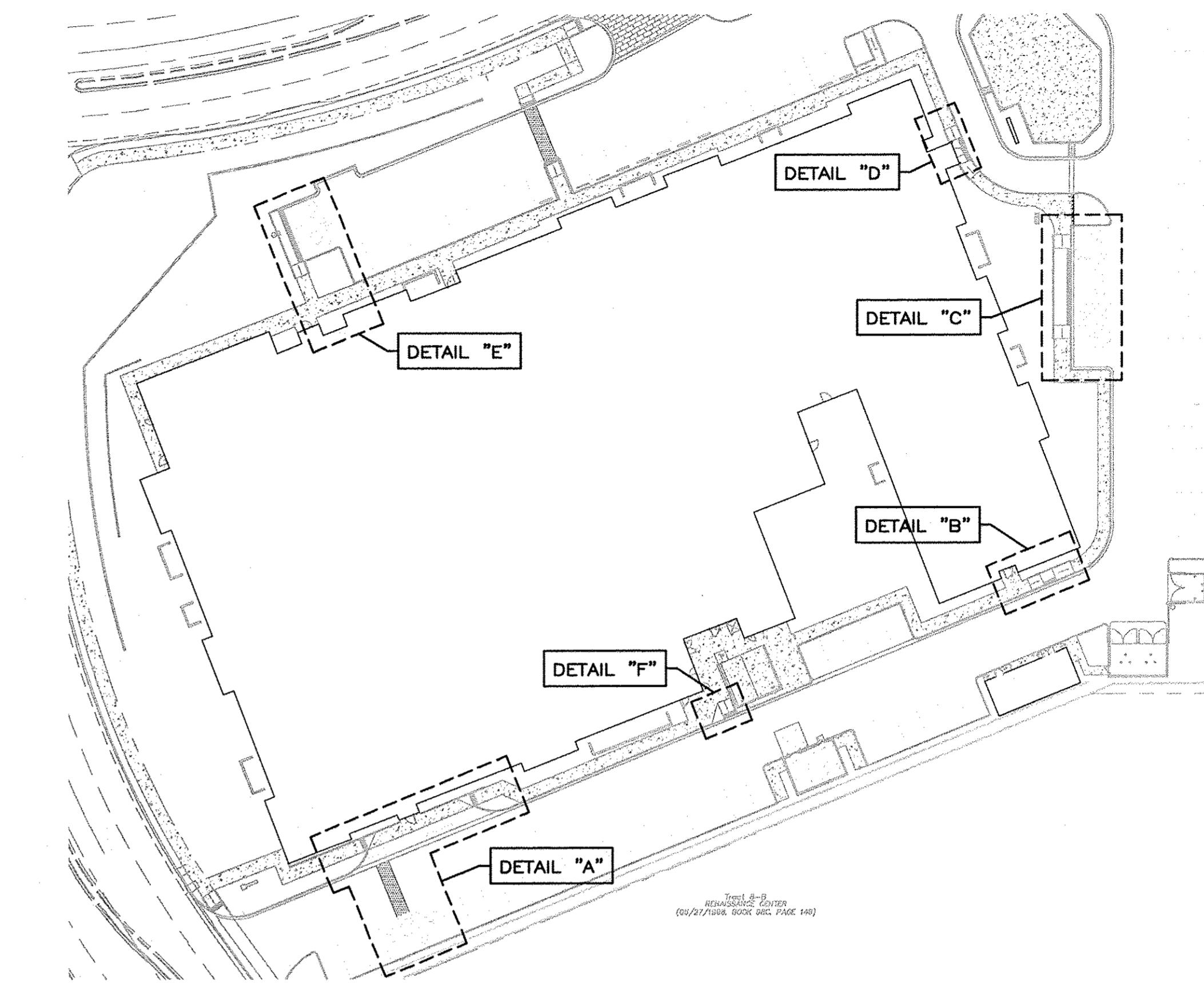


DETAIL "F"

DETAIL F

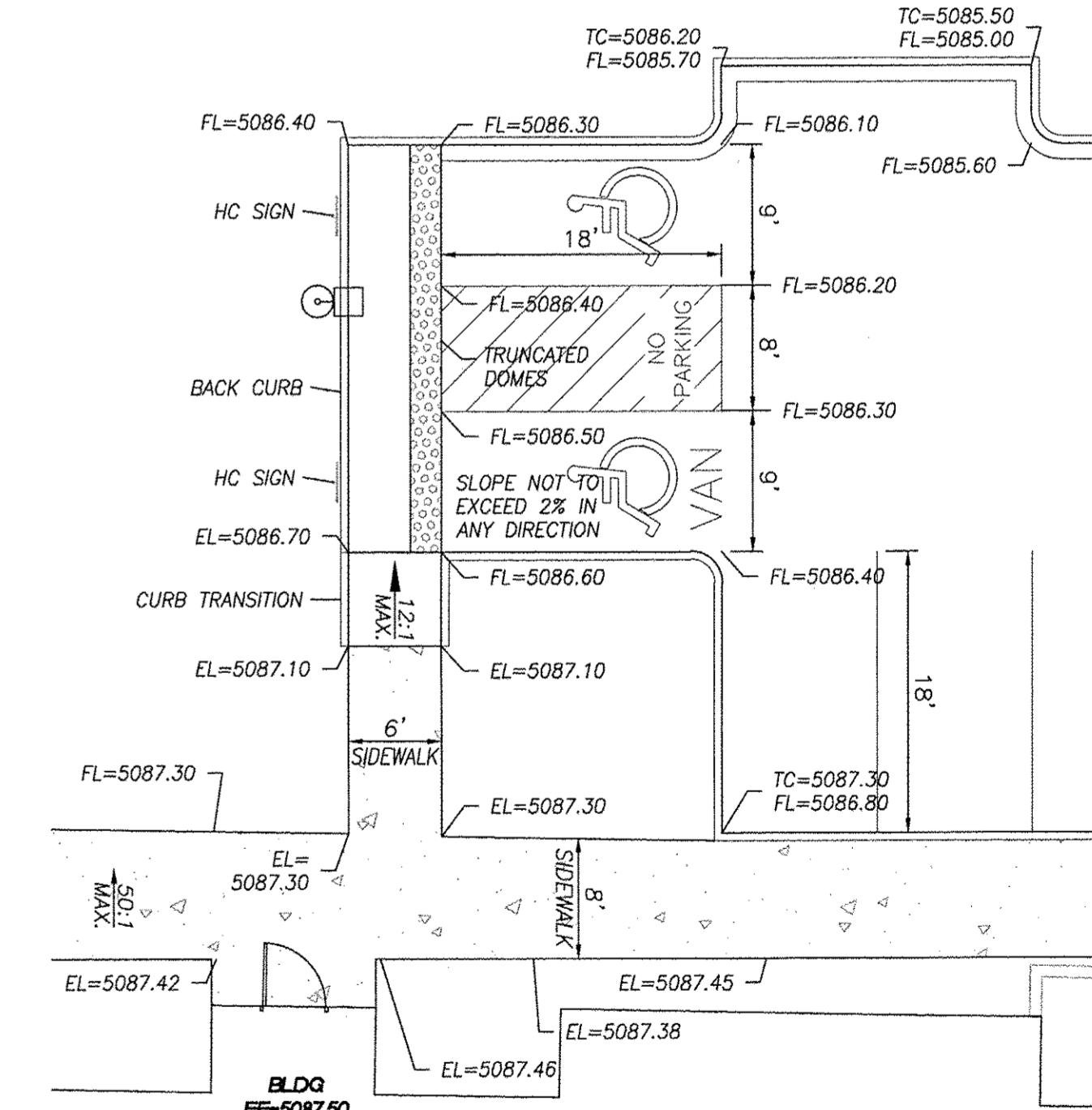


DETAIL "D"



KEY MAP FOR ADA RAMPS

SCALE: 1"=50'



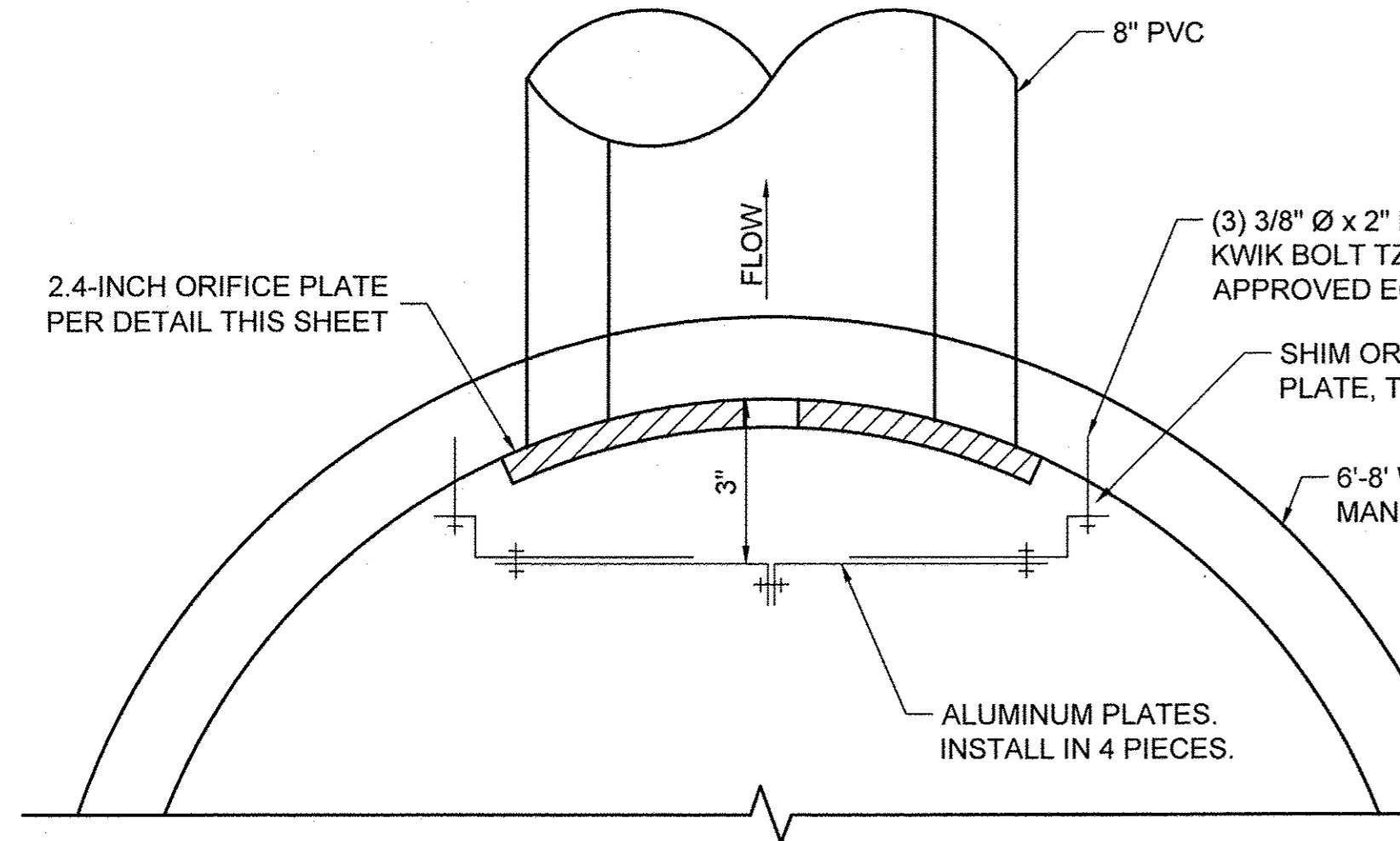
**SKILLED NURSING FACILITY
RENAISSANCE CENTER**

DETAIL SHEET

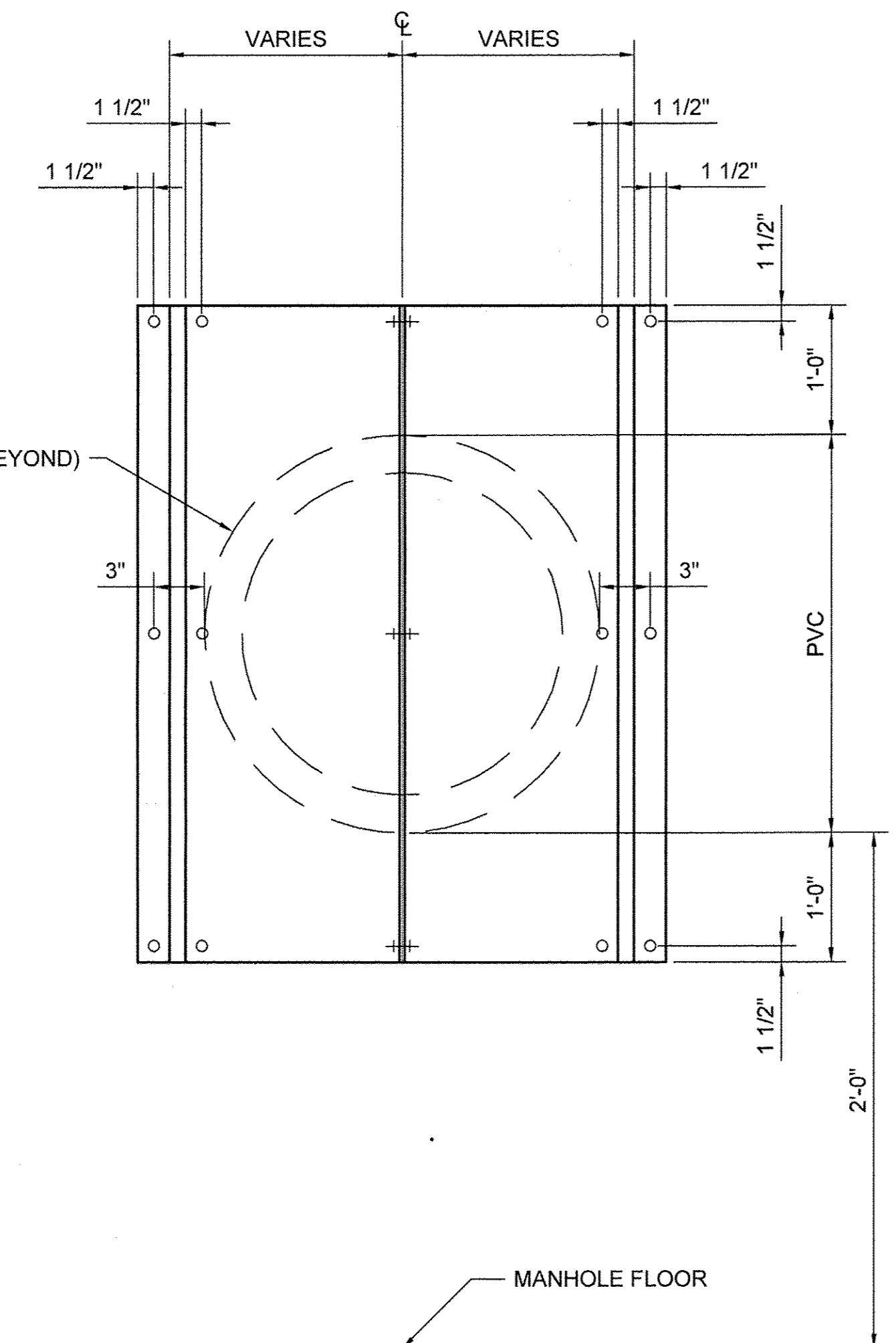
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DATE
4/08/16

2014088-DTE

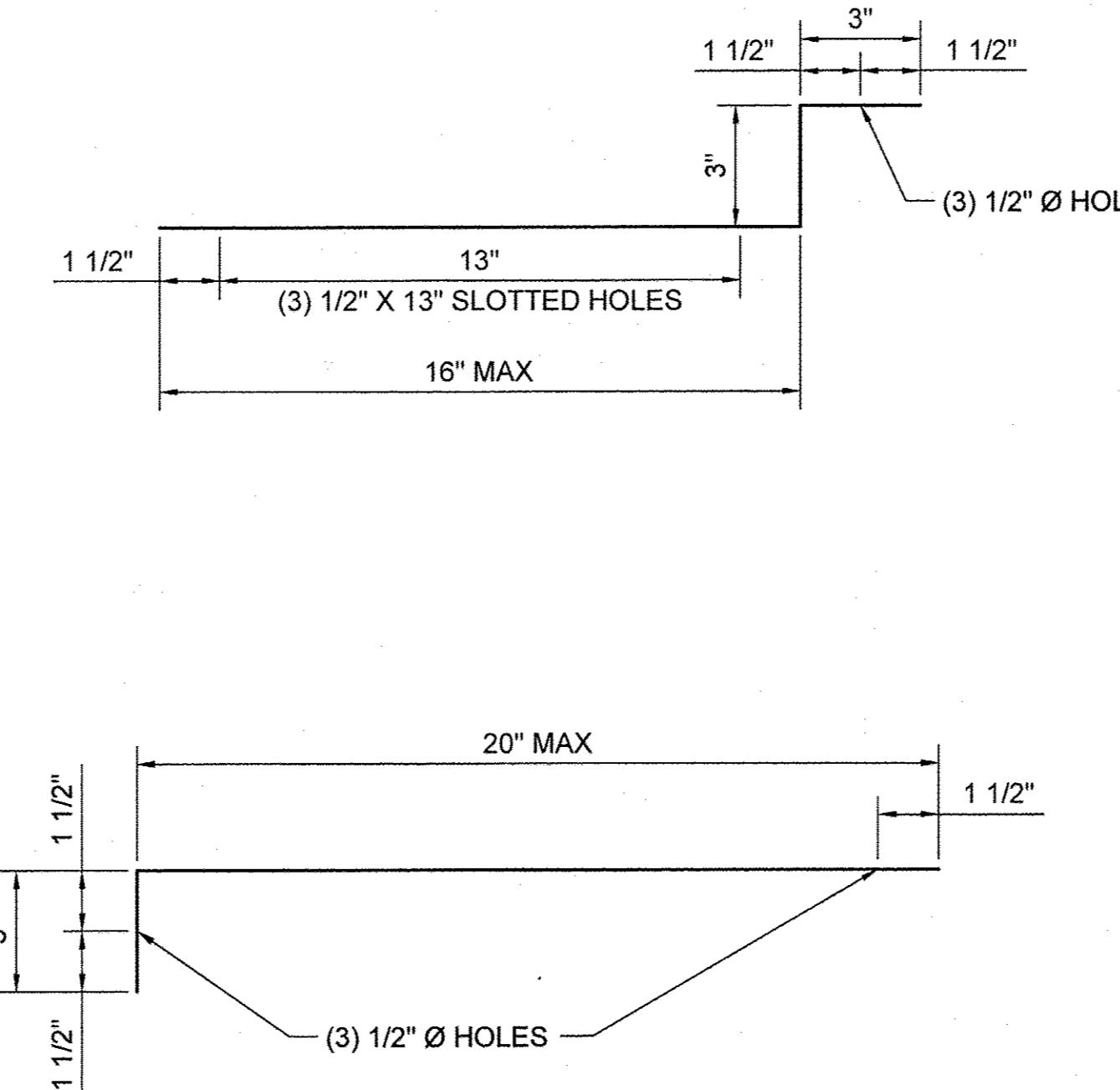
SHEET #
C6
JOB #
2014088



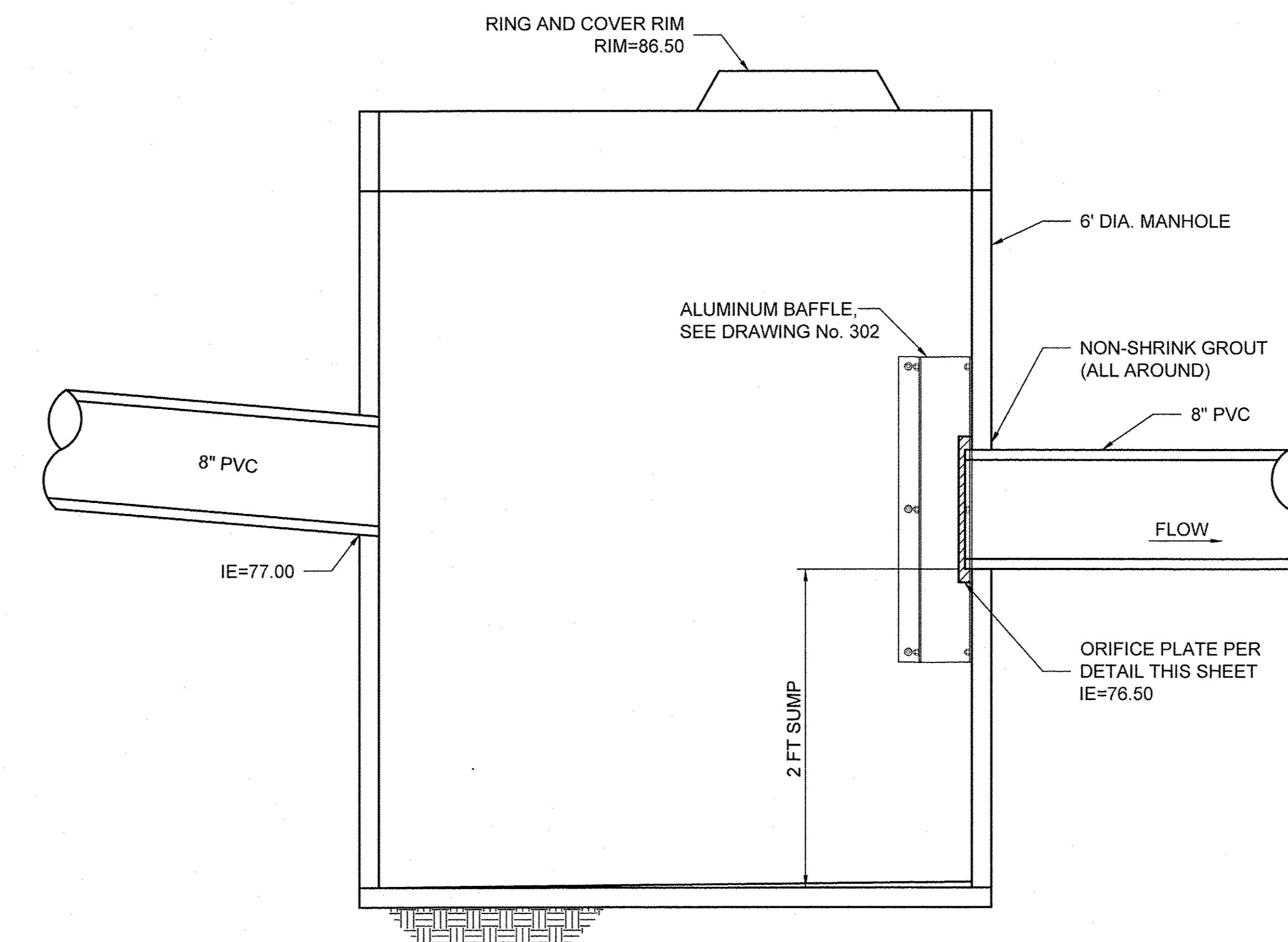
ALUMINUM BAFFLE PLAN



ALUMINUM BAFFLE ELEVATION



ALUMINUM PLATE BEND DIAGRAM



SECTION B-E



DRAINAGE REPORT

for

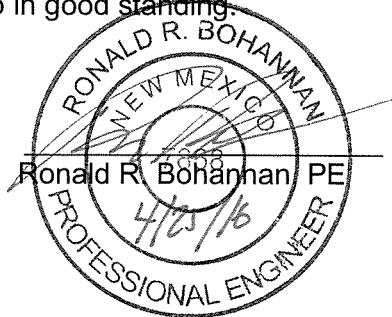
Skilled Nursing Facility 1610 Renaissance Boulevard

Prepared by:

Tierra West, LLC
5571 Midway Park Place NE
Albuquerque, New Mexico 87109

April, 2016

I certify that this report was prepared under my supervision, and I am a registered professional engineer in the State of New Mexico in good standing.



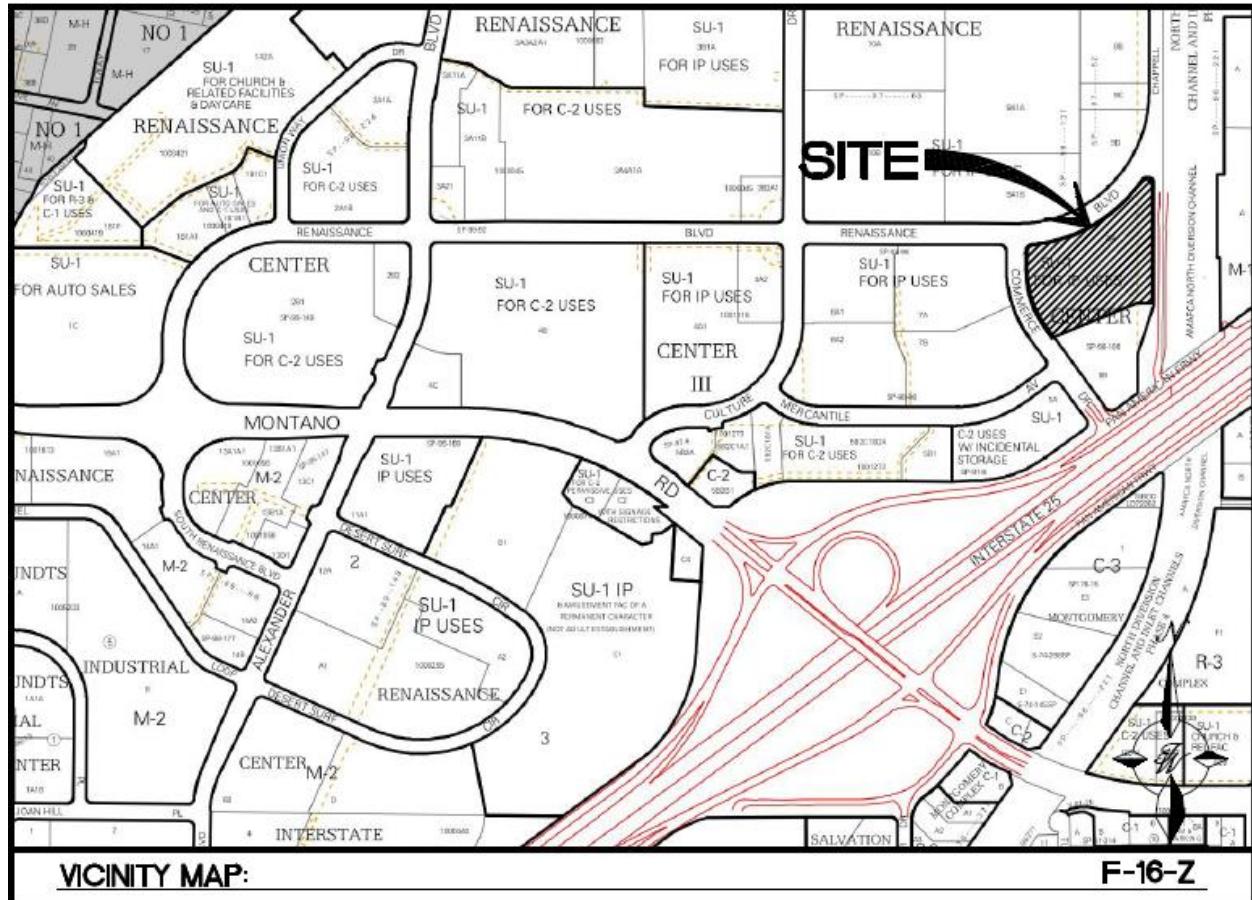
DRAINAGE MANAGEMENT PLAN

Introduction

The purpose of this drainage report is to present a drainage solution for the proposed development consisting of a single-story building for a skilled nursing facility and associated parking facility, and to document the waiver from the on-site retention of the first-flush flows. This report is a request for approval of the Grading and Drainage plan for Site Development Plan for Building Permit approval.

Project Location

The project site address is 1610 Renaissance Boulevard, NE which corresponds to Tract 8-A of the renaissance Center located on the southeast corner of Commerce Drive and Renaissance Boulevard, NE. The site is bounded by Renaissance Boulevard on the north, Commerce Drive on the west, Chappell Road on the east, and Tract 8-B to the south which is an existing hotel.

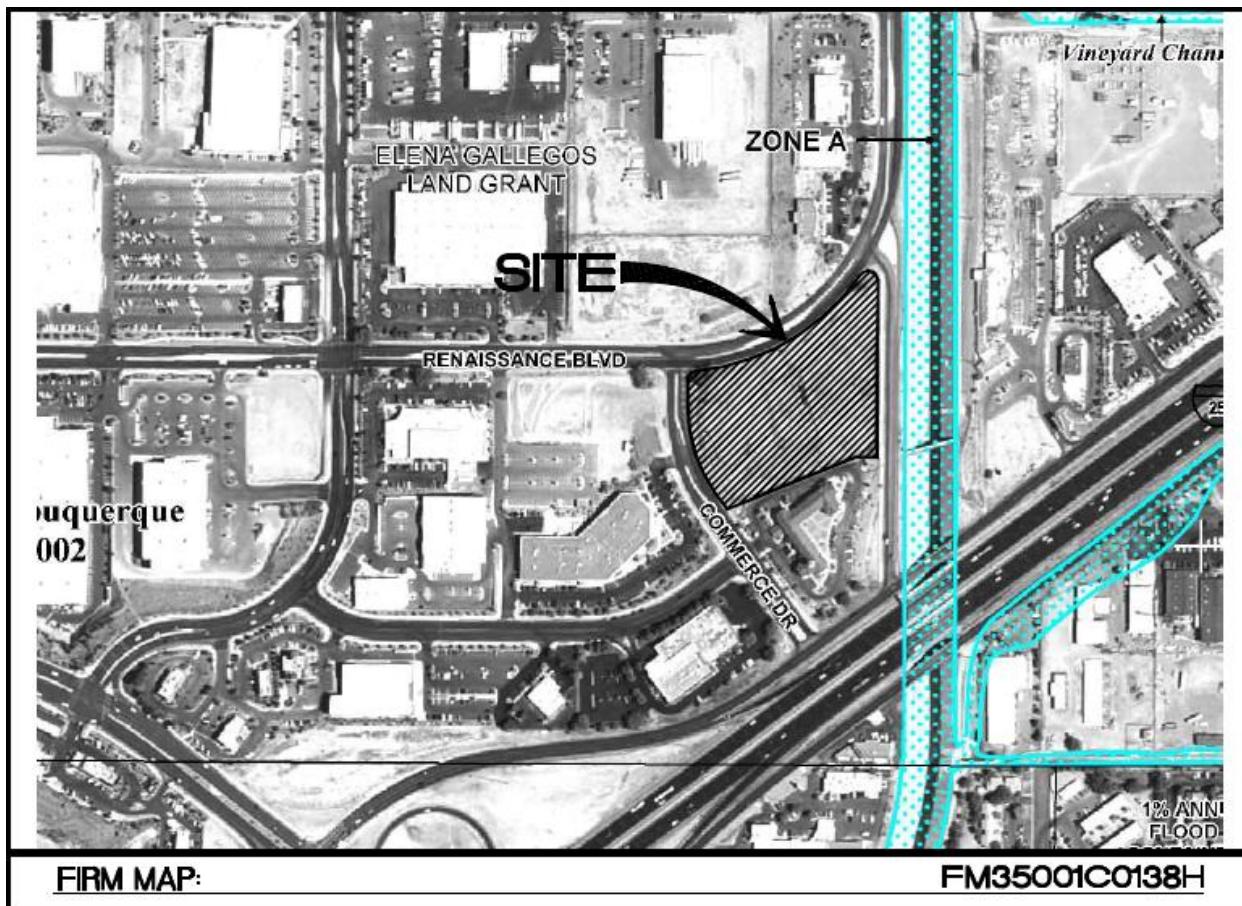


Existing Drainage Conditions

The site falls within the approved Renaissance Drainage Master Plan, and is currently undeveloped, although previously rough graded with two pads. The Renaissance Drainage Master Plan allows a controlled release runoff of 0.10 cfs per acre from each tract. The existing conditions were analyzed using the criteria set by the City of Albuquerque DPM.

Existing conditions, analyzed as a single basin with a runoff rate of 15.3 cfs., generally sheet flows from the southeast to the northwest portion of the site discharging onto Commerce Drive through a sidewalk culvert near the Renaissance Boulevard intersection. No offsite runoff enters the site.

The site is located outside any mapped 100 year floodplain, as indicated on FEMA FIRM Map 35001C0138H.



Proposed Drainage Management/Post-Developed Condition

The grading and drainage design is configured to accommodate the proposed building and associated improvements, conveying flows from the “developed” condition, while attenuating the outflow to not exceed the maximum rate of 0.5 cfs allowed by the Renaissance Drainage Master Plan for this site.

Drainage from the majority of the developed site will be collected through a network of storm drain pipes and routed through above-ground detention ponds and an underground detention storage system, such as a CMP pipe and manifold system, before releasing flows onto Commerce Drive at the existing sidewalk culvert location where the site currently flows. An area at the northeast portion of the site (Basin C1) will flow into a pond (Pond #1) which will be drained into Pond #2 through a 6-inch diameter pipe. The remaining sub-basins, with the exception of "Basin D2", are routed to Pond #2 which is interconnected with the 15,080 cubic-foot underground storage system which provides 0.6507 acre-feet of total storage available. Flow from the Pond #2 combined system is slowly released through a 2.4-inch orifice plate to the sidewalk culvert outfall. Flow from Pond #3, which accommodates flow from "Basin D2", is drained through a 4-inch pipe with a 1.4-inch orifice plate and connected to the outflow pipe from Pond #2 near the sidewalk culvert outfall.

A hydrologic analysis was performed using AHYMO to determine the flows generated by the 100-year storm in the developed condition, as well as to determine the maximum system outflow rate after routing through the onsite detention system. A drainage basin map, schematic of the system, pond volume storage tabulations, stage-discharge calculations, and the AHYMO input and output data are included in Appendix A.

The storm drain system is sized to accommodate the developed flows from the site, including the roof drains and patio areas internal to the building. Water quality manholes to minimize sediment and debris from entering the underground detention system will be constructed using a Bio Snout, EnviroHood, or equal. Hydraulic calculations for inlets, storm drain pipes, and concrete flume capacities are included in Appendix B along with a storm drain schematic exhibit.

Water Quality Management

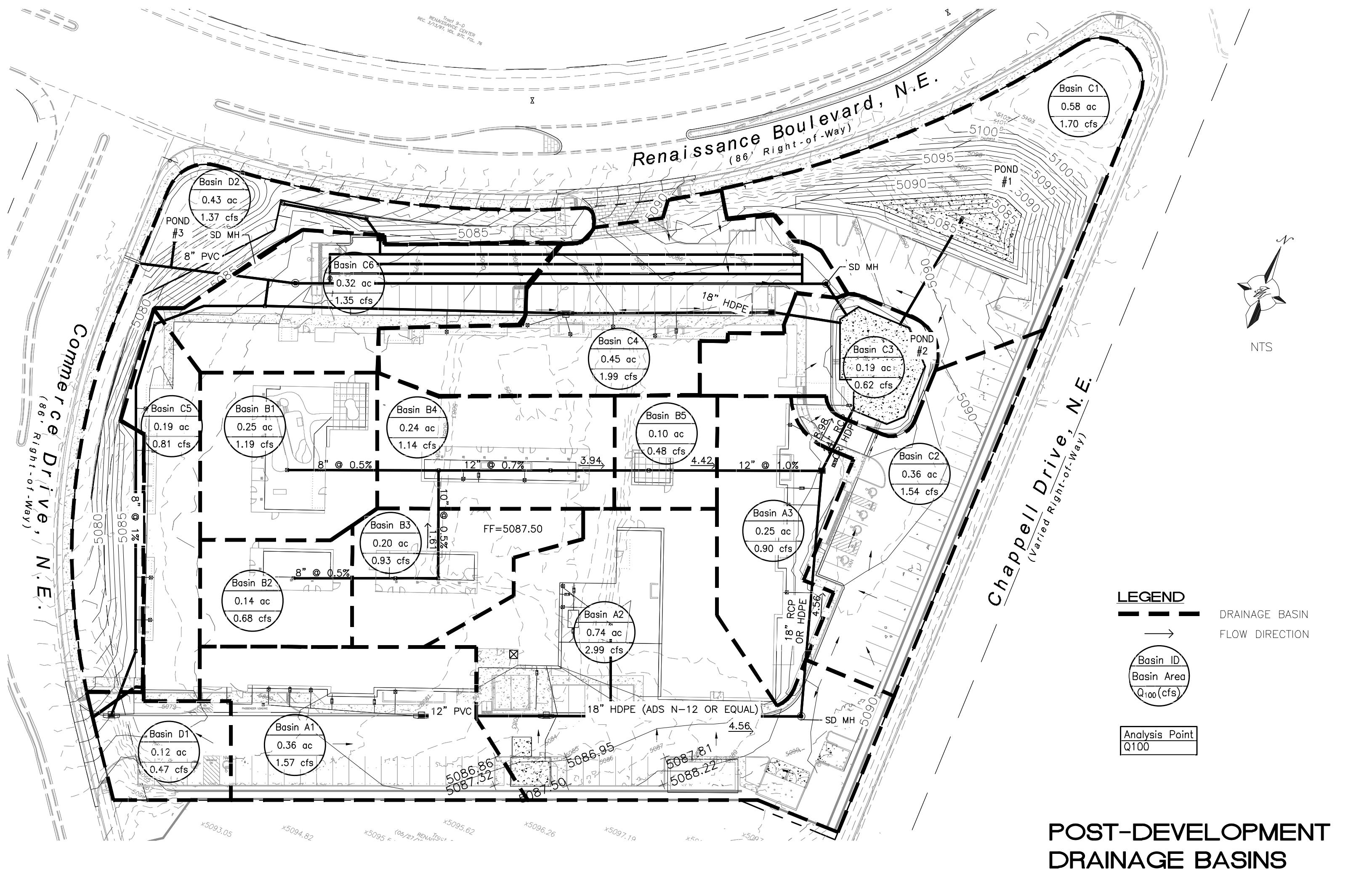
Given the potential for collapsible soils onsite, a waiver for onsite retention of the first-flush has been requested with this project. BMP's consisting of water quality manholes, as described above, will be implemented on-site to reduce the pollutants entering the underground detention system and the site, however, on-site retention of the first-flush volume is not feasible due to the geotechnical conditions and recommendations from the Geotechnical Investigation Report. It should also be noted that drainage from this area is conveyed to a regional pond which provides a disconnect from the Rio Grande.

Conclusion

This Drainage Management Plan provides for grading and drainage elements which are capable of safely conveying the 100-year, 6-hour storm and which meet the City requirements, as well as meeting the requirements of the Renaissance Center Master Drainage Plan. With this submittal we request Drainage Report and Grading Plan approvals for the Site Plan for Building Permit Application.

APPENDIX A

HYDROLOGY





TIERRA WEST, LLC

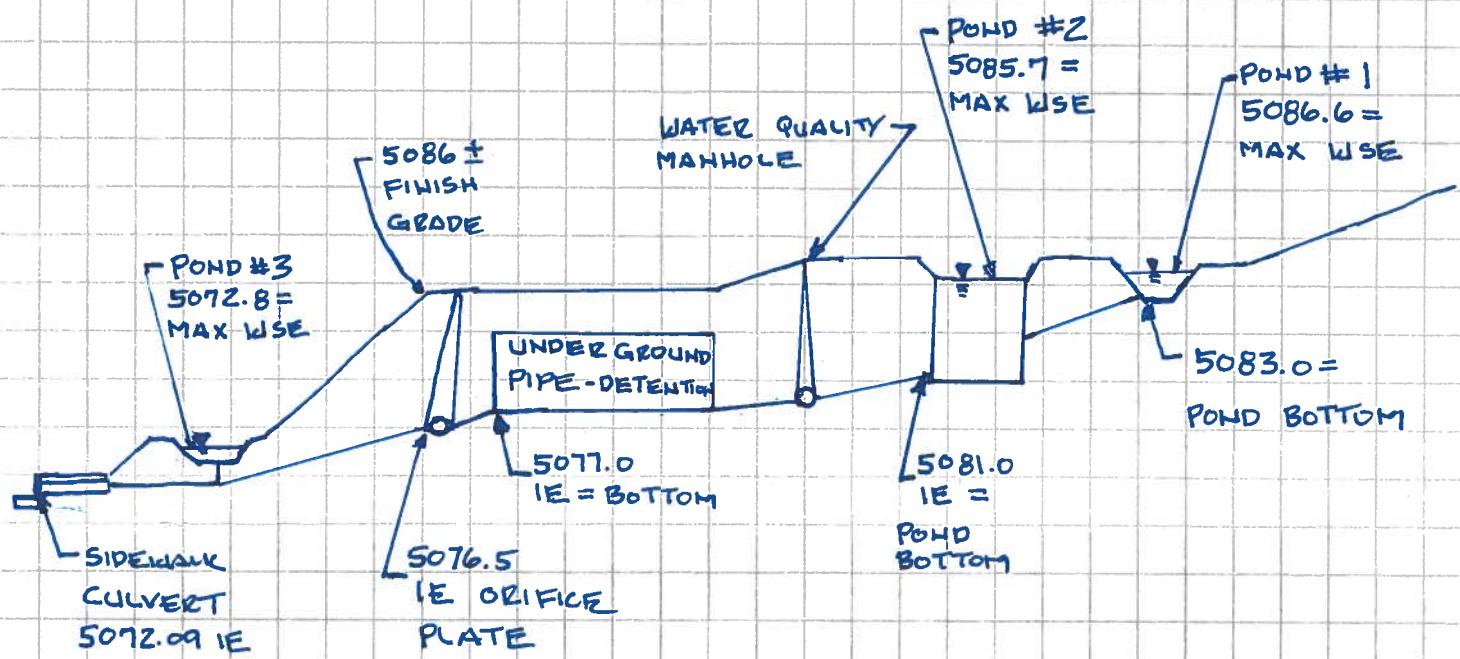
Project SKILLED NURSING Date _____

Project No. 2014088

Meeting Purpose _____ Sheet No. _____ of _____

Attendees _____

DETENTION POND SYSTEM SCHEMATIC





TIERRA WEST, LLC

Project SKILLED NURSING Date _____

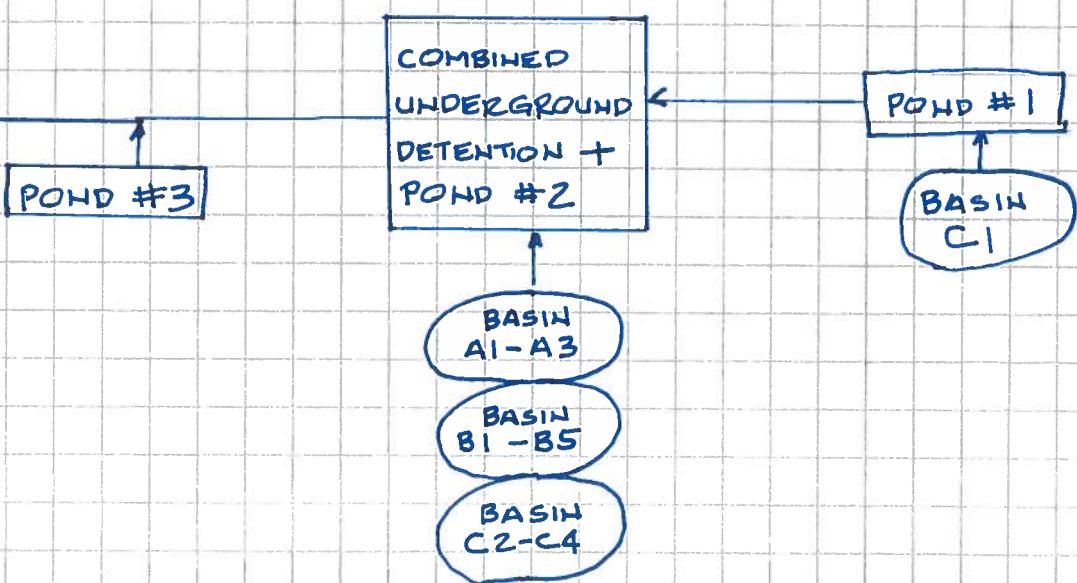
Project No. 2014088

Meeting Purpose _____ Sheet No. ____ of ____

Attendees _____

A HYMO ROUTING SCHEMATIC

MAX OUTFLOW
0.5 CFS



Tract 8A, RENAISSANCE CENTER

Existing and Proposed Conditions Basin Data Table

This table is based on the DPM Section 22.2, Zone: 2

BASIN	Area (SQ. FT)	Area (AC.)	Land Treatment Percentages				Q(100) (cfs/ac.)	Q(100) (CFS)	V(100) (inches)	V(100) (CF)
			A	B	C	D				
EXISTING CONDITIONS										
A	212000	4.87	0.0%	0.0%	99.0%	1.0%	3.16	15.36	1.14	20138
TOTAL		4.87						15.36	1.14	20138

Per the Renaissance Center Master Drainage Plan,
the Maximum Release from the Site is 0.10 cfs/acre.

This table is based on the DPM Section 22.2, Zone: 2

BASIN	Area (SQ. FT)	Area (AC.)	Land Treatment Percentages				Q(100) (cfs/ac.)	Q(100) (CFS)	V(100) (inches)	V(100) (CF)	1ST FLUSH	Area (SQ. MI)
	A	B	C	D								
PROPOSED CONDITIONS												
A1	15,835	0.36	0.0%	16.0%	0.0%	84.0%	4.31	1.57	1.91	2515	377	0.00057
A2	32,146	0.74	0.0%	27.0%	0.0%	73.0%	4.05	2.99	1.76	4710	665	0.00115
A3	10,825	0.25	0.0%	45.0%	0.0%	55.0%	3.61	0.90	1.52	1368	169	0.00039
B1	11,054	0.25	0.0%	0.0%	0.0%	100.0%	4.70	1.19	2.12	1953	313	0.00040
B2	6,271	0.14	0.0%	0.0%	0.0%	100.0%	4.70	0.68	2.12	1108	178	0.00022
B3	8,635	0.20	0.0%	0.0%	0.0%	100.0%	4.70	0.93	2.12	1526	245	0.00031
B4	10,545	0.24	0.0%	0.0%	0.0%	100.0%	4.70	1.14	2.12	1863	299	0.00038
B5	4,438	0.10	0.0%	0.0%	0.0%	100.0%	4.70	0.48	2.12	784	126	0.00016
C1	25,404	0.58	15.0%	54.0%	0.0%	31.0%	2.92	1.70	1.16	2451	223	0.00091
C2	15,594	0.36	0.0%	17.0%	0.0%	83.0%	4.29	1.54	1.89	2459	367	0.00056
C3	8,250	0.19	0.0%	20.0%	0.0%	80.0%	4.22	0.80	1.85	1273	187	0.00030
C4	19,802	0.45	0.0%	13.0%	0.0%	87.0%	4.39	1.99	1.95	3211	488	0.00071
C5	8,223	0.19	0.0%	17.0%	0.0%	83.0%	4.29	0.81	1.89	1297	193	0.00029
C6	14,016	0.32	0.0%	21.0%	0.0%	79.0%	4.19	1.35	1.84	2147	314	0.00050
D1	5,118	0.12	0.0%	30.0%	0.0%	70.0%	3.97	0.47	1.72	733	102	0.00018
D2	18,666	0.43	0.0%	0.0%	97.0%	3.0%	3.19	1.37	1.16	1804	16	0.00067
TOTAL		4.93						19.89	1.91	31201	4260	

DETENTION VOLUME CALCS

POND NO.1 (BASIN C1 ONLY) VOLUME CALCULATIONS

ELEVATION (ft)	AREA (sf)	VOLUME (cf)	CUMULATIVE VOLUME (cf)	CUMULATIVE VOLUME (ac-ft)
5083	216	0	0	0.0000
5084	500	358	358	0.0082
5085	902	701	1059	0.0243
5086	1423	1162.5	2222	0.0510
5087	2088	1755.5	3977	0.0913
5088	2936	2512	6489	0.1490

POND 2 + UNDERGROUND STORAGE VOLUME CALCULATION

PIPE DIA= 48	PIPE L= 1,040			
ELEVATION (ft)	AREA (sf)	VOLUME (cf)	CUMULATIVE VOLUME (cf)	CUMULATIVE VOLUME (ac-ft)
5077.0	0	0	0	0.0217
5077.5	0.91	946.4	946.4	0.0587
5078.0	2.46	2558.4	2558.4	0.1027
5078.5	4.3	4472	4472	0.1499
5079.0	6.28	6531.2	6531.2	0.1972
5079.5	8.26	8590.4	8590.4	0.2414
5080.0	10.11	10514.4	10514.4	0.2784
5080.5	11.66	12126.4	12126.4	0.3000
5081.0	12.57	13069	13069	0.3609
5082.0	2653	2653	15722	0.4218
5083.0	2653	2653	18375	0.4827
5084.0	2653	2653	21028	0.5436
5085.0	2653	2653	23681	0.6045
5086.0	2653	2653	26334	

POND 3 (BASIN D2 ONLY) VOLUME CALCULATIONS

ELEVATION (ft)	AREA (sf)	VOLUME (cf)	CUMULATIVE VOLUME (cf)	CUMULATIVE VOLUME (ac-ft)
5072	1426	0	0	0.0000
5073	1998	1712	1712	0.0393

STAGE-DISCHARGE CALCULATIONS

DETENTION POND #1

STAGE, VOLUME, DISCHARGE

Orifice Elevation: 5083.0

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
5083	0	0	0.0000
5084	1.00	0.0082	0.1554
5085	2.00	0.0243	0.2260
5086	3.00	0.0510	0.2793
5087	4.00	0.0913	0.3240
5088	5.00	0.1490	0.3632

Orifice Equation

$$Q = CA \sqrt{2gH}$$

$$C = 0.6$$

$$\text{Diameter } (i) = 2.5$$

$$\text{Area } (ft^2) = 0.034$$

$$g = 32.2$$

H (Ft) = Depth of water above center of orifice

Q (CFS) = Flow

STAGE-DISCHARGE CALCULATIONS

DETENTION POND NO. 2 COMBINED WITH UNDERGROUND STORAGE

STAGE, VOLUME, DISCHARGE

Orifice Elevation: 5076.5

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
5077.0	0.50	0	0.0957
5077.5	1.00	0.0217	0.1435
5078.0	1.50	0.0587	0.1790
5078.5	2.00	0.1027	0.2085
5079.0	2.50	0.1499	0.2343
5079.5	3.00	0.1972	0.2576
5080.0	3.50	0.2414	0.2789
5080.5	4.00	0.2784	0.2987
5081.0	4.50	0.3000	0.3173
5082.0	5.50	0.3609	0.3515
5083.0	6.50	0.4218	0.3827
5084.0	7.50	0.4827	0.4115
5085.0	8.50	0.5436	0.4384
5086.0	9.50	0.6045	0.4638

Orifice Equation

$$Q = CA \sqrt{2gH}$$

$$C = 0.6$$

$$\text{Diameter } (i) = 2.4$$

$$\text{Area } (ft^2) = 0.031$$

$$g = 32.2$$

H (Ft) = Depth of water above center of orifice

Q (CFS) = Flow

STAGE-DISCHARGE CALCULATIONS

DETENTION POND #3

STAGE, VOLUME, DISCHARGE

Orifice Elevation: 5072.0

Orifice Equation

$$Q = CA \sqrt{2gH}$$

C = 0.6

Diameter (in) 1.4

Area (ft²)= 0.011

g = 32.2

H (Ft) = Depth of water above center of orifice

Q (CFS)= Flow

Skilled Nursing COMBINED final

 * Skilled Nursing Renaissance, ABQ,NM *

 * 100-YEAR, 24-HR STORM (UNDER PROPOSED CONDITIONS) W/ routing *

 *
 START TIME=0.0
 *
 *
 RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 RAIN ONE=2.01 IN RAIN SIX=2.35 IN
 RAIN DAY=2.75 IN DT=0.05 HR
 *DEVELOPED CONDITIONS
 *
 *BASIN A1
 *
 COMPUTE NM HYD ID=1 HYD NO=100.1 AREA=0.00057 SQ MI
 PER A=0.00 PER B=16.0 PER C=0.00 PER D=84.00
 TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD ID=1 CODE=1
 *
 *
 *BASIN A2
 *
 COMPUTE NM HYD ID=2 HYD NO=100.2 AREA=0.00115 SQ MI
 PER A=0.00 PER B=27.0 PER C=0.00 PER D=73.00
 TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD ID=2 CODE=1
 *
 *
 *BASIN A3
 *
 COMPUTE NM HYD ID=3 HYD NO=100.3 AREA=0.00039 SQ MI
 PER A=0.00 PER B=45.0 PER C=0.00 PER D=55.00
 TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD ID=3 CODE=1
 *
 *
 *BASIN B1-B5
 *
 COMPUTE NM HYD ID=4 HYD NO=100.4 AREA=0.00147 SQ MI
 PER A=0.00 PER B=0.00 PER C=0.00 PER D=100.0
 TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD ID=4 CODE=1
 *
 *
 *BASIN C2
 *

COMPUTE NM HYD Skilled Nursing COMBINED final
 ID=5 HYD NO=100.5 AREA=0.00056 SQ MI
 PER A=0.00 PER B=17.0 PER C=0.0 PER D=83.00
 TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD ID=5 CODE=1
 *
 *
 *BASIN C3
 COMPUTE NM HYD ID=6 HYD NO=100.6 AREA=0.00030 SQ MI
 PER A=0.00 PER B=20.0 PER C=0.0 PER D=80.00
 TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD ID=6 CODE=1
 *
 *
 *BASIN C4
 *
 COMPUTE NM HYD ID=7 HYD NO=100.7 AREA=0.00071 SQ MI
 PER A=0.00 PER B=13.0 PER C=0.0 PER D=87.00
 TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD ID=7 CODE=1
 *
 *
 *BASIN C1
 *
 COMPUTE NM HYD ID=8 HYD NO=100.8 AREA=0.00091 SQ MI
 PER A=15.0 PER B=54.0 PER C=0.0 PER D=31.00
 TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD ID=8 CODE=1
 **
 *ROUTE BASIN C1 THROUGH DETENTION POND NO.1
 ROUTE RESERVOIR ID=55 HYD NO=200.1 INFLOW ID=8 CODE=24
 OUTFLOW (CFS) STORAGE(AC-FT) ELEVATION(FT)
 0.1000 0.0 83.00
 0.1554 0.0082 84.00
 0.2260 0.0243 85.00
 0.2793 0.0510 86.00
 0.3240 0.0913 87.00
 0.3632 0.1490 88.00
 *
 PRINT HYD ID=55 CODE=1
 *
 *
 *BASIN C6
 *
 COMPUTE NM HYD ID=9 HYD NO=100.9 AREA=0.00050 SQ MI
 PER A=0.00 PER B=21.0 PER C=0.0 PER D=79.0
 TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD ID=9 CODE=1
 *

Skilled Nursing COMBINED final

*

*BASIN C5

*

COMPUTE NM HYD ID=10 HYD NO=100.10 AREA=0.00029 SQ MI
PER A=0.00 PER B=17.0 PER C=0.0 PER D=83.0
TP=-0.1333 HR MASS RAINFALL=-1

PRINT HYD ID=10 CODE=1

*

*

*BASIN D1

*

COMPUTE NM HYD ID=11 HYD NO=100.11 AREA=0.00018 SQ MI
PER A=0.00 PER B=30.0 PER C=0.0 PER D=70.00
TP=-0.1333 HR MASS RAINFALL=-1

PRINT HYD ID=11 CODE=1

*

*

*COMBINE POND1 DISCHARGE WITH BASINS ROUTED TO POND NO.2

*

ADD HYD ID=50 HYD NO=100.21 ID=1 ID=2
ADD HYD ID=50 HYD NO=100.21 ID=50 ID=3
ADD HYD ID=50 HYD NO=100.21 ID=50 ID=4
ADD HYD ID=50 HYD NO=100.21 ID=50 ID=5
ADD HYD ID=50 HYD NO=100.21 ID=50 ID=6
ADD HYD ID=50 HYD NO=100.21 ID=50 ID=7
ADD HYD ID=50 HYD NO=100.21 ID=50 ID=9
ADD HYD ID=50 HYD NO=100.21 ID=50 ID=10
ADD HYD ID=50 HYD NO=100.21 ID=50 ID=11
ADD HYD ID=50 HYD NO=100.21 ID=50 ID=55

*

PRINT HYD ID=50 CODE=1

*

*ROUTE POND1 DISCHARGE & BASINS A1-3,B1-5,C2-6,D1 THRU COMBINED UG/POND 2 DETENTION SYSTEM

ROUTE RESERVOIR ID=56 HYD NO=200.3 INFLOW ID=50 CODE=24
OUTFLOW (CFS) STORAGE(AC-FT) ELEVATION(FT)

0.0957	0.0000	77.00
0.1435	0.0217	77.50
0.1790	0.0587	78.00
0.2085	0.1027	78.50
0.2343	0.1499	79.00
0.2576	0.1972	79.50
0.2789	0.2414	80.00
0.2987	0.2784	80.50
0.3173	0.3000	81.00
0.3515	0.3609	82.00
0.3827	0.4218	83.00
0.4115	0.4827	84.00

Skilled Nursing COMBINED final

0.4384	0.5436	85.00
0.4638	0.6045	86.00

*

PRINT HYD ID=56 CODE=1

*

*BASIN D2

*

COMPUTE NM HYD ID=12 HYD NO=100.12 AREA=0.00067 SQ MI
PER A=0.00 PER B=97.0 PER C=0.0 PER D=3.00
TP=-0.1333 HR MASS RAINFALL=-1

PRINT HYD ID=12 CODE=1

*

*

*ROUTE BASIN D2 THROUGH POND NO 3

ROUTE RESERVOIR ID=57 HYD NO=200.3 INFLOW ID=12 CODE=24
OUTFLOW (CFS) STORAGE(AC-FT) ELEVATION(FT)
0.0100 0.0000 72.00
0.0500 0.0393 73.00

*

PRINT HYD ID=57 CODE=1

*

ADD HYD ID=58 HYD NO=100.22 ID=56 ID=57

*

PRINT HYD ID=58 CODE=1

*

*

FINISH

AHYMO

AHYMO PROGRAM (AHYMO-S4) - Version: S4.01a - Rel: 01a
 RUN DATE (MON/DAY/YR) = 05/05/2016
 START TIME (HR:MIN:SEC) = 14:01:45 USER NO.=
 TierraWest-SiteA99368577
 INPUT FILE = C:\Users\Joel\Desktop\AHYMO IN\Skilled Nursing COMBINED
 final.txt

```
*****
*          Skilled Nursing Renaissance, ABQ,NM      *
*****
* 100-YEAR, 24-HR STORM (UNDER PROPOSED CONDITIONS) W/ routing *
*****
*  

*  

START           TIME=0.0  

*  

*  

RAINFALL        TYPE=2 RAIN QUARTER=0.0 IN  

                 RAIN ONE=2.01 IN RAIN SIX=2.35 IN  

                 RAIN DAY=2.75 IN DT=0.05 HR
```

24-HOUR RAINFALL DIST. - BASED ON NOAA ATLAS 14 FOR CONVECTIVE AREAS (NM & AZ) - D1

DT	0.050000 HOURS	END TIME	= 24.000002 HOURS
0.0000	0.0023	0.0046	0.0071 0.0099 0.0127 0.0159
0.0203	0.0272	0.0347	0.0424 0.0509 0.0595 0.0684
0.0776	0.0870	0.0974	0.1084 0.1204 0.1437 0.1728
0.2117	0.2559	0.3104	0.3831 0.4649 0.6062 0.8258
1.2021	1.4666	1.6752	1.7800 1.8719 1.9379 1.9905
2.0362	2.0697	2.1005	2.1259 2.1418 2.1530 2.1629
2.1722	2.1803	2.1879	2.1953 2.2025 2.2084 2.2118
2.2152	2.2186	2.2217	2.2247 2.2278 2.2307 2.2336
2.2363	2.2391	2.2417	2.2443 2.2469 2.2494 2.2518
2.2542	2.2565	2.2588	2.2611 2.2633 2.2654 2.2676
2.2697	2.2717	2.2738	2.2758 2.2778 2.2798 2.2817
2.2837	2.2856	2.2874	2.2893 2.2911 2.2930 2.2948
2.2965	2.2983	2.3000	2.3017 2.3034 2.3051 2.3068
2.3084	2.3100	2.3117	2.3133 2.3148 2.3164 2.3180
2.3195	2.3210	2.3225	2.3240 2.3255 2.3269 2.3284
2.3298	2.3313	2.3327	2.3341 2.3355 2.3368 2.3382
2.3396	2.3409	2.3422	2.3436 2.3449 2.3462 2.3474
2.3487	2.3500	2.3513	2.3525 2.3538 2.3551 2.3563
2.3576	2.3589	2.3601	2.3614 2.3627 2.3639 2.3652
2.3665	2.3677	2.3690	2.3702 2.3715 2.3728 2.3740
2.3753	2.3765	2.3778	2.3790 2.3803 2.3815 2.3828
2.3840	2.3853	2.3865	2.3878 2.3890 2.3903 2.3915
2.3927	2.3940	2.3952	2.3965 2.3977 2.3989 2.4002
2.4014	2.4027	2.4039	2.4051 2.4064 2.4076 2.4088

AHYMO							
2.4101	2.4113	2.4125	2.4137	2.4150	2.4162	2.4174	
2.4186	2.4199	2.4211	2.4223	2.4235	2.4247	2.4260	
2.4272	2.4284	2.4296	2.4308	2.4320	2.4333	2.4345	
2.4357	2.4369	2.4381	2.4393	2.4405	2.4417	2.4429	
2.4441	2.4453	2.4465	2.4478	2.4490	2.4502	2.4514	
2.4526	2.4538	2.4550	2.4561	2.4573	2.4585	2.4597	
2.4609	2.4621	2.4633	2.4645	2.4657	2.4669	2.4681	
2.4692	2.4704	2.4716	2.4728	2.4740	2.4752	2.4764	
2.4775	2.4787	2.4799	2.4811	2.4822	2.4834	2.4846	
2.4858	2.4869	2.4881	2.4893	2.4905	2.4916	2.4928	
2.4940	2.4951	2.4963	2.4975	2.4986	2.4998	2.5010	
2.5021	2.5033	2.5044	2.5056	2.5068	2.5079	2.5091	
2.5102	2.5114	2.5125	2.5137	2.5148	2.5160	2.5171	
2.5183	2.5194	2.5206	2.5217	2.5229	2.5240	2.5252	
2.5263	2.5274	2.5286	2.5297	2.5309	2.5320	2.5331	
2.5343	2.5354	2.5365	2.5377	2.5388	2.5399	2.5411	
2.5422	2.5433	2.5445	2.5456	2.5467	2.5478	2.5490	
2.5501	2.5512	2.5523	2.5535	2.5546	2.5557	2.5568	
2.5579	2.5590	2.5602	2.5613	2.5624	2.5635	2.5646	
2.5657	2.5668	2.5679	2.5691	2.5702	2.5713	2.5724	
2.5735	2.5746	2.5757	2.5768	2.5779	2.5790	2.5801	
2.5812	2.5823	2.5834	2.5845	2.5856	2.5867	2.5878	
2.5889	2.5899	2.5910	2.5921	2.5932	2.5943	2.5954	
2.5965	2.5976	2.5986	2.5997	2.6008	2.6019	2.6030	
2.6040	2.6051	2.6062	2.6073	2.6084	2.6094	2.6105	
2.6116	2.6126	2.6137	2.6148	2.6159	2.6169	2.6180	
2.6191	2.6201	2.6212	2.6223	2.6233	2.6244	2.6254	
2.6265	2.6276	2.6286	2.6297	2.6307	2.6318	2.6328	
2.6339	2.6350	2.6360	2.6371	2.6381	2.6392	2.6402	
2.6413	2.6423	2.6433	2.6444	2.6454	2.6465	2.6475	
2.6486	2.6496	2.6506	2.6517	2.6527	2.6538	2.6548	
2.6558	2.6569	2.6579	2.6589	2.6600	2.6610	2.6620	
2.6630	2.6641	2.6651	2.6661	2.6672	2.6682	2.6692	
2.6702	2.6712	2.6723	2.6733	2.6743	2.6753	2.6763	
2.6774	2.6784	2.6794	2.6804	2.6814	2.6824	2.6834	
2.6844	2.6854	2.6865	2.6875	2.6885	2.6895	2.6905	
2.6915	2.6925	2.6935	2.6945	2.6955	2.6965	2.6975	
2.6985	2.6995	2.7005	2.7015	2.7025	2.7034	2.7044	
2.7054	2.7064	2.7074	2.7084	2.7094	2.7104	2.7114	
2.7123	2.7133	2.7143	2.7153	2.7163	2.7172	2.7182	
2.7192	2.7202	2.7211	2.7221	2.7231	2.7241	2.7250	
2.7260	2.7270	2.7280	2.7289	2.7299	2.7309	2.7318	
2.7328	2.7338	2.7347	2.7357	2.7366	2.7376	2.7386	
2.7395	2.7405	2.7414	2.7424	2.7433	2.7443	2.7452	
2.7462	2.7472	2.7481	2.7491	2.7500			

*DEVELOPED CONDITIONS

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AHYMO

*BASIN A1

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COMPUTE NM HYD ID=1 HYD NO=100.1 AREA=0.00057 SQ MI
 PER A=0.00 PER B=16.0 PER C=0.00 PER D=84.00
 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE
 CONSTANT, N = 7.106428
 UNIT PEAK = 1.8903 CFS UNIT VOLUME = 0.9941 B = 526.28
 P60 = 2.0100
 AREA = 0.000479 SQ MI IA = 0.10000 INCHES INF = 0.04000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
 0.050000

K = 0.132088HR TP = 0.133300HR K/TP RATIO = 0.990905 SHAPE
 CONSTANT, N = 3.562974
 UNIT PEAK = 0.22229 CFS UNIT VOLUME = 0.9417 B = 324.90
 P60 = 2.0100
 AREA = 0.000091 SQ MI IA = 0.50000 INCHES INF = 1.25000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
 0.050000

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 100.10

RUNOFF VOLUME = 2.25684 INCHES = 0.0686 ACRE-FEET
 PEAK DISCHARGE RATE = 1.65 CFS AT 1.500 HOURS BASIN AREA =
 0.0006 SQ. MI.

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*BASIN A2

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COMPUTE NM HYD ID=2 HYD NO=100.2 AREA=0.00115 SQ MI
 PER A=0.00 PER B=27.0 PER C=0.0 PER D=73.00
 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE
 CONSTANT, N = 7.106428
 UNIT PEAK = 3.3144 CFS UNIT VOLUME = 0.9959 B = 526.28
 P60 = 2.0100

AHYMO

AREA = 0.000840 SQ MI IA = 0.10000 INCHES INF = 0.04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

K = 0.132088HR TP = 0.133300HR K/TP RATIO = 0.990905 SHAPE
CONSTANT, N = 3.562974
UNIT PEAK = 0.75681 CFS UNIT VOLUME = 0.9843 B = 324.90
P60 = 2.0100
AREA = 0.000311 SQ MI IA = 0.50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

PRINT HYD ID=2 CODE=1

PARTIAL HYDROGRAPH 100.20

RUNOFF VOLUME = 2.08616 INCHES = 0.1280 ACRE-FEET
PEAK DISCHARGE RATE = 3.14 CFS AT 1.500 HOURS BASIN AREA =
0.0012 SQ. MI.

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*BASIN A3
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COMPUTE NM HYD ID=3 HYD NO=100.3 AREA=0.00039 SQ MI
PER A=0.00 PER B=45.0 PER C=00.0 PER D=55.00
TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE
CONSTANT, N = 7.106428
UNIT PEAK = 0.84686 CFS UNIT VOLUME = 0.9865 B = 526.28
P60 = 2.0100
AREA = 0.000215 SQ MI IA = 0.10000 INCHES INF = 0.04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

K = 0.132088HR TP = 0.133300HR K/TP RATIO = 0.990905 SHAPE
CONSTANT, N = 3.562974
UNIT PEAK = 0.42776 CFS UNIT VOLUME = 0.9695 B = 324.90
P60 = 2.0100

AHYMO
AREA = 0.000176 SQ MI IA = 0.50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

PRINT HYD ID=3 CODE=1

PARTIAL HYDROGRAPH 100.30

RUNOFF VOLUME = 1.80685 INCHES = 0.0376 ACRE-FEET
PEAK DISCHARGE RATE = 0.98 CFS AT 1.500 HOURS BASIN AREA =
0.0004 SQ. MI.

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*BASIN B1-B5
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COMPUTE NM HYD ID=4 HYD NO=100.4 AREA=0.00147 SQ MI
PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.0
TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE
CONSTANT, N = 7.106428
UNIT PEAK = 5.8036 CFS UNIT VOLUME = 0.9971 B = 526.28
P60 = 2.0100
AREA = 0.001470 SQ MI IA = 0.10000 INCHES INF = 0.04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

PRINT HYD ID=4 CODE=1

PARTIAL HYDROGRAPH 100.40

RUNOFF VOLUME = 2.50511 INCHES = 0.1964 ACRE-FEET
PEAK DISCHARGE RATE = 4.53 CFS AT 1.500 HOURS BASIN AREA =
0.0015 SQ. MI.

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*BASIN C2
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AHYMO

COMPUTE NM HYD ID=5 HYD NO=100.5 AREA=0.00056 SQ MI
 PER A=0.00 PER B=17.0 PER C=0.0 PER D=83.00
 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE
 CONSTANT, N = 7.106428
 UNIT PEAK = 1.8351 CFS UNIT VOLUME = 0.9928 B = 526.28
 P60 = 2.0100
 AREA = 0.000465 SQ MI IA = 0.10000 INCHES INF = 0.04000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
 0.050000

K = 0.132088HR TP = 0.133300HR K/TP RATIO = 0.990905 SHAPE
 CONSTANT, N = 3.562974
 UNIT PEAK = 0.23204 CFS UNIT VOLUME = 0.9417 B = 324.90
 P60 = 2.0100
 AREA = 0.000095 SQ MI IA = 0.50000 INCHES INF = 1.25000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
 0.050000

PRINT HYD ID=5 CODE=1

PARTIAL HYDROGRAPH 100.50

RUNOFF VOLUME = 2.24132 INCHES = 0.0669 ACRE-FEET
 PEAK DISCHARGE RATE = 1.61 CFS AT 1.500 HOURS BASIN AREA =
 0.0006 SQ. MI.

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*BASIN C3

COMPUTE NM HYD ID=6 HYD NO=100.6 AREA=0.00030 SQ MI
 PER A=0.00 PER B=20.0 PER C=0.0 PER D=80.00
 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE
 CONSTANT, N = 7.106428
 UNIT PEAK = 0.94753 CFS UNIT VOLUME = 0.9891 B = 526.28
 P60 = 2.0100
 AREA = 0.000240 SQ MI IA = 0.10000 INCHES INF = 0.04000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =

AHYMO

0.050000

K = 0.132088HR TP = 0.133300HR K/TP RATIO = 0.990905 SHAPE
CONSTANT, N = 3.562974
UNIT PEAK = 0.14624 CFS UNIT VOLUME = 0.9143 B = 324.90
P60 = 2.0100
AREA = 0.000060 SQ MI IA = 0.50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

PRINT HYD ID=6 CODE=1

PARTIAL HYDROGRAPH 100.60

RUNOFF VOLUME = 2.19477 INCHES = 0.0351 ACRE-FEET
PEAK DISCHARGE RATE = 0.86 CFS AT 1.500 HOURS BASIN AREA =
0.0003 SQ. MI.

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*BASIN C4
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COMPUTE NM HYD ID=7 HYD NO=100.7 AREA=0.00071 SQ MI
PER A=0.00 PER B=13.0 PER C=0.0 PER D=87.00
TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE
CONSTANT, N = 7.106428
UNIT PEAK = 2.4387 CFS UNIT VOLUME = 0.9951 B = 526.28
P60 = 2.0100
AREA = 0.000618 SQ MI IA = 0.10000 INCHES INF = 0.04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

K = 0.132088HR TP = 0.133300HR K/TP RATIO = 0.990905 SHAPE
CONSTANT, N = 3.562974
UNIT PEAK = 0.22497 CFS UNIT VOLUME = 0.9417 B = 324.90
P60 = 2.0100
AREA = 0.000092 SQ MI IA = 0.50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =

AHYMO

0.050000

PRINT HYD ID=7 CODE=1

PARTIAL HYDROGRAPH 100.70

RUNOFF VOLUME = 2.30339 INCHES = 0.0872 ACRE-FEET
PEAK DISCHARGE RATE = 2.08 CFS AT 1.500 HOURS BASIN AREA =
0.0007 SQ. MI.

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*BASIN C1

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COMPUTE NM HYD ID=8 HYD NO=100.8 AREA=0.00091 SQ MI
PER A=15.0 PER B=54.0 PER C=0.0 PER D=31.00
TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE
CONSTANT, N = 7.106428
UNIT PEAK = 1.1137 CFS UNIT VOLUME = 0.9891 B = 526.28
P60 = 2.0100
AREA = 0.000282 SQ MI IA = 0.10000 INCHES INF = 0.04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

K = 0.138189HR TP = 0.133300HR K/TP RATIO = 1.036677 SHAPE
CONSTANT, N = 3.405054
UNIT PEAK = 1.4760 CFS UNIT VOLUME = 0.9909 B = 313.34
P60 = 2.0100
AREA = 0.000628 SQ MI IA = 0.53261 INCHES INF = 1.34130
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

PRINT HYD ID=8 CODE=1

PARTIAL HYDROGRAPH 100.80

RUNOFF VOLUME = 1.39894 INCHES = 0.0679 ACRE-FEET
PEAK DISCHARGE RATE = 1.90 CFS AT 1.500 HOURS BASIN AREA =
0.0009 SQ. MI.

AHYMO

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*ROUTE BASIN C1 THROUGH DETENTION POND NO.1

ROUTE RESERVOIR ID=55 HYD NO=200.1 INFLOW ID=8 CODE=24

	OUTFLOW (CFS)	STORAGE(AC-FT)	ELEVATION(FT)
	0.1000	0.0	83.00
	0.1554	0.0082	84.00
	0.2260	0.0243	85.00
	0.2793	0.0510	86.00
	0.3240	0.0913	87.00
	0.3632	0.1490	88.00

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TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
0.00	0.00	81.19	-0.015	0.00
1.20	0.14	83.00	0.000	0.10
2.40	0.06	85.45	0.036	0.25
3.60	0.00	84.46	0.016	0.19
4.80	0.00	83.14	0.001	0.11
6.00	0.00	83.00	0.000	0.10
7.20	0.00	83.00	0.000	0.10
8.40	0.00	83.00	0.000	0.10
9.60	0.00	83.00	0.000	0.10
10.80	0.00	83.00	0.000	0.10
12.00	0.00	83.00	0.000	0.10
13.20	0.00	83.00	0.000	0.10
14.40	0.00	83.00	0.000	0.10
15.60	0.00	83.00	0.000	0.10
16.80	0.00	83.00	0.000	0.10
18.00	0.00	83.00	0.000	0.10
19.20	0.00	83.00	0.000	0.10
20.40	0.00	83.00	0.000	0.10
21.60	0.00	83.00	0.000	0.10
22.80	0.00	83.00	0.000	0.10
24.00	0.00	83.00	0.000	0.10
25.20	0.00	83.00	0.000	0.10
26.40	0.00	83.00	0.000	0.10

			AHYMO	
27.60	0.00	83.00	0.000	0.10
28.80	0.00	83.00	0.000	0.10
30.00	0.00	83.00	0.000	0.10
31.20	0.00	83.00	0.000	0.10
32.40	0.00	83.00	0.000	0.10
33.60	0.00	83.00	0.000	0.10
34.80	0.00	83.00	0.000	0.10
36.00	0.00	83.00	0.000	0.10
37.20	0.00	83.00	0.000	0.10
38.40	0.00	83.00	0.000	0.10
39.60	0.00	83.00	0.000	0.10
40.80	0.00	83.00	0.000	0.10
42.00	0.00	83.00	0.000	0.10
43.20	0.00	83.00	0.000	0.10
44.40	0.00	83.00	0.000	0.10
45.60	0.00	83.00	0.000	0.10
46.80	0.00	83.00	0.000	0.10
48.00	0.00	83.00	0.000	0.10
49.20	0.00	83.00	0.000	0.10
50.40	0.00	83.00	0.000	0.10
51.60	0.00	83.00	0.000	0.10
52.80	0.00	83.00	0.000	0.10
54.00	0.00	83.00	0.000	0.10
55.20	0.00	83.00	0.000	0.10
56.40	0.00	83.00	0.000	0.10
57.60	0.00	83.00	0.000	0.10
58.80	0.00	83.00	0.000	0.10
60.00	0.00	83.00	0.000	0.10
61.20	0.00	83.00	0.000	0.10
62.40	0.00	83.00	0.000	0.10
63.60	0.00	83.00	0.000	0.10
64.80	0.00	83.00	0.000	0.10
66.00	0.00	83.00	0.000	0.10

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
67.20	0.00	83.00	0.000	0.10
68.40	0.00	83.00	0.000	0.10
69.60	0.00	83.00	0.000	0.10
70.80	0.00	83.00	0.000	0.10
72.00	0.00	83.00	0.000	0.10
73.20	0.00	83.00	0.000	0.10
74.40	0.00	83.00	0.000	0.10
75.60	0.00	83.00	0.000	0.10
76.80	0.00	83.00	0.000	0.10
78.00	0.00	83.00	0.000	0.10
79.20	0.00	83.00	0.000	0.10

			AHYMO	
TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
80.40	0.00	83.00	0.000	0.10
81.60	0.00	83.00	0.000	0.10
82.80	0.00	83.00	0.000	0.10
84.00	0.00	83.00	0.000	0.10
85.20	0.00	83.00	0.000	0.10
86.40	0.00	83.00	0.000	0.10
87.60	0.00	83.00	0.000	0.10
88.80	0.00	83.00	0.000	0.10
90.00	0.00	83.00	0.000	0.10
91.20	0.00	83.00	0.000	0.10
92.40	0.00	83.00	0.000	0.10
93.60	0.00	83.00	0.000	0.10
94.80	0.00	83.00	0.000	0.10
96.00	0.00	83.00	0.000	0.10
97.20	0.00	83.00	0.000	0.10
98.40	0.00	83.00	0.000	0.10
99.60	0.00	83.00	0.000	0.10
100.80	0.00	83.00	0.000	0.10
102.00	0.00	83.00	0.000	0.10
103.20	0.00	83.00	0.000	0.10
104.40	0.00	83.00	0.000	0.10
105.60	0.00	83.00	0.000	0.10
106.80	0.00	83.00	0.000	0.10
108.00	0.00	83.00	0.000	0.10
109.20	0.00	83.00	0.000	0.10
110.40	0.00	83.00	0.000	0.10
111.60	0.00	83.00	0.000	0.10
112.80	0.00	83.00	0.000	0.10
114.00	0.00	83.00	0.000	0.10
115.20	0.00	83.00	0.000	0.10
116.40	0.00	83.00	0.000	0.10
117.60	0.00	83.00	0.000	0.10
118.80	0.00	83.00	0.000	0.10
120.00	0.00	83.00	0.000	0.10
121.20	0.00	83.00	0.000	0.10
122.40	0.00	83.00	0.000	0.10
123.60	0.00	83.00	0.000	0.10
124.80	0.00	83.00	0.000	0.10
126.00	0.00	83.00	0.000	0.10
127.20	0.00	83.00	0.000	0.10
128.40	0.00	83.00	0.000	0.10
129.60	0.00	83.00	0.000	0.10
130.80	0.00	83.00	0.000	0.10
132.00	0.00	83.00	0.000	0.10
133.20	0.00	83.00	0.000	0.10

AHYMO

134.40	0.00	83.00	0.000	0.10
135.60	0.00	83.00	0.000	0.10
136.80	0.00	83.00	0.000	0.10
138.00	0.00	83.00	0.000	0.10
139.20	0.00	83.00	0.000	0.10
140.40	0.00	83.00	0.000	0.10
141.60	0.00	83.00	0.000	0.10
142.80	0.00	83.00	0.000	0.10
144.00	0.00	83.00	0.000	0.10
145.20	0.00	83.00	0.000	0.10
146.40	0.00	83.00	0.000	0.10
147.60	0.00	83.00	0.000	0.10
148.80	0.00	83.00	0.000	0.10
150.00	0.00	83.00	0.000	0.10
151.20	0.00	83.00	0.000	0.10
152.40	0.00	83.00	0.000	0.10
153.60	0.00	83.00	0.000	0.10
154.80	0.00	83.00	0.000	0.10
156.00	0.00	83.00	0.000	0.10
157.20	0.00	83.00	0.000	0.10
158.40	0.00	83.00	0.000	0.10
159.60	0.00	83.00	0.000	0.10
160.80	0.00	83.00	0.000	0.10
162.00	0.00	83.00	0.000	0.10
163.20	0.00	83.00	0.000	0.10
164.40	0.00	83.00	0.000	0.10
165.60	0.00	83.00	0.000	0.10
166.80	0.00	83.00	0.000	0.10
168.00	0.00	83.00	0.000	0.10
169.20	0.00	83.00	0.000	0.10
170.40	0.00	83.00	0.000	0.10
171.60	0.00	83.00	0.000	0.10
172.80	0.00	83.00	0.000	0.10
174.00	0.00	83.00	0.000	0.10
175.20	0.00	83.00	0.000	0.10
176.40	0.00	83.00	0.000	0.10
177.60	0.00	83.00	0.000	0.10
178.80	0.00	83.00	0.000	0.10
180.00	0.00	83.00	0.000	0.10
181.20	0.00	83.00	0.000	0.10
182.40	0.00	83.00	0.000	0.10
183.60	0.00	83.00	0.000	0.10
184.80	0.00	83.00	0.000	0.10
186.00	0.00	83.00	0.000	0.10
187.20	0.00	83.00	0.000	0.10
188.40	0.00	83.00	0.000	0.10
189.60	0.00	83.00	0.000	0.10

			AHYMO	
190.80	0.00	83.00	0.000	0.10
192.00	0.00	83.00	0.000	0.10
193.20	0.00	83.00	0.000	0.10
194.40	0.00	83.00	0.000	0.10
195.60	0.00	83.00	0.000	0.10
196.80	0.00	83.00	0.000	0.10
198.00	0.00	83.00	0.000	0.10
199.20	0.00	83.00	0.000	0.10
PEAK DISCHARGE =	0.259 CFS	- PEAK OCCURS AT HOUR	1.95	
MAXIMUM WATER SURFACE ELEVATION =	85.626	<87.0 OK		
MAXIMUM STORAGE =	0.0410 AC-FT	INCREMENTAL TIME=	0.050000HRS	

*

PRINT HYD ID=55 CODE=1

PARTIAL HYDROGRAPH 200.10

RUNOFF VOLUME = 34.64382 INCHES = 1.6814 ACRE-FEET
 PEAK DISCHARGE RATE = 0.26 CFS AT 1.950 HOURS BASIN AREA =
 0.0009 SQ. MI.

*

*

*BASIN C6

*

COMPUTE NM HYD ID=9 HYD NO=100.9 AREA=0.00050 SQ MI
 PER A=0.00 PER B=21.0 PER C=0.0 PER D=79.0
 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE
 CONSTANT, N = 7.106428
 UNIT PEAK = 1.5595 CFS UNIT VOLUME = 0.9928 B = 526.28
 P60 = 2.0100
 AREA = 0.000395 SQ MI IA = 0.10000 INCHES INF = 0.04000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
 0.050000

K = 0.132088HR TP = 0.133300HR K/TP RATIO = 0.990905 SHAPE
 CONSTANT, N = 3.562974
 UNIT PEAK = 0.25592 CFS UNIT VOLUME = 0.9487 B = 324.90
 P60 = 2.0100
 AREA = 0.000105 SQ MI IA = 0.50000 INCHES INF = 1.25000
 INCHES PER HOUR

AHYMO
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

PRINT HYD ID=9 CODE=1

PARTIAL HYDROGRAPH 100.90

RUNOFF VOLUME = 2.17926 INCHES = 0.0581 ACRE-FEET
PEAK DISCHARGE RATE = 1.41 CFS AT 1.500 HOURS BASIN AREA =
0.0005 SQ. MI.

*
*
*BASIN C5
*

COMPUTE NM HYD ID=10 HYD NO=100.10 AREA=0.00029 SQ MI
PER A=0.00 PER B=17.0 PER C=0.0 PER D=83.0
TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE
CONSTANT, N = 7.106428
UNIT PEAK = 0.95030 CFS UNIT VOLUME = 0.9891 B = 526.28
P60 = 2.0100
AREA = 0.000241 SQ MI IA = 0.10000 INCHES INF = 0.04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

K = 0.132088HR TP = 0.133300HR K/TP RATIO = 0.990905 SHAPE
CONSTANT, N = 3.562974
UNIT PEAK = 0.12016 CFS UNIT VOLUME = 0.8894 B = 324.90
P60 = 2.0100
AREA = 0.000049 SQ MI IA = 0.50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

PRINT HYD ID=10 CODE=1

PARTIAL HYDROGRAPH 100.10

RUNOFF VOLUME = 2.24132 INCHES = 0.0347 ACRE-FEET
PEAK DISCHARGE RATE = 0.84 CFS AT 1.500 HOURS BASIN AREA =

AHYMO

0.0003 SQ. MI.

*
*
*BASIN D1
*

COMPUTE NM HYD ID=11 HYD NO=100.11 AREA=0.00018 SQ MI
PER A=0.00 PER B=30.0 PER C=0.0 PER D=70.00
TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE
CONSTANT, N = 7.106428
UNIT PEAK = 0.49745 CFS UNIT VOLUME = 0.9791 B = 526.28
P60 = 2.0100
AREA = 0.000126 SQ MI IA = 0.10000 INCHES INF = 0.04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

K = 0.132088HR TP = 0.133300HR K/TP RATIO = 0.990905 SHAPE
CONSTANT, N = 3.562974
UNIT PEAK = 0.13162 CFS UNIT VOLUME = 0.9027 B = 324.90
P60 = 2.0100
AREA = 0.000054 SQ MI IA = 0.50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

PRINT HYD ID=11 CODE=1

PARTIAL HYDROGRAPH 100.11

RUNOFF VOLUME = 2.03961 INCHES = 0.0196 ACRE-FEET
PEAK DISCHARGE RATE = 0.50 CFS AT 1.500 HOURS BASIN AREA =
0.0002 SQ. MI.

*
*
*COMBINE POND1 DISCHARGE WITH BASINS ROUTED TO POND NO.2
*

ADD HYD ID=50 HYD NO=100.21 ID=1 ID=2

	AHYMO
ADD HYD	ID=50 HYD NO=100.21 ID=50 ID=3
ADD HYD	ID=50 HYD NO=100.21 ID=50 ID=4
ADD HYD	ID=50 HYD NO=100.21 ID=50 ID=5
ADD HYD	ID=50 HYD NO=100.21 ID=50 ID=6
ADD HYD	ID=50 HYD NO=100.21 ID=50 ID=7
ADD HYD	ID=50 HYD NO=100.21 ID=50 ID=9
ADD HYD	ID=50 HYD NO=100.21 ID=50 ID=10
ADD HYD	ID=50 HYD NO=100.21 ID=50 ID=11
ADD HYD	ID=50 HYD NO=100.21 ID=50 ID=55
*	
PRINT HYD	ID=50 CODE=1

PARTIAL HYDROGRAPH 100.21

RUNOFF VOLUME = 6.43692 INCHES = 2.4134 ACRE-FEET
 PEAK DISCHARGE RATE = 17.79 CFS AT 1.500 HOURS BASIN AREA =
 0.0070 SQ. MI.

*

*ROUTE POND1 DISCHARGE & BASINS A1-3,B1-5,C2-6,D1 THRU COMBINED UG/POND 2 DETENT
 ROUTE RESERVOIR ID=56 HYD NO=200.3 INFLOW ID=50 CODE=24

OUTFLOW (CFS)	STORAGE(AC-FT)	ELEVATION(FT)
0.0957	0.0000	77.00
0.1435	0.0217	77.50
0.1790	0.0587	78.00
0.2085	0.1027	78.50
0.2343	0.1499	79.00
0.2576	0.1972	79.50
0.2789	0.2414	80.00

AHYMO		
0.2987	0.2784	80.50
0.3173	0.3000	81.00
0.3515	0.3609	82.00
0.3827	0.4218	83.00
0.4115	0.4827	84.00
0.4384	0.5436	85.00
0.4638	0.6045	86.00

* * * * *

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
0.00	0.00	76.00	-0.043	0.00
1.20	2.59	77.60	0.029	0.15
2.40	0.77	85.72	0.588	0.46
3.60	0.22	85.52	0.575	0.45
4.80	0.16	85.09	0.549	0.44
6.00	0.18	84.65	0.522	0.43
7.20	0.18	84.26	0.499	0.42
8.40	0.18	83.88	0.476	0.41
9.60	0.18	83.52	0.453	0.40
10.80	0.18	83.17	0.432	0.39
12.00	0.18	82.84	0.412	0.38
13.20	0.18	82.52	0.392	0.37
14.40	0.17	82.21	0.374	0.36
15.60	0.17	81.92	0.356	0.35
16.80	0.17	81.64	0.339	0.34
18.00	0.17	81.37	0.322	0.33
19.20	0.17	81.11	0.307	0.32
20.40	0.17	80.82	0.292	0.31
21.60	0.17	80.50	0.278	0.30
22.80	0.16	80.33	0.265	0.29
24.00	0.16	80.16	0.253	0.29
25.20	0.10	79.94	0.236	0.28
26.40	0.10	79.74	0.219	0.27
27.60	0.10	79.56	0.203	0.26
28.80	0.10	79.39	0.187	0.25
30.00	0.10	79.24	0.172	0.25
31.20	0.10	79.09	0.158	0.24
32.40	0.10	78.95	0.145	0.23

			AHYMO	
33.60	0.10	78.81	0.132	0.22
34.80	0.10	78.68	0.120	0.22
36.00	0.10	78.56	0.109	0.21
37.20	0.10	78.45	0.098	0.21
38.40	0.10	78.33	0.088	0.20
39.60	0.10	78.22	0.078	0.19
40.80	0.10	78.12	0.070	0.19
42.00	0.10	78.03	0.061	0.18
43.20	0.10	77.93	0.054	0.17
44.40	0.10	77.84	0.047	0.17
45.60	0.10	77.75	0.040	0.16
46.80	0.10	77.67	0.034	0.16
48.00	0.10	77.60	0.029	0.15
49.20	0.10	77.54	0.024	0.15
50.40	0.10	77.46	0.020	0.14
51.60	0.10	77.38	0.016	0.13
52.80	0.10	77.31	0.014	0.13
54.00	0.10	77.26	0.011	0.12
55.20	0.10	77.22	0.009	0.12
56.40	0.10	77.18	0.008	0.11
57.60	0.10	77.16	0.007	0.11
58.80	0.10	77.14	0.006	0.11
60.00	0.10	77.12	0.005	0.11
61.20	0.10	77.10	0.004	0.11
62.40	0.10	77.09	0.004	0.10
63.60	0.10	77.08	0.004	0.10
64.80	0.10	77.08	0.003	0.10
66.00	0.10	77.07	0.003	0.10

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
67.20	0.10	77.06	0.003	0.10
68.40	0.10	77.06	0.003	0.10
69.60	0.10	77.06	0.003	0.10
70.80	0.10	77.06	0.002	0.10
72.00	0.10	77.05	0.002	0.10
73.20	0.10	77.05	0.002	0.10
74.40	0.10	77.05	0.002	0.10
75.60	0.10	77.05	0.002	0.10
76.80	0.10	77.05	0.002	0.10
78.00	0.10	77.05	0.002	0.10
79.20	0.10	77.05	0.002	0.10
80.40	0.10	77.05	0.002	0.10
81.60	0.10	77.05	0.002	0.10
82.80	0.10	77.05	0.002	0.10
84.00	0.10	77.05	0.002	0.10
85.20	0.10	77.05	0.002	0.10

			AHYMO	
86.40	0.10	77.05	0.002	0.10
87.60	0.10	77.05	0.002	0.10
88.80	0.10	77.05	0.002	0.10
90.00	0.10	77.05	0.002	0.10
91.20	0.10	77.05	0.002	0.10
92.40	0.10	77.05	0.002	0.10
93.60	0.10	77.05	0.002	0.10
94.80	0.10	77.05	0.002	0.10
96.00	0.10	77.05	0.002	0.10
97.20	0.10	77.05	0.002	0.10
98.40	0.10	77.05	0.002	0.10
99.60	0.10	77.05	0.002	0.10
100.80	0.10	77.05	0.002	0.10
102.00	0.10	77.05	0.002	0.10
103.20	0.10	77.05	0.002	0.10
104.40	0.10	77.04	0.002	0.10
105.60	0.10	77.04	0.002	0.10
106.80	0.10	77.04	0.002	0.10
108.00	0.10	77.04	0.002	0.10
109.20	0.10	77.04	0.002	0.10
110.40	0.10	77.04	0.002	0.10
111.60	0.10	77.04	0.002	0.10
112.80	0.10	77.04	0.002	0.10
114.00	0.10	77.04	0.002	0.10
115.20	0.10	77.04	0.002	0.10
116.40	0.10	77.04	0.002	0.10
117.60	0.10	77.04	0.002	0.10
118.80	0.10	77.04	0.002	0.10
120.00	0.10	77.04	0.002	0.10
121.20	0.10	77.04	0.002	0.10
122.40	0.10	77.04	0.002	0.10
123.60	0.10	77.04	0.002	0.10
124.80	0.10	77.04	0.002	0.10
126.00	0.10	77.04	0.002	0.10
127.20	0.10	77.04	0.002	0.10
128.40	0.10	77.04	0.002	0.10
129.60	0.10	77.04	0.002	0.10
130.80	0.10	77.04	0.002	0.10
132.00	0.10	77.04	0.002	0.10
133.20	0.10	77.04	0.002	0.10

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
134.40	0.10	77.04	0.002	0.10
135.60	0.10	77.04	0.002	0.10
136.80	0.10	77.04	0.002	0.10
138.00	0.10	77.04	0.002	0.10

			AHYMO	
139.20	0.10	77.04	0.002	0.10
140.40	0.10	77.04	0.002	0.10
141.60	0.10	77.04	0.002	0.10
142.80	0.10	77.04	0.002	0.10
144.00	0.10	77.04	0.002	0.10
145.20	0.10	77.04	0.002	0.10
146.40	0.10	77.04	0.002	0.10
147.60	0.10	77.04	0.002	0.10
148.80	0.10	77.04	0.002	0.10
150.00	0.10	77.04	0.002	0.10
151.20	0.10	77.04	0.002	0.10
152.40	0.10	77.04	0.002	0.10
153.60	0.10	77.04	0.002	0.10
154.80	0.10	77.04	0.002	0.10
156.00	0.10	77.04	0.002	0.10
157.20	0.10	77.04	0.002	0.10
158.40	0.10	77.04	0.002	0.10
159.60	0.10	77.04	0.002	0.10
160.80	0.10	77.04	0.002	0.10
162.00	0.10	77.04	0.002	0.10
163.20	0.10	77.04	0.002	0.10
164.40	0.10	77.04	0.002	0.10
165.60	0.10	77.04	0.002	0.10
166.80	0.10	77.04	0.002	0.10
168.00	0.10	77.04	0.002	0.10
169.20	0.10	77.04	0.002	0.10
170.40	0.10	77.04	0.002	0.10
171.60	0.10	77.04	0.002	0.10
172.80	0.10	77.04	0.002	0.10
174.00	0.10	77.04	0.002	0.10
175.20	0.10	77.04	0.002	0.10
176.40	0.10	77.04	0.002	0.10
177.60	0.10	77.04	0.002	0.10
178.80	0.10	77.04	0.002	0.10
180.00	0.10	77.04	0.002	0.10
181.20	0.10	77.04	0.002	0.10
182.40	0.10	77.04	0.002	0.10
183.60	0.10	77.04	0.002	0.10
184.80	0.10	77.04	0.002	0.10
186.00	0.10	77.04	0.002	0.10
187.20	0.10	77.04	0.002	0.10
188.40	0.10	77.04	0.002	0.10
189.60	0.10	77.04	0.002	0.10
190.80	0.10	77.04	0.002	0.10
192.00	0.10	77.04	0.002	0.10
193.20	0.10	77.04	0.002	0.10
194.40	0.10	77.04	0.002	0.10
195.60	0.10	77.04	0.002	0.10

AHYMO
196.80 0.10 77.04 0.002 0.10
198.00 0.10 77.04 0.002 0.10
199.20 0.10 77.04 0.002 0.10
PEAK DISCHARGE = 0.457 CFS - PEAK OCCURS AT HOUR 2.55
MAXIMUM WATER SURFACE ELEVATION = 85.751 <86, THEREFORE OK
MAXIMUM STORAGE = 0.5893 AC-FT INCREMENTAL TIME= 0.050000HRS

*

PRINT HYD ID=56 CODE=1

PARTIAL HYDROGRAPH 200.30

RUNOFF VOLUME = 6.43174 INCHES = 2.4115 ACRE-FEET
PEAK DISCHARGE RATE = 0.46 CFS AT 2.550 HOURS BASIN AREA =
0.0070 SQ. MI.

*

*BASIN D2

*

COMPUTE NM HYD ID=12 HYD NO=100.12 AREA=0.00067 SQ MI
PER A=0.00 PER B=97.0 PER C=0.0 PER D=3.00
TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE
CONSTANT, N = 7.106428
UNIT PEAK = 0.79356E-01CFS UNIT VOLUME = 0.8994 B = 526.28
P60 = 2.0100
AREA = 0.000020 SQ MI IA = 0.10000 INCHES INF = 0.04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

K = 0.132088HR TP = 0.133300HR K/TP RATIO = 0.990905 SHAPE
CONSTANT, N = 3.562974
UNIT PEAK = 1.5841 CFS UNIT VOLUME = 0.9932 B = 324.90
P60 = 2.0100
AREA = 0.000650 SQ MI IA = 0.50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =
0.050000

PRINT HYD ID=12 CODE=1

PARTIAL HYDROGRAPH 100.12

AHYMO

RUNOFF VOLUME = 0.99998 INCHES = 0.0357 ACRE-FEET
 PEAK DISCHARGE RATE = 1.19 CFS AT 1.500 HOURS BASIN AREA =
 0.0007 SQ. MI.

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*ROUTE BASIN D2 THROUGH POND NO 3

ROUTE RESERVOIR	ID=57 HYD NO=200.3 INFLOW ID=12 CODE=24
	OUTFLOW (CFS) STORAGE(AC-FT) ELEVATION(FT)
	0.0100 0.0000 72.00
	0.0500 0.0393 73.00

* * * * *

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
0.00	0.00	71.75	-0.010	0.00
1.20	0.01	72.00	0.000	0.01
2.40	0.04	72.79	0.031	0.04
3.60	0.00	72.71	0.028	0.04
4.80	0.00	72.62	0.024	0.03
6.00	0.00	72.54	0.021	0.03
7.20	0.00	72.46	0.018	0.03
8.40	0.00	72.39	0.015	0.03
9.60	0.00	72.33	0.013	0.02
10.80	0.00	72.28	0.011	0.02
12.00	0.00	72.22	0.009	0.02
13.20	0.00	72.18	0.007	0.02
14.40	0.00	72.14	0.005	0.02
15.60	0.00	72.10	0.004	0.01
16.80	0.00	72.07	0.003	0.01
18.00	0.00	72.04	0.001	0.01
19.20	0.00	72.01	0.000	0.01
20.40	0.00	72.00	0.000	0.01
21.60	0.00	72.00	0.000	0.01
22.80	0.00	72.00	0.000	0.01
24.00	0.00	72.00	0.000	0.01
25.20	0.00	72.00	0.000	0.01
26.40	0.00	72.00	0.000	0.01
27.60	0.00	72.00	0.000	0.01
28.80	0.00	72.00	0.000	0.01

			AHYMO	
30.00	0.00	72.00	0.000	0.01
31.20	0.00	72.00	0.000	0.01
32.40	0.00	72.00	0.000	0.01
33.60	0.00	72.00	0.000	0.01
34.80	0.00	72.00	0.000	0.01
36.00	0.00	72.00	0.000	0.01
37.20	0.00	72.00	0.000	0.01
38.40	0.00	72.00	0.000	0.01
39.60	0.00	72.00	0.000	0.01
40.80	0.00	72.00	0.000	0.01
42.00	0.00	72.00	0.000	0.01
43.20	0.00	72.00	0.000	0.01
44.40	0.00	72.00	0.000	0.01
45.60	0.00	72.00	0.000	0.01
46.80	0.00	72.00	0.000	0.01
48.00	0.00	72.00	0.000	0.01
49.20	0.00	72.00	0.000	0.01
50.40	0.00	72.00	0.000	0.01
51.60	0.00	72.00	0.000	0.01
52.80	0.00	72.00	0.000	0.01
54.00	0.00	72.00	0.000	0.01
55.20	0.00	72.00	0.000	0.01
56.40	0.00	72.00	0.000	0.01
57.60	0.00	72.00	0.000	0.01
58.80	0.00	72.00	0.000	0.01
60.00	0.00	72.00	0.000	0.01
61.20	0.00	72.00	0.000	0.01
62.40	0.00	72.00	0.000	0.01
63.60	0.00	72.00	0.000	0.01
64.80	0.00	72.00	0.000	0.01
66.00	0.00	72.00	0.000	0.01

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
67.20	0.00	72.00	0.000	0.01
68.40	0.00	72.00	0.000	0.01
69.60	0.00	72.00	0.000	0.01
70.80	0.00	72.00	0.000	0.01
72.00	0.00	72.00	0.000	0.01
73.20	0.00	72.00	0.000	0.01
74.40	0.00	72.00	0.000	0.01
75.60	0.00	72.00	0.000	0.01
76.80	0.00	72.00	0.000	0.01
78.00	0.00	72.00	0.000	0.01
79.20	0.00	72.00	0.000	0.01
80.40	0.00	72.00	0.000	0.01
81.60	0.00	72.00	0.000	0.01

			AHYMO	
TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
82.80	0.00	72.00	0.000	0.01
84.00	0.00	72.00	0.000	0.01
85.20	0.00	72.00	0.000	0.01
86.40	0.00	72.00	0.000	0.01
87.60	0.00	72.00	0.000	0.01
88.80	0.00	72.00	0.000	0.01
90.00	0.00	72.00	0.000	0.01
91.20	0.00	72.00	0.000	0.01
92.40	0.00	72.00	0.000	0.01
93.60	0.00	72.00	0.000	0.01
94.80	0.00	72.00	0.000	0.01
96.00	0.00	72.00	0.000	0.01
97.20	0.00	72.00	0.000	0.01
98.40	0.00	72.00	0.000	0.01
99.60	0.00	72.00	0.000	0.01
100.80	0.00	72.00	0.000	0.01
102.00	0.00	72.00	0.000	0.01
103.20	0.00	72.00	0.000	0.01
104.40	0.00	72.00	0.000	0.01
105.60	0.00	72.00	0.000	0.01
106.80	0.00	72.00	0.000	0.01
108.00	0.00	72.00	0.000	0.01
109.20	0.00	72.00	0.000	0.01
110.40	0.00	72.00	0.000	0.01
111.60	0.00	72.00	0.000	0.01
112.80	0.00	72.00	0.000	0.01
114.00	0.00	72.00	0.000	0.01
115.20	0.00	72.00	0.000	0.01
116.40	0.00	72.00	0.000	0.01
117.60	0.00	72.00	0.000	0.01
118.80	0.00	72.00	0.000	0.01
120.00	0.00	72.00	0.000	0.01
121.20	0.00	72.00	0.000	0.01
122.40	0.00	72.00	0.000	0.01
123.60	0.00	72.00	0.000	0.01
124.80	0.00	72.00	0.000	0.01
126.00	0.00	72.00	0.000	0.01
127.20	0.00	72.00	0.000	0.01
128.40	0.00	72.00	0.000	0.01
129.60	0.00	72.00	0.000	0.01
130.80	0.00	72.00	0.000	0.01
132.00	0.00	72.00	0.000	0.01
133.20	0.00	72.00	0.000	0.01
134.40	0.00	72.00	0.000	0.01

			AHYMO	
135.60	0.00	72.00	0.000	0.01
136.80	0.00	72.00	0.000	0.01
138.00	0.00	72.00	0.000	0.01
139.20	0.00	72.00	0.000	0.01
140.40	0.00	72.00	0.000	0.01
141.60	0.00	72.00	0.000	0.01
142.80	0.00	72.00	0.000	0.01
144.00	0.00	72.00	0.000	0.01
145.20	0.00	72.00	0.000	0.01
146.40	0.00	72.00	0.000	0.01
147.60	0.00	72.00	0.000	0.01
148.80	0.00	72.00	0.000	0.01
150.00	0.00	72.00	0.000	0.01
151.20	0.00	72.00	0.000	0.01
152.40	0.00	72.00	0.000	0.01
153.60	0.00	72.00	0.000	0.01
154.80	0.00	72.00	0.000	0.01
156.00	0.00	72.00	0.000	0.01
157.20	0.00	72.00	0.000	0.01
158.40	0.00	72.00	0.000	0.01
159.60	0.00	72.00	0.000	0.01
160.80	0.00	72.00	0.000	0.01
162.00	0.00	72.00	0.000	0.01
163.20	0.00	72.00	0.000	0.01
164.40	0.00	72.00	0.000	0.01
165.60	0.00	72.00	0.000	0.01
166.80	0.00	72.00	0.000	0.01
168.00	0.00	72.00	0.000	0.01
169.20	0.00	72.00	0.000	0.01
170.40	0.00	72.00	0.000	0.01
171.60	0.00	72.00	0.000	0.01
172.80	0.00	72.00	0.000	0.01
174.00	0.00	72.00	0.000	0.01
175.20	0.00	72.00	0.000	0.01
176.40	0.00	72.00	0.000	0.01
177.60	0.00	72.00	0.000	0.01
178.80	0.00	72.00	0.000	0.01
180.00	0.00	72.00	0.000	0.01
181.20	0.00	72.00	0.000	0.01
182.40	0.00	72.00	0.000	0.01
183.60	0.00	72.00	0.000	0.01
184.80	0.00	72.00	0.000	0.01
186.00	0.00	72.00	0.000	0.01
187.20	0.00	72.00	0.000	0.01
188.40	0.00	72.00	0.000	0.01
189.60	0.00	72.00	0.000	0.01
190.80	0.00	72.00	0.000	0.01
192.00	0.00	72.00	0.000	0.01

			AHYMO	
193.20	0.00	72.00	0.000	0.01
194.40	0.00	72.00	0.000	0.01
195.60	0.00	72.00	0.000	0.01
196.80	0.00	72.00	0.000	0.01
198.00	0.00	72.00	0.000	0.01
199.20	0.00	72.00	0.000	0.01
PEAK DISCHARGE =	0.042 CFS	- PEAK OCCURS AT HOUR	2.35	
MAXIMUM WATER SURFACE ELEVATION =	72.790	<73.0, THEREFORE OK		
MAXIMUM STORAGE =	0.0310 AC-FT	INCREMENTAL TIME=	0.050000HRS	

*

PRINT HYD ID=57 CODE=1

PARTIAL HYDROGRAPH 200.30

RUNOFF VOLUME = 5.18071 INCHES = 0.1851 ACRE-FEET
PEAK DISCHARGE RATE = 0.04 CFS AT 2.350 HOURS BASIN AREA =
0.0007 SQ. MI.

*

ADD HYD ID=58 HYD NO=100.22 ID=56 ID=57

*

PRINT HYD ID=58 CODE=1

PARTIAL HYDROGRAPH 100.22

RUNOFF VOLUME = 6.32291 INCHES = 2.5966 ACRE-FEET
PEAK DISCHARGE RATE = 0.50 CFS AT 2.550 HOURS BASIN AREA =
0.0077 SQ. MI.

PEAK DISCHARGE RATE=MAX Q ALLOWED,
THEREFORE OK

*

*

FINISH

NORMAL PROGRAM FINISH

END TIME (HR:MIN:SEC) = 14:01:45

APPENDIX B

HYDRAULIC ANALYSIS

Worksheet for Concrete Flume

Project Description

Friction Method	Manning Formula
Solve For	Discharge

Input Data

Roughness Coefficient	0.013
Channel Slope	0.01000 ft/ft
Normal Depth	0.50 ft
Bottom Width	2.00 ft

Results

Discharge	5.50	ft^3/s
Flow Area	1.00	ft^2
Wetted Perimeter	3.00	ft
Hydraulic Radius	0.33	ft
Top Width	2.00	ft
Critical Depth	0.62	ft
Critical Slope	0.00549	ft/ft
Velocity	5.50	ft/s
Velocity Head	0.47	ft
Specific Energy	0.97	ft
Froude Number	1.37	
Flow Type	Supercritical	

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.50	ft
Critical Depth	0.62	ft
Channel Slope	0.01000	ft/ft
Critical Slope	0.00549	ft/ft

Worksheet for Concrete Flume

Messages

Notes

Concrete flume capacity (5.5 cfs) at max flow depth of 0.5' exceeds required flow from Basin C2 (1.54 cfs) and Basin C4 (1.99 cfs).
OK

Worksheet for Circular Pipe - A1

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	0.00500 ft/ft
Diameter	12.00 in
Discharge	1.57 ft ³ /s

Results

Normal Depth	0.57	ft
Flow Area	0.46	ft ²
Wetted Perimeter	1.71	ft
Hydraulic Radius	0.27	ft
Top Width	0.99	ft
Critical Depth	0.53	ft
Percent Full	57.2	%
Critical Slope	0.00632	ft/ft
Velocity	3.38	ft/s
Velocity Head	0.18	ft
Specific Energy	0.75	ft
Froude Number	0.87	
Maximum Discharge	2.71	ft ³ /s
Discharge Full	2.52	ft ³ /s
Slope Full	0.00194	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	57.18	%
Downstream Velocity	Infinity	ft/s

Worksheet for Circular Pipe - A2

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	0.00500 ft/ft
Diameter	18.00 in
Discharge	4.56 ft ³ /s

Results

Normal Depth	0.85	ft
Flow Area	1.03	ft ²
Wetted Perimeter	2.56	ft
Hydraulic Radius	0.40	ft
Top Width	1.49	ft
Critical Depth	0.82	ft
Percent Full	56.6	%
Critical Slope	0.00561	ft/ft
Velocity	4.42	ft/s
Velocity Head	0.30	ft
Specific Energy	1.15	ft
Froude Number	0.93	
Maximum Discharge	7.99	ft ³ /s
Discharge Full	7.43	ft ³ /s
Slope Full	0.00188	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	56.64	%
Downstream Velocity	Infinity	ft/s

Worksheet for Circular Pipe - B1,B2

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient	0.010
Channel Slope	0.00500 ft/ft
Normal Depth	0.66 ft
Diameter	8.00 in

Results

Discharge	1.16 ft ³ /s
Flow Area	0.35 ft ²
Wetted Perimeter	1.96 ft
Hydraulic Radius	0.18 ft
Top Width	0.13 ft
Critical Depth	0.51 ft
Percent Full	99.0 %
Critical Slope	0.00624 ft/ft
Velocity	3.32 ft/s
Velocity Head	0.17 ft
Specific Energy	0.83 ft
Froude Number	0.36
Maximum Discharge	1.19 ft ³ /s
Discharge Full	1.11 ft ³ /s
Slope Full	0.00543 ft/ft
Flow Type	SubCritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.00 %
Normal Depth Over Rise	99.00 %
Downstream Velocity	Infinity ft/s

Worksheet for Circular Pipe - B3

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.010
Channel Slope	0.00500 ft/ft
Diameter	10.00 in
Discharge	1.61 ft ³ /s

Results

Normal Depth	0.56	ft
Flow Area	0.39	ft ²
Wetted Perimeter	1.61	ft
Hydraulic Radius	0.24	ft
Top Width	0.78	ft
Critical Depth	0.57	ft
Percent Full	67.6	%
Critical Slope	0.00487	ft/ft
Velocity	4.10	ft/s
Velocity Head	0.26	ft
Specific Energy	0.83	ft
Froude Number	1.02	
Maximum Discharge	2.17	ft ³ /s
Discharge Full	2.01	ft ³ /s
Slope Full	0.00320	ft/ft
Flow Type	SuperCritical	

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	67.60	%
Downstream Velocity	Infinity	ft/s

Worksheet for Circular Pipe - B4

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.010
Channel Slope	0.00700 ft/ft
Diameter	12.00 in
Discharge	3.94 ft ³ /s

Results

Normal Depth	0.84 ft
Flow Area	0.70 ft ²
Wetted Perimeter	2.31 ft
Hydraulic Radius	0.30 ft
Top Width	0.74 ft
Critical Depth	0.84 ft
Percent Full	83.6 %
Critical Slope	0.00691 ft/ft
Velocity	5.62 ft/s
Velocity Head	0.49 ft
Specific Energy	1.33 ft
Froude Number	1.02
Maximum Discharge	4.17 ft ³ /s
Discharge Full	3.87 ft ³ /s
Slope Full	0.00724 ft/ft
Flow Type	SuperCritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.00 %
Normal Depth Over Rise	83.57 %
Downstream Velocity	Infinity ft/s

Worksheet for Circular Pipe - B5

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.010
Channel Slope	0.01000 ft/ft
Diameter	12.00 in
Discharge	4.42 ft ³ /s

Results

Normal Depth	0.78 ft
Flow Area	0.66 ft ²
Wetted Perimeter	2.17 ft
Hydraulic Radius	0.30 ft
Top Width	0.83 ft
Critical Depth	0.88 ft
Percent Full	78.1 %
Critical Slope	0.00819 ft/ft
Velocity	6.71 ft/s
Velocity Head	0.70 ft
Specific Energy	1.48 ft
Froude Number	1.33
Maximum Discharge	4.98 ft ³ /s
Discharge Full	4.63 ft ³ /s
Slope Full	0.00911 ft/ft
Flow Type	SuperCritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.00 %
Normal Depth Over Rise	78.14 %
Downstream Velocity	Infinity ft/s

Worksheet for Circular Pipe - BASINS As+Bs TO POND #2

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	0.00500 ft/ft
Diameter	24.00 in
Discharge	8.98 ft ³ /s

Results

Normal Depth	1.07	ft
Flow Area	1.71	ft ²
Wetted Perimeter	3.29	ft
Hydraulic Radius	0.52	ft
Top Width	1.99	ft
Critical Depth	1.07	ft
Percent Full	53.6	%
Critical Slope	0.00503	ft/ft
Velocity	5.24	ft/s
Velocity Head	0.43	ft
Specific Energy	1.50	ft
Froude Number	1.00	
Maximum Discharge	17.21	ft ³ /s
Discharge Full	16.00	ft ³ /s
Slope Full	0.00158	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	53.58	%
Downstream Velocity	Infinity	ft/s

Worksheet for Circular Pipe - C1

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.010
Channel Slope	0.01000 ft/ft
Diameter	6.00 in
Discharge	0.26 ft ³ /s

Results

Normal Depth	0.21 ft
Flow Area	0.08 ft ²
Wetted Perimeter	0.70 ft
Hydraulic Radius	0.11 ft
Top Width	0.49 ft
Critical Depth	0.26 ft
Percent Full	41.2 %
Critical Slope	0.00463 ft/ft
Velocity	3.41 ft/s
Velocity Head	0.18 ft
Specific Energy	0.39 ft
Froude Number	1.52
Maximum Discharge	0.78 ft ³ /s
Discharge Full	0.73 ft ³ /s
Slope Full	0.00127 ft/ft
Flow Type	SuperCritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.00 %
Normal Depth Over Rise	41.23 %
Downstream Velocity	Infinity ft/s

Worksheet for Circular Pipe - C1

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	0.21	ft
Critical Depth	0.26	ft
Channel Slope	0.01000	ft/ft
Critical Slope	0.00463	ft/ft

Messages

Notes

Max Q from Pond #1 is 0.26 CFS per AHYMO.

Worksheet for Circular Pipe - C5

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.010
Channel Slope	0.01000 ft/ft
Diameter	8.00 in
Discharge	1.28 ft ³ /s

Results

Normal Depth	0.46	ft
Flow Area	0.26	ft ²
Wetted Perimeter	1.30	ft
Hydraulic Radius	0.20	ft
Top Width	0.62	ft
Critical Depth	0.53	ft
Percent Full	68.6	%
Critical Slope	0.00691	ft/ft
Velocity	5.01	ft/s
Velocity Head	0.39	ft
Specific Energy	0.85	ft
Froude Number	1.38	
Maximum Discharge	1.69	ft ³ /s
Discharge Full	1.57	ft ³ /s
Slope Full	0.00664	ft/ft
Flow Type	SuperCritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	68.62	%
Downstream Velocity	Infinity	ft/s

Worksheet for Circular Pipe - C6+C5+D1

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.010
Channel Slope	0.01000 ft/ft
Diameter	12.00 in
Discharge	2.63 ft ³ /s

Results

Normal Depth	0.54	ft
Flow Area	0.43	ft ²
Wetted Perimeter	1.65	ft
Hydraulic Radius	0.26	ft
Top Width	1.00	ft
Critical Depth	0.70	ft
Percent Full	54.0	%
Critical Slope	0.00468	ft/ft
Velocity	6.08	ft/s
Velocity Head	0.58	ft
Specific Energy	1.11	ft
Froude Number	1.63	
Maximum Discharge	4.98	ft ³ /s
Discharge Full	4.63	ft ³ /s
Slope Full	0.00322	ft/ft
Flow Type	SuperCritical	

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	53.96	%
Downstream Velocity	Infinity	ft/s

Worksheet for Circular Pipe - Pond 2 outlet

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.010
Channel Slope	0.01700 ft/ft
Diameter	18.00 in
Discharge	14.21 ft ³ /s

Results

Normal Depth	1.01 ft
Flow Area	1.27 ft ²
Wetted Perimeter	2.89 ft
Hydraulic Radius	0.44 ft
Top Width	1.40 ft
Critical Depth	1.39 ft
Percent Full	67.5 %
Critical Slope	0.00938 ft/ft
Velocity	11.19 ft/s
Velocity Head	1.95 ft
Specific Energy	2.96 ft
Froude Number	2.07
Maximum Discharge	19.15 ft ³ /s
Discharge Full	17.80 ft ³ /s
Slope Full	0.01083 ft/ft
Flow Type	SuperCritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.00 %
Normal Depth Over Rise	67.54 %
Downstream Velocity	Infinity ft/s

Worksheet for Circular Pipe - Pond 2 outlet

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	1.01	ft
Critical Depth	1.39	ft
Channel Slope	0.01700	ft/ft
Critical Slope	0.00938	ft/ft



ENVIROHOOD STRUCTURE

The Nyloplast® EnviroHood™ is an innovative stormwater management device attached to the inside of a catch basin or manhole designed to prevent the outflow of floating debris and oil.

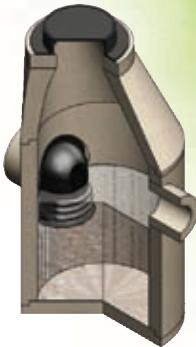
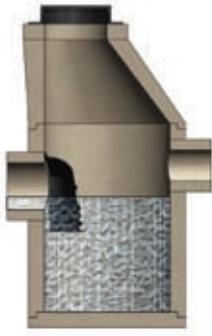
The need for cleaner stormwater has caused municipal leaders to demand forward-thinking solutions to improve their overall water quality. The EnviroHood offers lower installed costs and less intrusive installations than competitive devices.

ENGINEERED FOR OPTIMAL PERFORMANCE

The innovative design incorporates the same proven corrugation technology used on ADS N-12® pipe products. This delivers maximum strength to weight ratio and ensures the structure is capable of supporting the hydraulic forces of a rainfall event.

FEATURES & BENEFITS:

- Molded from High Density Polyethylene (HDPE) for lightweight and sturdy design
- Corrugated design eliminates flat surfaces and provides increased structural capacity
- Effective low-cost solution for storm water treatment
- Easy to clean
- Highly corrosion-resistant for long service life



ADS Service: ADS representatives are committed to providing you with the answers to all your questions, including specifications, installation and more.

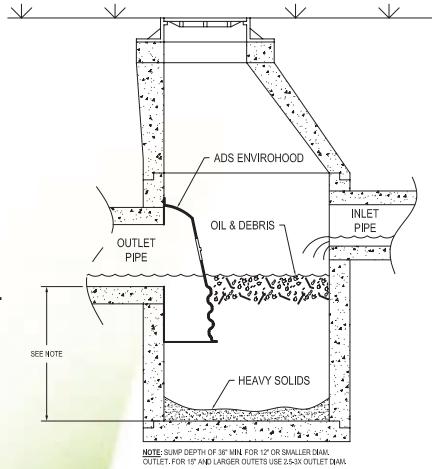
NYLOPLAST ENVIROHOOD SPECIFICATION

SCOPE

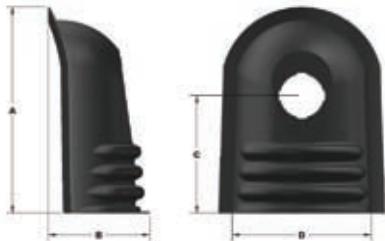
This specification describes the EnviroHood for use in stormwater conveyance systems.

REQUIREMENTS

- All hoods shall be constructed of polyethylene.
- The size and position of the hood shall be determined by the outlet pipe size as per manufacturer's recommendation.
- The bottom of the hood shall extend downward a minimum distance of 6" (15 cm) for pipes < 12" (30 cm).
- Installation hardware and instructions shall be provided by manufacturer.
- Installation shall be in accordance with Nyloplast installation procedures and those issued by local building/construction regulations.



TYPICAL INSTALLATION



STRUCTURE TYPE	OUTLET COVERED	PART NUMBER*	GENERAL DIMENSIONS in. (cm)			
			A	B	C	D
48" (120 cm) Round Concrete	up to 18" (45 cm)	5818AGR	30.2 (75)	14.9 (35)	17.2 (45)	20.5 (50)
48"-54" (120-135 cm) Round Concrete	up to 24" (60 cm)	5824AGR	41.7 (105)	18.0 (45)	26.9 (70)	26.9 (70)
54"-60" (135-150 cm) Round Concrete	up to 30" (75 cm)	5830AGR	48.7 (120)	20.5 (50)	30.5 (75)	33.1 (85)
Flat Concrete	up to 18" (45 cm)	5818AGF	30.2 (75)	11.8 (30)	17.2 (45)	20.4 (50)
Flat Concrete	up to 24" (60 cm)	5824AGF	41.8 (105)	15.3 (40)	26.9 (70)	27.0 (70)
Flat Concrete	up to 30" (75 cm)	5830AGF	48.8 (120)	18.3 (45)	30.5 (75)	34.0 (85)
18" (45 cm) Nyloplast	up to 12" (30 cm)	5818AG0412	19.4 (50)	9.8 (25)	12.3 (30)	13.8 (35)
24" (60 cm) Nyloplast	up to 15" (40 cm)	5824AG0415	26.5 (65)	12.8 (30)	14.5 (35)	20.0 (50)
30"(75 cm) Nyloplast	up to 18" (45 cm)	5830AG0418	32.8 (85)	15.4 (40)	18.7 (45)	26.0 (65)

*Includes installation hardware

For more information on EnviroHood and other ADS products, please contact our Customer Service Representatives at 1-800-821-6710

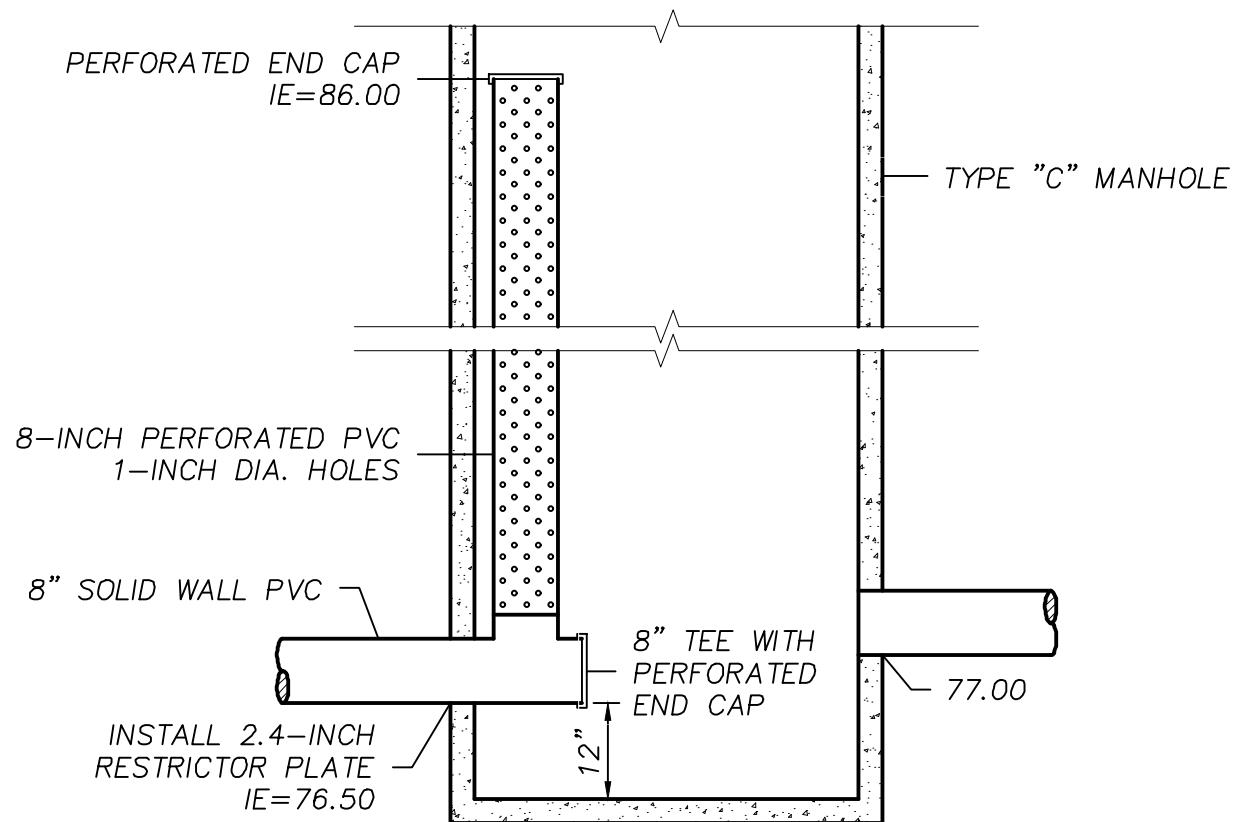
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UNDERGROUND STORAGE OUTLET MANHOLE DETAIL



CAPACITY OF SINGLE 'C' STORM DROP INLETS

Capacity of the grate:

$$\begin{aligned} L &= 47.375" - 2(6" \text{ ends}) - 14(1/2" \text{ middle bars}) \\ &= 28.375" \\ &= 2.365' \end{aligned}$$

$$\begin{aligned} W &= 30" - 13(1/2" \text{ middle bars}) \\ &= 23.5" \\ &= 1.958' \end{aligned}$$

$$\begin{aligned} \text{Area} &= 2.365' \times 1.958' \\ &= 4.63 \text{ ft}^2 \end{aligned}$$

$$\begin{aligned} \text{Effective Area} &= 4.63 - 4.63 (0.5 \text{ clogging factor}) \\ &= 2.3 \text{ ft}^2 \text{ at the grate} \end{aligned}$$

CHECK CAPACITY FOR MIN. H=0.10'

Orifice Equation

$$\begin{aligned} Q &= CA \sqrt{2gH} \\ Q &= 0.6 * 2.3 * \sqrt{2 * 32.2 * 0.10} \\ Q &= 3.50 \text{ cfs} \end{aligned}$$

Capacity of the throat:

$$\begin{aligned} L &= 47 - \frac{3}{8}" \\ &= 3.948' \end{aligned}$$

Weir Equation

$$\begin{aligned} Q &= CLH^{(3/2)} \\ Q &= 2.95 * 3.948 * 0.10^{(3/2)} \\ Q &= 0.37 \text{ cfs} \end{aligned}$$

Total Capacity (FOR MIN. H=0.10'):

$$\begin{aligned} Q &= 3.50_{\text{grate}} + 0.37_{\text{throat}} \\ \mathbf{Q = 3.87 \text{ cfs} = Q_{\text{available}}} \end{aligned}$$

Curb Inlet Area "A1" $Q_{\text{required}} = 1.57 \text{ cfs} < Q_{\text{available}}$, therefore **OK**.
Curb Inlet Area "A2" $Q_{\text{required}} = 2.99 \text{ cfs} < Q_{\text{available}}$, therefore **OK**.
Curb Inlet Area "C6" $Q_{\text{required}} = 1.35 \text{ cfs} < Q_{\text{available}}$, therefore **OK**.
Curb Inlet Area "D1" $Q_{\text{required}} = 0.47 \text{ cfs} < Q_{\text{available}}$, therefore **OK**.

CAPACITY OF SINGLE 'D' STORM GRATED INLETS

Capacity of the grate:

$$\begin{aligned} L &= 47.375" - 2(6" \text{ ends}) - 14(1/2" \text{ middle bars}) \\ &= 28.375" \\ &= 2.365' \end{aligned}$$

$$\begin{aligned} W &= 30" - 13(1/2" \text{ middle bars}) \\ &= 23.5" \\ &= 1.958' \end{aligned}$$

$$\begin{aligned} \text{Area} &= 2.365' \times 1.958' \\ &= 4.63 \text{ ft}^2 \end{aligned}$$

$$\begin{aligned} \text{Effective Area} &= 4.63 - 4.63 (0.5 \text{ clogging factor}) \\ &= 2.3 \text{ ft}^2 \text{ at the grate} \end{aligned}$$

CHECK CAPACITY FOR MIN. H=0.5'

Orifice Equation

$$\begin{aligned} Q &= CA \sqrt{2gH} \\ Q &= 0.6 * 2.3 * \sqrt{2 * 32.2 * 0.50} \\ Q &= 7.83 \text{ cfs} \end{aligned}$$

Grated Inlet Area "C4" $Q_{\text{required}} = 1.99 \text{ cfs} < Q_{\text{available}}$, therefore **OK**.
Curb Inlet Area "C6" $Q_{\text{required}} = 1.35 \text{ cfs} < Q_{\text{available}}$, therefore **OK**.