

CITY OF ALBUQUERQUE



Eugenio E. Valdez, P.E.
Wilson & Company, Inc.
4900 Lang Ave. NE
Albuquerque, NM 87109

**Re: Lincoln Complex, Building M Renovation
Drainage Report/Grading and Drainage Plan
Engineer's Stamp Date 7-31-2015 (K15/D047B)**

Dear Mr. Valdez,

Based upon the information provided in your submittal received 7/17/2015 and 8/3/2015, the above referenced report cannot be approved until the following comments are addressed:

- Please stamp the drainage report.
- Drainage report references flow numbers based on the 100yr/24hr storm. Please make sure all the flow calculations are based on the 100yr/6hr storm and volume calculations are based on the 100yr/24hr storm. The runoff calculations for the 100yr/6hr storm are using Type 2 Rainfall. Summary tables should indicate the 100yr/6hr storm for flows and 100yr/24hr storm for volumes.
- Provide an exhibit that clearly shows the pipe numbers and inlets number shown Table 4 & 5, Sheet 9 of the drainage report.
- First flush volume (0.34" x Impervious Area) must be provided for the new constructions and all the areas that are being reconstructed.
- Please provide all the sheets that are being referenced for details on the grading plans.
- An Erosion and Sediment Control Plan (ESC) submittal is also required for building permit approval. Please submit an ESC plan including a submittal sheet to Curtis Cherne for review and approval.

PO Box 1293

Albuquerque

New Mexico 87103

www.cabq.gov

If you have any questions, you can contact me at 924-3695.

Sincerely,

Shahab Biazar, P.E.
City Engineer, Planning Dept.
Development and Building Services

C: File

DRAINAGE REPORT FOR TRACTS A, B-1, AND C-1 SANDIA ADDITION

PREPARED FOR
SANDIA FOUNDATION

JULY 2015

Prepared By:

Floyd Development Services, LLC

918 Pinehurst Road

Rio Rancho, NM 87124

I, Hugh W. Floyd, hereby certify that I am a Registered Professional Engineer, registered in the State of New Mexico, and that the following report was prepared under my direction and is true and correct to the best of my knowledge and belief.



Hugh W. Floyd
NMPE # 16633

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I. INTRODUCTION

The purpose of this report is to maintain compliance with the City of Albuquerque's regulations and to design a more efficient ponding system so that Sandia Foundation can better utilize their remaining property (Tract C-1).

The site is located on the west side of San Mateo Boulevard in between Lincoln Road and Mcleod Road. The site is shaped like an L with the long side running east west, as shown on Sheet 1 of Exhibit 1. ABF Terminal, which used to be known as Navajo Freight Lines Terminal, is located on the west side of the site and wraps around the northwest corner. The Golden Corral restaurant (Tract A) is located north of the long side and east of the short side. There is a storage facility on the south side of the site. Davita's Del Norte Dialysis Center is in the process of developing on the east side of the property, between Golden Corral and the storage facility. Entitlement and Engineering Solutions, Inc. (EES) recently submitted a drainage report for the Davita site (Tract B-1) dated 5/5/2015 and that report is referenced in Appendix A.

II. BACKGROUND AND EXISTING CONDITIONS

For many years the area now occupied by Golden Corral, Davita's developing site, and the remaining Tract (C-1), was used as a garden nursery. The area has historically drained to the west through the Navajo Terminals. In 1974 an existing 42 in. storm drain was removed from the Navajo Terminals site due to the construction of a new storm drain on San Mateo Boulevard. At the same time Kruger, Lake and Associates prepared a report and plan set for a smaller storm drain system through the Navajo Terminals site. Their report and plans are shown in Appendix A.2. As can be seen in the Kruger drainage study, the intention was to accommodate free discharge from the nursery site. They calculated a runoff discharge of 21 cfs using a C factor of 0.6 for the nursery site. This discharge is collected in two soil cement swales that were constructed per the 1974 plan for the Navajo Terminal site and are still in existence. These swales have two inlets that ultimately tie into an 18" storm drain that runs through the ABF/Navajo Terminal property, as shown on the plan sheet found in Appendix A.2. Figure 1 shows the nursery in 2002 and displays the extent of the buildings and hardscape. It should be noted that the impervious area is comparable to a fully developed commercial site.

Currently the site is zoned C-3 and has a consistent slope to the west at about 3%. On the south side of the property there is a wall 1 to 3 feet in height, which prevents runoff from transferring between the storage facility and the existing site. The runoff from Tract C-1 and the Davita site (Tract B-1) flows into two ponds. One pond is located in the southwest corner of the existing site and the other is in the northwest corner. The Golden Corral (Tract A) site has part of the site, the building, draining to San Mateo, a small portion of the parking lot draining to the existing soil cement swale, and the remainder draining to the existing ponds. The ponds were built in 2013 under emergency conditions when two large storms occurred back to back. Prior to the construction of the emergency ponds, Tract C-1 had three makeshift ponds that neared full capacity during the second 2013 storm. According to the Engineer's Report by Isaacson and

Arfman dated 09/24/2013, located in Appendix A.3, the berms surrounding the makeshift ponds began to fail as the pond's water level approached the top. It is also noted in the Temporary Detention plan sheet dated 08/27/2013, found in Appendix A.3, that repairs were made to the western shotcrete channel. It is believed that repairs were necessary due to settlement, which allowed water to "pipe" under the shotcrete channel.

III. METHODOLOGY

The proposed and existing conditions are modeled using AHYMO and the 100 year, 24 hour storm event in accordance with chapter 22 of the Albuquerque Design Process Manual (DPM). The AHYMO data are found in Appendix B.

The water quality pond volume is calculated using the first 0.34 inches of runoff multiplied by the impervious area of the site. In this report the calculations for the water quality ponding includes Davita's developing site since their report specifies to use the existing pond for their first flush. Table 3 on Sheet 1 of Exhibit 1 shows the water quality volume calculations.

The downstream capacity of the ABF Terminals storm drains was analyzed using the orifice and Bernoulli equations based on the City of Albuquerque DPM, Section 22.3B. Appendix C contains the orifice calculations used to develop rating curves for each proposed pond outlet and ABF inlet. Table 1 from Sheet 1 of Exhibit 1 shows the combined outlet rating curves for the northern and southern pipe outlets. Appendix C contains the downstream analysis used to determine the best fit flowrate.

IV. PROPOSED CONDITIONS

In the past, the ABF/Navajo Terminal site was designed to receive 21 cfs from the garden nursery site. The calculations in Appendix C indicate that a flowrate of about 10 cfs lets water flow into the storm drain system without causing significant cross parking lot flow. This report recognizes that the design of the downstream storm drain system is undersized and that a large runoff rate produces flow over the paved areas. Due to the problems in 2013 and an attempt to limit flows to a level that can be contained in the existing storm drain, the discharge rate is reduced from 21 cfs to 10 cfs.

The proposed pond is located in the northwest corner of Tract C-1, and extends along the western border. In the northwest corner the pond is V-shaped and 4 feet deep with 3:1 side slopes. Along the western border the pond is only 2 feet deep with 3:1 side slopes and a flat bottom. The pond is designed to retain 3718 cubic feet of water within the lowest 2 foot depth to account for the first flush. The elevation range of the water quality pond is from 5192 feet to 5194 feet. The upper portion of the pond is detention and has an elevation range of 5194 feet to 5195.8 feet. There are two outlets that allow water to discharge into the ABF Terminal storm drain system. Both outlets have a 12 inch pipe which tie into the back of the ABF Terminal inlets, one on the north and the other to the south. The north outlet has an elevation 5194 feet, and the southern outlet elevation is 5193 feet. Surrounding the southern outlet is a weir with a

top elevation of 5194 feet. The weir is used to maintain a water quality volume and to allow additional head on the outlet so that more water enters the system sooner. Table 1 on Sheet 1 of Exhibit 1 shows the storage rating curve of the proposed pond. On the northwest corner there will be an emergency spillway with a top elevation of 5195.8 that extends to the south along the western border.

V. SUMMARY AND CONCLUSION

The plan outlined in this report provides a pond that retains the required first flush volume for Tract C-1 and Tract B-1, as well as providing detention ponding adequate to limit the total discharge to a maximum rate of 10 cfs rather than the previous allowed 21 cfs. If a storm larger than the design caused the spillway to become activated then water will flow into the soil cement channel as it has historically done.

additional head on the outlet so that more water enters the system sooner. Table 1 on Sheet 1 of Exhibit 1 shows the storage rating curve of the proposed pond. On the northwest corner there will be an emergency spillway with a top elevation of 5195.8 that extends to the south along the western border

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Sandia Foundation San Mateo Site

Figure 1



San Mateo Blvd NE

Figure 1
Garden Nursery 2002

**Sandia Foundation
San Mateo Site**

Sheet 1 of Exhibit 1

TABLE 1 - WATER QUALITY AND STORAGE POND RATING CURVE									
	Elev.	Area (sq. ft)	Vol (cu. ft)	Cum. (cu. ft)	Discharge N (cfs)	Discharge S outlet (cfs)	Emergency Spillway	Combined Discharge (cfs)	
Water Quality Pond	92	219.6	0.0	0.0	0.000	0.00	0.00	0.00	
	93	1708.5	964.1	964.1	0.022	0.00	0.00	0.00	
	94	3804.4	2766.5	3720.5	0.085	0.00	0.00	0.00	
	94.25	4556.0	1045.1	4765.6	0.109	1.89	1.69	0.00	3.58
	94.5	5276.1	1229.0	5994.6	0.138	2.67	4.63	0.00	7.30
	95	6766.8	3010.7	9005.3	0.207	3.78	5.00	0.00	8.78
	95.5	8242.9	3752.4	12757.7	0.293	4.63	5.00	0.00	9.63
Max. WS Elev.	95.79				0.352	4.84	5.00	0.00	9.84
	96	9771.4	4503.6	17261.3	0.396	5.00	5.00	37.60	10.00
	96.5	8462.1	4558.4	21819.7	0.501	5.00	5.00	245.00	10.00

TABLE 2 - TREATMENT TYPE PERCENTAGES					
Location	Area (Ac)	A	B	C	D
Tract A	2.506	0	0	5	95
Tract B-1	1.0455	0	5	15	80
Tract C-1	2.6442	0	12.5	12.5	75
Weighted Avg.	6.1957	0	10.4	9.9	83.9

TABLE 3 – WATER QUALITY VOLUME CALCULATIONS					
Location	Area (ft²)	%TTD	Area TTD	Runoff (in)	Volume (ft³)
Tract B-1	45541.8	80	36433.44	0.34	1032.3
Tract C-1	115180.3	75	86385.23	0.34	2447.6
				Total Vol. =	3479.9

SHOTCRETE CHANNEL CAPACITY ANALYSIS

Manning Formula:

Circular Channel
Input
Depth 0.5 ft
Slope 0.021 ft/ft
Manning's n 0.013
Diameter 36 in

Output
Flow 5.84 cfs
Flow Area 0.774 sf
Velocity 7.54 fps
Velocity Head 0.883 ft
Top Width 2.24 ft
Froude Number 2.26
Critical Depth 0.758 ft
Critical Slope 0.00391 ft/ft

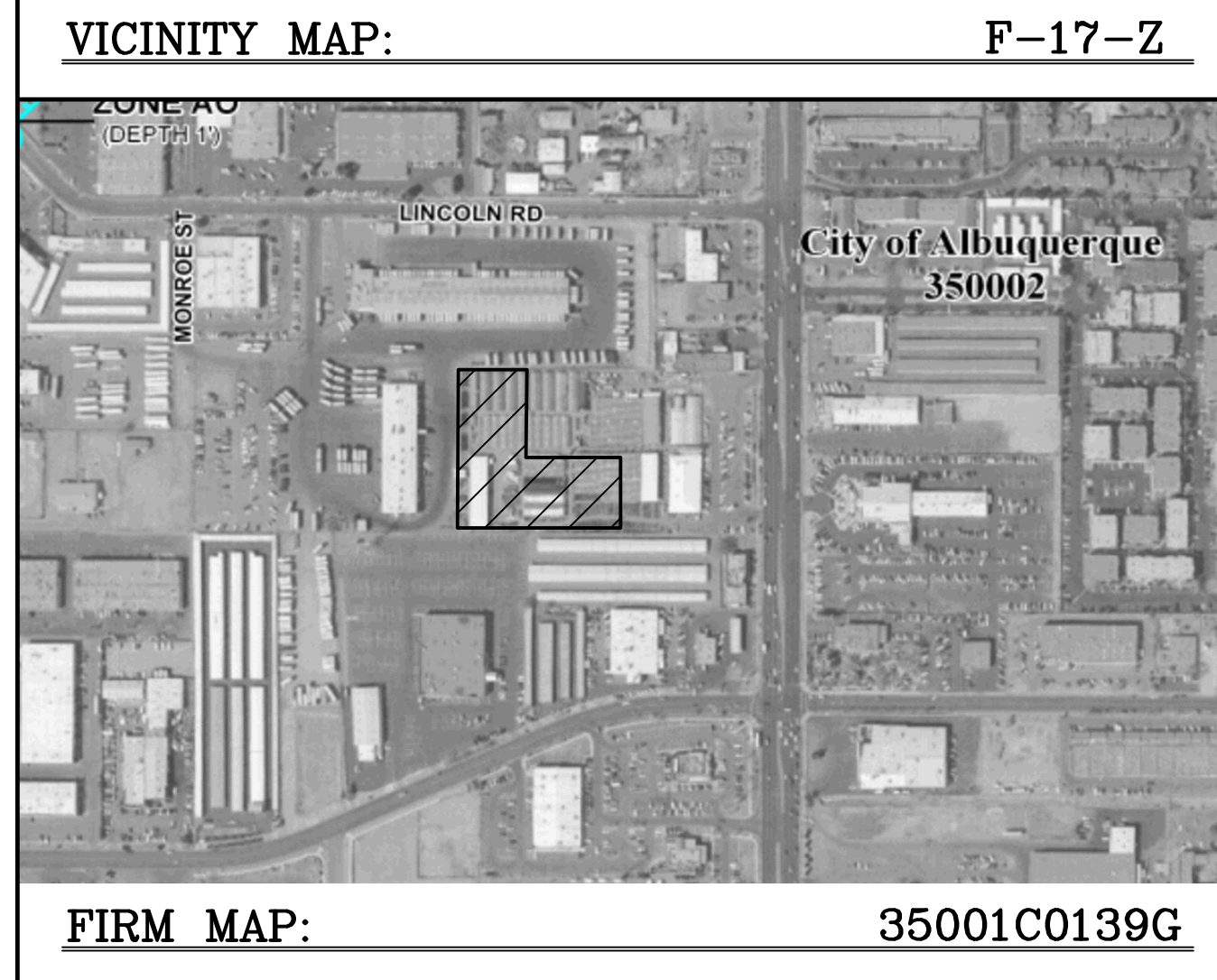
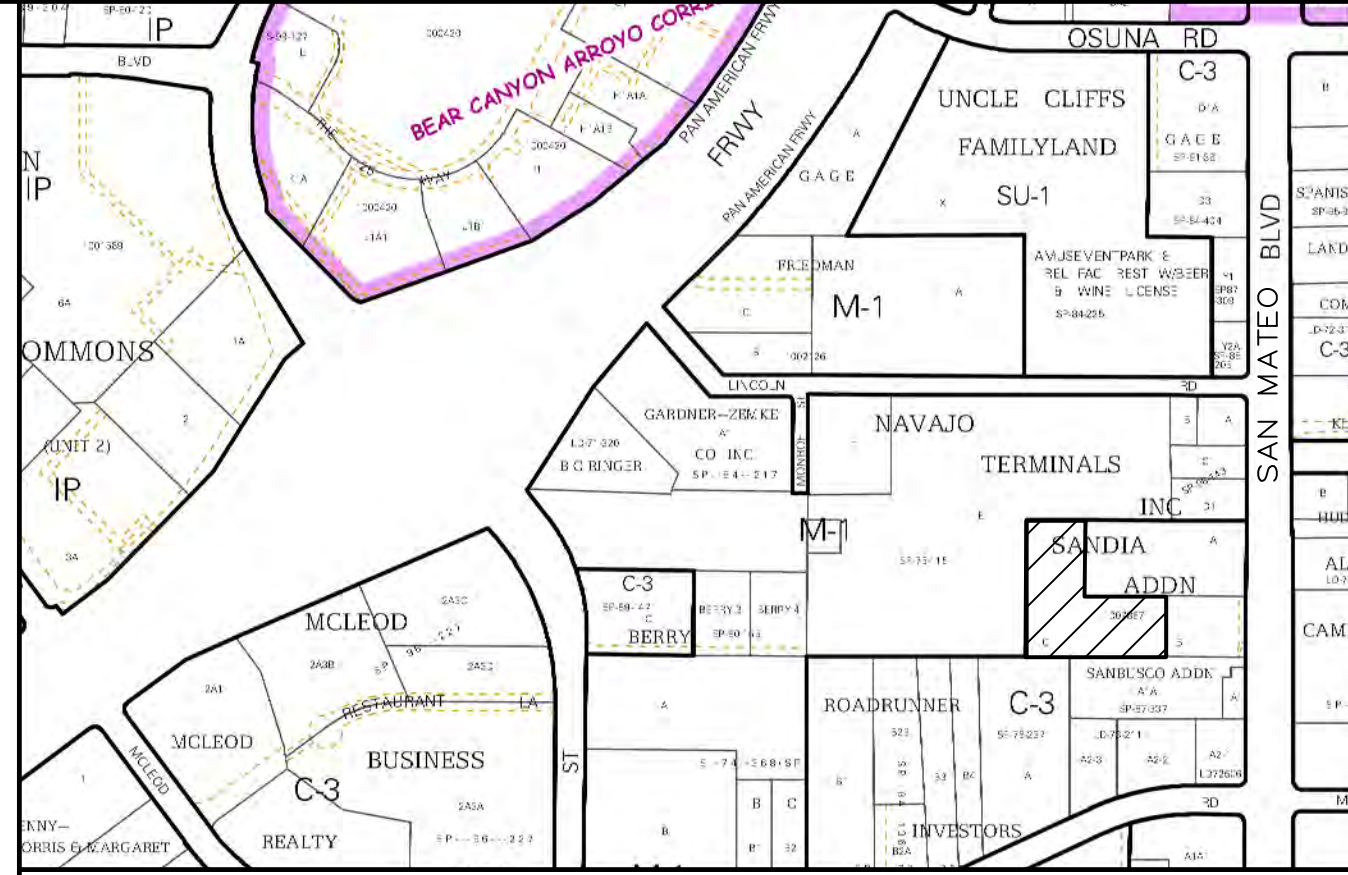
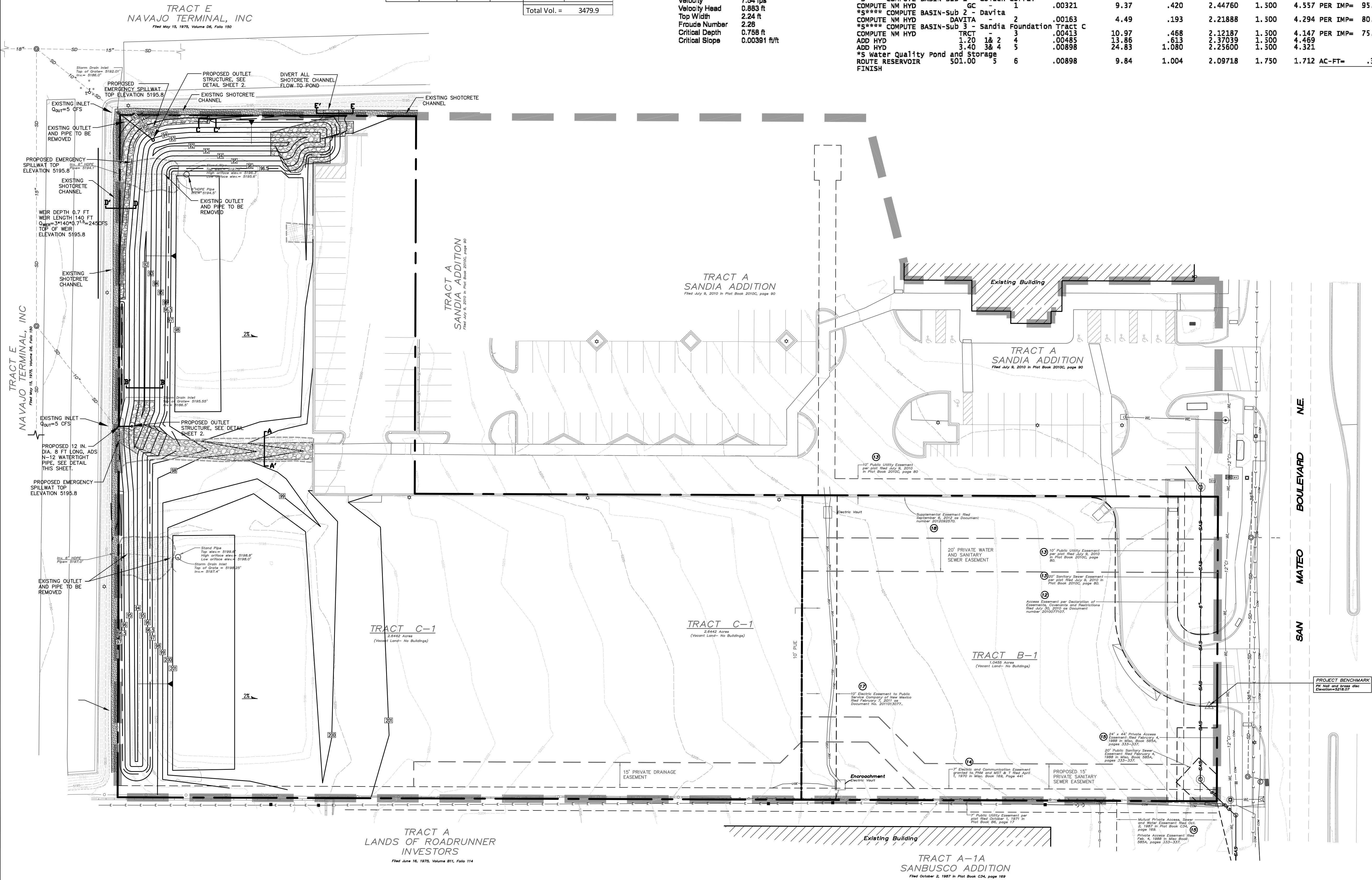
AHYMO SUMMARY RESULTS

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SF6.SUM - VERSION: 1997.02c

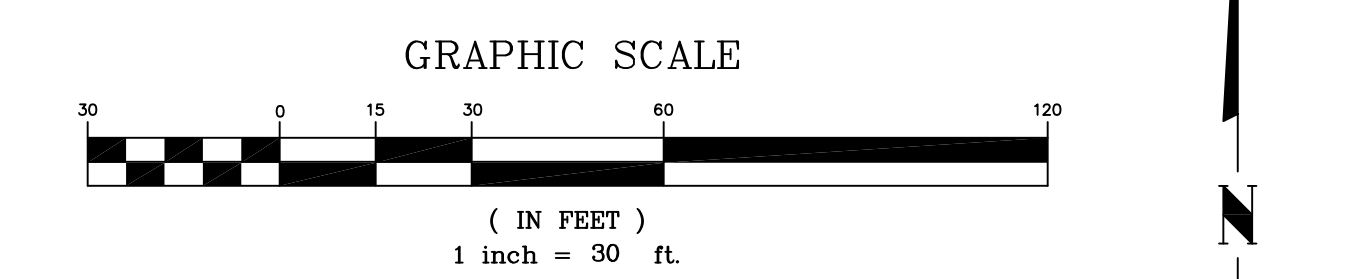
RUN DATE (MON/DAY/YR) =03/23/2008
USER NO. = AHYMO-C-9803c01UNMLIB-AH

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1	NOTATION
PROJECT NAME: Sandia Foundation, San Mateo Tract C											
JOB NO.											
DATE: June 2015											
RAINFALL TYPE= 2											RAIN24= 2.750
*SEDIMENT BULK CODE=1 FACTOR=1.06											
*S*** COMPUTE BASIN-Sub 1 - Golden Corral											
COMPUTE NM HYD GC 1 .00321 9.37 .420 2.44760 1.500 4.557 PER IMP= 95.00											
*S*** COMPUTE BASIN-Sub 2 - Davita 2 .00163 4.49 .193 2.21888 1.500 4.294 PER IMP= 80.00											
COMPUTE NM HYD DAVITA 2 .00163 4.49 .193 2.21888 1.500 4.294 PER IMP= 80.00											
*S*** COMPUTE BASIN-Sub 3 - Sandia Foundation TRACT C 3 .00413 10.97 .468 2.12187 1.500 4.147 PER IMP= 75.00											
COMPUTE NM HYD TRACT 3 .00413 10.97 .468 2.12187 1.500 4.147 PER IMP= 75.00											
ADD HYD 1.20 1& 2 4 .00485 13.86 .613 2.37039 1.500 4.469											
ADD HYD 3.40 3& 4 5 .00898 24.83 1.080 2.25600 1.500 4.321											
*S Water Quality Pond and Storage ROUTE RESERVOIR 501.00 5 6 .00898 9.84 1.004 2.09718 1.750 1.712 AC-FT= .352											
FINISH											



LEGAL DESCRIPTION:
TRACTS A, B-1, AND C-1
SANDIA ADDITION
CITY OF ALBUQUERQUE
BERNALILLO COUNTY, NEW MEXICO

LEGEND	
	PROPERTY BOUNDARY
	SUBBASIN BOUNDARY
	MAJOR CONTOURS PER SURV-TEK SURVEY 2015
	MINOR CONTOURS PER SURV-TEK SURVEY 2015
	PROPOSED POND CONTOURS



	TRACTS A, B-1, AND C-1 SANDIA ADDITION	DRAWN BY SMT
	EXHIBIT 1 DRAINAGE PLAN	DATE 07-28-15
	FLOYD DEVELOPMENT SERVICES, LLC DEVELOPMENT, ENGINEERING, & WATERSHED CONSULTING 918 PINEHURST RD SE, SUITE 102 RIO RANCHO, NM 87124 HUGH@DEVELOPNM.COM 505-366-4187	SHEET # 1 of 2
		JOB # 013-15-300

**Sandia Foundation
San Mateo Site**

Sheet 2 of Exhibit 1

Appendix A

Background Reports

Appendix A.1

Davita's Del Norte Dialysis Center Drainage Report

See DVD

Appendix A.2

Navajo Freight Lines Terminals Drainage Study

**A DRAINAGE STUDY
OF
NAVAJO FREIGHT LINES' TERMINAL SITE
AT
SAN MATEO AND LINCOLN ROAD, N. E.
ALBUQUERQUE, NEW MEXICO**

**Kruger, Lake and Associates
Architects and Engineers
601 San Pedro Dr. NE.
Albuquerque, New Mexico 87108**

Tel: 505 / 265-8452. -53

**December 29, 1973
(Revised January 29, 1974)**

I N D E X

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B.	Runoff Formulas	Page 1
C.	Runoff Calculations	Page 1
D.	Runoff Calculations After Construction	Page 1
E.	Runoff Calculations Prior to Construction	Page 1
F.	Conclusions	Page 2

Runoff Calculations:

A.	Flow in Arroyo Prior to Construction	Page 3
B.	Anticipated Flow in Arroyo After Construction	Page 3
C.	Flow onto Lincoln Rd., Prior to Construction	Page 4
D.	Flow onto Lincoln Rd., After Construction	Page 4

A DRAINAGE STUDY

NAVAJO FREIGHT LINES TERMINAL SITE San Mateo and Lincoln Road, N. E. Albuquerque, New Mexico

A. GENERAL INFORMATION

1. Legal Description: See Legal description on Plot Plan, (Exhibit "A").
2. Location: The area concerned in this study is bordered on the east by San Mateo Blvd. NE. and on the north by Lincoln Rd. NE.
3. Contributing Drainage Areas: Approximately 43 acres between San Pedro Dr., NE. and San Mateo Blvd., NE., contribute to the run-off through the subject property as indicated on the attached topo map, (Exhibit "B").
4. Arroyos: A small arroyo flows through the site covered by this study.
5. San Mateo Diversion Storm Sewer: The City of Albuquerque has designed a storm sewer along the west right-of-way of San Mateo to divert the arroyo flowing through this land to Bear Canyon Arroyo. This sewer will be constructed under the Cities Block-to-Block Contract. Navajo Freight Lines, Inc., is participating in the cost of this storm sewer.

B. RUNOFF FORMULA

Runoff quantities are calculated by the rational formula - $Q = C \cdot A$.

1. Coefficients (C):

a. Roofs	.95
b. Paved Areas	.90
c. Developed Residential Areas	.65
d. Nursery Areas	.60
e. Drive-In Theater (Paved and Gravel)	.80
f. Undeveloped Areas	.30

2. Intensity of Rainfall: ($i = 5.4''/\text{hr.}$)
Assume 10 minutes duration $i = \frac{189}{t + 25} = \frac{189}{10+25} = 5.4''/\text{hour.}$

$i = 5.4 \text{ in./hr}$

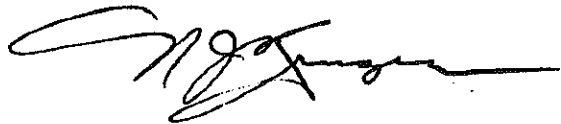
C. RUNOFF CALCULATIONS - See Sheets 3 and 4.

D. RUNOFF CALCULATIONS AFTER CONSTRUCTION are based on Project Site Plans - See Exhibit "A".

E. RUNOFF CALCULATIONS PRIOR TO CONSTRUCTION are based on a preliminary area topographical map prepared by Bohannon, Westman, Huston (See Exhibit "B").

F. CONCLUSIONS

1. The quantity of runoff flow in the arroyo at Point "B", the low point at the west end of the property has been reduced from 196.2 c.f.s., prior to construction, to 84.5 c.f.s. after construction is completed.
2. The quantity of flow on to Lincoln Road has been increased by only a fraction (.70 c.f.s.). When curb and gutter has been installed on San Mateo and a water stop constructed at San Mateo and Lincoln, the total flow in Lincoln Road will be less than at present.
3. We feel that all requirements of the 1972-2 AMAFCA Drainage Resolution have been met by our design.



N. J. Kruger, President
KRUGER, LAKE and ASSOCIATES
Architects and Engineers



RUN OFF CALCULATIONS

12-15-78 MJK

A. FLOW IN ARROYO PRIOR TO CONSTRUCTION

D. CLA

1. AT POINT "A" (OUTLET OF CULVERT)

WATER STOPPED AT 2ND INTERSECTION ON SAN PEDRO

AREA OF WATERSHED BETWEEN SAN PEDRO & SAN MATEO (EXHIBIT B)
FROM PRELIMINARY TOPO MAP BY BOHANNAN-WESMANN-HUSTON

DWELL	900 X 1000 =	900,000 / 43,500 =	20.6 A	C = .65
DOWN IN	100 X 150 =		15.25 A	C = .80
ON HIGHWAY	100 X 200		7.3 A	C = .80

$$Q_1 = 20.6 \times .65 \times 5.4 = 72.18 \text{ c.f.s.}$$

$$Q_2 = 15.25 \times .80 \times 5.4 = 66.0 \text{ c.f.s.}$$

$$Q_3 = 7.3 \times .80 \times 5.4 = 31.2 \text{ c.f.s.}$$

$$\text{TOTAL FLOW AT "A" = } 169.4 \text{ c.f.s.}$$

2. FLOW AT POINT "B"

SEE EXHIBIT B

NURSERY

700 ft x 400 ft

6.4 Ac

C = 0.60

NURSERY	700 X 400	280,000	6.4 A	C = .60
UNIMPROVED	340 X 370	125,800	2.85	
	250 X 350	87,500	2.20	
	200 X 450	90,000	2.98	
	250 X 250	62,500	2.18	
	250 X 200	50,000	2.10	
STREET	450 X 100	45,000	1.05 A	C = .75

FROM CULVERT PT "A" 1540 c.f.s.

$$Q_4 = 6.4 \times .60 \times 5.4 = 20.2 \text{ c.f.s.}$$

$$Q_5 = 12.14 \times .60 \times 5.4 = 39.2 \text{ c.f.s.}$$

$$Q_6 = 1.05 \times .90 \times 5.4 = 5.0 \text{ c.f.s.}$$

$$\text{TOTAL FLOW AT PT "B" = } 146.2 \text{ c.f.s.}$$

TOTAL FLOW IN ARROYO PRIOR TO CONSTRUCTION

B. ANTICIPATED FLOW IN ARROYO AFTER CONSTRUCTION

- ALL FLOW AT POINT "A" IS TO BE DIVERTED TO DEAR CANYON VIA NEW STORM SEWER ALONG SAN MATEO BY CITY OF ALBUQUERQUE

2. FLOW AT POINT "B"

NURSERY	700 X 400	280,000	6.4 A	C = .60
PAVED AREA	125 X 373	46,563		
	150 X 175	26,250		
	145 X 156	22,620		
	140 X 200	28,000		
	150 X 600	90,000	10.62 A	C = .90
	50 X 40	2,000		
	450 X 300	135,000		
	350 X 300	105,000		
	250 X 300	75,000		
	150 X 300	45,000		
	100 X 300	30,000		
UNIMPROVED	300 X 300	90,000	2.85 A	C = .80
	100 X 150	15,000		
ROAD	50 X 300	15,000	1.54 A	C = .90
	90 X 300	27,000		

Exhibit A of this drainage study shows this circled 1 in the same location as the old garden nursery.

89.50 cfs

21 cfs of the 89.5 cfs that goes into the Navajo Terminals storm drain system allowed to come from the garden nursery.

21.0 c.f.s.

TOTAL AVERAGE FLOW P1 B = 84.52 GPM @ 196.2 PSI

10	PAVED AREA	300x150	55,000	= 1.55 A.	C = 1.00
11	WOOD P 10.0 x 14.0		25,000	= .46 A.	C = .95

Q10	8.85	x	10	x	5.4	=	6.2
Q9	1.55	x	100	x	5.4	=	20.0
Q8	4664.95	x	5.4	=	2.4		

TOTAL FLOW ON TO LINCOLN ST. 16.6 CFS.

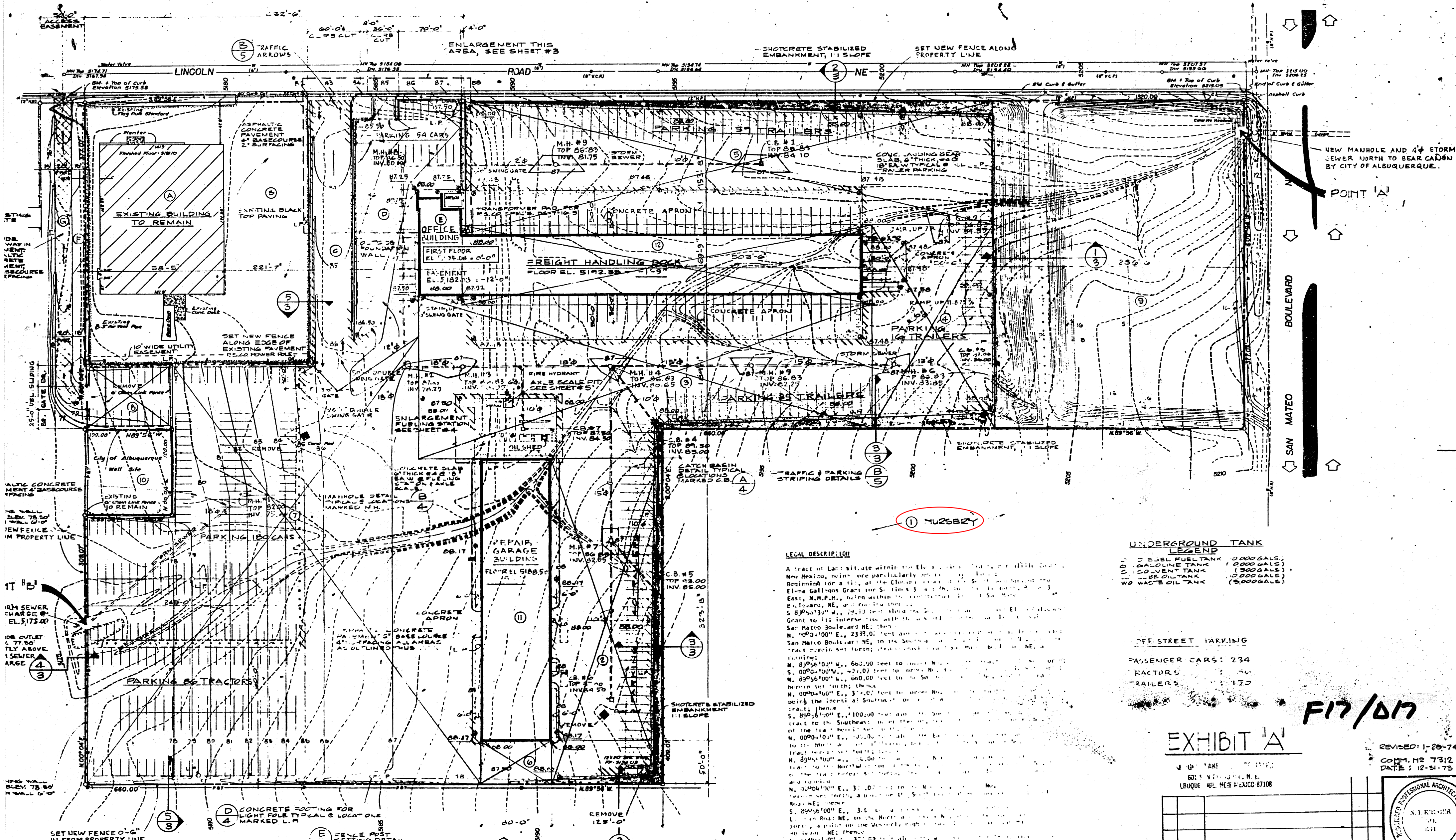
①	ROPS		466 A.
②	PAVED AREA		135 A.
③	✓	50 x 210	
④	✓	280 x 48	80 A.
	✓	30 x 110	
⑤	ROPS	6000 SE	178 A.
⑥	PAVED	20 x 350	16 A.
⑦	WIMP	30 x 350	142 A.

90	2		2.4
91	2		2.0
92	5	190 K. 40 x 5.4	4.8
93	2	170 K. 95 x 5.4	.9
94	2	16 K. 70 x 5.4	.8
95	3	242 K. 80 x 5.4	<u>.9</u>

TOTAL FLOW INTO LINCOLN = 17.3 cfs > 16.6 by 10 cfs. OK

Navajo Freight Lines Terminals Drainage Study

Plan Sheet Exhibit A



- NEW MANHOLE AND 4" STORM
SEWER NORTH TO BEAR CANYON
BY CITY OF ALBUQUERQUE.

POINT 1

 SAN MATEO · BOULEVARD

LEGAL DESCRIPTION

A tract of Land Situate within the El Paso County, State of New Mexico, being more particularly described as follows: Beginning for a 1/4 of the Clinton Grant of the Santa Fe and Santa Elena Gallons Grant of Sections 3 and 4, Township 20 N. R. 3 E., N.M.P.M., being within the same tract of the San Mateo Boulevard, NE, and running thence

N. 89°55'30" W. 29.12 feet along the San Mateo Boulevard NE to its intersection with the San Mateo Boulevard NE, thence

S. 100°41'00" E. 2339.07 feet along the San Mateo Boulevard NE to the Southwest corner of the tract herein set forth; thence about 1/4 of the San Mateo Boulevard NE, running:

N. 89°55'30" W. 662.90 feet to corner No. 1, thence

S. 00°06'10" W. 43.07 feet to corner No. 2, thence

N. 89°55'30" W. 662.90 feet to the San Mateo Boulevard NE, being set forth thence

N. 00°06'10" E. 37.07 feet to corner No. 3, thence

being the line of the Southwest corner of the tract herein set forth; thence

N. 89°55'30" E. 100.00 feet along the San Mateo Boulevard NE to the Southwest corner of the tract herein set forth; thence

N. 00°06'10" E. 435.90 feet along the El Paso and Santa Elena Gallons Grant of Sections 3 and 4, Township 20 N. R. 3 E., N.M.P.M., being set forth thence

N. 89°55'30" W. 662.90 feet to corner No. 4, thence

thence to the Northwest corner of the tract herein set forth; thence

about 1/4 of the San Mateo Boulevard NE, running:

N. 00°06'10" E. 37.07 feet to corner No. 5, thence

being set forth; a point on the Southwest corner of the

Road NE; thence

S. 89°56'10" W. 3.00 feet to corner No. 6, thence

to corner No. 7, thence

to corner No. 8, thence

S. 100°41'00" E. 37.07 feet to corner No. 9, thence

San Mateo Boulevard NE, to the Southwest corner of the tract herein set forth;

UNDERGROUND TANK
LEGEND

10	DIESEL FUEL TANK	(0000 GALS.)
11	GASOLINE TANK	(0000 GALS.)
12	SO-VENT TANK	(0000 GALS.)
13	BE-OIL TANK	(0000 GALS.)
14	WASTE OIL TANK	(0000 GALS.)

OFF STREET PARKING

PASSENGER CARS: 234

TRACTORS : 56

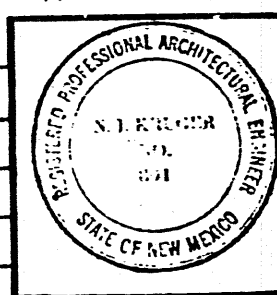
TRAILERS : 170

F17/Δ17

EXHIBIT "A"

REVISED: 1-20-74
COMM. NO 7312
DATE: 12-31-73

601 S. VICTOR ST. N. E.
 ALBUQUE. N. M. NEW MEXICO 87108

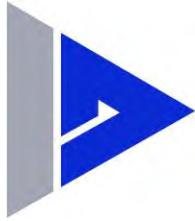
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For Information Only

200436

Appendix A.3

Isaacson and Arfman Engineer's Report



ENGINEER'S REPORT

Project: Sandia Foundation; San Mateo - Rowlands Tract Sept. 24, 2013
Owner: Sandia Foundation
Subject: Storm Water Flooding

Major Storm Event:

On September 12, 2013 Albuquerque experienced the start of a three-day major storm event where 3.65 inches of rain fell in the approximate area of the subject Sandia Foundation (SF) site. This event was preceded by a rain on Sept 10th which dropped 1.04 inches of rain thereby saturating the soil at the site (Photo #1). A total rainfall amount of 5.07 inches was measured at the Albuquerque Weather Services Station located at Montgomery Blvd. and San Mateo Blvd. for this time period.

Site Visit (09-12-13):

Karen Hudson (SF representative) contacted Fred Arfman (FA) with Isaacson & Arfman PA to perform a site visit to assess the condition of the existing storm water containment berms as a follow up to a meeting with Zack Lacombe, Manager of the ABF Freight Lines Terminal, the property west of the SF site. The following observations and actions were undertaken:

- FA arrived on site at approximately 10:45 AM and located Zack and Payam Ghoreishi (PG), an earthwork contractor, observing the storm waters from the Golden Corral and the undeveloped SF property entering into the three existing makeshift ponds between the SF property and ABF.
- The ponds were partially full from the earlier rains and were reaching full capacity from the morning rains.
- Zack was very concerned that the ponds would fail causing the stored rainwater to flow onto the ABF site forcing him to close down the terminal's shops and effectively crippling the terminal's productivity.
- PG called his office to get his personnel to the site to immediately begin work on reinforcing the makeshift berms. At this time Zack left the site. Laborers with shovels

arrived approximately 30 minutes later. It was before noon and the rains had started to let up after a storm duration of two hours.

- The ponds storm water levels reached the top of the berms and the interior berm between the middle pond and the north pond breached causing the water level in the north pond to rise (Photo #3). Payam and his laborers were directed to the pending breach point to reinforce the low point in the berm (Photo #2), now equal to the water level.
- PG and his laborers were then directed to the south end of the west berm of the middle pond. A controlled overflow outlet was excavated (Photo #5) to allow the captured storm waters to safely discharge into the ABF drainage rundown along the westerly property line of the SF property. Since the middle and north ponds were now connected, this outlet slowly relieved the pressure on both ponds.
- As soon as the outlet was conveying storm waters, it was noticed that the north berm of the southerly pond was breaching. Immediately, all those present worked to stop the breach by reconstructing the berm and placing rock from the adjacent rundown on the berm to fill in the breach. The breach was plugged (Photo #7).
- A backhoe from PG Enterprises arrived to fortify all of the areas that were compromised and then to stabilize the entire berm system (Photo #4).
- Two large capacity mobile pumps were placed at the NE corner of the north berm to drain the storm waters directly into the storm drain inlet on the ABF property (Photo #6).

Site Monitoring (09-13-13 through 09-16-13):

- The property was monitored by the personnel of PG Enterprises through the night and over the next four days (Photo #8).
- The ponds were continually drained of the captured storm waters and the berms inspected and maintained.

Conclusion:

- None of the ponded storm waters from the Sandia Foundation property entered onto the ABF facility other than at the drainage rundown and storm drain inlets constructed for this purpose.

- The ponds were continually drained from additional rains in order to keep the berms and the underlying earth from becoming overly saturated and prone for collapsing. As of 09-24-13, the areas are still too saturated to allow for reconstruction.



1: SEPTEMBER 10 - PRESTORM CONDITIONS



2: SEPTEMBER 12 - MANUAL FORTIFICATION OF BERMS



3: BREACH OF MIDDLE POND



4: FORTIFICATION OF BERMS – SOUTH POND



5: HAND EXCAVATED CONTROLLED RELEASE OUTLET



6: PUMP DISCHARGE TO EXISTING ABF INLET



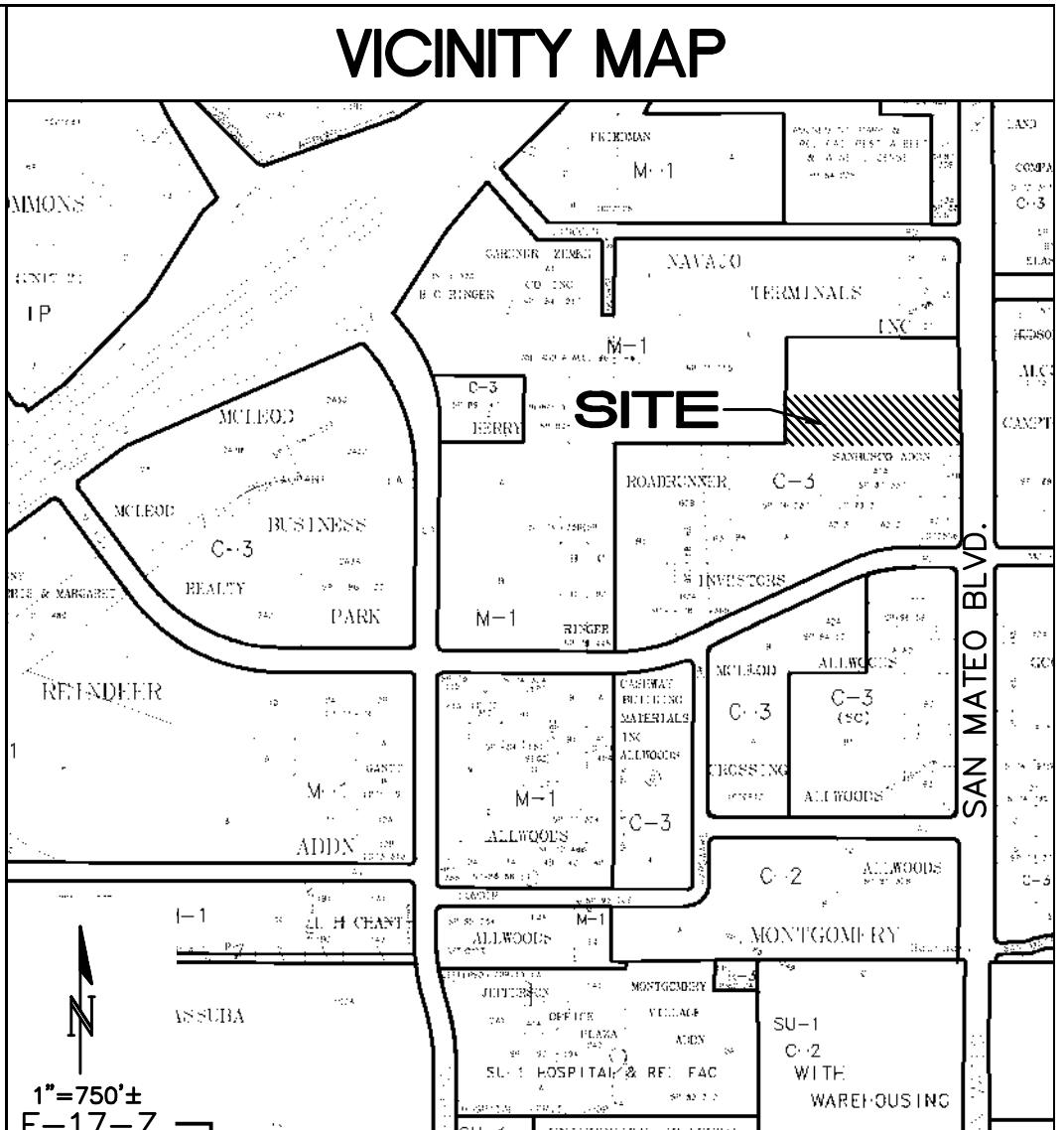
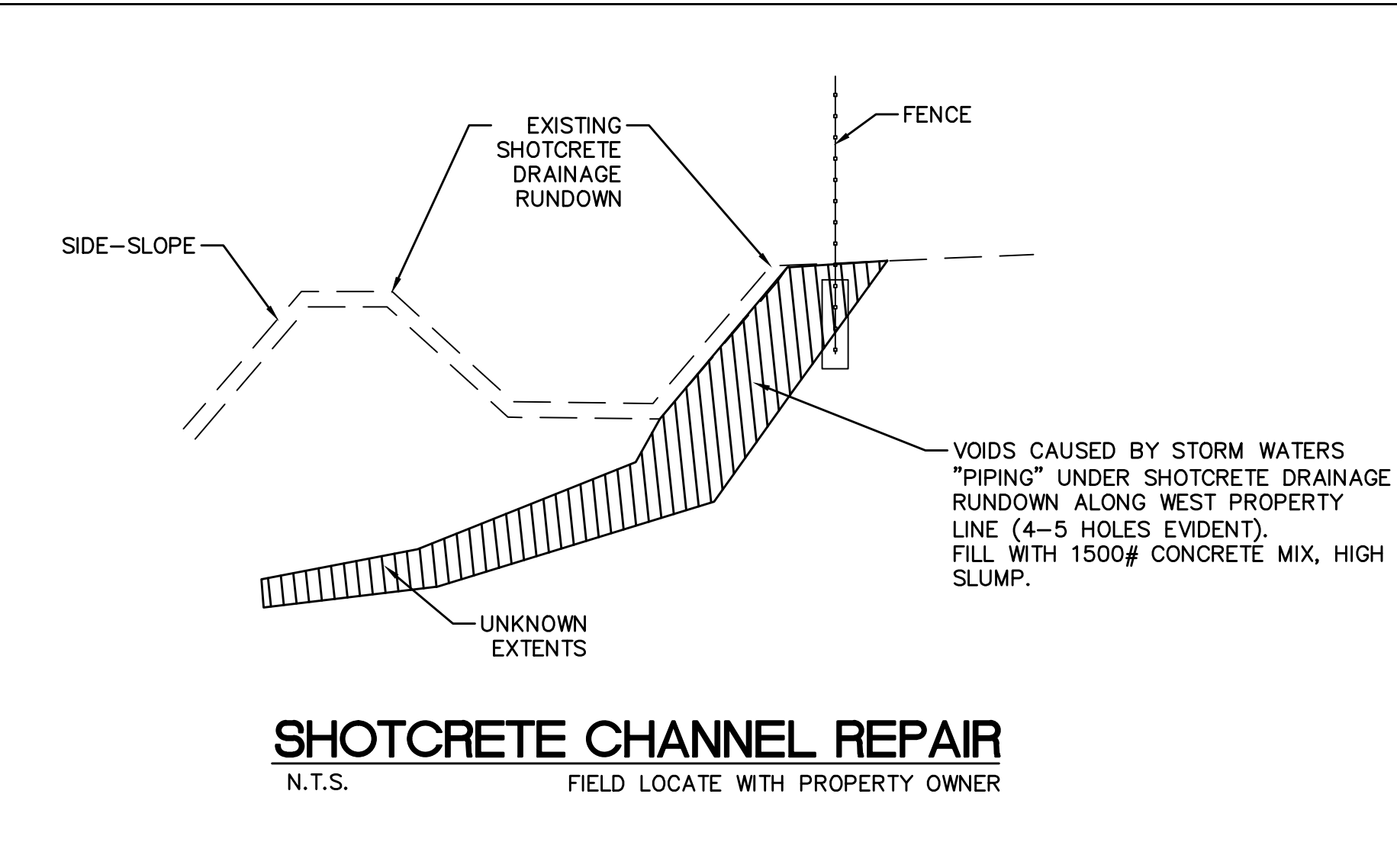
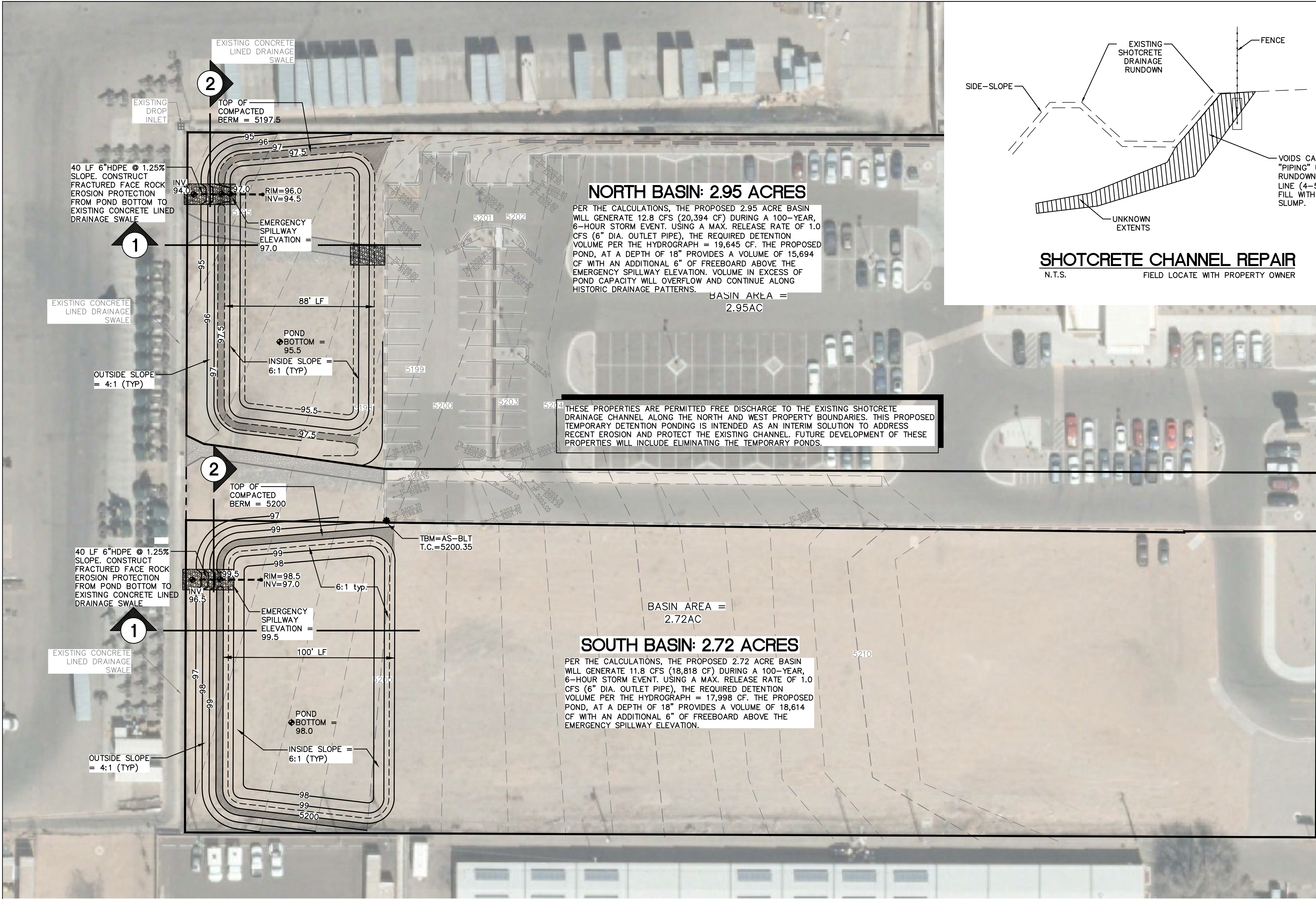
7: SOUTH POND OVERFLOW TO EXISTING RUNDOWN



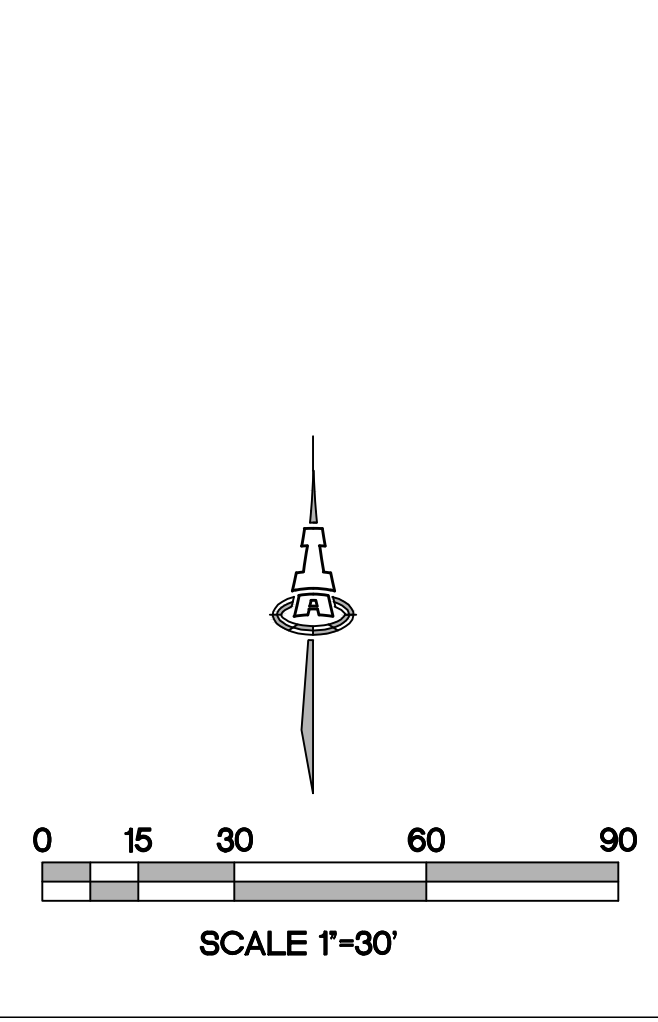
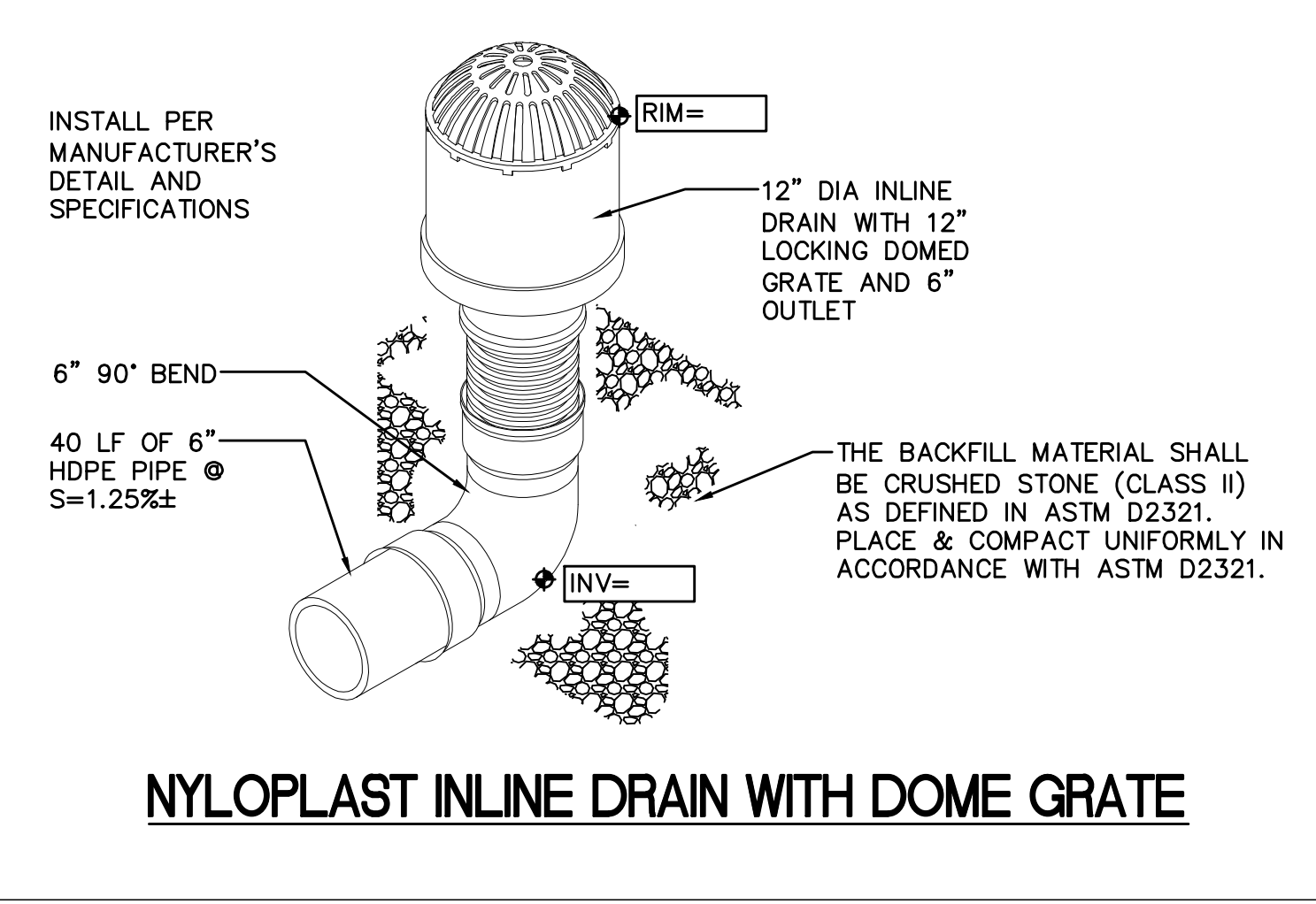
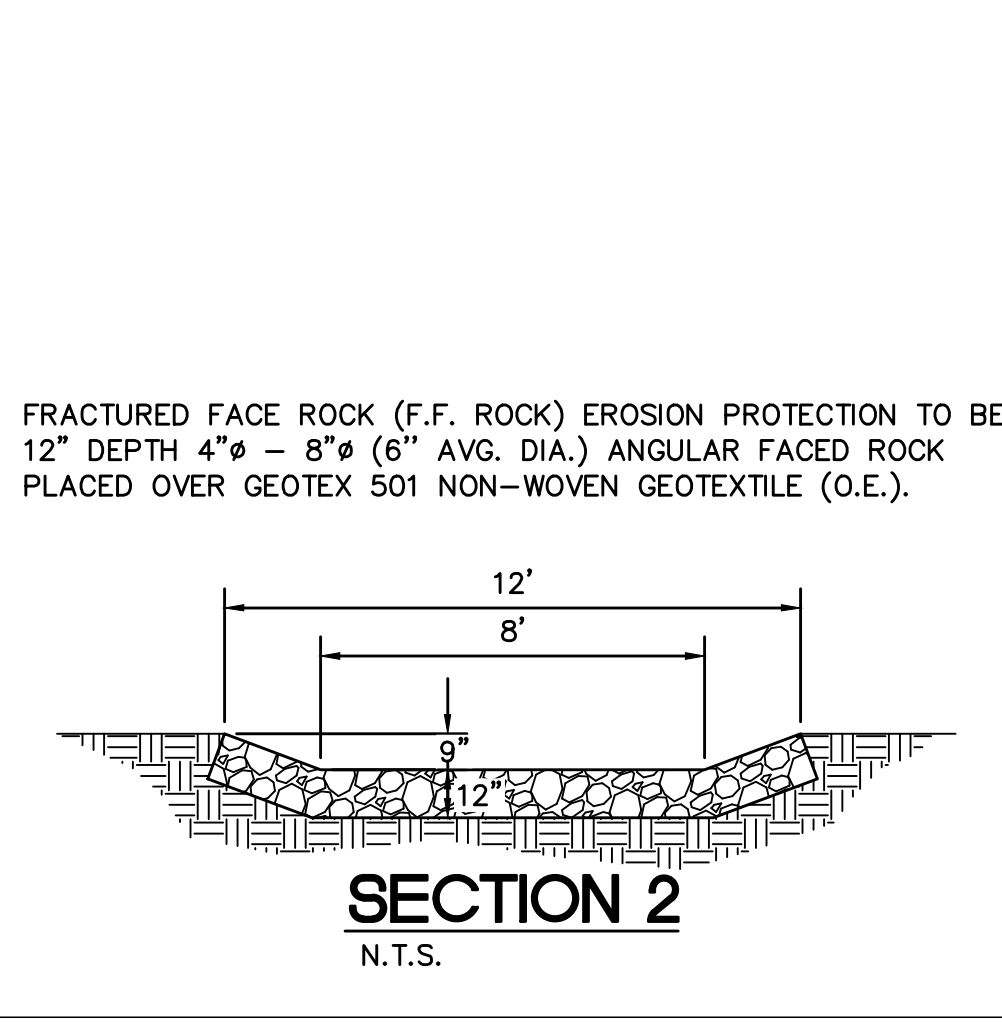
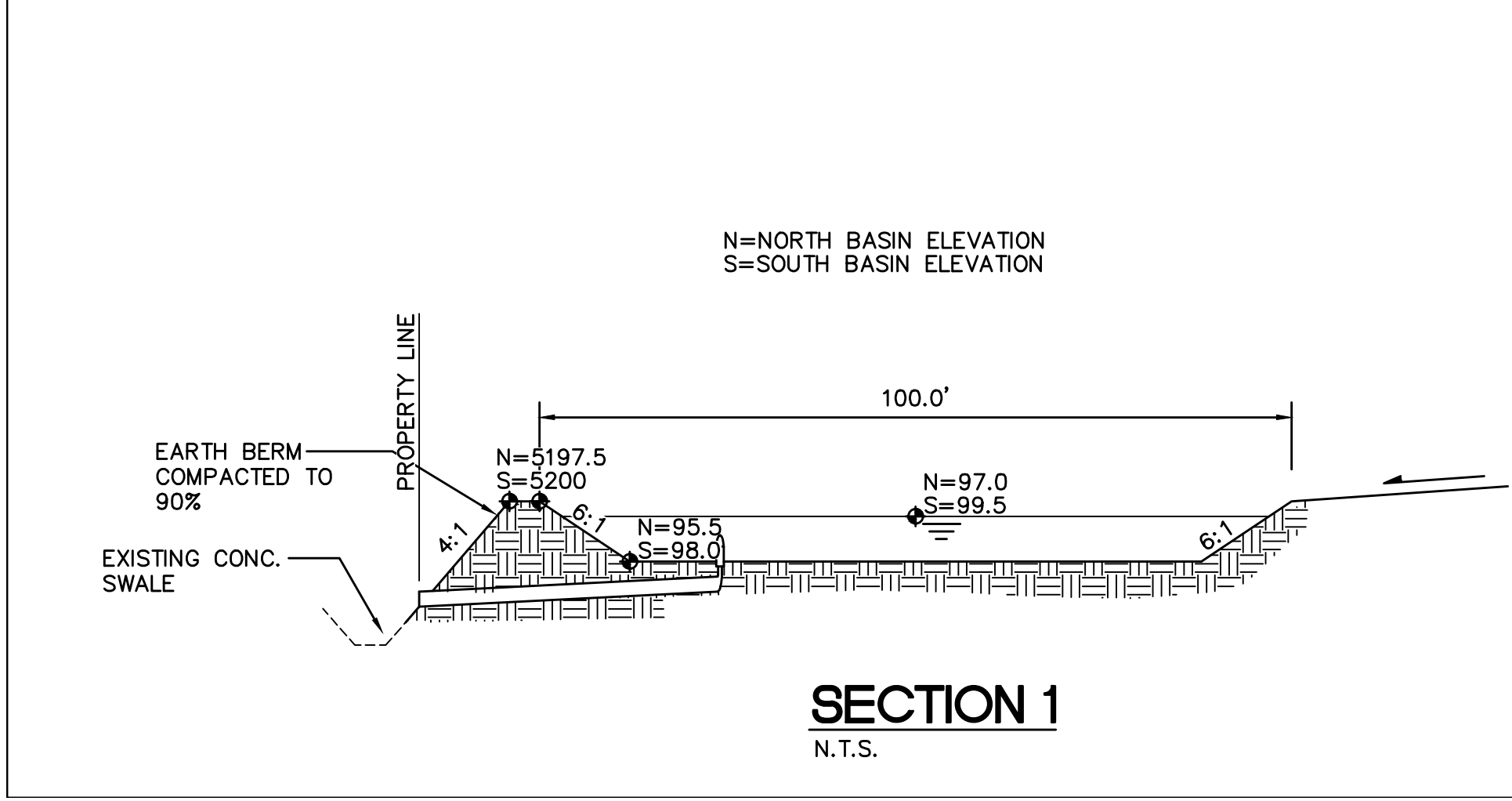
8: POST STORM WATER LEVEL WITH PUMPING

Isaacson And Arfman Engineer's Report

Temporary Detention Plan Sheet



PROJECT DATA	
LEGAL DESCRIPTION: TRACTS A, B AND C, SANDIA ADDITION, ALBUQUERQUE, BERNALILLO COUNTY, NM	
ADDRESS:	5207 SAN MATEO BLVD. 87108
SITE AREA:	6.0± ACRES
FLOOD_ZONE:	PER BERNALILLO COUNTY FIRM MAP #35001C0139G, THE SITE IS LOCATED WITHIN FLOODZONE 'X' DESIGNATED AS AREAS DETERMINED TO BE OUTSIDE 500-YEAR FLOODPLAIN.
ENGINEER:	FRED C. ARFMAN, PE ISAACSON & ARFMAN, P.A. 128 MONROE ST NE, ABQ, NM 87108 PHONE: (505) 268-8828
BENCHMARK:	BASED ON THE DRAINAGE & GRADING PLAN SUBMITTED FOR GOLDEN CORRAL RESTAURANT STAMP DATE 6-1-10 WHICH WAS USED TO MASS GRADE THIS PROPERTY, BENCHMARK USED WAS NM 367-1, A BRASS TABLET STAMPED "NM-367-1" SET IN TOP OF A CONCRETE POST FLUSH WITH THE GROUND LOCATED IN THE NORTH SAN MATEO MEDIAN AT THE INTERSECTION WITH OSUNA RD. ELEVATION = 5213.212 (NAVD 1988)
GENERAL NOTES	
A.	FINAL GRADES SHOWN REPRESENT TOP OF FINISH MATERIAL (I.E. TOP OF CONCRETE, TOP OF CONCRETE BUILDING PAD, TOP OF PAVEMENT MATERIAL, TOP OF LANDSCAPING MATERIAL, ETC.). CONTRACTOR SHALL GRADE, COMPACT SUBGRADE AND DETERMINE EARTHWORK ESTIMATES BASED ON ELEVATIONS SHOWN MINUS FINISH MATERIAL THICKNESSES.
B.	EXISTING UTILITY LINES ARE SHOWN IN AN APPROXIMATE MANNER ONLY AND MAY BE INCOMPLETE OR OBSOLETE. SUCH LINES MAY OR MAY NOT EXIST WHERE SHOWN OR NOT SHOWN. CONTRACTOR SHALL CONTACT NM-811 FOR UTILITY LINE SPOTS TWO WORKING DAYS PRIOR TO CONDUCTING SITE FIELD WORK. CONTRACTOR SHALL FIELD VERIFY AND LOCATE ALL UTILITIES PRIOR TO COMMENCEMENT OF ANY CONSTRUCTION. CONTRACTOR IS FULLY RESPONSIBLE FOR ANY AND ALL DAMAGE CAUSED BY ITS FAILURE TO LOCATE, IDENTIFY AND PRESERVE ANY AND ALL EXISTING UTILITIES, PIPELINES, AND UNDERGROUND UTILITY LINES.
C.	ENGINEER RECOMMENDS THAT OWNER MAINTAIN EROSION PROTECTION ELEMENTS. ENGINEER RECOMMENDS THAT OWNER INSPECT SITE YEARLY AND AFTER EACH RAINFALL TO IDENTIFY NEW AREAS OF EROSION AND INSTALL ADDITIONAL EROSION PROTECTION AS NEEDED BASED ON ACTUAL OCCURRENCES.



ISAACSON & ARFMAN, P.A. Consulting Engineering Associates 128 Monroe Street N.E. Albuquerque, New Mexico 87108 Ph. 505-268-8828 www.iacivil.com 1895 CG-101.dwg Aug 28, 2013			
This design, calculations, and concepts are owned by and remain the property of Isaacson & Arfman, P.A. and no part thereof shall be utilized by any person, firm or corporation for any purpose whatsoever except with the written permission of Isaacson & Arfman, P.A. ©			
5207 SAN MATEO ALBUQUERQUE, NM SANDIA FOUNDATION			
TEMPORARY DETENTION			
Date: 08-27-13	No. 13	Revised	Date: 1985
Drawn By: BJB			CG-101
Chd By: FCA			SH. OF

M:\CAD FILES\1800-1899\1895\dwg\1895 CG-101.dwg Layout1 8/29/2013 9:03:45 AM

Appendix B

Hydrology

Sandia Foundation San Mateo Site

AHYMO Input File

S PROJECT NAME: Sandia Foundation, San Mateo Tract C
 S JOB NO.
 S DATE: June 2015
 S
 S INPUT FILE NAME: SF-SanMateo.hym
 S OUTPUT FILE NAME: SF-SanMateo.out
 S FILES LOCATION: 56-07-02 Floyd Development Services\Active Projects\ENG\AHYMO\SF-SanMateo
 S
 S
 S

 S

*
 *
 * 100 year storm event
 RAINFALL TYPE=2 RAIN QUARTER=0.0 RAIN ONE=2.01
 RAIN SIX=2.35 RAIN DAY=2.75 DT=.05
 *

*SEDIMENT BULK CODE=1 FACTOR=1.06
 *
 *
 *

*S**** COMPUTE BASIN-Sub 1 - Golden Corral
 COMPUTE NM HYD ID=1 HYD NO=GC DA=0.003214
 PER A=0 PER B=0 PER C=5 PER D=95
 TP=0.133 RAIN=-1
 PRINT HYD ID=1 CODE=10
 *
 *
 *

*S**** COMPUTE BASIN-Sub 2 - Davita
 COMPUTE NM HYD ID=2 HYD NO=DAVITA DA=0.001634
 PER A=0 PER B=5 PER C=15 PER D=80
 TP=0.133 RAIN=-1
 PRINT HYD ID=2 CODE=10
 *
 *
 *

*S**** COMPUTE BASIN-Sub 3 - Sandia Foundation Tract C
 COMPUTE NM HYD ID=3 HYD NO=TRCT C DA=0.004132
 PER A=0 PER B=12.5 PER C=12.5 PER D=75
 TP=0.133 RAIN=-1
 PRINT HYD ID=3 CODE=10
 *
 *
 *

ADD HYD ID=4 HYD=1.2 ID I=1 ID II=2
 PRINT HYD ID=4 CODE=10
 *
 *

ADD HYD ID=5 HYD=3.4 ID I=3 ID II=4
 PRINT HYD ID=5 CODE=0
 *
 *
 *

*S Water Quality Pond and Storage
 ROUTE RESERVOIR ID=6 HYD=501 INFLOW ID=5 CODE=1

OUTFLOW(CFS)	STORAGE(AC FT)	ELEV(FT)
0.0	0.0	5192
0.01	0.022	5193
0.02	0.085	5194
3.5775	0.109	5194.25
7.301	0.138	5194.5
8.78	0.207	5195
9.629	0.293	5195.5
10.0	0.396	5196

 *
 *
 *

FINISH

Sandia Foundation San Mateo Site

AHYMO Summary File

SF6. SUM

AHYMO PROGRAM SUMMARY TABLE (AHYMO_97) -
INPUT FILE = SF6. hym

- VERSION: 1997.02c

RUN DATE (MON/DAY/YR) =03/23/2008
USER NO. = AHYMO-C-9803c01UNMLIB-AH

COMMAND	IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =
---------	----------------	-------------	-----------	--------------	----------------------	-----------------------	-----------------	----------------------	--------------	--------

S PROJECT NAME: Sandia Foundation, San Mateo Tract C
S JOB NO.
S DATE: June 2015

S INPUT FILE NAME: SF-SanMateo.hym
S OUTPUT FILE NAME: SF-SanMateo.out
S 56-07-02 Floyd Development Services\Active Projects\ENG\AHYM

RAINFALL TYPE= 2	CODE=1	FACTOR=1.06							RAIN24=	2.750
*SEDIMENT BULK	BASIN-Sub 1 - Golden Corral									
*S*** COMPUTE	GC - 1			.00321	9.37	.420	2.44760	1.500	4.557 PER IMP=	95.00
COMPUTE NM HYD										
*S*** COMPUTE	BASIN-Sub 2 - Davita			.00163	4.49	.193	2.21888	1.500	4.294 PER IMP=	80.00
COMPUTE NM HYD	DAVITA -									
*S*** COMPUTE	BASIN-Sub 3 - Sandia Foundation			.00413	10.97	.468	2.12187	1.500	4.147 PER IMP=	75.00
COMPUTE NM HYD	TRCT -									
ADD HYD	1.20 1& 2			.00485	13.86	.613	2.37039	1.500	4.469	
ADD HYD	3.40 3& 4			.00898	24.83	1.080	2.25600	1.500	4.321	
*S Water Quality Pond and Storage										
ROUTE RESERVOIR	501.00 5			.00898	9.84	1.004	2.09718	1.750	1.712 AC-FT=	.352
FINISH										

Appendix C

Hydraulics

Sandia Foundation San Mateo Site

Existing Downstream Capacity Analysis

Downstream Capacity

Analysis of existing ABF Terminal storm drain system

Elevations, lengths, and MH #s per Exhibit A of the Navajo Freight Lines Terminal Drainage Study revision dated 1/29/74 by Kruger, LAKE and ASSOCIATES Architects and Engineers.

The following MathCAD sheets are used to determine the downstream capacity by evaluating the hydraulic gradeline for a given flowrate. The equations used are from the City of Albuquerque Development Process Manual (DPM) Chapter 22, section 3B.

Point 1 is located at the Northern inlet, point 2 is located at MH #4

10 " diameter pipe leading from inlet to first manhole downstream

$$L := 91$$

$$Dia := 0.8333 \quad \text{ft}$$

$$Z_1 := 5185$$

$$R := \frac{Dia}{2} = 0.417 \quad \text{ft}$$

$$Z_2 := 5180.65$$

$$A := \pi \cdot R^2 = 0.545 \quad \text{ft}^2$$

$$S_0 := \frac{(Z_1 - Z_2)}{L} = 0.048$$

$$Q := 5 \quad \text{cfs}$$

$$n := 0.013$$

D2 represents the hydraulic gradeline at point 2. Assuming water elevation is half foot higher than top of MH #4.

$$P_w := \pi \cdot \left(\frac{Dia}{2} \right) \cdot 2 = 2.618 \quad \text{ft} \quad \text{Assuming full pipe, therefore the circumference is used as the wetted perimeter}$$

$$D_2 := 6.68$$

$$R_h := \frac{A}{P_w} = 0.208 \quad \text{ft}$$

$$S_f := \left[\frac{(Q \cdot n)}{1.486 A \cdot R_h^{\left(\frac{2}{3}\right)}} \right]^2 = 0.052$$

D1 represents the calculated difference between top of water elevation and invert. Assuming grate at northern inlet is covered to create more pressure.

$$D_1 := D_2 - S_0 \cdot L + S_f \cdot L = 7.07$$

Difference between top of proposed pond and invert at northern inlet = 10 ft

Sandia Foundation San Mateo Site

Calculations for the Existing ABF Terminals Inlet Rating Curves

Calculations for ABF inlet
rating curves

Analysis for 10" outlet pipes from inlets

Existing Northern Inlet

$$\text{AreaOrif} := 0.5454 \quad (\text{ft})$$

$$C1 := 0.6 \quad j := 0..8$$

h :=

Elevation	h north (ft)
5186	0
5187	0.5833
5188	1.5833
5189	2.5833
5190	3.5833
5191	4.5833
5192	5.5833
5193	6.5833

$$Q_{\max} := \text{AreaOrif} \cdot C1 \cdot \sqrt{2 \cdot 32.2 \cdot h}$$

$$Q_{\max} = \begin{pmatrix} 0 \\ 2.006 \\ 3.304 \\ 4.221 \\ 4.971 \\ 5.622 \\ 6.205 \\ 6.738 \end{pmatrix}$$

Existing Southern Inlet

$$\text{AreaOrif} := 0.5454 \quad (\text{ft})$$

$$C1 := 0.6 \quad j := 0..8$$

h1 :=

Elevation	h north (ft)
5186	0
5187	0.0833
5188	1.0833
5189	2.0833
5190	3.0833
5191	4.0833
5192	5.0833
5193	6.0833

$$Q_{\max 1} := \text{AreaOrif} \cdot C1 \cdot \sqrt{2 \cdot 32.2 \cdot h1}$$

$$Q_{\max 1} = \begin{pmatrix} 0 \\ 0.758 \\ 2.733 \\ 3.79 \\ 4.611 \\ 5.307 \\ 5.921 \\ 6.477 \end{pmatrix}$$

Sandia Foundation San Mateo Site

Calculations for the Proposed Pond Outlet Rating Curves

Calculations for proposed pond outlet rating curves

From pond to northern ABF Terminal inlet, through a 12 in. pipe

h :=

Elevation	Head (ft)
5194	0
5194.25	0.25
5194.5	0.5
5195	1
5195.5	1.5
5196	2

h1 := 1 ft
h2 := 2 ft

Weir Opening, $Q = C_w L H^{1.5}$

$C_w := 3$

$L := 7.9$

$$Q1 := C_w \cdot L \cdot (h1)^{1.5} = 23.7 \text{ cfs}$$

$$Q2 := C_w \cdot L \cdot (h2)^{1.5} = 67.034 \text{ cfs}$$

Orifice Opening, $Q_{orif} = C A (2GH)^{0.5}$

$C := 0.6$

$A := 0.785$

$$Q_{orif1} := C \cdot A \cdot (2 \cdot 32.2 \cdot h1)^{0.5} = 3.78 \text{ cfs}$$

$$Q_{orif2} := C \cdot A \cdot (2 \cdot 32.2 \cdot h2)^{0.5} = 5.345 \text{ cfs}$$

$$Q_{weir} := C_w \cdot L \cdot (h)^{1.5} = \begin{pmatrix} 0 \\ 2.963 \\ 8.379 \\ 23.7 \\ 43.54 \\ 67.034 \end{pmatrix}$$

$$Q_{orif} := C \cdot A \cdot (2 \cdot 32.2 \cdot h)^{0.5} = \begin{pmatrix} 0 \\ 1.89 \\ 2.673 \\ 3.78 \\ 4.629 \\ 5.345 \end{pmatrix}$$

Since the orifice equation produces smaller flowrates it is used rather than the weir equation for the 12 inch outlet pipes that lead to the ABF Terminal inlets.

Calculations for proposed pond outlet rating curves

From pond to southern ABF Terminal inlet, through a 12 in. pipe

$$\begin{pmatrix} h_{\text{weir}} \\ h_{\text{orifice}} \end{pmatrix} :=$$

Elevation	Wier Head (ft)	Orifice Head (ft)
5194	0	1
5194.25	0.25	1.25
5194.5	0.5	1.5
5194.75	0.75	1.75
5195	1	2

Calculations for weir surrounding
southern 12 inch pipe outlet.

Weir Opening, $Q = C_w L H^{1.5}$

$$\begin{aligned} C_w &:= 3 \\ L &:= 4.5 \end{aligned}$$

Orifice Opening, $Q_{\text{orif}} = C A (2GH)^{0.5}$

$$\begin{aligned} C &:= 0.6 \\ A &:= 0.785 \end{aligned}$$

$$Q_{\text{weir}} := C_w \cdot L \cdot (h_{\text{weir}})^{1.5} = \begin{pmatrix} 0 \\ 1.6875 \\ 4.77297 \\ 8.76851 \\ 13.5 \end{pmatrix}$$

$$Q_{\text{orif}} := C \cdot A \cdot (2 \cdot 32.2 \cdot h_{\text{orifice}})^{0.5} = \begin{pmatrix} 3.78 \\ 4.226 \\ 4.629 \\ 5 \\ 5.345 \end{pmatrix}$$

Weir controls flowrate up until water level reaches 5194.5 ft.

Sandia Foundation San Mateo Site

Minimum Slope Calculations for Proposed 12" Pipe

Manning Formula:

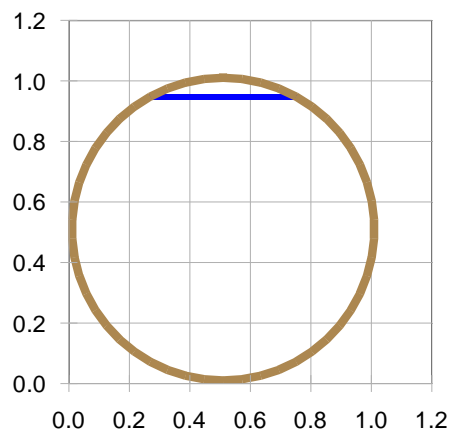
Circular Channel

Input

Flow	5 cfs
Slope	0.017022223 ft/ft
Manning's n	0.013
Diameter	12 in

Output

Depth	0.938 ft
Flow Area	0.765 sf
Velocity	6.53 fps
Velocity Head	0.664 ft
Top Width	0.482 ft
Froude Number	0.915
Critical Depth	0.917 ft
Critical Slope	0.0171 ft/ft



Sandia Foundation San Mateo Site

Rundown and Spillway Calculations

Rundown Calculations

According to the drainage report from Davita's Del Norte Dialysis Center the flowrate coming into the pond on the northern entrance is about 5.5 cfs.

Weir Depth

$$h1 := 1 \text{ ft}$$

Weir Equation: $Q = CwLH^{1.5}$

$$Cw := 3$$

$$L1 := 7.5$$

$$Q1 := Cw \cdot L1 \cdot (h1)^{1.5} = 22.5 \text{ cfs}$$

A total of about 24.8 cfs enters the pond, about 19.33 cfs enters the pond at the midway rundown

Midway Rundown

Weir Depth

$$h2 := 1 \text{ ft}$$

Weir Equation: $Q = CwLH^{1.5}$

$$Cw := 3$$

$$L2 := 14$$

$$Q1 := Cw \cdot L2 \cdot (h2)^{1.5} = 42 \text{ cfs}$$

Spillway calculations

Northwest Corner Spillway

Weir Depth

$$h3 := 0.7 \text{ ft}$$

Weir Equation: $Q = CwLH^{1.5}$

$$Cw := 3$$

$$L3 := 140$$

$$Q1 := Cw \cdot L3 \cdot (h3)^{1.5} = 245.97 \text{ cfs}$$

Midway Spillway

Weir Depth

$$h4 := 0.7 \text{ ft}$$

Weir Equation: $Q = CwLH^{1.5}$

$$Cw := 3$$

$$L4 := 8.5$$

$$Q1 := Cw \cdot L4 \cdot (h4)^{1.5} = 14.934 \text{ cfs}$$