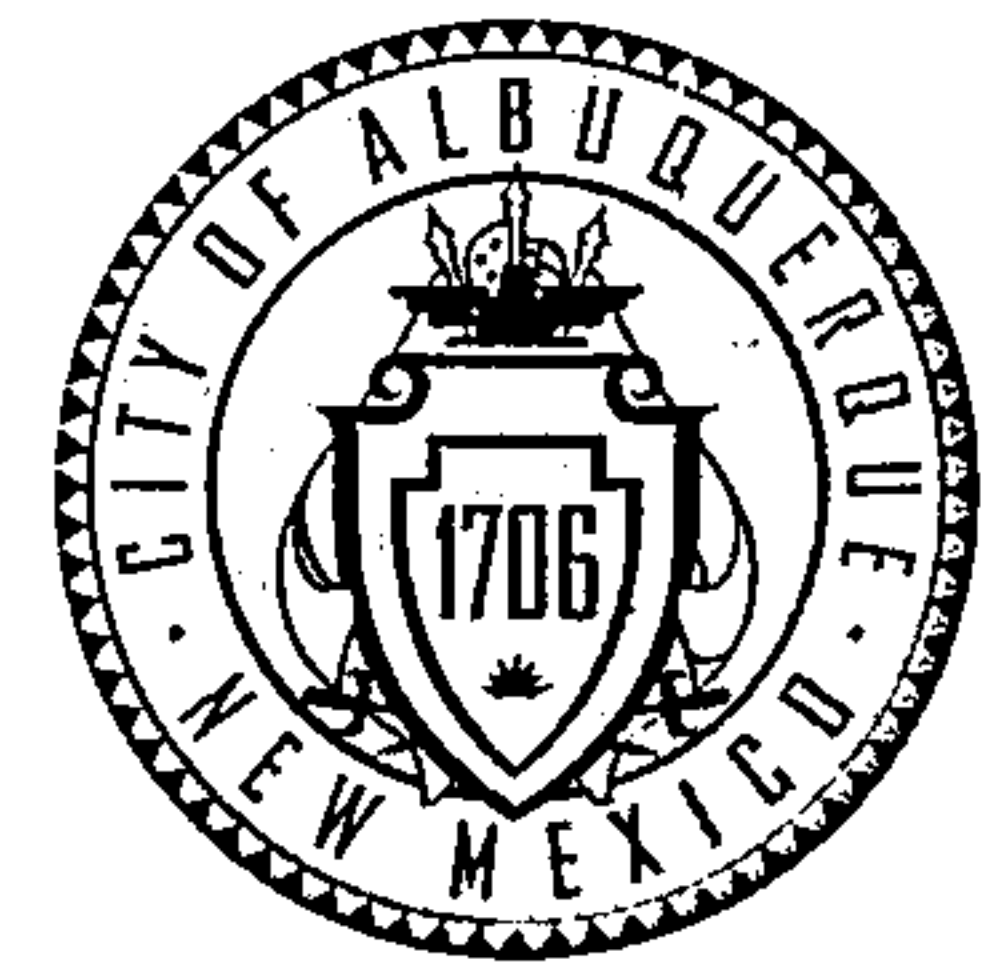


# CITY OF ALBUQUERQUE



November 13, 2015

Hugh Floyd, PE  
Floyd Development Services, LLC  
918 Pinehurst Rd. Suite 101  
Rio Rancho, NM 87124

RE: **Sandia Addition (F17D095B)**  
**Tracts A, B-1 and C-1**  
**Pond Certification - Accepted**  
**Engineer Stamp Date: 8/18/15**

Dear Mr. Floyd,

Based upon the information provided in your submittal received 11/12/2015, the above referenced Certification is acceptable for building permit.

If you have any questions, you can contact me at 924-3986 or Totten Elliott at 924-3982.

PO Box 1293

Albuquerque

NM 87103

Sincerely,

Shahab Biazar, P.E.  
City Engineer, Planning Dept.  
Development Review Services

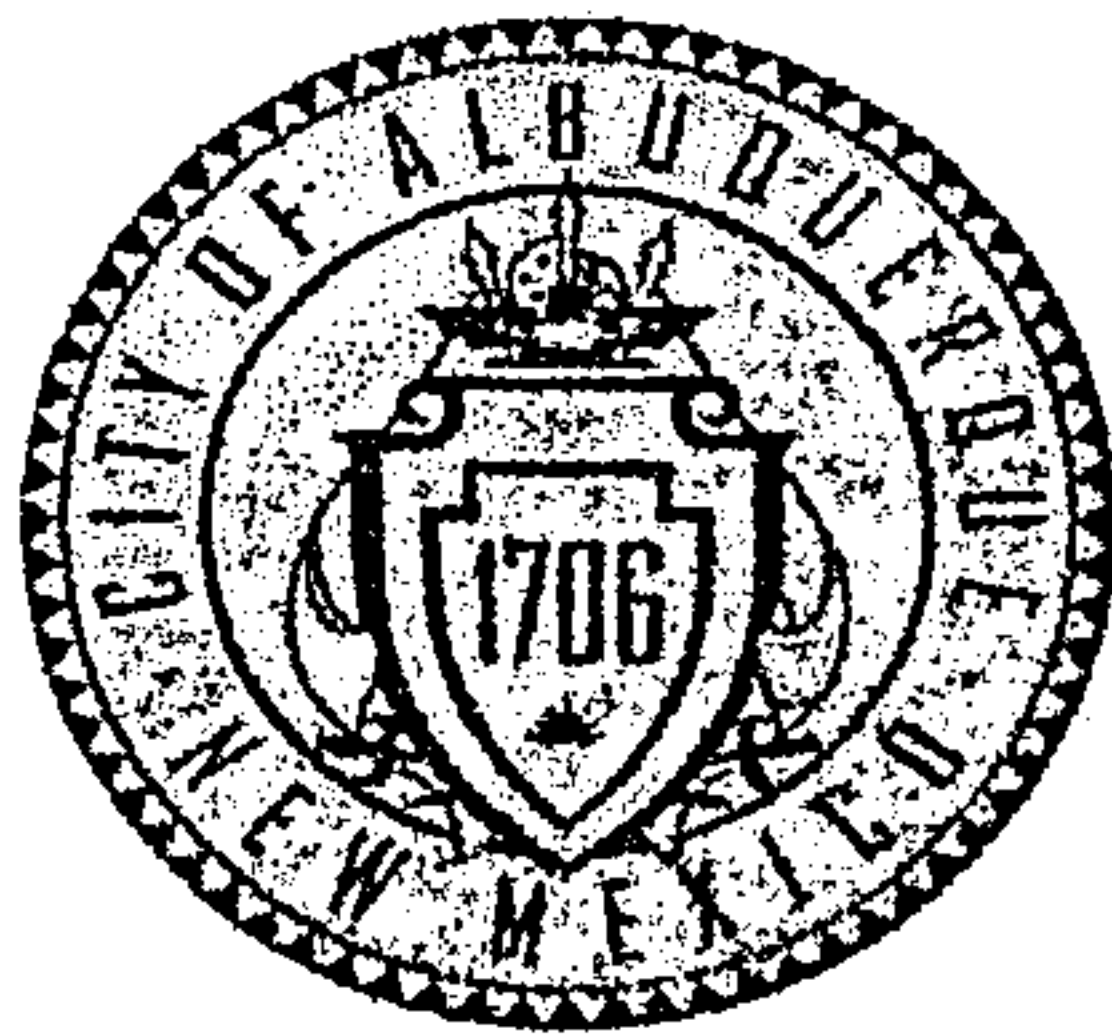
www.cabq.gov

C: TE/SB  
email

CD Contains Entire report  
for Sandia Foundation Drainage  
Report

Attached is the DTIS Sheet  
and Changes made to the  
Drainage report.

~~DTIS~~ Sheet 1 has been  
Stamped



# City of Albuquerque

Planning Department

Development & Building Services Division

## DRAINAGE AND TRANSPORTATION INFORMATION SHEET

(REV 02/2013)

Project Title: Tracts A, B-1 and C-1 Sandia Addition Building Permit #: \_\_\_\_\_ City Drainage #: F17D0953

DRB#: \_\_\_\_\_ EPC#: \_\_\_\_\_ Work Order#: \_\_\_\_\_

Legal Description: \_\_\_\_\_

City Address: \_\_\_\_\_

Engineering Firm: Floyd Development Services, LLC Contact: Hugh Floyd

Address: 918 Pinehurst Rd. Suite 101, Rio Rancho NM 87124

Phone#: 505-366-4187 Fax#: \_\_\_\_\_ E-mail: Hugh@developnm.com

Owner: Sandia Foundation Contact: Robert Goodman

Address: 6211 San Mateo Blvd. NE Suite 100. Albuquerque NM 87109

Phone#: 505-242-2684 Fax#: \_\_\_\_\_ E-mail: bob@sandiafoundation.org

Architect: \_\_\_\_\_ Contact: \_\_\_\_\_

Address: \_\_\_\_\_

Phone#: \_\_\_\_\_ Fax#: \_\_\_\_\_ E-mail: \_\_\_\_\_

Surveyor: Surv-Tek Contact: Rusty Hugg

Address: 9384 Valley View Drive, NW Albuquerque NM 87114

Phone#: 505-897-3366 Fax#: 505-897-3377 E-mail: russhugg@survtek.com

Contractor: \_\_\_\_\_ Contact: \_\_\_\_\_

Address: \_\_\_\_\_

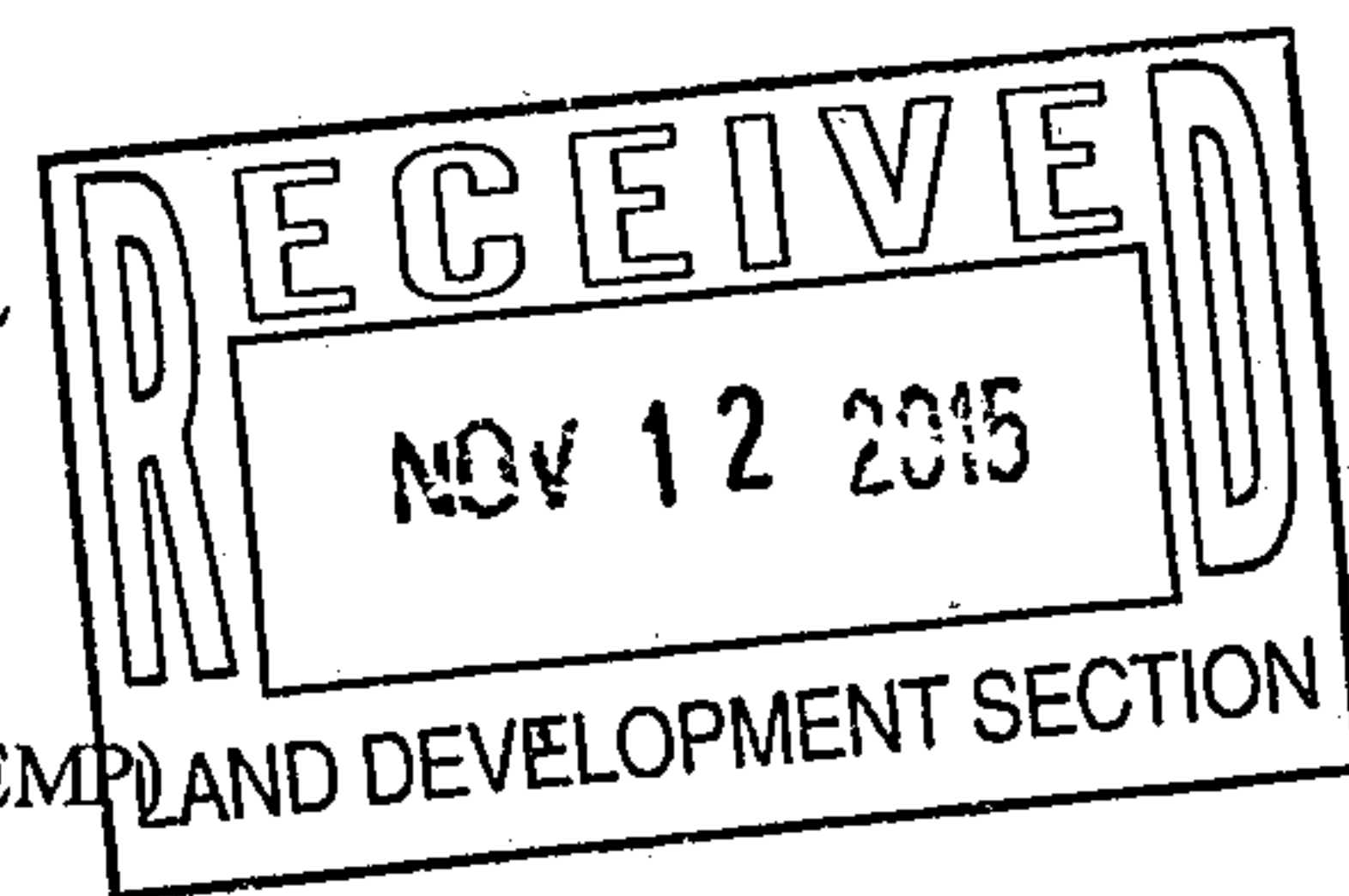
Phone#: \_\_\_\_\_ Fax#: \_\_\_\_\_ E-mail: \_\_\_\_\_

### TYPE OF SUBMITTAL:

- ☐ DRAINAGE REPORT
- ☐ DRAINAGE PLAN 1st SUBMITTAL
- ☐ DRAINAGE PLAN RESUBMITTAL
- ☐ CONCEPTUAL G & D PLAN
- ☐ GRADING PLAN
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- ☒ ENGINEER'S CERT (HYDROLOGY)
- ☐ CLOMR/LOMR
- ☐ TRAFFIC CIRCULATION LAYOUT (TCL)
- ☐ ENGINEER'S CERT (TCL)
- ☐ ENGINEER'S CERT (DRB SITE PLAN)
- ☐ ENGINEER'S CERT (ESC)
- ☐ SO-19
- ☐ OTHER (SPECIFY)

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- ☐ FOUNDATION PERMIT APPROVAL
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- ☐ WORK ORDER APPROVAL
- ☐ GRADING CERTIFICATION
- ☐ SO-19 APPROVAL
- ☐ ESC PERMIT APPROVAL
- ☐ ESC CERT. ACCEPTANCE
- ☒ OTHER (SPECIFY) Pond Certification



WAS A PRE-DESIGN CONFERENCE ATTENDED: \_\_\_\_\_ Yes ☒ No \_\_\_\_\_ Copy Provided

DATE SUBMITTED: 11/12/15 By: Floyd Development Services

Requests for approvals of Site Development Plans and/or Subdivision Plats shall be accompanied by a drainage submittal. The particular nature, location, and scope to the proposed development defines the degree of drainage detail. One or more of the following levels of submittal may be required based on the following:

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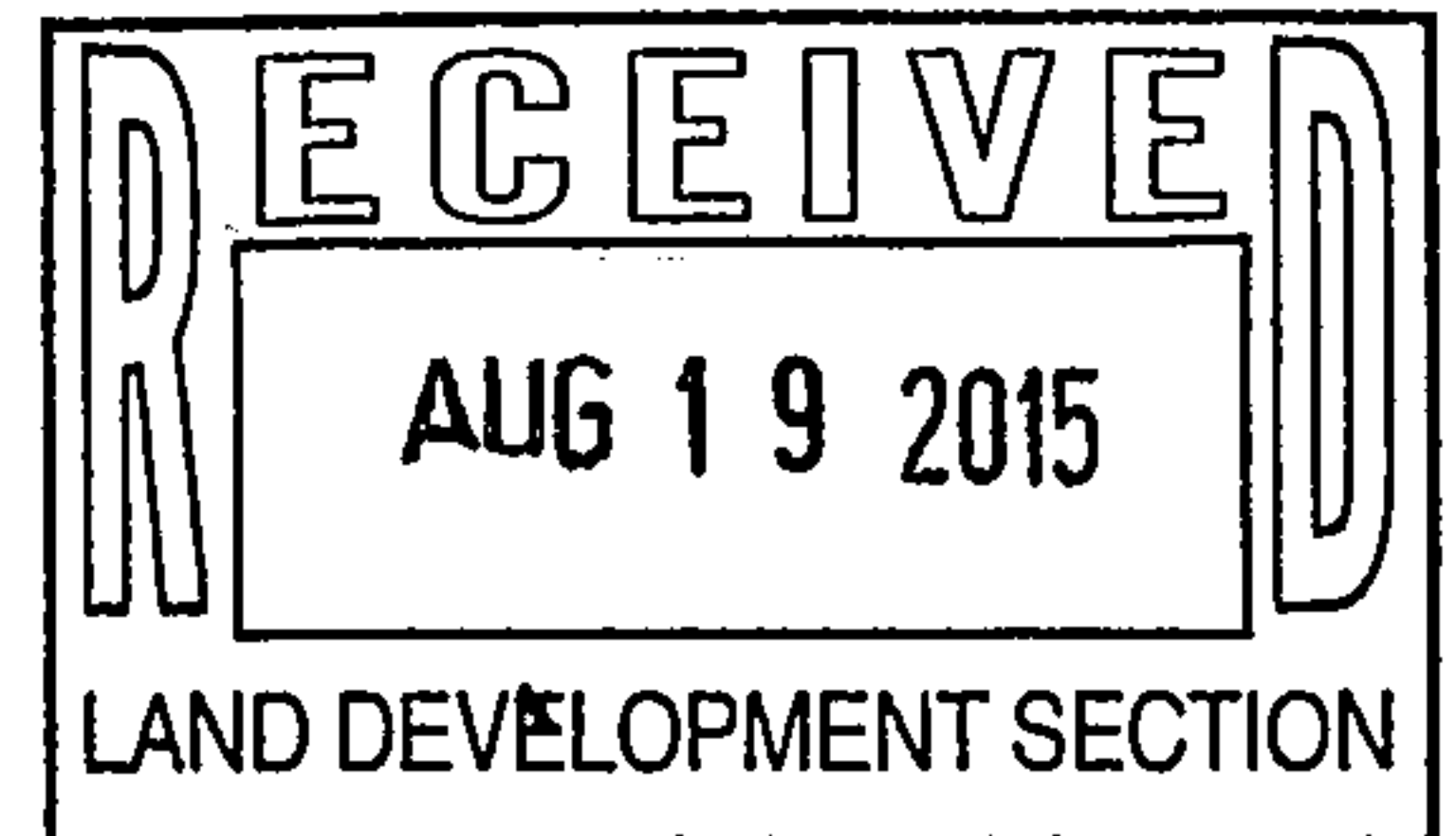
# City of Albuquerque

Planning Department

Development & Building Services Division

## DRAINAGE AND TRANSPORTATION INFORMATION SHEET

(REV 02/2013)



Project Title: Tracts A, B-1 and C-1 Sandia Addition Building Permit #: \_\_\_\_\_ City Drainage #: 417D095B  
DRB#: \_\_\_\_\_ EPC#: \_\_\_\_\_ Work Order#: \_\_\_\_\_  
Legal Description: \_\_\_\_\_  
City Address: \_\_\_\_\_

Engineering Firm: Floyd Development Services, LLC Contact: Hugh Floyd  
Address: 918 Pinehurst Rd. Suite 101, Rio Rancho NM 87124  
Phone#: 505-366-4187 Fax#: \_\_\_\_\_ E-mail: Hugh@developnm.com

Owner: Sandia Foundation Contact: Robert Goodman  
Address: 6211 San Mateo Blvd. NE Suite 100, Albuquerque NM 87109  
Phone#: 505-242-2684 Fax#: \_\_\_\_\_ E-mail: bob@sandiafoundation.org

Architect: \_\_\_\_\_ Contact: \_\_\_\_\_  
Address: \_\_\_\_\_  
Phone#: \_\_\_\_\_ Fax#: \_\_\_\_\_ E-mail: \_\_\_\_\_

Surveyor: Surv-Tek Contact: Rusty Hugg  
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Contractor: \_\_\_\_\_ Contact: \_\_\_\_\_  
Address: \_\_\_\_\_  
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☐ ESC PERMIT APPROVAL  
☐ ESC CERT. ACCEPTANCE  
☐ OTHER (SPECIFY) \_\_\_\_\_

WAS A PRE-DESIGN CONFERENCE ATTENDED: \_\_\_\_\_ Yes ☒ No \_\_\_\_\_ Copy Provided \_\_\_\_\_

DATE SUBMITTED: 7/29/2015 By: Floyd Development Services

Requests for approvals of Site Development Plans and/or Subdivision Plats shall be accompanied by a drainage submittal. The particular nature, location, and scope to the proposed development defines the degree of drainage detail. One or more of the following levels of submittal may be required based on the following:

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**Biazar, Shahab**

---

**From:** Biazar, Shahab  
**Sent:** Friday, August 07, 2015 4:46 PM  
**To:** 'Hugh Floyd (Hugh@development.com)'  
**Cc:** Harmon Rita T.; Ortiz, Monica; Elliott, Stanice; Rael, Rudy E.  
**Subject:** Tract A, B-1, and C-1 Sandia Addition (F17-D095E)

Hi,

- I did a 10 minute review of the plan and the pond concept looks ok. I will do a full review when we get a detailed plan next week. We will have to look at the emergency overflow and capacity of the existing channel on top and make sure that the runoff overflows into the channel. How will runoff reach the pond from Tract A-1, B-1, and C-1? Will there be any rundown to the ponds? Are there drainage easements in place?

Thanks

*Shahab Biazar, P.E.*

**City Engineer**

Planning Department

Development Review Services Division

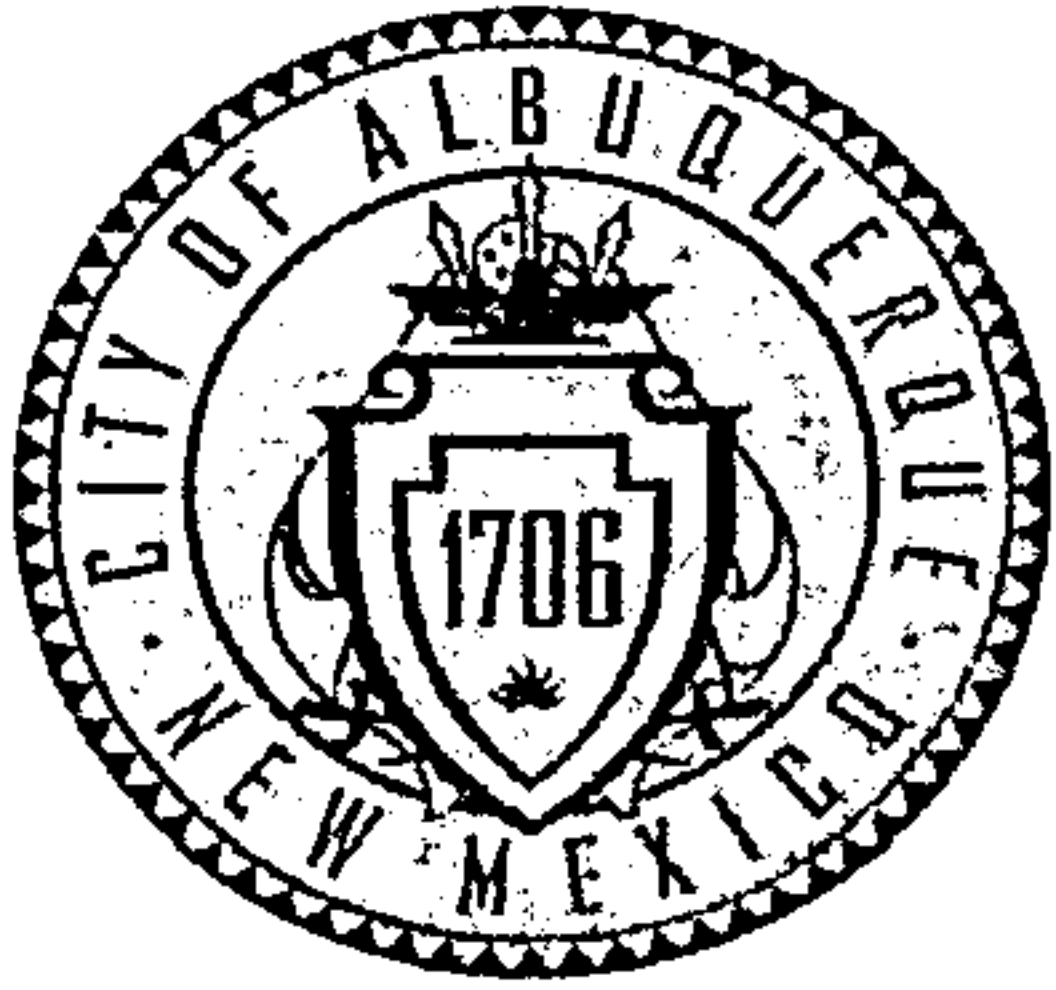
600 2nd St. NW, Suite 201

Albuquerque, NM 87102

t 505-924-3999

f 505-924-3864





# City of Albuquerque

Planning Department

Development & Building Services Division

## DRAINAGE AND TRANSPORTATION INFORMATION SHEET

(REV 02/2013)

Project Title: Tracts A, B-1 and C-1 Sandia Addition Building Permit #: \_\_\_\_\_ City Drainage #: F17D095B

DRB#: \_\_\_\_\_ EPC#: \_\_\_\_\_ Work Order#: \_\_\_\_\_

Legal Description: \_\_\_\_\_

City Address: \_\_\_\_\_

Engineering Firm: Floyd Development Services, LLC Contact: Hugh Floyd

Address: 918 Pinehurst Rd. Suite 101, Rio Rancho NM 87124

Phone#: 505-366-4187 Fax#: \_\_\_\_\_ E-mail: Hugh@developnm.com

Owner: Sandia Foundation Contact: Robert Goodman

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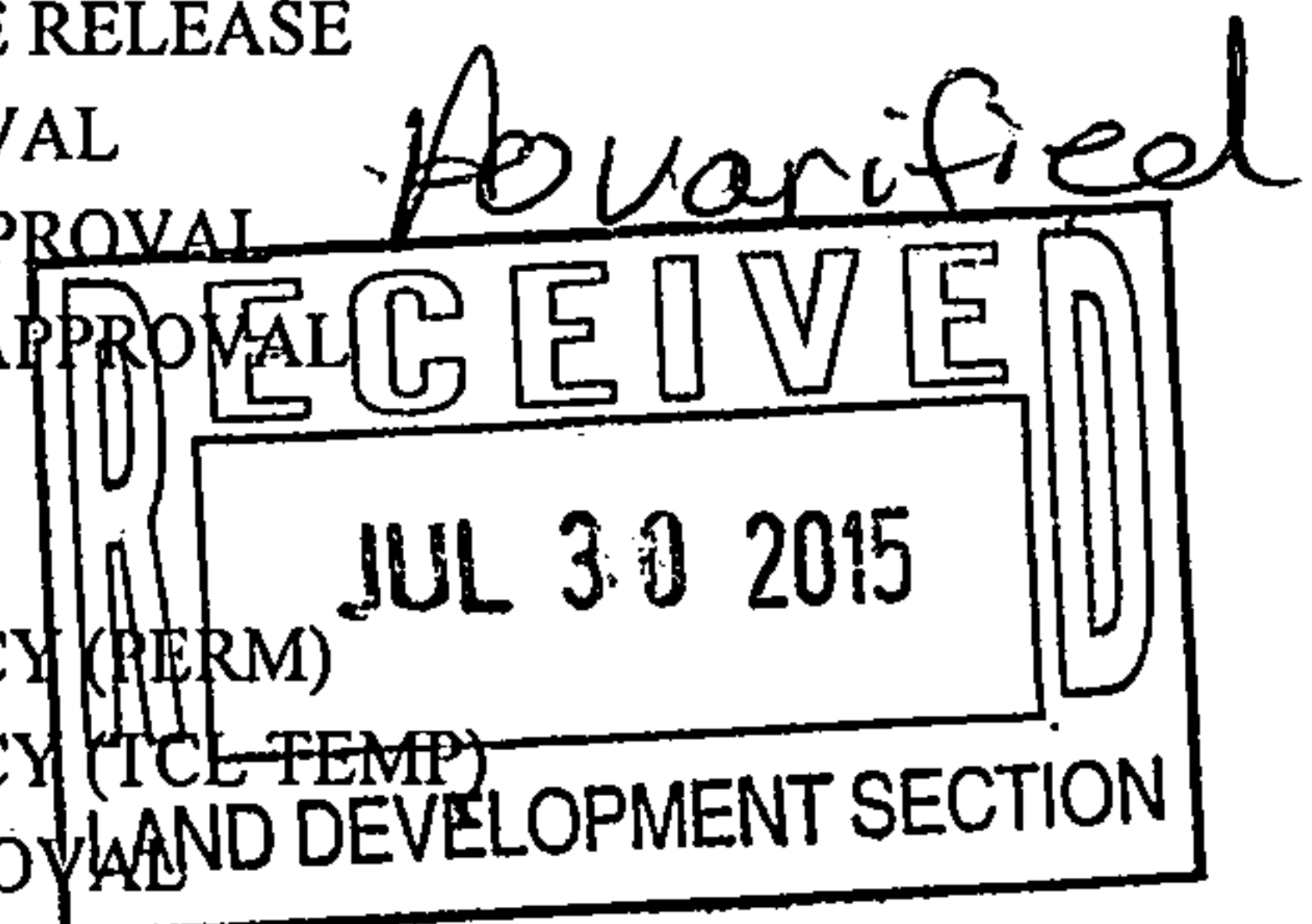
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DATE SUBMITTED: 7/29/2015 By: Floyd Development Services

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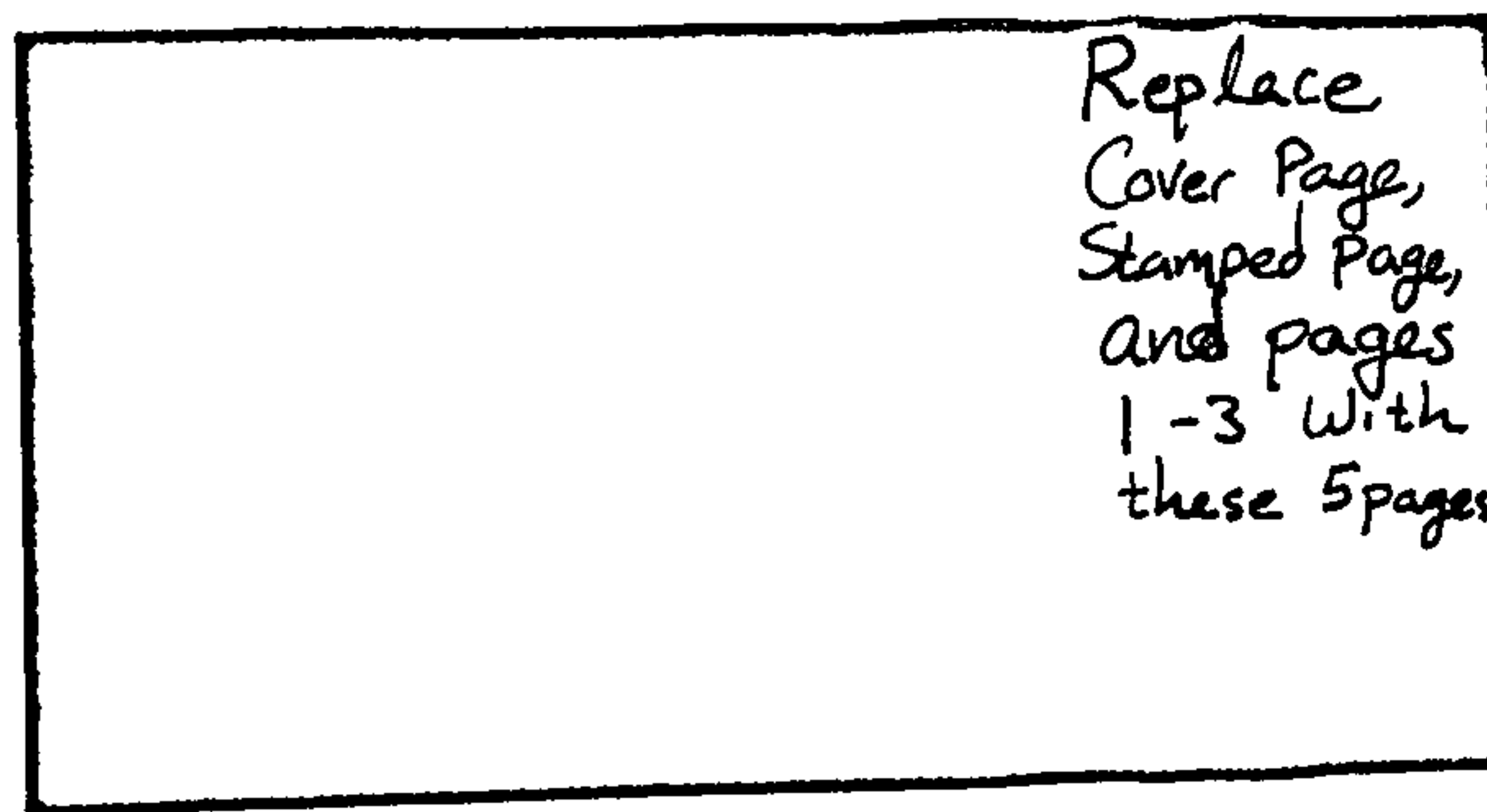
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# DRAINAGE REPORT FOR TRACTS A, B-1, AND C-1 SANDIA ADDITION

---

PREPARED FOR  
SANDIA FOUNDATION

JULY 2015



Prepared By:

**Floyd Development Services, LLC**

918 Pinehurst Road  
Rio Rancho, NM 87124

I, Hugh W. Floyd, hereby certify that I am a Registered Professional Engineer, registered in the State of New Mexico, and that the following report was prepared under my direction and is true and correct to the best of my knowledge and belief.



Hugh W. Floyd  
NMPE # 16633



## TABLE OF CONTENTS

I.	Introduction.....	1
II.	Background and Existing Conditions.....	1
III.	Methodology.....	2
IV.	Proposed Conditions.....	2
V.	Summary and Conclusion.....	3

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Figure 1 - 2002 Photo of the garden nursery

Table 1 - Water quality and storage pond rating curve

Table 2 - Treatment Type Percentages

Table 3 - Water quality Volume Calculations

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### APPENDIX A - Background Reports

- A.1 - Davita's Del Norte Dialysis Center Drainage Report
- A.2 - Navajo Terminals Drainage Study
- A.3 - Isaacson and Arfman Engineer's Report

### APPENDIX B - AHYMO

### APPENDIX C - Hydraulics

## **I. INTRODUCTION**

The purpose of this report is to maintain compliance with the City of Albuquerque's regulations and to design a more efficient ponding system so that Sandia Foundation can better utilize their remaining property (Tract C-1).

The site is located on the west side of San Mateo Boulevard in between Lincoln Road and Mcleod Road. The site is shaped like an L with the long side running east west, as shown on Sheet 1 of Exhibit 1. ABF Terminal, which used to be known as Navajo Freight Lines Terminal, is located on the west side of the site and wraps around the northwest corner. The Golden Corral restaurant (Tract A) is located north of the long side and east of the short side. There is a storage facility on the south side of the site. Davita's Del Norte Dialysis Center is in the process of developing on the east side of the property, between Golden Corral and the storage facility. Entitlement and Engineering Solutions, Inc. (EES) recently submitted a drainage report for the Davita site (Tract B-1) dated 5/5/2015 and that report is referenced in Appendix A.

## **II. BACKGROUND AND EXISTING CONDITIONS**

For many years the area now occupied by Golden Corral, Davita's developing site, and the remaining Tract (C-1), was used as a garden nursery. The area has historically drained to the west through the Navajo Terminals. In 1974 an existing 42 in. storm drain was removed from the Navajo Terminals site due to the construction of a new storm drain on San Mateo Boulevard. At the same time Kruger, Lake and Associates prepared a report and plan set for a smaller storm drain system through the Navajo Terminals site. Their report and plans are shown in Appendix A.2. As can be seen in the Kruger drainage study, the intention was to accommodate free discharge from the nursery site. They calculated a runoff discharge of 21 cfs using a C factor of 0.6 for the nursery site. This discharge is collected in two soil cement swales that were constructed per the 1974 plan for the Navajo Terminal site and are still in existence. These swales have two inlets that ultimately tie into an 18" storm drain that runs through the ABF/Navajo Terminal property, as shown on the plan sheet found in Appendix A.2. Figure 1 shows the nursery in 2002 and displays the extent of the buildings and hardscape. It should be noted that the impervious area is comparable to a fully developed commercial site.

Currently the site is zoned C-3 and has a consistent slope to the west at about 3%. On the south side of the property there is a wall 1 to 3 feet in height, which prevents runoff from transferring between the storage facility and the existing site. The runoff from Tract C-1 and the Davita site (Tract B-1) flows into two ponds. One pond is located in the southwest corner of the existing site and the other is in the northwest corner. The Golden Corral (Tract A) site has part of the site, the building, draining to San Mateo, a small portion of the parking lot draining to the existing soil cement swale, and the remainder draining to the existing ponds. The ponds were built in 2013 under emergency conditions when two large storms occurred back to back. Prior to the construction of the emergency ponds, Tract C-1 had three makeshift ponds that neared full capacity during the second 2013 storm. According to the Engineer's Report by Isaacson and

Arfman dated 09/24/2013, located in Appendix A.3, the berms surrounding the makeshift ponds began to fail as the pond's water level approached the top. It is also noted in the Temporary Detention plan sheet dated 08/27/2013, found in Appendix A.3, that repairs were made to the western shotcrete channel. It is believed that repairs were necessary due to settlement, which allowed water to "pipe" under the shotcrete channel.

### **III. METHODOLOGY**

The proposed and existing conditions are modeled using AHYMO and the 100 year, 24 hour storm event in accordance with chapter 22 of the Albuquerque Design Process Manual (DPM). The AHYMO data are found in Appendix B.

The water quality pond volume is calculated using the first 0.34 inches of runoff multiplied by the impervious area of the site. In this report the calculations for the water quality ponding includes Davita's developing site since their report specifies to use the existing pond for their first flush. Table 3 on Sheet 1 of Exhibit 1 shows the water quality volume calculations.

The downstream capacity of the ABF Terminals storm drains was analyzed using the orifice and Bernoulli equations based on the City of Albuquerque DPM, Section 22.3B. Appendix C contains the orifice calculations used to develop rating curves for each proposed pond outlet and ABF inlet. Table 1 from Sheet 1 of Exhibit 1 shows the combined outlet rating curves for the northern and southern pipe outlets. Appendix C contains the downstream analysis used to determine the best fit flowrate.

### **IV. PROPOSED CONDITIONS**

In the past, the ABF/Navajo Terminal site was designed to receive 21 cfs from the garden nursery site. The calculations in Appendix C indicate that a flowrate of about 10 cfs lets water flow into the storm drain system without causing significant cross parking lot flow. This report recognizes that the design of the downstream storm drain system is undersized and that a large runoff rate produces flow over the paved areas. Due to the problems in 2013 and an attempt to limit flows to a level that can be contained in the existing storm drain, the discharge rate is reduced from 21 cfs to 10 cfs.

The proposed pond is located in the northwest corner of Tract C-1, and extends along the western border. In the northwest corner the pond is V-shaped and 4 feet deep with 3:1 side slopes. Along the western border the pond is only 2 feet deep with 3:1 side slopes and a flat bottom. The pond is designed to retain 3718 cubic feet of water within the lowest 2 foot depth to account for the first flush. The elevation range of the water quality pond is from 5192 feet to 5194 feet. The upper portion of the pond is detention and has an elevation range of 5194 feet to 5195.8 feet. There are two outlets that allow water to discharge into the ABF Terminal storm drain system. Both outlets have a 12 inch pipe which tie into the back of the ABF Terminal inlets, one on the north and the other to the south. The north outlet has an elevation 5194 feet, and the southern outlet elevation is 5193 feet. Surrounding the southern outlet is a weir with a



top elevation of 5194 feet. The weir is used to maintain a water quality volume and to allow additional head on the outlet so that more water enters the system sooner. Table 1 on Sheet 1 of Exhibit 1 shows the storage rating curve of the proposed pond. On the northwest corner there will be an emergency spillway with a top elevation of 5195.8 that extends to the south along the western border.

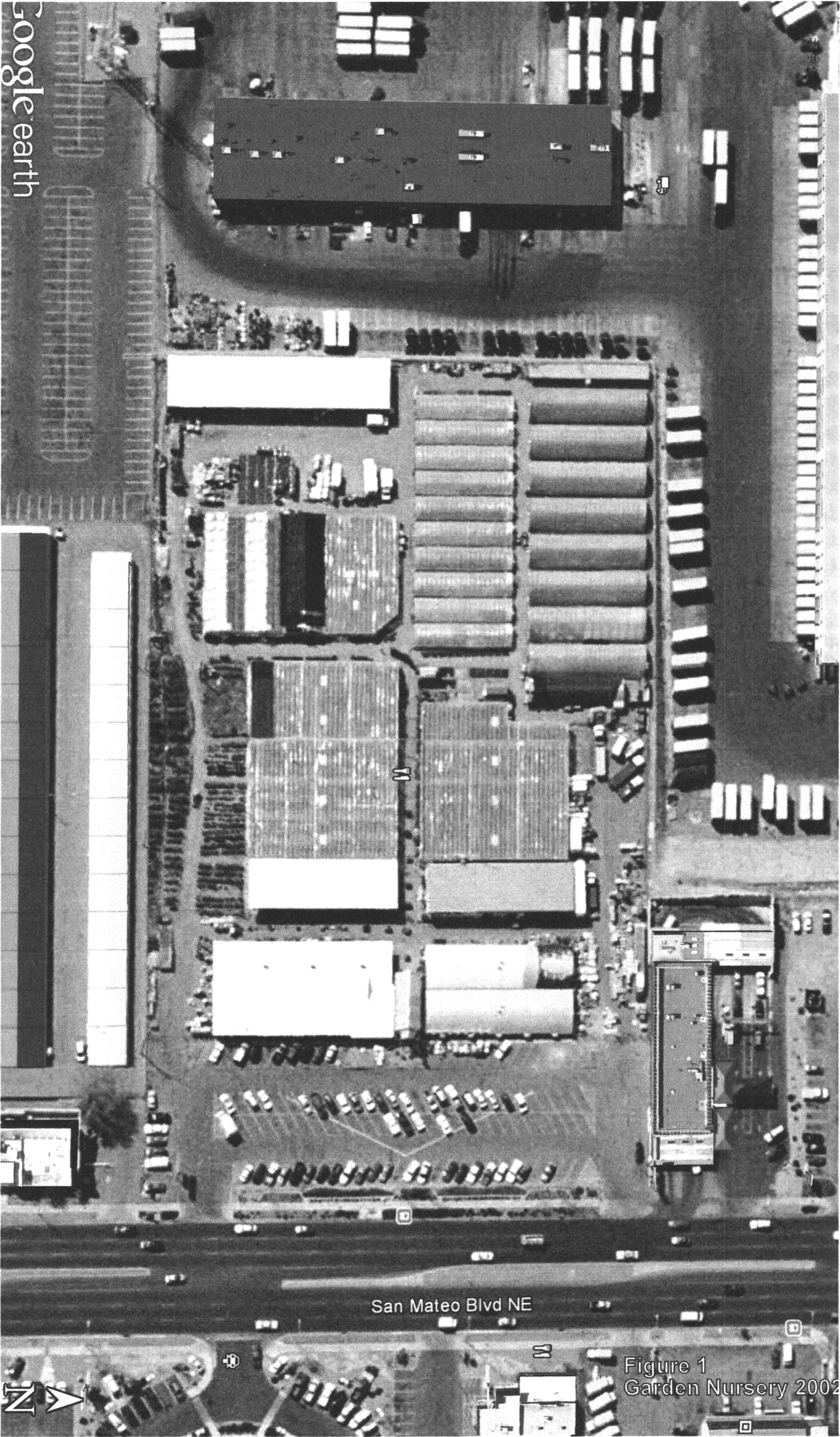
## **V. SUMMARY AND CONCLUSION**

The plan outlined in this report provides a pond that retains the required first flush volume for Tract C-1 and Tract B-1, as well as providing detention ponding adequate to limit the total discharge to a maximum rate of 10 cfs rather than the previous allowed 21 cfs. If a storm larger than the design caused the spillway to become activated then water will flow into the soil cement channel as it has historically done.

# **Sandia Foundation San Mateo Site**

## **Figure 1**

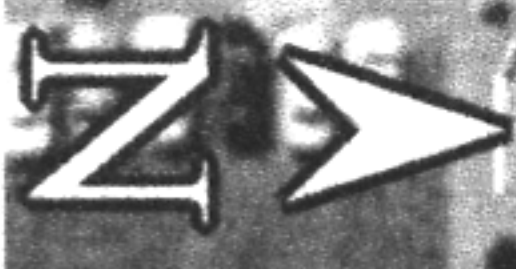




Google earth

San Mateo Blvd NE

Figure 1  
Garden Nursery 2002







# **Sandia Foundation San Mateo Site**

## **Exhibit 1**





# **Appendix A**

## **Background Reports**



# **Appendix A.1**

## **Davita's Del Norte Dialysis Center Drainage Report**

**See DVD**





**A DRAINAGE STUDY  
OF  
NAVAJO FREIGHT LINES' TERMINAL SITE  
AT  
SAN MATEO AND LINCOLN ROAD, N. E.  
ALBUQUERQUE, NEW MEXICO**

**Kruger, Lake and Associates  
Architects and Engineers  
601 San Pedro Dr. NE.  
Albuquerque, New Mexico 87108**

**Tel: 505 / 265-8452. -53**

**December 29, 1973  
(Revised January 29, 1974)**

## **I N D E X**

<b>A.</b>	<b>General Information</b>	<b>Page 1</b>
<b>B.</b>	<b>Runoff Formulas</b>	<b>Page 1</b>
<b>C.</b>	<b>Runoff Calculations</b>	<b>Page 1</b>
<b>D.</b>	<b>Runoff Calculations After Construction</b>	<b>Page 1</b>
<b>E.</b>	<b>Runoff Calculations Prior to Construction</b>	<b>Page 1</b>
<b>F.</b>	<b>Conclusions</b>	<b>Page 2</b>
 <b><u>Runoff Calculations:</u></b>		
<b>A.</b>	<b>Flow in Arroyo Prior to Construction</b>	<b>Page 3</b>
<b>B.</b>	<b>Anticipated Flow in Arroyo After Construction</b>	<b>Page 3</b>
<b>C.</b>	<b>Flow onto Lincoln Rd., Prior to Construction</b>	<b>Page 4</b>
<b>D.</b>	<b>Flow onto Lincoln Rd., After Construction</b>	<b>Page 4</b>

## A DRAINAGE STUDY

NAVAJO FREIGHT LINES TERMINAL SITE  
San Mateo and Lincoln Road, N. E.  
Albuquerque, New Mexico

### A. GENERAL INFORMATION

1. Legal Description: See Legal description on Plot Plan, (Exhibit "A").
2. Location: The area concerned in this study is bordered on the east by San Mateo Blvd. NE. and on the north by Lincoln Rd. NE.
3. Contributing Drainage Areas: Approximately 43 acres between San Pedro Dr., NE. and San Mateo Blvd., NE., contribute to the run-off through the subject property as indicated on the attached topo map, (Exhibit "B").
4. Arroyos: A small arroyo flows through the site covered by this study.
5. San Mateo Diversion Storm Sewer: The City of Albuquerque has designed a storm sewer along the west right-of-way of San Mateo to divert the arroyo flowing through this land to Bear Canyon Arroyo. This sewer will be constructed under the Cities Block-to-Block Contract. Navajo Freight Lines, Inc., is participating in the cost of this storm sewer.

### B. RUNOFF FORMULA

Runoff quantities are calculated by the rational formula -  $Q = C I A$ .

#### 1. Coefficients (C):

a. Roofs	.95
b. Paved Areas	.90
c. Developed Residential Areas	.65
d. Nursery Areas	.60
e. Drive-in Theater (Paved and Gravel)	.80
f. Undeveloped Areas	.30

2. Intensity of Rainfall: ( $i = 5.4''/\text{hr.}$ )  
Assume 10 minutes duration  $i = \frac{189}{t + 25} = \frac{189}{10+25} = 5.4''/\text{hour.}$

$i = 5.4 \text{ in./hr}$

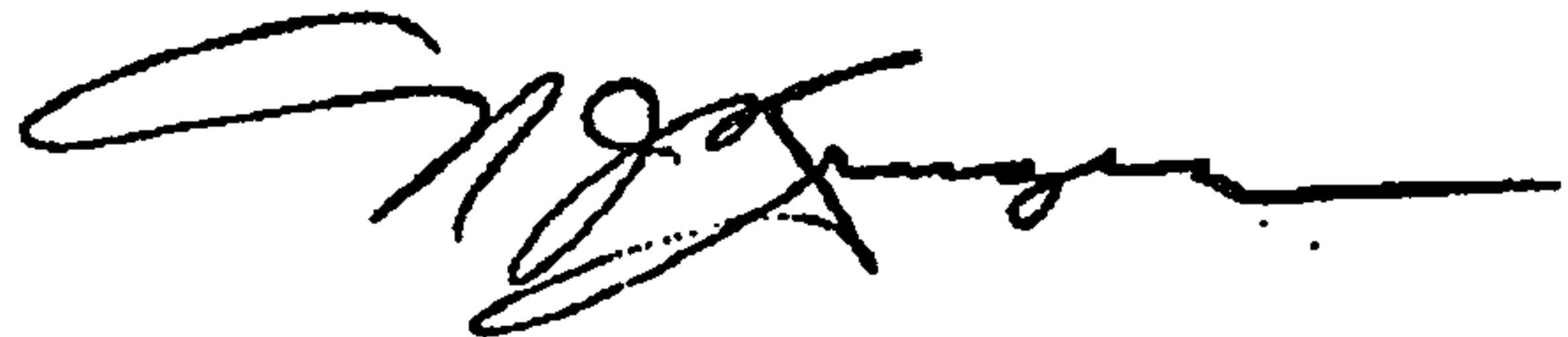
### C. RUNOFF CALCULATIONS - See Sheets 3 and 4.

### D. RUNOFF CALCULATIONS AFTER CONSTRUCTION are based on Project Site Plans - See Exhibit "A".

### E. RUNOFF CALCULATIONS PRIOR TO CONSTRUCTION are based on a preliminary area topographical map prepared by Bohannon, Westman, Huston (See Exhibit "B").

**F. CONCLUSIONS**

1. The quantity of runoff flow in the arroyo at Point "B", the low point at the west end of the property has been reduced from 196.2 c.f.s., prior to construction, to 84.5 c.f.s. after construction is completed.
2. The quantity of flow on to Lincoln Road has been increased by only a fraction (.70 c.f.s.). When curb and gutter has been installed on San Mateo and a water stop constructed at San Mateo and Lincoln, the total flow in Lincoln Road will be less than at present.
3. We feel that all requirements of the 1972-2 ANAFCA Drainage Resolution have been met by our design.



---

N. J. Kruger, President  
KRUGER, LAKE and ASSOCIATES  
Architects and Engineers





RUN OFF CALCULATIONS

12-15-78 MTC

A. FLOW IN ARROYO PRIOR TO CONSTRUCTION D. C. L. A

1. AT POINT A (OUTLET OF CULVERT)

WATER STOPS AT ALL INTERSECTIONS ON SAN PEDRO.

AREA OF WATER SHED BETWEEN SAN PEDRO & SAN MATEO (EXHIBIT B)  
FROM PRELIMINARY TOPO MAP BY DOMANNAN-WESMAN HUSTON

1. DWSR	700 x 1000	700,000 / 43,500	20.6 A	C = .65
2. DWSR	700 x 150		15.25 A	C = .80
3. UNIMPROVED	400 x 800		7.3 A	C = .80

$$Q_1 = 20.6 \times .65 \times 5.4 = 72.12 \text{ c.f.s.}$$

$$Q_2 = 15.25 \times .80 \times 5.4 = 66.0$$

$$Q_3 = 7.3 \times .80 \times 5.4 = 31.2$$

$$\text{TOTAL FLOW AT 'A'} = 169.3 \text{ c.f.s.}$$

2. FLOW AT POINT 'B' SEE EXHIBIT 'B'

1. NURSERY	700 ft x 400 ft	6.4 Ac	C = 0.60
2. NURSERY	700 x 400	6.43 A	C = .60
3. UNIMPROVED	500 x 375	2.88	
4. UNIMPROVED	500 x 375	2.30	
5. UNIMPROVED	500 x 375	2.30	
6. UNIMPROVED	500 x 375	2.12	
7. UNIMPROVED	500 x 375	2.10	
8. STREET	450 x 100	1.05 A	C = .70
FROM CULVERT PT 'A'		150.0 c.f.s.	
9. ST. 6.43 x .60 x 5.4		21.0	
10. ST. 12.34 x .80 x 5.4		53.2	
11. ST. 1.05 x .90 x 5.4		5.0	
TOTAL FLOW AT PT 'B'		199.2 c.f.s.	

TOTAL FLOW IN ARROYO PRIOR TO CONSTRUCTION

B. ANTICIPATED FLOW IN ARROYO AFTER CONSTRUCTION

1. ALL FLOW AT POINT 'A' IS TO BE DIVERTED TO DEAR CANYON VIA NEW STORM SEWER ALONG SAN MATEO BY CITY OF ALBUQUERQUE.
2. FLOW AT POINT 'B' IS

1. NURSERY	700 x 400	6.43 A	C = .60
2. PAVED AREA	125 x 375	46,875	
3. UNIMPROVED	125 x 375	10,000	
4. UNIMPROVED	125 x 375	10,000	
5. UNIMPROVED	125 x 375	10,000	
6. UNIMPROVED	125 x 375	10,000	
7. UNIMPROVED	125 x 375	10,000	
8. UNIMPROVED	125 x 375	10,000	
9. UNIMPROVED	125 x 375	10,000	
10. UNIMPROVED	125 x 375	10,000	
11. UNIMPROVED	125 x 375	10,000	
12. UNIMPROVED	125 x 375	10,000	
13. UNIMPROVED	125 x 375	10,000	
14. UNIMPROVED	125 x 375	10,000	
15. UNIMPROVED	125 x 375	10,000	
16. UNIMPROVED	125 x 375	10,000	
17. UNIMPROVED	125 x 375	10,000	
18. UNIMPROVED	125 x 375	10,000	
19. UNIMPROVED	125 x 375	10,000	
20. UNIMPROVED	125 x 375	10,000	
21. UNIMPROVED	125 x 375	10,000	
22. UNIMPROVED	125 x 375	10,000	
23. UNIMPROVED	125 x 375	10,000	
24. UNIMPROVED	125 x 375	10,000	
25. UNIMPROVED	125 x 375	10,000	
26. UNIMPROVED	125 x 375	10,000	
27. UNIMPROVED	125 x 375	10,000	
28. UNIMPROVED	125 x 375	10,000	
29. UNIMPROVED	125 x 375	10,000	
30. UNIMPROVED	125 x 375	10,000	
31. UNIMPROVED	125 x 375	10,000	
32. UNIMPROVED	125 x 375	10,000	
33. UNIMPROVED	125 x 375	10,000	
34. UNIMPROVED	125 x 375	10,000	
35. UNIMPROVED	125 x 375	10,000	
36. UNIMPROVED	125 x 375	10,000	
37. UNIMPROVED	125 x 375	10,000	
38. UNIMPROVED	125 x 375	10,000	
39. UNIMPROVED	125 x 375	10,000	
40. UNIMPROVED	125 x 375	10,000	
41. UNIMPROVED	125 x 375	10,000	
42. UNIMPROVED	125 x 375	10,000	
43. UNIMPROVED	125 x 375	10,000	
44. UNIMPROVED	125 x 375	10,000	
45. UNIMPROVED	125 x 375	10,000	
46. UNIMPROVED	125 x 375	10,000	
47. UNIMPROVED	125 x 375	10,000	
48. UNIMPROVED	125 x 375	10,000	
49. UNIMPROVED	125 x 375	10,000	
50. UNIMPROVED	125 x 375	10,000	
51. UNIMPROVED	125 x 375	10,000	
52. UNIMPROVED	125 x 375	10,000	
53. UNIMPROVED	125 x 375	10,000	
54. UNIMPROVED	125 x 375	10,000	
55. UNIMPROVED	125 x 375	10,000	
56. UNIMPROVED	125 x 375	10,000	
57. UNIMPROVED	125 x 375	10,000	
58. UNIMPROVED	125 x 375	10,000	
59. UNIMPROVED	125 x 375	10,000	
60. UNIMPROVED	125 x 375	10,000	
61. UNIMPROVED	125 x 375	10,000	
62. UNIMPROVED	125 x 375	10,000	
63. UNIMPROVED	125 x 375	10,000	
64. UNIMPROVED	125 x 375	10,000	
65. UNIMPROVED	125 x 375	10,000	
66. UNIMPROVED	125 x 375	10,000	
67. UNIMPROVED	125 x 375	10,000	
68. UNIMPROVED	125 x 375	10,000	
69. UNIMPROVED	125 x 375	10,000	
70. UNIMPROVED	125 x 375	10,000	
71. UNIMPROVED	125 x 375	10,000	
72. UNIMPROVED	125 x 375	10,000	
73. UNIMPROVED	125 x 375	10,000	
74. UNIMPROVED	125 x 375	10,000	
75. UNIMPROVED	125 x 375	10,000	
76. UNIMPROVED	125 x 375	10,000	
77. UNIMPROVED	125 x 375	10,000	
78. UNIMPROVED	125 x 375	10,000	
79. UNIMPROVED	125 x 375	10,000	
80. UNIMPROVED	125 x 375	10,000	
81. UNIMPROVED	125 x 375	10,000	
82. UNIMPROVED	125 x 375	10,000	
83. UNIMPROVED	125 x 375	10,000	
84. UNIMPROVED	125 x 375	10,000	
85. UNIMPROVED	125 x 375	10,000	
86. UNIMPROVED	125 x 375	10,000	
87. UNIMPROVED	125 x 375	10,000	
88. UNIMPROVED	125 x 375	10,000	
89. UNIMPROVED	125 x 375	10,000	
90. UNIMPROVED	125 x 375	10,000	
91. UNIMPROVED	125 x 375	10,000	
92. UNIMPROVED	125 x 375	10,000	
93. UNIMPROVED	125 x 375	10,000	
94. UNIMPROVED	125 x 375	10,000	
95. UNIMPROVED	125 x 375	10,000	
96. UNIMPROVED	125 x 375	10,000	
97. UNIMPROVED	125 x 375	10,000	
98. UNIMPROVED	125 x 375	10,000	
99. UNIMPROVED	125 x 375	10,000	
100. UNIMPROVED	125 x 375	10,000	

Exhibit A of this drainage study shows this circled 1 in the same location as the old garden nursery.

89.50 cfs

### RUN OFF CALCULATIONS

$Q_1 = ciA = 0.6(5.4)(6.4) = 20.74 \text{ cfs}$   
 $Q_2 = 4.4 \times 5.4 = 23.8 \text{ cfs}$   
 $Q_3 = 10.4 \times 5.4 = 56.2 \text{ cfs}$   
 $Q_4 = 2.0 \times 5.4 = 10.8 \text{ cfs}$   
 $Q_5 = 1.3 \times 5.4 = 7.0 \text{ cfs}$   
 $89.5$

21 cfs of the 89.5 cfs that goes into the Navajo Terminals storm drain system allowed to come from the garden nursery.

TOTAL AVAILABLE FLOW PA B = 84.52 cfs < 196.2 cfs

### C. FLOW ON TO LINCOLN PRIOR TO CONSTRUCTION

① UNIMPAVED 120x120 25000 3.82 C = .30  
 ② PAVED AREA 30x150 5500 1.55 A C = .90  
 ③ ROOF 100x140 14000 4.64 A C = .95

$Q_1 = 3.82 \times 5.4 = 6.2$   
 $Q_2 = 1.55 \times 5.4 = 8.4$   
 $Q_3 = 4.64 \times 5.4 = 2.4$

TOTAL FLOW ON TO LINCOLN = 16.6 cfs

### D. FLOW TO LINCOLN AFTER CONSTRUCTION

① ROOF 100x140 14000 4.64 A  
 ② PAVED AREA 30x150 5500 1.55 A  
 ③ UNIMPAVED 120x120 25000 3.82 A  
 ④ ROOF 6000 3.82 A  
 ⑤ PAVED 30x550 10000 1.55 A  
 ⑥ UNIMP 30x550 10000 1.55 A

$Q_1 = 2.4$   
 $Q_2 = 8.4$   
 $Q_3 = 4.8$   
 $Q_4 = .9$   
 $Q_5 = .8$   
 $Q_6 = .4$

TOTAL FLOW ON TO LINCOLN = 17.3 cfs > 16.6 cfs, 10 cfs. OK

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# **Navajo Freight Lines Terminals Drainage Study**

## **Plan Sheet Exhibit A**



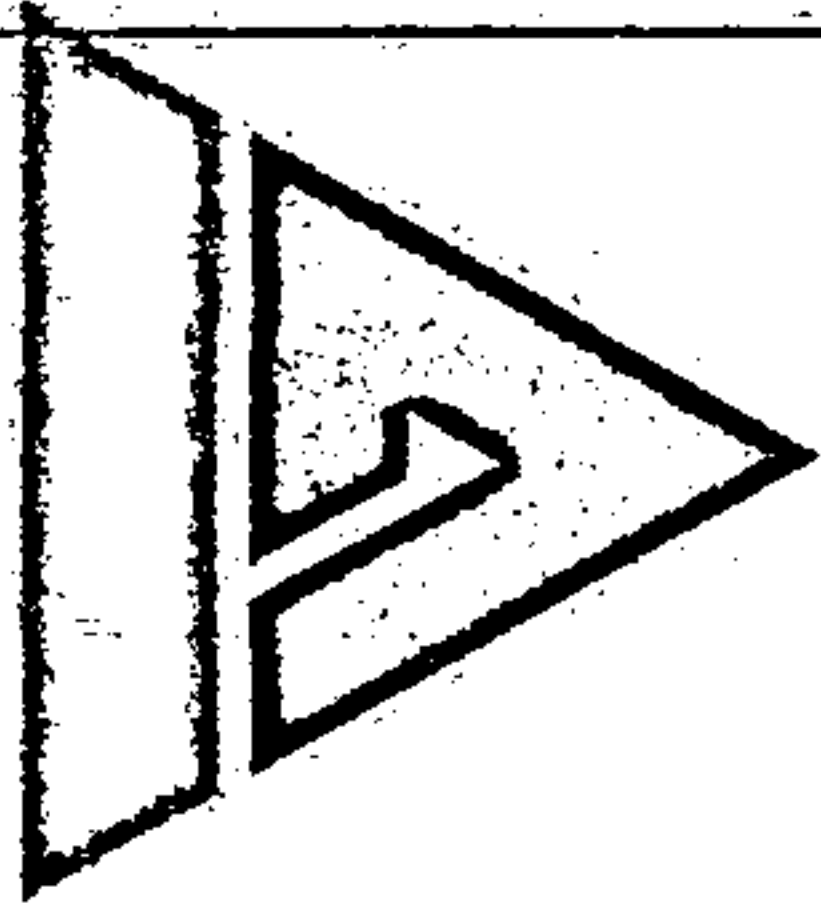


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# **Appendix A.3**

**Isaacson and  
Arfman**

**Engineer's Report**



## **ENGINEER'S REPORT**

Project: Sandia Foundation; San Mateo - Rowlands Tract

Sept. 24, 2013

Owner: Sandia Foundation

Subject: Storm Water Flooding

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### **Major Storm Event:**

On September 12, 2013 Albuquerque experienced the start of a three-day major storm event where 3.65 inches of rain fell in the approximate area of the subject Sandia Foundation (SF) site. This event was preceded by a rain on Sept 10<sup>th</sup> which dropped 1.04 inches of rain thereby saturating the soil at the site (Photo #1). A total rainfall amount of 5.07 inches was measured at the Albuquerque Weather Services Station located at Montgomery Blvd. and San Mateo Blvd. for this time period.

### **Site Visit (09-12-13):**

Karen Hudson (SF representative) contacted Fred Arfman (FA) with Isaacson & Arfman PA to perform a site visit to assess the condition of the existing storm water containment berms as a follow up to a meeting with Zack Lacombe, Manager of the ABF Freight Lines Terminal, the property west of the SF site. The following observations and actions were undertaken:

- FA arrived on site at approximately 10:45 AM and located Zack and Payam Ghoreishi (PG), an earthwork contractor, observing the storm waters from the Golden Corral and the undeveloped SF property entering into the three existing makeshift ponds between the SF property and ABF.
- The ponds were partially full from the earlier rains and were reaching full capacity from the morning rains.
- Zack was very concerned that the ponds would fail causing the stored rainwater to flow onto the ABF site forcing him to close down the terminal's shops and effectively crippling the terminal's productivity.
- PG called his office to get his personnel to the site to immediately begin work on reinforcing the makeshift berms. At this time Zack left the site. Laborers with shovels



arrived approximately 30 minutes later. It was before noon and the rains had started to let up after a storm duration of two hours.

- The ponds storm water levels reached the top of the berms and the interior berm between the middle pond and the north pond breached causing the water level in the north pond to rise (Photo #3). Payam and his laborers were directed to the pending breach point to reinforce the low point in the berm (Photo #2), now equal to the water level.
- PG and his laborers were then directed to the south end of the west berm of the middle pond. A controlled overflow outlet was excavated (Photo #5) to allow the captured storm waters to safely discharge into the ABF drainage rundown along the westerly property line of the SF property. Since the middle and north ponds were now connected, this outlet slowly relieved the pressure on both ponds.
- As soon as the outlet was conveying storm waters, it was noticed that the north berm of the southerly pond was breaching. Immediately, all those present worked to stop the breach by reconstructing the berm and placing rock from the adjacent rundown on the berm to fill in the breach. The breach was plugged (Photo #7).
- A backhoe from PG Enterprises arrived to fortify all of the areas that were compromised and then to stabilize the entire berm system (Photo #4).
- Two large capacity mobile pumps were placed at the NE corner of the north berm to drain the storm waters directly into the storm drain inlet on the ABF property (Photo #6).

#### **Site Monitoring (09-13-13 through 09-16-13):**

- The property was monitored by the personnel of PG Enterprises through the night and over the next four days (Photo #8).
- The ponds were continually drained of the captured storm waters and the berms inspected and maintained.

#### **Conclusion:**

- None of the ponded storm waters from the Sandia Foundation property entered onto the ABF facility other than at the drainage rundown and storm drain inlets constructed for this purpose.



- The ponds were continually drained from additional rains in order to keep the berms and the underlying earth from becoming overly saturated and prone for collapsing. As of 09-24-13, the areas are still too saturated to allow for reconstruction.



**1: SEPTEMBER 10 - PRESTORM CONDITIONS**



**2: SEPTEMBER 12 - MANUAL FORTIFICATION OF BERMS**





**3: BREACH OF MIDDLE POND**



**4: FORTIFICATION OF BERMS – SOUTH POND**





**5: HAND EXCAVATED CONTROLLED RELEASE OUTLET**



**6: PUMP DISCHARGE TO EXISTING ABF INLET**





**7: SOUTH POND OVERFLOW TO EXISTING RUNDOWN**



**8: POST STORM WATER LEVEL WITH PUMPING**



**Isaacson And Arfman  
Engineer's Report**

**Temporary Detention  
Plan Sheet**





---

- **Appendix B**

# **Hydrology**

# **Sandia Foundation San Mateo Site**

## **Calculations for the Proposed Pond Outlet Rating Curves**

\*S\* PROJECT NAME: Sandia Foundation, San Mateo Tract C  
 \*S\* JOB NO.  
 \*S\* DATE: June 2015  
 \*S\*  
 \*S\* INPUT FILE NAME: SF-SanMateo.hym  
 \*S\* OUTPUT FILE NAME: SF-SanMateo.out  
 \*S\* FILES LOCATION: 56-07-02 Floyd Development Services\Active Projects\ENG\AHYMO\SF-SanMateo  
 \*S\*  
 \*S\*  
 \*S\*

\*\*\*\*\*

\*S\*  
 \*\*\*\*\*

\* 100 year storm event  
 RAINFALL TYPE=2 RAIN QUARTER=0.0 RAIN ONE=2.01  
 RAIN SIX=2.35 RAIN DAY=2.75 DT=.05

\* SEDIMENT BULK CODE=1 FACTOR=1.06  
 \*  
 \*

\*S\*\*\*\* COMPUTE BASIN-Sub 1 - Golden Corral  
 COMPUTE NM HYD ID=1 HYD NO=GC DA=0.003214  
 PER A=0 PER B=0 PER C=5 PER D=95  
 TP=0.133 RAIN=-1  
 PRINT HYD ID=1 CODE=10  
 \*  
 \*

\*S\*\*\*\* COMPUTE BASIN-Sub 2 - Davita  
 COMPUTE NM HYD ID=2 HYD NO=DAVITA DA=0.001634  
 PER A=0 PER B=5 PER C=15 PER D=80  
 TP=0.133 RAIN=-1  
 PRINT HYD ID=2 CODE=10  
 \*  
 \*

\*S\*\*\*\* COMPUTE BASIN-Sub 3 - Sandia Foundation Tract C  
 COMPUTE NM HYD ID=3 HYD NO=TRCT C DA=0.004132  
 PER A=0 PER B=12.5 PER C=12.5 PER D=75  
 TP=0.133 RAIN=-1  
 PRINT HYD ID=3 CODE=10  
 \*  
 \*

ADD HYD ID=4 HYD=1.2 ID I=1 ID II=2  
 PRINT HYD ID=4 CODE=10  
 \*  
 \*

ADD HYD ID=5 HYD=3.4 ID I=3 ID II=4  
 PRINT HYD ID=5 CODE=0  
 \*  
 \*

\*S Water Quality Pond and Storage

ROUTE	RESERVOIR	ID=6	HYD=501	INFLOW	ID=5	CODE=1	ELEV(FT)
	OUTFLOW(CFS)			STORAGE(AC FT)			
	0.0			0.0			5192
	0.01			0.022			5193
	0.02			0.085			5194
	3.5775	0.109				5194.25	
	7.301			0.138			5194.5
	8.78			0.207			5195
	9.629			0.293			5195.5
	10.0			0.396			5196

FINISH

Replace  
 AHYMO input  
 file and  
 AHYMO Summary  
 file



**Sandia Foundation  
San Mateo Site**

**AHYMO Summary  
File**

RUN DATE (MON/DAY/YR) =03/23/2008  
USER NO.= AHYMO-C-9803C01UNMLIB-AH

Page 1





# Appendix C

## Hydraulics



# **Sandia Foundation San Mateo Site**

## **Existing Downstream Capacity Analysis**

## Downstream Capacity

### Analysis of existing ABF Terminal storm drain system

Elevations, lengths, and MH #s per Exhibit A of the Navajo Freight Lines Terminal Drainage Study revision dated 1/29/74 by Kruger, LAKE and ASSOCIATES Architects and Engineers.

The following MathCAD sheets are used to determine the downstream capacity by evaluating the hydraulic gradeline for a given flowrate. The equations used are from the City of Albuquerque Development Process Manual (DPM) Chapter 22, section 3B.

Point 1 is located at the Northern inlet, point 2 is located at MH #4

10 " diameter pipe leading from inlet to first manhole downstream

$$L := 91$$

$$Dia := 0.8333 \quad \text{ft}$$

$$Z_1 := 5185$$

$$R_w := \frac{Dia}{2} = 0.417 \quad \text{ft}$$

$$Z_2 := 5180.65$$

$$A_w := \pi \cdot R^2 = 0.545 \quad \text{ft}^2$$

$$S_0 := \frac{(Z_1 - Z_2)}{L} = 0.048$$

$$Q := 5 \quad \text{cfs}$$

$$n := 0.013$$

D2 represents the hydraulic gradeline at point 2. Assuming water elevation is half foot higher than top of MH #4.

$$P_w := \pi \cdot \left( \frac{Dia}{2} \right) \cdot 2 = 2.618 \quad \text{ft} \quad \text{Assuming full pipe, therefor the circumference is used as the wetted perimeter}$$

$$D_2 := 6.68$$

$$R_h := \frac{A}{P_w} = 0.208 \quad \text{ft}$$

$$S_f := \left[ \frac{(Q \cdot n)}{1.486 A \cdot R_h \left( \frac{2}{3} \right)} \right]^2 = 0.052$$

D1 represents the calculated difference between top of water elevation and invert. Assuming grate at northern inlet is covered to create more pressure.

$$D_1 := D_2 - S_0 \cdot L + S_f \cdot L = 7.07$$

Difference between top of proposed pond and invert at northern inlet = 10 ft



# **Sandia Foundation San Mateo Site**

## **Calculations for the Existing ABF Terminals Inlet Rating Curves**



Calculations for ABF inlet  
rating curves

Analysis for 10" outlet pipes from inlets

Existing Northern Inlet

$$\text{AreaOrif} := 0.5454 \quad (\text{ft})$$

$$C1 := 0.6 \quad j := 0..8$$

h :=

Elevation h north (ft)	
5186	0
5187	0.5833
5188	1.5833
5189	2.5833
5190	3.5833
5191	4.5833
5192	5.5833
5193	6.5833

$$Q_{\max} := \text{AreaOrif} \cdot C1 \cdot \sqrt{2 \cdot 32.2 \cdot h}$$

Q <sub>max</sub> =	0
	2.006
	3.304
	4.221
	4.971
	5.622
	6.205
	6.738

Existing Southern Inlet

$$\text{AreaOrif} := 0.5454 \quad (\text{ft})$$

$$C1 := 0.6 \quad j := 0..8$$

h1 :=

Elevation h north (ft)	
5186	0
5187	0.0833
5188	1.0833
5189	2.0833
5190	3.0833
5191	4.0833
5192	5.0833
5193	6.0833

$$Q_{\max 1} := \text{AreaOrif} \cdot C1 \cdot \sqrt{2 \cdot 32.2 \cdot h1}$$

Q <sub>max1</sub> =	0
	0.758
	2.733
	3.79
	4.611
	5.307
	5.921
	6.477



# **Sandia Foundation San Mateo Site**

## **Calculations for the Proposed Pond Outlet Rating Curves**

# Calculations for proposed pond outlet rating curves

From pond to northern ABF Terminal inlet, through a 12 in. pipe

h :=	
Elevation Head (ft)	
5194	0
5194.25	0.25
5194.5	0.5
5195	1
5195.5	1.5
5196	2

h1 := 1 ft  
h2 := 2 ft

Weir Opening,  $Q = C_w L H^{1.5}$

$C_w := 3$

$L := 7.9$

$$Q1 := C_w \cdot L \cdot (h1)^{1.5} = 23.7 \text{ cfs}$$

$$Q2 := C_w \cdot L \cdot (h2)^{1.5} = 67.034 \text{ cfs}$$

Orifice Opening,  $Q_{orif} = C A (2GH)^{0.5}$

$C := 0.6$

$A := 0.785$

$$Q_{orif1} := C \cdot A \cdot (2 \cdot 32.2 \cdot h1)^{0.5} = 3.78 \text{ cfs}$$

$$Q_{orif2} := C \cdot A \cdot (2 \cdot 32.2 \cdot h2)^{0.5} = 5.345 \text{ cfs}$$

$$Q_{weir} := C_w \cdot L \cdot (h)^{1.5} = \begin{pmatrix} 0 \\ 2.963 \\ 8.379 \\ 23.7 \\ 43.54 \\ 67.034 \end{pmatrix}$$

$$Q_{orif} := C \cdot A \cdot (2 \cdot 32.2 \cdot h)^{0.5} = \begin{pmatrix} 0 \\ 1.89 \\ 2.673 \\ 3.78 \\ 4.629 \\ 5.345 \end{pmatrix}$$

Since the orifice equation produces smaller flowrates it is used rather than the weir equation for the 12 inch outlet pipes that lead to the ABF Terminal inlets.



# Calculations for proposed pond outlet rating curves

From pond to southern ABF Terminal inlet, through a 12 in. pipe

$$\begin{pmatrix} h_{\text{weir}} \\ h_{\text{orifice}} \end{pmatrix} :=$$

Elevation	Wier Head (ft)	Orifice Head (ft)
5194	0	1
5194.25	0.25	1.25
5194.5	0.5	1.5
5194.75	0.75	1.75
5195	1	2

Calculations for weir surrounding  
southern 12 inch pipe outlet.

Weir Opening,  $Q = C_w L H^{1.5}$

$$\begin{aligned} C_w &:= 3 \\ L &:= 4.5 \end{aligned}$$

Orifice Opening,  $Q_{\text{orif}} = C A (2GH)^{0.5}$

$$\begin{aligned} C &:= 0.6 \\ A &:= 0.785 \end{aligned}$$

$$Q_{\text{weir}} := C_w \cdot L \cdot \begin{pmatrix} h_{\text{weir}} \end{pmatrix}^{1.5} = \begin{pmatrix} 0 \\ 1.6875 \\ 4.77297 \\ 8.76851 \\ 13.5 \end{pmatrix}$$

$$Q_{\text{orif}} := C \cdot A \cdot \begin{pmatrix} 2 \cdot 32.2 \cdot h_{\text{orifice}} \end{pmatrix}^{0.5} = \begin{pmatrix} 3.78 \\ 4.226 \\ 4.629 \\ 5 \\ 5.345 \end{pmatrix}$$

Weir controls flowrate up until water level reaches 5194.5 ft.

# **Sandia Foundation San Mateo Site**

## **Minimum Slope Calculations for Proposed 12" Pipe**



## Manning Formula:

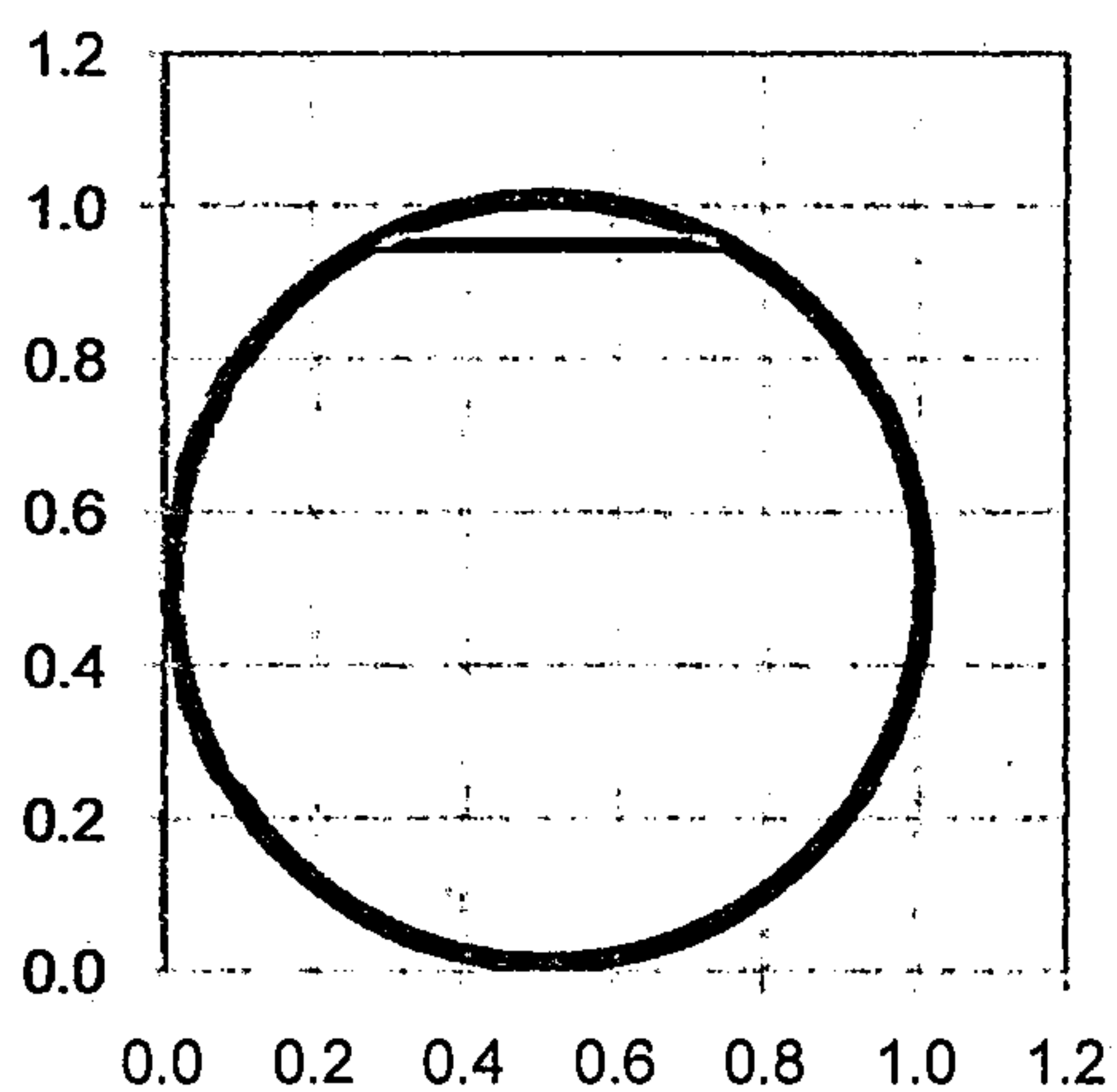
### Circular Channel

#### Input

Flow	5 cfs
Slope	0.017022223 ft/ft
Manning's n	0.013
Diameter	12 in

#### Output

Depth	0.938 ft
Flow Area	0.765 sf
Velocity	6.53 fps
Velocity Head	0.664 ft
Top Width	0.482 ft
Froude Number	0.915
Critical Depth	0.917 ft
Critical Slope	0.0171 ft/ft



# Sandia Foundation San Mateo Site

## Rundown and Spillway Calculations

Add at  
end of  
report



### Rundown Calculations

According to the drainage report from Davita's Del Norte Dialysis Center the flowrate coming into the pond on the northern entrance is about 5.5 cfs.

Weir Depth

$$h1 := 1 \text{ ft}$$

Weir Equation:  $Q = CwLH^{1.5}$

$$Cw := 3$$

$$L1 := 7.5$$

$$Q1 := Cw \cdot L1 \cdot (h1)^{1.5} = 22.5 \text{ cfs}$$

A total of about 24.8 cfs enters the pond, about 19.33 cfs enters the pond at the midway rundown

Midway Rundown

Weir Depth

$$h2 := 1 \text{ ft}$$

Weir Equation:  $Q = CwLH^{1.5}$

$$Cw := 3$$

$$L2 := 14$$

$$Q2 := Cw \cdot L2 \cdot (h2)^{1.5} = 42 \text{ cfs}$$

### Spillway calculations

Northwest Corner Spillway

Weir Depth

$$h3 := 0.7 \text{ ft}$$

Weir Equation:  $Q = CwLH^{1.5}$

$$Cw := 3$$

$$L3 := 140$$

$$Q3 := Cw \cdot L3 \cdot (h3)^{1.5} = 245.97 \text{ cfs}$$

Midway Spillway

Weir Depth

$$h4 := 0.7 \text{ ft}$$

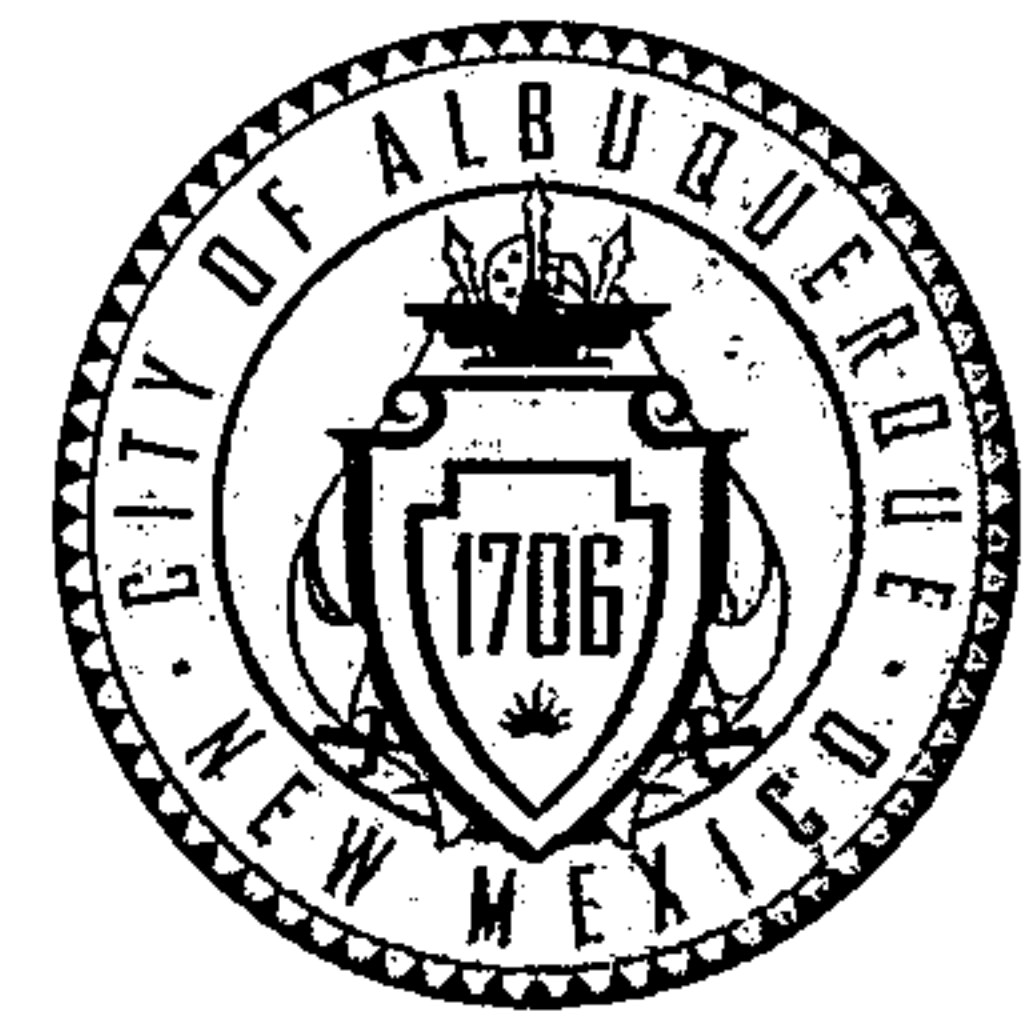
Weir Equation:  $Q = CwLH^{1.5}$

$$Cw := 3$$

$$L4 := 8.5$$

$$Q4 := Cw \cdot L4 \cdot (h4)^{1.5} = 14.934 \text{ cfs}$$

# CITY OF ALBUQUERQUE



August 21, 2015

Hugh Floyd, P.E.  
Floyd Development Services, LLC  
918 Pinehurst Road SE, Suite 102  
Rio Rancho, NM 87124

**Re: Tract A, B-1 and C-1 Sandia Addition  
Grading and Drainage Plan  
Engineer's Stamp Date 8-18-2015 (F17D095B)**

Dear Mr. Floyd,


Based upon the information provided in your submittal received 7/30/2015 and 8/19/2015, the above referenced Grading and Drainage Plan is approved based on the flowing conditions:

- Make sure that the top of beehive is constructed at 5194 and top of pipe is at 5193.
- An Erosion and Sediment Control Plan (ESC) submittal is also required. Please submit an ESC plan including a submittal sheet to Curtis Cherne for review and approval.

If the ponds are constructed and certified prior to Certification of Occupancy request for DaVita Dialysis Center (F17/D095A), then the temporary pond shown on DaVita Dialysis Center plans will be not required.

If you have any questions, you can contact me at 924-3999.

Sincerely,

  
Shahab Biazar, P.E.  
City Engineer, Planning Dept.  
Development and Building Services

C: File