

The following items concerning the Double Rainbow Drainage Plan are contained hereon:

- 1. Vicinity Map
- 2. Grading Plan
- 4. Pump Details & Calculations

As shown by the Vicinity Map, the site is located on the west side of Juan Tabo boulevard N.E. between Montgomery Boulevard N.E. and Lagrima de Oro N.E. At present, the site is undeveloped. Much of the surrounding area is developed, making this an infill site.

As shown by Panel 18 of 50 of the National Flood Insurance Program Flood Insurance Rate Maps for the city of Albuquerque, New Mexico, dated October 14, 1983, this site does not lie within a designated flood hazard zone. Further review of this mapping does not reveal downstream flooding to which this site contributes. At present, the site slopes from east to west onto adjacent undeveloped property. The site is situated down slope from Juan Tabo Boulevard N.E., which is a developed City

The Grading Plan shows 1) existing grades indicated by contours at 1'0" intervals, 2) proposed grades indicated by spot elevations and contours at 1'0" intervals, 3) the limit and character of the existing improvements, 4) the limit and character of the proposed improvements, and 5) continuity between existing and proposed grades. As shown this plan, the proposed improvements consist of the construction of a building along with adjacent paving and landscaping. Due to the fact that the site slopes away from Juan Tabo Boulevard N.E. at an average 5% gradient, it is not possible to obtain gravity drainage back to the street. Because of this, a pond is proposed to contain 100% of the 100-year developed runoff and to drain that pond with a submersible pump. The forced main discharge from the pond will discharge into Juan Tabo Boulevard N.E. Waterproofing of the adjacent walls will be necessary to allow for ponding within 15% of the structures.

The Calculations which appear hereon analyze both the existing and developed conditions for the 100-year, 6-hour rainfall event. The Procedure for 40-acre and Smaller Basins, as set forth in the Revision of Section 22.2, Hydrology of the Development Process Manual, Volume 2, Design Criteria, dated January, 1993, has been used to quantify the peak rate of discharge and volume of runoff generated. As shown by these calculations, an increase in runoff is generated. The maximum depth of the pond will be approximately 6, thereby requiring fencing of the pond area. The required volume was not calculated using the hydrograph method from the new hydrology criteria, in the event that the sumbersible pump malfunctions. Therefore, the  $V_{100}$  for the site was used so as to determine the volume of the pond. In order to provide erosion control for the pond, this area will be sodded.

#### **CALCULATIONS**

#### Site Characteristics

- Precipitation Zone = 4
- $P_{6,100} = P_{360} = 2.90$  in. Total Area  $(A_T) = 1.05$  acres Existing Land Treatment

# Treatment

5. Developed Land Treatment

_		
Treatment	Area (sf/ac)	9
В	9,900 / 0.23	21
D	35,840 / 0.82	78
D	35,840 / 0.82	

Area (sf/ac)

40,950 / 0.94

4,790 / 0.11

#### Existing Condition

1. Volume

 $E_W = (E_A A_A + E_B A_B + E_C A_C + E_D A_D) / A_T$   $E_W = [(0.80)(0.94) + (1.08)(0.11)] / 1.05 = 0.83 in.$  $V_{100} = (0.83/12)1.05 = 0.0726 \text{ ac.ft}$ ; 3,170 cf

#### 2. Peak Discharge

 $Q_p = Q_{pA} A_A + Q_{pB} A_B + Q_{pC} A_C + Q_{pD} A_D$   $Q_p = Q_{100} = (2.20)(0.94) + (2.92)(0.11) = 2.4 cfs$ 

#### Developed Condition

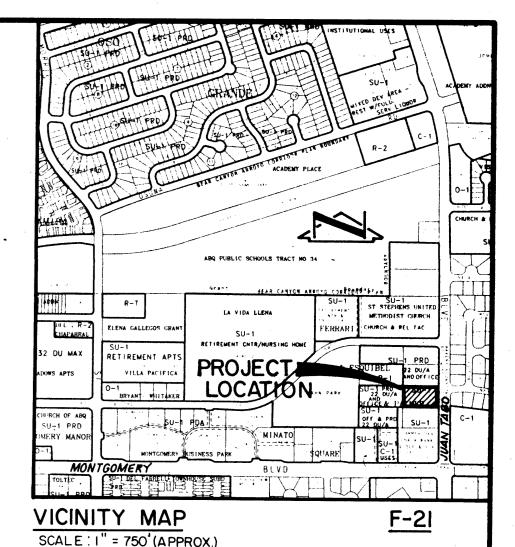
 $E_W = (E_A A_A + E_B A_B + E_C A_C + E_D A_D) / A_T$   $E_W = [(1.08)(0.23) + (2.64)(0.82)] / 1.05 = 2.30 in.$  $V_{100} = (2.30/12)(1.05) = 0.2011$  ac. ft.; 8,760 cf

## Peak Discharge

 $Q_p = Q_{pA} A_A + Q_{pB} A_B + Q_{pC} A_C + Q_{pD} A_D$   $Q_p = Q_{100} = (2.92)(0.23) + (5.25)(0.82) = 5.0 cfs$ 

- 1.  $\Delta V_{100} = 8,760 3,170 = 5,590$  cf (increase) 2.  $\Delta Q_{100} = 5.0 2.4 = 2.6$  cfs (increase)

APPROVALS	NAME	DATE
A.C.E. / DESIGN	B Menty	5/24/24
INSPECTOR		The second secon
A.C.E. / FIELD		e (,)-Symp



POND VOLUME (Calculated by the Average End Area Method)

ev (ft)	Area (ft <sup>2</sup> )	Vol (cf)	Σ Vol (cf)
10	0		
11	368	184	184
12	550	459	643
13	781	665.5	1,308.5
14	1,015	898	2,206.5
15	1,440	1,227.5	3,434
16	1,823	1,631.5	5,065.5
17	2,167	1,995	7,060.5
18	2,493	2,330	9,390.5
19	2,825	2,659	12,049.5

W.S.L. between 17 & 18 By interpolation 17.75 area of 2411.5 sf Vol = [(2167 + 2411.5)/2]0.7 = 1716.94 cf $\Sigma Vol = 7,060.5 + 1716.94 = 8,777.43 cf$ W.S.L. approximately 17.75

#### Construction Notes:

- 1. Two (2) working days prior to any excavation, contractor must contact New Mexico One Call System 260-1990, for location of existing utilities.
- 2. Prior to construction, the contractor shall excavate and verify the horizontal and vertical location of all potential obstructions. Should a conflict exist, the contractor shall notify the engineer in writing so that the conflict can be resolved with a minimum amount of delay.
- All work on this project shall be performed in accordance with applicable federal, state and local laws, rules and regulations concerning construction safety and health.
- 4. All construction within public right-of-way shall be performed in accordance with applicable City of Albuquerque Standards and Procedures.
- If any utility lines, pipelines, or underground utility lines are shown on these drawings, they are shown in an approximate manner only, and such lines may exist where none are shown. If any such existing lines are shown, the location is based upon information provided by the owner of said utility, and the information may be incomplete, or may be obsolete by the time construction commences. The engineer has conducted only preliminary investigation of the location, depth, size, or type of existing utility lines, pipelines, or underground utility lines. This investigation is not conclusive, and may not be complete, therefore, makes no representation pertaining thereto, and assumes no responsibility or liability therefor. The contractor shall inform itself of the location of any utility line, pipeline, or underground utility line in or near the area of the work in advance of and during excavation work. The contractor is fully responsible for any and all damage caused by its failure to locate, identify and preserve any and all existing utilities, pipelines, and underground utility lines. In planning and conducting excavation, the contractor shall comply with state statutes, municipal and local ordinances, rules and regulations, if any, pertaining to the location of these lines and facilities.
- 6. The design of planters and landscaped areas is not part of this plan. All planters and landscaped areas adjacent to the building(s) shall be provided with positive drainage to avoid any ponding adjacent to the structure. For construction details, refer to landscaping plan.

An Excavation/Construction Permit will be required before beginning any work within City right-of-way. An approved copy of these plans must be submitted at the time of application for this permit.

Backfill compaction shall be according to ARTERIAL street use.

Maintenance of these facilities shall be the responsibility of the owner of the property served.



GRADING AND DRAINAGE PLAN

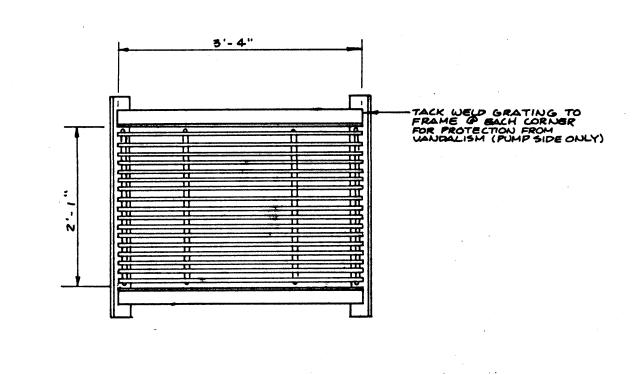
DOUBLE RAINBOW BAKERY & CAFE

NO. DATE BY REVISIONS JOB NO. 921122 15/94 M.F.D. REVISE DRAINAGE PLAN, SHOW EASEMENT, FLOOD PROOFING. DATE DRAWN BY T.P.H. 12-1993 APPROVED BY J.G.M.

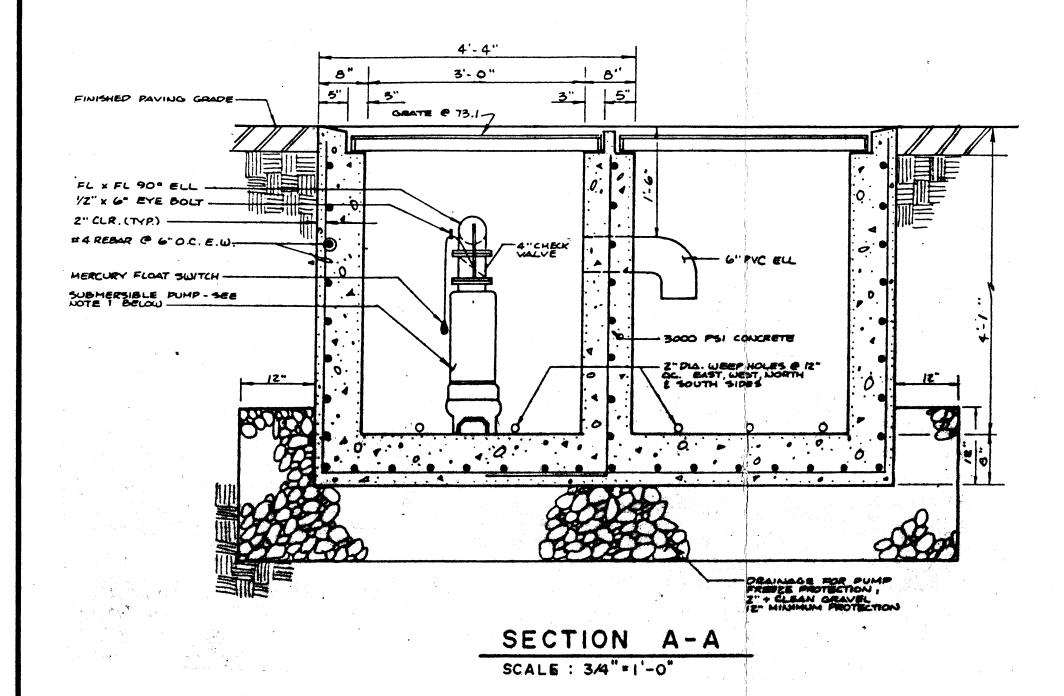
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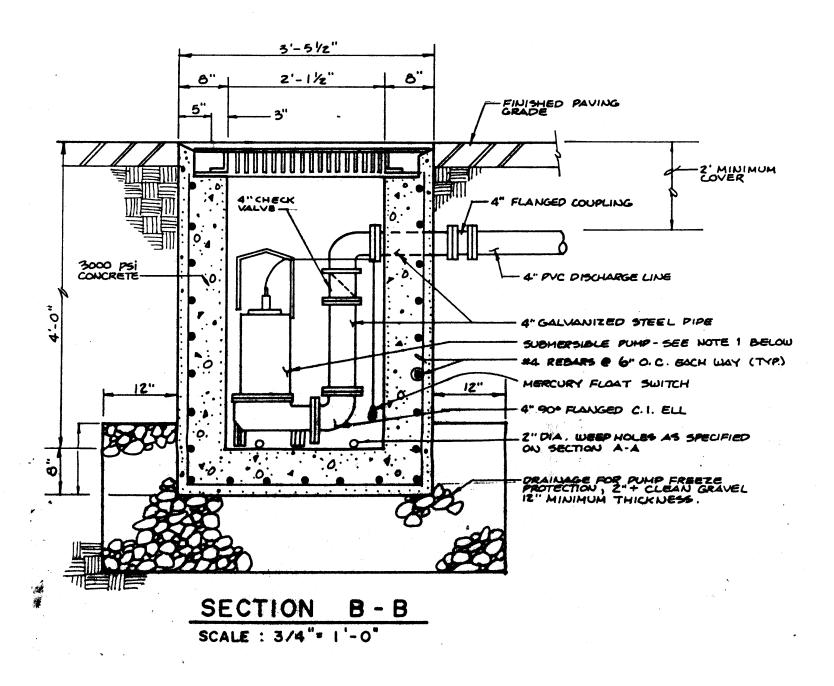
SUMP PIT AND INLET PLAN

SCALE : 3/4" = 1'-0"



TYPICAL INLET GRATE PLAN SCALE: 3/4"=1'-0"



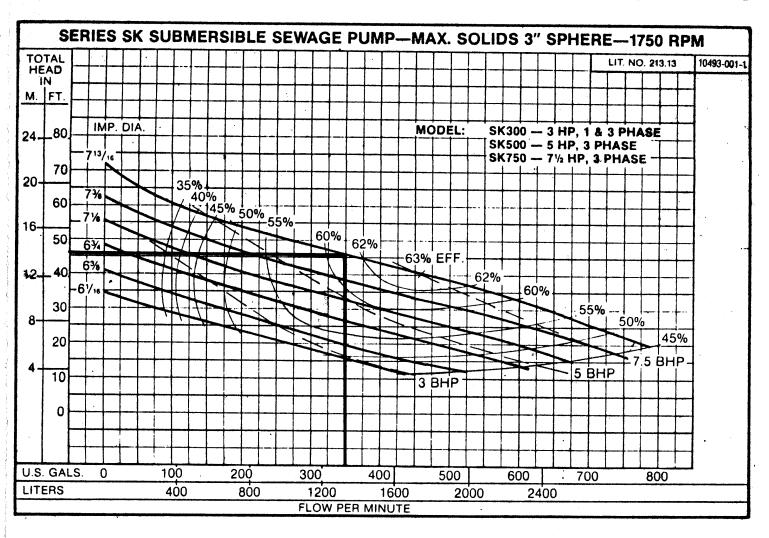


SUBMERSIBLE PUMP DETAILS & SECTIONS

DOUBLE RAINBOW BAKERY & CAFE

SECTION 200 DIMENSIONAL DRAWINGS & PERFORMANCE DATA

**HYDROMATIC** 



Pump Calculations

1. Estimated Discharge Rate 350 GPM

#### 2. Head Loss

A. Elevation 29'-10' = 19'

B. Friction (4" pipe) Type of Pipe: PVC Design C Value: 130 Chart C Value: 100 Correction Required = 0.62  $H_F = 0.2083*(100/C)^{1.85}*(q^{1.85}/d^{4.8655})$   $H_F = 6.1$  ft/100 ft (6.1/100)305 = 18.61 ft Length of Pipe = 305'±

C. Friction (4" pipe)
Type of Pipe: Steel Design C Value: 100 Chart C Value: 100 No Correction Required  $H_F = 24.12 \text{ ft/}100 \text{ ft}$ 

#### Length of Pipe = $8'\pm$

Equivalent Length of Pipe 2 90° Ell @ 11 ft ea For 22 ft 1 45° Ell @ 5 ft ea For 5 ft  $H_{F,S} = (8+22+5)(24.1/100) = 8.44 \text{ ft}$ 

## D. Total

 $H_T = H_Z + H_{F,P} + H_{F,S} = 19+18.61 + 8.44 = 46.05 ft$ 

Q = 350 GPM (1 cf/7.48 gallons) (1 min/60 sec) = 0.8 cfs

Reference: Cameron Hydraulic Data, 14th Edition Ingersoll-Rand Company, Woodcliff Lake, NM 1970, pp-27, 36 and 48.

#### Notes:

NO. DATE BY

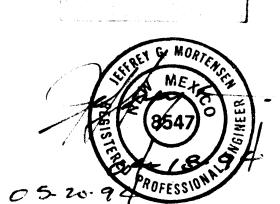
DESIGNED BY M.F.D.

DRAWN BY T.P.H.

APPROVED BY J.G.M.

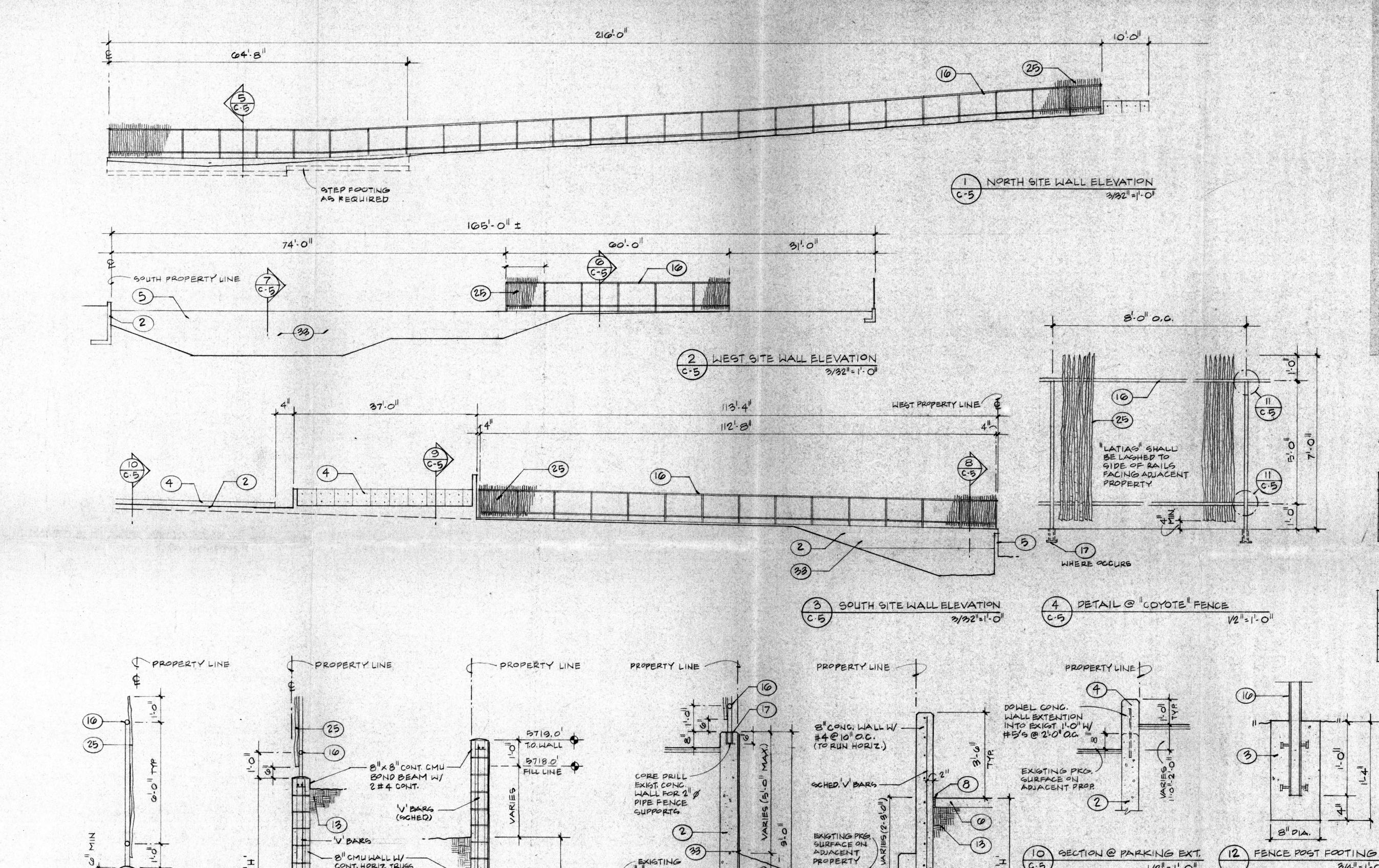
- Install one HYDRO-O-MATIC submersible pumps, Model SK500, 7½ HP motor, or approved equal. Pump installation shall include two mercury float switches with controls set for "OFF" and "ON" modes of operation.
- 2. Refer to Electrical Plans for location of pump control box, installation of electrical cable/conduit and pump/control oneline diagrams.
- Grating and frame shall be cleaned of all scale, rust and foreign materials and shall be painted with one shop coat of red oxide primer, then 2 finish coats of aluminum paint (AASHO
- Installation of the mercury float switches shall be at levels providing optimum pumping time without excessive pump cycling.

MAY 2 3 1994



REVISIONS 921122 12-1993

JEFF MORTENSEN & ASSOCIATES, INC. 6010-B MIDWAY PARK BLVD. N.E. ALBUQUERQUE, NEW MEXICO 87109 ENGINEERS & SURVEYORS (505)345-4250



EXIGTING OF UNDETERMINED WIDTH

SECTION @ EXIGT. RET. WALL

1X BARS

#4@ 1211 0,C,

SECTION @ WEST POND WALL

V BARDOWELS SAME SIZE & SPACING AG V BARS

X'BARS-

9 SECTION @ RET./GUARD WALL

#4@12"0.c -

2#4 CONT. -

-8" CMU WALL W/--CONT. HORIZ TRUGG TYPE DURWALL @ 16" O.C. VERT.

SECTION @ LOWER PKG.

'V'BAR DOWELS

SAME SIZE AND SPACING AS IV' BARG

(0.5)

8"x8" CONT CMU BOND BEAM W/ 2#4 CONT.

V BAR DOWELS

6

(c.5)

SAME SIZE & SPACING AS 'V' BARS

8" CMU WALL W/CONT. — HORIZ. TRUGG TYPE DURWALL @ 16" O.C.

(3)

KEYED NOTES

#### SITE WALLS AND PAVING (" SEE STRUCTURAL DRAWINGS)

EXISTING REIN. CONCRETE FOOTING (V.I.F.)
EXISTING REIN. CONCRETE RET. WALL (V.I.F.)
REIN. CONCRETE FOOTING ("L" FOOTING AT PROPERTY LINE) "
REIN. CONCRETE RET. WALL- ARCHITECTURAL WHERE EXPOSED

TO VIEW (SEE ELEVATIONS FOR JOINT AND TIE PATTERN) REIN. CMU WALL\* (CROWN TOP COURSE TO DRAIN)

4" REIN. CONC. SLAB ON GRADE" (SEE PLAN FOR JOINT PATTERN) SLIP RESISTANT SURFACE AT RAMP AND STAIR 6' REIN. CONC. SLAB AT TRASH ENCLOSURE APRON 1/2" EXPANSION JOINT OF COMPRESSIBLE FILLER 1/2" TROWELED CONTROL JOINT (SEE DETAIL)

PLASTIC CONE SNAP TIE PATTERN CAST-IN-PLACE RUSTICATION JOINT (SEE DETAIL 18/C-4)

ASPHALT PAVING

COMPACTED FILL CONCRETE CURB (SEE DETAIL)

#### HANDRAILS / GUARDRAILS / FENCING

1 1/2" O.D. STANDARD STEEL TUBING (PER ANSI AND ADA GUIDELINES)
2" O.D. STANDARD UNTREATED STEEL FENCE RAIL
STEEL PIPE SLEEVE WITH MIN. OF 2 ANCHOR STUDS. GROUT SOLID (I.D. MAX. 1/2" LARGER THAN VERTICAL RAIL SUPPORT)

SHRINK RESISTANT GROUT 3/8" STEEL ROD STOCK

3/8" STEEL PLATE (3/16" RADIUS AT ALL EXPOSED EDGES) 3/4 X 3/4 X 3/16 STEEL ANGLE FRAME W/ WELDED MITERED CORNERS 4" O.C. STEEL MESH OF 3/16" ROD (WELD TO FRAME AS REQ'D)
3/8" STEEL ROD WALL MOUNTED HANDRAIL SUPPORT

MACHINE BOLT AND SPACER 6" "LATIA" SLATS LASHED TO FENCE RAILS WITH BLACK WIRE (CUT TO UNIFORM HEIGHT AFTER INSTALLATION)

4" O.D. STEEL PIPE FILLED SOLID W/ CONC.
1 1/2" O.D. PAINTED STEEL BIKE RACK LOOP AND H.C. SIGN LOOP 4 X 4 X 1/4 STEEL ANGLE W/ ANCHORS, CAST-IN-PLACE DOCK BUMPER

WALKWAY LIGHT CAST IN CONC. WALL OR BOLLARD CAST-IN-PLACE CONCRETE BOLLARD WELD AS REQUIRED

"THOROSEAL" CEMENTIOS WATER PROOF
MEMBRANE @ EXPOSED RETAINING WALLS
AROUND DETENTION POND, APPLY TO WALLS AND FOOTINGS.

#### SITE WALL REIN, SCHEDULES

'H' MAX	الما	V' BARS	I'X' BARG
≤ 4'-0"	2'-0"	#4@10"	
6-01	31-411	#4 @ 121	
8-011	4-81	#5@12"	

'H' MAX,	'A'	V'BARG	X BARG
£ 4 ".0"	21-011	#4@241	#3@1611
6-0"	3'-4"	#50161	#4@101
8'-0"	41-811	#40881	#5@ 12"



FENCE POST FOOTING

MAY 2 3 1994

3/4"=1-0"

10 SECTION @ PARKING EXT.

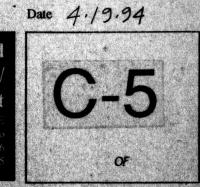
(I) DETAIL @ FENCE JOINTS

FLATTEN-PIPE END TO JI DIA. TO WELD (TYP.)

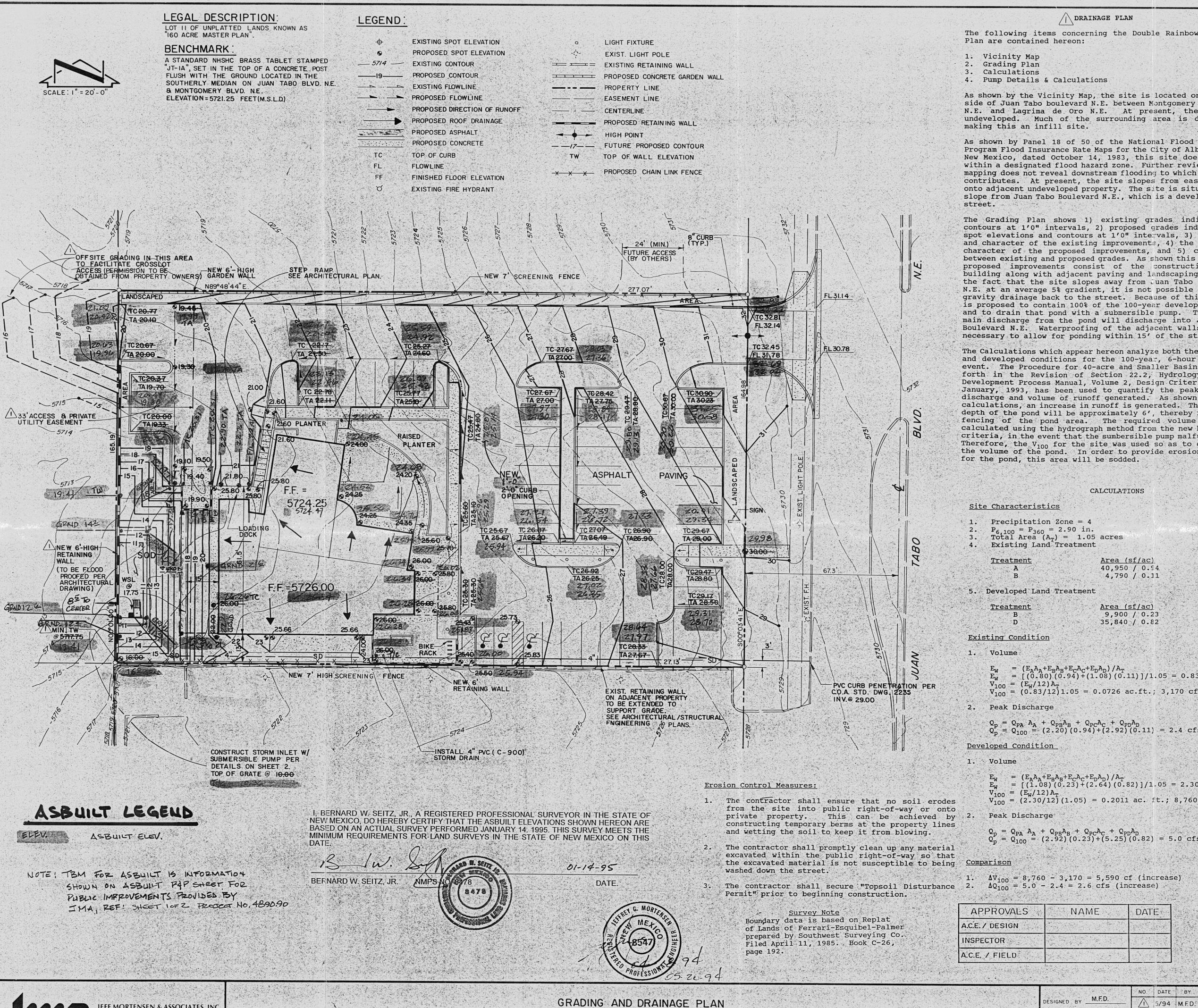


Juan Tabo NE Albuquerque / New Mexico

Drawn By KK.



Drawing SITE WALL ELEV. / DETAILS



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#### CALCULATIONS

#### Site Characteristics

1. Precipitation Zone = 4

2.  $P_{6,100} = P_{360} = 2.90$  in. 3. Total Area  $(A_T) = 1.05$  acres 4. Existing Land Treatment

> Area (sf/ac) 40,950 / 0.94 Treatment 4,790 / 0.11

5. Developed Land Treatment

Area (sf/ac) Treatment 9,900 / 0.23 35,840 / 0.82

#### Existing Condition

1. Volume

=  $(E_A A_A + E_B A_B + E_C A_C + E_D A_D) / A_T$ = [(0.80)(0.94) + (1.08)(0.11)] / 1.05 = 0.83 in.

Peak Discharge

 $Q_p = Q_{PA} A_A + Q_{PB} A_B + Q_{PC} A_C + Q_{PD} A_D$   $Q_p = Q_{100} = (2.20)(0.94) + (2.92)(0.11) = 2.4 cfs$ 

#### Developed Condition

1. Volume

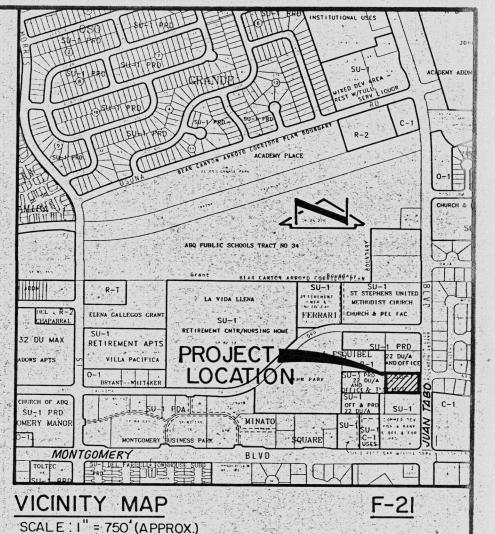
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1.  $\Delta V_{100} = 8,760 - 3,170 = 5,590$  cf (increase)

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	A.C.E. / DESIGN	统统计划的	
* *	INSPECTOR		
	A.C.E. / FIELD	<b>学者为</b> 学的文学体	(1) (1) (1)
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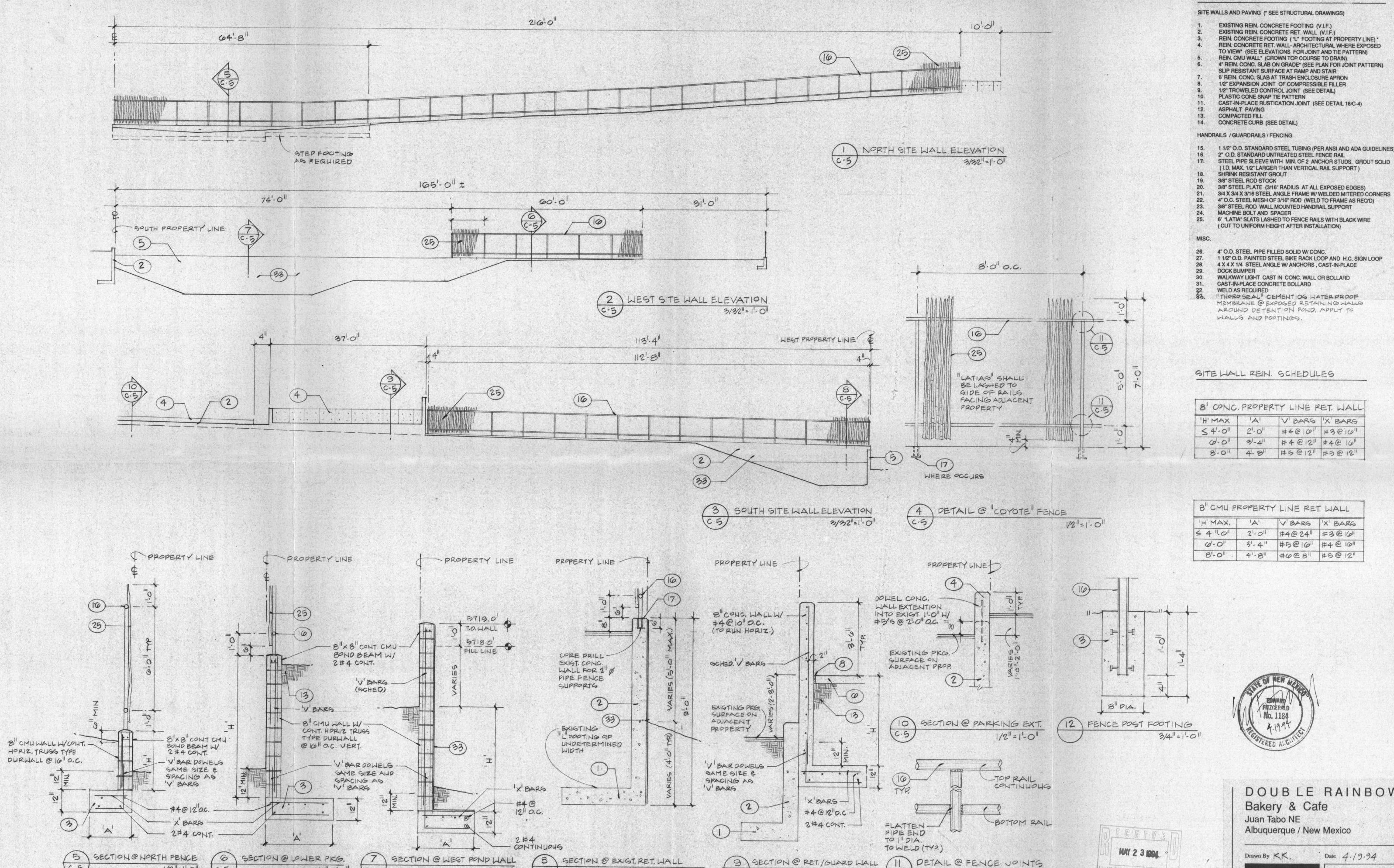
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EFF MORTENSEN & ASSOCIATES, INC. 6010-B MIDWAY PARK BLVD. N.E. ALBUQUERQUE, NEW MEXICO 87109 NGINEERS & SURVEYORS (505)345-4250

DOUBLE RAINBOW BAKERY & CAFE

DESIGNED BY M.F.D. 921122 5/94 M.F.D. REVISE DRAINAGE PLAN, SHOW EASEMENT, FLOOD PROOFING 12-1993 APPROVED BY J.G.M.



(0.5)

1/2"=1-01

KEYED NOTES

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15. 1 1/2" O.D. STANDARD STEEL TUBING (PER ANSI AND ADA GUIDELINES) 2" O.D. STANDARD UNTREATED STEEL FENCE RAIL

STEEL PIPE SLEEVE WITH MIN. OF 2 ANCHOR STUDS. GROUT SOLID (I.D. MAX. 1/2" LARGER THAN VERTICAL RAIL SUPPORT)

3/8" STEEL PLATE (3/16" RADIUS AT ALL EXPOSED EDGES)

4" O.C. STEEL MESH OF 3/16" ROD (WELD TO FRAME AS REQ'D) 3/8" STEEL ROD WALL MOUNTED HANDRAIL SUPPORT

6' "LATIA" SLATS LASHED TO FENCE RAILS WITH BLACK WIRE

4" O.D. STEEL PIPE FILLED SOLID W/ CONC. 1 1/2" O.D. PAINTED STEEL BIKE RACK LOOP AND H.C. SIGN LOOP 4 X 4 X 1/4 STEEL ANGLE W/ ANCHORS, CAST-IN-PLACE

MEMBRANE @ EXPOGED RETAINING WALLS AROUND DETENTION POND, APPLY TO

#### SITE WALL REIN, SCHEDULES

21-011		en a francisco problem en esperante anticipar de la constanta
5-0	#40 0	#301011
3-411	#4@121	#4@ 161
4-81	#5@1211	#5@ 12"
	31-411	3-41 #4@121

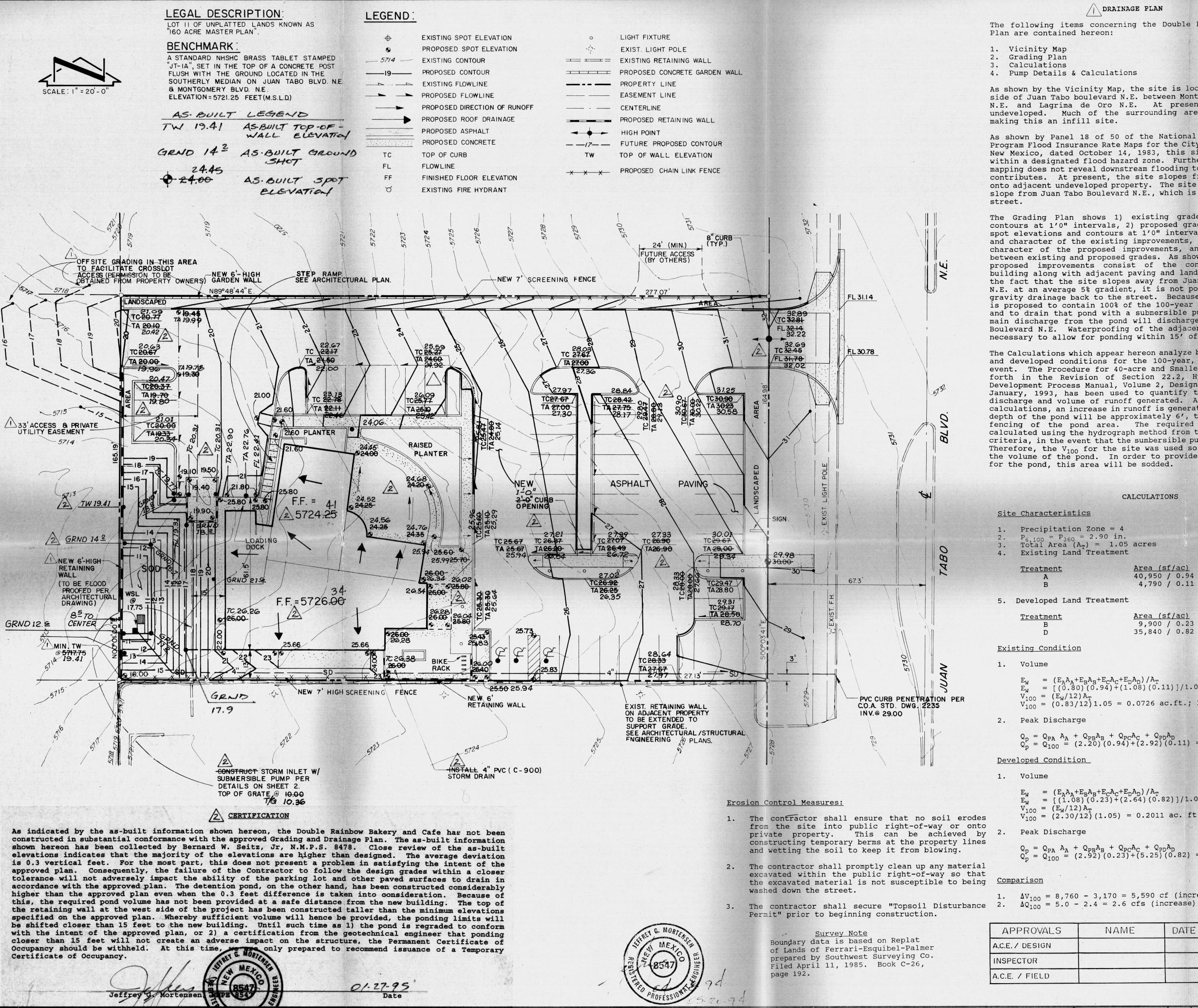
'H' MAX,	'A'	V'BARG	'X' BARG
£ 4 11.01	21-011	#4@241	#3@1611
6-01	3'-4"	#501011	#4@1011
8'-0"	41-811	#608	#5@121

## DOUBLE RAINBOW Bakery & Cafe

Albuquerque / New Mexico



Drawing SITE WALL ELEV! / DETAILS



The following items concerning the Double Rainbow Drainage Plan are contained hereon:

- 1. Vicinity Map
- 2. Grading Plan
- 3. Calculations
- 4. Pump Details & Calculations

As shown by the Vicinity Map, the site is located on the west side of Juan Tabo boulevard N.E. between Montgomery Boulevard N.E. and Lagrima de Oro N.E. At present, the site is undeveloped. Much of the surrounding area is developed, making this an infill site.

As shown by Panel 18 of 50 of the National Flood Insurance Program Flood Insurance Rate Maps for the City of Albuquerque, New Mexico, dated October 14, 1983, this site does not lie within a designated flood hazard zone. Further review of this mapping does not reveal downstream flooding to which this site contributes. At present, the site slopes from east to west onto adjacent undeveloped property. The site is situated down slope from Juan Tabo Boulevard N.E., which is a developed City

The Grading Plan shows 1) existing grades indicated by contours at 1'0" intervals, 2) proposed grades indicated by spot elevations and contours at 1'0" intervals, 3) the limit and character of the existing improvements, 4) the limit and character of the proposed improvements, and 5) continuity between existing and proposed grades. As shown this plan, the proposed improvements consist of the construction of a building along with adjacent paving and landscaping. Due to the fact that the site slopes away from Juan Tabo Boulevard N.E. at an average 5% gradient, it is not possible to obtain gravity drainage back to the street. Because of this, a pond is proposed to contain 100% of the 100-year developed runoff and to drain that pond with a submersible pump. The forced main discharge from the pond will discharge into Juan Tabo Boulevard N.E. Waterproofing of the adjacent walls will be necessary to allow for ponding within 15' of the structures.

The Calculations which appear hereon analyze both the existing and developed conditions for the 100-year, 6-hour rainfall event. The Procedure for 40-acre and Smaller Basins, as set forth in the Revision of Section 22.2, Hydrology of the Development Process Manual, Volume 2, Design Criteria, dated January, 1993, has been used to quantify the peak rate of discharge and volume of runoff generated. As shown by these calculations, an increase in runoff is generated. The maximum depth of the pond will be approximately 6', thereby requiring fencing of the pond area. The required volume was not calculated using the hydrograph method from the new hydrology criteria, in the event that the sumbersible pump malfunctions. Therefore, the  $V_{100}$  for the site was used so as to determine the volume of the pond. In order to provide erosion control for the pond, this area will be sodded.

#### CALCULATIONS

Area (sf/ac)

40,950 / 0.94

4,790 / 0.11

#### Site Characteristics

- 1. Precipitation Zone = 4
- $P_{6,100} = P_{360} = 2.90 \text{ in.}$ Total Area  $(A_T) = 1.05 \text{ acres}$ 4. Existing Land Treatment
- Treatment

Area (sf/ac) Treatment 9,900 / 0.23 35,840 / 0.82

#### Existing Condition

#### 1. Volume

 $E_W = (E_A A_A + E_B A_B + E_C A_C + E_D A_D) / A_T$   $E_W = [(0.80)(0.94) + (1.08)(0.11)] / 1.05 = 0.83 in.$  $V_{100} = (0.83/12)1.05 = 0.0726 \text{ ac.ft.}; 3,170 \text{ cf}$ 

2. Peak Discharge

 $Q_p = Q_{PA} A_A + Q_{PB} A_B + Q_{PC} A_C + Q_{PD} A_D$   $Q_p = Q_{100} = (2.20)(0.94) + (2.92)(0.11) = 2.4 cfs$ 

#### Developed Condition

#### 1. Volume

 $E_W = (E_A A_A + E_B A_B + E_C A_C + E_D A_D) / A_T$   $E_W = [(1.08)(0.23) + (2.64)(0.82)] / 1.05 = 2.30 in.$  $V_{100} = (2.30/12)(1.05) = 0.2011$  ac. ft.; 8,760 cf

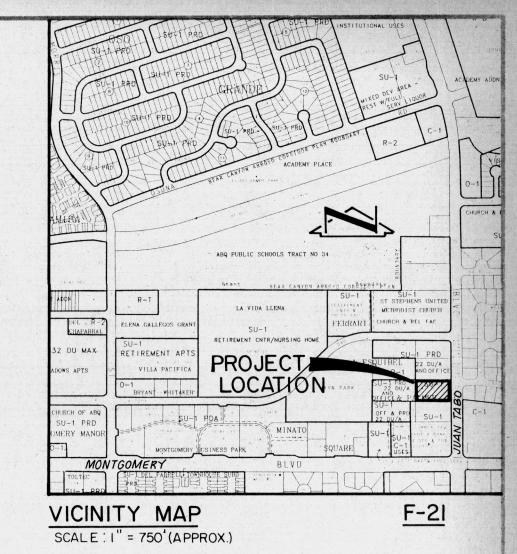
Peak Discharge

 $Q_p = Q_{PA} A_A + Q_{PB} A_B + Q_{PC} A_C + Q_{PD} A_D$   $Q_p = Q_{100} = (2.92)(0.23) + (5.25)(0.82) = 5.0 cfs$ 

1.  $\Delta V_{100} = 8,760 - 3,170 = 5,590 \text{ cf (increase)}$ 

PPROVED BY J.G.M.

APPROVALS	NAME	DATE
A.C.E. / DESIGN		
INSPECTOR		
A.C.E. / FIELD		



POND VOLUME (Calculated by the Average End Area Method)

ev (ft)	Area (ft <sup>2</sup> )	Vol (cf)	Σ Vol (cf)
10	0		
11	368	184	184
12	550	459	643
13	781	665.5	1,308.5
14	1,015	898	2,206.5
15	1,440	1,227.5	3,434
16	1,823	1,631.5	5,065.5
17	2,167	1,995	7,060.5
18	2,493	2,330	9,390.5
19	2,825	2,659	12,049.5

W.S.L. between 17 & 18 By interpolation 17.75 area of 2411.5 sf Vol = [(2167 + 2411.5)/2]0.7 = 1716.94 cf $\Sigma Vol = 7,060.5 + 1716.94 = 8,777.43 cf$ W.S.L. approximately 17.75

#### Construction Notes:

- 1. Two (2) working days prior to any excavation, contractor must contact New Mexico One Call System 260-1990, for location of existing utilities.
- 2. Prior to construction, the contractor shall excavate and verify the horizontal and vertical location of all potential obstructions. Should a conflict exist, the contractor shall notify the engineer in writing so that the conflict can be resolved with a minimum amount of delay.
- All work on this project shall be performed in accordance with applicable federal, state and local laws, rules and regulations concerning construction safety and health.
- 4. All construction within public right-of-way shall be performed in accordance with applicable City of Albuquerque Standards and Procedures.
- 5. If any utility lines, pipelines, or underground utility lines are shown on these drawings, they are shown in an approximate manner only, and such lines may exist where none are shown. If any such existing lines are shown, the location is based upon information provided by the owner of said utility, and the information may be incomplete, or may be obsolete by the time construction commences. The engineer has conducted only preliminary investigation of the location, depth, size, or type of existing utility lines, pipelines, or underground utility lines. This investigation is not conclusive, and may not be complete, therefore, makes no representation pertaining thereto, and assumes no responsibility or liability therefor. The contractor shall inform itself of the location of any utility line, pipeline, or underground utility line in or near the area of the work in advance of and during excavation work. The contractor is fully responsible for any and all damage caused by its failure to locate, identify and preserve any and all existing utilities, pipelines, and underground utility lines. In planning and conducting excavation, the contractor shall comply with state statutes, municipal and local ordinances, rules and regulations, if any, pertaining to the location of these lines and facilities.
- 6. The design of planters and landscaped areas is not part of this plan. All planters and landscaped areas adjacent to the building(s) shall be provided with positive drainage to avoid any ponding adjacent to the structure. For construction details, refer to landscaping plan.
- 7. An Excavation/Construction Permit will be required before beginning any work within City right-of-way. An approved copy of these plans must be submitted at the time of application for this permit.
- Backfill compaction shall be according to ARTERIAL street use.
- 9. Maintenance of these facilities shall be the responsibility of the owner of the property served.

15/94 M.F.D. REVISE DRAINAGE PLAN, SHOW EASEMENT, FLOOD PROOFING. 2 01/95 JM AS. BUILT & CERTIFY

10.5

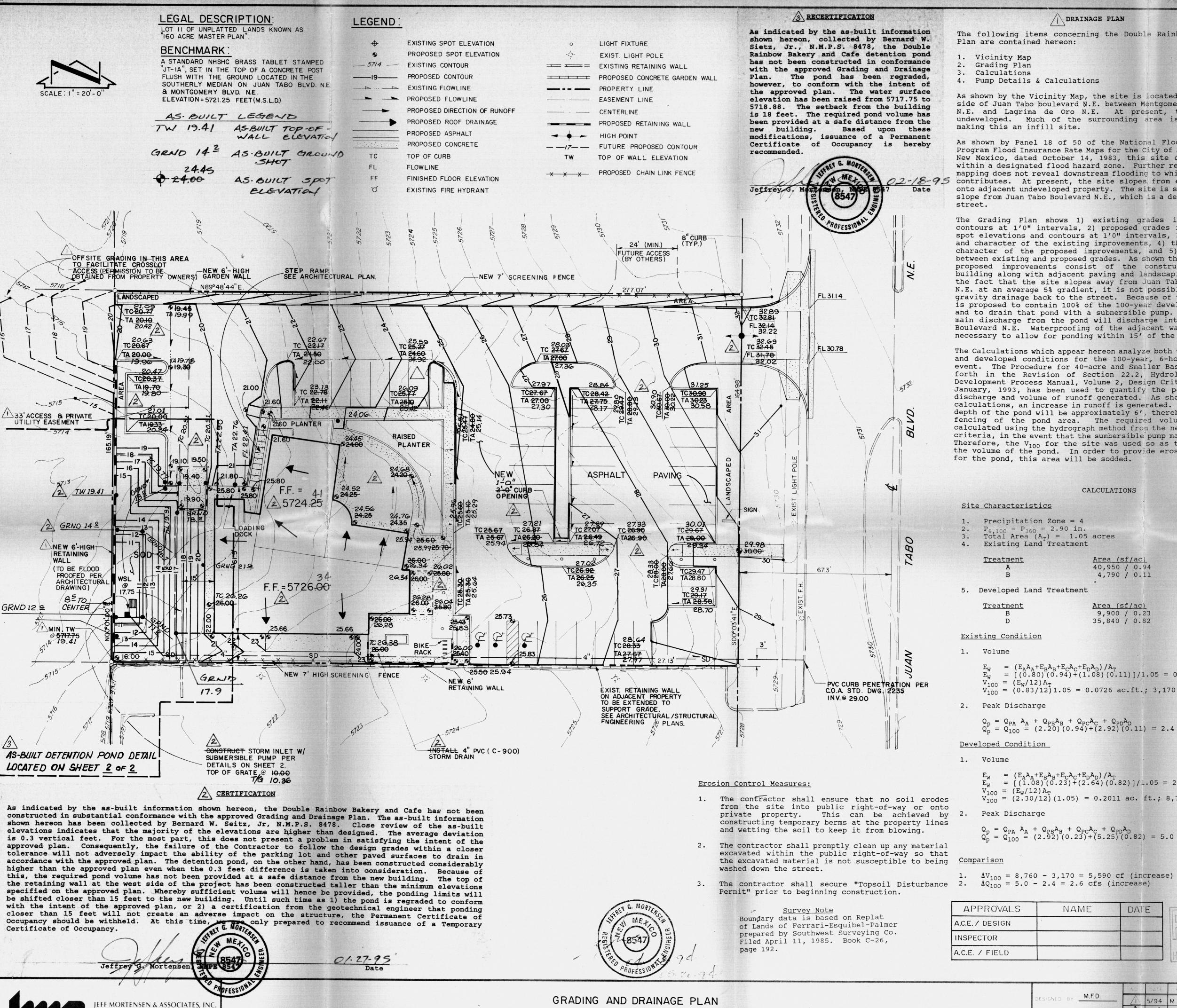
21.6

921122 12-1993

GRADING AND DRAINAGE PLAN

DOUBLE RAINBOW BAKERY & CAFE

EFF MORTENSEN & ASSOCIATES, INC 6010-B MIDWAY PARK BLVD. N.E BUQUERQUE, NEW MEXICO 87109 NGINEERS & SURVEYORS (505)345-4250



The following items concerning the Double Rainbow Drainage Plan are contained hereon:

- 1. Vicinity Map
- 2. Grading Plan
- 4. Pump Details & Calculations

As shown by the Vicinity Map, the site is located on the west side of Juan Tabo boulevard N.E. between Montgomery Boulevard N.E. and Lagrima de Oro N.E. At present, the site is undeveloped. Much of the surrounding area is developed, making this an infill site.

As shown by Panel 18 of 50 of the National Flood Insurance Program Flood Insurance Rate Maps for the City of Albuquerque, New Mexico, dated October 14, 1983, this site does not lie within a designated flood hazard zone. Further review of this mapping does not reveal downstream flooding to which this site 2-/8-95 contributes. At present, the site slopes from east to west onto adjacent undeveloped property. The site is situated down slope from Juan Tabo Boulevard N.E., which is a developed City

> The Grading Plan shows 1) existing grades indicated by contours at 1'0" intervals, 2) proposed grades indicated by spot elevations and contours at 1'0" intervals, 3) the limit and character of the existing improvements, 4) the limit and character of the proposed improvements, and 5) continuity between existing and proposed grades. As shown this plan, the proposed improvements consist of the construction of a building along with adjacent paving and landscaping. Due to the fact that the site slopes away from Juan Tabo Boulevard N.E. at an average 5% gradient, it is not possible to obtain gravity drainage back to the street. Because of this, a pond is proposed to contain 100% of the 100-year developed runoff and to drain that pond with a submersible pump. The forced main discharge from the pond will discharge into Juan Tabo Boulevard N.E. Waterproofing of the adjacent walls will be necessary to allow for ponding within 15' of the structures.

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#### CALCULATIONS

#### Site Characteristics

- 1. Precipitation Zone = 4
- $P_{6,100} = P_{360} = 2.90 \text{ in.}$ Total Area  $(A_T) = 1.05 \text{ acres}$

<u>Treatment</u>	Area (sf/ac)	%
A	40,950 / 0.94	89.5
В	4,790 / 0.11	10.5
Developed Land Treatment		
Treatment	Area (sf/ac)	%

9,900 / 0.23

35,840 / 0.82

#### Existing Condition

=  $(E_A A_A + E_B A_B + E_C A_C + E_D A_D) / A_T$ = [(0.80)(0.94) + (1.08)(0.11)] / 1.05 = 0.83 in. $V_{100} = (E_W/12) A_T$  $V_{100} = (0.83/12)1.05 = 0.0726 \text{ ac.ft.}; 3,170 \text{ cf}$ 

2. Peak Discharge

 $Q_p = Q_{PA} A_A + Q_{PB} A_B + Q_{PC} A_C + Q_{PD} A_D$   $Q_p = Q_{100} = (2.20)(0.94) + (2.92)(0.11) = 2.4 cfs$ 

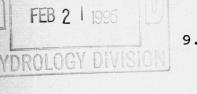
#### Developed Condition

 $E_W = (E_A A_A + E_B A_B + E_C A_C + E_D A_D) / A_T$   $E_W = [(1.08)(0.23) + (2.64)(0.82)] / 1.05 = 2.30 in.$  $V_{100} = (2.30/12)(1.05) = 0.2011$  ac. ft.; 8,760 cf

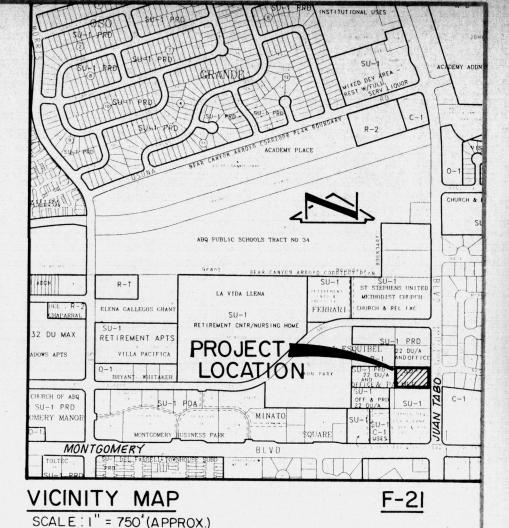
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APPROVALS	NAME	DATE
A.C.E. / DESIGN		
INSPECTOR		
A.C.E. / FIELD		



21.6



POND VOLUME (Calculated by the Average End Area Method)

lev (ft)	Area (ft <sup>2</sup> )	Vol (cf)	Σ Vol (cf)
10.4	0 ^		
11	<del>368</del> 130 <b>3</b>	39.0 184 3	184-39.0/3
12	<del>-550</del> 275	<b>2025</b> 459	643 241.5
13	<del>781</del> 585	430 665.5	1,308.5 671.5
14	1,015 940	7625 <del>898</del>	2,206.5 1434
15	<del>1,440</del> 1160	1050 <del>1,227.5</del>	3,434 2483.5
16	<del>1,823</del> <b>[397</b>	1278 <del>1,631.5</del>	5,065.5-3762.5
17	<del>2,167</del> <b>16</b> 39	1518 <del>1,995</del>	7,060.5-5280.5
18	<del>2,493</del> 1876	17515 <del>2,330</del>	9,390.5 7038.0
19	<del>2,825</del> 2083	19795 <del>2 , 659 -</del>	12,049.5 9017.5

W.S.L. between 17 & 18 18.88 3 By interpolation 17.75 area of 2411.5 sf Vol = [(2167 + 2411.5)/2]0.7 = 1716.94 cf $\Sigma Vol = 7,060.5 + 1716.94 = 8,777.43 cf$ W.S.L. approximately 17.75 18.88/3

#### Construction Notes:

- 1. Two (2) working days prior to any excavation, contractor must contact New Mexico One Call System 260-1990, for location of existing utilities.
- 2. Prior to construction, the contractor shall excavate and verify the horizontal and vertical location of all potential obstructions. Should a conflict exist, the contractor shall notify the engineer in writing so that the conflict can be resolved with a minimum amount of delay.
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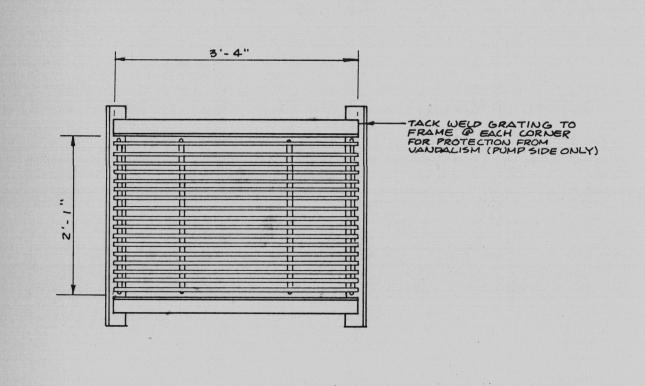
010-B MIDWAY PARK BLVD. N.E LBUQUERQUE, NEW MEXICO 87109 NGINEERS & SURVEYORS (505)345-4250

DOUBLE RAINBOW BAKERY & CAFE

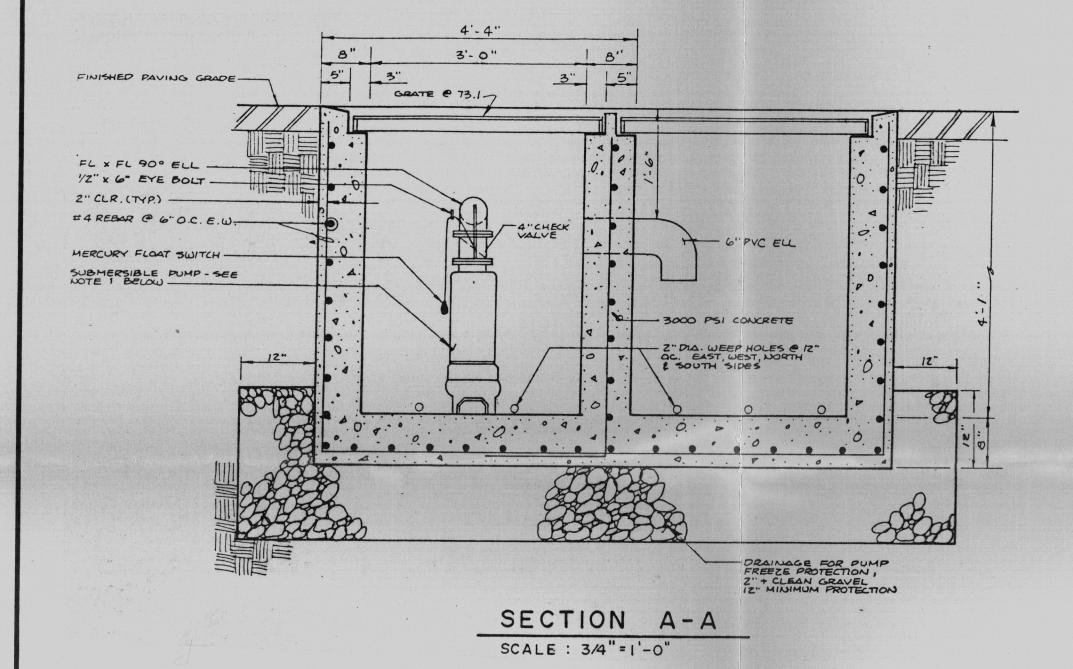
1 5/94 M.F.D. REVISE DRAINAGE PLAN, SHOW EASEMENT, FLOOD PROOFING 921122 2 01/95 JM AS. BUILT & CERTIFY T.P.H. 12-1993 3 2/95 SCK AS-BUILT AND RECERTIFY PPROVED BY J.G.M.

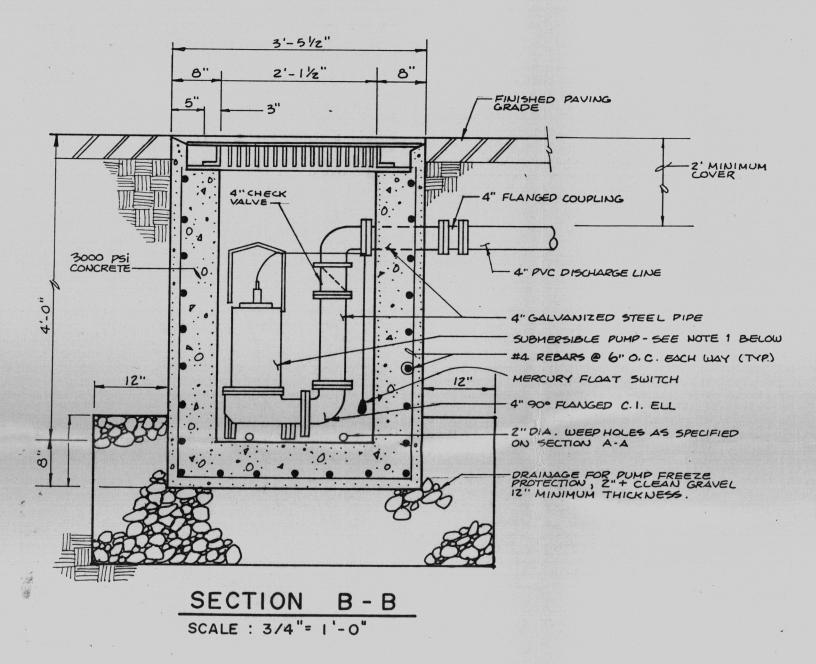
SUMP PIT AND INLET PLAN

SCALE : 3/4" = 1'-0"



# TYPICAL INLET GRATE PLAN SCALE: 3/4"=1'-0"





# 16.2 TW 19.41 F.F. = 5726.34 TW 19.41

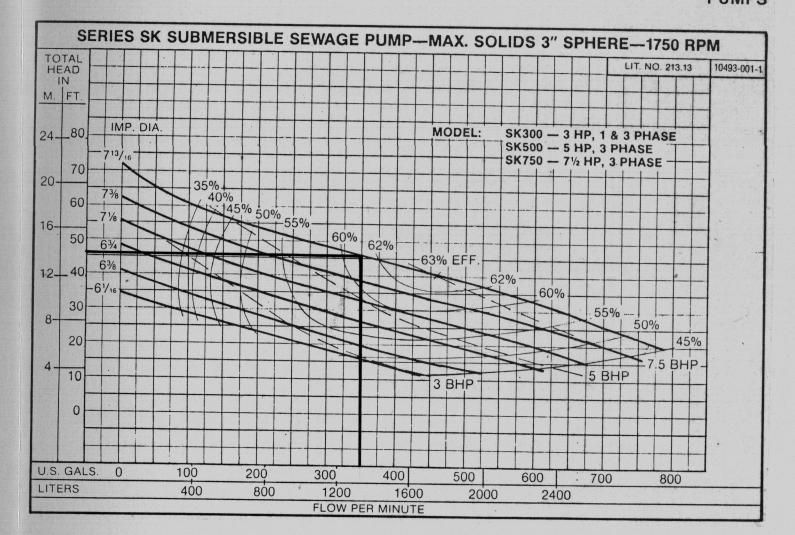
### 3 RECERTIFICATION

As indicated by the as-built information shown hereon, collected by Bernard W. Sietz, Jr., N.M.P.S. 8478, the Double Rainbow Bakery and Cafe detention pond has not been constructed in conformance with the approved Grading and Drainage Plan. The pond has been regraded, however, to conform with the intent of the approved plan. The water surface elevation has been raised from 5717.75 to 5718.88. The setback from the building is 18 feet. The required pond volume has been provided at a safe distance from the new building. Based upon these modifications, issuance of a Permanent Certificate of Occupancy is hereby



SECTION 200 DIMENSIONAL DRAWINGS & PERFORMANCE DATA

# HYDROMATIC



### Pump Calculations

- 1. Estimated Discharge Rate 350 GPM
- 2. Head Loss
  - A. Elevation 29'-10' = 19'
  - B. Friction (4" pipe) Type of Pipe: PVC Design C Value: 130 Chart C Value: 100 Correction Required = 0.62  $H_F = 0.2083*(100/C)^{1.85}*(q^{1.85}/d^{4.8655})$  $H_F = 6.1 \text{ ft/}100 \text{ ft} \quad (6.1/100)305 = 18.61 \text{ ft}$ Length of Pipe = 305'±
  - C. Friction (4" pipe) Type of Pipe: Steel Design C Value: 100 Chart C Value: 100 No Correction Required  $H_F = 24.12 \text{ ft/}100 \text{ ft}$

Length of Pipe = 8'±

Equivalent Length of Pipe 2 90° Ell @ 11 ft ea For 22 ft 1 45° Ell @ 5 ft ea For 5 ft  $H_{F,S} = (8+22+5)(24.1/100) = 8.44 \text{ ft}$ 

 $H_T = H_Z + H_{F,P} + H_{F,S} = 19+18.61 + 8.44 = 46.05 ft$ 

Q = 350 GPM (1 cf/7.48 gallons) (1 min/60 sec) = 0.8 cfs

Reference: Cameron Hydraulic Data, 14th Edition Ingersoll-Rand Company, Woodcliff Lake, NM 1970, pp-27, 36 and 48.

## Notes:

- 1. Install one HYDRO-O-MATIC submersible pumps, Model SK500,  $7\frac{1}{2}$  HP motor, or approved equal. Pump installation shall include two mercury float switches with controls set for "OFF" and "ON" modes of operation.
- 2. Refer to Electrical Plans for location of pump control box, installation of electrical cable/conduit and pump/control oneline diagrams.
- 3. Grating and frame shall be cleaned of all scale, rust and foreign materials and shall be painted with one shop coat of red oxide primer, then 2 finish coats of aluminum paint (AASHO
- 4. Installation of the mercury float switches shall be at levels providing optimum pumping time without excessive pump cycling.

AS-BUILT DETENTION POND DETAIL SCALE; 1"= 201

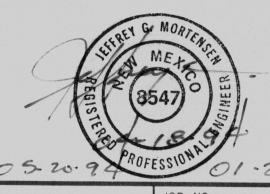
AS-BUILT GROUND ELEVATIONS

LEGEND

OTC 19.85 AS-BUILT SPOT ELEVATIONS - AS-BUILT CONTOURS ----- AS-BUILT MAXIMUM WSL

CONCRETE

RETAINING WALL



JEFF MORTENSEN & ASSOCIATES, INC. 6010-B MIDWAY PARK BLVD. N.E. ALBUQUERQUE, NEW MEXICO 87109

ENGINEERS & SURVEYORS (505)345-4250

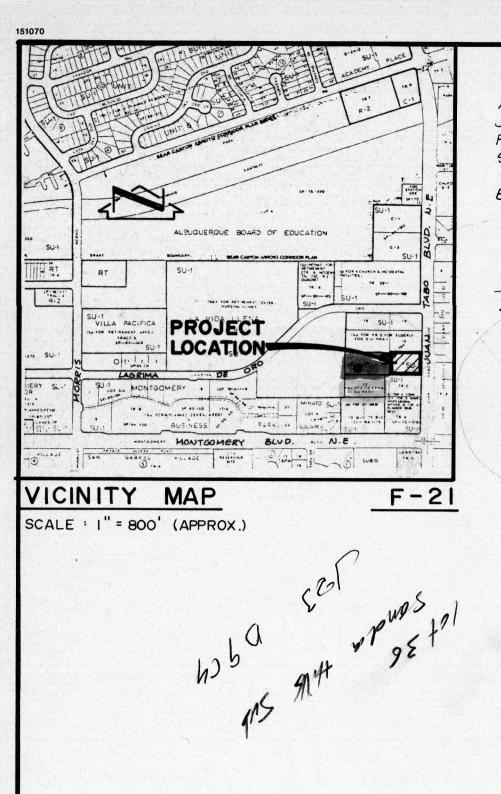
SUBMERSIBLE PUMP DETAILS & SECTIONS

DRAWING

RECORD

DOUBLE RAINBOW BAKERY & CAFE

NO. DATE BY REVISIONS ESIGNED BY M.F.D. 1-27-95 J.M. R.ECORD DRAWING 921122 3 2/95 SCK AS-BUILT AND RECERTIFY 12-1993 APPROVED BY J.G.M.



F71-60+

PROJECT BENCHMARK A STANDARD NMSHC BRASS TABLET STAMPED JT- 1A, SET IN THE TOP OF A CONCRETE POST

FLUSH WITH THE GROUND & LOCATED IN THE SOUTHERLY MEDIAN ON JUAN TABO BLUD., N.E. E MONTGOMERY BLUD. N.E. ELEVATION = 5721.25 FEET (M.S.L.D.)

## LEGEND

--- 5725- EXIST. CONTOUR -5725- PROPOSED CONTOUR PROPOSED SPOT ELEVATION ---- PROPOSED FLOWLINE - PROPOSED DIRECTION OF RUNOFF PROPOSED CONCRETE PROPOSED ASPHALT TC TOP OF CURB FL FLOWLINE

TOP OF WALL

TW 20.0

N 89° 56' 00" E

13 PRIVATE ACCESS

-38' PRIVATE ACESS

TW5722.0 N89° 56' 00" E TW 5722.57

E UTILITY EASEMENT

TW 20.2

TW 22.5

TRENCH DRAIN

PROPOSED BUILDING

DRAINAGE PLAN

The following items concerning the Double Rainbow Drainage Plan are contained hereon:

1. Vicinity Map

2. Grading Plan 3. Calculations

As shown by the Vicinity Map, the site is located on the west side of Juan Tabo Boulevard N.E. between Montgomery Boulevard N.E. and Lagrima de Oro N.E. At present, the site is undeveloped. Much of the surrounding area is developed, making this an infill site.

As shown by Panel 18 of 50 of the National Flood Insurance Program Flood Insurance Rate Maps for the City of Albuquerque, New Mexico, dated October 14, 1983, this site does not lie within a designated flood hazard zone. Further review of this mapping does not reveal downstream flooding to which this site contributes. At present, the site slopes from east to west onto adjacent undeveloped property. The site is situated down slope from Juan Tabo Boulevard N.E., which is a developed City street.

The Grading Plan shows 1) existing grades indicated by contours at 1'0" intervals, 2) proposed grades indicated by spot elevations and contours at 1'0" intervals, 3) the limit and character of the existing improvements, 4) the limit and character of the proposed improvements, and 5) continuity between existing and proposed grades. As shown this plan, the proposed improvements consist of the construction of a building along with adjacent paving and landscaping. Due to the fact that the site slopes away from Juan Tabo Boulevard N.E. at an average 5% gradient, it is not possible to obtain gravity drainage back to the street. Because of this, a pond is proposed to contain 100% of the 100-year developed runoff and to drain that pond with a submersible pump. The forced main discharge from the pond will discharge into Juan Tabo Boulevard N.E. Waterproofing of the adjacent walls will be necessary to allow for ponding within 15' of the structures.

The Calculations which appear hereon analyze both the existing and developed conditions for the 100-year, 6-hour rainfall event. The Rational Method has been used to calculate the peak rate of discharge, while the SCS Method has been used to compute the volume of runoff generated. Both Methods have been used in accordance with the City of Albuquerque Development Process Manual, Volume II, combined with the Mayor's Emergency Rule dated January 14, 1986. As shown by these calculations, the proposed improvements will result in a net increase in runoff generated by this site. The pond volume has been calculated using the Average End Area Method. As shown by the volume computation, the pond has adequate capacity to hold the 100-year developed runoff volume without credit for the mechanical discharge of the runoff. The maximum depth of pond will be approximately 4', thereby requiring fencing of the pond area.

From SCS Bernalillo County Soil Survey, Plate 22: EtC - Embudo - Tijeras Complex Hydrologic Soil Group: B Existing Pervious CN = 61 (DPM Plate 22.2 C-2 Pasture or Range Land: good condition) Developed Pervious CN = 61 (DPM Plate 22.2 C-2 Open Space: good condition)

CALCULATIONS

Time of Concentration/Time to Peak

 $T_c = 0.0078 L^{0.77}/S^{0.385}$  (Kirpich Equation)

 $T_p = T_c = 10 \text{ min.}$ 

Point Rainfall

 $P_6 = 2.51$  in. (DPM Plate 22.2 D-1)

Rational Method

Discharge: Q = CiA

Ground Cover Information

Where C varies  $i = P_6(6.84)T_c^{-0.51} = 5.31in/hr$   $P_6 = 2.51$  in (DPM Plate 22.2D-1)  $T_c = 10 \text{ min (minimum)}$ 

A = area, acres SCS Method

Volume: V = 3630(DRO)A

Where DRO = Direct runoff in inches A = area, acres

Existing Condition

A<sub>total</sub> = 46,080 sf = 1.06 Ac C = 0.40 (Weighted average per Emergency Rule, 1/14/86)  $Q_{100} = CiA = 2.3 cfs$ % impervious =-0-% Composite CN = 61 (DPM Plate 22.2 C-3) DRO = 0.2 in (DPM Plate 22.2 C-4)  $V_{100} = 3630 \text{ (DRO)A} = 770 \text{ cf}$ 

Developed Condition

 $A_{total} = 46,080 \text{ sf} = 1.06 \text{ Ac}$ Roof area = 4,820 sf (10%) Paved area = 30,090 sf (65%)Landscaped area = 11,170 sf (25%)C = 0.77 (Weighted average per Emergency Rule, 1/14/86)  $Q_{100} = CiA = 4.3 cfs$ % impervious = 75 % Composite CN = 88 (DPM Plate 22.2 C-3) DRO = 1.4 in (DPM Plate 22.2 C-4)

Comparison

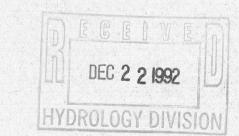
 $\Delta Q_{100} = 4.3 - 2.3 = 2.0 \text{ cfs (increase)}$  $\Delta V_{100} = 5,390 - 770 = 4,620 \text{ cf (increase)}$ 

 $V_{100} = 3630 \text{ (DRO) A} = 5,390 \text{ cf}$ 

POND VOLUME

2011 4 Hydnology

,75 (2.64) = 1.98 ,25(1,08)=,27 2,25



CONCEPTUAL GRADING AND DRAINAGE PLAN

DOUBLE RAINBOW

2'-0" CONC. RUNDOWN IN DISCHARGE TO DETENTION

MONTGOMERY BUSINESS PARK

LOT 12

MONTGOMERY BUSINESS PARK

277.58

TW 5726.86 277.58' TW 5728.48 TW 5728.48

NO. DATE BY REVISIONS 921121 DESIGNED BY JGM DRAWN BY SGH/CEN 12 - 92 SHEET APPROVED BY JGM



STORM INLET W/SUBMERSIBLE
PUMP
GRATE @ 15.0