

City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

October 29, 1999

Tucker Green
Per Se Engineering
9109 La Barranca NE
Albuquerque, New Mexico 87111

RE: Drainage Report and Grading and Drainage Plan for Economy Sales and Service (G15/D10) Submitted for Building Permit Approval, Engineer's Stamp Dated 10/28/99.

Dear Mr. Green:

Based on the information provided, the above referenced report, and the plan dated October 28, 1999, are approved for Building Permit release. This approval for Building Permit also includes approval for grading, paving and the foundation.

The owner should be aware that he is responsible for maintaining the on-site pond.

As you are aware, the Engineer's Certification of this plan is required prior to release of the Certificate of Occupancy for this site.

If you have any questions, or if I may be of further assistance to you, please call me at 924-3982.

Sincerely,

Susan M. Calongne, P.E.

City/County Floodplain Administrator

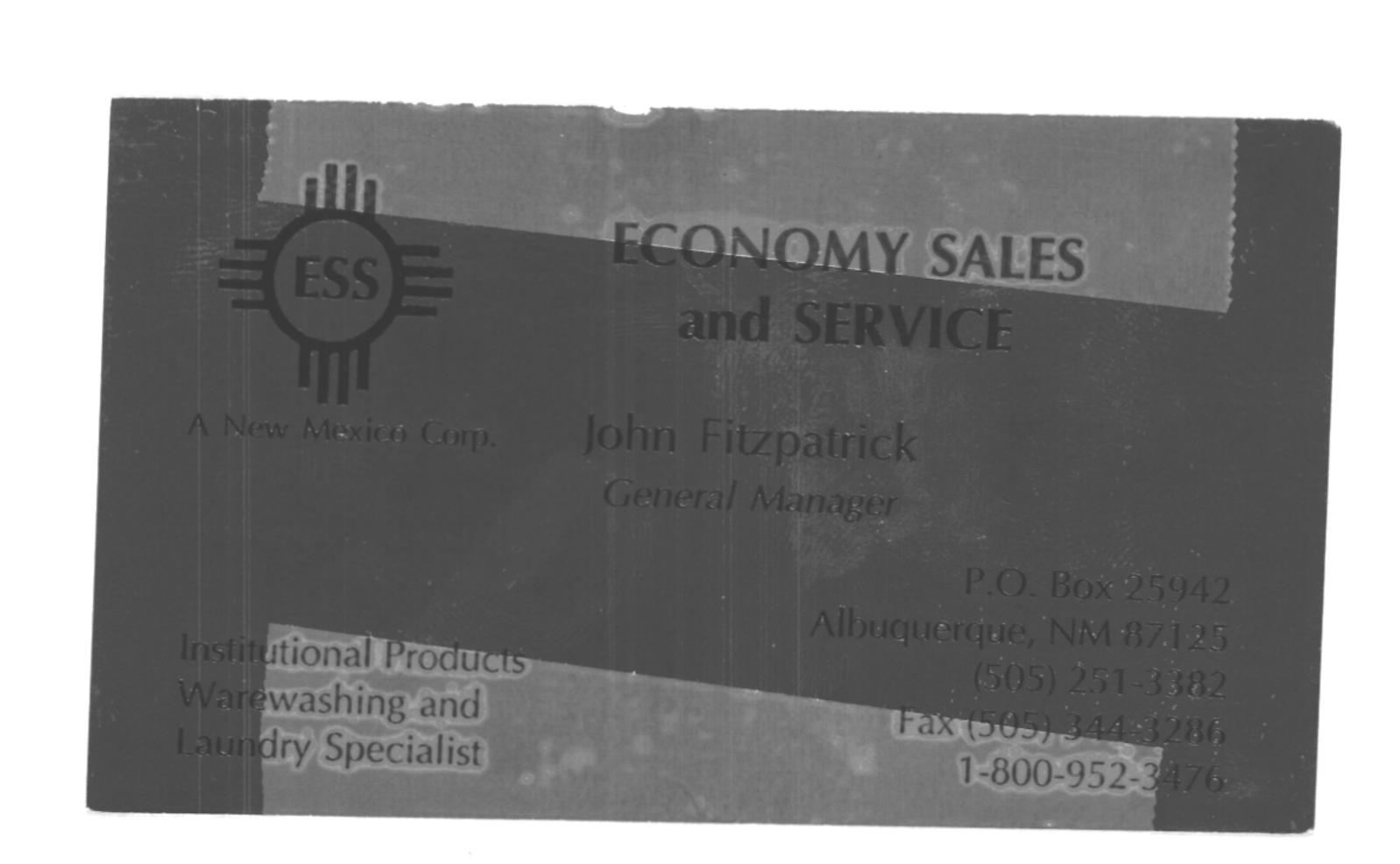
C: Whitney Reierson, City Hydrology
John Fitzpatrick, Economy Sales and Service
File

DEVELOPMENT & BUILDING SERVICE CENTER ONE STOP

600 SECOND ST. N.W./2ND FLOOR

ATTENTION:
505-924-3900
Records Withdrawal Form
Project No Date:
Project Title: <u>Economy Sales & Service</u>
a. File b. Mylars c. Redlines/Comments G15-1010 d. Other
Requested By: Gold Bordenauen Phone No.: 823-1344 Company
Comments:
Anticipated Return Date: Receipt Acknowledged
I here by accept full responsibility for the security of the above noted records/plans until return receipt acknowledgement is completed. Records/plans will be returned to the Development & Building Services Center on or before the indicated anticipated return date.
Delivery Picked Up By: Note: Didn't sign for check-out!!
Name: Organization: Old. Repro:
Signed: Date: Phone No
Office Use Only Return Acknowledged

Received by: Arlene V. Portillo Date: 7/17/00
Print



DRAINAGE INFORMATION SHEET

PROJE	CI TITLE: ESONOMY SALES ESTEUCE 2	ONE ATLAS/DRNG. FILE #: GIS-DIO
DRB #	: EPC #:	WORK ORDER #:
	DESCRIPTION: LOT 13-13, BLECK 1, C	
CITY	ADDRESS: 621 RANKIN RO VE	12BQ 87188
	EERING FIRM: PERSETUGING	
•	ADDRESS: 9109 LA BARRANCA NE	PHONE: 275-0451 239-7855MoB
OWNER	Economy Sares & Sozuice	CONTACT: JOHN FITZPATIZION
	ADDRESS: 821 RAMIN RO MG	PHONE: 344-3242
ARCHI	TECT: ENGINEERING ASSOCIATES	CONTACT: UNCE MEGES
	ADDRESS: 540 CHAMA NE # 11	PHONE: 266-3311
SURVE	YOR:	CONTACT:
	ADDRESS:	PHONE:
CONTR	ACTOR:	CONTACT:
	ADDRESS:	PHONE:
TYPE	OF SUBMITTAL:	CK TYPE OF APPROVAL SOUGHT:
	DRAINAGE REPORT	SKETCH PLAT APPROVAL
	DRAINAGE PLAN	PRELIMINARY PLAT APPROVAL
	CONCEPTUAL GRADING & DRAINAGE PLAN	_ S. DEV. PLAN FOR SUB'D. APPROVAL
	GRADING PLAN	_ S. DEV. PLAN FOR BLDG. PERMIT APPROVAL
	EROSION CONTROL PLAN	SECTOR PLAN APPROVAL
	ENGINEER'S CERTIFICATION	FINAL PLAT APPROVAL
	OTHER	FOUNDATION PERMIT APPROVAL
		BUILDING PERMIT APPROVAL
PRE-D	ESIGN MEETING:	CERTIFICATE OF OCCUPANCY APPROVAL
	YES JOHN MURRAY	GRADING PERMIT APPROVAL
	NO	PAVING PERMIT APPROVAL ON SINE ONLY
	COPY PROVIDED んつ	S.A.D. DRAINAGE REPORT
		DRAINAGE REQUIREMENTS
		OTHER (SPECIFY)
DATE	SUBMITTED:	
•	BY: <u>Lunch Opens</u>	

DRAINAGE REPORT and CALCULATIONS ECONOMY SALES & SERVICE 821 Rankin Rd. NE Albuquerque NM C.O.A. Drainage File G15/D10

LEGAL DESCRIPTION: ESS (Economy Sales & Service) is located on Lot 13-B, Block 1, Coman Industrial District.

FLOOD ZONE: Per FEMA Panel 35001CO 351 D the site is not located in a 100-year flood zone.

REVISION NOTE: The drainage plan and report for this site was originally for review on August 13, 1999, along with a Site/Traffic Control Layout plan. Comments regarding the TCL forced revisions to the site layout and thus to drainage. Per Se "withdrew" the original drainage submittal before it was reviewed by PWD Hydrology. This history accounts for the fact that some of the calculations are dated mid-August and others are dated mid-October.

SPECIAL NOTE: This plan actually addresses Lots 13A and 13B, even though it is prompted only by proposed changes to Lot 13B. The 1988 plat that created 13A & 13B from Lot 13 (Talos Log # 11-28-2161, Franklin Wilson, November 1988) contained a "reciprocal access easement for ingress and egress and drainage, parking, and refuse easements ..." (copy herewith). The approved drainage plan (G15/D10A, Marvin Kortum, March 1989) that went along with that plat action called for some (not all) of the flow from both lots to be directed to the EVEN-then-existing small concrete pond in the southwest corner of Lot 13A - the "other guy's" lot, not ESS's. The 1989 drainage plan referred to another approved plan from the early 1980's which established the allowable outflow rate for the site. The present design relies on that rate, which is 0.80 cfs peak.

EXISTING CONDITIONS: The site is located at the northeast end of the Rankin Rd. cul-de-sac. The east side of the site is actually part of the embankment for the on-ramp and frontage road forsouthbound Interstate 25. The embankment continues up past the east property line and a small part of the I-25 ROW drains onto and through the site. Flow from the main part of I-25, and from the pavement of the frontage road, is diverted past the site in a bar ditch and does not reach the site. Generally the land slopes down from the east to the west, parallel to I-25. As a result, there is no flow onto the site from the north and south adjoining lots, nor to those lots from the site.

Lot 13B, the site, occupies about 0.55 acres and Lot 13A occupies about 0.49; the combined total is 1.0317 acres per the plat. A significant portion of the combined site does not drain directly to the pond and/or Rankin Rd. but instead drains northwest to the Irrigation Supply company located on Lot 12. There is some question about how much of the site is affected. The topo for the 1989 drainage plan shows a high area in approximately the same place as the 1999 topo prepared for this project, and this is approximately the middle of the combined site (13A & 13B). A concrete-block retaining wall (partly hidden behind the honeysuckle) along the east edge of lot 12 raises up above grade keeps overland flow from 13A from sliding directly onto 12.

The 1989 plan indicates that a swale drained much of 13A to the pond but the evidence presented on the plan was not strong. The swale does not appear to exist today. The 1989 plan claimed only about 7200 sf of 13A was excluded from the pond. While this is obviously low, it is used in the present analysis: it's wrong, but it's consistent and it's conservative.

Current development on 13A and 13B is very much the same as for the 1989 plan, with the exception of 2 additional metal "ship's container" storage sheds on 13B, occupying about 160 sf each. Each site has a building and a concrete pad. 13B, the ESS site, has a small amount of landscaping. All parking areas are currently paved with gravel and/or crusher fines. The pond is not functional. It is filled with dirt, as it was at the time of the 1989 plan, and the drain hole called for by that plan was never built. At some time in the past, a shelf was cut into the bank east of the existing ESS building and an existing retaining wall extending north from the ESS building.

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PROPOSED CONDITIONS: ESS proposes to add a new warehouse north of the existing one and contiguous to it. New paving will extend from the north end of the addition to the west property line. The existing pond will be cleaned out and the walls will be raised to provide additional capacity. There will be landscaping in the pond.

Total runoff as analyzed by this plan presumably represents an increase over the 1989 plan. Not only will more of the site be impervious but also the methods of calculating runoff have changed to ones that tend to yield higher peak runoff. The allowable peak rate has not changed, however; it is still at the 0.80 cfs set by the early 1980's drainage plan, based on then-acceptable formulas and criteria. A excerpt from that plan is included with this report; the copy quality is poor, but it's the best readily available. The 0.80 cfs is the allowable peak rate for runoff generated from Lots 13A & 13B. The total peak rate for runoff out of the site includes uncontrolled runoff from I-25 ROW. As shown in the calcs, this amounts to 0.44 cfs, making a total of 1.24 cfs.

In the present plan, the existing building and the front part of the site continue to discharge directly to the street. The peak rate for this area is apx 0.45 cfs, leaving 1.24-0.45 = 0.79 cfs as the allowable peak outflow from the rest of the site and the contributing part of I25 ROW. To achieve this rate, the pond will be enlarged upward (the walls will be extended) and there will be temporary ponding in the parking area (both asphalt and gravel paving) for the 100-year storm. The overflow spillway for the pond is actually a "sideways level" grade break in the newly paved area, so the overflow path is out the driveway.

Everyday outflow from the pond will be from a pair of 3-inch diameter holes to be cored in the driveway side of the existing concrete wall of the pond. The orifice location, at the southeast corner of the pond, is the same as for previously approved plans for the site. The peak outflow rate is 0.75 cfs at a water surface elevation of 43.31, compared to an available-(for the orifices analyzed) 0.78 cfs at the overflow elevation of 43.5. Thus the plan allows for some additional runoff from future improvements not currently proposed, without further regrading the parking area..

The same AHYMO run also analyzed a single 4-inch diameter orifice. This would also work: peak outflow is 0.67 cfs at an elevation of 43.35, compared to an available 0.69 at 43.5. The pair of 3-inch orifices appears to be preferable because of having slightly more capacity to handle additional (future) development on site.

The new warehouse will primarily be a metal building, whereas the existing ESS building is CMU block construction. However, the east wall of the new building will be CMU designed by EAI (Engineering Associates, Inc, see structural plans for details) to retain soil at the levels shown on the plan. The north bay of the new structure will be open for the time being but is expected to be enclosed in the future. The retaining wall is not affected. The proposed wall extends past the end of the building, providing room for a notch carrying for flow from the upper level, and for finished grade slopes to tie back to the foot of the wall.

The "upper level" consists of the area between the buildings and a (2nd) new CMU wall to be built with this project (also designed by EAI). Most of the ground there slopes at 3H or 4H to 1V. Runoff from the embankment will pass over the wall without being concentrated and flow to a swale, which leads to the notch in the lower wall, previously mentioned. The swale collects only runoff from the embankment and the "upper level" area; the new roof flows to the west, away from the swale.

A NOTE ON GRADING: Paving in the front part of the site will be moderately steep asphalt. To avoid visual clutter, per General Note 5, grading in this area is specified only by spot elevations. Grading elsewhere is specified by a combination of contour lines and spot elevations.

END OF REPORT



Notes

- l. Legal: Lot 13, Replat of Coman Industrial District, Albuquerque, New Mexico 'Area = 1.03 Acres:
- 2. Surveyor: Way John Surveying Co., April, 1982
- 3. Bench Mark: \MSHC Brass Cap No. I-25-21, Elev. 5079.47
- 4. IBM: I.C. at South Lot line Projection, Elev. 5041.38
- 5. Zoning: M-1
- 6. SCS Soil Type A (BKD)

Drainage Criteria

The site is located in the valley area, but not in a flood hazard area. In a pre-design meeting with Mr. fred Aguirre, City Hydrology Department, it was determined that the site would be subject to Valley Criteria, i.e., pond Q50 with a Q1 release rate onto public streets.

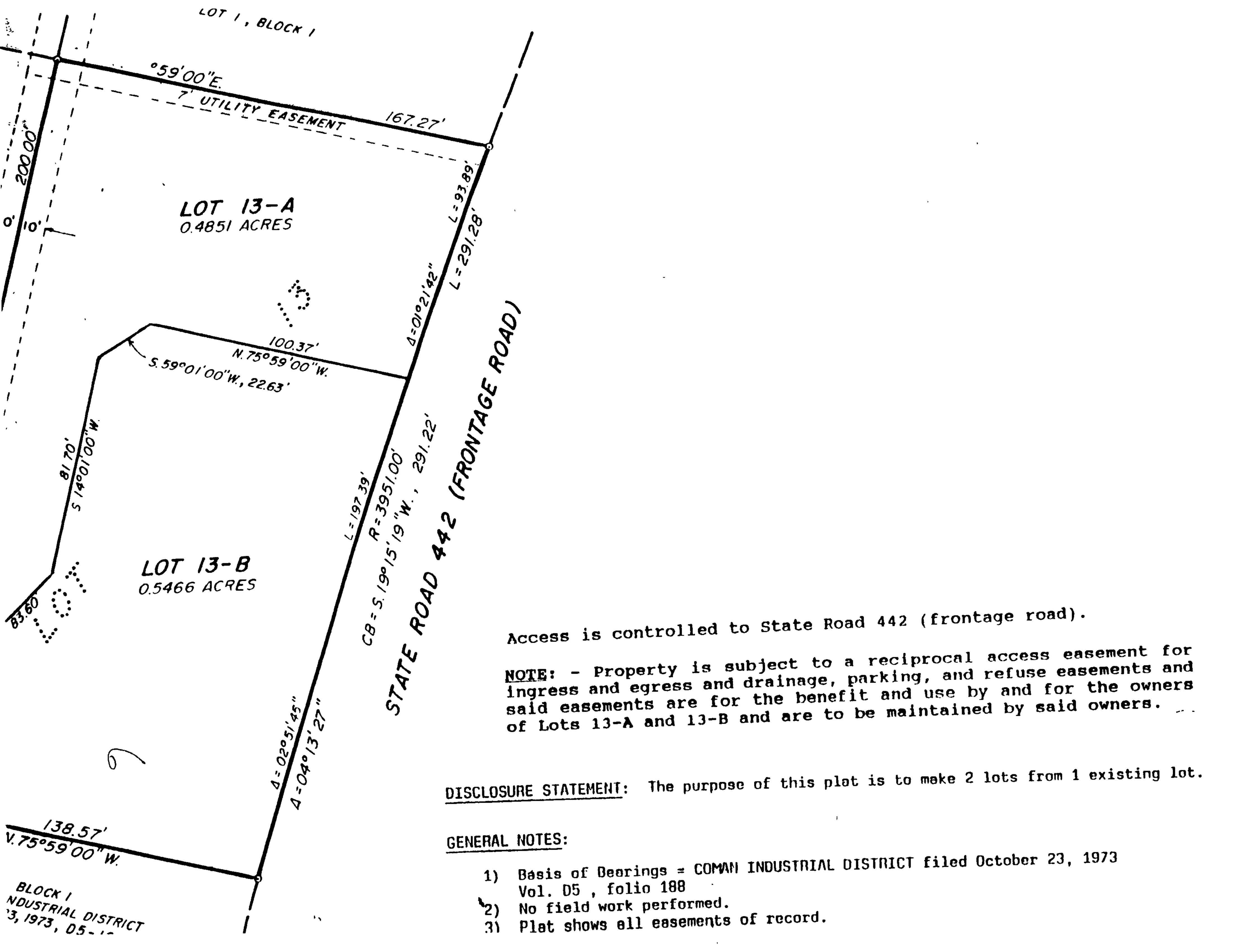
The offsite drainage is limited to a portion of the frontage road adjacent to the east side of the site. The areas north and south of the site drain in a parallel pattern to the site. Runoff from these two areas do not affect this site.

Offsite Area = 7500 ft.² draining to and across site. Q_{50} offsite = (0.65)(4.87)(0.17 Ac.) = 0.5 cfs Vol.50 offsite = $(0.65)(2.0/12)(7500) = 813 \text{ ft.}^3$

An equivalent on-site volume will be discharged directly to the site drivepad. The remaining site, plus the offsite drainage area along I-25 will be captured or controlled release from a pond at the SW corner of the site.

On-Site Drainage

- Equivalent from discharge area-to account for offsite flows $813 \text{ ft.}^3 = (0.70)(2.0/12)(x) = 7000 \text{ ft.}^2 + \frac{1}{2}$
- On-Site drainage to pond. plus offsite drainage area = 1.04 Ac.
- inligu to pend = (0.47)(2.0/12)(45,302 ft.2) = 3549 ft.3 450 to pend = (0.47)(4.87)(1.04) = 2 cfs = - 01 outflow rate = (0.47)(1.62)(1.04) = 0.8 cfs
- Peak vol. stored while simultaneously outflowing Q1 of 0.8 cfs = 2131 ft.3 at a time of 41 min. from start of condition (programable calculator .
- Pipe size for a head of 1.5' while outflowing 0.8 cfs = 0.10 ft.2, use 1- 4" diameter pipe.
- Pond Size = 10' wide x 1.5' deep x 145' long
- Spillway capacity, based on Q_{100} = (0.47)(5.4)(1.04) = 2.6 cfs. Broad crested wier = CLH 3/2 available head = 0.2° Breadth = 12° to be discharged over drivepad.
- 5.0. #19 submitted to City Design for outllow drain of pond to Rankin Rd.



2-2-99 OFFSITE FZOW -PASS THROUGH NMSHTD ROW FOR W IZS FRONTHER RD € ON-RAMO

NATIVE, STEED TREAT AS CLASS"C" - QPLUGE=3.14 CFS/AC ZONE Z ANEAS BY AMPOCATO POLY LINE -

OPP SITE - LOT 13-13
4659 SF
OPP 13-A
1498 SF

6157 x 3,14 = 0.4438 20.44 CF5, 43560 EXIST OFFS ITE MOUABLE OUT FROW

FROM 13-13 (SIRE) + 13-A 0.80 CFS 1982 PLAINTEE PLAN

PASS THROUGH FROM NMSHID ROW 0.44 CFS

1.24 TOTAL CES

8-7-99

TOTAL AREA OF SITE + LOT 13-A

FROM FRANK WILSON 1988 PLAT

15466 AC + 14851AC = 1.0317 AC

23,9105F + 21,1315F ~ 449415F

517E=13-B 13-A

LET 13-A CONTRIBUTIONS

PER MARCIN KONTUM 1989 DRAINAGE PLAN

APX 7700 SF OF 13-A FROWS OFFSITEON

TO A SUMP ON SITE @ 13-A. IN ANY CASE

DOES NOT CONTRIBUTE TO 13-BOR RANKINED.

THIS PLAN REPRESENTED THEN-EXISTING CONNITIONS, ESSENTIALY THE SAME SMUTURES AS EXIST NOW.

7200 SF CORPOS PONDS CLOSELY DITHE WEST

HALF OF 13-A NORTH OF THE PANHAMOLE MONE 13-B

SUPPOSEDLY, A SWATE EAST OF THE BLDGS &

CONC PARO TOOK ENST FROM TO WHEN BANKIN

VIA A SWALE.

ACTUALLY, THE HIGH POINT, THEN & NOW, LASS

APX GO FT S OF THE START OF THE PANHANDELY

SO ACTUALLY MUST \$ 13 A \$ SOME OF 18-13 DRAINS

OFFSITE TO NW.

FOR PRESENT PURPOSES ASSUME

ALL OF 13-A EXCEPT 7200 SE CONTRIBUTES

ALL EXISTING AS PRINT C, EITHER

GRAVEL PARKING ON STEEP NOTIVE ON

THE FRONTAGE RD EMBANKMET.

10-17-99

ESS PRODUSED COND

· UNCONTROLED RENOFF-- DIRECTLY TO SMEET

616 - 3 OF BLDG, CX IST

43
42
3 EXIST DEAWTERS AT BLDG

139
103
3 NEW PLANTERS

943 ST

1 M PERELIOUS QP100 = 4.37 CFS/AR ZONE Z

2174 EXIST BLDG

1795 PAVING \$ 5 W

 $(943)(2.29) + (3969)(4.37)_{=} 0.049 + 0.398$

8-10-99 255

ALLOWABLE OUTEROW RATE FROM POND

OUT ANEW = (ALLOWOLT, SITE) + (PASS TIMELLEH)
POND - (UNCONTROCCED TO STREET)

> = 0.80 + 0.44-0.45 & HISTORICAL BY SENSEUF PREVIOUS

BRAINAGE PLANS FOR THE SITE

OUT = 0.79 US PEAK POND ALLOWED

AREA TO DETENTION/DE LAY PONDING

LOTS (13A+13-B) + OFFS, TE 120W

- 13A NON CONTRUB

- 13B DIRECTLY TO STREET

13A. 13B 13A-RW 13B-ROW
21 126 + 23 808 + (4659+ 1498)

- 7200 - (6/6+43+ 2/74+1915)

- MANBALLY

(44934+6157)-(7200+4748)

= 51091 - 11948 = 39,143 SF

WEIR CARACITY - 1 16" (MU OMITTED) $Q = C L H^{\frac{3}{2}}$ C = 3, SAY 2.75 $Q = 2.75 \left(\frac{16}{12}\right) \left(\frac{e}{12}\right)^{\frac{3}{2}}$ $C = \frac{1}{2} \cdot 9959$ $C = \frac{1}{2} \cdot 9959$ $C = \frac{1}{2} \cdot 9959$

AREA DRAINING TO CUIT OUT

ANGA BY AUTOCAD POLYUM

EAST OF BLPG & WALL (MONG MERIDGE)

UP TO TOP OF DRAINAGE @ IZT ROW.

A = 11032 SF ALL SPEED NATURAL - RAIN ZUNG Z LND PRT A -> TRTE'

12 PM TABLE A-9

11032 SP 3.14 CFS 2 . 2533 ACX 3.14 CFS
43560 SF/A AC

~ 0.7952 ~0.80 CFS

0.20 CL 2.00 => 1 CM 4 CM 1047 to

SINCE | CUTOUT HAS ADEQUATE CAPACITY (VEST WALL)
SEVERAL WILL HAVE MORE THAN ENDUGAL THAN

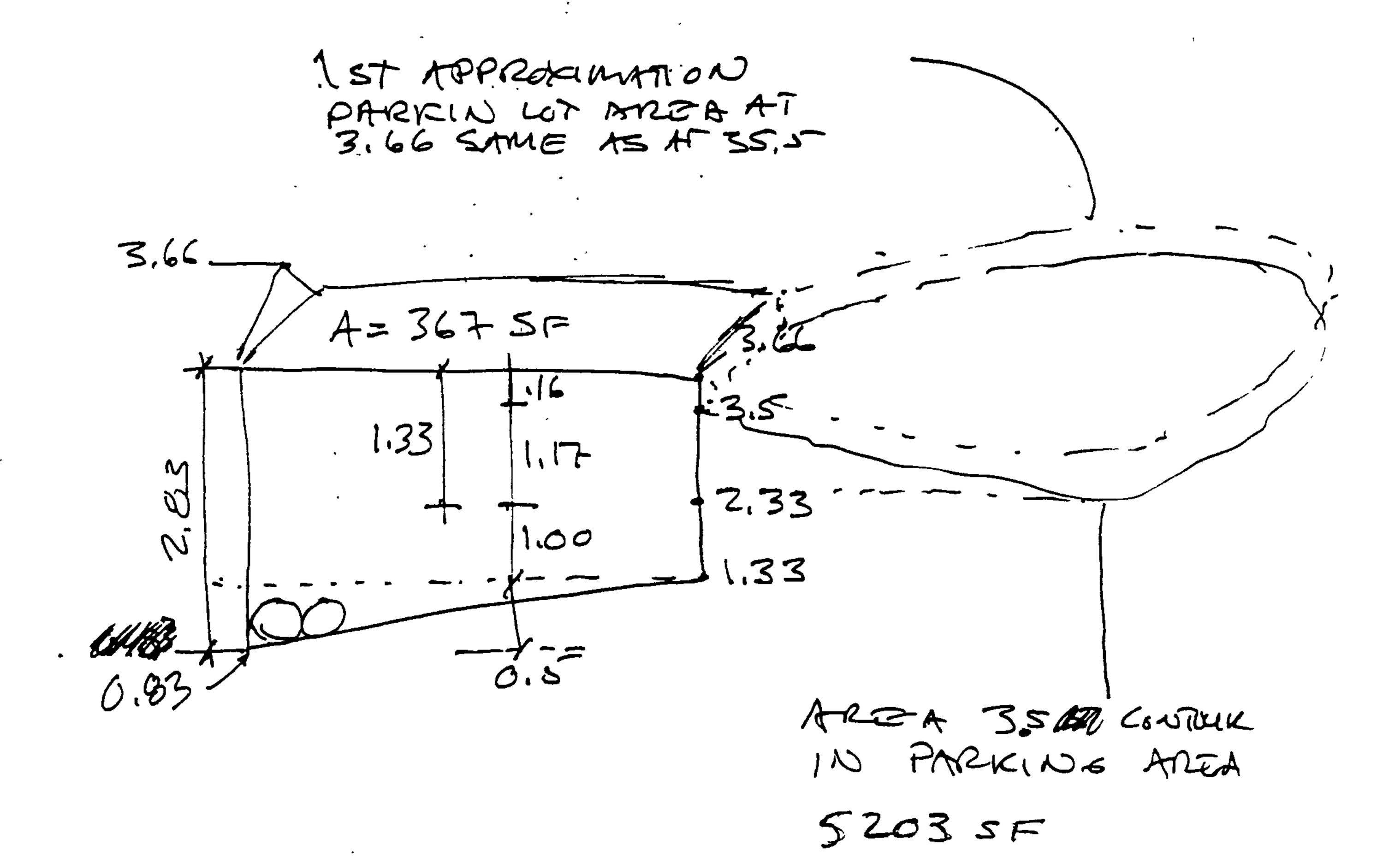
NOTE: ACTUAL NOTE WIDTH = 24" > 16" OK

14't/ 5t'/3 +3'0 51 26 _120 tell 14 DS 1204100,0=24 23PB,0=92 541,PE 29515 = 3754-57165 7577 5254 EB54 トカノマ 350 SCLZHS XIZ 七と七か INU CEN 2 CM 80 MAN 9-252 5 no model wil +95 ((1000) 57 ZUMS UNIW UPS UNIN INION ZUMEN !! 9

Then s / mentions of spent mens sites and the same of spent mens sites and the standard of spent mens sites and the standard some from the standard of spent mens of spent

55-E1-01

U2500001- 55 7



AREA 3.0 CONFOUR IN PARKING 1418 SF FILE=ESSVOL.WQ1

10/17/99

07:49 AM

ECONOMY SALES AND SERVICE - 421 RANKIN RD. NE SMALL RECTANGULAR POND W/ VERICAL WALLS AS AVERAGE END AREA, PLUS PARKING LOT PONDING AS "PYRAMID", ELEV 2.33 AND UP

RFCTANGUI	AR POND	IN CORNER	
KELLIANISUL	AR PUND	III GUNIYEN	

		PYRAMID	AV END AREA			
ELEV FT	AREA	DVOL CONE	VOL FT ^ 3	VOL AC-FT	DVOL AV ARE/ VOL FT ^ 3	VOL AC-FT
3.66	36	57 59	916	0.0210	59 94	17 0.0217
3.5	36	7 184	858	0.0197	184 88	0.0204
3		7 246	674	0.0155	246 70	0.0162
2.33	36	367	428	0.0098	367 45	0.0105
1.33	_	7 61	61	0.0014	92	0.0021
0.83		0	0	0.0000		0.0000

PARKING AREA PONDING

PYRAMID							AV END AREA			
ELEV FT	AREA		DVOL CONE	VOL FT ^ 3	VOL AC-FT	DVOL AV ARE	F VOL FT ^ 3	VOL AC-FT		
3.66	6	5203	832	2705	0.0621	832	2963	0.0680		
3.5		5203	1556	1873	0.0430	1655	2130	0.0489		
	3	1418	317	317	0.0073	475	475	0.0109		
2.33	3	0	•	0	0.0000		0	0.0000		

ELEV =	H =	TOTAL VOLUME =	TOTAL VOLUME =
3.66	2.83	3,652 CU FT, OR	0.0838 AC FT
3.5	2.67	2,761 CU FT, OR	0.0634 AC FT
3	2.17	1,021 CU FT, OR	0.0234 AC FT
2.33	1.5	459 CU FT, OR	0.0105 AC FT
1.33	0.5	92 CU FT, OR	0.0021 AC FT
0.83	0	0 CU FT, OR	0.0000 AC FT

FILE = ESorfice2.123 08/13/99

ORIFICES FOR POND ROUTING

HEAD MATCH ELEVS FOR POND VOULUMES

09:48 AM

FREE DISCHARGE FLOW THROUGH ORFICE: Q = C*A*SQRT(2*g*h)

C=COEFFICIENT, APX 5/8; A= FLOW AREA, SF; g=GRAVITY=32.17 FT/SEC ^ 2

h=HT OF WATER SURFACE ABOVE *CENTROID* OF FLOW AREA, FT

H=HT OF WATER ABOVE BOTTOM OF ORIFICE, = CENTROID + h)

C*SQRT(2*g) OFTEN TAKEN AS 5.0, = > C=0.623346

MATHEMATICALLY NOT VALID FOR WATER SURFACE BELOW CENTROID OF ORIFICE!

==> ENTER THIS NUMBER

CIRCULAR 5*A*SQRT(h) # H, FT	0.200	0.500	1.500	2.170	2.670	2.830	3.000		
# DIAM,FT	0.2500	0.2500	0.2500	0.2500	0.2500	0.2500	0.2500		
h, FT	0.075	0.375	1.375	2.045	2.545	2.705	2.875		
AREA, SF	0.049	0.049	0.049	0.049	0.049	0.049	0.049		
Q, CFS	0.067	0.150	0.288	0.351	0.392	0.404	0.416		
V, FPS	1.369	3.062	5.863	7.150	7.977	8.223	8.478		
Q * 2 (2 ORIFICES)	0.134	0.301	0.576	0.702	0.783	0.807	0.832		
CIRCULAR 5*A*SQRT(h) # H, FT	0.200	0.500	1.500	2.170	2.670	' 2.830 • • • • • • •	3.000	3.200	3.400
# DIAM,FT	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333
h, FT	0.033	0.333	1.333	2.003	2.503	2.663	2.833	3.033	3.233
AREA, SF	0.087	0.087	0.087	0.087	0.087	0.087	0.087	0.087	0.087
Q, CFS	0.080	0.252	0.504	0.618	0.690	0.712	0.734	0.760	0.785
V, FPS	0.913	2.887	5.774	7.077	7.911	8.160	8.416	8.708	8.991

FINISHre

```
*C PRINT CODES: 0=ALL; 1=TOTALS ONLY; 2=EVERY 2ND + TOTALS; 3,5,10,20 SIMILAR
*C RATING CURVE ID NEGATIVE => COMPUTE BUT NOT PRINT RATING CURVE
 > PATING CURVE IN NEGATIVE ⇒ FLOODPLAIN SLOPE, IN POSITIVE ⇒ CHANNEL SLOPE
*S FILE ESS600b - Economy Sales & Service, 6-hour, 100 year storm, run b
               421 Rankin Rd NE at I-25 west frontage road
*S CUTFLOW LIMITED TO 0.79cfs so entire (site + offsite) matches exist allowable
*S
*S FLOW IS **NOT** BULKED FOR SEDIMENT
*C RAINFALLL ESTIMATED FROM CITY OF ALBUQUERQUE D.P.M. FIGURES C-1, C-2, & C-3
       1 hr \Rightarrow 1.95 INCHES; 6hrs \Rightarrow 2.3 INCHES; 24 hrs \Rightarrow 2.6 INCHES
*C
*C BASIN & CHANNEL POUTING PARAMETERS REFLECT THE JUDGMENT OF THE ENGINEER,
*C AND MAY DIFFER FROM OTHER STUDIES IN THE AREA.
*C
*C REVISION NOTES: ORIGINAL FILE CREATED 8-11-99 BY TUCKER CREEN P.E.
                10-17-99: REVISED PARKING AND PAVING, AND REV'D PONDING CONTOURS
*C
* PAINFALLS PER ALBUCLERGLE NM DPM - COMMENT OUT THOSE THAT DON'T APPLY
* TYPE 1 IS 6-HR STORM PER NOAA ATLAS 2 W PEAK INTENSITY @ 1.4 HRS (EQ C1-C5)
    FOR 6-HR USE DT = 0.0333333 HR = 2 MINUTES
* TYPE 2 IS 24-HR STORM PER NOAA ATLAS 2 W PEAK INTENSITY @ 1.4 HRS (EQ C1-C6)
    FOR 24-HR USE DT = 0.0500 HR = 5 MINUTES
* PAIN CLIARTER = 0.0 EXCEPT FOR TYPE 3 (6-HR PMP: SEE AHMO MANUAL)
* FOR 10-YR STORM, USE 0.667 * 100-YR VALUES (PER DPM 22.2 TABLE A-3, JAN 1993)
RAINFALL AMOUNTS, INCHES
                    HUNDRED TYPE= 2 RAIN GLARTER= 0.0 RAIN ONE= 1.97
* RAINFALL
                  PAIN SIX= 2.31  PAIN DAY= 2.7  DT= .05 HR
                  HUNDRED TYPE= 1 0.0 1.95 2.3 2.6
                                                           0.033333
 AINFALL
                                                           0.033333
                    TENYEAR TYPE= 1 0.0 1.31
                                              1.54 1.80
* RAINFALL
*S ALL CONTRIBUTING. INCLUDES 125 HOW, EXCLUDES EX.BLDG & FRONT OF SITE
                  ID= 1 HYD= WEST
                                             DA=0.0014041 SQ MI
COMPUTE NM HYD
                  PER A= 0 B= 0.84 C= 81.75 D= 17.41
                  TP= -0.13333 HRS RAIN= -1
                  ID= 1 CODE= 5
PRINT HYD
 *S HYD PONDOUT.2D3 IS FOR 2 3-INCH DIAWETER OFIFICES
                                                    CODE=5.
               ID=3 HYD=PONDOUT.2D3 INFLOW ID=1
ROUTE RESERVOIR
                               STORAGE AC-FT ELEVATION FT
                  CUTTFLOW CFS
                                              0.83
                               0.000
                   0.000
                                              1.33
                         0.0021
                   0.301
                                              2.33
                               0.0105
                   0.576
                                              3.0
                               0.0236
                   0.702
                                              3.5
                               0.0619
                   0.783
                                              3.66
                               0.0809
                   0.807
*S HYD PONDOUT. 1D4 IS FOR 1 4-INCH DIAMETER CRIFICE
                                                      CODE=5.
                   ID=4 HYD=PONDOUT.1D4
                                        INFLOW ID=1
 ROUTE RESERVOIR
                                             ELEVATION FT
                               STORAGE AC-FT
                   CUTTFLOW CFS
                                              0.83
                                0.000
                   0.000
                                              1.33
                                0.0021
                   0.252
                                              2.33
                                0.0105
                    0.504
                                              3.0
                                0.0236
                    0.618
                                              3.5
                                0.0619
                    0.690
                                              3.66
                                0.0809
                    0.712
```

```
AHMMO PROGRAM (AHMMO194) - AMAFCA Hydrologic Model - January, 1994
FLIN DATE (MON/DAY/YR) = 10/17/1999
START TIME (HR:MIN:SEC) = 08:13:22 USER NO. = PERSEENG. 194
INPUT FILE = ESS600b.dta
```

```
*C PRINT CODES: 0=ALL; 1=TOTALS ONLY; 2=EVERY 2ND + TOTALS; 3,5,10,20 SIMILAR
*C RATING CURVE ID NEGATIVE ⇒ COMPUTE BUT NOT PRINT RATING CURVE
*C RATING CURVE IN NEGATIVE ⇒ FLOODPLAIN SLOPE, IN POSITIVE ⇒ CHANNEL SLOPE
*S
*S FILE ESS600b - Economy Sales & Service, 6-hour, 100 year storm, run b
                  421 Rankin Rd NE at I-25 west frontage road
*S
*S OUTFLOW LIMITED TO 0.79cfs so entire (site + offsite) matches exist allowable
*S FLOW IS **NOT** BULKED FOR SEDIMENT
*C RAINFALLL ESTIMATED FROM CITY OF ALBUQUERGLE D.P.M. FIGURES C-1, C-2, & C-3
                     hr \Rightarrow 1.95 INCHES; 6hrs \Rightarrow 2.3 INCHES; 24 hrs \Rightarrow 2.6 INCHES
*C
*C
*C BASIN & CHANNEL POUTING PARAMETERS REFLECT THE JUDGMENT OF THE ENGINEER,
*C AND MAY DIFFER FROM OTHER STUDIES IN THE AREA.
*C
*C REVISION NOTES: CRIGINAL FILE CREATED 8-11-99 BY TUCKER CREEN P.E.
                   10-17-99: REVISED PARKING AND PAVING, AND REV'D PONDING CONTO
*C
*C
 *C
* RAINFALLS PER ALBUCLERGLE NM DPM - COMMENT OUT THOSE THAT DON'T APPLY
 * TYPE 1 IS 6-HR STORM PER NOAA ATLAS 2 W PEAK INTENSITY @ 1.4 HRS (EQ C1-C5)
     FOR 6-HR USE DT = 0.0333333 HR = 2 MINUTES
 * TYPE 2 IS 24-HR STORM PER NOAA ATLAS 2 W PEAK INTENSITY @ 1.4 HRS (EQ C1-O6)
     FOR 24-HR USE DT = 0.0500 HR = 5 MINUTES
 * RAIN CLIARTER = 0.0 EXCEPT FOR TYPE 3 (6-HR PMP: SEE AHMO MANUAL)
 * FOR 10-YR STORM, USE 0.667 * 100-YR VALUES (PER DPM 22.2 TABLE A-3, JAN 1993)
 *
                           PAINFALL AMOUNTS, INCHES
 *
                        HUNDRED TYPE= 2 PAIN QUARTER= 0.0 PAIN ONE= 1.97
 * RAINFALL
                                                       DT = .05 HR
                      RAIN SIX= 2.31 RAIN DAY= 2.7
                                                                     0.033333
                                          0.0 1.95 2.3
                                                              2.6
                      HUNDRED TYPE= 1
 RAINFALL
```

COMPUTED 6-HOUR PAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2 - PEAK AT 1.40 HR. 5.999940 HURS END TIME = .033333 HOURS DT = .0111 .0092 .0072 .0054 .0035 .0018 ∞ .0262.0239 .0216 .0194 .0173 .0152 .0131 .0447 .0418 .0390 .0363 .0336.0311 .0286 .0686 .0648 .0610 .0575 .0541 .0508 .0477 .1122 .0999 .0928.0870 .0816 .0771 .0727 .7959 .6095 .4597 .3423 .2529 . 1874 . 1418 1.5781 1.5227 1.4625 1.3963 1.32220 1.2339 1.0234 1.8787 1.8429 1.8051 1.7651 1.6776 1.6295 2.0316 2.0380 2.0441 1.9752 2.0041 2.0553 2.0605 2.0655 2.0703 2.0749 2.0794 2.0837 2.0879 2.0919 2.0958 2.0996 2.1033 2.1070 2.1105 2.1139 2.1172 2.1205 2.1237 2.1268 2.1299 2.1329 2.1358 2.1387 2.1416 2.1443 2.1471 2.1497 2.1524 2.1550 2.1575 2.1600 2.1625 2.1649 2.1673 2.1697 2.1720 2.1743 2.1765 2.1788 2.1810 2.1831 2.1853 2.1874 2.1895 2.1916 2.1936 2.1956 2.1976 2.1996 2.2015 2.2034 2.2053 2.2072 2.2091 2.2109 2.2128 2.2146 2.2164 2.2181 2.2199 2.2216 2.2233 2.2250 2.2267 2.2284 2.2301 2.2317 2.2333 2.2350 2.2366 2.2381 2.2397 2.2413 2.2428 2.2444 2.2459

```
      2.2474
      2.2489
      2.2504
      2.2519
      2.2533
      2.2548
      2.2562

      2.2577
      2.2591
      2.2605
      2.2619
      2.2633
      2.2647
      2.2661

      2.2674
      2.2688
      2.2701
      2.2715
      2.2728
      2.2741
      2.2754

      2.2767
      2.2780
      2.2793
      2.2806
      2.2818
      2.2831
      2.2844

      2.2856
      2.2968
      2.2881
      2.2993
      2.2905
      2.2917
      2.2929

      2.2941
      2.2953
      2.2965
      2.2977
      2.2988
      2.3000
```

* RAINFALL

TENYEAR TYPE= 1 0.0 1.31 1.54 1.80 0.033333

*S ALL CONTRIBUTING. INCLUDES 125 ROW, EXCLUDES EX.BLDG & FRONT OF SITE COMPUTE NM HYD

ID= 1 HYD= WEST DA=0.0014041 SQ MI

PER A= 0 B= 0.84 C= 81.75 D= 17.41

TP= -0.13333 HRS RAIN= -1

K = .072665HR TP = .1333330HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420 UNIT PEAK = .96490 CFS UNIT VOLUME = .9881 B = .526.28 P60 = 1.9500 APEA = .000244 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR PUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .107043HR TP = .133330HR K/TP RATIO = .802846 SHAPE CONSTANT, N = 4.460466 UNIT PEAK = 3.3466 CFS UNIT VOLUME = .9965 B = 384.78 P60 = 1.9500 APEA = .001160 SQ MI IA = .35153 INCHES INF = .83427 INCHES PER HOUR PLNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD

ID= 1 CODE= 5

HYDROGRAPH FROM AREA WEST

TIME HRS .000 .167 .333 .500 .667 .833 1.000	FLOW CFS .0 .0 .0 .0 .0 .0 .0	TIME HRS 1.333 1.500 1.667 1.833 2.000 2.167 2.333	FLOW CFS .4 3.0 1.6 .8 .5 .2 .1	TIME HRS 2.667 2.833 3.000 3.167 3.333 3.500 3.667	FLOW CFS .0 .0 .0 .0 .0 .0	TIME HRS 4.000 4.167 4.333 4.500 4.667 4.833 5.000	FLOW CFS .0 .0 .0 .0 .0 .0 .0	TIME HRS 5.333 5.500 5.667 5.833 6.000 6.167	FLOW CFS .0 .0 .0 .0 .0
1.000 1.167	.0 .0	2.333 2.500	.1 .1	3.833	.0	5.167	.0		

RUNOFF VOLUME = 1.24383 INCHES = .0931 ACPE-FEET
PEAK DISCHARGE RATE = 2.98 CFS AT 1.500 HOURS BASIN APEA = .0014 SQ. MI.

*S HYD PONDOUT.2D3 IS FOR 2 3-INCH DIAWETER OFIFICES

ROUTE RESERVOIR ID=3 HYD=PONDOUT.2D3 INFLOW ID=1 CODE=5.

CUTFLOW CFS STORAGE AC-FT ELEVATION FT

ELEVATION FT 0.830.000 0.0001.33 0.0021 0.301 2.33 0.576 0.0105 3.0 0.0236 0.702 3.5 0.0619 0.783 3.66 0.0809 0.807

* * * * * * * * * * * * *

TIME INFLOW ELEV VOLUME CUTFLOW (HRS) (CFS) (FEET) (AC-FT) (CFS)

.00	.00	.83	.000	.00				
.17	.00	.83	.000	.00		7		
.33	.00	.83	.000	.00				
.50	.00	.83	.000	.00				
.67	.00	.83	.000	.00				
.83	.00	.83	.000	.00				
1.00	.00	.83	.000	.00				
1.17	.00	.83	.000	.00				
1.33	.41	1.07	.001	.14				
1.50	2.98	2.77	.019	.66				
1.67	1.57	3.23	.042	.74				
1 .8 3	.82	3.30	.047	.75				
2.00	.48	3.28	.045	.75				
2.17	.22	3.21	.040	.74				
2.33	.11	3.11	.032	.72				
2.50	.07	2.99	.023	.70				
2.67	.04	2.56	.015	.62				
2.83	.02	1.99	.008	.48				
3.00	.01	1.37	.002	.31				
3.17	.01	.92	.000	.06				
3.33	.01	.8 5	.000	.01				
3.50	.01	.84	.000	.01				
3.67	.00	.84	.000	.01		.		
3.83	.00		.000	.00				
PEAK DISCHAF				XURS AT HOUR	1.87			
MAXIMUM WATE	R SURFA	CE ELEVATION =		.305				
MAXIMUM STOP	PAGE =	.0470	C-FT	INCREMENTAL TI	√E=	.033333 HR S		

*S HYD PONDO	Л.1D4	IS FOR 1 4-II	VCH DIAWETE	RORIFICE				
ROUTE RESERV	OIR	ID=4 HYD=Pa	VDOUT. 1D4	INFLOW ID=1	CODE	≓ 5.		
		CUTTFLOW CFS	STORAGE	AC-FT ELEVAT	ION FT			
		0.000	0.000	0.83				
		0.252	0.0021	1.33				
		0.504	0.0105	2.33				

2.33 0.504 0.0105 3.0 0.0236 0.618 3.5 0.0619 0.690 3.66 0.0809 0.712

TIME	INFLOW	ELEV	VOLUME	CUTFLOW
(HRS)	(CFS)	(FEET)	(AC-FT)	(CFS)
~	.00	.83	.000	.00
.00	_			.00
.17	.00	.83	.000	
.33	.00	.83	.000	.00
.50	.00	.83	.000	.00
.67	.00	.83	.000	.00
.83	.00	.83	.000	.00
1.00	.00	.83	.000	.00
1.17	.00	.83	.000	.00
1.33	.41	1.08	.001	.13
1.50	2.98	2.81	.020	.58
1.67	1.57	3.26	.044	.66
1.83	.82	3.34	.050	.67
2.00	.48	3.34	.050	.67
2.17	.22	3.28	.045	.66
2.33	.11	3.19	.038	.65
2.50	.07	3.09	.031	.ස
2.67	.04	2.96	.023	.61
2.83	.02	2.58	.015	.55

10/17/99	8:46 AM			I:\E	SS\non4CAD\Ah	ymRpt\Ess	eccopcon.Jwb
	3.00	.01	2.10	.009	.45		
	3.17	.01	1.51	.004	.30		
	3.33	.01	1.03	.001	.10		
	3.50	.01	.88	.000	.02		
	3.67	.00	.85	.000	.01		
	3.83	.00	.84	.000	.01		
	4.00	.00	.84	.000	.00		
PE	AK DISCHARG	E =	.668 CFS	s - PEAK O	COURS AT HOUR	1.90	
	XIM.M WATER		ELEVATION =	= 3	.350		
	XIMUM STORA		.0504		INCREMENTAL T	IME=	.033333HRS

FINISH

NORMAL PROGRAM FINISH

END TIME (HR:MIN:SEC) = 08:13:22

Page 4 of 4

ADDENDUM/REVISION

ГО

DRAINAGE REPORT and CALCULATIONS ECONOMY SALES & SERVICE

821 Rankin Rd. NE Albuquerque NM C.O.A. Drainage File G15/D10

LEGAL DESCRIPTION: ESS (Economy Sales & Service) is located on Lot 13-B, Block 1, Coman Industrial District.

THE DUMPSTER LADY STRIKES AGAIN:

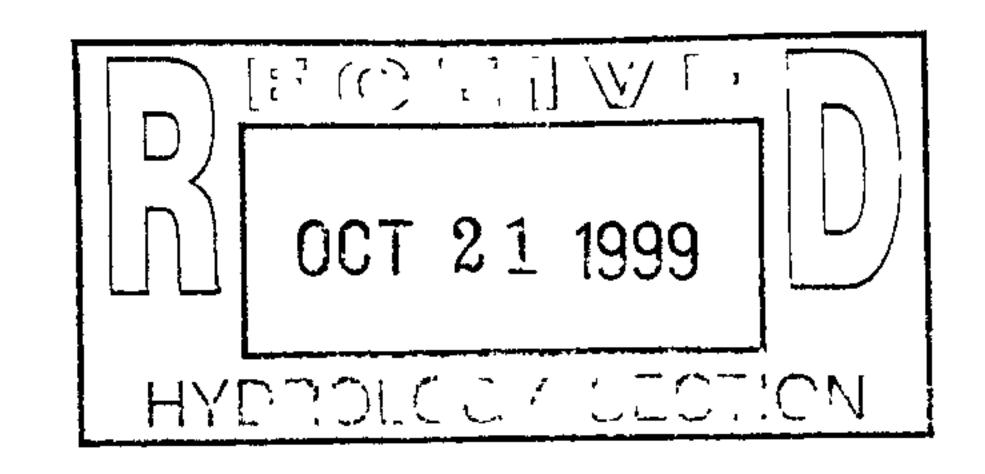
Shortly after the 10-17-99 drainage plan was submitted, Theresa Baca, reviewing for the City of Albuquerque, disapproved the location of the dumpster enclosure and pad. The plan dated 10-21-99 and submitted herewith shows the revised location.

Moving the dumpster forced minor changes to the grading, which are shown on the new plan. How minor? So minor that the calculations and AHYMO run were not redone. The table below provides before-and-after comparisons of the pavement areas draining to the street and to the pond, and also of the 43.0 & 43.5 contours used in calculating ponding volumes. Then the attached spreadsheet gives ponding volumes corresponding to the revised 43.0 and 43.5 contours. As shown, the changes are very minor, yeah, even trivial.

ITEM	OLD	NEW	NEW-OLD
Paving to street, sf	1795	1823	+28
Paving to pond, sf	4737	4710	-27
43.0 contour, sf	5203	5291	+88
43.5 contour, sf	1418	1420	+2

END OF ADDENDUM/REVISION





FILE=ESVOL2.123

10/21/99 12:26 AM

ECONOMY SALES AND SERVICE - 421 RANKIN RD. NE SMALL RECTANGULAR POND W/ VERICAL WALLS AS AVERAGE END AREA, PLUS PARKING LOT PONDING AS "PYRAMID", ELEV 2.33 AND UP

RECTANGULAR POND IN CORNER

PYRAMID					AV END AREA	AV END AREA		
ELEV FT	AREA	DVOL CONE	VOL FT ^ 3	VOL AC-FT	DVOL AV AREA VOL FT ^ 3 VOL	AC-FT		
3.66	367	59	916	0.0210	59 947	0.0217		
3.5	367	184	858	0.0197	184 888	0.0204		
3	367	246	674	0.0155	246 705	0.0162		
2.33	367	367	428	0.0098	367 459	0.0105		
1.33	367	61	61	0.0014	92 92	0.0021		
0.83	(0	0.0000	0	0.0000		

PARKING AREA PONDING

PYRAMID						AV END AREA		
ELEV FT	AREA		DVOL CONE	VOLFT^3	VOL AC-FT	DVOL AV AREA	VOL FT ^ 3	VOL AC-FT
3.	66	5291	847	2739	0.0629	847	3000	0.0689
	3.5	5291	1575	1892	0.0434	1678	2153	0.0494
	3	1420	317	317	0.0073	476	476	0.0109
2.	33	0		0	0.0000		0	0.0000

ELEV =	H =	TOTAL VOLUME =	TOTAL VOLUME =
3.66	2.83	3,686 CU FT, OR	0.0846 AC FT
3.5	2.67	2,781 CU FT, OR	0.0638 AC FT
3	2.17	1,022 CU FT, OR	0.0235 AC FT
2.33	1.5	459 CU FT, OR	0.0105 AC FT
1.33	0.5	92 CUFT, OR	0.0021 AC FT
0.83	0	0 CU FT, OR	0.0000 AC FT



City of Albuquerque

Mr. Vincent Meyer Engineering Associates, Inc. 540 Chama NE, Suite #11 Albuquerque, NM 87108

September 14, 1999

RE:

TRAFFIC CIRCULATION LAYOUT REVIEW FOR BUILDING PERMIT

APPROVAL

ECONOMY SALES & SERVICES WAREHOUSE ADDITION, G15-D010, Engineer's

Stamp dated August 17, 1999

Dear Mr. Meyer:

The above referenced Traffic Circulation Layout (TCL) requires modifications to the site plan prior to review for Building Permit. The comments are indicated in red ink on the attached marked-up site plan.

Please note on the site plan that the engineer's certification required by the Hydrology section needs to include certification that this site was constructed in accordance with the TCL before Certificate of Occupancy (C.O.) is released.

Please return the attached marked-up site plan with your next submittal.

You can reach me at 924-3993 to set up a meeting to discuss this project.

Sincerely,

Afsaneh Yavari Associate Engineer

Attachments

cc: Tucker Green, Per Se Engineering

NKYTUVPE TULNKUYTINU ZHEEI

PROJECT TITLE:	ECONDMY SALES ESTRUC	ZONE ATLAS/DE	RNG. FILE #:	G15-D010
	BPC #:			
	10N: <u>Lot 13-13</u> , <u>Bleck 1</u>			··
CITY ADDRESS:	621 RANKIN ROL	EALBQ	87188	
	RM: Peiz Se Englieri			
	9109 LA BARRANCA NE		275-0451	239-7855M013
OWNER:	Jony Sace & Source	CONTACT	: JOHN FITZ	HTRICK
	921 RANKIN 120 NG		344	
ARCHITECT:	NGINERING ASSOCIATES	CONTACT:	· Unce	4e4e25
ADDRESS:	S40 CHAMA NE # 11	PHONE:	266-3	3
SURVEYOR:		CONTACT	• •	
ADDRESS:		PHONE:	-	· · · · · · · · · · · · · · · · · · ·
CONTRACTOR:		CONTACT	•	
ADDRESS:		PHONE:		
GRADING PI EROSION CO ENGINEER'S OTHER PRE-DESIGN MEET	PLAN L GRADING & DRAINAGE PLAN LAN ONTROL PLAN S CERTIFICATION FING: AUG 1 3 1999	PRELIMINAL S. DEV. PI S. DEV. PI SECTOR PL FINAL PLAT FOUNDATION BUILDING I GRADING PI	AT APPROVAL RY PLAT APPROVAL LAN FOR SUB'D. LAN FOR BLDG. AN APPROVAL APPROVAL PERMIT APPROVAL ERMIT APPROVAL ERMIT APPROVAL RMIT APPROVAL ANAGE REPORT	APPROVAL PERMIT APPROVAL VAL L Y APPROVAL
•	9_17_99			
DATE SUBMITTED	<u> </u>			
BY:	Tuner Oren		•	

DRAINAGE REPORT and CALCULATIONS ECONOMY SALES & SERVICE 821 Rankin Rd. NE Albuquerque NM Map G-15

LEGAL DESCRIPTION: ESS (Economy Sales & Service) is located on Lot 13-B, Block 1, Coman Industrial District.

FLOOD ZONE: Per FEMA Panel 35001CO 351 D the site is not located in a 100-year flood zone.

SPECIAL NOTE: This plan actually addresses Lots 13A and 13B, even though it is prompted only by proposed changes to Lot 13B. The 1988 plat that created 13A & 13B from Lot 13 (Talos Log # 11-28-2161, Franklin Wilson, November 1988) contained a "reciprocal access easement for ingress and egress and drainage, parking, and refuse easements ..." (copy herewith). The approved drainage plan (G15/D10A, Marvin Kortum, March 1989) that went along with that plat action called for some (not all) of the flow from both lots to be directed to the EVEN-then-existing small concrete pond in the southwest corner of Lot 13A – the "other guy's" lot, not ESS's. The 1989 drainage plan referred to another approved plan from the early 1980's which established the allowable outflow rate for the site. The present design relies on that rate, which is 0.80 cfs peak.

EXISTING CONDITIONS: The site is located at the northeast end of the Rankin Rd. cul-de-sac. The east side of the site is actually part of the embankment for the on-ramp and frontage road for Interstate 25. The embankment continues up past the east property line and a small part of the I-25 ROW drains onto and through the site. Flow from the main part of I-25, and from the pavement of the frontage road, is diverted past the site in a bar ditch and does not reach the site. Generally the land slopes down from the east to the west, parallel to I-25. As a result, there is no flow onto the site from the north and south adjoining lots, nor to those lots from the site.

Lot 13B, the site, occupies about 0.55 acres and Lot 13A occupies about 0.49; the combined total is 1.0317 acres per the plat. A significant portion of the combined site does not drain directly to the pond and/or Rankin Rd. but instead drains northwest to the Irrigation Supply company located on Lot 12. There is some question about how much of the site is affected. The topo for the 1989 drainage plan shows a high area in approximately the same place as the 1999 topo prepared for this project, and this is approximately the middle of the combined site (13A & 13B). A concrete-block retaining wall (partly hidden behind the honeysuckle) along the east edge of lot 12 raises up above grade keeps overland flow from 13A from sliding directly onto 12.

The 1989 plan indicates that a swale drained much of 13A to the pond but the evidence presented on the plan was not strong. The swale does not appear to exist today. The 1989 plan claimed only about 7200 sf of 13A was excluded from the pond. While this is obviously low, it is used in the present analysis: it's wrong, but it's consistent and it's conservative.

Current development on 13A and 13B is very much the same as for the 1989 plan, with the exception of 2 additional metal "ship's container" storage sheds on 13B, occupying about 160 sf each. Each site has a building and a concrete pad. 13B, the ESS site, has a small amount of landscaping. All parking areas are currently paved with gravel and/or crusher fines. The pond is not functional. It is filled with dirt, as it was at the time of the 1989 plan, and the drain hole called for by that plan was never built. At some time in the past, a shelf was cut into the bank east of the existing ESS building and an existing retaining wall extending north from the ESS building.

PROPOSED CONDITIONS: ESS proposes to add a new warehouse north of the existing one and contiguous to it. Largely in response to current criteria for parking and landscaping, the front part of the site is being revised, with some asphalt paving and probably some additional landscaping. Part of the landscaping may be in the ponding area. However: the site has very little frontage, all in the southwest corner; and the site has existing landscaping.

HYDROLOGY SECTION

along the south side; and there is extensive existing landscaping along the west side - it's just located on Lot 12. In short, the landscaping discussion is ongoing. Thus, while this plan shows proposed additional landscaping near the HC access path, the calculations do not rely on it: for calculation purposes that area is considered paved.

Total runoff as analyzed by this plan presumably represents an increase over the 1989 plan. Not only will more of the site be impervious but also the methods of calculating runoff have changed to ones that tend to yield higher peak runoff. The allowable peak rate has not changed, however; it is still at the 0.80 cfs set by the early 1980's drainage plan, based on then-acceptable formulas and criteria. A excerpt from that plan is included with this report; the copy quality is poor, but it's the best readily available. The 0.80 cfs is the allowable peak rate for runoff generated from Lots 13A & 13B. The peak rate for existing uncontrolled runoff onto the site from I-25 ROW. As shown in the calcs, this amounts to 0.44 cfs, making a total of 1.24 cfs.

In the present plan, the existing building and the front part of the site continue to discharge directly to the street. The peak rate for this area is apx 0.45 cfs, leaving 1.24-0.45 = 0.79 cfs as the allowable peak outflow from the rest of the site and the contributing part of 125 ROW. To achieve this rate, the pond will be enlarged upward (the walls will be extended) and there will be temporary ponding in the parking lot for the 100-year storm. The overflow spillway for the pond is actually a "sideways level" grade break in the newly paved area; the flow path is out the driveway.

Everyday outflow from the pond will be from a pair of 3-inch diameter holes to be cored in the driveway side of the existing concrete wall of the pond. This results in a peak outflow rate of 0.75 cfs at an elevation of 43.28, compared to an available (for the orifices analyzed) 0.78 cfs at the overflow elevation of 43.5. Thus the plan allows for additional runoff from future improvements not currently proposed, without further regrading the parking area...

The same AHYMO run also analyzed a single 4-inch diameter orifice. This would also work: peak outflow is 0.66 cfs at an elevation of 43.32, compared to an available 0.69 at 43.5. The pair of 3-inch orifices appears to be preferable because of having slightly more capacity to handle additional (future) development on site.

The new warehouse will primarily be a metal building, whereas the existing ESS building is CMU block construction. However, the east wall of the new building will be CMU designed by EAI (Engineering Associates, Inc.) to retain soil at the levels shown on the plan. The east end of the new structure will be open for the time being but is expected to be enclosed in the future. The retaining wall is not affected. The proposed wall extends past the end of the building, providing a notch for flow from the upper level and room for finished grade slopes to tie back to the foot of the wall.

The "upper level" consists of the area between the buildings and a (2nd) new CMU wall to be built with this project (also designed by EAI). Actually, most of the ground slopes at 3H or 4H to 1V. Runoff from the embankment will pass over the wall without being concentrated and flow to a swale, which leads to the single notch in the lower wall, previously mentioned. The swale collects only runoff from the embankment and the "upper level" area; the new roof flows to the west, away from the swale.

A NOTE ON GRADING: Paving in the front part of the site will be moderately steep asphalt. To avoid visual clutter, per General Note 5, grading in this area is specified only by spot elevations. Grading elsewhere is specified by a combination of contour lines and spot elevations.

H. GA

10731

END OF REPORT

DRAINAGE REPORT and CALCULATIONS ECONOMY SALES & SERVICE 821 Rankin Rd. NE Albuquerque NM Map G 5 AUG 1 3 1999 LEGAL DESCRIPTION: ESS (Economy Sales & Service) is located on Lot 13-B, Blogo A. Qoo any industrial location.

FLOOD ZONE: Per FEMA Panel 35001CO 351 D the site is not located in a 100-year flood zone.

SPECIAL NOTE: This plan actually addresses Lots 13A and 13B, even though it is prompted only by proposed changes to Lot 13B. The 1988 plat that created 13A & 13B from Lot 13 (Talos Log # 11-28-2161, Franklin Wilson, November 1988) contained a "reciprocal access easement for ingress and egress and drainage, parking, and refuse easements ..." (copy herewith). The approved drainage plan (G15/D10A, Marvin Kortum, March 1989) that went along with that plat action called for some (not all) of the flow from both lots to be directed to the EVEN-then-existing small concrete pond in the southwest corner of Lot 13A – the "other guy's" lot, not ESS's. The 1989 drainage plan referred to another approved plan from the early 1980's which established the allowable outflow rate for the site. The present design relies on that rate, which is 0.80 cfs peak.

EXISTING CONDITIONS: The site is located at the northeast end of the Rankin Rd. cul-de-sac. The east side of the site is actually part of the embankment for the on-ramp and frontage road for Interstate 25. The embankment continues up past the east property line and a small part of the I-25 ROW drains onto and through the site. Flow from the main part of I-25, and from the pavement of the frontage road, is diverted past the site in a bar ditch and does not reach the site. Generally the land slopes down from the east to the west, parallel to I-25. As a result, there is no flow onto the site from the north and south adjoining lots, nor to those lots from the site.

Lot 13B, the site, occupies about 0.55 acres and Lot 13A occupies about 0.49; the combined total is 1.0317 acres per the plat. A significant portion of the combined site does not drain directly to the pond and/or Rankin Rd. but instead drains northwest to the Irrigation Supply company located on Lot 12. There is some question about how much of the site is affected. The topo for the 1989 drainage plan shows a high area in approximately the same place as the 1999 topo prepared for this project, and this is approximately the middle of the combined site (13A & 13B). A concrete-block retaining wall (partly hidden behind the honeysuckle) along the east edge of lot 12 raises up above grade keeps overland flow from 13A from sliding directly onto 12.

The 1989 plan indicates that a swale drained much of 13A to the pond but the evidence presented on the plan was not strong. The swale does not appear to exist today. The 1989 plan claimed only about 7200 sf of 13A was excluded from the pond. While this is obviously low, it is used in the present analysis: it's wrong, but it's consistent and it's conservative.

Current development on 13A and 13B is very much the same as for the 1989 plan, with the exception of 2 additional metal "ship's container" storage sheds on 13B, occupying about 160 sf each. Each site has a building and a concrete pad. 13B, the ESS site, has a small amount of landscaping. All parking areas are currently paved with gravel and/or crusher fines. The pond is not functional. It is filled with dirt, as it was at the time of the 1989 plan, and the drain hole called for by that plan was never built. At some time in the past, a shelf was cut into the bank east of the existing ESS building and an existing retaining wall extending north from the ESS building.

PROPOSED CONDITIONS: ESS proposes to add a new warehouse north of the existing one and contiguous to it. Largely in response to current criteria for parking and landscaping, the front part of the site is being revised, with some asphalt paving and probably some additional landscaping. Part of the landscaping may be in the ponding

* ,****

area. However: the site has very little frontage, all in the southwest corner; and the site has existing landscaping along the south side; and there is extensive existing landscaping along the west side – it's just located on Lot 12. In short, the landscaping discussion is ongoing. Thus, while this plan shows proposed additional landscaping near the HC access path, the calculations do not rely on it: for calculation purposes that area is considered paved.

Total runoff as analyzed by this plan presumably represents an increase over the 1989 plan. Not only will more of the site be impervious but also the methods of calculating runoff have changed to ones that tend to yield higher peak runoff. The allowable peak rate has not changed, however; it is still at the 0.80 cfs set by the early 1980's drainage plan, based on then-acceptable formulas and criteria. A excerpt from that plan is included with this report; the copy quality is poor, but it's the best readily available. The 0.80 cfs is the allowable peak rate for runoff generated from Lots 13A & 13B. The peak rate for existing uncontrolled runoff onto the site from I-25 ROW. As shown in the calcs, this amounts to 0.44 cfs, making a total of 1.24 cfs.

In the present plan, the existing building and the front part of the site continue to discharge directly to the street. The peak rate for this area is apx 0.45 cfs, leaving 1.24-0.45 = 0.79 cfs as the allowable peak outflow from the rest of the site and the contributing part of I25 ROW. To achieve this rate, the pond will be enlarged upward (the walls will be extended) and there will be temporary ponding in the parking lot for the 100-year storm. The overflow spillway for the pond is actually a "sideways level" grade break in the newly paved area; the flow path is out the driveway.

Everyday outflow from the pond will be from a pair of 3-inch diameter holes to be cored in the driveway side of the existing concrete wall of the pond. This results in a peak outflow rate of 0.75 cfs at an elevation of 43.28, compared to an available (for the orifices analyzed) 0.78 cfs at the overflow elevation of 43.5. Thus the plan allows for additional runoff from future improvements not currently proposed, without further regrading the parking area.

The same AHYMO run also analyzed a single 4-inch diameter orifice. This would also work: peak outflow is 0.66 cfs at an elevation of 43.32, compared to an available 0.69 at 43.5. The pair of 3-inch orifices appears to be preferable because of having slightly more capacity to handle additional (future) development on site.

The new warehouse will primarily be a metal building, whereas the existing ESS building is CMU block construction. However, the east wall of the new building will be CMU designed by EAI (Engineering Associates, Inc.) to retain soil at the levels shown on the plan. The east end of the new structure will be open for the time being but is expected to be enclosed in the future. The retaining wall is not affected. The proposed wall extends past the end of the building, providing a notch for flow from the upper level and room for finished grade slopes to tie back to the foot of the wall.

The "upper level" consists of the area between the buildings and a (2nd) new CMU wall to be built with this project (also designed by EAI). Actually, most of the ground slopes at 3H or 4H to 1V. This wall has several notches (omitted blocks) in the top course to allow runoff from the embankment to pass over and flow to a swale, which leads to the single notch in the lower wall, previously mentioned. The swale collects only runoff from the embankment and the "upper level" area; the new roof flows to the west, away from the swale.

A NOTE ON GRADING: Paving in the front part of the site will be moderately steep asphalt. To avoid visual clutter, per General Note 5, grading in this area is specified only by spot elevations. Grading elsewhere is specified by a combination of contour lines and spot elevations.

END OF REPORT

8/13/99, 2:41:35 PM (2) 1/5 Page 2 of 2



Notes

- 2. Surveyor: Way John Surveying Co., April, 1982
- 4. Bench Mark: \MSHC Brass Cap No. I-25-21, Elev. 5079.47
- 4. IBM: I.C. at South Lot Line Projection, Elev. 5041.38
- 5. Zoning: M-1
- 6. SCS Soil Type A (BKD)

Drainage Criteria

The site is located in the valley area, but not in a flood hazard area. In a pre-design meeting with Mr. Fred Aguirre, City Hydrology Department, it was determined that the site would be subject to Valley Criteria, i.e., pond Q50 with a Q1 release rate onto public streets:

The offsite drainage is limited to a portion of the frontage road adjacent to the east side of the site. The areas north and south of the site drain in a parallel pattern to the site. Runoff from these two areas do not affect this site.

```
Offsite Area = 7500 \text{ ft.}^2 draining to and across site.

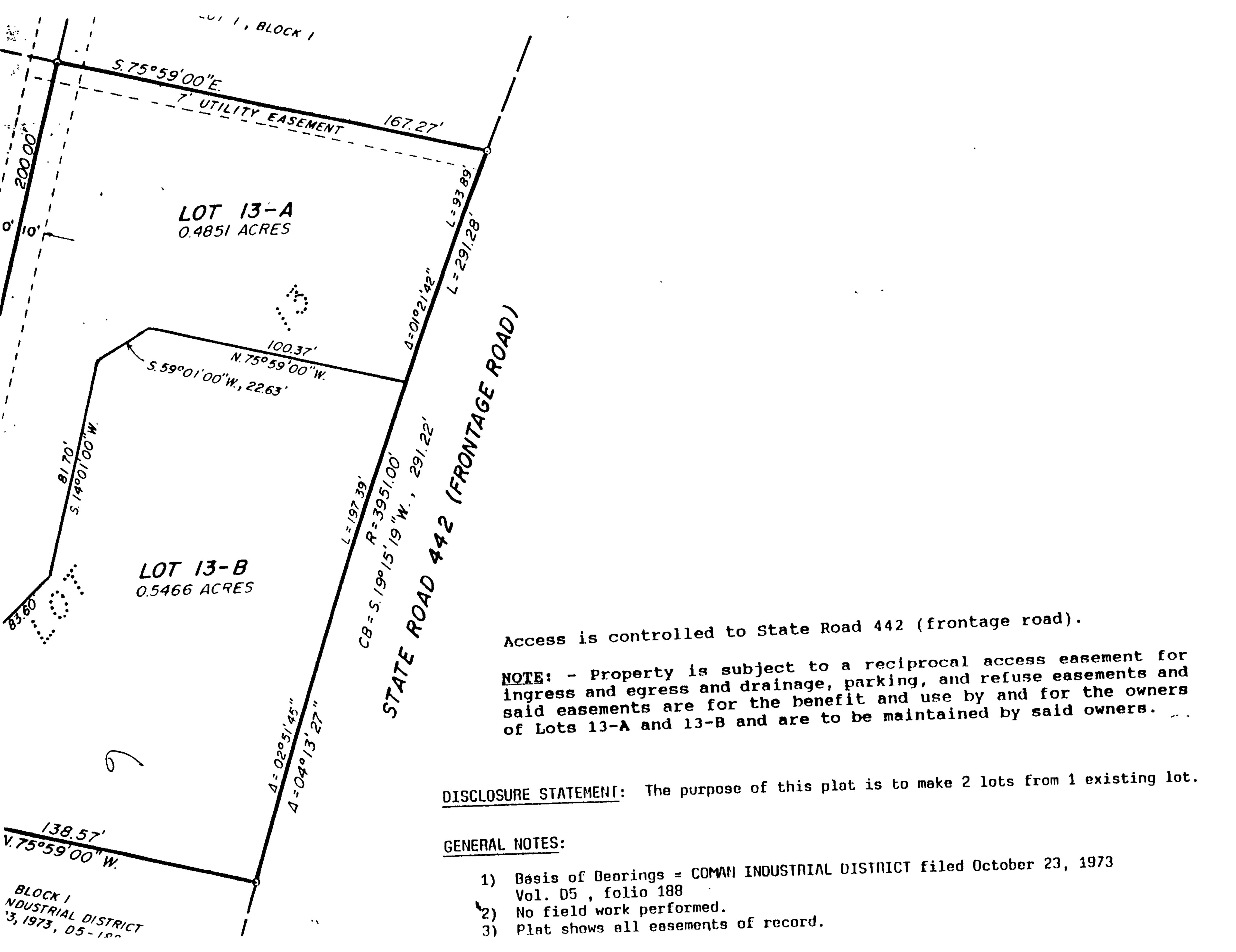
Q_{50} offsite = (0.65)(4.87)(0.17 \text{ Ac.}) = 0.5 \text{ cfs}

Vol.50 offsite = (0.65)(2.0/12)(7500) = 813 \text{ ft.}^3
```

An equivalent on-site volume will be discharged directly to the site drive-pad. The remaining site, plus the offsite drainage area along I-25 will be captured or controlled release from a pond at the SW corner of the site.

On-Site Drainage

- Equivalent free discharge area-to account for offsite flows 813 ft. 3 = (0.70)(2.0/12)(x) = 7000 ft. 2 +
- On-Site drainage to pond, plus offsite drainage area = 1.04 Ac.
- .01.50 to pend = $(0.47)(2.0/12)(45,302 \text{ ft.}^2) = 3549 \text{ ft.}^3$ $450 \text{ to pend} = (0.47)(4.87)(1.04) = 2 \text{ cfs}^2$ = 0.8 cfs
 - Peak vol. stored while simultaneously outflowing Q1 of 0.8 cfs = 2131 ft. 3 at a time of 41 min. from start of condition (programable calculator .
 - Pipe size for a head of 1.5' while outflowing 0.8 cfs = 0.10 ft.², use 1-4" diameter pipe.
 - Pond Size = 10' wide x 1.5' deep x 145' long
 - Spillway capacity, based on Q $_{100}$ = (0.47)(5.4)(1.04) = 2.6 cfs. Broad crested wier = CLH 3/2 available head = 0.2 breadth = 12 to be discharged over drivepad.
 - 5.0. #19 submitted to City Design for outllow drain of pond to Rankin Rd.



2-2-99

OFFSITE FLOW -PASS THROUGH

NMSHTD ROW FOR W IZS FRONTHER

RD #

ON-RAMO

NATIVE I STEEP

TREAT AS CLASS"C" - QPINCIG=314 CFS/AL ZONEZ

ANEAS BY AMPOCAD POLYUNG=

OPP SITE - LOT 13-13

4659 SF

1498 SF -6157 SE

6157 × 3.14 = 0.4438 20.44 CF5, 43560 EXIST OFFS ITE 0

5202426 72.1

577 bb.0

CODY WORLD WORLD SSUND

CAN BOLD 113-A

P-E1+(S12) 21-E/ MONTY

CAN 32001000 2991

63-28

8-7-99

TOTAL AREA DE SITE + LOT 13-A

FROM FRANK WILSON 1988 PLAT

15466 AZ + 14851AZ = 1.0317 AZ

23,8105F + 21,1315F 249941 SF

517E=13-B 13-A

LET 13-A CONTRIBUTIOS

PER MARCIN KORTUM 1989 DRAINAGE PLAN

APX 7700 SF OF 13-A FLOWS OFFSITEOR

TO A SUMP ON SITE @ 13-A. IN ANY CASE,

DO ES NOT CONTRIBUTE TO 13-BOR RANKINED

-> + TO AD JACENT PROPERTY, NO CORNER

THIS PLAN REPRESENTED THEN-EXISTING

CONSTITONS, ESSENTIALY THE SAME SMUTURES

AS EXIST NOW.

7700 SF CORPES: PONDS CLOSELY DO THE WEST

HALF OF 13-A NORTH OF THE PANHAMOLE MONE 18-18

SUPPOSEDLY, A SWATE EGST OF THE BLOGS F

CONC PARO TOOK EAST FLOW TO WARD ISANKIN

ULA A SWALE.

ACTUALLY, THE HIGH POINT, THEN & NOW, LASS

APX BOFTS OF THE START OF THE PANHANDEC;

SO ACTUALLY MUST & 13 A & SOME OF 13-B DRAINS

OFFSITE TO NW.

FOR PRESENT PURPOSES ASSUME

ALL OF 13-A EXCEPT 7200 SF CONTRIBUTES

ALL EXISTING AS TRAIT C, EITHER

OPANEL PARKING ON STEEP NOTIVE ON

THE FRONTAGE RD EMBANKMET.

8-10-99 UNCONTROUTED RUNOFF - DIRECTLY tO STREET 15T LIST ANEAS - MAPIONS COMBINATIONS POSSIBLE LAMO SCAPING, SQ FT 616 SOF EX BUDG S PLANTER, W END SHI ADD'L DOSSIBLE, SOF HE KEESS WALK NO 11 / NOF HE ACCESS IM PER WOUS 2174 EXISTING BLD6 1915 NEW AS PHART

CLESS MY OF THE LS WEAR THE HC ACCESS WARK EC 140+80=220)

1ST ASSUME NEGLEST LS NEAR HE ALLESS WARK ASSUME THIS 140+80=2205F AMED

QPEAR 100 YR 61M DPM 22.2 RAIN FONE 2 LS 2.28 CFS/AC IMPV 4.37 CFS/AC

(616+43)(ZZ2) + (Z174+1965)(4.37) 43560

= 659 (2.28) + (4089)(4.37) = 0.034+ 0.410 = 0.445 43560 20.45 CFS E=== E-10-99

ALLOWABLE OUTFLOW RATE FROM POND

OUT ANEW = (ANOWOLT, SITE)+ (PASS TARCUSH)

POND

- (UNCONTROLLED TO STREET)

= 0.80 + 0.44-0.45

E HISTORICAL BY SENSEUF PREMIOUS BRAINAGE PLANS FOR THE SITE

OUT = 0.79 US PEAK POND ALLOWED AREA TO DETENTION/PELAY PONDING

LOTS (13A+13-B) + OFFSITE 120W

- 13A NON CONTRIB

- 13B DIRECTLY TO STREET

13A 13B 13A-RW 1313-ROW
21 126 + 23808 + (4659+ 1498)

- 7200 - (6/6+43+ 2/74+1915)

> MANTERLY

(44934+6157)-(7200+4748)

= 51091-11948 = 39,143 SF

WEIR CARACITY - 1 16" CMU OMITTED $Q = C L H^{\frac{3}{2}}$ C = 3, SAY 2.75 $Q = 2.75 \left(\frac{16}{12}\right) \left(\frac{2}{12}\right)^{\frac{3}{2}}$ 2.9959 2.200 cfs

AREA DRAINING TO CUIT OUT

ANGA BY AUTOCAD POLYLING

EAST OF BLPG & WALL (MONG MARIPGE)

UP TO TOP OF DRAINAGE @ F25 ROW.

A = 11032 SF ALL SPEED NATURAL - RAIN ZUNG Z LND TRT A -> TRT E'

12 PM TABLE A-9

11032 SP 3.14 CFS 2.2533 ACX 3.14 CFS
43560 SF/A AC

~ 0.7952 ~0.80 CFS

0.20 CL 7.00 = 1 CM4 CUT OUT AND ON ALL FROD

SINCE | CUTOUT HAS ADEQUATE CAPACITY (VESTUAL)
SEVENAL WILL HAVE MONE THAN ENDUGH (EAST WAL)

NOTE: ACTUAL NOTH = 24" > 16" OK

FLOWS / TREATMENT AREAS TO POND

TOTAL = 39143 SP ± - PREVIOUS SHEET

· ALL NATIVE MEAS STEEP - TREATMENT'C'

À" NATURALINIO 5 COPE O

B MILLO SLOPE LS

PLANTER + DOND

42 1367 = 409

D IMPERUIOUS

NOW BLDG, NEW PAVE & 2546

CONC PAP, + 2 SHEDS + 1772

+ 2(149) = 4616

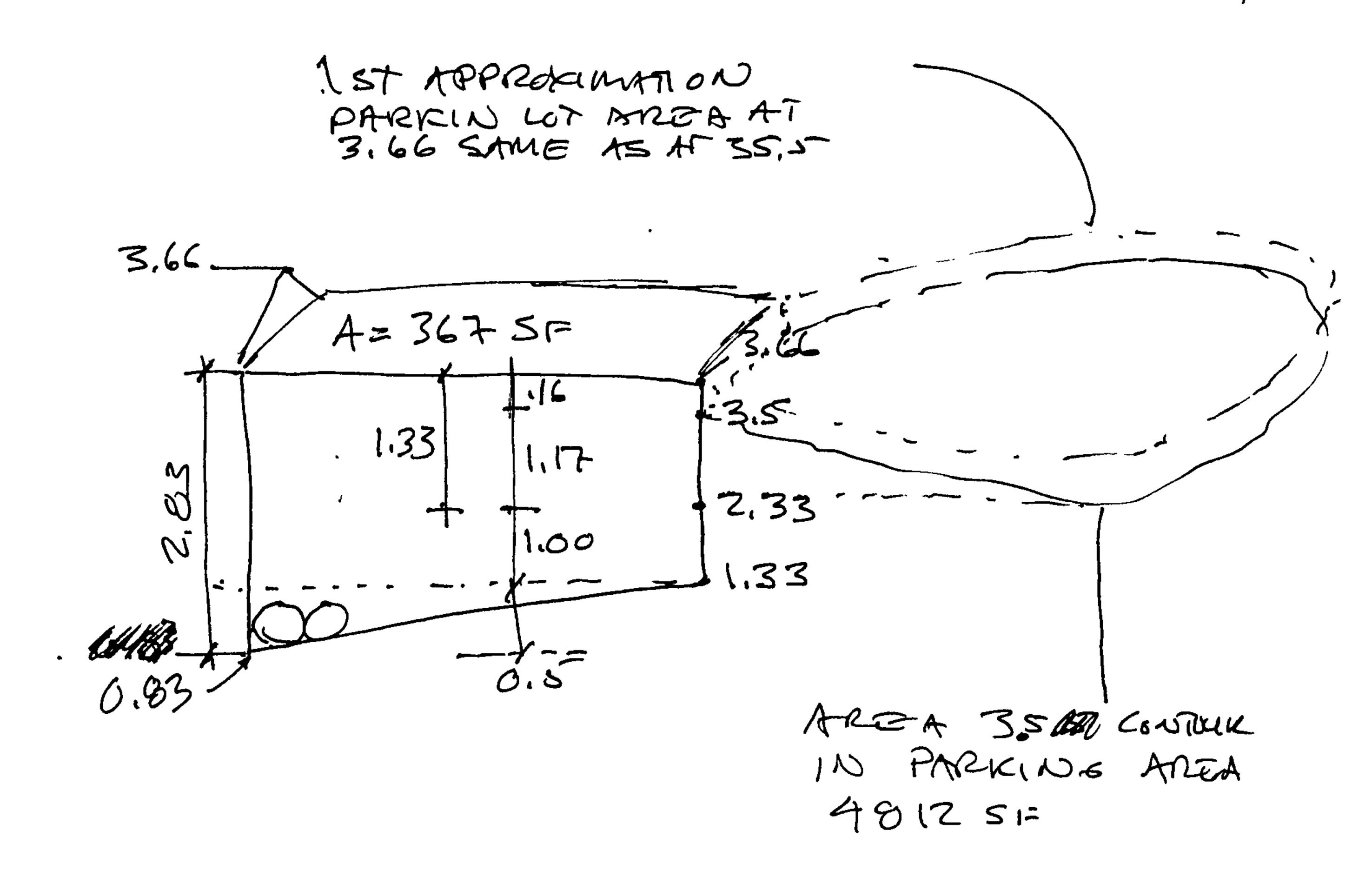
C=ALL ECSE = 39143-5025 = 34,1185FX 20,783ZACX

* THIS INCLUDES NMHSTD ROW CONTRIBUTING
FLOW TO THE SITE.

MS %'S A B MA MAS

0 1.04 11.79 27.16

39143 5FN 0.8986 ACN ,0014041 SCM



AREA 3.0 CONTOUR IN PARKING 1447 SF FILE=ESSVOL.WQ1

08/13/99

11:34 AM

ECONOMY SALES AND SERVICE - 421 RANKIN RD. NE SMALL RECTANGULAR POND W/ VERICAL WALLS AS AVERAGE END AREA, PLUS PARKING LOT PONDING AS "PYRAMID", ELEV 2.33 AND UP

RECTANGULAR POND IN CORNER

		PYRAMID			AV END AREA
ELEV FT	AREA	DVOL CONE	VOL FT ^ 3	VOL AC-FT	DVOL AV AREA VOL FT ^ 3 VOL AC-FT
3.66	367	59	916	0.0210	59 947 0.0217
3.5	367	184	858	0.0197	184 888 0.0204
3	367	• 246	674	0.0155	246 705 0.0162
2.33	367	. 367	428	0.0098	367 459 0.0105
1.33	367	61	61	0.0014	92 92 0.0021
0.83	0		0	0.0000	0.0000

PARKING AREA PONDING

		PYRAMID		AV END AREA				
ELEV FT	AREA	DVOL CONE	VOL FT ^ 3	VOL AC-FT	DVOL AV ARE VOL FT 3 VOL AC-FT			
3.66	4812	770	2576	0.0591	770 2819 0.064			
3.5	4812	1483	1806	0.0415	1565 2049 0.0470			
3	1447	323	323	0.0074	485 485 0.011			
2.33	0		0	0.0000	0.0000			

ELEV =	H =	TOTAL VOLUME =	TOTAL VOLUME =
3.66	2.83	3,523 CU FT, OR	0.0809 AC FT
3.5	2.67	2,694 CU FT, OR	0.0619 AC FT
3	2.17	1,028 CU FT, OR	0.0236 AC FT
2.33	1.5	459 CU FT, OR	0.0105 AC FT
1.33	0.5	92 CU FT, OR	0.0021 AC FT
0.83	0	0 CU FT, OR	0.0000 AC FT

FILE = ESorfice2.123

ORIFICES FOR POND ROUTING

08/13/99

HEAD MATCH ELEVS FOR POND VOULUMES

09:48 AM

FREE DISCHARGE FLOW THROUGH ORFICE: Q = C*A*SQRT(2*g*h)

C=COEFFICIENT, APX 5/8; A= FLOW AREA, SF; g=GRAVITY=32.17 FT/SEC ^ 2

h=HT OF WATER SURFACE ABOVE *CENTROID* OF FLOW AREA, FT

H=HT OF WATER ABOVE BOTTOM OF ORIFICE, = CENTROID + h)

C*SQRT(2*g) OFTEN TAKEN AS 5.0, = > C=0.623346

MATHEMATICALLY NOT VALID FOR WATER SURFACE BELOW CENTROID OF ORIFICE!

==> ENTER THIS NUMBER

CIRCULAR 5*A*SQRT(h) # H, FT # DIAM,FT h, FT AREA, SF Q, CFS V, FPS Q * 2 (2 ORIFICES)	0.200 0.2500 0.075 0.049 0.067 1.369 0.134	0.500 0.2500 0.375 0.049 0.150 3.062 0.301	1.500 0.2500 1.375 0.049 0.288 5.863 0.576	2.170 0.2500 2.045 0.049 0.351 7.150 0.702	2.670 0.2500 2.545 0.049 0.392 7.977 0.783	2.830 0.2500 2.705 0.049 0.404 8.223 0.807	3.000 0.2500 2.875 0.049 0.416 8.478 0.832		
CIRCULAR 5*A*SQRT(h) # H, FT # DIAM,FT h, FT AREA, SF Q, CFS V, FPS	0.200	0.500	1.500	2.170	2.670	2.830	3.000	3.200	3.400
	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333
	0.033	0.333	1.333	2.003	2.503	2.663	2.833	3.033	3.233
	0.087	0.087	0.087	0.087	0.087	0.087	0.087	0.087	0.087
	0.080	0.252	0.504	0.618	0.690	0.712	0.734	0.760	0.785
	0.913	2.887	5.774	7.077	7.911	8.160	8.416	8.708	8.991

17

```
INPUT FILE = ESS600A.dta
*C PRINT CODES: 0=ALL; 1=TOTALS ONLY; 2=EVERY 2ND + TOTALS; 3,5,10,20 SIMILAR
*C RATING CURVE ID NEGATIVE ⇒ COMPUTE BUT NOT PRINT RATING CURVE
*C PATING CURVE IN NEGATIVE ⇒ FLOODPLAIN SLOPE, IN POSITIVE ⇒ CHANNEL SLOPE
*S
*S FILE ESS600a - Economy Sales & Service, 6-hour, 100 year storm
                421 Rankin Rd NE at I-25 west frontage road
*S CUTFLOW LIMITED TO 0.79cfs so entire (site + offsite) matches exist allowable
*S
*S FLOW IS **NOT** BULKED FOR SEDIMENT
*C RAINFALLL ESTIMATED FROM CITY OF ALBUQUERQUE D.P.M. FIGURES C-1, C-2, & C-3
                   hr ⇒ 1.95 INCHES; 6hrs ⇒ 2.3 INCHES; 24 hrs ⇒ 2.6 INCHES
*C
*C
*C BASIN & CHANNEL POUTING PARAMETERS REFLECT THE JUDGMENT OF THE ENGINEER,
*C AND MAY DIFFER FROM OTHER STUDIES IN THE AREA.
*C
*C REVISION NOTES: CRIGINAL FILE CREATED 8-11-99 BY TUCKER CREEN P.E.
*C
*C
* RAINFALLS PER ALBUQUERQUE NM DPM - COMMENT OUT THOSE THAT DON'T APPLY
* TYPE 1 IS 6-HR STORM PER NOAA ATLAS 2 W PEAK INTENSITY @ 1.4 HRS (EQ C1-C5)
    FOR 6-HR USE DT = 0.0333333 HR = 2 MINUTES
* TYPE 2 IS 24-HR STORM PER NOAA ATLAS 2 W PEAK INTENSITY @ 1.4 HRS (EQ C1-06)
    FOR 24-HR USE DT = 0.0500 HR = 5 MINUTES
* PAIN CLARTER = 0.0 EXCEPT FOR TYPE 3 (6-HR PMP: SEE AHMO MANUAL)
* FOR 10-YR STORM, USE 0.667 * 100-YR VALUES (PER DPM 22.2 TABLE A-3, JAN 1993)
PAINFALL AMOUNTS, INCHES
* RAINFALL
                     HUNDRED TYPE= 2 RAIN QUARTER= 0.0 RAIN ONE= 1.97
                   RAIN SIX= 2.31 RAIN DAY= 2.7 DT= .05 HR
                   HUNDRED TYPE= 1 0.0 1.95 2.3 2.6
RAINFALL
                                                              0.033333
```

AHYMO PROGRAM (AHYMO194) - AWAFCA Hydrologic Model - January, 1994

START TIME (HR:MIN:SEC) = 11:48:15 USER NO. = PERSEENG. 194

RUN DATE (MON/DAY/YR) = 08/13/1999

COMPUTED 6-HOLR PAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2 - PEAK AT 1.40 HR.

W	MEGIED	O-DUN N	ACTIALNET	DISIUIDO	ITON DAG		MY AILAS	Z - PEAN AI	1.40 m
DT	=	.033333 F	DURS .	END T	IME =	5.9999	40 HOURS		
	.0000	.0018	.0035	.0054	.0072	.0092	.0111		
	.0131	.0152	.0173	.0194	.0216	.0239	.0262		
	.0286	.0311	.0336	.0363	.0390	.0418	.0447		
	.0477	.0508	.0541	.0575	.0610	.0648	.0686		
	.0727	.0771	.0816	.0870	.0928	.0989	.1122		
	.1418	.1874	.2529	.3423	.4597	.6095	.7959		
	1.0234	1.2339	1,3220	1.3963	1.4625	1.5227	1.5781		
	1.6295	1.6776	1.7227	1.7651	1.8051	1.8429	1.8787		
	1.9126	1.9447	1.9752	2.0041	2.0316	2.0380	2.0441		
!	2.0498	2.0553	2.0605	2.0655	2.0703	2.0749	2.0794		
1	2.0837	2.0879	2.0919	2.0958	2.0996	2.1033	2.1070		
	2.1105	2.1139	2.1172	2.1205	2.1237	2.1268	2.1299		
,	2.1329	2.1358	2.1387	2.1416	2.1443	2.1471	2.1497		
	2.1524	2.1550	2.1575	2.1600	2.1625	2.1649	2.1673		
	2.1697	2.1720	2.1743	2.1765	2.1788	2.1810	2.1831		
	2.1853	2.1874	2.1895	2.1916	2.1936	2.1956	2.1976		

 2.1996
 2.2015
 2.2034
 2.2053
 2.2072
 2.2091
 2.2109

 2.2128
 2.2146
 2.2164
 2.2181
 2.2199
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 2.2233

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 2.2780
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 2.2844

 2.2856
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 2.2881
 2.2893
 2.2905
 2.2917
 2.2929

 2.2941
 2.2953
 2.2965
 2.2977
 2.2988
 2.3000

* RAINFALL

*

TENYEAR TYPE= 1 0.0 1.31 1.54 1.80 0.033333

*S AL CONTRIBUTING. INCLUDES 125 POW, EXCLUDES EX.BLDG & FRONT OF SITE

COMPUTE NM HMD ID= 1 HMD= WEST DA=0.0014041 SQ MI PER A= 0 B= 1.04 C= 87.16 D= 11.79

TP= -0.13333 HRS RAIN= -1

*****WARNING***** SUM OF TREATMENT TYPES DOES NOT EQUAL 100 PERCENT OR TOTAL AREA

K = .072665HR TP = .133330HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420 UNIT PEAK = .66349 CFS UNIT VOLUME = .9815 B = 526.28 P60 = 1.9500 AREA = .000166 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR PUNCFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .107083HR TP = .1333330HR K/TP RATIO = .803145 SHAPE CONSTANT, N = 4.458608 UNIT PEAK = 3.5732 CFS UNIT VOLUME = .9969 B = 384.66 P60 = 1.9500 AREA = .001239 SQ MI IA = .35177 INCHES INF = .83495 INCHES PER HOUR PUNCEF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 1 CODE= 5

HYCROGRAPH FROM AREA WEST

TIME	FLOW								
HRS	CFS								
.000	.0	1.333	.4	2.667	.0	4.000	.0	5.333	.0
.167	.0	1.500	2.9	2.833	.0	4.167	.0	5.500	.0
.333	.0	1.667	1.5	3.000	.0	4.333	.0	5.667	.0
.500	.0	1.833	.8	3.167	.0	4.500	.0	5.833	.0
.667	.0	2.000	.4	3.333	.0	4.667	.0	6.000	.0
.833	.0	2.167	.2	3.500	.0	4.833	.0	6.167	.0
1.000	.0	2.333	.1	3.667	.0	5.000	.0		
1.167	.0	2.500	.1	3.833	.0	5.167	.0		

FUNOFF VOLUME = 1.18740 INCHES = .0889 ACPE-FEET

PEAK DISCHARGE PATE = 2.90 CFS AT 1.500 HOURS BASIN APEA = .0014 SQ. MI.

*S HYD PONDOUT.203 IS FOR 2 3-INCH DIAWETER OFIFICES
ROUTE RESERVOIR ID=3 HYD=PONDOUT.203 INFLOW ID=1

ID=3 HYD=PONDOUT.2D3 INFLOW ID=1 CODE=5.

OUTFLOW CFS STOPAGE AC-FT ELEVATION FT

31. WCH ()

		0.000 0.301 0.576 0.702 0.783 0.807	0.000 0.0021 0.0105 0.0236 0.0619 0.0809		0.83 1.33 2.33 3.0 3.5 3.66				
* * *	* * *	* * * :	* * * *	* * *					
TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	CUTFLOW (CFS)					
.00	.00	.83	.000	.00					
.17	.00	.83	.000	.00					
.33	.00	.83	.000	.00					
.50	.00	.83	.000	.00					
.67	.00	.83	.000	.00					
.83	.00	.83	.000	.00					
1.00	.00	.83	.000	.00					
1.17	.00	.83	.000	.00					
1.33	.35	1.02	.001	.11					
1.50	2.90	2.72	.018	.65		4			
1.67	1.54	3.21	.040	.74					
1.83	.78	3.28	.045	.75					
2.00	.44	3.25	.043	.74					
2.17	.20	3.18	.037	.73					
2.33	.10	3.07	.029	.71					
2.50	.06	2.84	.021	.67					
2.67	.04	2.43	.012	.60					
2.83	.02	1.77	.006	.42					
3.00	.01	1.16	.001	.20					
3.17	.01	.89	.000	.03					
3.33	.00	.84	.000	.01				-1/ - 1 A A	
3.50	.00	.84	.000	.00			7	34 DIAM	
PEAK DISCHA	RGE =	.747 C	FS - PEAK C	COURS AT	HOUR 1.83			34 DIAM ORIFICES	
MAXIMLM WAT	ER SURFACE	ELEVATION	= 3	3.278				CYCIT	
MAXIMUM STO	RAGE =	.0449	AC-FT	INCREMEN	TAL TIME=	.033333HR	S _		
					********	****	***	1	. ,
*S HYD PONDO ROUTE RESERV	OIR I		INCG DIAMET ONDOUT. 1D4 STORAGE 0.000	INFLOW		E≒5.		4' DIAM CHIF	(CC
		0.252	0.0021		1.33				
		0.504	0.0105		2.33				
		0.618	0.0236		3.0				
		0.690	0.0619		3.5				
		0.712	0.0809		3.66				
* * *	* * *	* * *	* * *	* * *					
TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	CUTFLOW (CFS)					
			^^^	~~					
.00	.00	.83	.000	.00					
.17	.00	.83	.000	.00					
.33	.00	.83	.000	.00					
.50	.00	.83	.000	.00				7/1	

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                                     .020
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                .02
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PEAK DISCHARGE =
                         .664 CFS - PEAK COOURS AT HOUR
                                                           1.90
MAXIMUM WATER SURFACE ELEVATION =
                                         3.320
MAXIMUM STORAGE =
                          .0481 AC-FT
                                           INCREMENTAL TIME=
                                                                  .033333HRS
```

FINISH

*

NORMAL PROGRAM FINISH

END TIME (HR:MIN:SEC) = 11:48:15



City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

MOTICE

all applications for BUILDING PERMITS and/or SITE PLAN APPROVALS

now require a **DUAL** submittal: the standard grading and drainage plan for Hydrology plus the site plan for the traffic circulation layout (TCL) for Transportation. The following also are needed for the TCL:

A. Building elevations showing all entrances and overhead doors including dimensions of overhead doors.

B. Landscape plan unless all landscaped areas are clearly called out on the Site Plan.

C. Include the estimated value of project to be constructed.

*****EFFECTIVE APRIL 15, 1999*****
-See Asst. PWD Director Letter of April 15, 1999-



City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

April 15, 1999

SUPERCEDES LETTER DATED MARCH 15, 1999

TO:

Distribution

FROM:

John R. Castillo, Acting City Engineer, and Public Works Department

SUBJECT:

MODIFICATION OF REVIEW AND APPROVAL PROCESS FOR ALL COMMERCIAL BUILDING PERMIT AND SITE PLAN APPPLICATIONS WITHIN

THE TRANSPORTATION AND HYDROLOGY SECTIONS AT ONE-STOP SHOP

In an effort to continue to streamline the One-Stop Shop process, we will be combining the reviews and approvals of all commercial building permit and site plan applications submitted to the Transportation and Hydrology Sections, effective immediately. The intent of the modified process is to minimize the time needed for the approvals of building permits and site plans by allowing the applicant to make a submittal in advance of their building permit/site plan application.

The new procedure will be accomplished by requiring that transportation design elements per the DPM be addressed in combination with the drainage plan submittal. The transportation design elements can either be:

- illustrated on the drainage plan, or

the engineer or the architect can provide a separate plan showing the parking layout and the circulation with an engineer and/or architect signature, stamp and date.

All applications for building permit and site plan approvals will require two copies of the submittal. These copies will be routed to the Transportation staff and to the Hydrology staff for their review and approval. A combined response will be issued to the applicant either approving the plans or addressing deficiencies on the application. All response from the City will reference an engineer's dated stamp.

An engineer's certification of the approved drainage/transportation plan will be required for approval of the CERTIFICATE OF OCCUPANCY (CO). The Hydrology Section will be responsible for releasing all building permits and issue CO's once the certification has been accepted by the City. This new process will eliminate the need for individual site inspections by the Transportation Section.

If you have any questions regarding the above, please feel free to contact me or my staff (Fred J. Aguirre/Richard Dourte) at 924-3979.

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	drafting/plotting supplies	
	miscellaneous	

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contact:						

3330 candelaria ne • albuquerque, nm • call 505.884.2080 visit our home page on the world wide web www.sun-graphix.com



KEN SCHULTZ

MAYOR

City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

March 31, 1989

Marvin R. Kortum, P.E. 1605 Speakman Drive, SE Albuquerque, New Mexico 87123

> DRAINAGE PLAN FOR LOT 13A & 13B OF COMAN INDUSTRIAL DISTRICT (G-15/D10) ENGINEER'S STAMP DATED MARCH 20, 1989

Dear Mr. Kortum:

Based on the information provided on your submittal of March 21, 1989, the referenced drainage plan is approved for Final Plat.

If I can be of further assistance, please feel free to call me at 768-2650.

Cordially,

Bernie J. Montoya, C.E.

Engineering Assistant

BJM/bsj (WP+1060)

DRAINAGE INFORMATION SHEET

F'ROJECT TITLE:	Lot 1 and 13-B Coman industrial Dist	rictzone	TLAS/DRN	G. FILE #• C	1-15 /15 (RA)
LEGAL DESCRIPTI					
CITY ADDRESS:	821 Rankin Road NE				
ENGINEERING FIR	M. Marvin R Kortum 1605 Speakman Drive	C	ONTACT:	Marvin R	Kortum
ADDRESS:	Albuquerque, New Meise	xico 87123	PHONE:	(505) 299	-0774
OWNER: New Mex	cico Millwright		ONTACT:		
ADDRESS:	821 AMKIN RS NG	P	HONE:	······································	
ARCHITECT:			ONTACT:		
ADDRESS:		P	HONE:		
SURVEYOR:	Southwest Survey Co.	Inc. C	ONTACT:	Dan Graney	
ADDRESS:	333 Lomas Blvd NE Albuquerque, New Mexic	30 PI	HONE:	247-4444	
CONTRACTOR:			INTACT:		
ADDRESS:		<u></u>	10NE:		
PRE-DESIGN MEETI YES X NO COPY OF CONSHEET PROVIS	MAR 2 1 1989 HYDROLOGY SECTION FERENCE RECAP	DRB NC EPC NC ON PROJ.	}.	21	
GRADING PLAN	PORT AN Revision SRADING & DRAINAGE PLAN N Revision	SKET PREL SITE FINA BUIL FOUN CERT ROUG	CH PLAT A IMINARY A DEVELOPA L PLAT AA DING PERM DATION PE H GRADING ING/PAVIN	PLAT APPROVAL MENT PLAN APPROVAL AIT APPROVAL ERMIT APPROVAL OF OCCUPANCY A EPERMIT APPROVAL OF PERMIT APPRO	ROVAL APPROVAL OVAL
DATE SUBMITTED: BY:	March 21, 1989 Arvin R Kortum Mortum	26.			•



KEN SCHULTZ

MAYOR

City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

March 31, 1989

Marvin R. Kortum, P.E. 1605 Speakman Drive, SE Albuquerque, New Mexico 87123

RE: DRAINAGE PLAN FOR LOT 13A & 13B OF COMAN INDUSTRIAL DISTRICT (G-15/D10) ENGINEER'S STAMP DATED MARCH 20, 1989

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Cordially,

Bernie J. Montoya, C.E. Engineering Assistant

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