

CITY OF ALBUQUERQUE

Planning Department
Brennon Williams, Director



Mayor Timothy M. Keller

June 29, 2020

Donald Duneman
Wilson & Company Inc.
4401 Masthead St NE, Suite 150
Albuquerque, NM, 87109

**RE: 4600 Edith Blvd NE – SWMD Admin. Office and Vehicle Maintenance
Drainage Report (Engineer's Stamp 6/16/2020)
Hydrology File: G15D202**

Based upon the information provided in your submittal received 6/16/2020, the Conceptual Grading and Drainage Plan and Drainage Report are approved for Building Permit and Work Order. All comments in the Drainage Report have been addressed.

PO Box 1293

Prior to Certificate of Occupancy

1. An engineer's Certification will be required for each building with site improvements complete according to the approved phasing plan.

Albuquerque

NM 87103

If you have any questions, please contact me at 924-3986 or earmijo@cabq.gov.

Sincerely,

www.cabq.gov

Ernest Armijo, P.E.
Principal Engineer, Planning Dept.
Development Review Services



City of Albuquerque

Planning Department

Development & Building Services Division

DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 11/2018)

Project Title: _____ Building Permit #: _____ Hydrology File #: _____

DRB#: _____ EPC#: _____ Work Order#: _____

Legal Description: All or a portion of a northerly portion of Tract 107B1A1, Tract 107B1A1 excl portion to right-of-way & excl a northerly portion, Tract 107B1A2 excl portion to right-of-way, Tract in the SW corner-Tract 107B1B, Tract 108A3A1A, Tract 108A3A1B, and Tract 108A3B, Tracts 108A1A2B1B & 108A1A2B2, Tract 108A1A2B1A, Tract 107B2A2 excl portion to the right-of-way, Tract 107B2A1 excl portion to the right-of-way, MRGCD Map #33

City Address: _____

Applicant: _____ Contact: _____

Address: _____

Phone#: _____ Fax#: _____ E-mail: _____

Owner: _____ Contact: _____

Address: _____

Phone#: _____ Fax#: _____ E-mail: _____

TYPE OF SUBMITTAL: _____ PLAT (____# OF LOTS) _____ RESIDENCE _____ DRB SITE _____ ADMIN SITE

IS THIS A RESUBMITTAL?: _____ Yes _____ No

DEPARTMENT: _____ TRAFFIC/ TRANSPORTATION _____ HYDROLOGY/ DRAINAGE

Check all that Apply:

TYPE OF SUBMITTAL:

- _____ ENGINEER/ARCHITECT CERTIFICATION
- _____ PAD CERTIFICATION
- _____ CONCEPTUAL G & D PLAN
- _____ GRADING PLAN
- _____ DRAINAGE MASTER PLAN
- _____ DRAINAGE REPORT
- _____ FLOODPLAIN DEVELOPMENT PERMIT APPLIC
- _____ ELEVATION CERTIFICATE
- _____ CLOMR/LOMR
- _____ TRAFFIC CIRCULATION LAYOUT (TCL)
- _____ TRAFFIC IMPACT STUDY (TIS)
- _____ OTHER (SPECIFY) _____
- _____ PRE-DESIGN MEETING?

TYPE OF APPROVAL/ACCEPTANCE SOUGHT:

- _____ BUILDING PERMIT APPROVAL
- _____ CERTIFICATE OF OCCUPANCY
- _____ PRELIMINARY PLAT APPROVAL
- _____ SITE PLAN FOR SUB'D APPROVAL
- _____ SITE PLAN FOR BLDG. PERMIT APPROVAL
- _____ FINAL PLAT APPROVAL
- _____ SIA/ RELEASE OF FINANCIAL GUARANTEE
- _____ FOUNDATION PERMIT APPROVAL
- _____ GRADING PERMIT APPROVAL
- _____ SO-19 APPROVAL
- _____ PAVING PERMIT APPROVAL
- _____ GRADING/ PAD CERTIFICATION
- _____ WORK ORDER APPROVAL
- _____ CLOMR/LOMR
- _____ FLOODPLAIN DEVELOPMENT PERMIT
- _____ OTHER (SPECIFY) _____

DATE SUBMITTED: _____ By: _____

COA STAFF:

ELECTRONIC SUBMITTAL RECEIVED: _____

FEE PAID: _____

June 16, 2020

Ernest Armijo, PE
Principal Engineer, Planning Dept.
Development Review Services
City of Albuquerque

Re: G15D202 SWMD Administration & Maintenance Building Project

Dear Mr. Armijo,

Wilson & Company has reviewed the comments provided in an email dated June 15, 2020 on the SWMD Admin. Office & Vehicle Maintenance Project. **Below are the responses to the comments:**

1. StormCAD inlet and manhole numbering does not match up structure numbers on plan sheets. No tables or references explain or tabulate the structure numbers used in the plan and profile sheets. Please provide construction specifications and details for all of the hydraulic structures (build notes). The numbering system (nodes) in the calculations should be shown match those used on the Plan and Profile sheets. **StormCAD labels of manhole and inlets were revised to match the CADD structure numbers on the plan & profile sheets. Please see Appendix D for updated results. Keynotes on updated sheets C-408 to C-412 indicate structure specs. Please refer to Appendix F.**
2. Sheet C-408: This sheet and the corresponding calculations in the report do not match with the Work Order plan set. This includes pipe lengths, slopes, HGL's, and velocities. Please determine which is to be used and make sure all calculations work with chosen layout. **Sheet updated and all information added.**
 - On Detail D5-01 please add roadway identification or call out on overall sheet to identify where this detail sits overall. **Labels and notes added.**
 - Add a north arrow to Detail SD-01 so not to confuse the orientation with Detail D5-01. **North arrow was added.**
 - Call out size and type of manhole on detail of SD-01. **Type and size manhole added.**
 - Inlet structure (104) appears on the plan to be located in the middle of the road, but is called out as a Type "C" which has a curb inlet. **Inlet type was changed to area inlet. See sheets C-408**
3. Sheets C-410 to C-412: Manhole and Inlet labels have not been added. **Structure labels in profile view matching revised StormCAD labels and keynotes in plan view. See sheets C-410 to C-412.**
4. Please specify the Curb type/height on the G&D Plans. I see you added the calculation but the type and height need to be called out on the plans. **Key notes for curb type/heights were specified on sheets C-110 to C-112.**
5. Typical sections should be shown in the north-south direction also. Please indicate what direction the cross section is looking. Each section should show the property line, both the existing and proposed grades, slopes and walls with dimensions, both horizontal and vertical, as necessary to demonstrate

compliance with DPM 22.5.B. **Site sections in the north and south direction were added. See sheets C-302 to C-307 for site section sheets.**

Prior to Certificate of Occupancy

6. An engineer's Certification will be required for each building with site improvements complete according to the approved phasing plan. **Engineer's certification will be completed upon completion of each phase of construction.**

Please feel free to contact me, should you have any further questions or comments on these responses. Thank you for your time.

Sincerely,

A handwritten signature in black ink, appearing to read "Don Duneman", with a stylized, flowing script.

Donald Duneman, PE
Project Manager
donald.duneman@wilsonco.com
505-238-0152

Attachments:
Drainage Report – PDF Copy

June 2020

**Drainage Analysis
For
Maintenance & Administration Building Project
COA Project Number 700693**

City of Albuquerque, NM

**WILSON
& COMPANY**

discipline | intensity | collaboration | shared ownership | solutions

Drainage Analysis for

SWMD Administration & Maintenance Building Project

June 2020



Prepared by:

Wilson & Company, Inc.
4401 Masthead Street, NE, Suite 150
Albuquerque, New Mexico 87109
(505) 348-4000

WCI File No: 14-100-132-01

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DRAINAGE ANALYSIS

1. Introduction

The project site is located in northeast Albuquerque at 4600 Edith Blvd. The site is bounded by the Alameda Drain/Edith Blvd. to the west, Comanche Road to the north, Rankin Road to the south, and commercial businesses to the east of the site. See Figure 1, Vicinity Map. The site is not located within a designated FEMA flood plain firm maps 35001C0119G and 35001C0332G. See attached FIRMETT at the end of this section. The drainage report has been prepared in accordance with the latest revision to volume 2 section 22.2 of the City of Albuquerque (COA) Development Process Manual (DPM).



Figure 1 – Vicinity Map

2. Methodology

The AHYMO S-4 program was used to calculate peak flows and runoff volume for the existing and proposed development. Bentley FlowMaster v8i were utilized to determine roadway and inlet capacities. Bentley CulvertMaster v3.3 was used to analyze ponds outfall pipes. StormCAD v10.1 software was used to analyze and design the underground storm drain systems. See Appendices A to E for results.

3. Existing Conditions

The site is 23.8 ac and majority of the site is impervious. The existing site topography generally slopes from east to west. The existing drainage infrastructure diverts all the sites flows through a series of water/oil separators and inlets into two ponds located on the north and south of the site. The larger detention pond to the north has an outlet structure that discharges through a 30 inch Reinforced Concrete Pipe (RCP) into a drainage system in Comanche Road. The construction plans for storm water control improvements for Solid Waste Management Facility COA Project Number 700691 prepared by Applied Engineering and Surveying, Inc. Dated 07/22/03 sheet 2 of 17 shows an outlet from the pond with peak flow of 44.3 cfs and an allowable discharge of 47.6 cfs from the site. The northern three quarters of the site drains into this pond. The remainder of the site drains into the smaller retention pond to the southwest corner of the site.

The commercial businesses to the east of the site also drain from the east to west. The buildings on these commercial sites are approximately 10-15 ft higher than the sites existing grades. The offsite flows will flow directly to the east. The north half drains into the north pond and the south half flows into the south retention pond. The south pond is a shallow pond with rock riprap spillway draining into Rankin Road. The area to the north of the site is Comanche Road which has drainage infrastructure in place to prevent flows from being discharged into the project site. Rankin Road drains east to west and runoff sheet flow to a cattle guard inlet east of intersection of Rankin Road and Edith Blvd. Flows do not enter the property. The area to the west drains east to west and those flows will enter the Alameda Drain. The AHYMO S-4 program was used to calculate existing peak flows and runoff volumes for the 100-yr, 24-hr storm event. See AHYMO summary and input files in Appendix A and Table 1, Existing Basin Data Summary.

Basin	Total	Total	C		D		Peak Discharge (cfs), Q_{100} yr-24 hr	Volume (ac-ft) V_{100} yr-24 hr
	Area (sq ft)	Area (Ac)	%	Ac	%	Ac		
A	62474.32	1.434	5	0.07	95	1.36	5.9	0.267
B	93252.44	2.141	5	0.11	95	2.03	8.9	0.401
C	48109.31	1.104	5	0.06	95	1.05	4.6	0.207
J	358117.7	8.221	5	0.41	95	7.81	34.5	1.556
K	345257	7.926	5	0.40	95	7.53	33.4	1.507
Offsite 1	55,490	1.274	10	0.13	90	1.15	5.3	0.235
Offsite 2	46,468	1.067	10	0.11	90	0.96	4.4	0.197

Table 1 – Existing Conditions Basin Data

4. Proposed Conditions

The proposed site will maintain the general flow direction of east to west and south to north. See Grading & Drainage Plan in Appendix F. The AHYMO S-4 program was used to calculate proposed peak flows and runoff volumes for the 100-yr, 24-hr storm event. See AHYMO summary and input files in Appendix A and Table 2, Proposed Basin Data Summary.

Basin	Total	Total	C		D		Peak Discharge (cfs), Q_{100} yr-24 hr	Volume (ac-ft) V_{100} yr-24 hr
	Area (sq ft)	Area	%	Ac	%	Ac		
201	48,732	1.119	10	0.11	90	1.01	4.7	0.207
202	78,424	1.800	10	0.18	90	1.62	7.5	0.332
203	48,462	1.113	5	0.06	95	1.06	4.3	0.195
204	105,306	2.417	5	0.12	95	2.30	10.2	0.460
205	54,819	1.258	5	0.06	95	1.20	5.3	0.239
206	59,717	1.371	5	0.07	95	1.30	6.0	0.271
207	23,213	0.533	5	0.03	95	0.51	2.3	0.101
208	38,436	0.882	5	0.04	95	0.84	3.7	0.168
209	39,485	0.906	2	0.02	98	0.89	3.9	0.176
210	40,798	0.937	2	0.02	98	0.92	4.0	0.181
211	71,721	1.646	5	0.08	95	1.56	6.9	0.312
212	56,736	1.302	5	0.07	95	1.24	5.5	0.248
213	6,289	0.144	75	0.11	25	0.04	0.6	0.025
214	38,158	0.876	75	0.66	25	0.22	3.5	0.147
215	10,070	0.231	10	0.02	90	0.21	1.0	0.042
216	5,758	0.132	5	0.01	95	0.13	0.6	0.026
217	12,735	0.292	20	0.06	80	0.23	1.2	0.051
218	90,301	2.073	10	0.21	90	1.87	8.6	0.382
219	10,416	0.239	5	0.01	95	0.23	1.0	0.045
220	38,671	0.888	15	0.13	85	0.75	3.6	0.159
221	16,629	0.382	10	0.04	90	0.34	1.6	0.071
222	41,098	0.943	2	0.02	98	0.92	4.0	0.182
Offsite 1	55,490	1.274	10	0.13	90	1.15	5.3	0.235
Offsite 2	46,468	1.067	10	0.11	90	0.96	4.4	0.197

Table 2 – Proposed Conditions Basin Data

The contour data used in computation of the pond volumes were extracted from graded area using AutoCAD software. CulvertMaster application was used in calculating the pond discharge table. StormCAD was used to design storm systems. The water surface elevation at maximum peak inflow time was extracted from AHYMO model as the starting HGL elevation of pipes draining into the ponds. The pond discharge rating table was developed using CulvertMaster. The tail water elevation was extracted from the StormCAD model and used as input in the culvert discharge rating curve. FlowMaster was used to compute roadway and inlet capacities. See Appendices A to E for calculations.

All the basins except basin 206 will ultimately drain into Pond A located in basin 220. Runoff from basins 201-205 and offsite basins 1 and 2 will be captured and routed through Pond B in basin 204. This pond will be lined to capture any oil from the site runoff. Pond B outlet pipe will ultimately discharge into the new Pond A in basin 220. Pond A outfall will be connected to the existing pond drainage infrastructure that discharges to the storm drain system in Comanche Road. This pond will have a water quality riser to help remove trash and sediment from the runoff. The pond discharge will be 44.3 cfs which will be less than the allowable site discharge of 47.6 cfs. The existing 60 inch drainage system in Comanche Road is about 19 ft deep. No data related to hydraulic grade line of this system was found. The pond outfall will tie to the existing 30 inch pipe upstream of the existing system in Comanche Road. The existing retention pond in basin 206 located on the southwest corner will be removed. Runoff from this basin sheet flows to a water quality inlet draining into an underground pond. A new storm drain line will connect the pond outfall to the existing cattle guard inlet at the intersection of Edith Blvd and Rankin Road.

The COA storm water quality volume for the 80th percentile event for the site impervious areas was calculated using 0.26 inch of rainfall depth. This volume was calculated to be 0.23 ac-ft for Pond A, 0.21 ac-ft for Pond B and 0.03 ac-ft for underground Pond C. This retention volume will be accommodated in all ponds. See Table 3, 80th Percentile Volume Calculations.

Pond	Impervious Area (ac)	V _{80th%} (ac-ft)	Elevation
A	10.55	0.23	4989.00 to 4990.86
B	9.63	0.21	4994.00 to 4989.00
C	1.30	0.03	4984.00 to 4985.00
The required 80th percentile required volume is 0.26 inches of excess precipitation from the impervious area			

Table 3 – 80th Percentile Volume Calculation

5. Conclusions

The project site was analyzed to determine any increase in runoff in the developed conditions. The existing drainage pattern will be kept, existing ponds modified and one new pond added to capture generated runoff. Runoff from south of the site will drain into Pond B. Pond B outfall and runoff from the north end will drain into Pond A. As in the current conditions, Pond A outfall will be connected to the existing storm system in Comanche Road. The outflow from the pond will be approximately 44 cfs which is less than the allowable discharge of 47.6 cfs. The new underground pond adjacent to Rankin Road will be connected to a new storm system in Rankin Road to convey about 3 cfs which will drain into the existing cattle guard inlet east of the Edith Blvd intersection. All three ponds will accommodate additional volume to capture the 80th percentile runoff due to addition of impervious areas. Regular maintenance of all the storm drain structure is highly recommended.

National Flood Hazard Layer FIRMette



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS		Without Base Flood Elevation (BFE) Zone A, V, A99
		With BFE or Depth Zone AE, AO, AH, VE, AR
		Regulatory Floodway
OTHER AREAS OF FLOOD HAZARD		0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
		Future Conditions 1% Annual Chance Flood Hazard Zone X
		Area with Reduced Flood Risk due to Levee. See Notes. Zone X
		Area with Flood Risk due to Levee Zone D
OTHER AREAS		NO SCREEN Area of Minimal Flood Hazard Zone X
		Effective LOMRs
		Area of Undetermined Flood Hazard Zone D
GENERAL STRUCTURES		Channel, Culvert, or Storm Sewer
		Levee, Dike, or Floodwall
OTHER FEATURES		20.2 Cross Sections with 1% Annual Chance Water Surface Elevation
		17.5
		Coastal Transect
		Base Flood Elevation Line (BFE)
		Limit of Study
		Jurisdiction Boundary
		Coastal Transect Baseline
MAP PANELS		Digital Data Available
		No Digital Data Available
		Unmapped



The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 5/8/2020 at 3:36:36 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

35°7'48.31"N



USGS The National Map: Orthoimagery. Data refreshed April, 2019.

0 250 500 1,000 1,500 2,000 Feet 1:6,000

35°7'18.88"N

106°37'32.12"W

FIGURE 2

APPENDIX A

AHYMO Calculations.....A-1 to A-12

- AHYMO – Existing Conditions
- AHYMO – Proposed Conditions

AHYMO PROGRAM SUMMARY TABLE (AHYMO-S4) - Ver. S4.01a, Rel: 01a RUN DATE (MON/DAY/YR) =04/07/2020
 INPUT FILE = 32-01\2_Disciplines\Drainage_or_Sitework\Calculations\AHYMO\SWMD - EXIST.txt USER NO.= WilsonCoANMSiteA96476897

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1 NOTATION
---------	---------------------------	-------------	-----------	--------------	----------------------	-----------------------	-----------------	----------------------	--------------	----------------------

*S "EXISTING" CONDITION MODEL FOR SWMD Maintenance & Admin Project

START

TIME= 0.00

LOCATION

ALBUQUERQUE

*S

RAINFALL DATA FROM NOAA ATLAS 14

*S*****

*S 100 YEAR 24HR STORM

RAINFALL TYPE= 2 NOAA 14

RAIN24= 2.600

COMPUTE NM HYD	A	-	1	0.00220	5.94	0.267	2.27932	1.500	4.216	PER IMP= 95.00
COMPUTE NM HYD	B	-	2	0.00330	8.90	0.401	2.27932	1.500	4.212	PER IMP= 95.00
COMPUTE NM HYD	C	-	3	0.00170	4.59	0.207	2.27932	1.500	4.219	PER IMP= 95.00
COMPUTE NM HYD	J	-	4	0.01280	34.45	1.556	2.27932	1.500	4.206	PER IMP= 95.00
COMPUTE NM HYD	K	-	5	0.01240	33.38	1.507	2.27932	1.500	4.206	PER IMP= 95.00
COMPUTE NM HYD	OFF1	-	6	0.00199	5.29	0.235	2.21326	1.500	4.151	PER IMP= 90.00
COMPUTE NM HYD	OFF2	-	7	0.00167	4.44	0.197	2.21326	1.500	4.153	PER IMP= 90.00

FINISH

```

* SWMD Maintenance & Admin Project Proposed Basins
* Drainage Basin Analysis
*S "EXISTING" CONDITION MODEL FOR SWMD Maintenance & Admin Project
*
START                TIME=0.0  PUNCH CODE=0  PRINT CODE=0
LOCATION              ALBUQUERQUE
*
* RAINFALL FROM NOAA COA DEVELOPMENT PROCESS MANUAL
*S  RAINFALL DATA FROM NOAA ATLAS 14
*S*****
*S 100 YEAR 24HR STORM
RAINFALL              TYPE=2
                      QUARTER=0.00 IN
                      HOUR=   1.77 IN
                      SIX HR=  2.29 IN
                      DAY=    2.60 IN   DT=0.03333
*
*** Sub-BASIN A ****
*
COMPUTE LT TP          LCODE=1  UPLAND/LAG TIME METHOD
                      NK=2  ISLOPE=1
                      LENGTH=100 FT  SLOPE=0.050  K=0.7
                      LENGTH=105 FT  SLOPE=0.011  K=2.0
*
COMPUTE NM HYD         ID=1  HYD NO=A  DA=0.0022 SQ MI
                      PER A=00 PER B=00 PER C=5 PER D=95
                      TP=0 hr  MASSRAIN=-1
*
PRINT HYD              ID=1  CODE=1
*
*
*** Sub-BASIN B ****
*
COMPUTE LT TP          LCODE=1  UPLAND/LAG TIME METHOD
                      NK=2  ISLOPE=1
                      LENGTH=100 FT  SLOPE=0.020  K=0.7
                      LENGTH=140 FT  SLOPE=0.020  K=2.0
*
COMPUTE NM HYD         ID=2  HYD NO=B  DA=0.0033 SQ MI
                      PER A=00 PER B=00 PER C=5 PER D=95
                      TP=0 hr  MASSRAIN=-1
*
PRINT HYD              ID=2  CODE=1
*
*
*** Sub-BASIN C ****
*
COMPUTE LT TP          LCODE=1  UPLAND/LAG TIME METHOD
                      NK=2  ISLOPE=1
                      LENGTH=100 FT  SLOPE=0.020  K=0.7
                      LENGTH=100 FT  SLOPE=0.020  K=2.0
*
COMPUTE NM HYD         ID=3  HYD NO=C  DA=0.0017 SQ MI
                      PER A=00 PER B=00 PER C=5 PER D=95
                      TP=0 hr  MASSRAIN=-1
*
PRINT HYD              ID=3  CODE=1
*
*
*** Sub-BASIN J ****
*
COMPUTE LT TP          LCODE=1  UPLAND/LAG TIME METHOD
                      NK=2  ISLOPE=1
                      LENGTH=100 FT  SLOPE=0.020  K=0.7
                      LENGTH=170 FT  SLOPE=0.020  K=2.0
*
COMPUTE NM HYD         ID=4  HYD NO=J  DA=0.0128 SQ MI
                      PER A=00 PER B=00 PER C=5 PER D=95
                      TP=0 hr  MASSRAIN=-1
*
PRINT HYD              ID=4  CODE=1

```

```

*
*
*** Sub-BASIN K ****
*
COMPUTE LT TP          LCODE=1  UPLAND/LAG TIME METHOD
                        NK=2  ISLOPE=1
                        LENGTH=100 FT  SLOPE=0.020  K=0.7
                        LENGTH=600 FT  SLOPE=0.020  K=2.0
*
COMPUTE NM HYD          ID=5  HYD NO=K  DA=0.0124 SQ MI
                        PER A=00 PER B=00 PER C=5 PER D=95
                        TP=0 hr  MASSRAIN=-1
*
PRINT HYD              ID=5  CODE=1
*
*
*****
*** Sub-BASIN OFF1 ****
*
COMPUTE LT TP          LCODE=1  UPLAND/LAG TIME METHOD
                        NK=2  ISLOPE=1
                        LENGTH=100 FT  SLOPE=0.010  K=0.7
                        LENGTH=200 FT  SLOPE=0.050  K=2.0
*
COMPUTE NM HYD          ID=6  HYD NO=OFF1  DA=0.00199 SQ MI
                        PER A=00 PER B=00 PER C=10 PER D=90
                        TP=0 hr  MASSRAIN=-1
*
PRINT HYD              ID=6  CODE=1
*
*
*** Sub-BASIN OFF2 ****
*
COMPUTE LT TP          LCODE=1  UPLAND/LAG TIME METHOD
                        NK=2  ISLOPE=1
                        LENGTH=100 FT  SLOPE=0.010  K=0.7
                        LENGTH=200 FT  SLOPE=0.050  K=2.0
*
COMPUTE NM HYD          ID=7  HYD NO=OFF2  DA=0.00167 SQ MI
                        PER A=00 PER B=00 PER C=10 PER D=90
                        TP=0 hr  MASSRAIN=-1
*
PRINT HYD              ID=7  CODE=1
*
*
*
FINISH

```

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1 NOTATION
*S "PROPOSED" CONDITION MODEL FOR SWMD Maintenance & Admin Project										
START										TIME= 0.00
LOCATION				ALBUQUERQUE						
*S				RAINFALL DATA FROM NOAA ATLAS 14						
*S*****										
*S				100 YEAR 24HR STORM						
RAINFALL	TYPE= 2 NOAA 14									RAIN24= 2.600
COMPUTE NM HYD	OFF2 -	1		0.00167	4.44	0.197	2.21326	1.500	4.153	PER IMP= 90.00
COMPUTE NM HYD	201.00 -	97		0.00175	4.65	0.207	2.21326	1.500	4.152	PER IMP= 90.00
ADD HYD	201SUM 1&97	12		0.00342	9.09	0.404	2.21308	1.500	4.153	
COMPUTE NM HYD	203.00 -	2		0.00160	4.32	0.195	2.27932	1.500	4.220	PER IMP= 95.00
ADD HYD	203SUM 12& 2	10		0.00502	13.41	0.598	2.23414	1.500	4.174	
COMPUTE NM HYD	OFF1 -	1		0.00199	5.29	0.235	2.21326	1.500	4.151	PER IMP= 90.00
COMPUTE NM HYD	202.00 -	98		0.00281	7.46	0.332	2.21326	1.500	4.147	PER IMP= 90.00
ADD HYD	202SUM 1&98	3		0.00480	12.74	0.567	2.21314	1.500	4.149	
COMPUTE NM HYD	204.00 -	2		0.00378	10.19	0.460	2.27931	1.500	4.211	PER IMP= 95.00
ADD HYD	204SUM 3& 2	1		0.00858	22.93	1.026	2.24226	1.500	4.176	
COMPUTE NM HYD	221.00 -	2		0.00060	1.61	0.071	2.21326	1.500	4.181	PER IMP= 90.00
COMPUTE NM HYD	205.00 -	5		0.00197	5.32	0.239	2.27932	1.500	4.217	PER IMP= 95.00
ADD HYD	205SUM 2& 5	4		0.00257	6.92	0.310	2.26367	1.500	4.209	
ADD HYD	205SUMA 1& 4	6		0.01115	29.85	1.336	2.24719	1.500	4.184	
ADD HYD	205SUMB 10& 6	1		0.01617	43.27	1.934	2.24314	1.500	4.181	
ROUTE RESERVOIR	PONDB 1	30		0.01617	41.09	1.858	2.15465	1.567	3.971	AC-FT= 0.383
COMPUTE NM HYD	206.00 -	1		0.00223	6.02	0.271	2.27932	1.500	4.216	PER IMP= 95.00
ROUTE RESERVOIR	PONDC 1	2		0.00223	2.71	0.271	2.27919	1.700	1.901	AC-FT= 0.097
COMPUTE NM HYD	208.00 -	8		0.00138	3.73	0.168	2.27932	1.500	4.222	PER IMP= 95.00
COMPUTE NM HYD	209.00 -	9		0.00142	3.87	0.176	2.31895	1.500	4.260	PER IMP= 98.00
ADD HYD	209SUM 9& 8	11		0.00280	7.60	0.343	2.29921	1.500	4.241	
COMPUTE NM HYD	222.00 -	12		0.00147	4.01	0.182	2.31895	1.500	4.260	PER IMP= 98.00
ADD HYD	222SUM 11&12	13		0.00427	11.61	0.525	2.30593	1.500	4.248	
COMPUTE NM HYD	215.00 -	14		0.00036	0.97	0.042	2.21326	1.500	4.210	PER IMP= 90.00
ADD HYD	215SUM 14&13	15		0.00463	12.58	0.568	2.29867	1.500	4.245	
COMPUTE NM HYD	216.00 -	16		0.00021	0.58	0.026	2.27932	1.500	4.286	PER IMP= 95.00
ADD HYD	216SUM 16&15	17		0.00484	13.15	0.593	2.29780	1.500	4.247	
COMPUTE NM HYD	213.00 -	2		0.00023	0.60	0.025	2.01509	1.533	4.064	PER IMP= 75.00
COMPUTE NM HYD	214.00 -	99		0.00137	3.48	0.147	2.01509	1.533	3.964	PER IMP= 75.00
ADD HYD	214SUM 99& 2	3		0.00160	4.07	0.172	2.01481	1.533	3.978	
COMPUTE NM HYD	210.00 -	1		0.00146	3.98	0.181	2.31895	1.500	4.260	PER IMP= 98.00
ADD HYD	210SUM 1& 3	31		0.00306	8.05	0.352	2.15982	1.500	4.111	
ADD HYD	210SUMA 17&31	18		0.00790	21.20	0.946	2.24435	1.500	4.194	
COMPUTE NM HYD	207.00 -	1		0.00083	2.25	0.101	2.27932	1.500	4.237	PER IMP= 95.00
COMPUTE NM HYD	211.00 -	11		0.00257	6.93	0.312	2.27932	1.500	4.214	PER IMP= 95.00
ADD HYD	211SUM 1&11	10		0.00340	9.18	0.413	2.27914	1.500	4.219	
COMPUTE NM HYD	212.00 -	3		0.00204	5.51	0.248	2.27932	1.500	4.216	PER IMP= 95.00
ADD HYD	212SUM 10& 3	11		0.00544	14.69	0.661	2.27915	1.500	4.218	
COMPUTE NM HYD	218.00 -	1		0.00324	8.60	0.382	2.21326	1.500	4.146	PER IMP= 90.00
ADD HYD	218SUM 18& 1	10		0.01114	29.80	1.328	2.23528	1.500	4.180	
COMPUTE NM HYD	219.00 -	1		0.00037	1.01	0.045	2.27932	1.500	4.258	PER IMP= 95.00
ADD HYD	219SUM 10& 1	19		0.01151	30.81	1.373	2.23668	1.500	4.183	



COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 2 NOTATION
ADD HYD	219SUMA	19&11	18	0.01695	45.50	2.034	2.25031	1.500	4.194	
COMPUTE NM HYD	220.00	-	20	0.00139	3.64	0.159	2.14720	1.500	4.091	PER IMP= 85.00
ADD HYD	220SUM	18&20	21	0.01834	49.14	2.193	2.24248	1.500	4.186	
ADD HYD	POND.IN	21&30	1	0.03451	89.50	4.052	2.20133	1.533	4.052	
ROUTE RESERVOIR	PONDA	1	96	0.03451	44.75	3.821	2.07613	1.733	2.026	AC-FT= 1.243
COMPUTE NM HYD	217.00	-	6	0.00046	1.20	0.051	2.08115	1.533	4.064	PER IMP= 80.00
FINISH										

```

* SWMD Maintenance & Admin Project Proposed Basins
* Drainage Basin Analysis
*S "PROPOSED" CONDITION MODEL FOR SWMD Maintenance & Admin Project
*
START          TIME=0.0  PUNCH CODE=0  PRINT CODE=0
LOCATION         ALBUQUERQUE
*
* RAINFALL FROM NOAA COA DEVELOPMENT PROCESS MANUAL
*S          RAINFALL DATA FROM NOAA ATLAS 14
*S*****
*S 100 YEAR 24HR STORM
RAINFALL      TYPE=2
              QUARTER=0.00 IN
              HOUR=   1.77 IN
              SIX HR=  2.29 IN
              DAY=    2.60 IN   DT=0.03333

*** Sub-BASIN OFF2 ***
*
COMPUTE LT TP      LCODE=1  UPLAND/LAG TIME METHOD
                  NK=2   ISLOPE=1
                  LENGTH=100 FT  SLOPE=0.010  K=0.7
                  LENGTH=200 FT  SLOPE=0.050  K=2.0
*
COMPUTE NM HYD     ID=1   HYD NO=OFF2  DA=0.00167 SQ MI
                  PER A=00 PER B=00 PER C=10 PER D=90
                  TP=0.0 hr  MASSRAIN=-1
*
PRINT HYD          ID=1   CODE=1
*
*
*** Sub-BASIN 201 ***
*
COMPUTE LT TP      LCODE=1  UPLAND/LAG TIME METHOD
                  NK=2   ISLOPE=1
                  LENGTH=100 FT  SLOPE=0.050  K=0.7
                  LENGTH=185 FT  SLOPE=0.011  K=2.0
*
COMPUTE NM HYD     ID=97  HYD NO=201  DA=0.00175 SQ MI
                  PER A=00 PER B=00 PER C=10 PER D=90
                  TP=0.0 hr  MASSRAIN=-1
*
PRINT HYD          ID=97  CODE=1
*
*
* Total Flow from Basin (OFF2 + 201)
ADD HYD            ID=12  HYD NO=201SUM ID I=1  ID II=97
PRINT HYD          ID=12  CODE=1
*
*
*** Sub-BASIN 203 ***
*
COMPUTE LT TP      LCODE=1  UPLAND/LAG TIME METHOD
                  NK=2   ISLOPE=1
                  LENGTH=100 FT  SLOPE=0.020  K=0.7
                  LENGTH=190 FT  SLOPE=0.020  K=2.0
*
COMPUTE NM HYD     ID=2   HYD NO=203  DA=0.0016 SQ MI
                  PER A=00 PER B=00 PER C=5 PER D=95
                  TP=0.0 hr  MASSRAIN=-1
*
PRINT HYD          ID=2   CODE=1
*
*
* Total Flow from Basin (OFF2+201+203)
ADD HYD            ID=10  HYD NO=203SUM ID I=12  ID II=2
PRINT HYD          ID=10  CODE=1
*
*
*****
*** Sub-BASIN OFF1 ***
*
COMPUTE LT TP      LCODE=1  UPLAND/LAG TIME METHOD
                  NK=2   ISLOPE=1
                  LENGTH=100 FT  SLOPE=0.010  K=0.7
                  LENGTH=200 FT  SLOPE=0.050  K=2.0
*
COMPUTE NM HYD     ID=1   HYD NO=OFF1  DA=0.00199 SQ MI
                  PER A=00 PER B=00 PER C=10 PER D=90
                  TP=0.0 hr  MASSRAIN=-1
*
PRINT HYD          ID=1   CODE=1

```

```

*
*
*** Sub-BASIN 202 ****
*
COMPUTE LT TP          LCODE=1  UPLAND/LAG TIME METHOD
                        NK=2  ISLOPE=1
                        LENGTH=100 FT  SLOPE=0.048  K=0.7
                        LENGTH=240 FT  SLOPE=0.052  K=2.0
*
COMPUTE NM HYD          ID=98  HYD NO=202  DA=0.00281 SQ MI
                        PER A=00 PER B=00 PER C=10 PER D=90
                        TP=0.0 hr  MASSRAIN=-1
*
PRINT HYD              ID=98  CODE=1
*
*
* Total Flow from Basin (OFF1+202)
ADD HYD                ID=3  HYD NO=202SUM ID I=1  ID II=98
PRINT HYD              ID=3  CODE=1
*
*
*** Sub-BASIN 204 ****
*
COMPUTE LT TP          LCODE=1  UPLAND/LAG TIME METHOD
                        NK=2  ISLOPE=1
                        LENGTH=90 FT  SLOPE=0.050  K=0.7
*
COMPUTE NM HYD          ID=2  HYD NO=204  DA=0.00378 SQ MI
                        PER A=00 PER B=00 PER C=5 PER D=95
                        TP=0.0 hr  MASSRAIN=-1
*
PRINT HYD              ID=2  CODE=1
*
*
* Total Flow from Basin (OFF1 +202 + 204)
ADD HYD                ID=1  HYD NO=204SUM ID I=3  ID II=2
PRINT HYD              ID=1  CODE=1
*
*
*** Sub-BASIN 221 ****
*
COMPUTE LT TP          LCODE=1  UPLAND/LAG TIME METHOD
                        NK=2  ISLOPE=1
                        LENGTH=100 FT  SLOPE=0.045  K=0.7
                        LENGTH=200 FT  SLOPE=0.032  K=2.0
*
COMPUTE NM HYD          ID=2  HYD NO=221  DA=0.0006 SQ MI
                        PER A=00 PER B=00 PER C=10 PER D=90
                        TP=0.0 hr  MASSRAIN=-1
*
PRINT HYD              ID=2  CODE=1
*
*
*** Sub-BASIN 205 ****
*
COMPUTE LT TP          LCODE=1  UPLAND/LAG TIME METHOD
                        NK=2  ISLOPE=1
                        LENGTH=100 FT  SLOPE=0.025  K=0.7
                        LENGTH=239 FT  SLOPE=0.014  K=2.0
*
COMPUTE NM HYD          ID=5  HYD NO=205  DA=0.00197 SQ MI
                        PER A=00 PER B=00 PER C=05 PER D=95
                        TP=0.0 hr  MASSRAIN=-1
*
PRINT HYD              ID=5  CODE=1
*
*
* Total Flow from Basin (205 + 221)
ADD HYD                ID=4  HYD NO=205SUM ID I=2  ID II=5
PRINT HYD              ID=4  CODE=1
*
*
* Total Flow from Basin (OFF1 TO 205)
ADD HYD                ID=6  HYD NO=205SUMA ID I=1  ID II=4
PRINT HYD              ID=6  CODE=1
*
*
* Total Flow TO POND B
ADD HYD                ID=1  HYD NO=205SUMB ID I=10  ID II=6
PRINT HYD              ID=1  CODE=1
*

```

```

*
***Route HYD 205sum to Sub-Basin Through a Pipe

***Route Hyd through POND B
*
ROUTE RESERVOIR      ID=30  HYD NO=PONDB  INFLOW ID=1  CODE=1
OUTFLOW (CFS)        STORAGE (AC FT)      ELEV
0                    0.0                  4994
0.01                 0.0626                4995
0.02                 0.1469                4996
0.03                 0.2561                4997
44.36                0.3932                4998
72.44                0.5613                4999

*
*PRINT HYD           ID=30  CODE=1
*
*****
*** Sub-BASIN 206, Sheet Flow Out ***
*
COMPUTE LT TP        LCODE=1  UPLAND/LAG TIME METHOD
NK=2  ISLOPE=1
LENGTH=100 FT  SLOPE=0.020  K=0.7
LENGTH=187 FT  SLOPE=0.033  K=2.0

*
COMPUTE NM HYD        ID=1  HYD NO=206  DA=0.00223 SQ MI
PER A=00 PER B=00 PER C=05 PER D=95
TP=0.0 hr  MASSRAIN=-1

*
PRINT HYD            ID=1  CODE=1
*

*
****Route HYD to Sub-Basin Through a Pipe
*COMPUTE RATING CURVE  CID=1  VS NO=1 CODE=-1  SLP=0.023
DIA=24 IN  N=0.013

*
*ROUTE MCUNGE         ID=2  HYD NO=206Rt  INFLOW ID=1
*DT=0 HR  LENGTH=200 FT
*NS=0  SLOPE=0.010
*
*PRINT HYD            ID=2  CODE=1
*
*
*****
***Route Hyd through POND C - Underground
*
ROUTE RESERVOIR      ID=2  HYD NO=PONDC  INFLOW ID=1  CODE=1
OUTFLOW (CFS)        STORAGE (AC FT)      ELEV
0.0                  0.00                  4985.0
2.8                  0.10                  4986
5.3                  0.13                  4986.5

*
*PRINT HYD           ID=2  CODE=1

*
*****
*** Sub-BASIN 208 ***
*
COMPUTE LT TP        LCODE=1  UPLAND/LAG TIME METHOD
NK=2  ISLOPE=1
LENGTH=100 FT  SLOPE=0.025  K=0.7
LENGTH=485 FT  SLOPE=0.018  K=2.0

*
COMPUTE NM HYD        ID=8  HYD NO=208  DA=0.00138 SQ MI
PER A=00 PER B=00 PER C=05 PER D=95
TP=0.0 hr  MASSRAIN=-1

*
PRINT HYD            ID=8  CODE=1
*
*
*** Sub-BASIN 209 ***
*
COMPUTE LT TP        LCODE=1  UPLAND/LAG TIME METHOD
NK=2  ISLOPE=1
LENGTH=100 FT  SLOPE=0.018  K=0.7
LENGTH=410 FT  SLOPE=0.004  K=2.0

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COMPUTE NM HYD          ID=9  HYD NO=209  DA=0.00142 SQ MI
                          PER A=00 PER B=00 PER C=02 PER D=98
                          TP=0.0 hr  MASSRAIN=-1

*
PRINT HYD               ID=9  CODE=1
*
*
* Total Flow from Basin (208 + 209)
ADD HYD                 ID=11  HYD NO=209SUM ID I=9  ID II=8
PRINT HYD               ID=11  CODE=1
*
*** Sub-BASIN 222 ****
*
COMPUTE LT TP           LCODE=1  UPLAND/LAG TIME METHOD
                          NK=2  ISLOPE=1
                          LENGTH=89 FT  SLOPE=0.032  K=0.7

*
COMPUTE NM HYD          ID=12  HYD NO=222  DA=0.00147 SQ MI
                          PER A=00 PER B=00 PER C=2 PER D=98
                          TP=0.0 hr  MASSRAIN=-1

*
PRINT HYD               ID=12  CODE=1
*
*
* Total Flow from Basin (208 + 209 + 222)
ADD HYD                 ID=13  HYD NO=222SUM ID I=11  ID II=12
PRINT HYD               ID=13  CODE=1
*
*** Sub-BASIN 215 ****
*
COMPUTE LT TP           LCODE=1  UPLAND/LAG TIME METHOD
                          NK=2  ISLOPE=1
                          LENGTH=100 FT  SLOPE=0.029  K=0.7
                          LENGTH=206 FT  SLOPE=0.003  K=2.0

*
COMPUTE NM HYD          ID=14  HYD NO=215  DA=0.00036 SQ MI
                          PER A=00 PER B=00 PER C=10 PER D=90
                          TP=0.0 hr  MASSRAIN=-1

*
PRINT HYD               ID=14  CODE=1
*
*
* Total Flow from Basin (208 TO 215)
ADD HYD                 ID=15  HYD NO=215SUM ID I=14  ID II=13
PRINT HYD               ID=15  CODE=1
*

*** Sub-BASIN 216 ****
*
COMPUTE LT TP           LCODE=1  UPLAND/LAG TIME METHOD
                          NK=2  ISLOPE=1
                          LENGTH=100 FT  SLOPE=0.011  K=0.7
                          LENGTH=479 FT  SLOPE=0.023  K=2.0

*
COMPUTE NM HYD          ID=16  HYD NO=216  DA=0.00021 SQ MI
                          PER A=00 PER B=00 PER C=05 PER D=95
                          TP=0.0 hr  MASSRAIN=-1

*
PRINT HYD               ID=16  CODE=1
*
*
* Total Flow from Basin (208 TO 216)
ADD HYD                 ID=17  HYD NO=216SUM ID I=16  ID II=15
PRINT HYD               ID=17  CODE=1
*
*****
*** Sub-BASIN 213 ****
*
COMPUTE LT TP           LCODE=1  UPLAND/LAG TIME METHOD
                          NK=2  ISLOPE=1
                          LENGTH=100 FT  SLOPE=0.025  K=0.7
                          LENGTH=50 FT  SLOPE=0.060  K=2.0

*
COMPUTE NM HYD          ID=2  HYD NO=213  DA=0.00023 SQ MI
                          PER A=00 PER B=00 PER C=25 PER D=75
                          TP=0.0 hr  MASSRAIN=-1

*
PRINT HYD               ID=2  CODE=1
*
*** Sub-BASIN 214 ****
*
COMPUTE LT TP           LCODE=1  UPLAND/LAG TIME METHOD

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```

NK=2 ISLOPE=1
LENGTH=100 FT SLOPE=0.028 K=0.7
LENGTH=90 FT SLOPE=0.061 K=2.0
*
COMPUTE NM HYD ID=99 HYD NO=214 DA=0.00137 SQ MI
PER A=00 PER B=00 PER C=25 PER D=75
TP=0.0 hr MASSRAIN=-1
*
PRINT HYD ID=99 CODE=1
*
* Total Flow from Basin (214 + 213)
ADD HYD ID=3 HYD NO=214SUM ID I=99 ID II=2
PRINT HYD ID=3 CODE=1
*
*
*****
*
*****
*** Sub-BASIN 210 ****
*
COMPUTE LT TP LCODE=1 UPLAND/LAG TIME METHOD
NK=2 ISLOPE=1
LENGTH=300 FT SLOPE=0.005 K=0.7
*
COMPUTE NM HYD ID=1 HYD NO=210 DA=0.00146 SQ MI
PER A=00 PER B=00 PER C=02 PER D=98
TP=0.0 hr MASSRAIN=-1
*
PRINT HYD ID=1 CODE=1
*
* Total Flow from Basin (213 + 214 + 210)
ADD HYD ID=31 HYD NO=210SUM ID I=1 ID II=3
PRINT HYD ID=31 CODE=1
*
*
* Total Flow from Basin (208 TO 216 TO 210, 213 + 214)
ADD HYD ID=18 HYD NO=210SUMA ID I=17 ID II=31
PRINT HYD ID=18 CODE=1
*
*****
*** Sub-BASIN 207 ****
*
COMPUTE LT TP LCODE=1 UPLAND/LAG TIME METHOD
NK=2 ISLOPE=1
LENGTH=100 FT SLOPE=0.025 K=0.7
LENGTH=545 FT SLOPE=0.015 K=2.0
*
COMPUTE NM HYD ID=1 HYD NO=207 DA=0.00083 SQ MI
PER A=00 PER B=00 PER C=05 PER D=95
TP=0.0 hr MASSRAIN=-1
*
PRINT HYD ID=1 CODE=1
*
*
*** Sub-BASIN 211 ****
*
COMPUTE LT TP LCODE=1 UPLAND/LAG TIME METHOD
NK=2 ISLOPE=1
LENGTH=100 FT SLOPE=0.055 K=0.7
LENGTH=114 FT SLOPE=0.037 K=2.0
*
COMPUTE NM HYD ID=11 HYD NO=211 DA=0.00257 SQ MI
PER A=00 PER B=00 PER C=5 PER D=95
TP=0.0 hr MASSRAIN=-1
*
PRINT HYD ID=11 CODE=1
*
*
* Total Flow from Basin (211 + 207)
ADD HYD ID=10 HYD NO=211SUM ID I=1 ID II=11
PRINT HYD ID=10 CODE=1
*
*** Sub-BASIN 212 ****
*
COMPUTE LT TP LCODE=1 UPLAND/LAG TIME METHOD
NK=2 ISLOPE=1
LENGTH=100 FT SLOPE=0.005 K=0.7
LENGTH=50 FT SLOPE=0.260 K=2.0
*
COMPUTE NM HYD ID=3 HYD NO=212 DA=0.00204 SQ MI
PER A=00 PER B=00 PER C=5 PER D=95

```

```

TP=0.0 hr  MASSRAIN=-1
*
PRINT HYD          ID=3  CODE=1
*
*
* Total Flow from Basin (207+211+212)
ADD HYD            ID=11  HYD NO=212SUM ID I=10  ID II=3
PRINT HYD          ID=11  CODE=1
*

*** Sub-BASIN 218 ****
*
COMPUTE LT TP      LCODE=1  UPLAND/LAG TIME METHOD
                   NK=2  ISLOPE=1
                   LENGTH=100 FT  SLOPE=0.040  K=0.7
                   LENGTH=50 FT  SLOPE=0.040  K=2.0
*
COMPUTE NM HYD     ID=1  HYD NO=218  DA=0.00324 SQ MI
                   PER A=00 PER B=00 PER C=10 PER D=90
                   TP=0.0 hr  MASSRAIN=-1
*
PRINT HYD          ID=1  CODE=1
*
*
* Total Flow from Basins
ADD HYD            ID=10  HYD NO=218SUM ID I=18  ID II=1
PRINT HYD          ID=10  CODE=1
*

*** Sub-BASIN 219 ****
*
COMPUTE LT TP      LCODE=1  UPLAND/LAG TIME METHOD
                   NK=2  ISLOPE=1
                   LENGTH=100 FT  SLOPE=0.025  K=0.7
                   LENGTH=143 FT  SLOPE=0.019  K=2.0
*
COMPUTE NM HYD     ID=1  HYD NO=219  DA=0.00037 SQ MI
                   PER A=00 PER B=00 PER C=05 PER D=95
                   TP=0.0 hr  MASSRAIN=-1
*
PRINT HYD          ID=1  CODE=1
*
*
* Total Flow from Basins
ADD HYD            ID=19  HYD NO=219SUM ID I=10  ID II=1
PRINT HYD          ID=19  CODE=1
*
*
* Add Flows from West Basins
ADD HYD            ID=18  HYD NO=219SUMA ID I=19  ID II=11
PRINT HYD          ID=18  CODE=1
*
*** Sub-BASIN 220 ****
*
COMPUTE LT TP      LCODE=1  UPLAND/LAG TIME METHOD
                   NK=2  ISLOPE=1
                   LENGTH=100 FT  SLOPE=0.016  K=0.7
                   LENGTH=127 FT  SLOPE=0.032  K=2.0
*
COMPUTE NM HYD     ID=20  HYD NO=220  DA=0.00139 SQ MI
                   PER A=00 PER B=00 PER C=15 PER D=85
                   TP=0.0 hr  MASSRAIN=-1
*
PRINT HYD          ID=20  CODE=1
*
*
* Total Flows from All Basins
ADD HYD            ID=21  HYD NO=220SUM ID I=18  ID II=20
PRINT HYD          ID=21  CODE=1
*
*

* Add Outflow From Pond B
ADD HYD            ID=1  HYD NO=POND.IN ID I=21  ID II=30
PRINT HYD          ID=1  CODE=1
*

****Route Hyd through POND A- 27 inch orifice
*
ROUTE RESERVOIR    ID=96  HYD NO=PONDA  INFLOW ID=1  CODE=1
                   OUTFLOW (CFS)  STORAGE (AC FT)  ELEV

```

	0.0	0.00	4989
	0.01	0.1097	4990
	0.02	0.2491	4991
	11.1	0.4241	4992
	30.9	0.6403	4993
	38.0	0.8999	4994
	43.0	1.0112	4995
	47.1	1.5550	4996
	51.2	1.9531	4997

*
 *PRINT HYD ID=96 CODE=1
 *
 *
 *** Sub-BASIN 217, Sheet flow Out ***
 *
 COMPUTE LT TP LCODE=1 UPLAND/LAG TIME METHOD
 NK=2 ISLOPE=1
 LENGTH=100 FT SLOPE=0.005 K=0.7
 LENGTH=230 FT SLOPE=0.004 K=2.0
 *
 COMPUTE NM HYD ID=6 HYD NO=217 DA=0.00046 SQ MI
 PER A=00 PER B=00 PER C=20 PER D=80
 TP=0.0 hr MASSRAIN=-1
 *
 PRINT HYD ID=6 CODE=1
 *
 *
 *
 FINISH

APPENDIX B

FlowMaster Calculations –B-1 to B-38

- Parking Capacity
- Inlet Capacity

Project Description

Input Data

Elevation (ft)

Roughness Segment Definitions

0.017

Options

Current Roughness weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results

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Worksheet for Irregular Section - Basin 201&202 Combined

Results

Critical Slope	0.00750	ft/ft
Velocity	2.32	ft/s
Velocity Head	0.08	ft
Specific Energy	0.37	ft
Froude Number	1.03	
Flow Type	Supercritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.28	ft
Critical Depth	0.29	ft
Channel Slope	0.00800	ft/ft
Critical Slope	0.00750	ft/ft

Worksheet for Irregular Section - Basin 203

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.04500	ft/ft
Discharge	13.41	ft ³ /s
Section Definitions		

Station (ft)	Elevation (ft)
0+00	5002.50
0+00	5002.00
0+66	5005.00

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 5002.50)	(0+00, 5002.00)	0.013
(0+00, 5002.00)	(0+66, 5005.00)	0.016

Options

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results

Normal Depth	0.42	ft
Elevation Range	5002.00 to 5005.00 ft	
Flow Area	1.96	ft ²
Wetted Perimeter	9.73	ft
Hydraulic Radius	0.20	ft
Top Width	9.29	ft
Normal Depth	0.42	ft
Critical Depth	0.62	ft
Critical Slope	0.00577	ft/ft

Worksheet for Irregular Section - Basin 203

Results

Velocity	6.83	ft/s
Velocity Head	0.73	ft
Specific Energy	1.15	ft
Froude Number	2.62	
Flow Type	Supercritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.42	ft
Critical Depth	0.62	ft
Channel Slope	0.04500	ft/ft
Critical Slope	0.00577	ft/ft

Worksheet for Irregular Section - Basin 204

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.04000	ft/ft
Discharge	22.93	ft ³ /s
Section Definitions		

Station (ft)	Elevation (ft)
0+00	5009.00
0+63	5001.50
0+63	5002.17
0+64	5002.17

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 5009.00)	(0+63, 5002.17)	0.016
(0+63, 5002.17)	(0+64, 5002.17)	0.013

Options

Current Roughness weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results

Normal Depth	0.77	ft
Elevation Range	5001.50 to 5009.00 ft	
Flow Area	2.61	ft ²
Wetted Perimeter	8.33	ft
Hydraulic Radius	0.31	ft
Top Width	7.52	ft
Normal Depth	0.77	ft
Critical Depth	1.10	ft

Worksheet for Irregular Section - Basin 204

Results

Critical Slope	0.00506	ft/ft
Velocity	8.77	ft/s
Velocity Head	1.20	ft
Specific Energy	1.97	ft
Froude Number	2.62	
Flow Type	Supercritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.77	ft
Critical Depth	1.10	ft
Channel Slope	0.04000	ft/ft
Critical Slope	0.00506	ft/ft

Worksheet for Irregular Section - Basin 205

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.02130	ft/ft
Discharge	6.92	ft ³ /s
Section Definitions		

Station (ft)	Elevation (ft)
0+00	0.50
0+00	0.00
0+32	0.00
0+32	0.50

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 0.50)	(0+32, 0.50)	0.017

Options

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results

Normal Depth	0.09	ft
Elevation Range	0.00 to 0.50 ft	
Flow Area	2.74	ft ²
Wetted Perimeter	31.87	ft
Hydraulic Radius	0.09	ft
Top Width	31.70	ft
Normal Depth	0.09	ft
Critical Depth	0.11	ft
Critical Slope	0.00846	ft/ft

Worksheet for Irregular Section - Basin 205

Results

Velocity	2.53	ft/s
Velocity Head	0.10	ft
Specific Energy	0.19	ft
Froude Number	1.52	
Flow Type	Supercritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.09	ft
Critical Depth	0.11	ft
Channel Slope	0.02130	ft/ft
Critical Slope	0.00846	ft/ft

Worksheet for Irregular Section - Basin 206

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.04440	ft/ft
Discharge	6.00	ft ³ /s
Section Definitions		

Station (ft)	Elevation (ft)
0+00	4991.50
0+00	4991.00
0+94	4995.00

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 4991.50)	(0+00, 4991.00)	0.013
(0+00, 4991.00)	(0+94, 4995.00)	0.016

Options

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results

Normal Depth	0.31	ft
Elevation Range	4991.00 to 4995.00 ft	
Flow Area	1.09	ft ²
Wetted Perimeter	7.49	ft
Hydraulic Radius	0.15	ft
Top Width	7.17	ft
Normal Depth	0.31	ft
Critical Depth	0.44	ft
Critical Slope	0.00646	ft/ft

Worksheet for Irregular Section - Basin 206

Results

Velocity	5.48	ft/s
Velocity Head	0.47	ft
Specific Energy	0.77	ft
Froude Number	2.47	
Flow Type	Supercritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.31	ft
Critical Depth	0.44	ft
Channel Slope	0.04440	ft/ft
Critical Slope	0.00646	ft/ft

Worksheet for Irregular Section - Basin 211 & 212

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.01000	ft/ft
Discharge	6.93	ft ³ /s
Section Definitions		

Station (ft)	Elevation (ft)
0+00	5000.00
0+00	4999.50
0+89	5001.00

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 5000.00)	(0+00, 4999.50)	0.013
(0+00, 4999.50)	(0+89, 5001.00)	0.016

Options

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results

Normal Depth	0.30	ft
Elevation Range	4999.50 to 5001.00 ft	
Flow Area	2.66	ft ²
Wetted Perimeter	18.08	ft
Hydraulic Radius	0.15	ft
Top Width	17.78	ft
Normal Depth	0.30	ft
Critical Depth	0.32	ft
Critical Slope	0.00698	ft/ft

Worksheet for Irregular Section - Basin 211 & 212

Results

Velocity	2.60	ft/s
Velocity Head	0.11	ft
Specific Energy	0.40	ft
Froude Number	1.19	
Flow Type	Supercritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.30	ft
Critical Depth	0.32	ft
Channel Slope	0.01000	ft/ft
Critical Slope	0.00698	ft/ft

Worksheet for Irregular Section - Basin 218

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.02860	ft/ft
Discharge	14.00	ft ³ /s
Section Definitions		

Station (ft)	Elevation (ft)
0+00	5001.17
0+00	5000.67
0+50	5002.00

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 5001.17)	(0+00, 5000.67)	0.013
(0+00, 5000.67)	(0+50, 5002.00)	0.016

Options

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results

Normal Depth	0.38	ft
Elevation Range	5000.67 to 5002.00 ft	
Flow Area	2.73	ft ²
Wetted Perimeter	14.71	ft
Hydraulic Radius	0.19	ft
Top Width	14.32	ft
Normal Depth	0.38	ft
Critical Depth	0.51	ft
Critical Slope	0.00604	ft/ft

Worksheet for Irregular Section - Basin 218

Results

Velocity	5.13	ft/s
Velocity Head	0.41	ft
Specific Energy	0.79	ft
Froude Number	2.07	
Flow Type	Supercritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.38	ft
Critical Depth	0.51	ft
Channel Slope	0.02860	ft/ft
Critical Slope	0.00604	ft/ft

Worksheet for Rankin Road

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Channel Slope 0.04800 ft/ft
Discharge 64.00 ft³/s
Section Definitions

Station (ft)	Elevation (ft)
0+00	0.67
0+01	0.67
0+01	0.00
0+03	0.13
0+15	0.36
0+27	0.13
0+29	0.00
0+29	0.67
0+29	0.67

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 0.67)	(0+03, 0.13)	0.013
(0+03, 0.13)	(0+27, 0.13)	0.016
(0+27, 0.13)	(0+29, 0.67)	0.013

Options

Current Roughness Weighted Method Pavlovskii's Method
Open Channel Weighting Method Pavlovskii's Method
Closed Channel Weighting Method Pavlovskii's Method

Results

Normal Depth 0.48 ft
Elevation Range 0.00 to 0.67 ft
Flow Area 7.50 ft²
Wetted Perimeter 28.98 ft
Hydraulic Radius 0.26 ft
Top Width 28.00 ft

Worksheet for Rankin Road

Results

Normal Depth	0.48	ft
Critical Depth	0.77	ft
Critical Slope	0.00465	ft/ft
Velocity	8.53	ft/s
Velocity Head	1.13	ft
Specific Energy	1.62	ft
Froude Number	2.90	
Flow Type	Supercritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.48	ft
Critical Depth	0.77	ft
Channel Slope	0.04800	ft/ft
Critical Slope	0.00465	ft/ft

Worksheet for Basin 201-Dbl D_Sag

Project Description

Solve For Spread

Input Data

Discharge	9.10	ft ³ /s
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.03	ft/ft
Grate Width	2.08	ft
Grate Length	6.66	ft
Local Depression	1.00	in
Local Depression Width	2.37	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%

Results

Spread	16.97	ft
Depth	0.58	ft
Gutter Depression	0.08	ft
Total Depression	0.16	ft
Open Grate Area	6.23	ft ²
Active Grate Weir Length	8.74	ft

Worksheet for Basin 202-Dbl D_Sag

Project Description

Solve For Spread

Input Data

Discharge	12.70	ft ³ /s
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.03	ft/ft
Grate Width	2.08	ft
Grate Length	6.66	ft
Local Depression	1.00	in
Local Depression Width	2.37	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%

Results

Spread	21.07	ft
Depth	0.71	ft
Gutter Depression	0.08	ft
Total Depression	0.16	ft
Open Grate Area	6.23	ft ²
Active Grate Weir Length	8.74	ft

Worksheet for Basin 203-Sgl C_Sag

Project Description

Solve For Spread

Input Data

Discharge	5.20	ft ³ /s
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.04	ft/ft
Local Depression	2.25	in
Local Depression Width	3.95	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	3.95	ft
Opening Height	0.50	ft
Curb Throat Type	Horizontal	
Throat Incline Angle	90.00	degrees

Options

Calculation Option Use Both

Results

Spread	7.08	ft
Depth	0.31	ft
Gutter Depression	0.06	ft
Total Depression	0.25	ft
Open Grate Area	3.12	ft ²
Active Grate Weir Length	5.41	ft

Worksheet for Basin 204-1 Sgl C

Project Description

Solve For Efficiency

Input Data

Discharge	22.93	ft ³ /s
Slope	0.04000	ft/ft
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.01	ft/ft
Roughness Coefficient	0.013	
Local Depression	2.25	in
Local Depression Width	3.95	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	3.95	ft

Options

Calculation Option	Use Both
Grate Flow Option	Exclude None

Results

Efficiency	29.40	%
Intercepted Flow	6.74	ft ³ /s
Bypass Flow	16.19	ft ³ /s
Spread	30.76	ft
Depth	0.35	ft
Flow Area	3.48	ft ²
Gutter Depression	0.13	ft
Total Depression	0.32	ft
Velocity	6.59	ft/s
Splash Over Velocity	7.39	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.01	
Grate Flow Ratio	0.25	
Equivalent Cross Slope	0.03051	ft/ft
Active Grate Length	1.67	ft
Length Factor	0.02	
Total Interception Length	93.57	ft

Project Description

Input Data

Options

Results

Spread	9.18	ft
Depth	0.48	ft
Gutter Depression	0.03	ft
Total Depression	0.21	ft
Open Grate Area	6.23	ft ²
Active Grate Weir Length	8.74	ft

Worksheet for Basin 204-1 Sgl C

Messages

Messages Grate Length should be within the
defined range of HEC-22's Chart 5
(approx. 0.5-4.5 ft / 0.15-1.35 m).

Notes

Each Side

Worksheet for Basin 206-Sgl C_Sag

Project Description

Solve For Spread

Input Data

Discharge	6.40	ft ³ /s
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.05	ft/ft
Local Depression	2.25	in
Local Depression Width	3.95	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	3.95	ft
Opening Height	0.50	ft
Curb Throat Type	Horizontal	
Throat Incline Angle	90.00	degrees

Options

Calculation Option Use Both

Results

Spread	6.94	ft
Depth	0.36	ft
Gutter Depression	0.04	ft
Total Depression	0.23	ft
Open Grate Area	3.12	ft ²
Active Grate Weir Length	5.41	ft

Worksheet for Basin 207-1-Dbl C

Project Description

Solve For Efficiency

Input Data

Discharge	5.52	ft ³ /s
Slope	0.00300	ft/ft
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.01	ft/ft
Roughness Coefficient	0.013	
Local Depression	2.25	in
Local Depression Width	7.40	ft
Grate Width	2.08	ft
Grate Length	6.66	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	7.40	ft

Options

Calculation Option	Use Both
Grate Flow Option	Exclude None

Results

Efficiency	65.13	%
Intercepted Flow	3.60	ft ³ /s
Bypass Flow	1.92	ft ³ /s
Spread	23.26	ft
Depth	0.36	ft
Flow Area	2.87	ft ²
Gutter Depression	0.13	ft
Total Depression	0.32	ft
Velocity	1.92	ft/s
Splash Over Velocity	10.50	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.25	
Grate Flow Ratio	0.31	
Equivalent Cross Slope	0.02536	ft/ft
Active Grate Length	3.33	ft
Length Factor	0.15	
Total Interception Length	26.43	ft

Messages

Messages

Grate Length should be within the defined range of HEC-22's Chart 5 (approx. 0.5-4.5 ft / 0.15-1.35 m).

Worksheet for Basin 207-2-Sgl C

Project Description

Solve For Efficiency

Input Data

Discharge	4.42	ft ³ /s
Slope	0.00300	ft/ft
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.01	ft/ft
Roughness Coefficient	0.013	
Local Depression	2.25	in
Local Depression Width	3.95	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	3.95	ft

Options

Calculation Option	Use Both
Grate Flow Option	Exclude None

Results

Efficiency	55.45	%
Intercepted Flow	2.45	ft ³ /s
Bypass Flow	1.97	ft ³ /s
Spread	21.19	ft
Depth	0.34	ft
Flow Area	2.41	ft ²
Gutter Depression	0.13	ft
Total Depression	0.32	ft
Velocity	1.84	ft/s
Splash Over Velocity	7.39	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.07	
Grate Flow Ratio	0.34	
Equivalent Cross Slope	0.04176	ft/ft
Active Grate Length	1.67	ft
Length Factor	0.13	
Total Interception Length	17.85	ft

Messages

Notes

Bypass to Basin 2017

Worksheet for Basin 208-Sgl C

Project Description

Solve For Efficiency

Input Data

Discharge	4.20	ft ³ /s
Slope	0.02800	ft/ft
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.01	ft/ft
Roughness Coefficient	0.013	
Local Depression	2.25	in
Local Depression Width	3.95	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	3.95	ft

Options

Calculation Option	Use Both
Grate Flow Option	Exclude None

Results

Efficiency	68.52	%
Intercepted Flow	2.88	ft ³ /s
Bypass Flow	1.32	ft ³ /s
Spread	12.29	ft
Depth	0.25	ft
Flow Area	0.92	ft ²
Gutter Depression	0.13	ft
Total Depression	0.32	ft
Velocity	4.57	ft/s
Splash Over Velocity	7.39	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.01	
Grate Flow Ratio	0.58	
Equivalent Cross Slope	0.06264	ft/ft
Active Grate Length	1.67	ft
Length Factor	0.09	
Total Interception Length	26.77	ft

Messages

Notes

Each Side

Worksheet for Basin 209-Sgl C_Sag

Project Description

Solve For Spread

Input Data

Discharge	5.77	ft ³ /s
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.05	ft/ft
Local Depression	2.25	in
Local Depression Width	3.95	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	3.95	ft
Opening Height	0.50	ft
Curb Throat Type	Horizontal	
Throat Incline Angle	90.00	degrees

Options

Calculation Option Use Both

Results

Spread	6.43	ft
Depth	0.33	ft
Gutter Depression	0.04	ft
Total Depression	0.23	ft
Open Grate Area	3.12	ft ²
Active Grate Weir Length	5.41	ft

Worksheet for Basin 210-Sgl C

Project Description

Solve For Efficiency

Input Data

Discharge	1.48	ft ³ /s
Slope	0.02100	ft/ft
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.01	ft/ft
Roughness Coefficient	0.013	
Local Depression	2.25	in
Local Depression Width	3.95	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	3.95	ft

Options

Calculation Option	Use Both
Grate Flow Option	Exclude None

Results

Efficiency	93.83	%
Intercepted Flow	1.39	ft ³ /s
Bypass Flow	0.09	ft ³ /s
Spread	6.87	ft
Depth	0.20	ft
Flow Area	0.40	ft ²
Gutter Depression	0.13	ft
Total Depression	0.32	ft
Velocity	3.70	ft/s
Splash Over Velocity	7.39	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.02	
Grate Flow Ratio	0.83	
Equivalent Cross Slope	0.08270	ft/ft
Active Grate Length	1.67	ft
Length Factor	0.17	
Total Interception Length	13.41	ft

Messages

Notes

Each Side

Worksheet for Basin 211-Dbl C_Sag

Project Description

Solve For Spread

Input Data

Discharge	7.70	ft ³ /s
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.02	ft/ft
Local Depression	2.25	in
Local Depression Width	7.40	ft
Grate Width	2.08	ft
Grate Length	6.66	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	7.40	ft
Opening Height	0.50	ft
Curb Throat Type	Horizontal	
Throat Incline Angle	90.00	degrees

Options

Calculation Option Use Both

Results

Spread	5.65	ft
Depth	0.29	ft
Gutter Depression	0.10	ft
Total Depression	0.29	ft
Open Grate Area	6.23	ft ²
Active Grate Weir Length	8.74	ft

Worksheet for Basin 212-Dbl C_Sag

Project Description

Solve For Spread

Input Data

Discharge	6.10	ft ³ /s
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.02	ft/ft
Local Depression	2.25	in
Local Depression Width	7.40	ft
Grate Width	2.08	ft
Grate Length	6.66	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	7.40	ft
Opening Height	0.50	ft
Curb Throat Type	Horizontal	
Throat Incline Angle	90.00	degrees

Options

Calculation Option Use Both

Results

Spread	5.12	ft
Depth	0.25	ft
Gutter Depression	0.10	ft
Total Depression	0.29	ft
Open Grate Area	6.23	ft ²
Active Grate Weir Length	8.74	ft

Worksheet for Basin 214-Sgl D_Sag

Project Description

Solve For Spread

Input Data

Discharge	4.54	ft ³ /s
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.04	ft/ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Local Depression	1.00	in
Local Depression Width	2.37	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%

Results

Spread	11.32	ft
Depth	0.50	ft
Gutter Depression	0.05	ft
Total Depression	0.13	ft
Open Grate Area	3.12	ft ²
Active Grate Weir Length	5.41	ft

Worksheet for Basins 215-Sgl C

Project Description

Solve For Efficiency

Input Data

Discharge	1.24	ft ³ /s
Slope	0.01500	ft/ft
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.01	ft/ft
Roughness Coefficient	0.013	
Local Depression	2.25	in
Local Depression Width	3.95	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	3.95	ft

Options

Calculation Option	Use Both
Grate Flow Option	Exclude None

Results

Efficiency	95.33	%
Intercepted Flow	1.18	ft ³ /s
Bypass Flow	0.06	ft ³ /s
Spread	6.82	ft
Depth	0.20	ft
Flow Area	0.40	ft ²
Gutter Depression	0.13	ft
Total Depression	0.32	ft
Velocity	3.13	ft/s
Splash Over Velocity	7.39	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.03	
Grate Flow Ratio	0.83	
Equivalent Cross Slope	0.08287	ft/ft
Active Grate Length	1.67	ft
Length Factor	0.20	
Total Interception Length	11.24	ft

Messages

Messages Grate Length should be within the defined range of HEC-22's Chart 5 (approx. 0.5-4.5 ft / 0.15-1.35 m).

Worksheet for Basin 218-Dbl C

Project Description

Solve For Efficiency

Input Data

Discharge	14.05	ft ³ /s
Slope	0.03000	ft/ft
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.01	ft/ft
Roughness Coefficient	0.013	
Local Depression	2.25	in
Local Depression Width	7.40	ft
Grate Width	2.08	ft
Grate Length	6.66	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	7.40	ft

Options

Calculation Option	Use Both
Grate Flow Option	Exclude None

Results

Efficiency	44.56	%
Intercepted Flow	6.26	ft ³ /s
Bypass Flow	7.79	ft ³ /s
Spread	21.23	ft
Depth	0.34	ft
Flow Area	2.42	ft ²
Gutter Depression	0.13	ft
Total Depression	0.32	ft
Velocity	5.81	ft/s
Splash Over Velocity	10.50	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.04	
Grate Flow Ratio	0.34	
Equivalent Cross Slope	0.02691	ft/ft
Active Grate Length	3.33	ft
Length Factor	0.05	
Total Interception Length	75.33	ft

Messages

Messages Grate Length should be within the defined range of HEC-22's Chart 5 (approx. 0.5-4.5 ft / 0.15-1.35 m).

Notes

Each Side

Worksheet for Basins 219-1-DbI C

Project Description

Solve For Efficiency

Input Data

Discharge	8.91	ft ³ /s
Slope	0.01500	ft/ft
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.01	ft/ft
Roughness Coefficient	0.013	
Local Depression	2.25	in
Local Depression Width	7.40	ft
Grate Width	2.08	ft
Grate Length	6.66	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	7.40	ft

Options

Calculation Option	Use Both
Grate Flow Option	Exclude None

Results

Efficiency	51.85	%
Intercepted Flow	4.62	ft ³ /s
Bypass Flow	4.29	ft ³ /s
Spread	20.27	ft
Depth	0.33	ft
Flow Area	2.22	ft ²
Gutter Depression	0.13	ft
Total Depression	0.32	ft
Velocity	4.02	ft/s
Splash Over Velocity	10.50	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.08	
Grate Flow Ratio	0.36	
Equivalent Cross Slope	0.02775	ft/ft
Active Grate Length	3.33	ft
Length Factor	0.08	
Total Interception Length	49.62	ft

Messages

Messages Grate Length should be within the defined range of HEC-22's Chart 5 (approx. 0.5-4.5 ft / 0.15-1.35 m).

Worksheet for Basin 219-2-Sgl C

Project Description

Solve For Efficiency

Input Data

Discharge	4.29	ft ³ /s
Slope	0.01500	ft/ft
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.01	ft/ft
Roughness Coefficient	0.013	
Local Depression	2.25	in
Local Depression Width	3.95	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	3.95	ft

Options

Calculation Option	Use Both
Grate Flow Option	Exclude None

Results

Efficiency	62.88	%
Intercepted Flow	2.70	ft ³ /s
Bypass Flow	1.59	ft ³ /s
Spread	14.55	ft
Depth	0.28	ft
Flow Area	1.22	ft ²
Gutter Depression	0.13	ft
Total Depression	0.32	ft
Velocity	3.51	ft/s
Splash Over Velocity	7.39	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.02	
Grate Flow Ratio	0.50	
Equivalent Cross Slope	0.05576	ft/ft
Active Grate Length	1.67	ft
Length Factor	0.10	
Total Interception Length	24.01	ft

Messages

Notes

Each Side

Worksheet for Grate Inlet On Grade - Rankin

Project Description

Solve For Efficiency

Input Data

Discharge	64.00	ft ³ /s
Slope	0.04800	ft/ft
Gutter Width	0.00	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%

Options

Grate Flow Option Exclude None

Results

Efficiency	14.24	%
Intercepted Flow	9.11	ft ³ /s
Bypass Flow	54.89	ft ³ /s
Spread	23.64	ft
Depth	0.47	ft
Flow Area	5.59	ft ²
Gutter Depression	0.00	ft
Total Depression	0.00	ft
Velocity	11.45	ft/s
Splash Over Velocity	7.39	ft/s
Frontal Flow Factor	0.63	
Side Flow Factor	0.01	
Grate Flow Ratio	0.22	
Active Grate Length	1.67	ft

Worksheet for Ditch Inlet On Grade - 1

Project Description

Solve For Efficiency

Input Data

Roughness Coefficient	0.013	
Slope	0.01500	ft/ft
Left Side Slope	0.10	ft/ft (H:V)
Right Side Slope	0.10	ft/ft (H:V)
Bottom Width	24.00	ft
Discharge	64.00	ft ³ /s
Grate Width	24.00	ft
Grate Length	2.00	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%

Options

Grate Flow Option Exclude None

Results

Efficiency	86.76	%
Intercepted Flow	55.53	ft ³ /s
Bypass Flow	8.47	ft ³ /s
Flow Area	8.98	ft ²
Wetted Perimeter	24.75	ft
Top Width	24.07	ft
Velocity	7.12	ft/s
Splash Over Velocity	5.66	ft/s
Frontal Flow Factor	0.87	
Side Flow Factor	0.66	
Grate Flow Ratio	1.00	
Active Grate Length	1.00	ft
Critical Depth	0.60	ft
Critical Slope	0.00309	ft/ft
Froude Number	2.06	
Flow Type	Supercritical	
Specific Energy	1.16	ft
Velocity Head	0.79	ft
Depth	0.37	ft

Messages

Messages Grate Length should be within the defined range of HEC-22's Chart 5 (approx. 0.5-4.5 ft / 0.15-1.35 m).

Inlet Calculations

Basin ID	Flows (cfs)			Inlet Type	Notes
	Total	Intercepted	Bypass		
Offsite 1	4.94	0	4.94	-	Sheet flow to basin 201
Offsite 2	5.9	0	5.90	-	Sheet flow to basin 202
201	10.12	10.12	0.00	Double D	Sump inlet
202	14.20	14.20	0.00	Double D	Sump inlet
203	5.20	5.20	0.00	Single C	Sump inlet
204-1	22.93	6.74	16.19	Single C	Inlet at grade
204-2	16.19	16.19	0.00	Double C	Sump inlet
205	9.02	6.00	3.02	Single C	Inlets at grade, each side, 205 and 221
206	6.40	6.40	0.00	Single C	Sump inlet
207-1	5.52	3.60	1.92	Double C	bypass to second inlet
207-2	4.42	2.45	1.97	Single C	to Edith
208	4.20	2.88	1.32	Single C	bypass to basin 205
209	5.77	5.77	0.00	Single C	Sump inlet, 209 and third of 210 runoff
210	1.47	1.39	0.08	Single C	third of runoff , rest to basin 215
211	7.70	7.70	0.00	Double C	Sump inlet
212	6.10	6.10	0.00	Double C	Sump inlet
213	0.66	0.00	0.66	-	to Basin 214
214	4.54	4.54	0.00	Single C	Sump inlet
215	1.24	1.18	0.06	Single C	bypass of 210 and Basins 215, 216
216	0.60	0.00	0.60	-	to Basin 215 and Edith
217	1.33	0.00	1.33	-	to Edith
218	14.05	6.26	7.79	Single C	Basins 219
219-1	8.91	4.62	4.29	Double C	bypass of 218 and Basin 219
219-2	4.29	2.70	1.59	Single C	bypass to Edith
220	4.10	4.10	0.00	-	Pond
221	1.78	0.00	1.78	-	to Basin 205
222	4.45	0.00	4.45	-	sheet flow to Basin 218
Rankin Rd	64.00	9.11	54.89	Single D	sheet flow to Cattle Guard Inlet

APPENDIX C

CulvertMaster CalculationsC-1 to C-6

- Pond A Outfall Pipe
- Pond B Outfall Pipe
- Pond C Outfall Pipe

Culvert Calculator Report

Pond A Outlet

Comments: Maximum Allowable Discharge = 47.6 cfs

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	4,997.00 ft	Headwater Depth/Height	3.56
Computed Headwater Elev.	4,997.00 ft	Discharge	51.20 cfs
Inlet Control HW Elev.	4,997.00 ft	Tailwater Elevation	4,989.19 ft
Outlet Control HW Elev.	4,995.11 ft	Control Type	Inlet Control

Grades			
Upstream Invert	4,989.00 ft	Downstream Invert	4,984.42 ft
Length	48.60 ft	Constructed Slope	0.094239 ft/ft

Hydraulic Profile			
Profile CompositePressureProfileS1S2		Depth, Downstream	1.40 ft
Slope Type	N/A	Normal Depth	1.18 ft
Flow Regime	N/A	Critical Depth	2.18 ft
Velocity Downstream	19.73 ft/s	Critical Slope	0.024098 ft/ft

Section			
Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	2.25 ft
Section Size	27 inch	Rise	2.25 ft
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	4,995.11 ft	Upstream Velocity Head	2.62 ft
Ke	0.50	Entrance Loss	1.31 ft

Inlet Control Properties			
Inlet Control HW Elev.	4,997.00 ft	Flow Control	Submerged
Inlet Type	Square edge w/headwall	Area Full	4.0 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

C-1

Rating Table Report

Pond A Outlet

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	4,989.00	4,997.00	1.00 ft

HW Elev. (ft)	Discharge (cfs)
4,989.00	0.00
4,990.00	3.69
4,991.00	12.84
4,992.00	24.17
4,993.00	32.13
4,994.00	37.81
4,995.00	42.74
4,996.00	47.16
4,997.00	51.20

C-2

Culvert Calculator Report POND B Outlet

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	4,999.00 ft	Headwater Depth/Height	1.50
Computed Headwater Elev.	4,999.00 ft	Discharge	72.89 cfs
Inlet Control HW Elev.	4,998.37 ft	Tailwater Elevation	4,997.38 ft
Outlet Control HW Elev.	4,999.00 ft	Control Type	Outlet Control
Grades			
Upstream Invert	4,993.75 ft	Downstream Invert	4,993.54 ft
Length	53.70 ft	Constructed Slope	0.003911 ft/ft
Hydraulic Profile			
Profile	Pressure Profile	Depth, Downstream	3.84 ft
Slope Type	N/A	Normal Depth	N/A ft
Flow Regime	N/A	Critical Depth	2.67 ft
Velocity Downstream	7.58 ft/s	Critical Slope	0.006051 ft/ft
Section			
Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.50 ft
Section Size	42 inch	Rise	3.50 ft
Number Sections	1		
Outlet Control Properties			
Outlet Control HW Elev.	4,999.00 ft	Upstream Velocity Head	0.89 ft
Ke	0.50	Entrance Loss	0.45 ft
Inlet Control Properties			
Inlet Control HW Elev.	4,998.37 ft	Flow Control	Submerged
Inlet Type	Square edge w/headwall	Area Full	9.6 ft²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

C-3

Rating Table Report

POND B Outlet

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	4,994.00	4,999.00	1.00 ft

HW Elev. (ft)	Discharge (cfs)
4,994.00	0.00
4,995.00	0.00
4,996.00	0.00
4,997.00	0.00
4,998.00	45.09
4,999.00	72.89

C-4

Culvert Calculator Report

POND C Outlet

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	4,986.44 ft	Headwater Depth/Height	0.96
Computed Headwater Elev.	4,986.44 ft	Discharge	5.30 cfs
Inlet Control HW Elev.	4,986.29 ft	Tailwater Elevation	4,984.70 ft
Outlet Control HW Elev.	4,986.44 ft	Control Type	Entrance Control
Grades			
Upstream Invert	4,985.00 ft	Downstream Invert	4,982.52 ft
Length	35.40 ft	Constructed Slope	0.070056 ft/ft
Hydraulic Profile			
Profile	CompositePressureProfileS1S2	Depth, Downstream	2.18 ft
Slope Type	N/A	Normal Depth	0.44 ft
Flow Regime	N/A	Critical Depth	0.89 ft
Velocity Downstream	3.00 ft/s	Critical Slope	0.005902 ft/ft
Section			
Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	1.50 ft
Section Size	18 inch	Rise	1.50 ft
Number Sections	1		
Outlet Control Properties			
Outlet Control HW Elev.	4,986.44 ft	Upstream Velocity Head	0.37 ft
Ke	0.50	Entrance Loss	0.18 ft
Inlet Control Properties			
Inlet Control HW Elev.	4,986.29 ft	Flow Control	N/A
Inlet Type	Square edge w/headwall	Area Full	1.8 ft²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

C-5

Rating Table Report

POND C Outlet

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	4,985.00	4,986.50	0.50 ft

HW Elev. (ft)	Discharge (cfs)
4,985.00	0.00
4,985.50	0.78
4,986.00	2.82
4,986.50	5.66

C-6

APPENDIX D

StormCAD CalculationsD-1 to D-18

- Conduit Table
- Manhole Table
- Catch Basin Table
- Storm Drain Profiles

SWMD STORMCAD CONDUIT TABLE

Label	Start Node	Stop Node	Length (User Defined) (ft)	Slope (Calculated) (ft/ft)	Section Type	Diameter (in)	Rise (ft)	Span (ft)	Flow (cfs)	Capacity (Full Flow) (cfs)	Velocity (ft/s)	Invert (Start) (ft)	Invert (Stop) (ft)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
P-1	CB 01	CB 104	60	0.01	Circle	18			2.5	10.5	4.88	4,985.01	4,984.41	4,990.80	4,986.99	4,985.83	4,985.45	4,985.61	4,985.39
P-2	CB 104	MH 02	14.2	0.02	Circle	18			13.67	14.75	7.74	4,982.40	4,982.12	4,986.99	4,986.63	4,985.07	4,984.83	4,984.14	4,983.90
P-3	CB-04	MH-05	83.3	0.005	Circle	24			10.12	16.07	3.22	5,004.50	5,004.08	5,007.78	5,008.78	5,007.12	5,006.96	5,006.96	5,006.79
P-4	CB-21	MH-2	48.6	0.094	Circle	30			44.8	125.91	23.48	4,989.00	4,984.42	4,997.00	4,998.85	4,992.69	4,990.59	4,991.22	4,989.30
P-4.1	MH-05	MH-65	170.3	0.007	Circle	24			10.12	18.91	3.22	5,004.08	5,002.89	5,008.78	5,008.77	5,006.77	5,006.43	5,006.61	5,006.27
P-5	MH-65	MH-06	222.8	0.005	Circle	30			24.32	28.95	4.95	5,002.89	5,001.78	5,008.77	5,008.77	5,006.16	5,005.38	5,005.78	5,005.00
P-6	MH-06	MH-63	149.4	0.01	Circle	30			24.32	40.96	8.7	5,001.78	5,000.29	5,008.77	5,007.39	5,004.21	5,003.38	5,003.46	5,003.00
P-7	CB-10	MH-11	212.9	0.006	Circle	24			5.2	17.47	1.66	4,997.02	4,995.75	5,002.10	5,001.89	4,999.36	4,999.25	4,999.32	4,999.21
P-8	CB-24	O-7	12.5	0.025	Circle	18			6.02	16.57	3.41	4,985.44	4,985.13	4,990.80	4,991.00	4,987.72	4,987.68	4,987.54	4,987.50
P-8.1	MH-11	CB-102	233.1	0.006	Circle	24			5.2	17.53	1.66	4,995.75	4,994.35	5,001.89	5,001.49	4,999.22	4,999.10	4,999.18	4,999.05
P-9	MH-2	O-6	80.9	0.05	Circle	30			44.8	91.88	9.13	4,984.42	4,980.36	4,998.85	4,998.90	4,989.18	4,988.21	4,987.89	4,986.92
P-10	CB-102	CB-87	20	0.006	Circle	24			10.9	17.52	3.47	4,994.35	4,994.23	5,001.49	5,001.42	4,999.02	4,998.97	4,998.83	4,998.79
P-15	MH-30	MH-20	300.7	0.004	Circle	42			41.1	63.81	4.27	4,993.29	4,992.08	4,999.92	4,999.15	4,997.36	4,996.86	4,997.08	4,996.57
P-17	MH-20	MH-91	49.7	0.004	Circle	42			58.5	63.82	6.08	4,992.08	4,991.88	4,999.15	4,999.04	4,996.54	4,996.37	4,995.97	4,995.80
P-18	MH-91	MH-22	245.4	0.004	Circle	48			60.95	90.77	7.74	4,991.88	4,990.90	4,999.04	5,000.25	4,996.06	4,995.63	4,995.68	4,995.26
P-19	MH-22	MH-49	59.8	0.004	Circle	48			60.95	91	4.85	4,990.90	4,990.66	5,000.25	5,000.71	4,995.33	4,995.22	4,994.97	4,994.86
P-20	CB-103	CB-51		0.018	Circle	12			2.7	4.84	3.44	4,996.96	4,996.56	4,999.93	5,000.56	4,998.79	4,998.66	4,998.60	4,998.48
P-20	MH 02	CB-Exist Cattle Guard Inlet	178.8	0.01	Circle	24			13.67	22.51	7.51	4,982.12	4,980.35	4,986.63	4,983.35	4,984.29	4,984.67	4,983.98	4,983.35
P-21	CB-Exist Cattle Guard Inlet	O-5-Existing MH at Edith	97.2	0.015	Ellipse		2.2	3.6	66.67	65.57	10.93	4,978.35	4,976.88	4,983.35	4,981.41	4,984.18	4,982.66	4,982.33	4,980.80
P-22	CB-26	CB-25	30.6	0.02	Circle	24			3	31.67	6.34	4,996.10	4,995.50	5,000.93	5,000.77	4,997.91	4,997.91	4,997.90	4,997.90
P-23	H-1	MH-30	53.7	0.004	Circle	42			41.1	62.89	4.27	4,993.50	4,993.29	4,999.00	4,999.92	4,997.75	4,997.66	4,997.47	4,997.38
P-24	CB-25	O-2	24.8	0.02	Circle	24			6	32.13	1.91	4,995.50	4,995.00	5,000.77	4,999.00	4,997.88	4,997.87	4,997.83	4,997.81
P-26	MH-58	MH-33	197.4	0.01	Circle	18			8.65	10.49	6.63	5,002.01	5,000.04	5,007.81	5,006.88	5,003.78	5,002.46	5,003.38	5,002.09
P-27	CB-34	MH-20	61.4	0.02	Circle	24			13.8	32.03	4.39	4,994.03	4,992.80	4,999.24	4,999.15	4,997.09	4,996.86	4,996.79	4,996.56
P-28	CB-35	MH-20	12.1	0.05	Circle	18			3.6	23.48	2.04	4,993.33	4,992.73	4,999.03	4,999.15	4,996.78	4,996.77	4,996.72	4,996.71

P-29	MH-33	MH -36	54.1	0.01	Circle	24			8.65	22.61	2.75	5,000.04	4,999.50	5,006.88	5,006.34	5,002.27	5,002.19	5,002.15	5,002.07
P-30	MH -36	MH-42	93.7	0.02	Circle	24			14.58	31.96	9.94	4,999.50	4,997.63	5,006.34	5,005.23	5,001.50	5,000.58	5,000.88	5,000.24
P-31	MH-42	MH-38	128	0.02	Circle	24			15.76	31.74	10.08	4,997.63	4,995.11	5,005.23	5,003.28	4,999.73	4,997.98	4,999.06	4,997.59
P-32	MH-38	O-4	68.4	0.02	Circle	24			15.76	32.01	10.15	4,995.11	4,993.74	5,003.28	4,997.00	4,997.21	4,996.23	4,996.54	4,994.77
P-33	CB-40	CB-79	70.9	0.02	Circle	18			4.54	14.82	7.37	5,001.35	4,999.94	5,006.67	5,005.43	5,002.72	5,002.59	5,002.58	5,002.48
P-34	CB-79	MH -36	21.8	0.02	Circle	18			5.93	14.92	3.36	4,999.94	4,999.50	5,005.43	5,006.34	5,002.28	5,002.21	5,002.11	5,002.04
P-36	CB-43	MH-42	60.7	0.03	Circle	18			1.18	18.19	5.8	5,001.19	4,999.37	5,005.46	5,005.23	5,001.74	5,000.45	5,001.60	5,000.44
P-38	MH-44	O-3	87.7	0.009	Circle	54			74.53	185.49	11.03	4,990.28	4,989.50	5,001.25	4,999.00	4,994.26	4,994.14	4,993.77	4,993.79
P-42	MH-49	MH-44	95.9	0.004	Circle	48			74.53	90.43	8.04	4,990.66	4,990.28	5,000.71	5,001.25	4,994.93	4,994.69	4,994.33	4,994.14
P-43	CB-50	MH-49	20.8	0.02	Circle	18			6.26	14.94	8.08	4,996.55	4,996.13	5,000.55	5,000.71	4,997.94	4,997.69	4,997.52	4,996.87
P-44	CB-51	MH-49	14.1	0.02	Circle	18			7.32	14.82	8.37	4,996.56	4,996.28	5,000.56	5,000.71	4,998.09	4,997.93	4,997.61	4,997.12
P-47	MH-86	CB-87	35.1	0.02	Circle	30			24.32	57.91	4.95	4,994.93	4,994.23	5,002.14	5,001.42	4,999.17	4,999.05	4,998.79	4,998.67
P-48	MH-63	MH-86	126.8	0.042	Circle	30			24.32	84.31	14.85	5,000.29	4,994.93	5,007.39	5,002.14	5,002.72	4,999.41	5,001.97	4,999.03
P-49	CB-87	O-1	22.6	0.01	Circle	36			46.02	67.21	6.51	4,994.23	4,994.00	5,001.42	4,999.00	4,998.58	4,998.47	4,997.92	4,997.81
P-55	CB-64	MH-65	82.1	0.005	Circle	24			14.2	15.98	4.52	5,004.00	5,003.59	5,007.51	5,008.77	5,006.82	5,006.49	5,006.50	5,006.18
P-75	CB-92	MH-91	14.4	0.02	Circle	18			2.45	14.92	1.39	4,992.17	4,991.88	4,998.91	4,999.04	4,996.16	4,996.15	4,996.13	4,996.13
P-78	CB-94	MH-58	46.9	0.01	Circle	18			5.77	10.52	3.27	5,002.48	5,002.01	5,006.00	5,007.81	5,004.33	5,004.18	5,004.16	5,004.02
P-80	MH-100	MH-58	236.7	0.01	Circle	18			2.88	10.51	5.07	5,004.38	5,002.01	5,007.72	5,007.81	5,005.27	5,004.13	5,005.02	5,004.09
P-81	CB-97	MH-100	74.5	0.03	Circle	18			2.88	18.19	7.52	5,006.62	5,004.38	5,010.18	5,007.72	5,007.50	5,005.47	5,007.26	5,005.40
P-82	CB-89	CB-34	60.4	0.02	Circle	24			7.7	32.01	2.45	4,995.24	4,994.03	4,999.24	4,999.24	4,997.36	4,997.29	4,997.26	4,997.19

SWMD STORMCAD MANHOLE TABLE

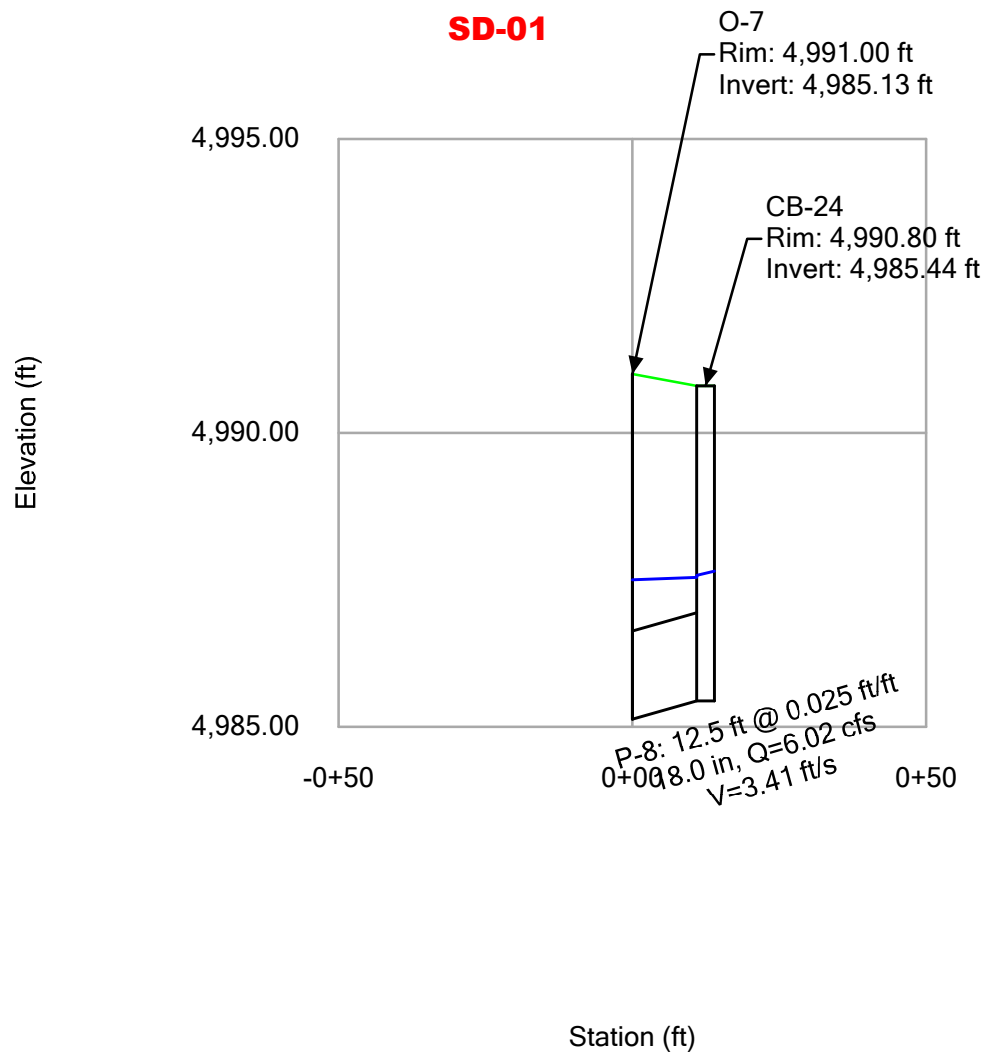
Label	Elevation (Ground) (ft)	Elevation (Rim) (ft)	Elevation (Invert in 1) (ft)	Elevation (Invert in 2) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
MH-58	5,007.81	5,007.81	5,002.01	5,002.01	5,003.71	5,003.50
MH-100	5,007.72	5,007.72	5,004.38	(N/A)	5,005.20	5,005.07
MH-33	5,006.88	5,006.88	5,000.04	(N/A)	5,002.19	5,002.18
MH -36	5,006.34	5,006.34	4,999.50	4,999.50	5,001.52	5,001.10
MH-42	5,005.23	5,005.23	4,997.63	4,999.37	4,999.78	4,999.30
MH-38	5,003.28	5,003.28	4,995.11	(N/A)	4,997.16	4,996.78
MH-05	5,008.78	5,008.78	5,004.08	(N/A)	5,006.73	5,006.64
MH-65	5,008.77	5,008.77	5,002.89	5,003.59	5,005.99	5,005.86
MH-06	5,008.77	5,008.77	5,001.78	(N/A)	5,004.48	5,003.72
MH-63	5,007.39	5,007.39	5,000.29	(N/A)	5,002.48	5,002.23
MH-86	5,002.14	5,002.14	4,994.93	(N/A)	4,998.88	4,998.87
MH-11	5,001.89	5,001.89	4,995.75	(N/A)	4,999.19	4,999.18
MH-44	5,001.25	5,001.25	4,990.28	(N/A)	4,993.98	4,993.87
MH-49	5,000.71	5,000.71	4,990.66	4,996.13	4,994.49	4,994.45
MH-22	5,000.25	5,000.25	4,990.90	(N/A)	4,995.12	4,995.04
MH-30	4,999.92	4,999.92	4,993.29	(N/A)	4,997.27	4,997.13
MH-20	4,999.15	4,999.15	4,992.08	4,992.80	4,996.17	4,996.08
MH-91	4,999.04	4,999.04	4,991.88	4,991.88	4,995.76	4,995.76
MH-2	4,998.85	4,998.85	4,984.42	(N/A)	4,988.78	4,988.14
MH 02	4,986.63	4,986.63	4,982.12	(N/A)	4,984.15	4,984.04

SWMD STORMCAD CATCH BASIN TABLE

Label	Elevation (Rim) (ft)	Flow (Total Out) (cfs)	Elevation (Invert) (ft)	Elevation (Invert in 2) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
CB-10	5,002.10	5.2	4,997.02	(N/A)	4,999.34	4,999.33
CB-87	5,001.42	46.02	4,994.23	4,994.23	4,998.24	4,998.05
CB-26	5,000.93	3	4,996.10	(N/A)	4,997.91	4,997.90
CB-25	5,000.77	6	4,995.50	(N/A)	4,997.85	4,997.84
CB-89	4,999.24	7.7	4,995.24	(N/A)	4,997.30	4,997.28
CB-34	4,999.24	13.8	4,994.03	(N/A)	4,996.95	4,996.85
CB-35	4,999.03	3.6	4,993.04	(N/A)	4,996.75	4,996.73
CB-92	4,998.91	2.45	4,992.17	(N/A)	4,996.15	4,996.14
CB-50	5,000.55	6.26	4,996.55	(N/A)	4,997.89	4,997.66
CB-51	5,000.56	7.32	4,996.56	(N/A)	4,998.11	4,997.78
CB-43	5,005.46	1.18	5,001.19	(N/A)	5,001.69	5,001.63
CB-40	5,006.67	4.54	5,001.35	(N/A)	5,002.68	5,002.61
CB-79	5,005.43	5.93	4,999.94	(N/A)	5,002.41	5,002.11
CB-94	5,006.00	5.77	5,002.48	(N/A)	5,004.23	5,004.19
CB-97	5,010.18	2.88	5,006.62	(N/A)	5,007.39	5,007.31
CB-04	5,007.78	10.12	5,004.50	(N/A)	5,007.00	5,006.99
CB-64	5,007.51	14.2	5,004.00	(N/A)	5,006.58	5,006.56
CB 01	4,990.80	2.5	4,985.01	(N/A)	4,985.61	4,985.61
CB-102	5,001.49	10.9	4,994.35	(N/A)	4,998.89	4,998.87
CB-103	4,999.93	2.7	4,996.96	(N/A)	4,998.68	4,998.64
CB-21	4,997.00	44.8	4,989.00	(N/A)	4,992.13	4,991.58
CB 104	4,986.99	13.67	4,982.40	(N/A)	4,984.50	4,984.33
CB-Exist Cattle Guard Inlet	4,983.35	66.67	4,977.35	(N/A)	4,982.70	4,982.70
CB-24	4,990.80	6.02	4,985.44	(N/A)	4,987.65	4,987.58

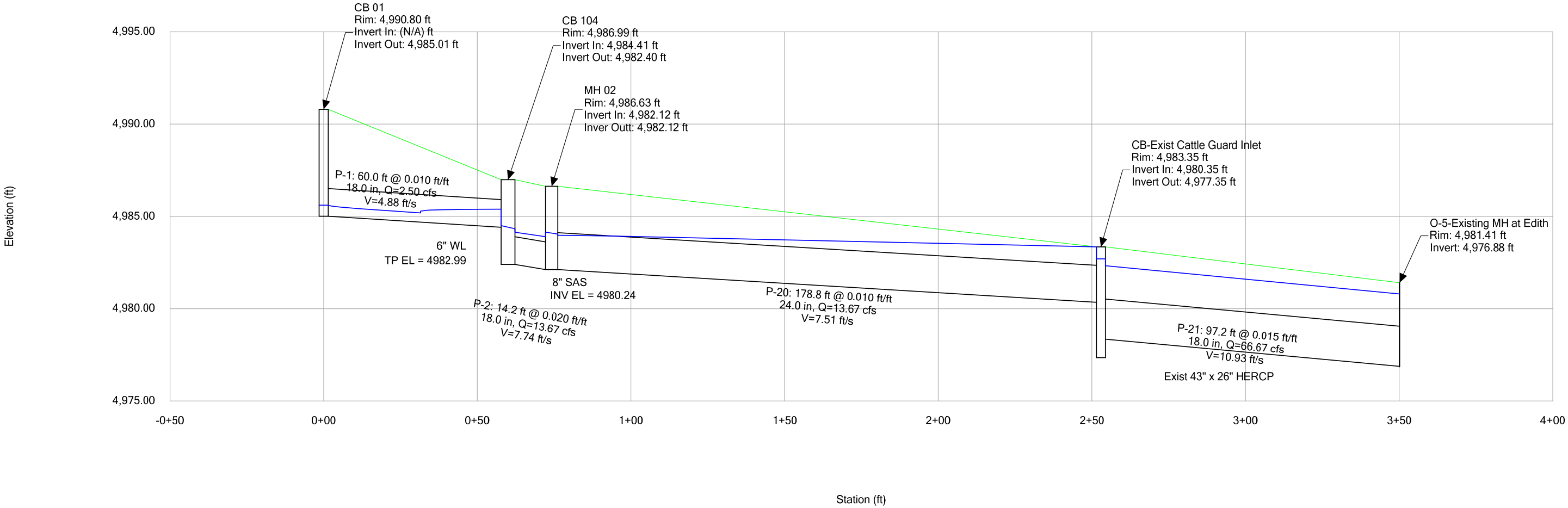
Profile Report **Engineering Profile - Profile - Basin 206 to Pond C (SWMD SD.stsw)**

SD-01

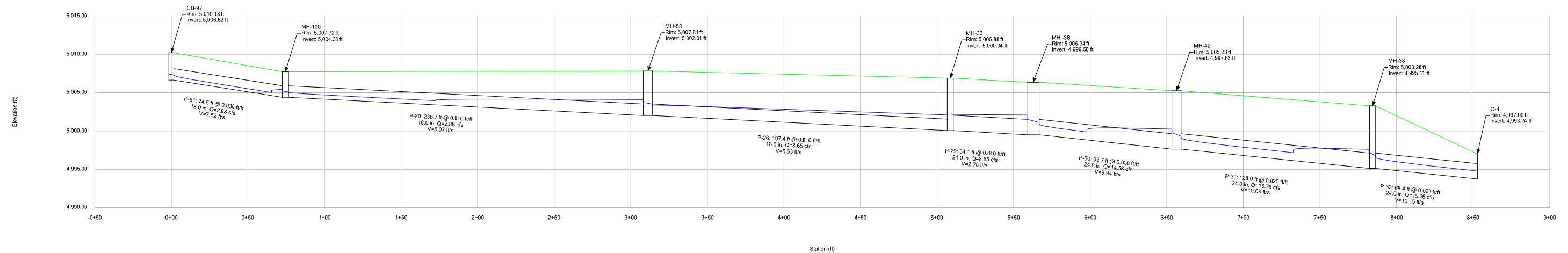


Profile Report
Engineering Profile - Profile - Basin 206 (SWMD SD.stsw)

SD-01

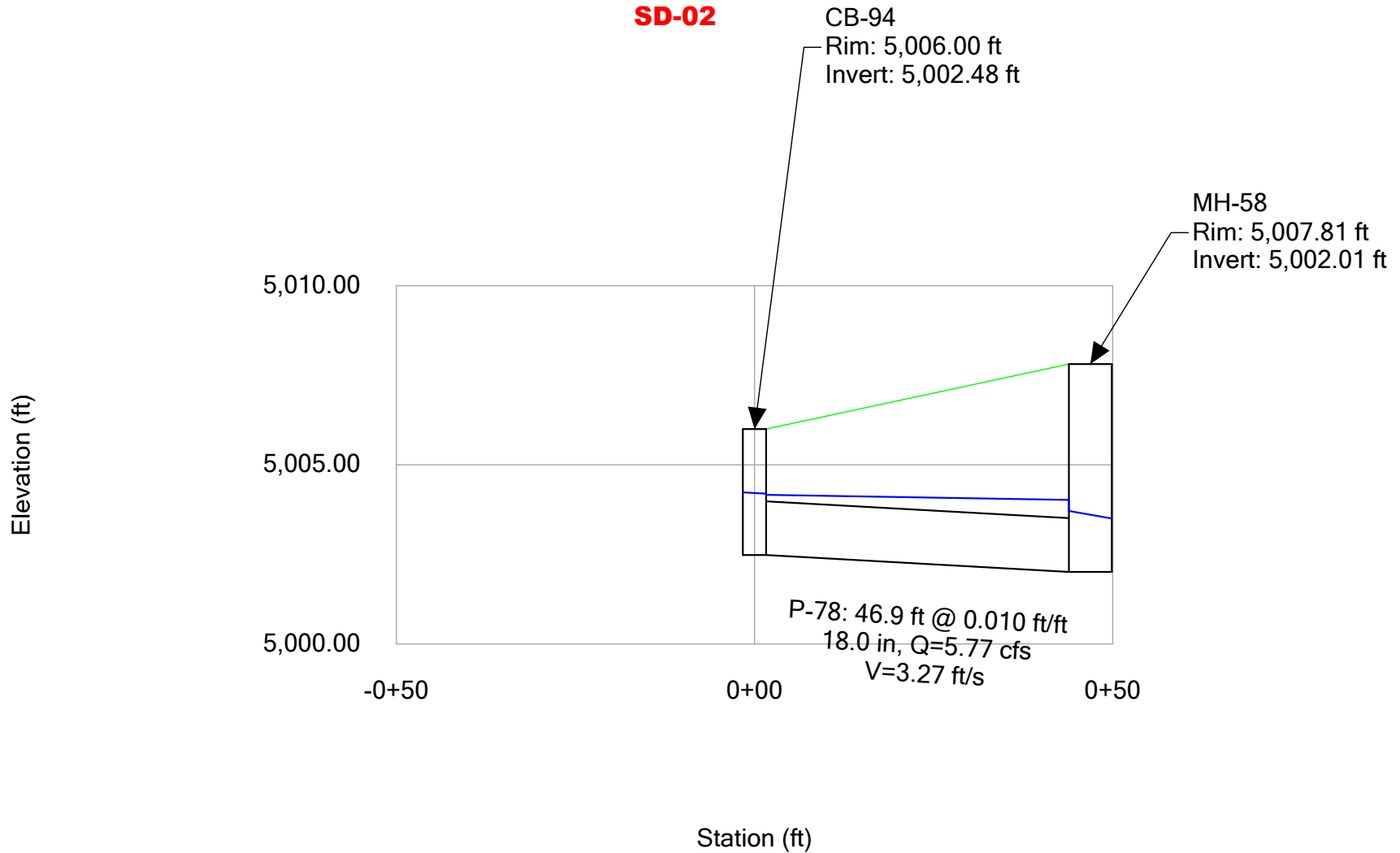


Profile Report
Engineering Profile - Profile - Basin 208 to Pond A (SWMD SD.stsw)
SD-02

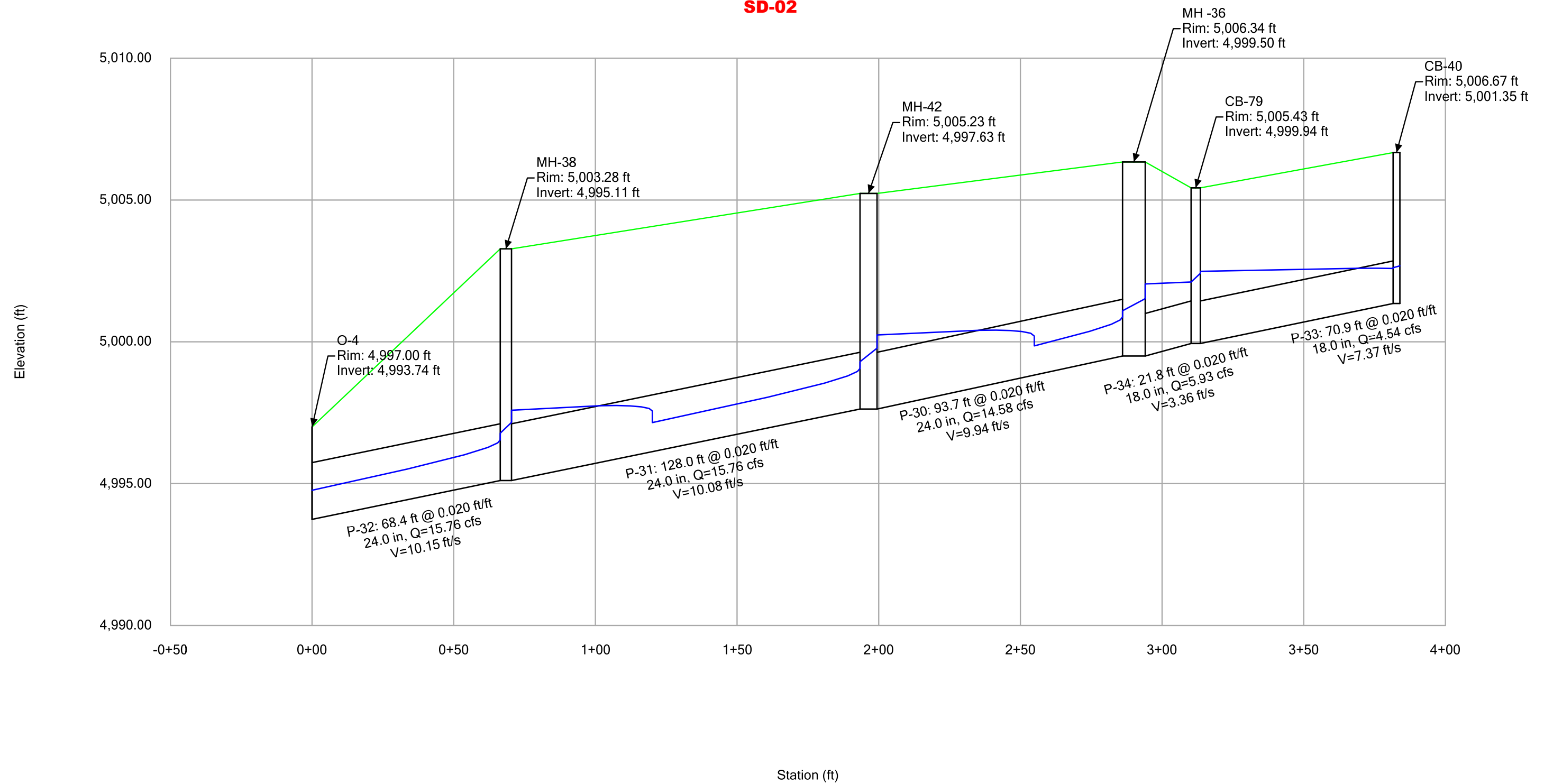


Profile Report **Engineering Profile - Basin 209 (SWMD SD.stsw)**

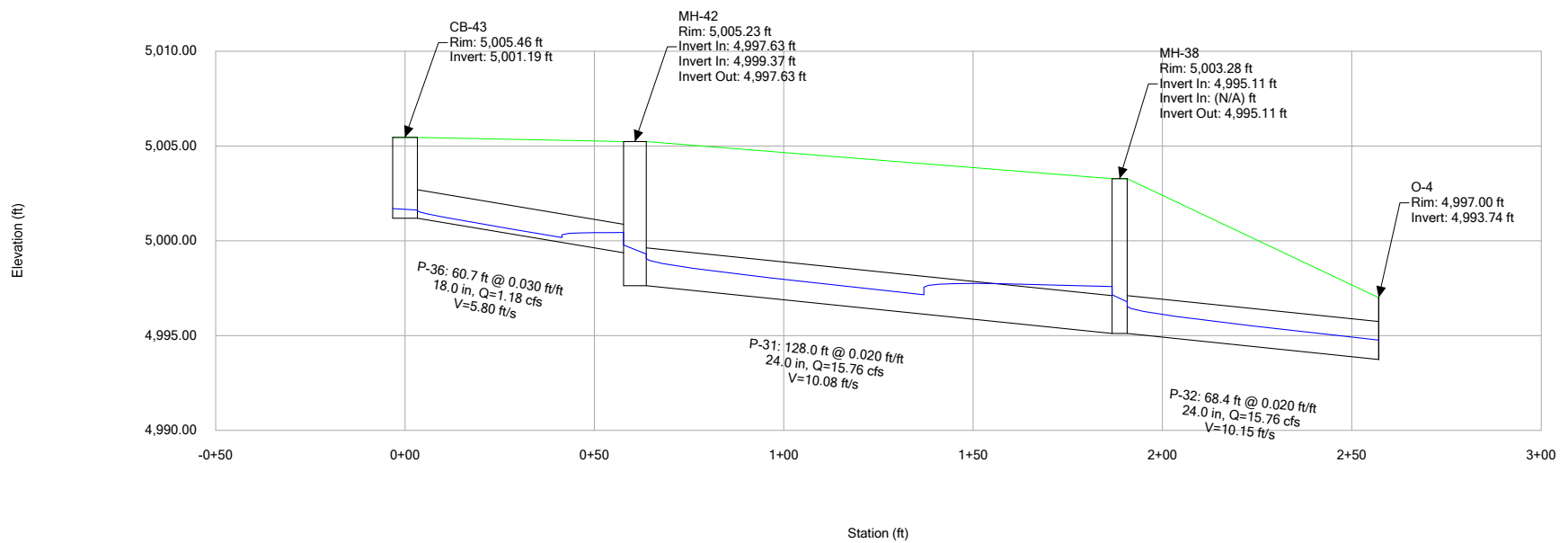
SD-02



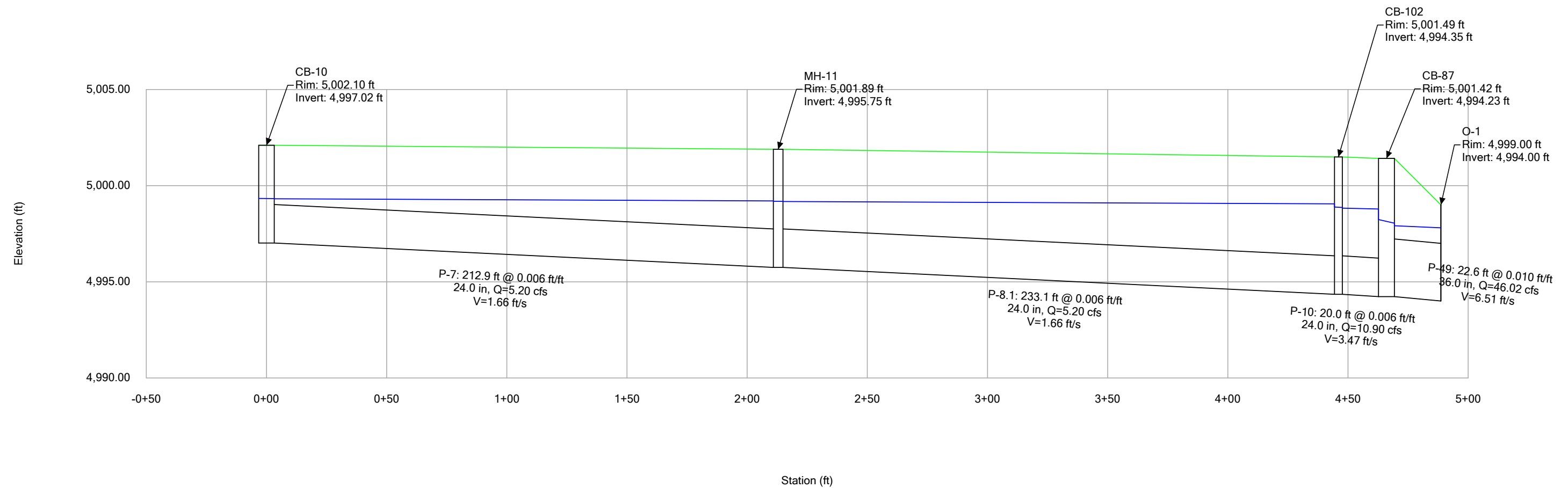
Profile Report
Engineering Profile - Profile - Basin 214 to Pond A (SWMD SD.stsw)
SD-02



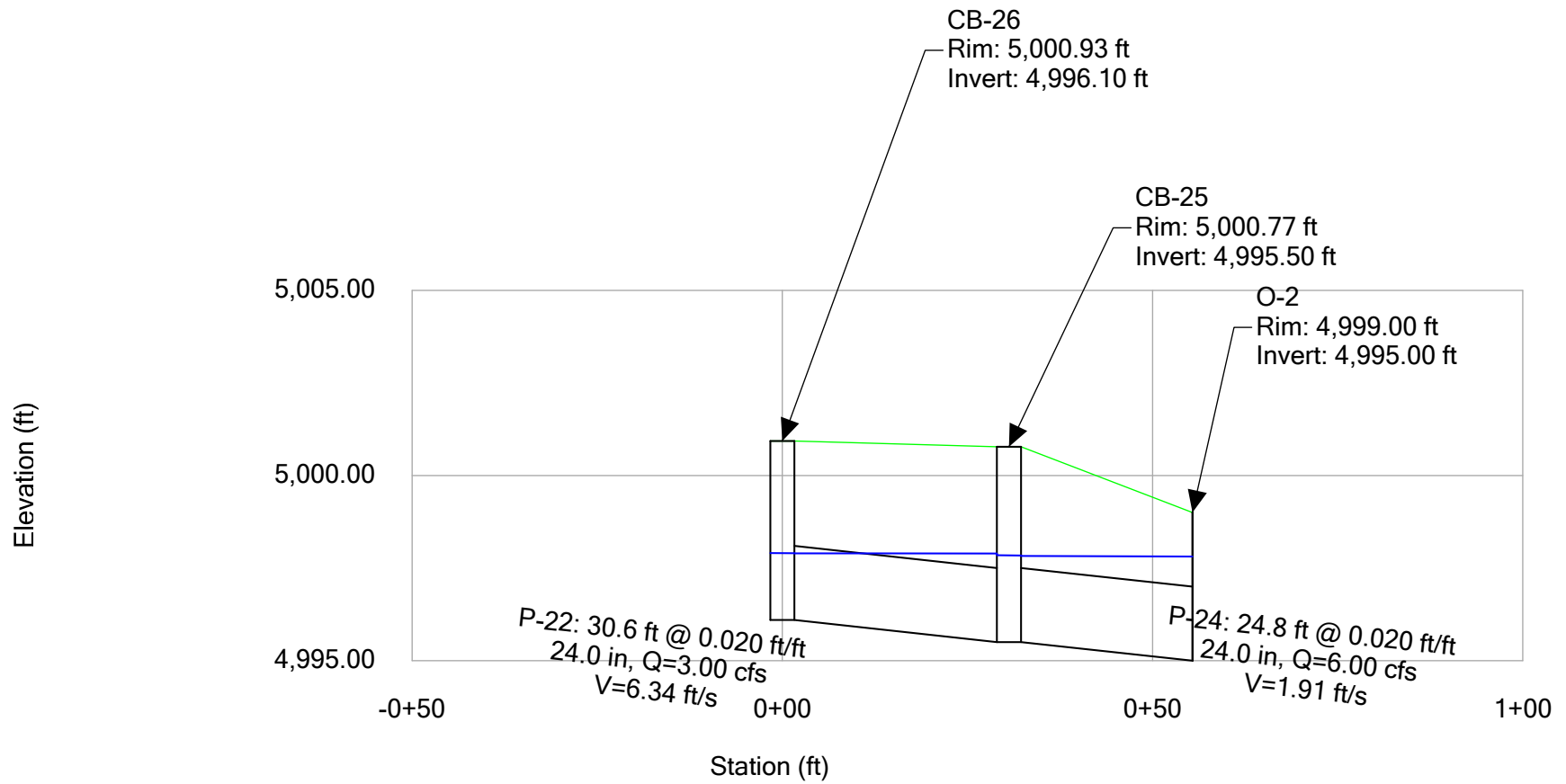
Profile Report **Engineering Profile - Profile - Basin 215 to Pond A (SWMD SD.stsw)** **SD-02**



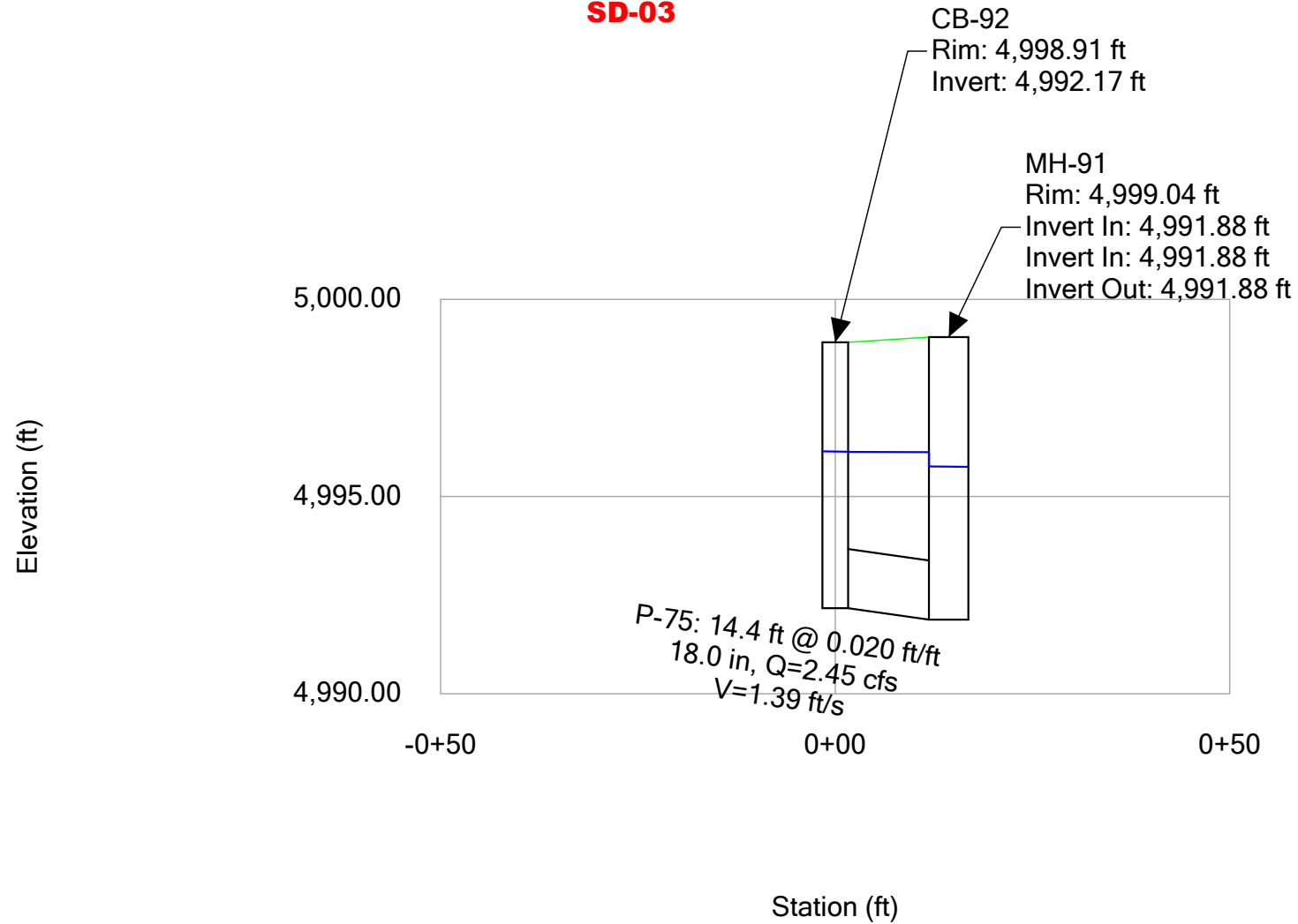
Profile Report
Engineering Profile - Profile - Basin 203 to Pond B (SWMD SD.stsw)
SD-03



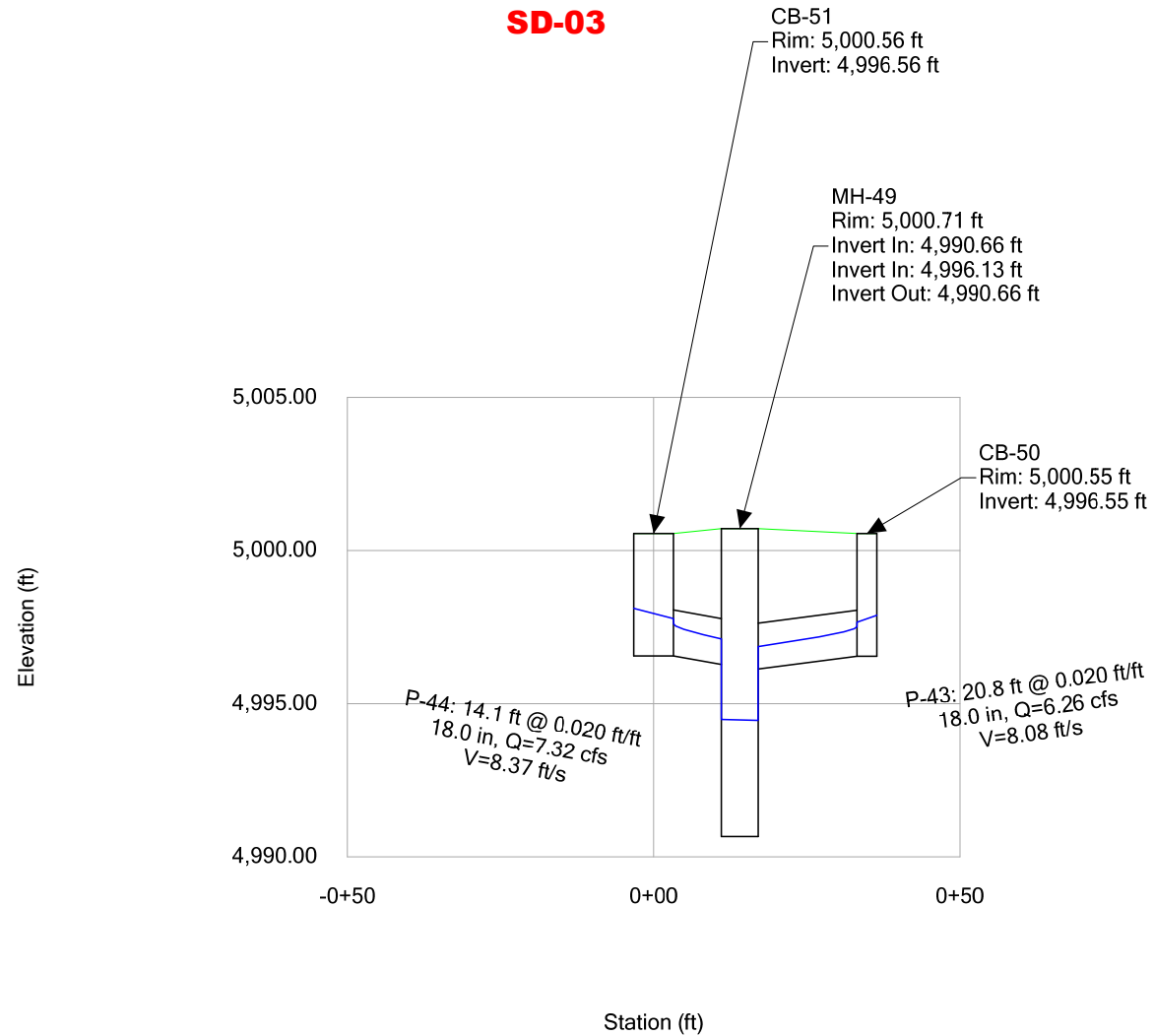
Profile Report **Engineering Profile - Profile - Basin 205 to Pond B (SWMD SD.stsw)** **SD-03**



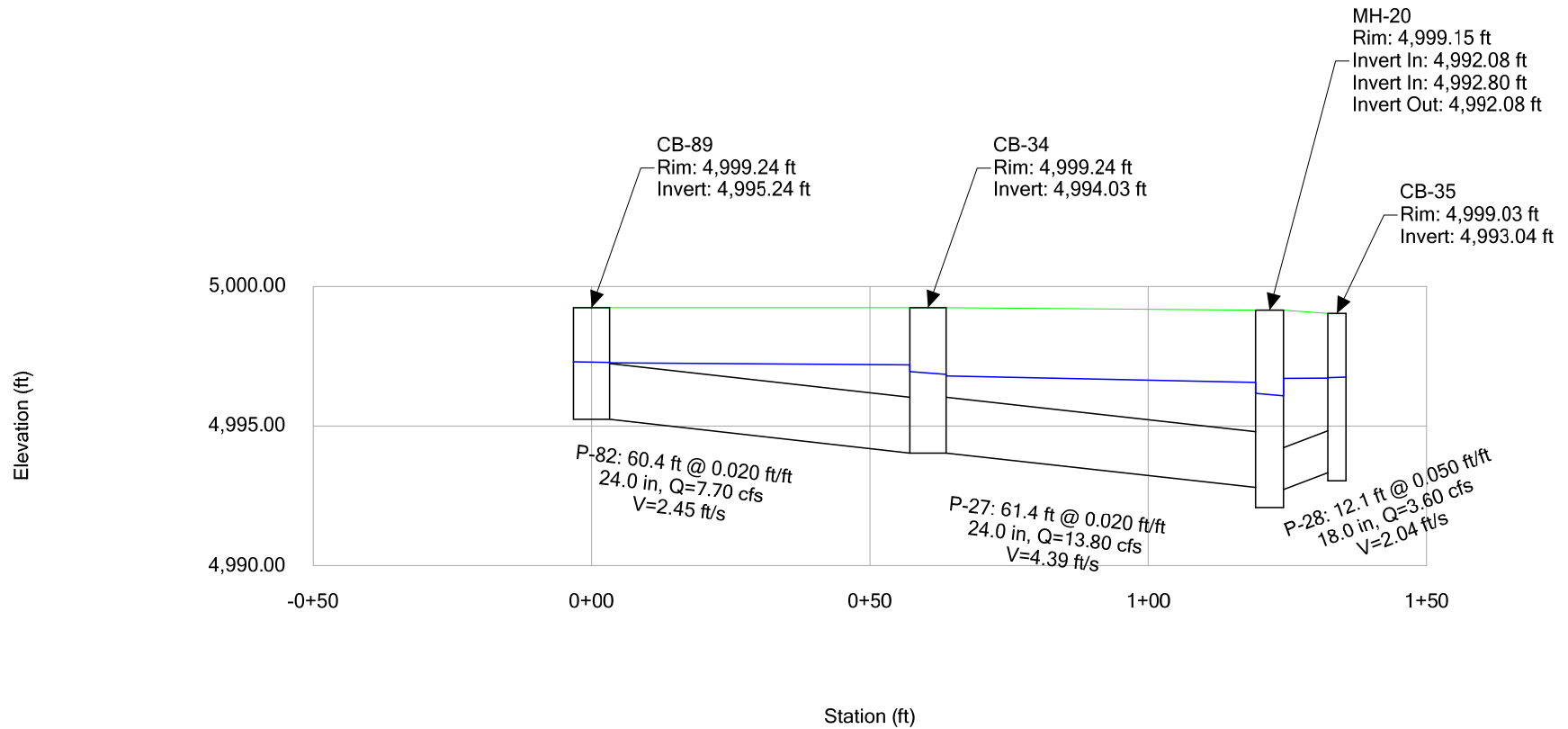
Profile Report
Engineering Profile - Profile - Basin 207 (SWMD SD.stsw)
SD-03



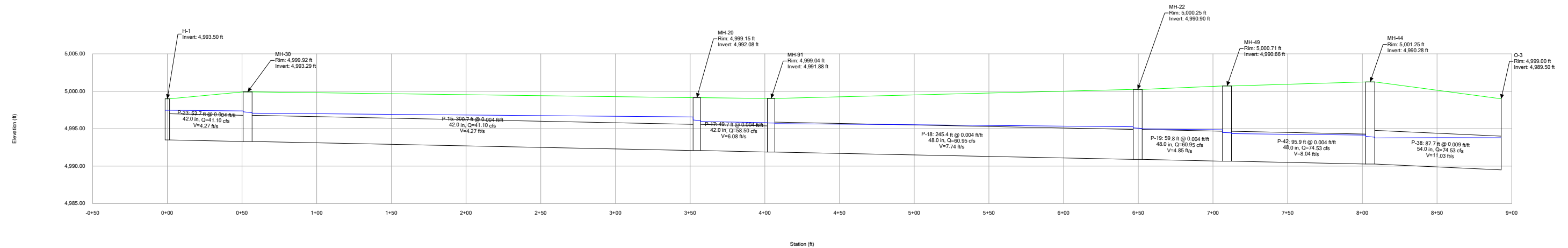
Profile Report **Engineering Profile - Profile - Basin 219 (SWMD SD.stsw)** **SD-03**



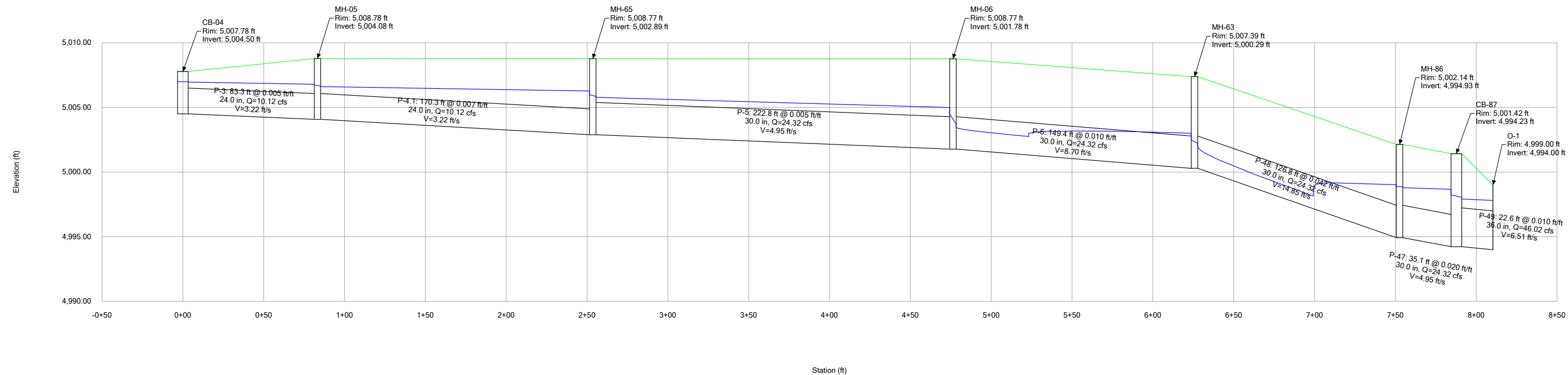
Profile Report **Engineering Profile - Profile - Basins 211 to 212 (SWMD SD.stsw)** **SD-03**



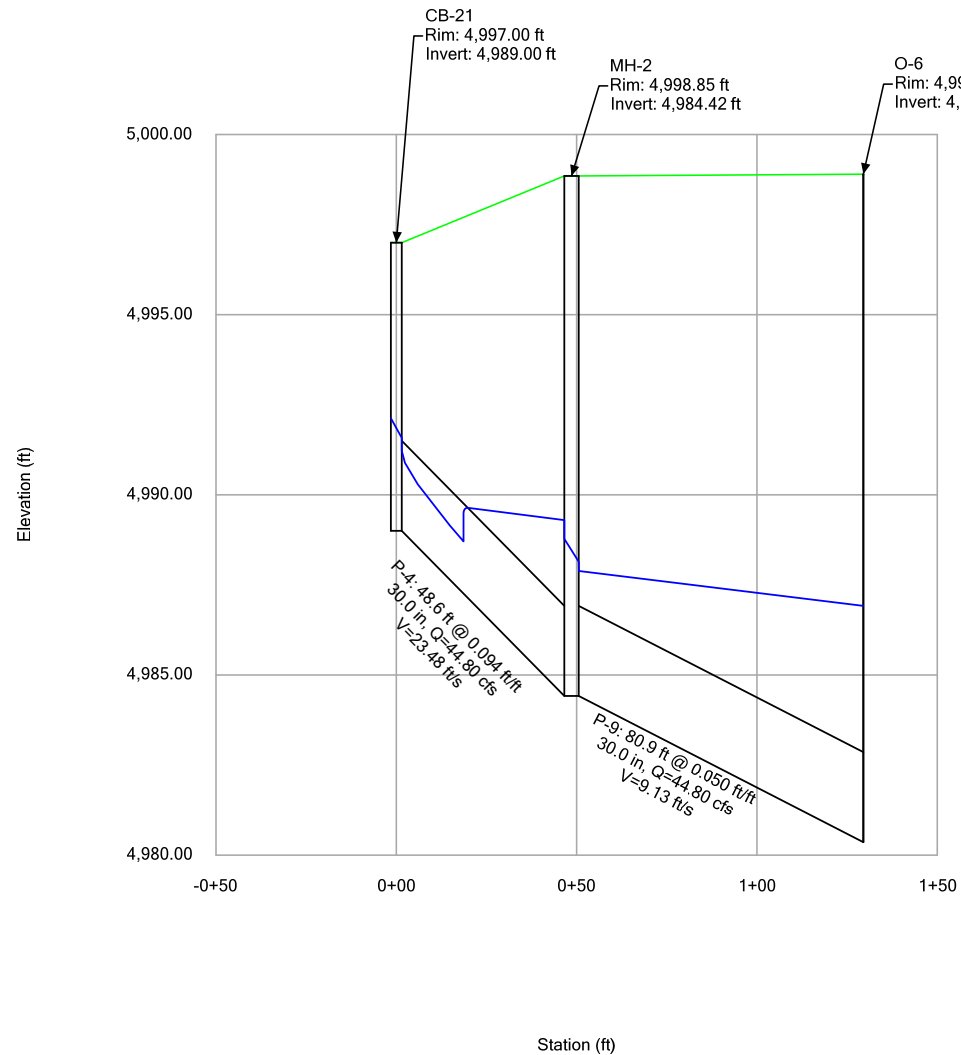
Profile Report
Engineering Profile - Profile - Pond B to Pond A (SWMD SD.stsw)
SD-03



Profile Report
Engineering Profile - Profile - Basin 201 to Pond B (SWMD SD.stsw)
SD-04



Profile Report **Engineering Profile - Profile - Pond A Outfall (SWMD SD.stsw)**



APPENDIX E

Miscellaneous Calculations..... E-1 to E-5

- Pond Calculation Tables
- Pond Discharge Rating Table
- 80th Percentile Volume Calculations
- Pond Riser Calculations
- Cultec Underground Chamber Calculations

Pond Calculations							
Pond	Peak Flow (cfs)		Volume (ac-ft)		Elevation (ft)		
	In	Out	Prv'd	Req'd	Top	Bottom	WSEL
A	90	44.8	1.95	1.24	4997	4989	4995.4
B	43	41.1	0.56	0.38	4999	4994	4997.9
C	6	2.7	0.13	0.10	4986.5	4985	4986.0
Starting HGL elevation for pipes draining into Ponds A & B were extracted from AHYMO, Pond A WSEL = 4993.79 Peak Inflow @ 1.53 hr and Pond B WSEL= 4997.81, Peak Inflow @ 1.50 hr							
Tailwater elevations were extracted from StormCAD which were used as input in CulvertMaster to attain pond discharge rates							
80th percentile volume is additional and is not included in provided volume							

Ponds Discharge Rating Table

Pond A - 27" Orifice					
Elev	Contour Area (sf)	Vol (cf)	Vol (ac-ft)	Pipe Outflow (cfs)	* Actual Outflow (cfs)
4989	4,198	0	0.0000	0	0
4990	5,387	4,780	0.1097	3.69	0
4991	6,784	10,850	0.2491	12.84	0
4992	6,498	18,475	0.4241	24.17	11.06
4993	10,362	27,891	0.6403	32.11	30.89
4994	12,258	39,200	0.8999	37.79	38.2
4995	14,265	52,464	1.2044	42.73	44.31
4996	16,303	67,737	1.5550	47.14	47.14
4997	18,396	85,075	1.9531	51.18	51.18
* Indicates the lesser of the riser and pipe outflow					

Pond B				
Elev	Contour Area (sf)	Vol (cf)	Vol (ac-ft)	Outflow (cfs)
4994	2,297	0	0.0000	0
4995	3,176	2,725	0.0626	0
4996	4,193	6,398	0.1469	0
4997	5,344	11,155	0.2561	0
4998	6,626	17,129	0.3932	45.1
4999	8,039	24,450	0.5613	72.9

Pond C			
Elev	Vol (cf)	Vol (ac-ft)	Outflow (cfs)
4985	0	0.0000	0
4986	4,356	0.1000	2
4986.5	5,663	0.1300	5.3

80th Percentile Volume Calculation			
Pond	Impervious Area (ac)	V ^{80th%} (ac-ft)	Elevation
A	10.55	0.23	4989.00 to 4990.86
B	9.63	0.21	4994.00 to 4990.70
C	1.30	0.03	4985.00 to 4984.00
The required 80th percentile required volume is 0.26 inches of excess precipitation from the impervious area			

SWMD Maintenance & Admin Buildings Project

CONCRETE RISER
 INVERT OF PERFORATION(S) 4990.86 cfs
 DIAM OF PERFORATION(S) (in) 6
 Total Outflow (Needed) = 45.45
 Total Outflow (provided) = 46.54

# PERFORATIONS			1	2	3	5	6	12
ELEVATION	A (sf)	h (ft)	Q (cfs)	Q (cfs)	Q (cfs)	Q (cfs)	Q (cfs)	Q (cfs)
4991.5	0.20	0.39	0.61	1.22	1.83	3.05	3.66	7.32
4992	0.20	0.89	0.92	1.84	2.76	4.61	5.53	11.06
4993	0.20	1.89	1.34	2.69	4.03	6.72	8.06	16.12
4994	0.20	2.89	1.66	3.32	4.98	8.30	9.96	19.93
4995	0.20	3.89	1.93	3.85	5.78	9.63	11.56	23.12
4995.4	0.20	4.29	2.02	4.05	6.07	10.12	12.14	24.28
4996.1	0.20	4.99	2.18	4.36	6.55	10.91	13.09	26.19

2nd row of holes
 INVERT OF PERFORATION(S) 4991.91
 DIAM OF PERFORATION(S) (in) 6

# PERFORATIONS			1	2	4	5	6	11
ELEVATION	A (sf)	h (ft)	Q (cfs)	Q (cfs)	Q (cfs)	Q (cfs)	Q (cfs)	Q (cfs)
4992.5	0.20	0.34	0.57	1.14	2.28	2.85	3.42	6.27
4993	0.20	1.89	1.34	2.69	5.37	6.72	8.06	14.77
4994	0.20	2.89	1.66	3.32	6.64	8.30	9.96	18.27
4995	0.20	3.89	1.93	3.85	7.71	9.63	11.56	21.19
4995.4	0.20	4.29	2.02	4.05	8.09	10.12	12.14	22.26
4996.1	0.20	4.99	2.18	4.36	8.73	10.91	13.09	24.01
4997.1	0.20	5.99	2.39	4.78	9.56	11.95	14.35	26.30

* MAXIMUM WATER SURFACE ELEVATION

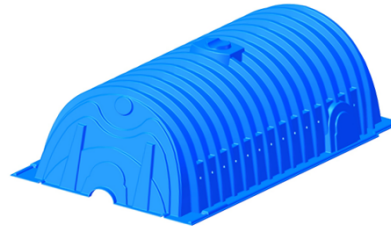


CULTEC Stormwater Design Calculator

Date:	May 08, 2020
Project Information:	
SWMD POND C	

Calculations Performed By:	

RECHARGER 330XLHD



Recharger 330XLHD Chamber Specifications		
Height	30.5	inches
Width	52.0	inches
Length	8.50	feet
Installed Length	7.00	feet
Bare Chamber Volume	52.21	cu. feet
Installed Chamber Volume	92.41	cu. feet

Breakdown of Storage Provided by Recharger 330XLHD Stormwater System		
Within Chambers	2,595.73	cu. feet
Within Feed Connectors	-	cu. feet
Within Stone	2,235.75	cu. feet
Total Storage Provided	4,831.5	cu. feet
Total Storage Required	4356.00	cu. feet

Materials List

Recharger 330XLHD		
Total Number of Chambers Required	48	pieces
Starter Chambers	8	pieces
Intermediate Chambers	32	pieces
End Chambers	8	pieces
HVLV FC-24 Feed Connectors	14	pieces
CULTEC No. 410 Non-Woven Geotextile	634	sq. yards
CULTEC No. 4800 Woven Geotextile	84	feet
Stone	207	cu. yards

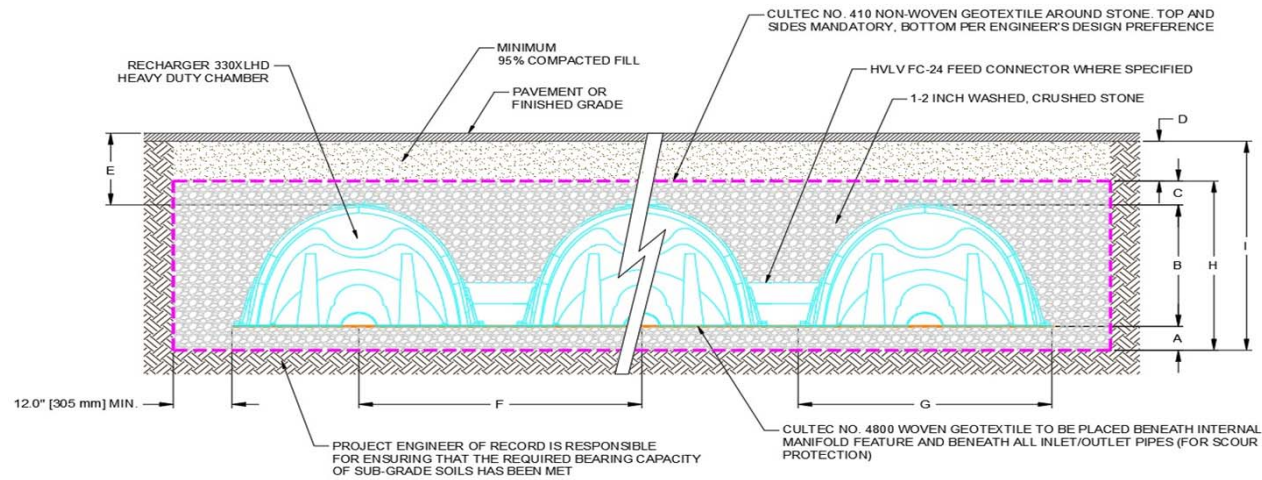
Based on 2 Internal Manifolds

Bed Detail



Bed Layout Information		
Number of Rows Wide	8	pieces
Number of Chambers Long	6	pieces
Chamber Row Width	39.92	feet
Chamber Row Length	43.50	feet
Bed Width	41.92	feet
Bed Length	45.50	feet
Bed Area Required	1907.21	sq. feet
Length of Separator Row	N/A	feet

Bed detail for reference only. Not project specific. Not to scale.



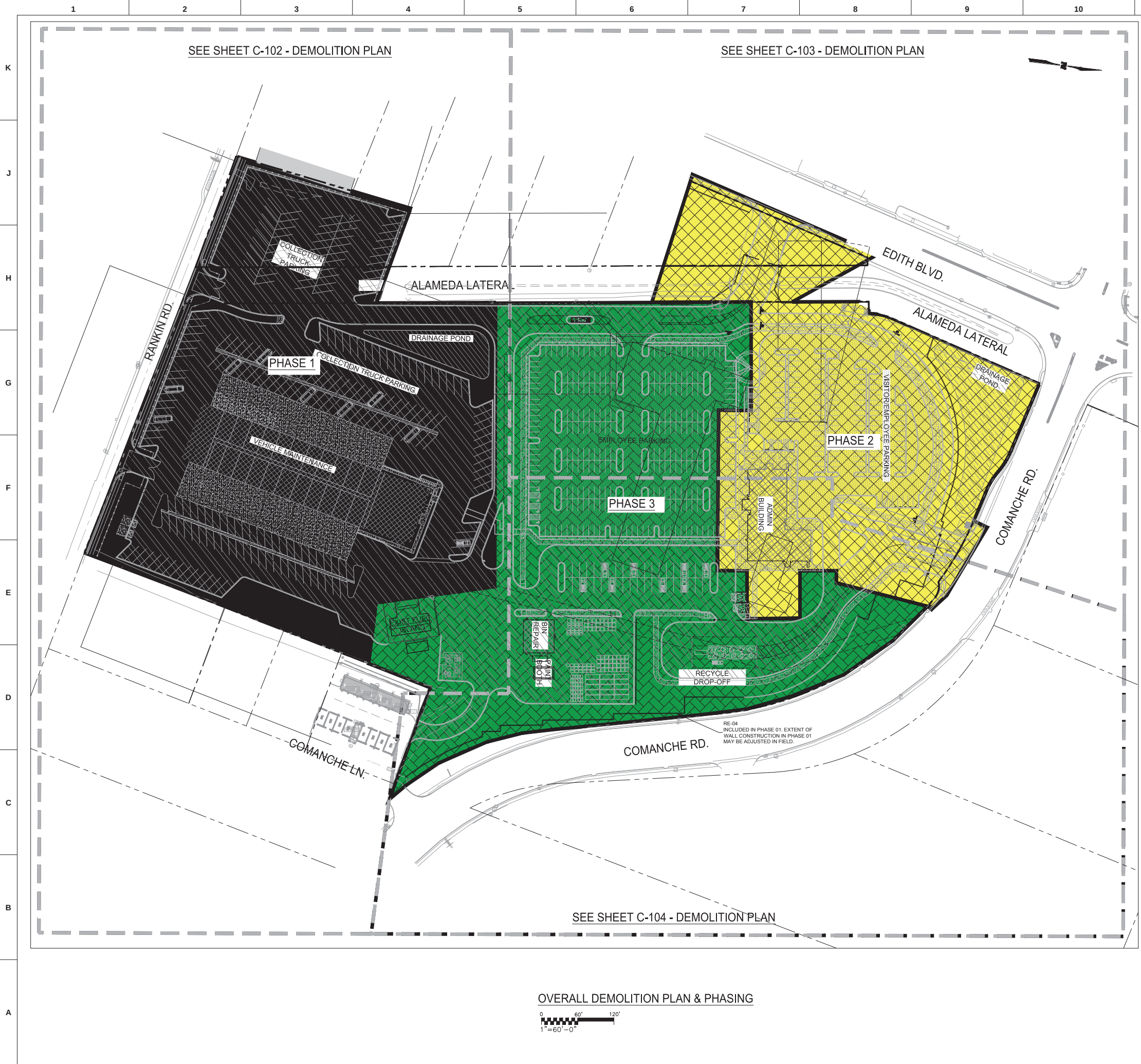
Conceptual graphic only. Not job specific.

Cross Section Table Reference			
A	Depth of Stone Base	9.0	inches
B	Chamber Height	30.5	inches
C	Depth of Stone Above Units	12.0	inches
D	Depth of 95% Compacted Fill	10.0	inches
E	Max. Depth Allowed Above the Chamber	12.00	feet
F	Chamber Width	52.0	inches
G	Center to Center Spacing	5.08	feet
H	Effective Depth	4.29	feet
I	Bed Depth	5.13	feet

APPENDIX F

Selected Pages from Construction Plans F-1 to F-19

- C-101, Phasing Plan
- C-109, Overall Grading & Drainage Plan
- C-110 to C-112, Grading Plan
- C-302 to C-307, Site Sections
- C-408, SD-01 Plan & Profile Sheet
- C-409, SD-02 Plan & Profile Sheet
- C-410 & C-411, SD-03 Plan & Profile Sheets
- C-412, SD-04 Plan & Profile Sheet
- C-500, Rankin Road Typical Section & Water Quality Inlet Detail
- C-502, Pond Outlet Structure Detail
- C-510, Underground Pond C & Pond Lining Details



- GENERAL NOTES**
1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
 2. IF THIS SHEET IS NOT 30"x42", THEN IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.
 3. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
 4. ALL DIMENSIONS ARE TO FACE OF CURB UNLESS OTHERWISE NOTED.

PHASE 1

DEMOLITION OF EXISTING STORAGE BUILDINGS

PERFORM EARTHWORK AND RE-GRADING OF SITE INCLUDING RETAINING WALLS

CONSTRUCT RANKIN ROAD WIDENING

CONSTRUCT VEHICLE MAINTENANCE BUILDING

INSTALL UTILITIES (WATER, SAS, GAS, ELECTRIC, STORM DRAIN)

INSTALL NEW PAVEMENT (ASPHALT AND PCC)

PHASE 2

DEMOLITION OF EXISTING ADMINISTRATION BUILDING AND VEHICLE MAINTENANCE BUILDINGS

PERFORM EARTHWORK AND RE-GRADING OF SITE INCLUDING RETAINING WALLS AND DRAINAGE POND

CONSTRUCT ADMINISTRATION BUILDING & GUARD SHACK

INSTALL UTILITIES (WATER, SAS, GAS, ELECTRIC, STORM DRAIN)

INSTALL NEW PAVEMENT (ASPHALT & PCC), CURB & GUTTER, SIDEWALK

PHASE 3

DEMOLITION OF EXISTING CURB & GUTTER, AND OTHER APPURTENANCES

PERFORM EARTHWORK AND RE-GRADING OF SITE INCLUDING GARDEN WALLS AND RETAINING WALLS

CONSTRUCT BIN REPAIR/WELD SHOP BUILDING AND RECYCLING AREA

INSTALL UTILITIES (WATER, SAS, GAS, ELECTRIC, STORM DRAIN)

INSTALL NEW PAVEMENT (ASPHALT & PCC), CURB & GUTTER, SIDEWALK

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PROJECT NO. 700693

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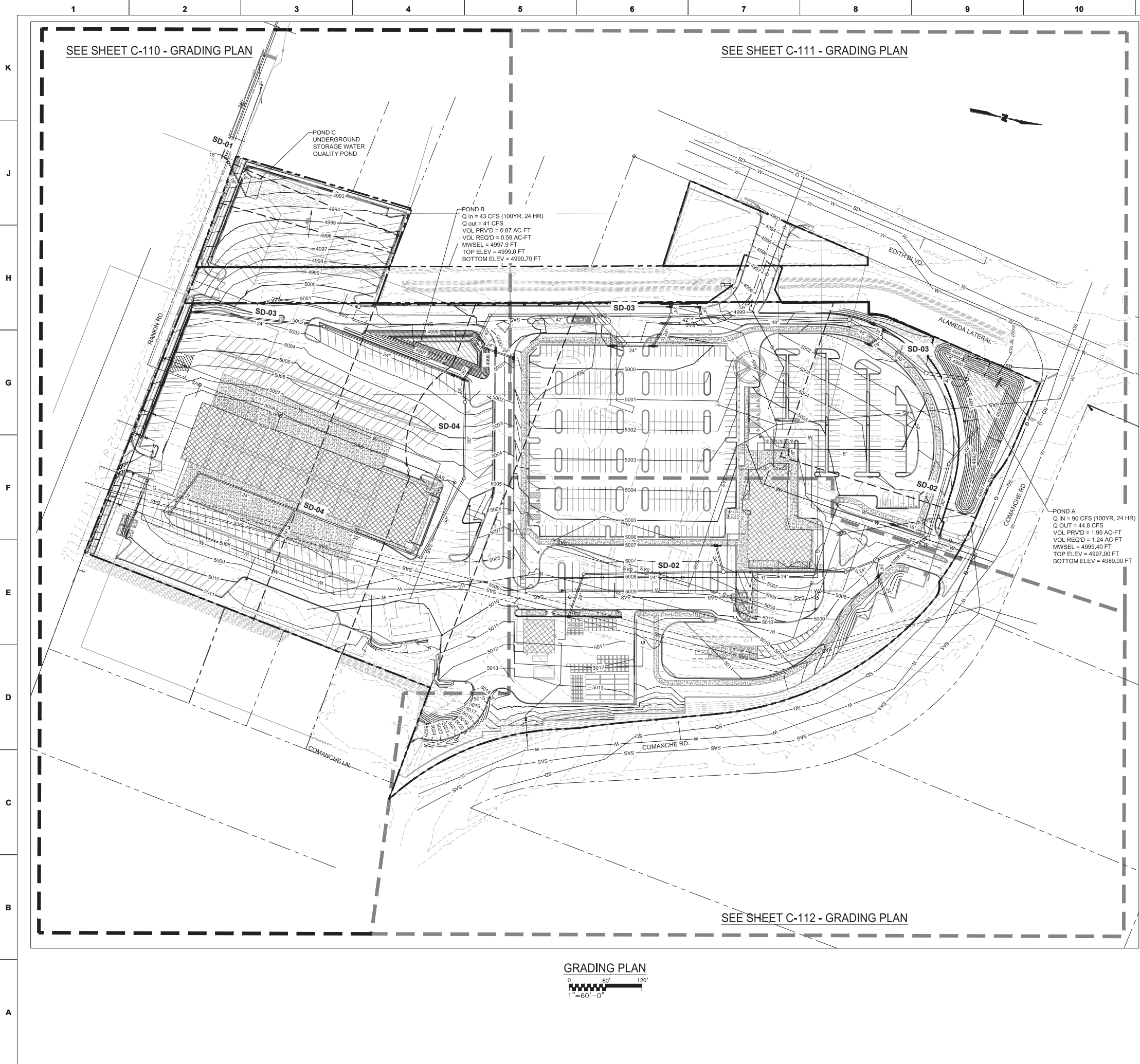


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OVERALL DEMOLITION PLAN & PHASING

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C-101



- GENERAL NOTES
1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
 2. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
 3. ALL DIMENSIONS ARE TO EDGE OF PAVEMENT UNLESS OTHERWISE NOTED.
 4. SEE SHEETS C-408 - C-412 FOR STORM DRAIN PLAN AND PROFILES.
 5. SEE SHEETS C-302 - C-304 FOR SITE CROSS SECTIONS.
 6. SEE SHEETS C-110 - C-112 FOR GRADING AND DRAINAGE DETAILS.
 7. SEE SHEET C-408 FOR SD-01 PLAN AND PROFILE.
 8. SEE SHEET C-409 FOR SD-02 PLAN AND PROFILE.
 9. SEE SHEET C-410 & C-411 FOR SD-03 PLAN AND PROFILE.
 10. SEE SHEET C-412 FOR SD-04 PLAN AND PROFILE.
 11. SEE SHEET C-510 FOR UNDERGROUND STORAGE FACILITY.

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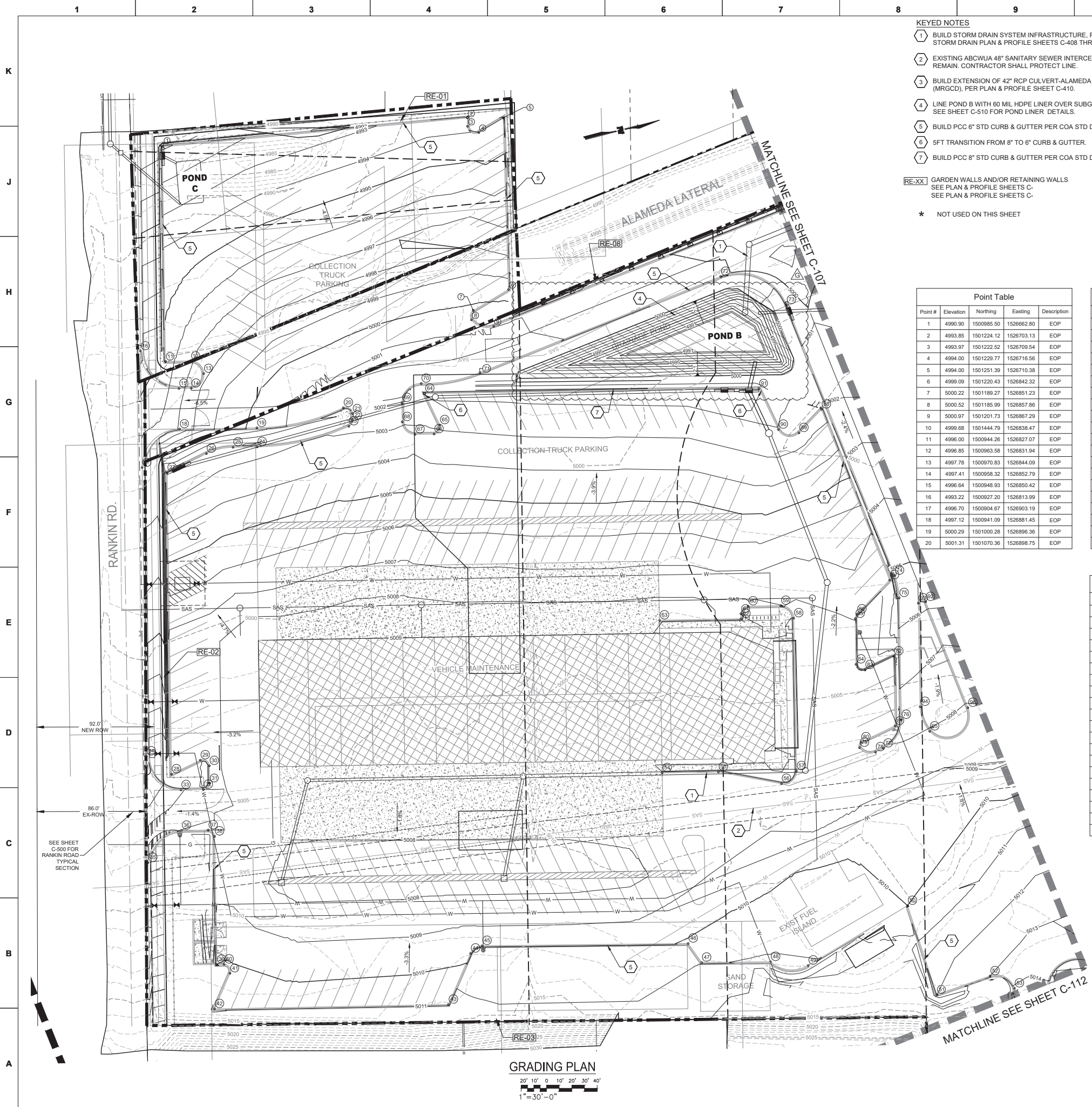
OVERALL
GRADING
PLAN

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DATE
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DWN

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SCALE
SDG
CHK

JRMA Project No.
4907-B
W&C - 14-100-132-01

C-109



GRADING PLAN
20' 10' 0 10' 20' 30' 40'
1"=30'-0"

KEYED NOTES

- 1 BUILD STORM DRAIN SYSTEM INFRASTRUCTURE. PER STORM DRAIN PLAN & PROFILE SHEETS C-408 THROUGH C-412
- 2 EXISTING ABCWUA 48" SANITARY SEWER INTERCEPTOR LINE TO REMAIN. CONTRACTOR SHALL PROTECT LINE.
- 3 BUILD EXTENSION OF 42" RCP CULVERT-ALAMEDA LATERAL (MRGCD), PER PLAN & PROFILE SHEET C-410.
- 4 LINE POND B WITH 60 MIL HDPE LINER OVER SUBGRADE PREP. SEE SHEET C-510 FOR POND LINER DETAILS.
- 5 BUILD PCC 6" STD CURB & GUTTER PER COA STD DWG 2415B.
- 6 5FT TRANSITION FROM 8" TO 6" CURB & GUTTER.
- 7 BUILD PCC 8" STD CURB & GUTTER PER COA STD DWG 2415A.

RE-XX GARDEN WALLS AND/OR RETAINING WALLS
SEE PLAN & PROFILE SHEETS C-
SEE PLAN & PROFILE SHEETS C-

* NOT USED ON THIS SHEET

GENERAL NOTES

- 1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
- 2. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
- 3. ALL DIMENSIONS ARE TO EDGE OF PAVEMENT UNLESS OTHERWISE NOTED.
- 4. SEE SHEET C-510 FOR POND C DETAILS.

Point Table				
Point #	Elevation	Northing	Easting	Description
1	4990.90	1500985.50	1526962.80	EOP
2	4993.85	1501224.12	1526703.13	EOP
3	4993.97	1501222.52	1526709.54	EOP
4	4994.00	1501229.77	1526716.56	EOP
5	4994.00	1501251.39	1526710.38	EOP
6	4999.09	1501220.43	1526842.32	EOP
7	5000.22	1501189.27	1526851.23	EOP
8	5000.52	1501185.99	1526857.86	EOP
9	5000.97	1501201.73	1526867.29	EOP
10	4999.68	1501444.79	1526838.47	EOP
11	4996.00	1500944.26	1526827.07	EOP
12	4996.85	1500963.58	1526831.94	EOP
13	4997.78	1500970.63	1526844.09	EOP
14	4997.41	1500958.32	1526852.79	EOP
15	4996.64	1500948.93	1526850.42	EOP
16	4993.22	1500927.20	1526813.99	EOP
17	4996.70	1500904.67	1526903.19	EOP
18	4997.12	1500941.09	1526881.45	EOP
19	5000.29	1501000.28	1526896.36	EOP
20	5001.31	1501070.36	1526898.75	EOP

Point Table				
Point #	Elevation	Northing	Easting	Description
21	5002.10	1501076.10	1526904.90	EOP
22	5002.28	1501074.77	1526910.20	EOP
23	5002.46	1501070.74	1526913.91	EOP
24	5002.63	1500996.61	1526910.91	EOP
25	5002.44	1500978.17	1526906.28	EOP
26	5002.23	1500956.56	1526905.68	EOP
27	5002.31	1500922.69	1526912.19	EOP
28	5007.25	1500864.43	1527142.89	EOP
29	5007.50	1500889.24	1527138.11	EOP
30	0.00	1500895.03	1527144.25	EOP
31	5007.00	1500891.67	1527157.55	EOP
32	5007.16	1500885.61	1527161.18	EOP
33	5008.87	1500868.51	1527156.90	EOP
34	5003.29	1500848.89	1527124.09	EOP
35	5008.20	1500828.32	1527205.54	EOP
36	5008.14	1500860.63	1527187.89	EOP
37	5008.47	1500881.01	1527193.04	EOP
38	5008.73	1500884.63	1527199.10	EOP
39	0.00	1500860.07	1527297.22	EOP
40	5010.06	1500865.69	1527298.33	EOP

Point Table				
Point #	Elevation	Northing	Easting	Description
41	5010.17	1500868.40	1527306.59	EOP
42	0.00	1500849.31	1527330.63	EOP
43	5010.86	1501028.49	1527375.12	EOP
44	5009.80	1501055.85	1527340.66	EOP
45	5009.62	1501066.16	1527337.19	EOP
46	5010.12	1501223.84	1527377.55	EOP
47	5010.52	1501230.24	1527394.82	EOP
48	5011.14	1501282.96	1527408.36	EOP
49	5011.04	1501310.86	1527418.82	EOP
50	5010.48	1501398.84	1527393.53	EOP
51	0.00	1501402.94	1527467.28	EOP
52	5013.56	1501447.43	1527463.99	EOP
53	5014.13	1501463.52	1527478.36	EOP
54	5008.79	1501238.88	1527242.21	EOP
55	5008.75	1501281.91	1527252.93	EOP
56	5008.76	1501327.64	1527274.77	EOP
57	5008.96	1501341.65	1527268.16	EOP
58	5008.53	1501370.81	1527151.08	EOP
59	5008.01	1501363.52	1527138.96	EOP
60	5008.17	1501338.45	1527132.72	EOP

Point Table				
Point #	Elevation	Northing	Easting	Description
61	5008.52	1501331.38	1527136.97	EOP
62	5008.68	1501330.43	1527140.82	EOP
63	5008.71	1501268.00	1527125.28	EOP
64	5001.75	1501135.34	1526904.53	EOP
65	5002.84	1501140.29	1526931.56	EOP
66	5003.14	1501134.16	1526937.31	EOP
67	5003.44	1501119.57	1526933.63	EOP
68	5002.88	1501112.32	1526921.49	EOP
69	5001.93	1501115.99	1526906.89	EOP
70	5001.58	1501134.65	1526886.12	EOP
71	0.00	1501181.67	1526889.88	EOP
72	5000.14	1501384.86	1526875.78	EOP
73	5000.73	1501429.29	1526910.78	EOP
74	5005.12	1501456.46	1527139.24	EOP
75	5005.50	1501455.33	1527157.23	EOP
76	5007.53	1501432.10	1527250.48	EOP
77	5008.12	1501412.51	1527268.62	EOP
78	5008.14	1501405.78	1527269.87	EOP
79	5008.22	1501394.49	1527263.25	EOP
80	5008.43	1501396.78	1527259.34	EOP

Point Table				
Point #	Elevation	Northing	Easting	Description
81	5008.30	1501426.10	1527253.89	EOP
82	5008.00	1501439.38	1527200.57	EOP
83	5008.00	1501414.61	1527205.17	EOP
84	5008.30	1501408.84	1527199.05	EOP
85	5007.97	1501417.54	1527164.11	EOP
86	5008.00	1501419.80	1527161.04	EOP
87	5007.33	1501451.71	1527141.66	EOP
88	5002.60	1501434.58	1526997.61	EOP
89	5002.63	1501412.63	1527010.94	EOP
90	5002.04	1501397.61	1527004.20	EOP
91	5001.40	1501391.13	1526998.86	EOP
92	5005.81	1501474.69	1527165.56	EOP
93	5005.76	1501468.80	1527165.19	EOP
94	5007.53	1501449.06	1527244.45	EOP
95	5008.07	1501451.36	1527265.16	EOP
96	5008.08	1501485.32	1527254.96	EOP

Project Revision
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CITY OF ALBUQUERQUE
PROJECT NO. 700693

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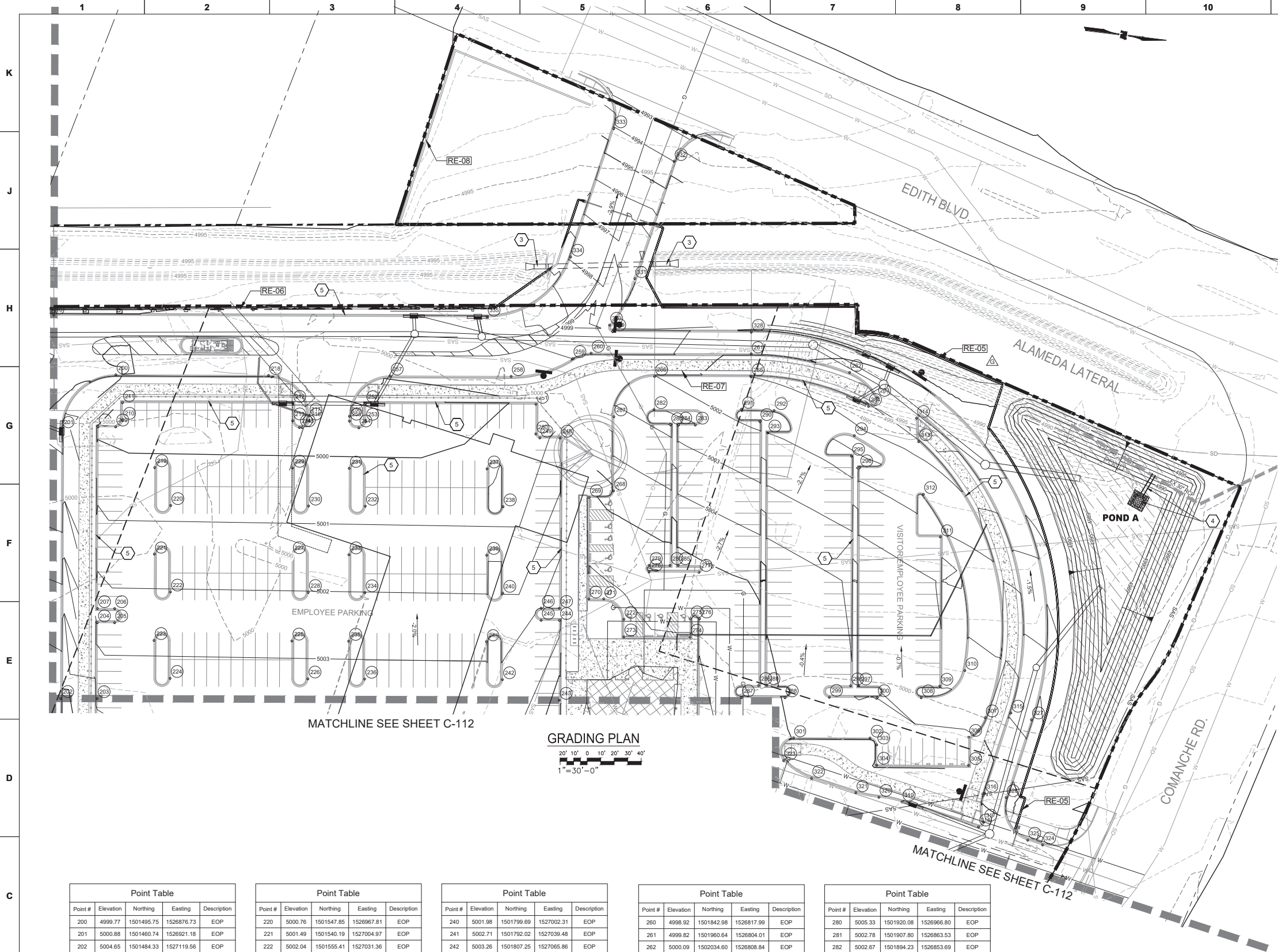


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GRADING PLAN

AS NOTED
DATE: 06/17/2020
CHK: [Signature]

JRMA Project No. 4907-B
W&C - 14-100-132-01
C-110



- GENERAL NOTES
1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
 2. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
 3. ALL DIMENSIONS ARE TO EDGE OF PAVEMENT UNLESS OTHERWISE NOTED.

- KEYED NOTES
- 1 BUILD STORM DRAIN SYSTEM INFRASTRUCTURE, PER STORM DRAIN PLAN & PROFILE SHEETS C-408 THROUGH C-412
 - 2 EXISTING ABCWUA 48" SANITARY SEWER INTERCEPTOR LINE TO REMAIN. CONTRACTOR SHALL PROTECT LINE.
 - 3 BUILD EXTENSION OF 42" RCP CULVERT-ALAMEDA LATERAL (MRGCD), PER PLAN & PROFILE SHEET C-410.
 - 4 BUILD CONCRETE RISER STRUCTURE. SEE SHEET C-502 FOR POND A OUTLET STRUCTURE DETAILS. INSTALL APPROXIMATELY 20 LF OF 30 INCH RCP STORM DRAIN, INV ELEV = 4989.00, S = ±9.0 %, CONNECT TO THE EXISTING 30 INCH RCP. FIELD VERIFY LOCATION & EXISTING PIPE INVERT ELEVATION. MATCH EXISTING INVERT.
 - 5 BUILD PCC 6" STD CURB & GUTTER PER COA STD DWG 24158.
- RE-XX GARDEN WALLS AND/OR RETAINING WALLS
SEE PLAN & PROFILE SHEETS C-
SEE PLAN & PROFILE SHEETS C-
* NOT ON THIS SHEET

Project Revision
BID SET 06.17.2020



CITY OF
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PROJECT NO. 700693

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GRADING
PLAN

AS NOTED
DATE: DAP SCALE: SBC
DWN CHK

JRMA Project No.
4907-B
W&C - 14-100-132-01
C-111

Point Table				
Point #	Elevation	Northing	Eastng	Description
200	4999.77	1501495.75	1526876.73	EOP
201	5000.88	1501460.74	1526921.18	EOP
202	5004.65	1501484.33	1527119.56	EOP
203	5003.83	1501511.14	1527116.36	EOP
204	5002.76	1501504.50	1527060.57	EOP
205	5002.55	1501517.17	1527059.07	EOP
206	5002.38	1501515.93	1527048.64	EOP
207	5002.22	1501503.26	1527050.15	EOP
208	4999.81	1501487.38	1526916.59	EOP
209	4999.65	1501500.29	1526915.05	EOP
210	4999.55	1501504.67	1526909.50	EOP
211	4999.39	1501503.13	1526896.59	EOP
212	4999.32	1501628.25	1526881.71	EOP
213	4999.45	1501629.79	1526894.62	EOP
214	4999.45	1501635.34	1526898.99	EOP
215	4999.44	1501637.33	1526898.76	EOP
216	4999.89	1501641.70	1526893.20	EOP
217	4999.72	1501641.28	1526889.67	EOP
218	4999.72	1501607.96	1526863.42	EOP
219	5000.21	1501532.63	1526941.42	EOP

Point Table				
Point #	Elevation	Northing	Eastng	Description
220	5000.76	1501547.85	1526967.81	EOP
221	5001.49	1501540.19	1527004.97	EOP
222	5002.04	1501555.41	1527031.36	EOP
223	5002.80	1501547.75	1527068.52	EOP
224	5003.33	1501562.97	1527094.91	EOP
225	5002.74	1501649.03	1527056.48	EOP
226	5003.30	1501664.25	1527082.87	EOP
227	5001.46	1501641.48	1526992.93	EOP
228	5002.02	1501656.70	1527019.31	EOP
229	5000.18	1501633.92	1526929.37	EOP
230	5000.74	1501649.14	1526995.76	EOP
231	5000.17	1501675.62	1526924.42	EOP
232	5000.73	1501690.85	1526950.80	EOP
233	5001.45	1501683.18	1526987.97	EOP
234	5002.01	1501696.40	1527014.35	EOP
235	5002.73	1501690.74	1527051.52	EOP
236	5003.29	1501705.96	1527077.91	EOP
237	5000.37	1501776.91	1526912.37	EOP
238	5000.76	1501792.13	1526938.76	EOP
239	5001.43	1501784.47	1526975.92	EOP

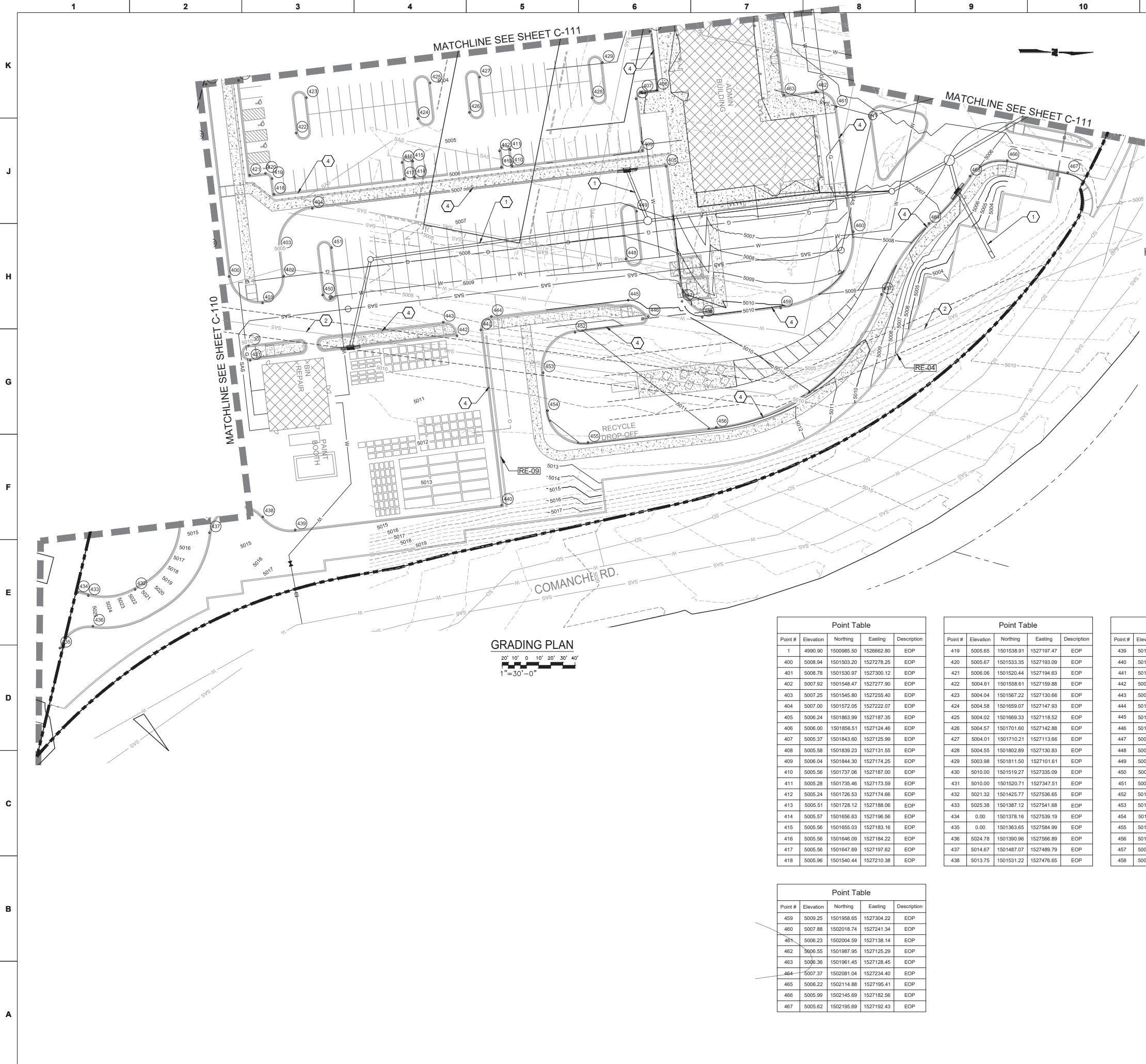
Point Table				
Point #	Elevation	Northing	Eastng	Description
240	5001.98	1501799.69	1527002.31	EOP
241	5002.71	1501792.02	1527039.48	EOP
242	5003.26	1501807.25	1527065.86	EOP
243	5005.45	1501850.73	1527075.85	EOP
244	5003.79	1501843.76	1527017.21	EOP
245	5003.29	1501830.35	1527018.81	EOP
246	5003.00	1501829.29	1527009.87	EOP
247	5003.00	1501842.89	1527008.28	EOP
248	5001.15	1501827.82	1526883.16	EOP
249	5000.87	1501812.92	1526884.93	EOP
250	5000.78	1501809.59	1526882.30	EOP
251	5000.38	1501806.99	1526880.46	EOP
252	4999.24	1501881.87	1526875.33	EOP
253	4999.25	1501883.41	1526888.24	EOP
254	4999.26	1501679.03	1526893.80	EOP
255	4999.76	1501671.49	1526889.66	EOP
256	4999.64	1501671.08	1526886.16	EOP
257	4999.50	1501697.33	1526852.83	EOP
258	4999.27	1501786.31	1526842.27	EOP
259	4999.00	1501829.99	1526823.56	EOP

Point Table				
Point #	Elevation	Northing	Eastng	Description
260	4998.92	1501842.98	1526817.99	EOP
261	4999.82	1501960.64	1526804.01	EOP
262	5000.09	1502034.60	1526808.84	EOP
263	5000.57	1502057.38	1526824.48	EOP
264	5000.51	1502051.50	1526832.04	EOP
265	5001.00	1501962.65	1526820.89	EOP
266	5002.03	1501891.65	1526829.33	EOP
267	5003.23	1501865.40	1526862.66	EOP
268	5004.64	1501871.88	1526917.14	EOP
269	5005.13	1501854.60	1526924.23	EOP
270	5006.25	1501863.45	1526998.71	EOP
271	5006.20	1501874.37	1526997.41	EOP
272	5006.10	1501891.04	1527010.54	EOP
273	5006.05	1501892.57	1527023.45	EOP
274	5006.05	1501941.23	1527017.67	EOP
275	5005.85	1501939.64	1527004.25	EOP
276	5005.90	1501946.59	1527003.43	EOP
277	5005.23	1501942.02	1526969.23	EOP
278	5005.58	1501905.28	1526973.60	EOP
279	5005.48	1501904.69	1526968.63	EOP

Point Table				
Point #	Elevation	Northing	Eastng	Description
280	5005.33	1501920.08	1526966.80	EOP
281	5002.78	1501907.80	1526863.53	EOP
282	5002.67	1501894.23	1526853.69	EOP
283	5002.51	1501926.00	1526861.37	EOP
284	5002.69	1501913.76	1526862.82	EOP
285	5005.28	1501926.04	1526966.09	EOP
286	5005.31	1501996.08	1527047.02	EOP
287	5005.60	1501984.38	1527057.55	EOP
288	5004.94	1502016.51	1527053.66	EOP
289	5005.18	1502002.04	1527046.32	EOP
290	5001.82	1501973.01	1526852.89	EOP
291	5001.73	1501958.54	1526845.55	EOP
292	5001.53	1501982.56	1526843.60	EOP
293	5001.99	1501979.97	1526860.62	EOP
294	5001.22	1502043.82	1526854.80	EOP
295	5001.62	1502043.54	1526870.19	EOP
296	5001.74	1502050.50	1526877.92	EOP
297	5003.94	1502069.56	1527038.29	EOP
298	5004.05	1502063.61	1527039.00	EOP
299	5004.36	1502049.03	1527049.40	EOP

Point Table				
Point #	Elevation	Northing	Eastng	Description
300	5003.97	1502084.19	1527045.22	EOP
301	5004.99	1502026.33	1527082.31	EOP
302	5004.64	1502082.57	1527075.62	EOP
303	5004.59	1502088.12	1527080.00	EOP
304	5004.50	1502089.89	1527094.88	EOP
305	5004.50	1502157.42	1527086.85	EOP
306	5004.10	1502154.96	1527066.16	EOP
307	5003.75	1502165.38	1527050.32	EOP
308	5003.67	1502116.54	1527041.37	EOP
309	5003.52	1502129.15	1527031.21	EOP
310	5003.30	1502146.17	1527017.47	EOP
311	5002.11	1502116.10	1526921.48	EOP
312	5001.59	1502099.85	1526891.73	EOP
313	5000.74	1502091.56	1526853.42	EOP
314	5000.48	1502087.88	1526836.50	EOP
315	5003.95	1502183.83	1527044.56	EOP
316	5004.91	1502171.82	1527105.96	EOP
317	5005.17	1502173.73	1527127.11	EOP
318	0.00	1502170.36	1527131.15	EOP
319	5005.06	1502111.82	1527119.70	EOP

Point Table				
Point #	Elevation	Northing	Eastng	Description
320	5005.24	1502094.44	1527118.36	EOP
321	5005.41	1502077.07	1527117.03	EOP
322	5005.32	1502043.33	1527110.43	EOP
323	5005.15	1502021.15	1527099.96	EOP
324	0.00	1502219.03	1527138.64	EOP
325	0.00	1502207.63	1527136.41	EOP
326	5004.72	1502187.90	1527107.07	EOP
327	5003.79	1502199.53	1527047.64	EOP
328	4999.66	1501958.75	1526788.12	EOP
329	4998.72	1501856.86	1526800.23	EOP
330	4998.32	1501853.94	1526795.70	EOP
331	4997.44	1501868.22	1526759.20	EOP
332	4993.99	1501886.55	1526669.56	EOP
333	4994.06	1501839.32	1526650.94	EOP
334	4997.94	1501819.23	1526749.18	EOP
335	4998.88	1501763.21	1526800.70	EOP



- GENERAL NOTES**
1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
 2. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
 3. ALL DIMENSIONS ARE TO EDGE OF PAVEMENT UNLESS OTHERWISE NOTED.

- KEYED NOTES**
- 1 BUILD STORM DRAIN SYSTEM INFRASTRUCTURE, PER STORM DRAIN PLAN & PROFILE SHEETS C-408 THROUGH C-412
 - 2 EXISTING ABCWUA 48" SANITARY SEWER INTERCEPTOR LINE TO REMAIN. CONTRACTOR SHALL PROTECT LINE.
 - 3 BUILD EXTENSION OF 42" RCP CULVERT-ALAMEDA LATERAL (MRGCD), PER PLAN & PROFILE SHEET C-410.
 - 4 BUILD PCC 6" STD CURB & GUTTER PER COA STD DWG 2415B.
- RE-XX** GARDEN WALLS AND/OR RETAINING WALLS
SEE PLAN & PROFILE SHEETS C-
SEE PLAN & PROFILE SHEETS C-

Project Revision

Rev	Description	Date
1	BID SET	06.17.2020



CITY OF ALBUQUERQUE
PROJECT NO. 700693

MAINTENANCE & ADMINISTRATION BUILDING PROJECT
4600 EDITH BLVD NE
ALBUQUERQUE, NM 87107



ONE ALBUQUE RQUE

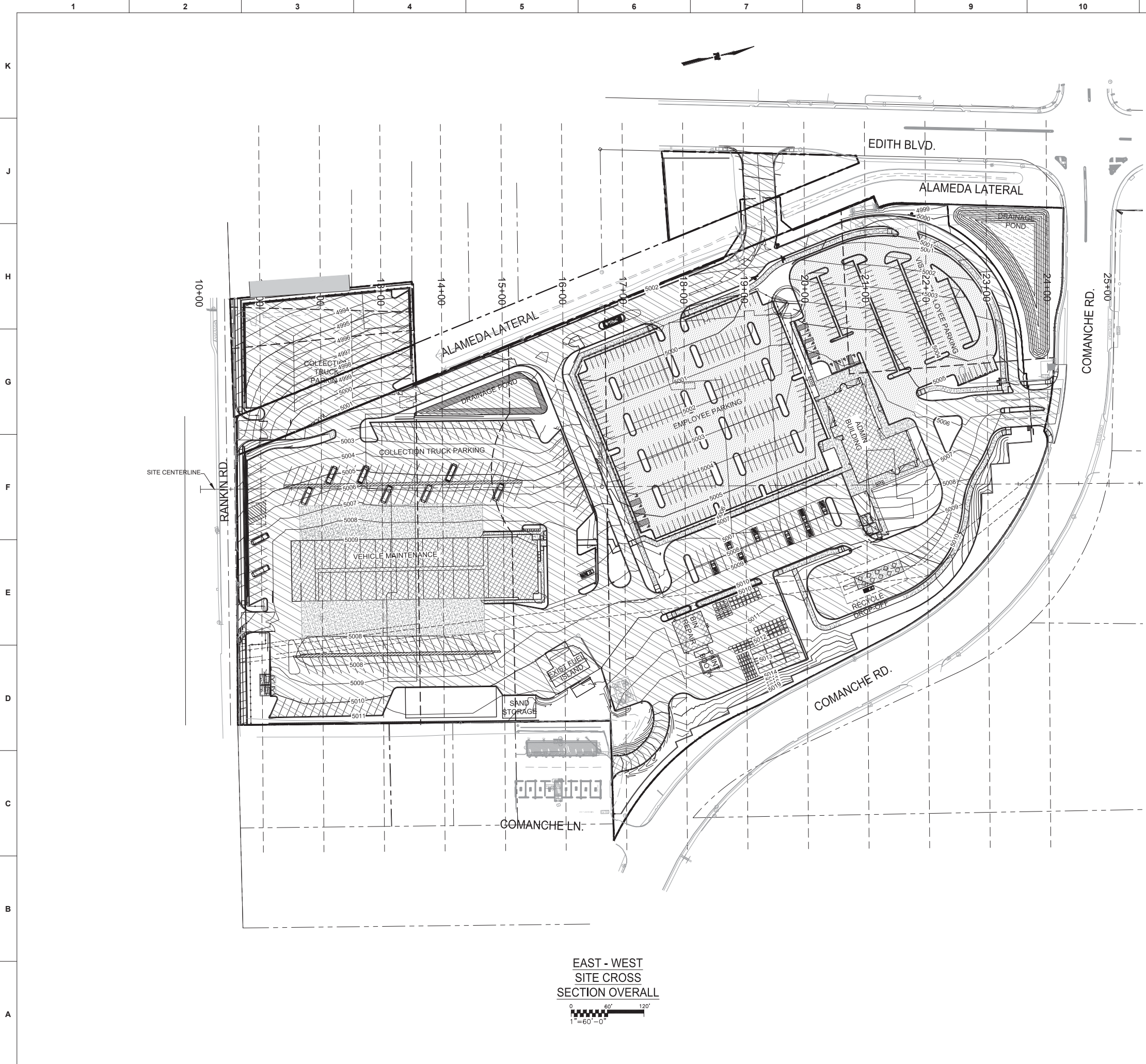


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GRADING PLAN

AS NOTED	AS NOTED
DATE	SCALE
DWG	SGG
DWN	CHK

JRMA Project No.
4907-B
W&C - 14-100-132-01
C-112



- GENERAL NOTES
1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
 2. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
 3. ALL DIMENSIONS ARE TO FACE OF CURB UNLESS OTHERWISE NOTED.

Project Revision	
Δ BID SET	06.17.2020



CITY OF
ALBUQUERQUE
PROJECT NO. 700693

MAINTENANCE &
ADMINISTRATION
BUILDING PROJECT
4600 EDITH BLVD NE
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EAST - WEST
SITE CROSS
SECTION
OVERALL

AS NOTED	AS NOTED
DATE	SCALE
DWN	CHK

JRMA Project No.
4907-B
W&C - 14-100-132-01
C-302

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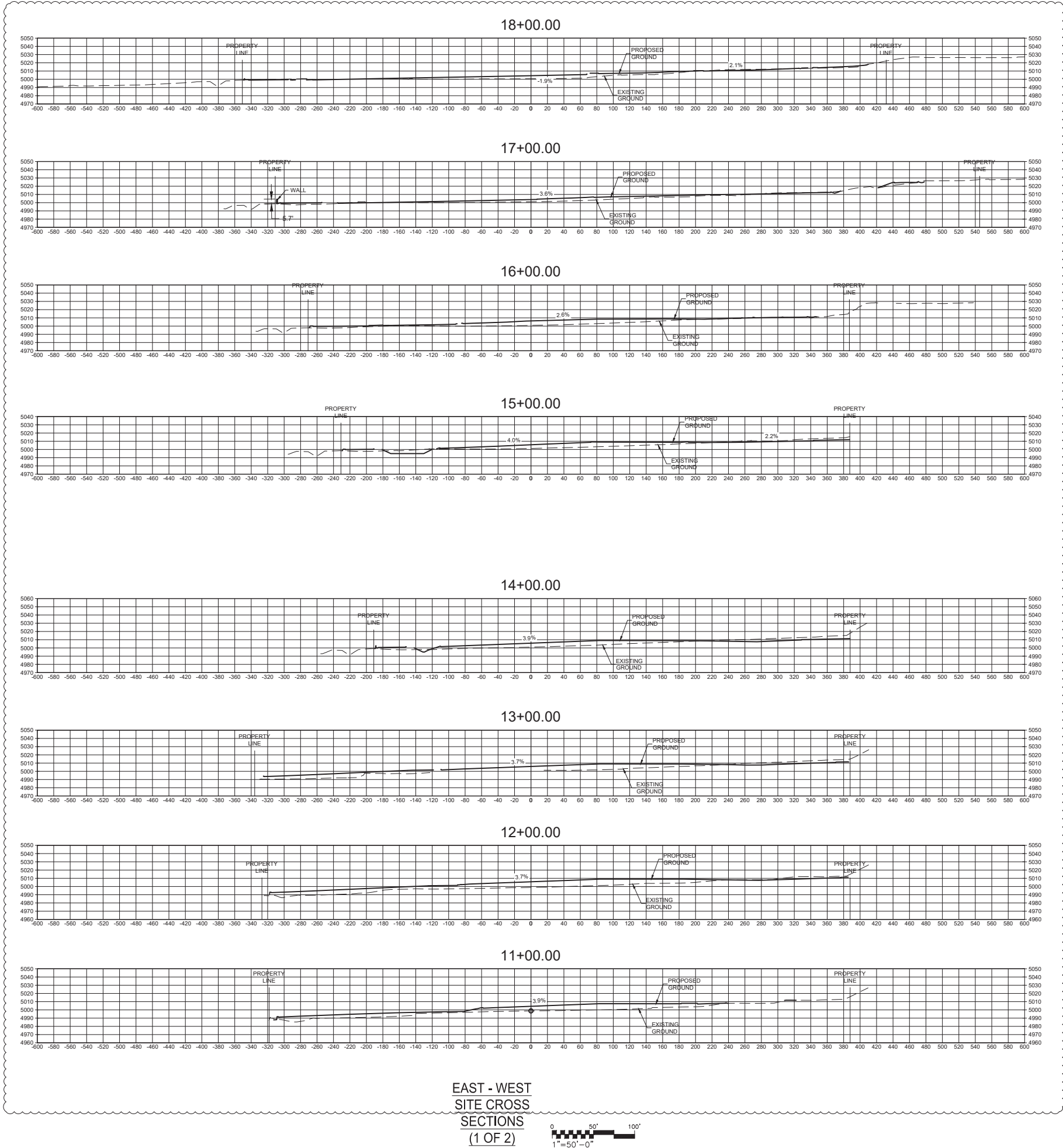
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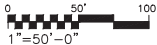
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B

A



EAST - WEST
SITE CROSS
SECTIONS
(1 OF 2)



GENERAL NOTES

1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
2. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
3. ALL DIMENSIONS ARE TO FACE OF CURB UNLESS OTHERWISE NOTED.

Project Revision

BID SET 06.17.2020



CITY OF
ALBUQUERQUE
PROJECT NO. 700693

MAINTENANCE &
ADMINISTRATION
BUILDING PROJECT
4600 EDITH BLVD NE
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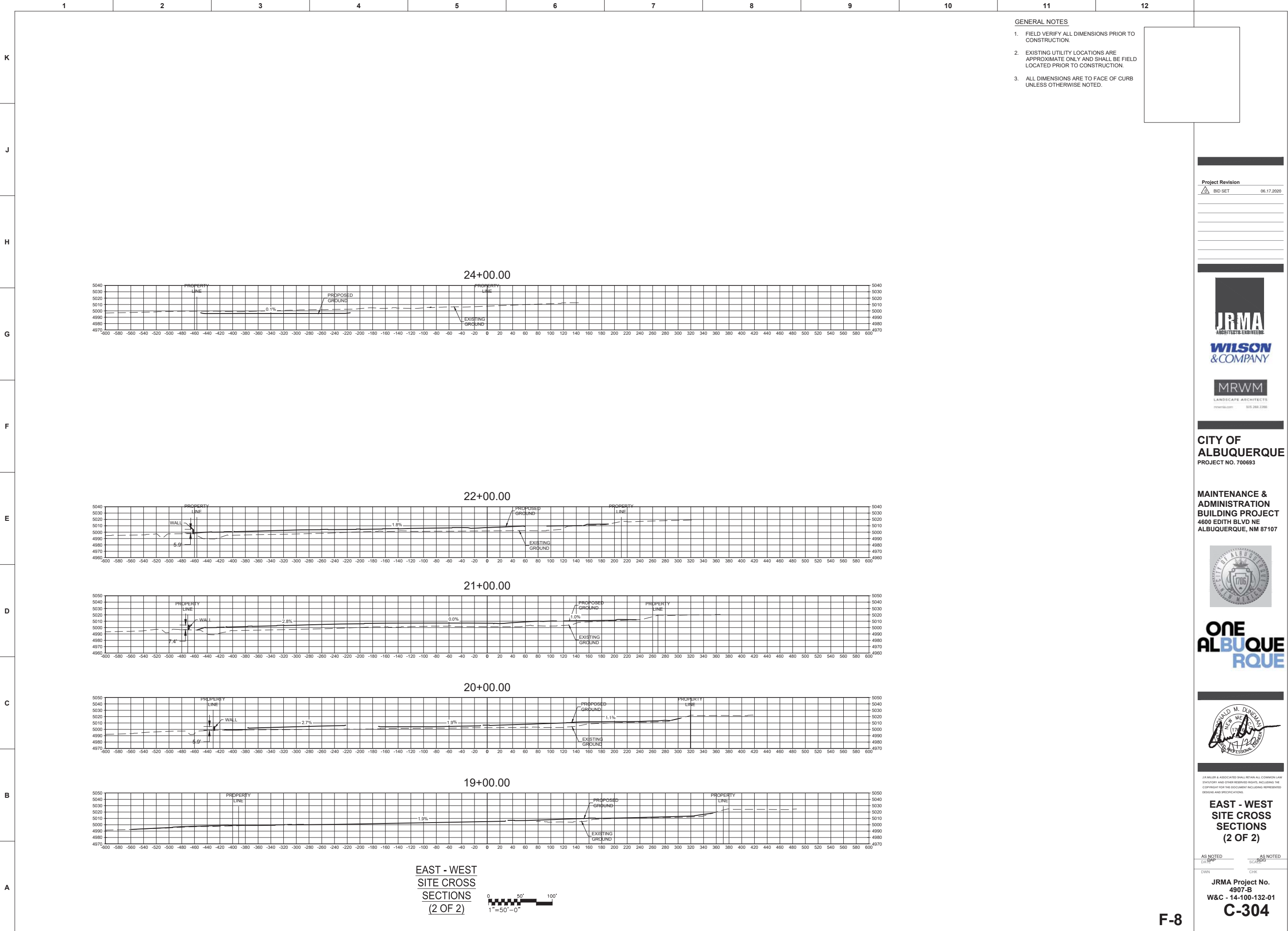
EAST - WEST
SITE CROSS
SECTIONS
(1 OF 2)

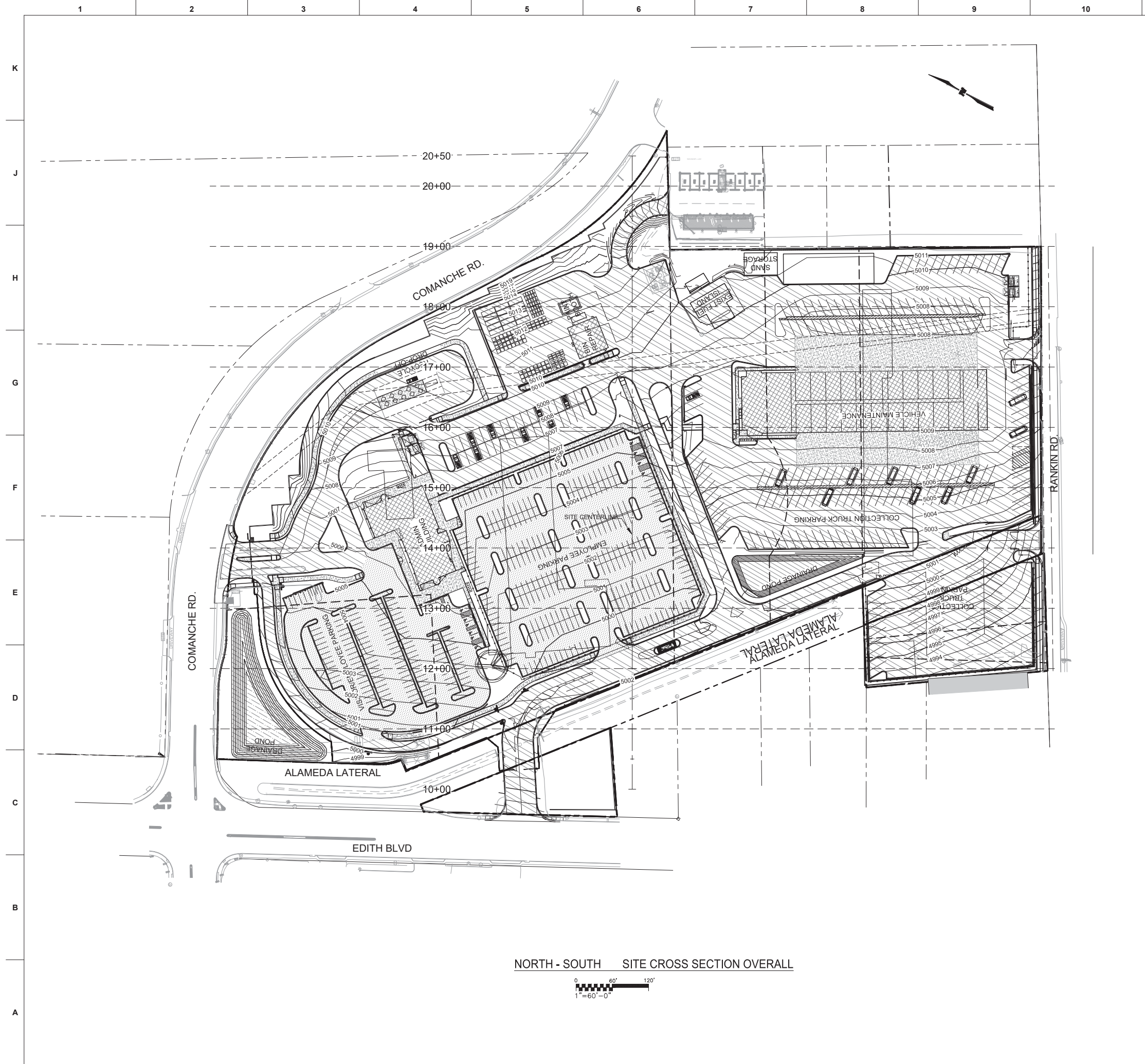
AS NOTED
DATE: DAP
DWN: CHK

AS NOTED
SCALE: SGG
CHK

JRMA Project No.
4907-B
W&C - 14-100-132-01

C-303





- GENERAL NOTES
1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
 2. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
 3. ALL DIMENSIONS ARE TO FACE OF CURB UNLESS OTHERWISE NOTED.

Project Revision	
△ BID SET	06.17.2020



CITY OF ALBUQUERQUE
PROJECT NO. 700693

MAINTENANCE & ADMINISTRATION BUILDING PROJECT
4600 EDITH BLVD NE
ALBUQUERQUE, NM 87107



ONE ALBUQUE RQUE

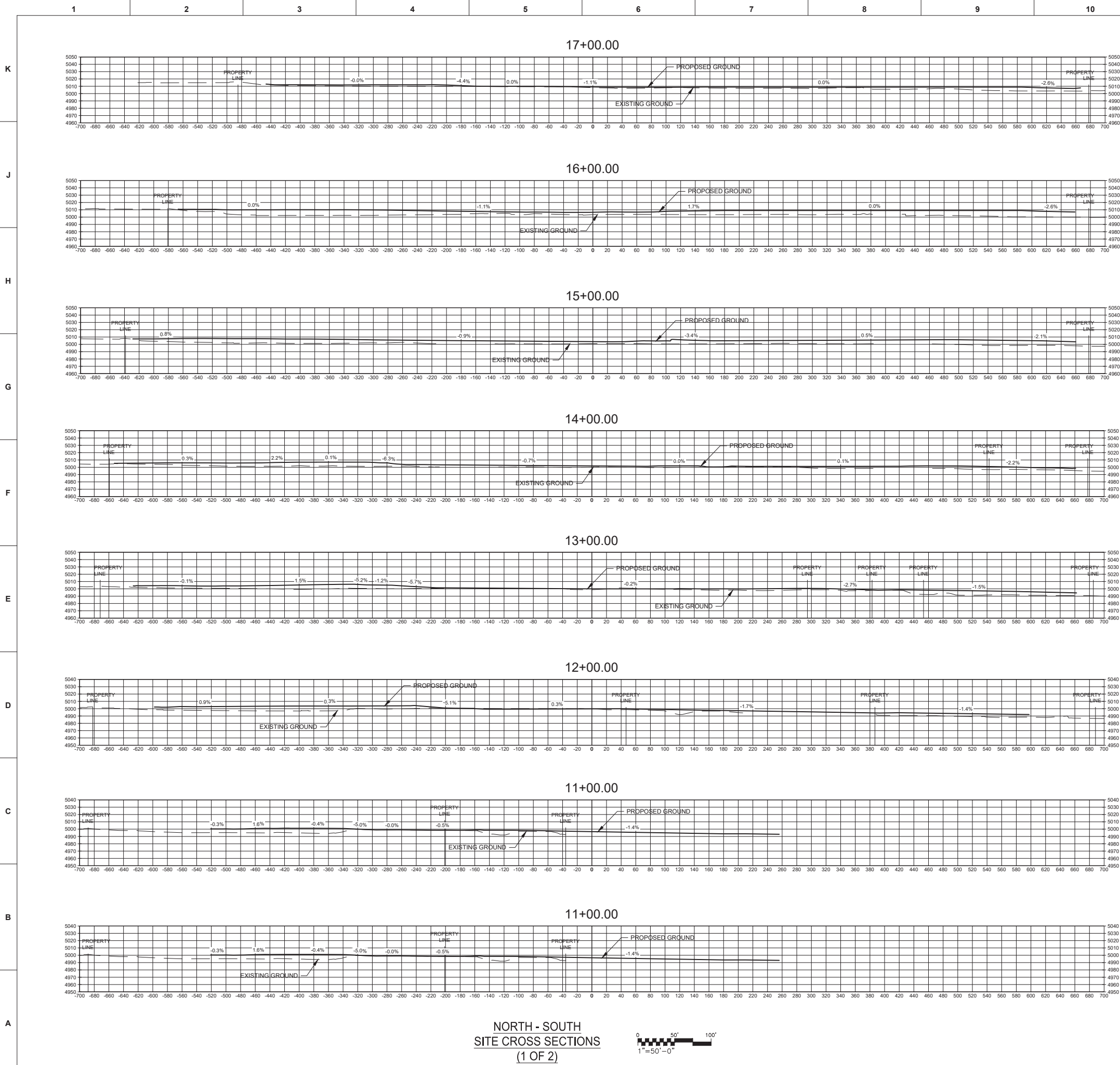


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NORTH - SOUTH
SITE CROSS
SECTION
OVERALL

AS NOTED DATE: 06/17/2020	AS NOTED SCALE: 1"=60'-0"
DWN	CHK

JRMA Project No. 4907-B
W&C - 14-100-132-01
C-305



- GENERAL NOTES**
1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
 2. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
 3. ALL DIMENSIONS ARE TO FACE OF CURB UNLESS OTHERWISE NOTED.

Project Revision

Rev	Description	Date
1	BID SET	06.17.2020



CITY OF ALBUQUERQUE
PROJECT NO. 700693

MAINTENANCE & ADMINISTRATION BUILDING PROJECT
4600 EDITH BLVD NE
ALBUQUERQUE, NM 87107

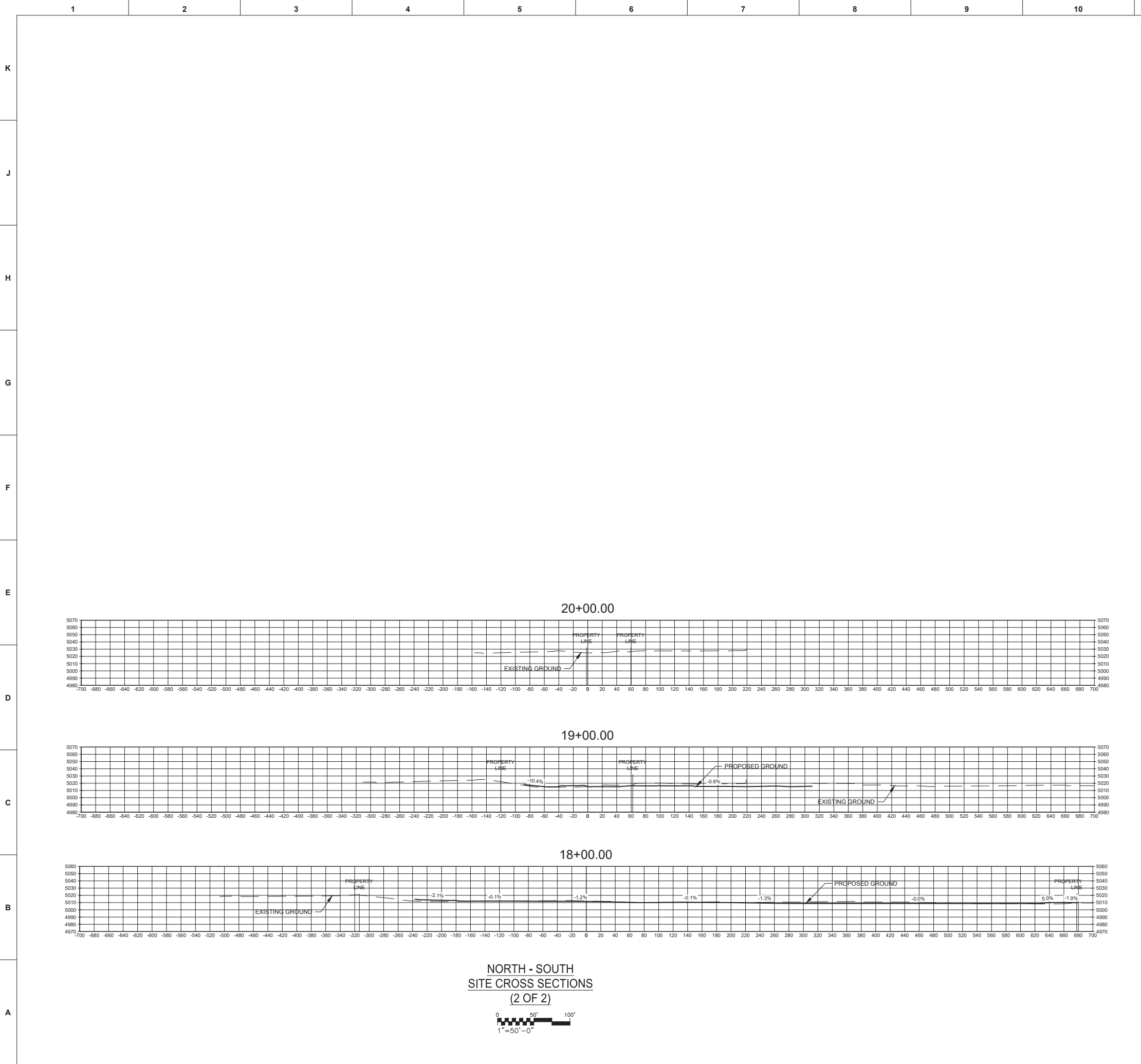


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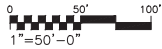
NORTH - SOUTH SITE CROSS SECTIONS (1 OF 2)

AS NOTED	AS NOTED
DATE: DAP	SCALE: SGG
DWN	CHK

JRMA Project No. 4907-B
W&C - 14-100-132-01
C-306



NORTH - SOUTH
SITE CROSS SECTIONS
(2 OF 2)



GENERAL NOTES

1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
2. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
3. ALL DIMENSIONS ARE TO FACE OF CURB UNLESS OTHERWISE NOTED.

Project Revision

BID SET 06.17.2020



CITY OF
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PROJECT NO. 700693

MAINTENANCE &
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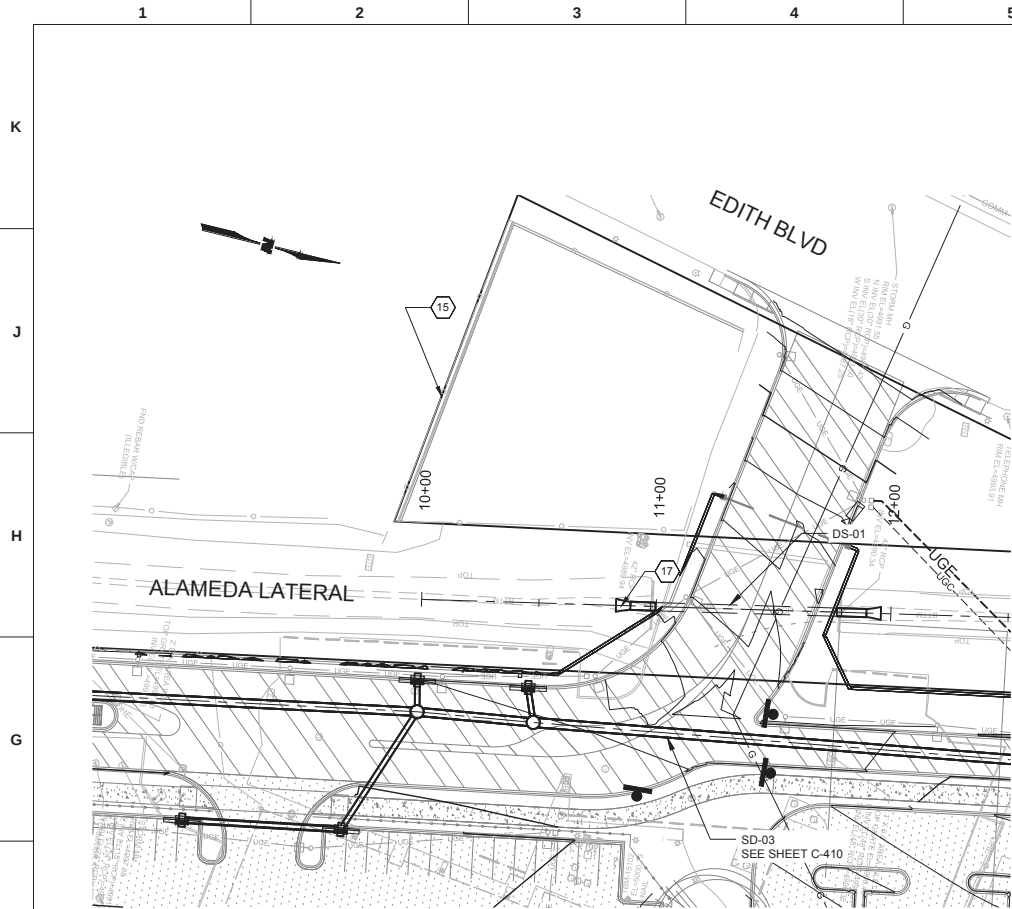
NORTH - SOUTH
SITE CROSS
SECTIONS
(2 OF 2)

AS NOTED
DATE: DAP
DWN

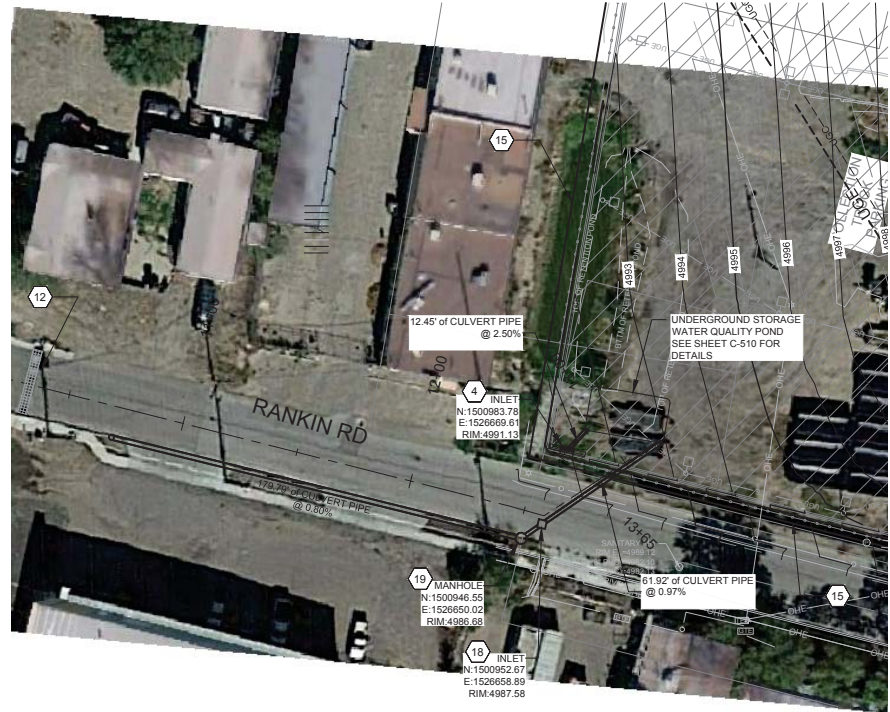
AS NOTED
SCALE: SGG
CHK

JRMA Project No.
4907-B
W&C - 14-100-132-01

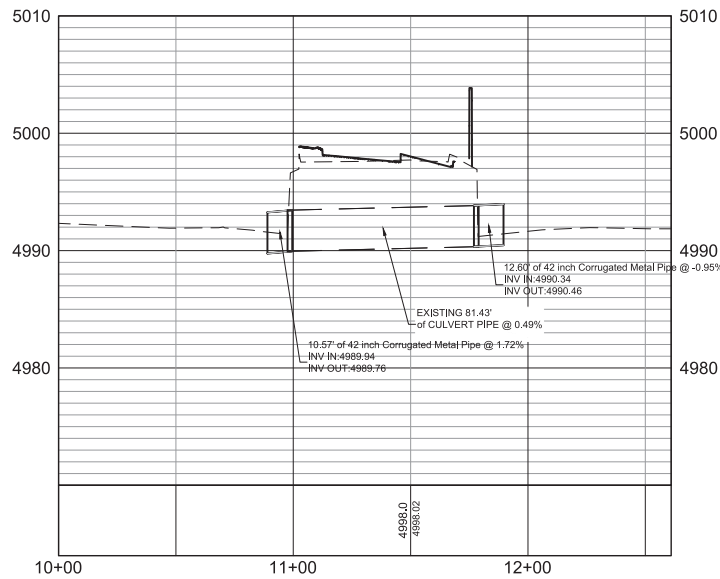
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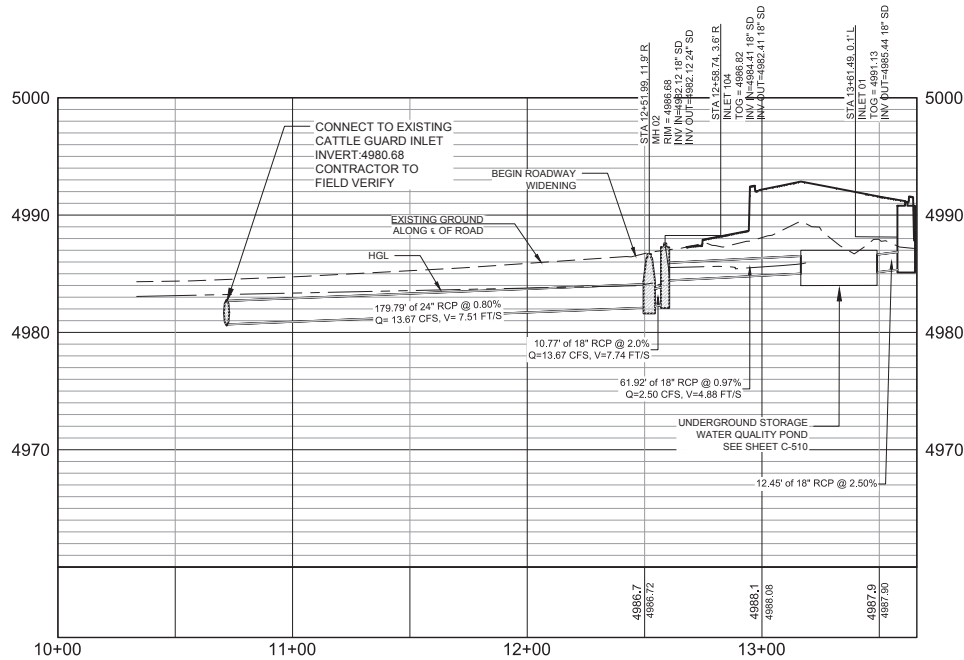
DS-01 DRAIN STRUCTURE PLAN
SEE SHEET C-109 FOR LOCATION



SD-01 STORM DRAIN PLAN
SEE SHEET C-109 FOR LOCATION
NOTE: RANKIN STORM DRAIN SHOWN FOR INFORMATION ONLY. SEE WORK ORDER PLANS PROJECT NUMBER 7006.92.



ALAMEDA LATERAL
DS-01 DRAIN STRUCTURE PPROFILE



SD-01 DRAIN STRUCTURE PPROFILE

- GENERAL NOTES
1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
 2. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
 3. ALL DIMENSIONS ARE TO FACE OF CURB UNLESS OTHERWISE NOTED.

KEYED NOTES

- * 1 BUILD 4' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
- * 2 BUILD 6' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
- * 3 BUILD 8' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
- * 4 BUILD STORM DRAIN INLET, TYPE "C" PER COA STD DWG 2205
- * 5 BUILD STORM DRAIN INLET, TYPE "A" PER COA STD DWG 2201
- * 6 BUILD STORM DRAIN INLET, SINGLE, TYPE "D" PER COA STD DWG 2206
- * 7 BUILD STORM DRAIN INLET, MEDIAN STORM INLET PER COA STD DWG 2273
- * 8 DRAINAGE POND - SEE GRADING PLAN AND SHEET C-510 FOR DETAILS
- * 9 EXISTING STORM DRAIN INLET TO REMAIN IN PLACE
- * 10 EXISTING STORM DRAIN MANHOLE TO REMAIN IN PLACE
- * 11 ADJUST EXISTING MANHOLE TO GRADE
- * 12 BUILD SIDEWALK CULVERT WITH STEEL GRATE PER COA STD DWG 2236
- * 13 PROPOSED SAS LINE. SEE SHEETS C-404, C-405, AND C-406 FOR PLAN & PROFILES AND ADDITIONAL DETAILS.
- * 14 PROPOSED WATER LINE. SEE SHEETS C-406 & C-407 FOR PLAN & PROFILES AND ADDITIONAL DETAILS.
- 15 PROPERTY LINE
- * 16 6" ROOF DRAIN PIPE
- 17 EXTEND EXISTING 42" CULVERT
- 18 INSTALL 1 - TYPE 'D' SINGLE INLET PER COA STD DWG 2206
- 19 INSTALL 1 - 6' DIA TYPE 'C' STORM MANHOLE PER COA STD DWG 2208
- * NOT USED ON THIS SHEET

Project Revision
BID SET 06.17.2020

JRMA
ARCHITECTS-ENGINEERS

WILSON
& COMPANY

MRWM
LANDSCAPE ARCHITECTS

CITY OF
ALBUQUERQUE
PROJECT NO. 700693

MAINTENANCE &
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BUILDING PROJECT
4600 EDITH BLVD NE
ALBUQUERQUE, NM 87107



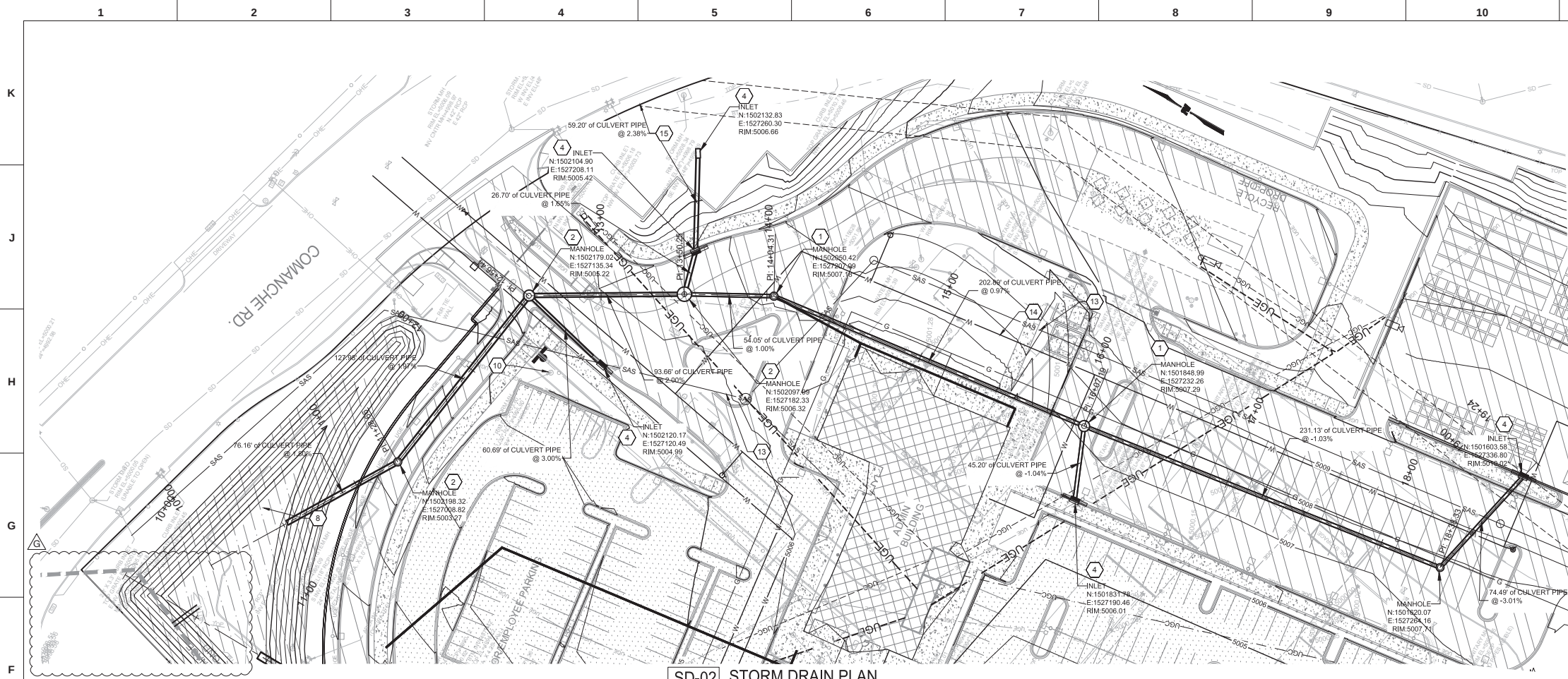
ONE
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Professional Engineer
New Mexico
17122

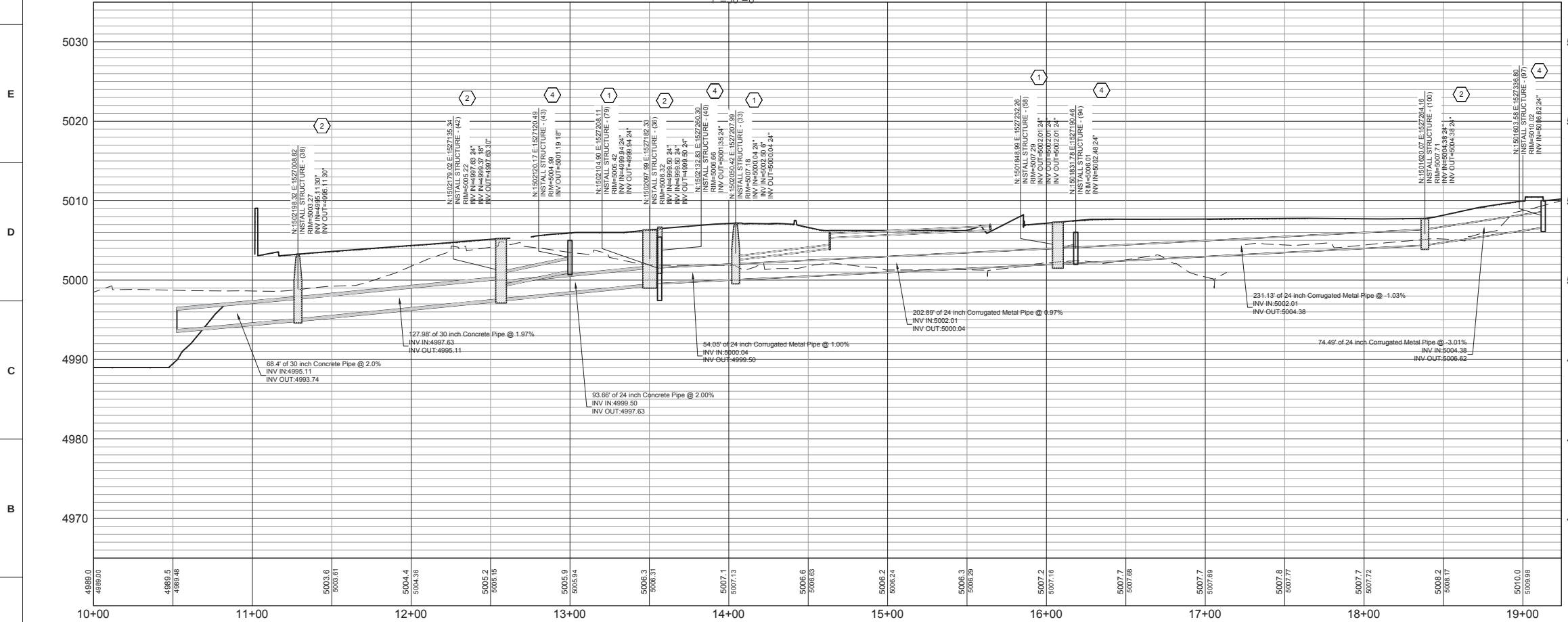
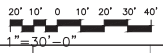
STORM DRAIN
PLAN & PROFILE
SD-01

AS NOTED
DATE
DWN
CHK

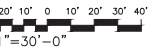
JRMA Project No.
4907-B
W&C - 14-100-132-01
C-408



SD-02 STORM DRAIN PLAN



SD-02 STORM DRAIN PROFILE



- GENERAL NOTES
1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
 2. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
 3. ALL DIMENSIONS ARE TO FACE OF CURB UNLESS OTHERWISE NOTED.

- KEYED NOTES
- 1 BUILD 4' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
 - 2 BUILD 6' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
 - * 3 BUILD 8' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
 - * 4 BUILD STORM DRAIN INLET, TYPE "A" PER COA STD DWG 2205
 - * 5 BUILD STORM DRAIN INLET, TYPE "C" PER COA STD DWG 2205
 - * 6 BUILD STORM DRAIN INLET, SINGLE, TYPE "D" PER COA STD DWG 2206
 - 7 BUILD STORM DRAIN INLET, DOUBLE, TYPE "C" PER COA STD DWG 2205
 - 8 DRAINAGE POND - SEE GRADING PLAN AND SHEET C-505 FOR DETAILS
 - * 9 EXISTING STORM DRAIN INLET TO REMAIN IN PLACE
 - 10 EXISTING STORM DRAIN MANHOLE TO REMAIN IN PLACE
 - * 11 ADJUST EXISTING MANHOLE TO GRADE
 - 12 BUILD SIDEWALK CULVERT WITH STEEL GRATE PER COA STD DWG 2236
 - 13 PROPOSED SAS LINE. SEE SHEETS C-404, C-405, AND C-406 FOR PLAN & PROFILES AND ADDITIONAL DETAILS.
 - 14 PROPOSED WATER LINE. SEE SHEETS C-406 & C-407 FOR PLAN & PROFILES AND ADDITIONAL DETAILS.
 - 15 PROPERTY LINE
 - * 16 6" ROOF DRAIN PIPE
 - * 17 BUILD PRINCIPAL SPILLWAY STRUCTURE PER SHEET C-502
 - * NOT USED ON THIS SHEET

Project Revision

BID SET	06.17.2020
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CITY OF ALBUQUERQUE
PROJECT NO. 700693

MAINTENANCE & ADMINISTRATION
BUILDING PROJECT
4600 EDITH BLVD NE
ALBUQUERQUE, NM 87107



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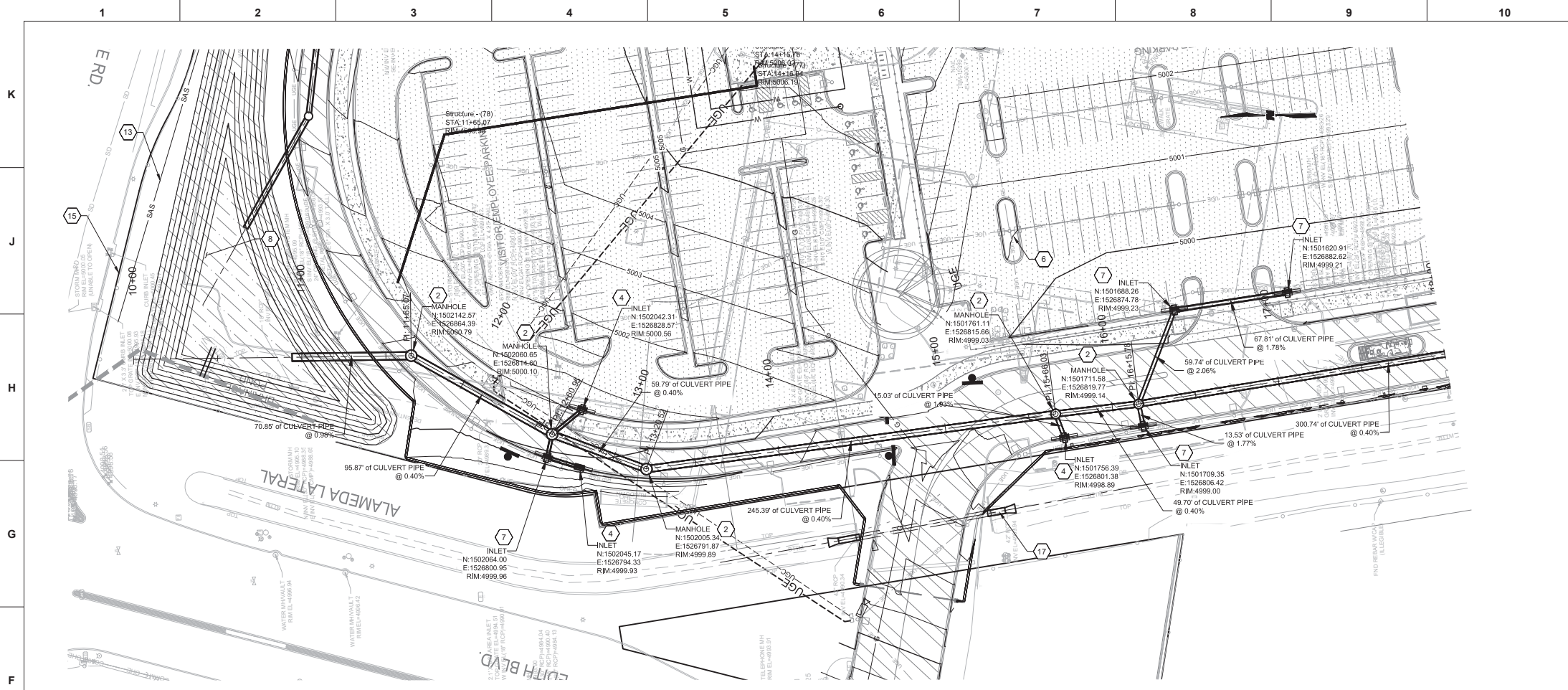


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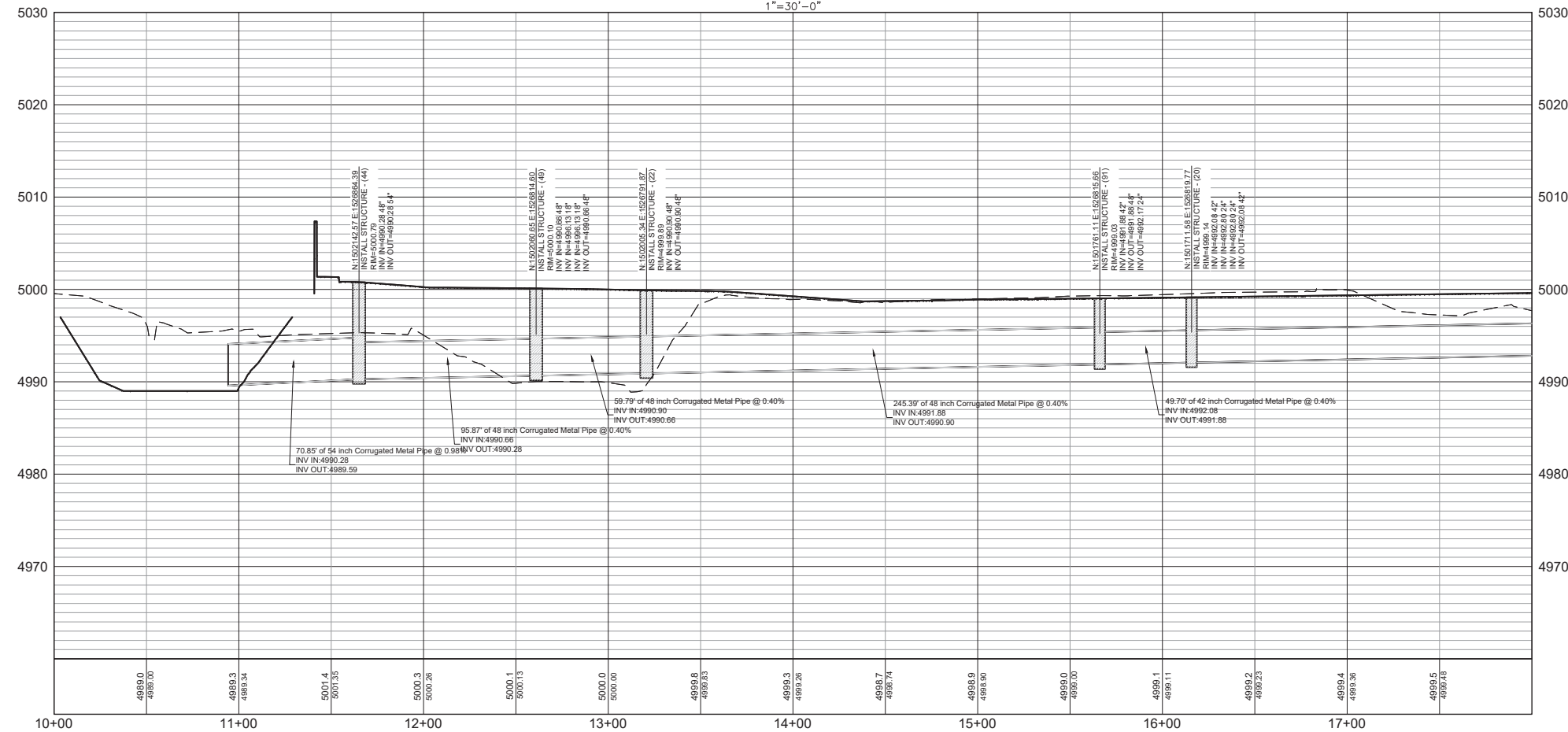
STORM DRAIN
PLAN & PROFILE
SD-02

AS NOTED	AS NOTED
DATE	SCALE
DWN	CHK

JRMA Project No.
4907-B
W&C - 14-100-132-01
C-409



SD-03 STORM DRAIN PLAN



SD-03 STORM DRAIN PROFILE

- GENERAL NOTES
1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
 2. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
 3. ALL DIMENSIONS ARE TO FACE OF CURB UNLESS OTHERWISE NOTED.

- KEYED NOTES
- 1 BUILD 4' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
 - 2 BUILD 6' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
 - * 3 BUILD 8' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
 - 4 BUILD STORM DRAIN INLET, TYPE "C" PER COA STD DWG 2205
 - 5 BUILD STORM DRAIN INLET, TYPE "A" PER COA STD DWG 2201
 - 6 BUILD STORM DRAIN INLET, SINGLE, TYPE "D" PER COA STD DWG 2206
 - 7 BUILD STORM DRAIN INLET, DOUBLE, TYPE "C" PER COA STD DWG 2205
 - 8 DRAINAGE POND - SEE GRADING PLAN AND SHEET C-505 FOR DETAILS
 - * 9 EXISTING STORM DRAIN INLET TO REMAIN IN PLACE
 - * 10 EXISTING STORM DRAIN MANHOLE TO REMAIN IN PLACE
 - * 11 ADJUST EXISTING MANHOLE TO GRADE
 - * 12 BUILD SIDEWALK CULVERT WITH STEEL GRATE PER COA STD DWG 2236
 - 13 PROPOSED SAS LINE. SEE SHEETS C-404, C-405, AND C-406 FOR PLAN & PROFILES AND ADDITIONAL DETAILS.
 - * 14 PROPOSED WATER LINE. SEE SHEETS C-406 & C-407 FOR PLAN & PROFILES AND ADDITIONAL DETAILS.
 - 15 PROPERTY LINE
 - * 16 6" ROOF DRAIN PIPE
 - 17 EXTEND EXISTING 42" CULVERT PER SHEET C-408
- * NOT USED ON THIS SHEET

Project Revision
BID SET 06.17.2020



CITY OF ALBUQUERQUE
PROJECT NO. 700693

MAINTENANCE & ADMINISTRATION
BUILDING PROJECT
4600 EDITH BLVD NE
ALBUQUERQUE, NM 87107

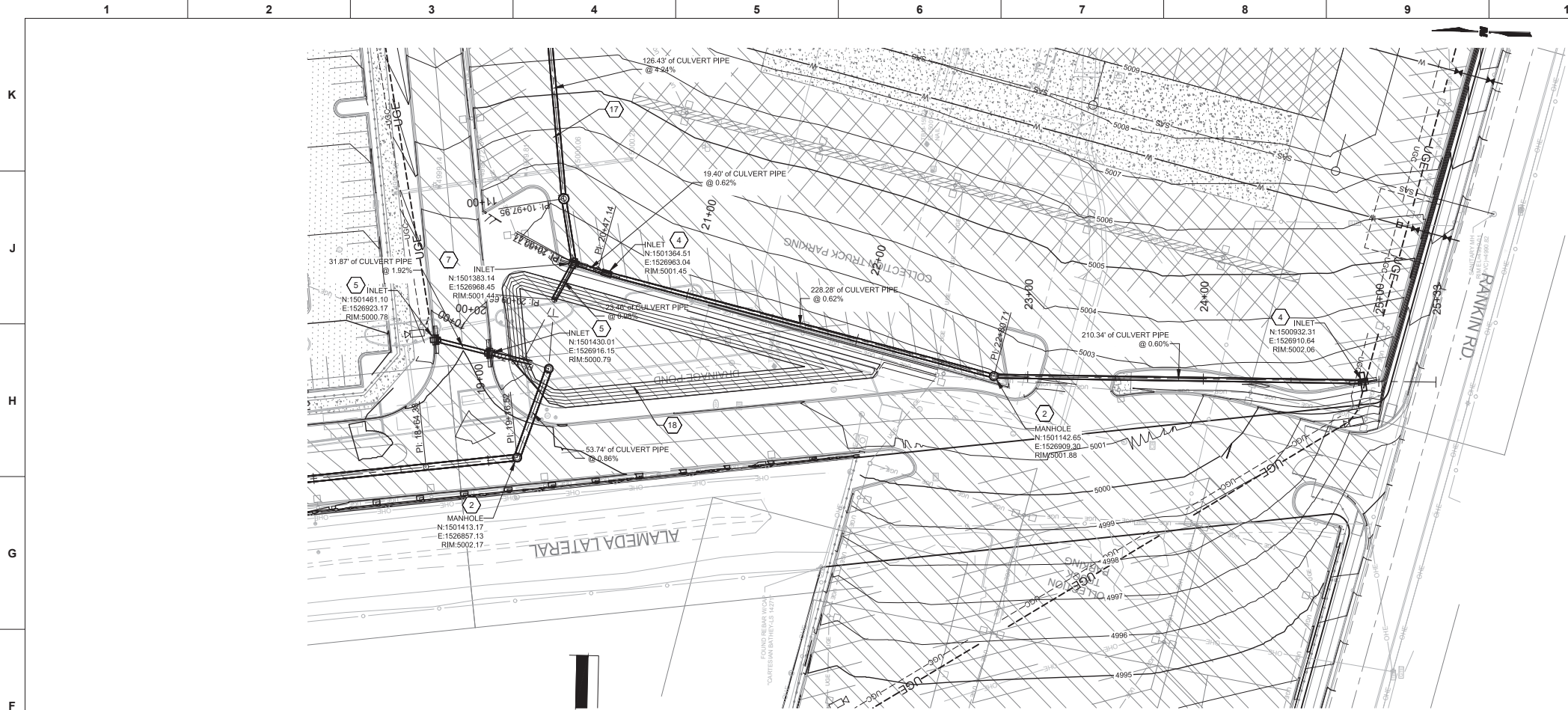


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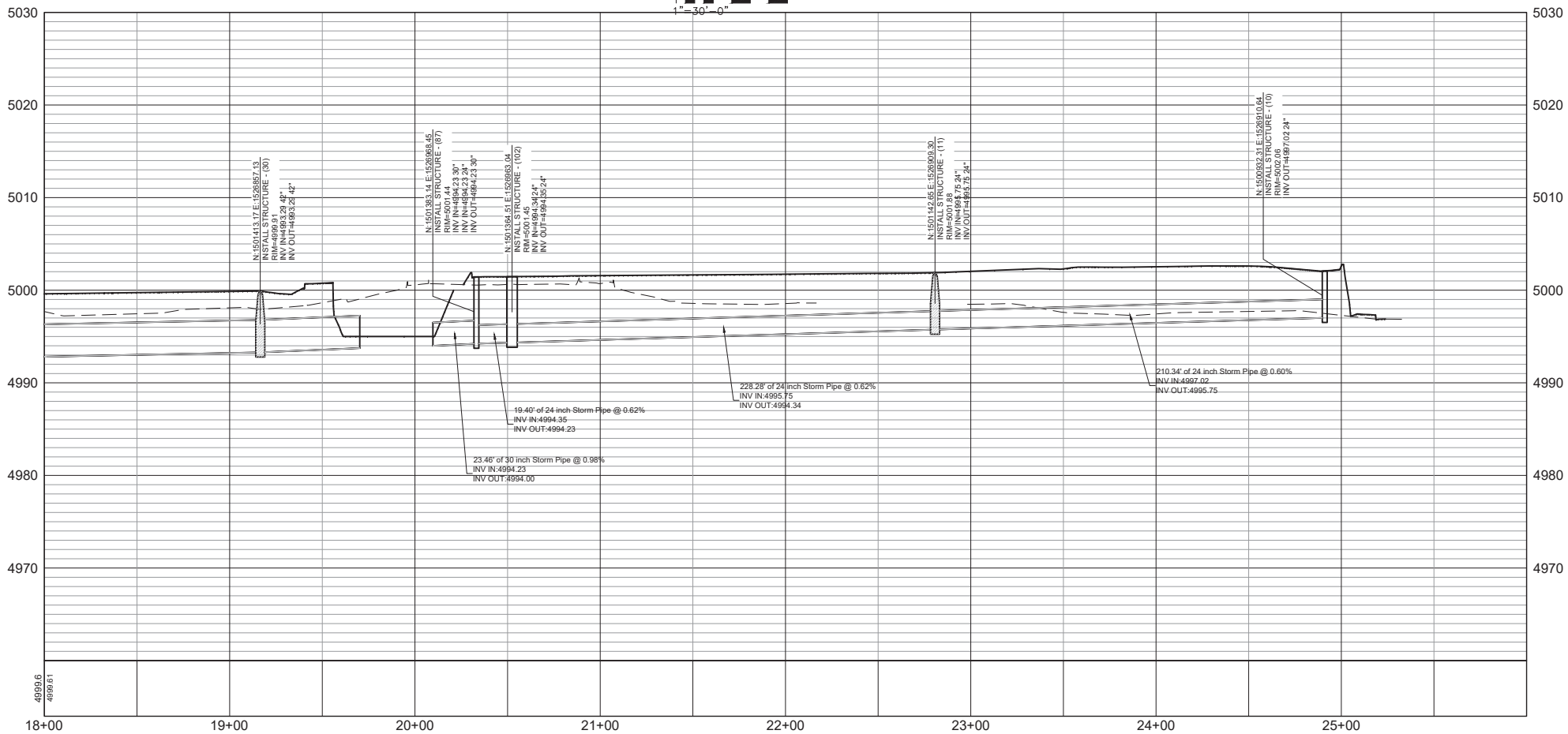
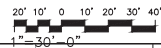


STORM DRAIN
PLAN & PROFILE
SD-03 (1 OF 2)

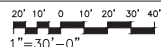
AS NOTED
DATE
DWG
JRMA Project No. 4907-B
W&C - 14-100-132-01
C-410



SD-03 STORM DRAIN PLAN



SD-03 STORM DRAIN PROFILE



GENERAL NOTES

1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
2. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
3. ALL DIMENSIONS ARE TO FACE OF CURB UNLESS OTHERWISE NOTED.

KEYED NOTES

- 1 BUILD 4' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
 - 2 BUILD 6' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
 - * 3 BUILD 8' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
 - 4 BUILD STORM DRAIN INLET, TYPE "C" PER COA STD DWG 2205
 - 5 BUILD STORM DRAIN INLET, TYPE "A" PER COA STD DWG 2201
 - * 6 BUILD STORM DRAIN INLET, SINGLE, TYPE "D" PER COA STD DWG 2206
 - 7 BUILD STORM DRAIN INLET, DOUBLE, TYPE "C" PER COA STD DWG 2205
 - * 8 DRAINAGE POND - SEE GRADING PLAN AND SHEET C-505 FOR DETAILS
 - * 9 EXISTING STORM DRAIN INLET TO REMAIN IN PLACE
 - * 10 EXISTING STORM DRAIN MANHOLE TO REMAIN IN PLACE
 - * 11 ADJUST EXISTING MANHOLE TO GRADE
 - * 12 BUILD SIDEWALK CULVERT WITH STEEL GRATE PER COA STD DWG 2236
 - * 13 PROPOSED SAS LINE. SEE SHEETS C-404, C-405, AND C-406 FOR PLAN & PROFILES AND ADDITIONAL DETAILS.
 - * 14 PROPOSED WATER LINE. SEE SHEETS C-406 & C-407 FOR PLAN & PROFILES AND ADDITIONAL DETAILS.
 - * 15 PROPERTY LINE
 - * 16 6" ROOF DRAIN PIPE
 - 17 SEE SHEET C-412 FOR INFORMATION
 - 18 BUILD PRINCIPAL SPILLWAY STRUCTURE PER SHEET C-502
- * NOT USED ON THIS SHEET

Project Revision

BID SET 06.17.2020



CITY OF ALBUQUERQUE
PROJECT NO. 700693

MAINTENANCE & ADMINISTRATION
BUILDING PROJECT
4600 EDITH BLVD NE
ALBUQUERQUE, NM 87107



ONE ALBUQUE RQUE



STORM DRAIN
PLAN & PROFILE
SD-03 (2 OF 2)

AS NOTED DATE DWN

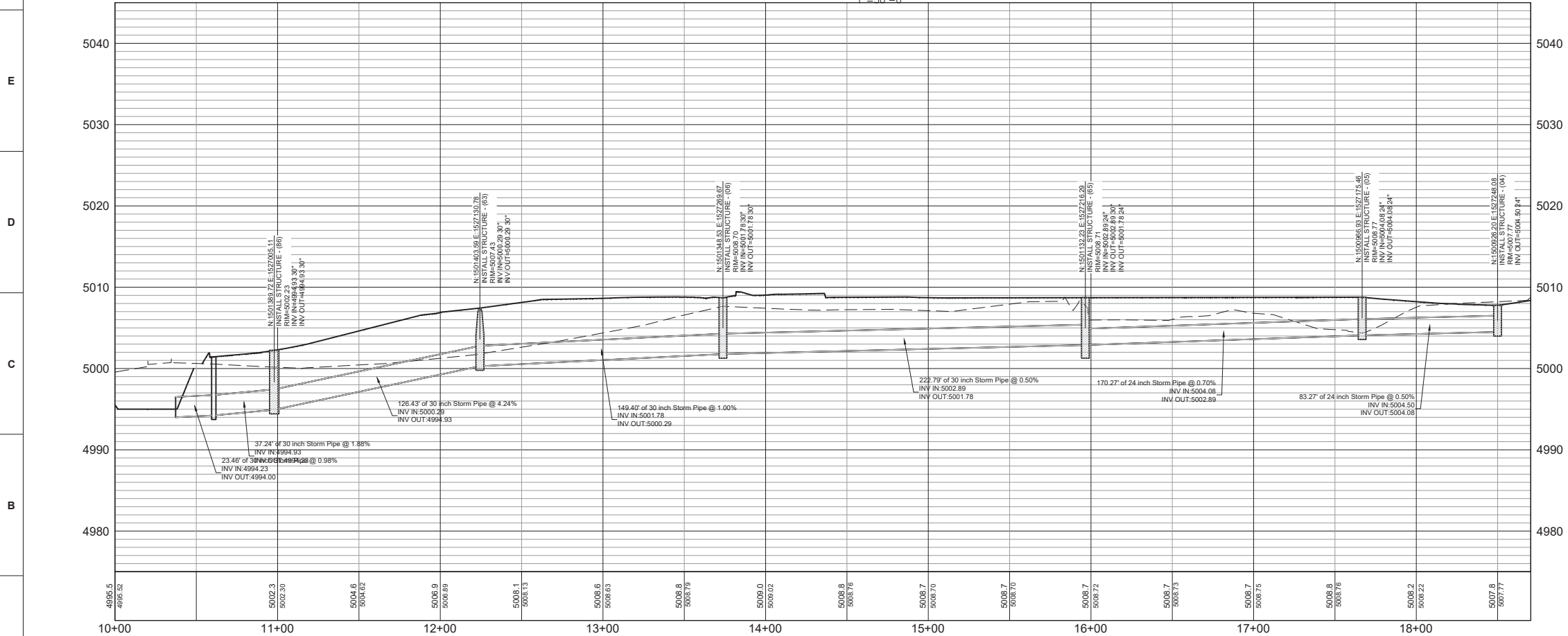
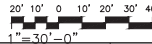
AS NOTED SCALE CHK

JRMA Project No. 4907-B
W&C - 14-100-132-01

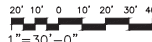
C-411



SD-04 STORM DRAIN PLAN



SD-04 STORM DRAIN PROFILE



GENERAL NOTES

1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
2. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
3. ALL DIMENSIONS ARE TO FACE OF CURB UNLESS OTHERWISE NOTED.

KEYED NOTES

- 1 BUILD 4' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
- 2 BUILD 6' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
- * 3 BUILD 8' DIA. MANHOLE TYPE "C" PER COA STD DWG 2208
- 4 BUILD STORM DRAIN INLET, TYPE "C" PER COA STD DWG 2205
- 5 BUILD STORM DRAIN INLET, TYPE "A" PER COA STD DWG 2201
- 6 BUILD STORM DRAIN INLET, DOUBLE, TYPE "D" PER COA STD DWG 2206
- 7 BUILD STORM DRAIN INLET, DOUBLE, TYPE "C" PER COA STD DWG 2205
- 8 DRAINAGE POND - SEE GRADING PLAN AND SHEET C-502 FOR DETAILS
- * 9 EXISTING STORM DRAIN INLET TO REMAIN IN PLACE
- * 10 EXISTING STORM DRAIN MANHOLE TO REMAIN IN PLACE
- * 11 ADJUST EXISTING MANHOLE TO GRADE
- * 12 BUILD SIDEWALK CULVERT WITH STEEL GRATE PER COA STD DWG 2236
- 13 PROPOSED SAS LINE. SEE SHEETS C-404, C-405, AND C-406 FOR PLAN & PROFILES AND ADDITIONAL DETAILS.
- 14 PROPOSED WATER LINE. SEE SHEETS C-406 & C-407 FOR PLAN & PROFILES AND ADDITIONAL DETAILS.
- 15 PROPERTY LINE
- * 16 6" ROOF DRAIN PIPE
- * NOT USED ON THIS SHEET

Project Revision

BID SET	06.17.2020
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CITY OF ALBUQUERQUE
PROJECT NO. 700693

MAINTENANCE & ADMINISTRATION
BUILDING PROJECT
4600 EDITH BLVD NE
ALBUQUERQUE, NM 87107



ONE ALBUQUE RQUE



STORM DRAIN PLAN & PROFILE
SD-04

AS NOTED DATE: 06/17/2020

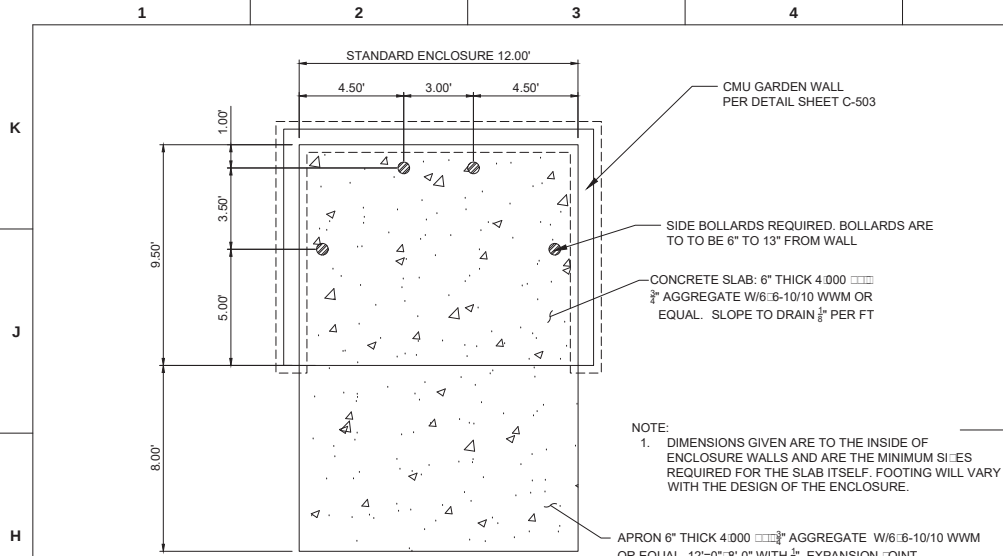
AS NOTED SCALE: 1"=30'-0"

DWN: [Signature] CHK: [Signature]

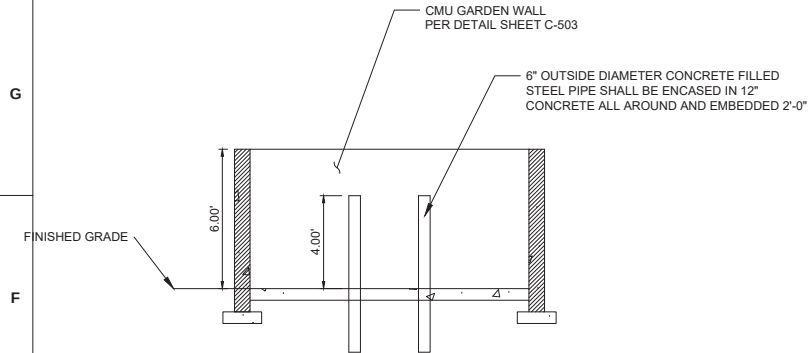
JRMA Project No. 4907-B

W&C - 14-100-132-01

C-412



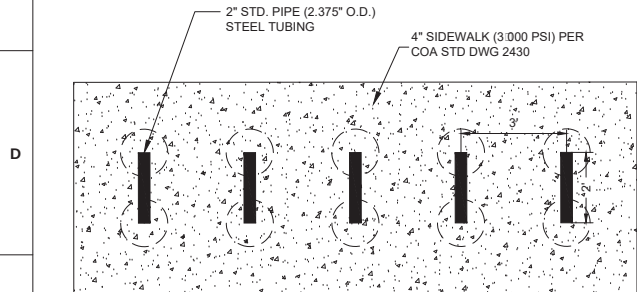
PLAN VIEW



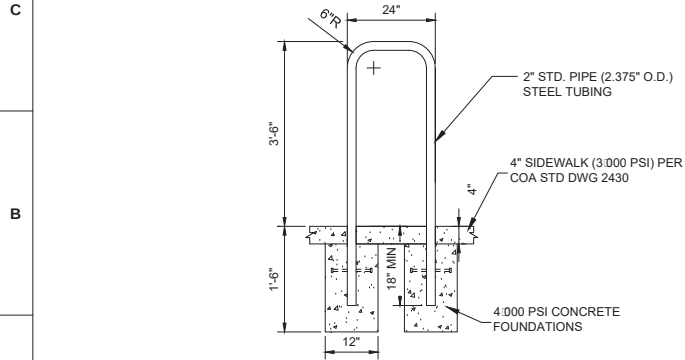
SECTION VIEW

TRASH ENCLOSURE DETAIL

SCALE: NONE



PLAN VIEW

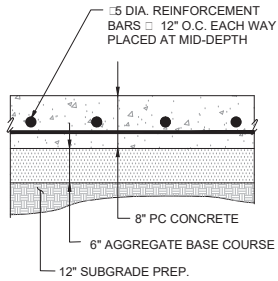


SECTION VIEW

BICYCLE RACK DETAILS

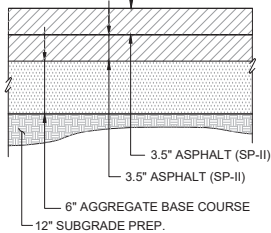
SCALE: NONE

1. POST PAINT SHALL BE SHERWIN WILLIAMS 6069 FRENCH ROAST OR APPROVED EQUAL



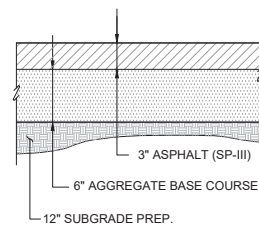
RIGID PAVEMENT SECTION - 8" CONCRETE PAVEMENT

SCALE: NONE



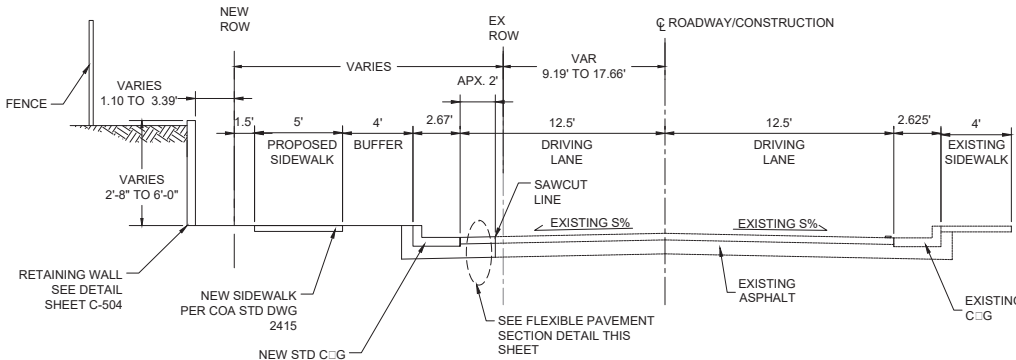
FLEXIBLE PAVEMENT SECTION

SCALE: NONE



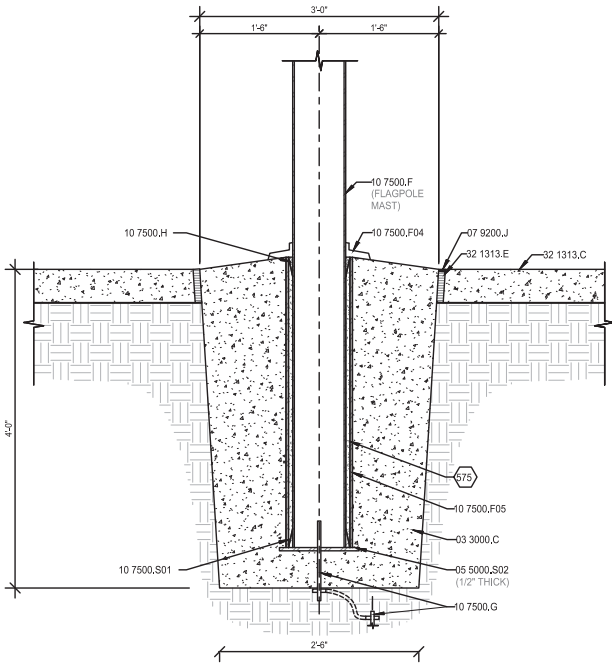
PARKING LOT PAVEMENT DETAIL

SCALE: NONE



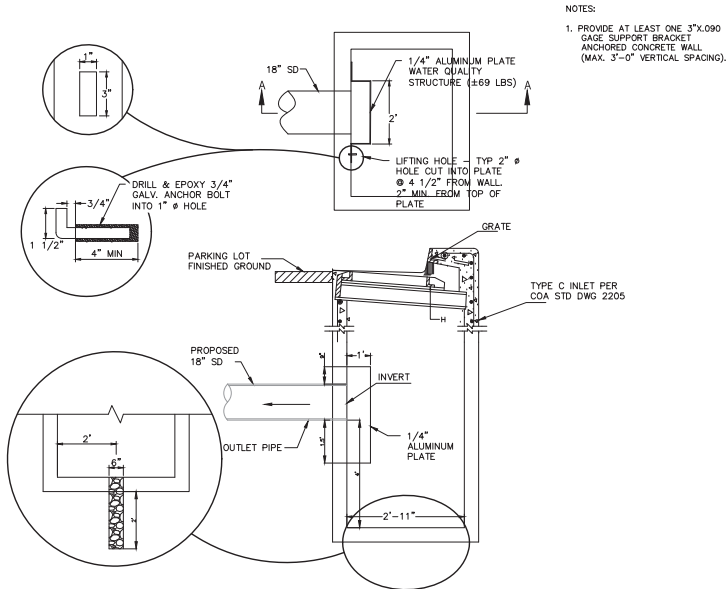
ROADWAY TYPICAL SECTION - RANKIN RD.

SCALE: .25" = 1'



FLAGPOLE BASE SECTION DETAIL

SCALE: NTS



WATER QUALITY STORM DRAIN INLET DETAIL

SCALE: NTS

GENERAL NOTES

1. FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
2. IF THIS SHEET IS NOT 30" $\times$ 42" THEN IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.
3. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
4. ALL DIMENSIONS ARE TO FACE OF CURB UNLESS OTHERWISE NOTED.
5. COORDINATE WITH CITY SOLID WASTE DEPARTMENT TO SCHEDULE A CONCRETE PRE-POUR INSPECTION FOR ALL 4 TRASH ENCLOSURES.

Project Revision

DRB SUBMITTAL	01.25.2019
50% OWNER REVIEW	02.05.2019
95% OWNER REVIEW	11.20.2019
BDLG. DEPT. SUBMIT.	03.10.2020
BDLG. DEPT. RESUB.	04.08.2020
BDLG. DEPT. RESUB.	04.28.2020
BDLG. DEPT. RESUB.	05.14.2020



WILSON & COMPANY

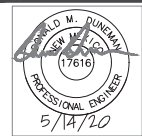


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5/14/2020

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CIVIL DETAILS

AS NOTED

DATE

DWN

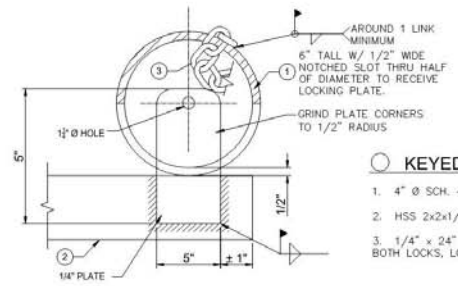
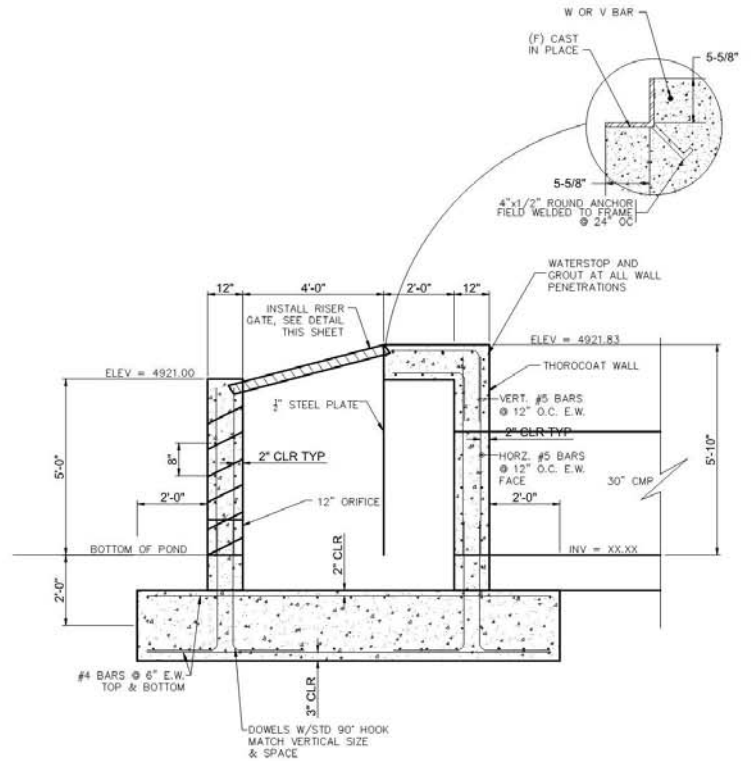
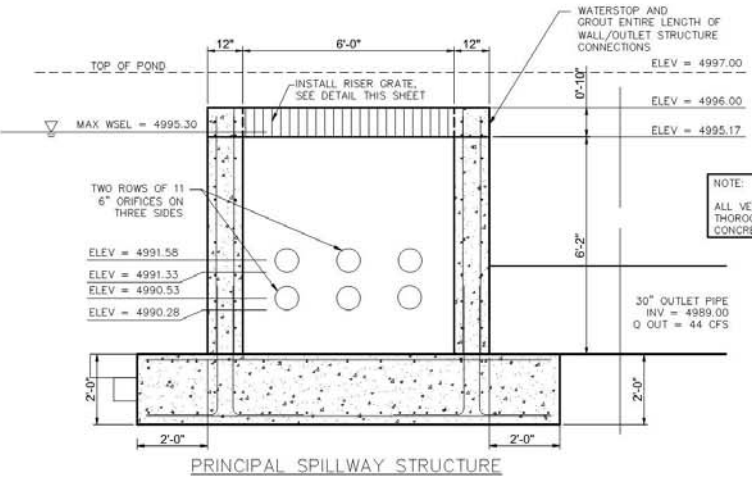
AS NOTED

SCALE

CHK

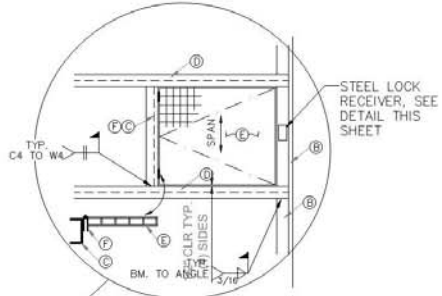
JRMA Project No.
4907-B
W&C - 14-100-132-01

C-500

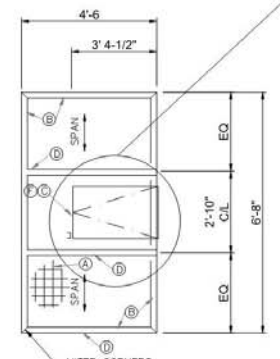


- KEYED NOTES**
- 4" Ø SCH. 40 PIPE.
 - HSS 2x2x1/8 TUBE FRAME.
 - 1/4" x 24" LONG GALVANIZED CHAIN WELDED TO FRAME AND BOTH LOCKS. LOCKS SUPPLIED BY CITY OF BELEN.

STEEL LOCK RECEIVER



- KEYED NOTES:**
- GRATING - STEEL, TYPE W-38-4 W/ 1 1/2" x 1/16" BEARING BARS, SPAN AS SHOWN
 - L5 x 5 x 5/16 LLV EDGE BEARING ANGLE WITH ANCHORS, CLIP LONG LEG TO 5 1/2" LENGTH
 - HATCH SUPPORT CHANNEL - C4 x 5.4
 - GRATING SUPPORT BEAM - W4 x 13
 - GRATING HATCH - STEEL, TYPE W-38-4 W/ 1 1/2" x 3/16" BEARING BARS, SPAN SHOWN, W/ BANDING AT ENDS
 - HEAVY DUTY WELDABLE BARREL HINGE
 - WELD 2- 1/2"x2"x3" STEEL LOCK RECEIVER.



RISER GATE-PLAN

(A1) PRINCIPAL SPILLWAY STRUCTURE DETAIL

Project Revision

DRB SUBMITTAL	01.25.2019
50% OWNER REVIEW	02.06.2019
95% OWNER REVIEW	11.20.2019
BDLG. DEPT. SUBMIT.	03.10.2020
BDLG. DEPT. RESUB.	04.08.2020



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ALBUQUERQUE, NM 87107



ONE ALBUQUERQUE



DRAINAGE DETAILS

AS NOTED
DATE: 4/8/20

JRMA Project No. 4907-B
W&C - 14-100-132-01
C-502

