## CITY OF ALBUQUERQUE

*Planning Department* David Campbell, Director



Mayor Timothy M. Keller

October 9, 2018

Ronald Bohannan, P.E. Tierra West, LLC 5571 Midway Park Place NE Albuquerque, NM, 87109

RE: Maverik Fuel Center 3737 Princeton Drive NE Grading and Drainage Plan & Drainage Report Engineer's Stamp Date: 10/03/18 Hydrology File: G16D029

Dear Mr. Bohannan:

PO Box 1293 Based upon the information provided in your submittal received 10/03/2018, the Grading & Drainage Plan and Drainage Report are not approved for Building Permit and SO-19 Permit. The following comments need to be addressed for approval of the above referenced project: Albuquerque 1. The site currently shows more than 1 acre of disturbance is being proposed. An Erosion and Sediment Control Plan is required and has to be submitted to the storm water quality engineer (Curtis Cherne, PE, ccherne@cabq.gov). Hydrology's approval for Grading or NM 87103 Building Permit will not be given until the submittal of the ESC Plan. 2. Sheet C5. Please provide the FIRM Map's effective date (8/16/12). www.cabq.gov 3. Sheet C5. Please provide the benchmark information for the survey contour information provided. 4. Sheet C5. Please provide the top of wall and bottom of wall (grade level) of the existing retaining wall at both ends and the middle. Since it appears that there will be some grading on both sides of the wall. 5. Sheet C5. In the water quality pond sections, please change the word "detention" to "water quality". 6. Sheet D1. Please darken the proposed storm sewer pipes so that they can be seen. 7. Sheet D1. Please turn off the accessible path layer. This is not needed on this sheet and is a little confusing with the drainage area lines.

## CITY OF ALBUQUERQUE

*Planning Department* David Campbell, Director



8. Please provide a detail or cut sheet of what kind of water quality inlet you are proposing in the back of the drainage report.

Prior to approval letter in support of Permanent Release of Occupancy by Hydrology, please provide an approval from NMDOT. An email of this will suffice.

If you have any questions, please contact me at 924-3995 or <u>rbrissette@cabq.gov</u>.

Sincerely,

Renée C. Brissette

Renée C. Brissette, P.E. CFM Senior Engineer, Hydrology Planning Department

PO Box 1293

Albuquerque

NM 87103

www.cabq.gov

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## City of Albuquerque

Planning Department Development & Building Services Division DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 6/2018)

Project Title: Maverik- Comanche/Princeton	Building Permit #:	Hydrology File #:
DRB#:	EPC#:	Work Order#:
Legal Description:		
City Address: 3737 Princeton Dr NE Albuquerque NM	87107	
Applicant: Tierra West, LLC		Contact: Richard Stevenson
Address: 5571 Midway Park Place NE Albuquerque NM	И 87109	
Phone#:	Fax#:505-858-1118	E-mail: <u>rstevenson@tierrawestllc.com</u>
Other Contact:		Contact:
Address:		
Phone#:	Fax#:	E-mail:
TYPE OF DEVELOPMENT: PLAT (#	e of lots) RESIDENCE	DRB SITE 🗹 ADMIN SITE
IS THIS A RESUBMITTAL? Yes	No	
DEPARTMENT TRANSPORTATION	HYDROLOGY/DRAINAGE	
Check all that Apply:	<b>TYPE OF APPRO</b>	VAL/ACCEPTANCE SOUGHT:
TYPE OF SUBMITTAL:	CERTIFICATI	E OF OCCUPANCY
ENGINEER/ARCHITECT CERTIFICATION		
PAD CERTIFICATION	PRELIMINAR	Y PLAT APPROVAL
CONCEPTUAL G & D PLAN	SITE PLAN F	OR SUB'D APPROVAL
DRADING PLAN	SITE PLAN F	OR BLDG. PERMIT APPROVAL
DRAINAGE MASTER PLAN	FINAL PLAT	APPROVAL
FLOODPLAIN DEVELOPMENT PERMIT AN     ELEVATION CERTIFICATE     CLOMR/LOMR     TRAFFIC CIRCULATION LAYOUT (TCL)     TRAFFIC IMPACT STUDY (TIS)     STREET LIGHT LAYOUT     OTHER (SPECIFY)	PPLICSIA/ RELEAS FOUNDATION GRADING PE SO-19 APPRC PAVING PER GRADING/ PA WORK ORDER	E OF FINANCIAL GUARANTEE N PERMIT APPROVAL ERMIT APPROVAL OVAL MIT APPROVAL AD CERTIFICATION R APPROVAL
PRE-DESIGN MEETING?	CLOMR/LOM FLOODPLAIN OTHER (SPE	R N DEVELOPMENT PERMIT CIFY)
DATE SUBMITTED: 10/3/2018	By: Richard Stevenson	
COA STAFF:	ELECTRONIC SUBMITTAL RECEIVED:	

FEE PAID:\_\_\_\_\_

### **DRAINAGE REPORT**

For

## **Maverik Fuel Center**

3737 Princeton Drive NE Albuquerque, NM 87107

Prepared for:

Maverik, Inc. 185 South State Street, Salt Lake City, Utah 84111

Prepared by:

Tierra West, LLC 5571 Midway Park Place NE Albuquerque, New Mexico 87109

October, 2018

I certify that this report was prepared under my supervision, and I am a registered professional engineer in the State of New Mexico in good standing.



### Job No. 2018039

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## Purpose

The purpose of this report is to outline the Drainage Plan and present a solution for the redevelopment of the site to a Maverik Gas Station and Convenience Store. The site will consist of a single-story 4,300 square foot c-store with twenty gasoline refueling pumps for vehicles and recreational users. No truck refueling is proposed.

This report outlines the developed flows associated in redeveloping the 1.56 acre site and describes the on-site surface improvements needed to safely convey the developed flows. As the site is a gas station with fueling activities, the design is required to demonstrate control of oil from vehicle refueling areas and will be addressing the 80<sup>th</sup> percentile flows from the site. These provisions are included in the proposed drainage solution.

In the pre-submittal meeting with Hydrology it was confirmed the downstream capacity will not be required to be verified. Coordination with New Mexico Department of Transportation will be required for this site as a portion drains directly into the Interstate 25 (I-25) right-of-way. A copy of this report shall be submitted to the DOT for review and comment.

## Location and Background

The site is located on the southwest corner of Comanche Road and Princeton Drive. The address of the parcel is 3737 Princeton Dr NE, Albuquerque, NM 87107. The subject property is legally described as LOT NUMBERED SEVEN (7), OF CUTTER INDUSTRIAL PARK, UNIT 6, A SUBDIVISION, ALBUQUERQUE, NEW MEXICO, AS THE SAME IS SHOWN AND DESIGNATED ON THE PLAT OF SAID SUBDIVISION, FILED IN THE OFFICE OF THE COUNTY CLEERK OF BERNALILLO COUNTY, NEW MEXICO, ON JULY 27, 1972, IN PLAT BOOK B6, FOLIO 200. The site is currently developed with a single story 16,237 square foot office building on the parcel. The site Hydronum number is G16D029.

The site is bordered to the south by an existing warehouse building, Princeton Drive to the east, Comanche Road to the north and Interstate-25 north bound frontage road to the west.

The parcel in its current developed condition does not have any storm water facilities or first flush retention ponds. The site is developed which freely discharge the developed runoff. The approximate area of unimproved areas is 25%, 5% is landscaped areas and the balance is paved or concrete surface. The property directs storm water runoff generated on-site to the east to the existing Princeton curb and gutter via an existing vehicle access point. Flows are

conveyed to Comanche Road via the gutter system for approximately 360 lineal feet west to an existing grate inlet in Comanche Road. Sheet flow is also directed to the north along the north boundary of the parcel and enters into Comanche Road right-of-way and is conveyed in the gutter system to the grate inlet. There is also an existing catch basin within the landscape right-of-way area on the east side of the I-25 frontage road. A small portion of the parcels western area sheet flows to this grate inlet. The proposed re-development will require all existing on-site improvements, pavement and structures to be demolished.

In June 1995 an addition to the paved parking areas and an all-weather entryway to the existing structure was approved by City Hydrology. On file is the Drainage and Grading Plans detailing the calculations presented by Celia S. Tomlinson, P.E. The report references the installation of a retention pond to maintain the historic discharge, however, a letter on file from the City states this pond is to be removed when the County constructed the storm drain in Greigos Rd. downstream of the site. At some point in the past decade the retention ponds were removed and the site freely discharges to Comanche Road.

The drainage information associated with the Special Assessment District BC-83-1 / 216 detailing the Greigos Detention Pond was reviewed in preparing this report. The parcel is labeled #136 and falls within the Drainage Basin Boundary for the pond. Included in the appendix is the Griegos Detention Pond Location Map and Drainage Area sheet. No further review of the detention pond capacity was completed or is justified.



## Exhibit A – Vicinity Map



## Exhibit B – Site Aerial Image

## **Flood Plain**

The floodplain information is published for the site by the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) for Bernalillo County, New Mexico and Incorporated Areas. The subject site is detailed on Community Panel Number 35001C0351H dated August 16, 2012 and is shown below.

The subject site is located within Flood Zone X, which is which is defined as, "Areas determined to be outside the 0.2% annual chance floodplain". The site does not lie within a Flood Hazard Area as shown on the FEMA map requiring no further flood-proofing or other flood mitigation.



## Exhibit C – FIRM Map

### Calculations

The site is located within Precipitation Zone 2, between the Rio Grande and San Mateo as specified in Chapter 22, Section A.1 of the City of Albuquerque Development Process Manual Volume I – Design Criteria, 2006 Revision (DPM). The principal design storm is the 100-year 6 hour event. No detention basins or retention basins are proposed and therefore longer duration design storms are not considered in the calculations. As stated in the DPM in Chapter 22 Section A.2, the 100-year 6 hour event is 2.35 inches.

The appropriate land treatments A through D, as defined in the DPM Chapter 22 Section A.3, will be applied to the various pervious and impervious areas for the proposed re-developed site.

Excess precipitation is the depth of runoff remaining after the initial volume of rainfall retained on the surface and infiltration has been subtracted from the design storm hydrograph. The DPM defines the excess precipitation for the 100-year 6 hour event in Chapter 22 Table A-8 for Zone 2 with the corresponding land treatments.

A weighted excess precipitation rate is used to calculate the volume runoff as defined in the DPM Chapter 22 (a-5, a-6). The calculation requires the sum of excess precipitation multiplied by the corresponding treatment areas divided by the total area, multiplied by the weighted excess precipitation of the watershed area.

To determine the peak discharge for the re-development the corresponding treatment areas are multiplied by the peak rate for each treatment and sum to compute the total flow. The peak rates for the treatment areas are defined in the DPM Chapter 22 Table A-9 for the 100 year event.

As this site is a re-development the storm water quality volume is calculated based on the 0.48 inch storm. To calculate the required storm water quality volume to be captured and retained onsite, the impervious areas are multiplied by 0.28 inches for the 80th percentile storm.

## **Existing (Pre-Developed) Conditions**

No offsite flows enter the site. The site is divided into two drainage basins consisting of Treatment B and C for the landscape and slope areas, and Treatment D for the impervious areas for the existing buildings and pavement areas. The site is bounded by developed streets and a building warehouse to the south. The property drains to Princeton Drive from the east and south sides; to the north side to Comanche Road and to the west to the I-25 Frontage Road. The entire site sheet flows to these discharge locations with no drainage infrastructure installed.

The peak discharge calculated for the site matches the approved peak discharge presented in the 1995 drainage report for the parcel of 6.6 cfs for the 100-year 6 hour event, as to be expected as the calculation methods listed in the DPM have not significantly changed. The runoff and volume calculations for the existing condition, based on the drainage criteria detailed in the DPM and discussed previously, is included in the appendix.

### **Proposed Conditions**

The proposed condition involves developing slightly more landscaping and installing water quality retention treatment ponding on site. A 1,590 square foot reduction of impervious areas is proposed which results in a slightly reduced volume of runoff and peak discharge. Included in the appendix are the calculations for the proposed site conditions. The expected total runoff from the site for the 100-year 6 hour event is 6.47 cfs with a volume of 0.231 ac-ft.

To manage the developed flows from the impervious areas the site is generally divided into three basin areas based on the design elevations for the site.

Roof drains will collect runoff from the proposed c-store and discharge directly into the first flush basins. Roof drains are planned for the fuel center canopy with runoff collected and conveyed to an 8-inch diameter drain that will discharge flows directly to the oil/water separator.

Per DPM Chapter 22.9.E, Table 1 all fueling stations must demonstrate control of oil from vehicle parking areas. Basin B4 covers the majority of the pavement area, including all of the sheet flow generated from the re-fueling area under the canopy, and sheet flow is directed to a single modified oil-water separator Type C curb inlet at the north east corner of the site. The curb inlet has the capacity of 3.87 cfs and will convey the calculated 2.87 cfs that will flow to inlet. The single inlet will be modified to include a 24-inch deep sump box and installation of a baffle plate to restrict the passing of trash with a 12-inch by 12-inch exfiltration opening at the base of the concrete box to release the stormwater held in the sump. For the designed sump depth of 24-inches the box inlet will retain 130 gallons which is adequate for any major fuel spill/s that may occur during operations at the site. During regular site maintenance the inlet shall be cleaned of debris and sediment that accumulates over time in the sump.

A 12-inch storm drain is connected to the inlet box and discharges the treated stormwater directly to the first flush pond located at the north east corner of the parcel. This method will provide a 'double action' protection to retain on site any debris or hydrocarbon particles that were able to pass through the oil-water separator inlet box. The water quality pond #3 will retain

a volume of 800 cubic feet before releasing the additional flow to Comanche Road right-of-way through a concrete weir and a 2-foot concrete rundown / sidewalk culvert conforming to the SO19 Permit. The concrete rundown sidewalk channel is required to have the capacity to pass the 100-year 6 hour event combined flows that enter into the pond which is a total of 5.3 cfs. At the proposed 2% grade the sidewalk culvert has a capacity of 6.97 cfs. The proposed concrete weir design has the capacity of 17.5 cfs and will safely convey the required 5.3 cfs into the concrete rundown.

All other site runoff generated from the pervious areas (Basins B2, B4 and B5) will be conveyed as surface flows to the on-site curb and gutters and be released via curb cuts to the respective first flush ponds.

Basin B2 calculated flow is 1.45 cfs which enters into the water quality pond #1. The pond has the capacity to retain a volume of 660 cubic feet. At the designed inlet elevation additional flow shall enter the proposed Nyloplast 12-inch dome inlet and drain basin and be conveyed through an 8-inch HDPE storm pipe. This storm pipe is connected to the Nyloplast 12-inch dome inlet proposed at the water quality pond #2. This pond is associated with the runoff from Basin B5 which totals 0.98 cfs. The Nyloplast 12-inch dome inlet has the adequate capacity based on designed storage head in the ponds to pass the runoff flows. In the case of a blockage at an inlet, emergency overflow riprap rundowns are proposed. The calculations confirming the riprap weirs and the rundown have capacity to pass and carry the design flows is included in Appendix A. The weir invert elevations are listed on the plans for each water quality pond.

The water quality pond #2 has the capacity to retain a volume of 580 cubic feet. At the designed inlet elevation the additional flow shall enter the inlet and into the 12-inch HDPE storm drain. This storm drain passes the additional flows from basins B2 and B5, a total of 2.44 cfs. The storm drain at the designed slope of 1.40% has the capacity to discharge a total of 4.23 cfs. This storm drain discharges the additional flows from ponds #1 and #2 into the water quality pond #3.

All site runoff generated from the landscaped slope areas (Basins B1 and B6) will freely discharge to the north and west into the respective right-of-ways. A small portion of runoff totaling 0.05 cfs discharges directly into the Princeton Drive right-of-way at the driveway entrances (Basins B8 and B9). The basin map is shown in the figure below.

8

As the sheet flow runoff from Basin B1 and a portion of B6 enter directly into the New Mexico DOT right-of-way, the drainage report and solution for the re-development will be presented to the District 3 Drainage Engineer. As the flows are not increased from the existing site discharge, no offsite drainage improvements are proposed in DOT the right-of-way.





## Water Quality Management

As this site is a re-development, the water quality volume is calculated based on the 0.48 inch storm. The impervious area is multiplied by 0.28 inches for the 80th percentile storm to determine the volume to be captured and retained onsite.

The total impervious area is 1.06 acres and requires a total water quality volume of 1,081 cubic feet for the basin areas. Three water quality ponds are proposed across the re-developed site. They are located in the landscape areas where the impervious area sheet flow runoff is directed to, or discharged into from the storm drain. The proposed total volume of the three water quality pond areas is 2,040 cubic feet. All developed flows from impervious areas are routed through the landscape ponds meeting the intent of the ordinance. Basin B1 and B6 are landscape slope areas with runoff entering directly into the street right-of-way.

The water quality volume calculations are detailed on the hydrology table in the appendix.

A Drainage Covenant will be required for the water quality ponds. As the ponds only function as first flush ponds the appropriate covenant is the Private Facility Drainage Covenant. This will be submitted to the City with the final Building Permit set.

## Summary

This report outlines the Drainage Plan and present the on-site surface and subsurface drainage improvements needed to safely convey the developed flows for the re-development of the site to a Maverik Gas Station and Convenience Store.

Per the DPM the design is required to control the oil wash-off from vehicle refueling areas and is achieved with the oil-water separator. Three first flush ponds are proposed to retain a total of 2,040 cubic feet, meeting the water quality ponding requirements. The site does not increase the historic flow released from the site and the solution adheres to best practices for stormwater quality management.

# APPENDIX A



ALL EXISTING UTILITIES SHOWN WERE OBTAINED FROM RESEARCH, AS-BUILTS, SURVEYS OR INFORMATION PROVIDED BY OTHERS. IT SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR TO CONDUCT ALL NECESSARY FIELD INVESTIGATIONS PRIOR TO AND INCLUDING ANY EXCAVATION, TO DETERMINE THE ACTUAL LOCATION OF UTILITIES AND OTHER IMPROVEMENTS, PRIOR TO STARTING THE WORK. ANY CHANGES FROM THIS PLAN SHALL BE COORDINATED WITH AND APPROVED BY THE ENGINEER.





PER DPM CHAPTER 22.9.E, TABLE 1 ALL FUELING STATIONS MUST DEMONSTRATE CONTROL OF OIL FROM VEHICLE PARKING AREAS. BASIN B4 IS THE MAJORITY OF THE PAVEMENT AREA, INCLUDING ALL OF THE SHEET FLOW GENERATED FROM THE RE-FUELING AREA UNDER THE CANOPY, IS DIRECTED TO A SINGLE TYPE C CURB INLET AT THE NORTH EAST CORNER OF THE SITE. THE CURB INLET HAS THE CAPACITY FOR THE CALCULATED 2.87 CFS THAT WILL FLOW TO INLET. THE SINGLE INLET WILL BE MODIFIED TO INCLUDE A SUMP BOX AND BAFFLE PLATE TO RESTRICT THE PASSING OF TRASH AND INCLUDE A 12-INCH BY 12-INCH EXFILTRATION OPENING AT THE BASE OF THE CONCRETE BOX TO PASS ANY REMAINING HYDROCARBON FLUID THAT ENTERS INTO THE INLET. WITH A DESIGNED SUMP DEPTH OF 24-INCHES THE BOX INLET WILL RETAIN 130 GALLONS WHICH IS

ADEQUATE FOR ANY MAJOR FUEL SPILL/S THAT MAY OCCUR DURING REGULAR OPERATIONS AT THE SITE. DURING REGULAR MAINTENANCE THE INLET SHALL BE CLEANED OF DEBRIS AND SEDIMENT THAT ACCUMULATE OVER TIME. AN 18-INCH STORM DRAIN IS CONNECTED TO THE INLET BOX AND DISCHARGES THE TREATED STORMWATER DIRECTLY TO THE FIRST FLUSH POND LOCATED AT THE NORTH EAST CORNER OF THE PARCEL. THE FIRST FLUSH POND WILL RETAIN A VOLUME OF 800 CUBIC FEET BEFORE RELEASING THE ADDITIONAL FLOW TO COMANCHE ROAD RIGHT-OF-WAY VIA A 2-FOOT CONCRETE RUNDOWN AND 2-FOOT SIDEWALK CULVERT.

ALL SITE RUNOFF GENERATED FROM THE PERVIOUS AREAS (BASINS B2, B4 AND B5) WILL BE CONVEYED AS SURFACE FLOWS TO THE ON-SITE CURB AND GUTTERS AND BE RELEASED VIA CURB CUTS TO THE RESPECTIVE FIRST FLUSH PONDS. ALL SITE RUNOFF GENERATED FROM THE LANDSCAPED SLOPE AREAS (BASINS B1 AND B6) WILL FREELY DISCHARGE TO THE NORTH AND WEST INTO THE RESPECTIVE RIGHT-OF-WAYS. A SMALL PORTION OF RUNOFF TOTALING 0.05 CFS DISCHARGES DIRECTLY INTO THE PRINCETON DRIVE RIGHT-OF-WAY AT THE DRIVEWAY ENTRANCES (BASINS B8 AND B9).

Dasin Daseri	0110110												ee rear, e m			10 1001) 0 11		
Basin	Area	Area	Area	Treatment A	Т	reatment	:В Т	reatment	t C	Treatment D		Weighted E	Volume	Flow	Weighted E	Volume	Flow	FF P
ID	(sf)	(acres)	(sq miles)	%	(acres)	%	(acres)	%	(acres)	%	(acres)	(in)	(ac-ft)	cfs	(in)	(ac-ft)	cfs	Requir
1	4,793	0.11	0.00017	0%	0.000	100%	0.110	0%	0.000	0%	0.000	0.780	0.007	0.25	0.280	0.003	0.10	
2	16,120	0.37	0.00058	0%	0.000	32%	0.118	0%	0.000	68%	0.252	1.691	0.052	1.45	1.001	0.031	0.90	
3	1,477	0.03	0.00005	0%	0.000	100%	0.034	0%	0.000	0%	0.000	0.780	0.002	0.08	0.280	0.001	0.03	
4	26,570	0.61	0.00095	0%	0.000	0%	0.000	0%	0.000	100%	0.610	2.120	0.108	2.87	1.340	0.068	1.92	
5	9,939	0.23	0.00036	0%	0.000	16%	0.037	0%	0.000	84%	0.192	1.906	0.036	0.98	1.170	0.022	0.64	
6	10,066	0.23	0.00036	0%	0.000	10%	0.023	90%	0.208	0%	0.000	1.095	0.021	0.71	0.496	0.010	0.38	
7	1,440	0.03	0.00005	0%	0.000	100%	0.033	0%	0.000	0%	0.000	0.780	0.002	0.08	0.280	0.001	0.03	
8	397	0.01	0.00001	0%	0.000	0%	0.000	0%	0.000	100%	0.009	2.120	0.002	0.04	1.340	0.001	0.03	
9	135	0.00	0.00000	0%	0.000	0%	0.000	0%	0.000	100%	0.003	2.120	0.001	0.01	1.340	0.000	0.01	
Total	70,937	1.63	0.003		0.000		0.355		0.208		1.065		0.231	6.470		0.136	4.039	1,0

### CURRENT SITE DRAINAGE

NO OFFSITE FLOWS ENTER THE SITE. THE SITE IS BOUNDED BY DEVELOPED STREETS AND A BUILDING WAREHOUSE TO THE SOUTH. THE PROPERTY DRAINS TO PRINCETON DRIVE FROM THE EAST AND SOUTH SIDES; TO THE NORTH SIDE TO COMANCHE ROAD AND TO THE WEST TO THE I-25 FRONTAGE ROAD. THE ENTIRE SITE SHEET FLOWS TO THESE DISCHARGE LOCATIONS WITH NO DRAINAGE INFRASTRUCTURE INSTALLED. THE PEAK DISCHARGE CALCULATED FOR THE SITE MATCHES THE APPROVED PEAK DISCHARGE PRESENTED IN THE 1995 DRAINAGE REPORT FOR THE PARCEL OF 6.6 CFS FOR THE 100-YEAR 6 HOUR EVENT.

Excess Precip	oitation, E (in.)		Peak Dischar	ge (cfs/acre)	
Zone 2	100-Year	10-Year	Zone 2	100-Year	10-Year
Ea	0.53	0.13	Qa	1.56	0.38
Eb	0.78	0.28	Qb	2.28	0.95
Ec	1.13	0.52	Qc	3.14	1.71
Ed	2.12	1.34	Qd	4.70	3.14

## Pipe Capacity

Pipe Number	D	Slope	Area	R	Q Provided	Velocity
	(in)	(%)	(ft^2)		(cfs)	(ft/s)
1	4	1.00	0.09	0.083	0.23	2.58
2	6	1.00	0.20	0.125	0.66	3.39
3	8	1.00	0.35	0.167	1.43	4.10
4	12	1.00	0.79	0.250	4.22	5.38
5	18	2.00	1.77	0.375	14.90	8.43

Manning's Equation: Q = 1.49/n \* A \* R^(2/3) \* S^(1/2) A = Area R = D/4 S = Slope n = 0.011 PVC

Total Impervious Area =

Retainage depth = 0.28"

Retention Volume =

# n = 0.013 HDPE

Water Quality Volume - "First Flush Pond" - Redevelopment Site

## CAUTION:

ΣArea in "Treatment D"

0.0233 foot

=**0.0233 x area** CF

ALL EXISTING UTILITIES SHOWN WERE OBTAINED FROM RESEARCH, AS-BUILTS, SURVEYS OR INFORMATION PROVIDED BY OTHERS. IT SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR TO CONDUCT ALL NECESSARY FIELD INVESTIGATIONS PRIOR TO AND INCLUDING ANY EXCAVATION, TO DETERMINE THE ACTUAL LOCATION OF UTILITIES AND OTHER IMPROVEMENTS, PRIOR TO STARTING THE WORK. ANY CHANGES FROM THIS PLAN SHALL BE COORDINATED WITH AND APPROVED BY THE ENGINEER.



Qua	lity Volume
nd	FF Pond
ed CF	Provided CF
0	0
255	660
0	0
619	800
195	580
0	0
0	0
9	0
3	0
1	2,040



## CURRENT SITE DRAINAGE

NO OFFSITE FLOWS ENTER THE SITE. THE SITE IS BOUNDED BY DEVELOPED STREETS AND A BUILDING WAREHOUSE TO THE SOUTH. THE PROPERTY DRAINS TO PRINCETON DRIVE FROM THE EAST AND SOUTH SIDES; TO PRINCETON DRIVE FROM THE EAST AND SOUTH SIDES; TO THE NORTH SIDE TO COMANCHE ROAD AND TO THE WEST TO THE I-25 FRONTAGE ROAD. THE ENTIRE SITE SHEET FLOWS TO THESE DISCHARGE LOCATIONS WITH NO DRAINAGE INFRASTRUCTURE INSTALLED. THE PEAK DISCHARGE CALCULATED FOR THE SITE MATCHES THE APPROVED PEAK DISCHARGE PRESENTED IN THE 1995 DRAINAGE REPORT FOR THE PARCEL OF 6.6 CFS FOR THE 100-YEAR 6 HOUR EVENT.

Basin Descri	ptions											1	00-Year, 6-Hr			10-Year, 6-Hr	•
Basin	Area	Area	Area	Treatment A	Tı	eatment	B T	reatment	С	Treatment D		Weighted E	Volume	Flow	Weighted E	Volume	Flow
ID	(sf)	(acres)	(sq miles)	%	(acres)	%	(acres)	%	(acres)	%	(acres)	(in)	(ac-ft)	cfs	(in)	(ac-ft)	cfs
1	22,935	0.53	0.00082	0%	0.000	50%	0.263	50%	0.263	0%	0.000	0.955	0.042	1.43	0.400	0.018	0.70
2	48,003	1.10	0.00172	0%	0.000	0%	0.000	0%	0.000	100%	1.102	2.120	0.195	5.18	1.340	0.123	3.46
Total	70,937	1.63	0.003		0.000		0.263		0.263		1.102		0.237	6.606		0.141	4.161

Excess Precip	itation, E (in.)		Peak Dischar	ge (cfs/acre)	
Zone 2	100-Year	10-Year	Zone 2	100-Year	10-Year
Ea	0.53	0.13	Qa	1.56	0.38
Eb	0.78	0.28	Qb	2.28	0.95
Ec	1.13	0.52	Qc	3.14	1.71
Ed	2.12	1.34	Qd	4.70	3.14

## Equations:

Weighted E = Ea\*Aa + Eb\*Ab + Ec\*Ac + Ed\*Ad / (Total Area)

Volume = Weighted E \* Total Area

Flow = Qa\*Aa + Qb\*Ab + Qc\*Ac + Qd\*Ad

## CAUTION:

AND APPROVED BY THE ENGINEER.



ALL EXISTING UTILITIES SHOWN WERE OBTAINED FROM RESEARCH, AS-BUILTS, SURVEYS OR INFORMATION PROVIDED BY OTHERS. IT SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR TO CONDUCT ALL NECESSARY FIELD INVESTIGATIONS PRIOR TO AND INCLUDING ANY EXCAVATION, TO DETERMINE THE ACTUAL LOCATION OF UTILITIES AND OTHER IMPROVEMENTS, PRIOR TO STARTING THE WORK. ANY CHANGES FROM THIS PLAN SHALL BE COORDINATED WITH

Historic Conditions - See Basin Map Exhibit

<b>Basin Descri</b>	ptions											1(	00-Year, 6-Hr			10-Year, 6-Hr	
Basin	Area	Area	Area	Treatment A	Tr	eatment E	Tr.	eatment C		Treatment D		Weighted E	Volume	Flow	Weighted E	Volume	Flow
Q	(sf)	(acres)	(sq miles)	%	(acres)	%	(acres)	%	(acres)	%	(acres)	(in)	(ac-ft)	cfs	(in)	(ac-ft)	cfs
1	22,935	0.53	0.00082	%0	0.000	50%	0.263	50%	0.263	%0	0.000	0.955	0.042	1.43	0.400	0.018	0.70
2	48,003	1.10	0.00172	%0	0.000	%0	0.000	%0	0.000	100%	1.102	2.120	0.195	5.18	1.340	0.123	3.46
Total	70,937	1.63	0.003		0.000		0.263		0.263		1.102		0.237	6.606		0.141	4.161

ush Volume	uo	87107	8/15/2018
d E Method & First Flu	- Id Light Vehicle Fueling Statio	NE # 100, Albuquerque, NM	Date
DPM Weighter	Maverik C-Store an	3737 Princeton Dr I	TWLLC

Proposed Conditions - See Basin Map Exhibit

	w FF Pond FF Pond		s Required CF Provided CF	s Required CF Provided CF	s         Required CF         Provided CF           0	s         Required CF         Provided CF           0         0         0         0         0         3         555         660 <th>s         Required CF         Provided CF           0         0         0         0           3         255         660         0           2         619         800         0</th> <th>s         Required CF         Provided CF           0         0         0         0           0         255         660           3         0         0         0           3         619         800           4         195         580</th> <th>s         Required CF         Provided CF           0         0         0         0         0           3         0         255         660         0           3         0         255         660         0           2         619         0         0         0         0           2         619         580         800</th> <th>s         Required CF         Provided CF           0         0         0         0           3         0         255         660           3         0         0         0           2         619         800         0           8         0         0         0           8         0         0         0           3         0         0         0</th> <th>s         Required CF         Provided CF           0         0         0         0           0         0         0         0           1         0         0         0           2         619         800         0           8         195         580         0           8         0         0         0         0           3         0         0         0         0           3         9         0         0         0</th> <th>s         Required CF         Provided CF           0         0         0         0           10         255         660         0           2         0         0         0         0           3         0         195         580         0           8         195         580         0         0           3         0         0         0         0         1           1         3         9         0         0         0         1</th>	s         Required CF         Provided CF           0         0         0         0           3         255         660         0           2         619         800         0	s         Required CF         Provided CF           0         0         0         0           0         255         660           3         0         0         0           3         619         800           4         195         580	s         Required CF         Provided CF           0         0         0         0         0           3         0         255         660         0           3         0         255         660         0           2         619         0         0         0         0           2         619         580         800	s         Required CF         Provided CF           0         0         0         0           3         0         255         660           3         0         0         0           2         619         800         0           8         0         0         0           8         0         0         0           3         0         0         0	s         Required CF         Provided CF           0         0         0         0           0         0         0         0           1         0         0         0           2         619         800         0           8         195         580         0           8         0         0         0         0           3         0         0         0         0           3         9         0         0         0	s         Required CF         Provided CF           0         0         0         0           10         255         660         0           2         0         0         0         0           3         0         195         580         0           8         195         580         0         0           3         0         0         0         0         1           1         3         9         0         0         0         1
	ume FIOW FF PON	-#\ rec Damirod	us in incluied	03 0.10 heyanea	11 0.90 0.10 0.90 0.10 0.90 0.10 0.10 0.	03 0.10 headened	org         org         org           03         0.10         0           31         0.03         0           01         0.03         0           01         0.03         0           06         1.92         0	N         US         Network           31         0.10         1           31         0.33         1           68         1.92         1           22         0.64         1	13         0.10         Insequence           131         0.10         0         0           101         0.03         0         0         0           122         0.64         1         0         1           10         0.38         0.64         0         0         1		N         us         mediance           131         0.10         1           131         0.90         1           101         0.03         1           122         0.64         1           101         0.38         1           101         0.38         1           101         0.03         1           101         0.03         1           101         0.03         1           101         0.03         1	33         0.10         Median           131         0.30         0.10         0           101         0.33         0.13         0           101         0.33         0.192         0           110         0.34         0         0           110         0.33         0.03         0           110         0.33         0.03         0           101         0.03         0         0           101         0.03         0         0
	eighted E Volume	(in) (ac-ft)		0.280 0.003	0.280 0.003 1.001 0.031	0.280 0.003 1.001 0.031 0.280 0.001	0.280         0.003           1.001         0.031           0.280         0.001           1.340         0.068	0.280         0.003           1.001         0.031           0.280         0.001           1.340         0.068           1.170         0.022	0.280         0.003           1.001         0.031           0.280         0.031           1.340         0.068           1.340         0.022           0.496         0.010	0.280         0.003           1.001         0.031           0.280         0.031           0.280         0.031           1.340         0.068           1.170         0.022           0.496         0.010           0.280         0.010	0.280 0.003 1.001 0.031 0.280 0.001 1.1340 0.068 1.1740 0.022 0.028 0.010 0.280 0.010	0.280 0.003 1.001 0.031 0.230 0.001 1.340 0.002 1.340 0.058 0.495 0.010 0.280 0.010 1.340 0.001 1.340 0.001
	Flow Weigh	cfs (ir		0.25 0.2	0.25 0.27 0.27 1.00	0.25 0.2 1.45 1.0 0.08 0.2	0.25 0.21 1.45 1.00 0.08 0.21 2.87 1.3	0.25 0.21 1.45 1.0 0.08 0.21 2.87 1.3 0.98 1.1	0.25 0.2 1.45 1.0 0.08 0.2 2.87 1.3 0.28 1.1 0.21 0.4	0.25 0.21 1.45 1.00 0.08 0.22 0.287 1.13 0.98 1.11 0.41 0.71 0.41 0.28	0.25 0.23 0.23 0.21 0.02 0.02 0.02 0.02 0.28 1.13 0.02 0.28 1.13 0.29 1.13 0.21 0.21 0.21 0.01 0.01 0.02 0.21 0.02 0.21 0.02 0.21 0.02 0.21 0.02 0.21 0.02 0.22 0.2	0.25 0.23 1.45 1.00 0.08 0.23 2.87 1.32 0.71 0.49 0.71 0.44 0.04 1.33 0.01 1.33
A STATE AND A STAT	eighted E Volume	(in) (ac-ft)		0.780 0.007	0.780 0.007 1.691 0.052	0.780 0.007 1.691 0.052 0.780 0.002	0.780 0.007 1.691 0.052 0.780 0.002 2.120 0.108	0.780 0.007 1.691 0.052 0.780 0.002 2.120 0.108 1.906 0.036	0.780         0.007           1.691         0.052           0.780         0.002           2.120         0.108           1.906         0.036           1.095         0.021	0.780 0.007 1.691 0.052 0.780 0.002 2.120 0.108 1.906 0.036 1.095 0.021 0.780 0.002	0.780 0.007 1.691 0.052 0.780 0.002 2.120 0.108 1.906 0.036 1.095 0.021 1.095 0.021 2.120 0.002	0.780 0.007 1.691 0.052 2.120 0.002 2.120 0.008 1.906 0.036 1.905 0.021 0.780 0.002 0.780 0.002 2.120 0.002 2.120 0.002
	weig	(acres) (i.		0.000 0.0	0.000 0.7	0.000 0.7 0.252 1.6 0.000 0.7	0.000 0.7 0.252 1.6 0.000 0.7 0.610 2.1	0.000 0.74 0.72 0.76 0.72 0.76 0.72 0.76 0.72 0.71 0.71 0.71 0.71 0.71 0.71 0.71 0.71	0.000 0.252 1.6 0.252 1.6 0.200 0.7 0.610 2.1 0.192 1.9 0.100 1.6	0.000 0.71 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72	0.000 0.7 0.7 0.7 0.7 0.6 0.7 0.6 0.0 0.7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.0 0.252 1.6 0.0252 1.6 0.000 0.7 0.192 1.1 0.000 1.0 0.000 0.7 0.000 2.1 0.003 2.1
	Treatment D	%	707	0.70	0% 68%	0% 0%	0% 68% 100%	0% 68% 0% 100% 84%	0% 68% 0% 100% 84% 0%	68% 68% 0% 100% 84% 0%	0% 68% 0% 100% 84% 0% 0% 100%	0.% 68% 0% 100% 84% 84% 0% 100% 100%
	ment C	% (acres)	0000 %	_	0.000	% 0.000 % 0.000	0.000 % 0.000 % 0.000	% 0.000 % 0.000 % 0.000 % 0.000 %	%         0.000           %         0.000           %         0.000           %         0.000           %         0.000           %         0.000           %         0.000	%         0.000           %         0.000           %         0.000           %         0.000           %         0.000           %         0.000           %         0.000           %         0.000	%         0.000           %         0.000           %         0.000           %         0.000           %         0.000           %         0.000           %         0.000           %         0.000           %         0.000           %         0.000	%         0.000           1%         0.000           1%         0.000           1%         0.000           1%         0.000           1%         0.000           1%         0.000           1%         0.000           1%         0.000           1%         0.000           1%         0.000           1%         0.000
	nt B Treati	(acres)	0.110 0		0.118 0	0.118 0 0.034 0	0.118 0 0.034 0 0.000 0	0.118 0 0.034 0 0.000 0 0.037 C	0.118 0. 0.034 0 0.000 0 0.037 0 0.023 9(	0.118         0           0.034         0           0.000         0           0.037         0           0.037         0           0.037         0           0.033         9           0.033         0	0.118         0           0.034         0           0.037         0           0.033         9           0.033         0           0.033         0	0.118         0.           0.034         0           0.037         0           0.033         9           0.033         0           0.033         0           0.000         0           0.000         0
Trontmon	ן במרווובוו	cres) %	.000 100%		.000 32%	.000 32% 1.000 100%	.000 32% .000 100% .000 0%	.000 32% .000 100% .000 0% 1.000 16%	.000         32%           .000         100%           .000         0%           .000         16%           .000         16%           .000         10%	.000         32%           .000         100%           .000         0%           .000         16%           .000         10%           .000         10%           .000         10%	.000         32%           .000         100%           .000         0%           .000         16%           .000         10%           .000         10%           .000         10%           .000         10%           .000         0%           .000         0%           .000         0%           .000         0%           .000         0%           .000         0%	.000         32%           .000         100%           .000         10%           .000         16%           .000         10%           .000         10%           .000         10%           .000         10%           .000         10%           .000         10%           .000         10%           .000         0%           .000         0%           .000         0%
reatment A		% (a	0% 0	/00/	0.2%	0%	0% 0		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	0% 0 0% 0 0% 0 0% 0 0% 0 0% 0 0% 0 0% 0	0% 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.00 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0
	Area	(sq miles)	0.00017	0.00058		0.00005	0.00095	0.00036	0.00036	0.00036	0.00035 0.00035 0.00036 0.00036 0.00036 0.000036	0.0000 0.000036 0.000036 0.000036 0.000036 0.000000 0.000000 0.000000
	Area	(acres)	0.11	0.37		0.03	0.03	0.03 0.61 0.23	0.03 0.61 0.23 0.23	0.03 0.61 0.23 0.23 0.23	0.03 0.61 0.23 0.23 0.03 0.03	0.03 0.61 0.23 0.23 0.23 0.03 0.03
	Area	(sf)	4,793	16,120		1,477	1,477 26,570	1,477 26,570 9,939	1,477 26,570 9,939 10,066	1,477 26,570 9,939 10,066 1,440	1,477 26,570 9,939 10,066 1,440 397	1,477 26,570 9,939 10,066 1,440 397 135
	Basin	٩	1	2	-	m	4 3	о 5 4 3	3 5 6	3 3 6 5 5 4	8 7 6 5 4 3	9 8 4 0 U

# Equations:

Weighted E = Ea\*Aa + Eb\*Ab + Ec\*Ac + Ed\*Ad / (Total Area)

Volume = Weighted E \* Total Area

 $\mathsf{Flow} = \mathsf{Qa}^*\mathsf{Aa} + \mathsf{Qb}^*\mathsf{Ab} + \mathsf{Qc}^*\mathsf{Ac} + \mathsf{Qd}^*\mathsf{Ad}$ 

Excess Precipi	tation, E (in.)		Peak Discharge	e (cfs/acre)	
Zone 2	100-Year	10-Year	Zone 2	100-Year	10-Year
Ea	0.53	0.13	Qa	1.56	0.38
Eb	0.78	0.28	qp	2.28	0.95
Ec	1.13	0.52	Qc	3.14	1.71
Ed	2.12	1.34	pQ	4.70	3.14

# "Firet Fluch Do union valieno. Wate

Water Quality Volume - "First Flush Pond"		
Total Impervious Area =	ΣArea in "Treatment I	<u>"</u>
Retainage depth = 0.44"-0.1" = 0.34" =	0.0283 foot	
Retention Volume =	=0.0283 x area CF	

### Worksheet for 2' Concrete Sidewalk Culvert at 2% Slope

Project Description					
Friction Method	Manning Formula				
Solve For	Discharge				
Input Data					
Channel Slope		0.02000	ft/ft		
Normal Depth		0.50	ft		
Section Definitions					
Station (ft)	Elevatio	on (ft)			
	0+00		0 58		
	0+00		0.00		
	0+01		0.00		
	0+02		0.08		
1	0+02		0.58		
Roughness Segment Definitions					
Start Station	Ending §	Station		Roughness Coefficient	
(0+00,	0.58)	(0+	02, 0.58)		0.013
Options					
Current Roughness Weighted Method	Pavlovskii's Method				
Open Channel Weighting Method	Pavlovskii's Method				
Closed Channel Weighting Method	Pavlovskii's Method				
Results					
Discharge		6.97	ft³/s		
Elevation Range	0.00 to 0.58 ft				
Flow Area		0.92	ft²		
Wetted Perimeter		2.84	ft		
Hydraulic Radius		0.32	ft		
Top Width		2.00	ft		
Normal Depth		0.50	ft		
Critical Depth		0.76	ft		

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## Worksheet for 2' Concrete Sidewalk Culvert at 2% Slope

Results					
Critical Slope		0.00550	ft/ft		
Velocity		7.61	ft/s		
Velocity Head		0.90	ft		
Specific Energy		1.40	ft		
Froude Number		1.98			
Flow Type	Supercritical				
GVF Input Data					
Downstream Depth		0.00	ft		
Length		0.00	ft		
Number Of Steps		0			
GVF Output Data					
Upstream Depth		0.00	ft		
Profile Description					
Profile Headloss		0.00	ft		
Downstream Velocity		Infinity	ft/s		
Upstream Velocity		Infinity	ft/s		
Normal Depth		0.50	ft		
Critical Depth		0.76	ft		
Channel Slope		0.02000	ft/ft		
Critical Slope		0.00550	ft/ft		

	Cross Section for 2% Slope				
Project Description					
Friction Method	Manning Formula				
Solve For	Discharge				
Input Data					
Channel Slope		0.02000	ft/ft		
Normal Depth		0.50	ft		
Discharge		6.97	ft³/s		

#### **Cross Section Image**



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<b>Pipe Number</b>	۵	Slope	Area	ĸ	Q Provided	Velocity
	(in)	(%)	(ft^2)		(cfs)	(ft/s)
+	4	1.00	0.09	0.083	0.23	2.58
2	9	1.00	0.20	0.125	0.66	3.39
S	8	1.00	0.35	0.167	1.43	4.10
4	12	1.00	0.79	0.250	4.22	5.38
5	18	2.00	1.77	0.375	14.90	8.43

Manning's Equation: $Q = 1.49/n * A * R^{2}(3) * S^{1}(1/2)$  $Q = 1.49/n * A * R^{2}(2/3) * S^{1}(1/2)$ A = AreaA = AreaR = D/4S = Slopen = 0.011n = 0.013HDPE

## CAPACITY OF SINGLE 'C' STORM DROP INLET

### Capacity of the grate:

- L =  $47.375" 2(6"_{ends}) 14(\frac{1}{2}"_{middle bars})$ = 28.375" = 2.365'
- W =  $30" 13(\frac{1}{2"} \text{ middle bars})$ = 23.5" = 1.958'
- Area =  $2.365' \times 1.958'$ =  $4.63 \text{ ft}^2$
- Effective Area =  $4.63 4.63 (0.5_{\text{clogging factor}})$ = 2.3 ft<sup>2</sup> at the grate

#### CHECK CAPACITY FOR MIN. H=0.10'

 $\frac{\text{Orifice Equation}}{Q = CA \text{ sqrt(2gH)}}$  Q = 0.6\*2.3\*sqrt(2\*32.2\*0.10)Q = 3.50 cfs

### Capacity of the throat:

L =  $47-\frac{3}{8}$ " = 3.948'

<u>Weir Equation</u> Q = CLH<sup>^</sup>(3/2) Q = 2.95 \* 3.948 \* 0.10<sup>^</sup>(3/2) Q = 0.37 cfs

### Total Capacity (FOR MIN. H=0.10'):

 $Q = 3.50_{grate} + 0.37_{throat}$  $Q = 3.87 \text{ cfs} = Q_{available}$ 

Curb Inlet Area "B4" Q <sub>required</sub> =2.87 cfs < Q <sub>available</sub>, therefore **OK**.

# Nyloplast<sup>®</sup> Tomorrow's Storm Drainage Structures Today.

## **Nyloplast Grate Inlet Capacity Charts**

These charts are based on equations from the USDOT/FAA Advisory Circular pertaining to Surface Drainage Design, AC No: AC150/5320-5C and the USDOT/FHWA Urban Drainage Design Manual, Hydraulic Engineering Circular No. 22, Third Edition, Publication No. FHWA-NHI-10-009. Certain assumptions have been made, and no two installations will necessarily perform the same way. Safety factors should change with site conditions and is left to the discretion of the design engineer.



June 2012

Nyloplast 12" Dome Grate Inlet Capacity Chart



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## Worksheet for Concrete Weir at Water Quality Pond #3

Project Description					
Friction Method Solve For	Manning Formula Discharge				
Input Data					
Channel Slope Normal Depth	0.0	02000 ft/1 0.50 ft	ft		
Section Definitions					
Station (ft)	Elevation (ft)				
	0+00		2.00		
	0+02		1.50		
	0+04		1.50		
	0+06		2.00		
Roughness Segment Definitions					
Start Station	Ending Statio	n		Roughness Coefficient	
(0+00,	2.00)	(0+06,	2.00)		0.012
Options					
Current Roughness Weighted	Pavlovskii's Method				
Open Channel Weighting Method	Pavlovskii's Method				
Closed Channel Weighting Method	Pavlovskii's Method				
Results					
Discharge		17.50 ft <sup>3</sup> /	/s		
Elevation Range	1.50 to 2.00 ft				
Flow Area		2.00 ft <sup>2</sup>	1		
Wetted Perimeter		5.66 ft			
Hydraulic Radius		0.35 ft			
Top Width					
		5.50 ft			
Normal Depth		5.50 ft 0.50 ft			
Normal Depth Critical Depth		5.50 ft 0.50 ft 0.82 ft			

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## Worksheet for Concrete Weir at Water Quality Pond #3

Results		
Velocity	8.75	ft/s
Velocity Head	1.19	ft
Specific Energy	1.69	ft
Froude Number	2.56	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.50	ft
Critical Depth	0.82	ft
Channel Slope	0.02000	ft/ft
Critical Slope	0.00286	ft/ft

## **Cross Section for Concrete Weir at Water Quality Pond #3**

Project Description		
Friction Method Solve For	Manning Formula Discharge	
Input Data		
Channel Slope	0.02000	ft/ft
Normal Depth	0.50	ft
Discharge	17.50	ft³/s
Cross Section Image		



	Overfl	ow Weir	,		
	Overni				
Project Description					
Friction Method	Manning Formula				
Solve For	Discharge				
Input Data					
Channel Slope		0.02000	ft/ft		
Normal Depth		0.50	ft		
Section Definitions					
Station (ft)	Eleva	ation (ft)			
oration (ity					
	0+00		2.00		
	0+02		1.50		
	0+04		1.50		
	0+06		2.00		
Roughness Segment Definitions					
Start Station	Ending	g Station		Roughness Coefficient	
(0+00	, 2.00)	(0+	06, 2.00)		0.069
Options					
Current Roughness Weighted	Pavlovskii's Method				
Open Channel Weighting Method	Pavlovskii's Method				
Closed Channel Weighting Method	Pavlovskii's Method				
Results					
Discharge		3.04	ft³/s		
Elevation Range	1.50 to 2.00 ft				
Flow Area		2.00	ft²		
Wetted Perimeter		5.66	ft		
Hydraulic Radius		0.35	ft		
Top Width		5.50	ft		
Normal Depth		0.50	ft		
Critical Depth		0.31	ft		
Critical Slope		0.11408	ft/ft		

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 Page 1 of 2

	Overflow Weir	
Results		
Velocity	1.52	ft/s
Velocity Head	0.04	ft
Specific Energy	0.54	ft
Froude Number	0.44	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.50	ft
Critical Depth	0.31	ft
Channel Slope	0.02000	ft/ft
Critical Slope	0.11408	ft/ft

Cro	oss Section for Irregul	lar Section - 1
Project Description		
Friction Method	Manning Formula	
Solve For	Discharge	
Input Data		
Channel Slope	0.0200	00 ft/ft
Normal Depth	0.5	50 ft
Discharge	3.04	04 ft³/s
Cross Section Image		



## Worksheet for 2' Rock Riprap Rundown

Project Description					
Friction Method	Manning Formula				
Solve For	Discharge				
Input Data					
Channel Slope		0.10000	ft/ft		
Normal Depth		0.83	ft		
Section Definitions					
Station (ft)	Eleva	ition (ft)			
	0+00		0.83		
	0+00		0.33		
	0+01		0.00		
	0+02		0.33		
	0+02		0.83		
Roughness Segment Definitions					
Start Station	Ending	Station		Roughness Coefficient	
Clart Clarton		Jolation			
(0+00, 0	0.83)	(0+	02, 0.83)		0.069
Options					
Current Roughness Weighted	Pavlovskii's Method				
Open Channel Weighting Method	Pavlovskii's Method				
Closed Channel Weighting Method	Pavlovskii's Method				
Results					
Discharge		5.15	ft³/s		
Elevation Range	0.00 to 0.83 ft				
Flow Area		1.33	ft²		
Wetted Perimeter		3.11	ft		
Hydraulic Radius		0.43	ft		
Top Width		2.00	ft		
Normal Depth		0.83	ft		
Critical Depth		0.76	ft		

Bentley Systems, Inc. Haestad Methods SoBatitile CEnterMaster V8i (SELECTseries 1) [08.11.01.03]

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## Worksheet for 2' Rock Riprap Rundown

Results				
Critical Slope		0.13928	ft/ft	
Velocity		3.87	ft/s	
Velocity Head		0.23	ft	
Specific Energy		1.06	ft	
Froude Number		0.84		
Flow Type	Subcritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Downstream Velocity		Infinity	ft/s	
Upstream Velocity		Infinity	ft/s	
Normal Depth		0.83	ft	
Critical Depth		0.76	ft	
Channel Slope		0.10000	ft/ft	
Critical Slope		0.13928	ft/ft	

## **Cross Section for 2' Concrete Rundown**

Project Description		
Friction Method Solve For	Manning Formula Discharge	
Input Data		
Channel Slope	0.10000	ft/ft
Normal Depth	0.83	ft
Discharge	5.15	ft³/s

#### **Cross Section Image**



### Worksheet for 2' Concrete Sidewalk Culvert at 2% Slope

Project Description	
Friction MethodManning FormulaSolve ForDischarge	
Input Data	
Channel Slope 0.02000 ft/ft	
Normal Depth 0.50 ft	
Section Definitions	
Station (ft) Elevation (ft)	
0+00 0.58	
0+00 0.08	
0+01 0.00	
0+02 0.08	
0+02 0.58	
Roughness Segment Definitions	
Start Station Ending Station Roughness Coefficient	
(0+00, 0.58) (0+02, 0.58)	0.013
Options	
Current Roughness weighted Pavlovskii's Method	
Open Channel Weighting Method Pavlovskii's Method	
Closed Channel Weighting Method Pavlovskii's Method	
Results	
Discharge 6.97 ft <sup>3</sup> /s	
Elevation Range 0.00 to 0.58 ft	
Flow Area 0.92 ft <sup>2</sup>	
Wetted Perimeter 2.84 ft	
Hydraulic Radius 0.32 ft	
Top Width 2.00 ft	
Normal Depth 0.50 ft	
Critical Depth 0.76 ft	

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## Worksheet for 2' Concrete Sidewalk Culvert at 2% Slope

Results				
Critical Slope		0.00550	ft/ft	
Velocity		7.61	ft/s	
Velocity Head		0.90	ft	
Specific Energy		1.40	ft	
Froude Number		1.98		
Flow Type	Supercritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Downstream Velocity		Infinity	ft/s	
Upstream Velocity		Infinity	ft/s	
Normal Depth		0.50	ft	
Critical Depth		0.76	ft	
Channel Slope		0.02000	ft/ft	
Critical Slope		0.00550	ft/ft	

### **Cross Section for 2' Concrete Sidewalk Culvert at 2% Slope**

Project Description		
Friction Method Solve For	Manning Formula Discharge	
Input Data		
Channel Slope	0.02000	ft/ft
Normal Depth	0.50	ft
Discharge	6.97	ft³/s

#### **Cross Section Image**



## **APPENDIX B**



· . . . . .

![](_page_45_Figure_0.jpeg)

![](_page_46_Figure_0.jpeg)

OF ANY PROJECT.

ALL EXISTING UTILITIES SHOWN WERE OBTAINED FROM CONTRACTOR TO CONDUCT ALL NECESSARY FIELD TO DETERMINE THE ACTUAL LOCATION OF UTILITIES AND CHANGES FROM THIS PLAN SHALL BE COORDINATED WITH AND APPROVED BY THE ENGINEER.

![](_page_46_Figure_5.jpeg)

RESEARCH, AS-BUILTS, SURVEYS OR INFORMATION PROVIDED BY OTHERS. IT SHALL BE THE SOLE RESPONSIBILITY OF THE INVESTIGATIONS PRIOR TO AND INCLUDING ANY EXCAVATION, OTHER IMPROVEMENTS, PRIOR TO STARTING THE WORK. ANY

![](_page_47_Figure_0.jpeg)

### PROPOSED DRAINAGE SOLUTION

THE EXPECTED TOTAL RUNOFF FROM THE SITE FOR THE 100-YEAR 6 HOUR EVENT IS 6.47 CFS WITH A VOLUME OF 0.231 AC-FT. ROOF DRAINS WILL COLLECT RUNOFF FROM THE PROPOSED C-STORE AND DISCHARGE DIRECTLY INTO THE FIRST FLUSH BASINS. PER DPM CHAPTER 22.9.E, TABLE 1 ALL FUELING STATIONS MUST DEMONSTRATE CONTROL OF OIL FROM VEHICLE PARKING AREAS. BASIN B4 COVERS THE MAJORITY OF THE PAVEMENT AREA, INCLUDING ALL OF THE SHEET FLOW GENERATED FROM THE RE-FUELING AREA UNDER THE CANOPY, AND SHEET FLOW IS DIRECTED TO A SINGLE MODIFIED OIL-WATER SEPARATOR TYPE C CURB INLET AT THE NORTH EAST CORNER OF THE SITE. THE CURB INLET HAS THE CAPACITY OF 3.87 CFS AND WILL CONVEY THE CALCULATED 2.87 CFS THAT WILL FLOW TO INLET. THE SINGLE INLET WILL BE MODIFIED TO INCLUDE A 24-INCH DEEP SUMP BOX AND INSTALLATION OF A BAFFLE PLATE TO RESTRICT THE PASSING OF TRASH WITH A 12-INCH BY 12-INCH EXFILTRATION OPENING AT THE BASE OF THE CONCRETE BOX TO RELEASE THE STORMWATER HELD IN THE SUMP. FOR THE DESIGNED SUMP DEPTH OF 24-INCHES THE BOX INLET WILL RETAIN 130 GALLONS WHICH IS ADEQUATE FOR ANY MAJOR FUEL SPILL/S THAT MAY OCCUR DURING OPERATIONS AT THE SITE. DURING REGULAR SITE MAINTENANCE THE INLET SHALL BE CLEANED OF DEBRIS AND SEDIMENT THAT ACCUMULATES OVER TIME IN THE SUMP.

A 12-INCH STORM DRAIN IS CONNECTED TO THE INLET BOX AND DISCHARGES THE TREATED STORMWATER DIRECTLY TO THE FIRST FLUSH POND LOCATED AT THE NORTH EAST CORNER OF THE PARCEL. THE WATER QUALITY POND #3 WILL RETAIN A VOLUME OF 800 CUBIC FEET BEFORE RELEASING THE ADDITIONAL FLOW TO COMANCHE ROAD RIGHT-OF-WAY THROUGH A CONCRETE WEIR AND A 2-FOOT CONCRETE RUNDOWN / SIDEWALK CULVERT CONFORMING TO THE SO19 PERMIT. ALL OTHER SITE RUNOFF GENERATED FROM THE PERVIOUS AREAS (BASINS B2, B4 AND B5) WILL BE CONVEYED AS SURFACE FLOWS TO THE ON-SITE CURB AND GUTTERS AND BE RELEASED VIA CURB CUTS TO THE RESPECTIVE FIRST FLUSH PONDS.

THE POND #1 HAS THE CAPACITY TO RETAIN A VOLUME OF 660 CUBIC FEET. AT THE DESIGNED INLET ELEVATION ADDITIONAL FLOW SHALL ENTER THE PROPOSED NYLOPLAST 12-INCH DOME INLET AND DRAIN BASIN AND BE CONVEYED THROUGH AN 8-INCH HDPE STORM PIPE. THIS STORM PIPE IS CONNECTED TO THE NYLOPLAST 12-INCH DOME INLET PROPOSED AT THE WATER QUALITY POND #2. THIS POND IS ASSOCIATED WITH THE RUNOFF FROM BASIN B5 WHICH TOTALS 0.98 CFS. IN THE CASE OF A BLOCKAGE AT AN INLET, EMERGENCY OVERFLOW RIPRAP RUNDOWNS ARE PROPOSED. THE WATER QUALITY POND #2 HAS THE CAPACITY TO RETAIN A VOLUME OF 580 CUBIC FEET. AT THE DESIGNED INLET ELEVATION THE ADDITIONAL FLOW SHALL ENTER THE INLET AND INTO THE 12-INCH HDPE STORM DRAIN. THIS STORM DRAIN PASSES THE ADDITIONAL FLOWS FROM BASINS B2 AND B5, A TOTAL OF 2.44 CFS. ALL SITE RUNOFF GENERATED FROM THE LANDSCAPED SLOPE AREAS (BASINS B1 AND B6) WILL FREELY DISCHARGE TO THE NORTH AND WEST INTO THE RESPECTIVE RIGHT-OF-WAYS. A SMALL PORTION OF RUNOFF TOTALING 0.05 CFS DISCHARGES DIRECTLY INTO THE PRINCETON DRIVE RIGHT-OF-WAY AT THE DRIVEWAY ENTRANCES (BASINS BB AND B9), NO OFFSITE DRAINAGE IMPROVEMENTS ARE PROPOSED IN THE DOT RIGHT-OF-WAY,

Basin Descriptions								100-Year, 6-Hr			10-Year, 6-Hr			Water Q				
Basin	Area	Area	Area	Treatment A	T	reatment	t B 1	Freatment	t C	Treatment D		Weighted E	Volume	Flow	Weighted E	Volume	Flow	FF Pond
ID	(sf)	(acres)	(sq miles)	%	(acres)	%	(acres)	%	(acres)	%	(acres)	(in)	(ac-ft)	cfs	(in)	(ac-ft)	cfs	Required
1	4,793	0.11	0.00017	0%	0.000	100%	0.110	0%	0.000	0%	0.000	0.780	0.007	0.25	0.280	0.003	0.10	0
2	16,120	0.37	0.00058	0%	0.000	32%	0.118	0%	0.000	68%	0.252	1.691	0.052	1.45	1.001	0.031	0.90	255
3	1,477	0.03	0.00005	0%	0.000	100%	0.034	0%	0.000	0%	0.000	0.780	0.002	0.08	0.280	0.001	0.03	0
4	26,570	0.61	0.00095	0%	0.000	0%	0.000	0%	0.000	100%	0.610	2.120	0.108	2.87	1.340	0.068	1.92	619
5	9,939	0.23	0.00036	0%	0.000	16%	0.037	0%	0.000	84%	0.192	1.906	0.036	0.98	1.170	0.022	0.64	195
6	10,066	0.23	0.00036	0%	0.000	10%	0.023	90%	0.208	0%	0.000	1.095	0.021	0.71	0.496	0.010	0.38	0
7	1,440	0.03	0.00005	0%	0.000	100%	0.033	0%	0.000	0%	0.000	0.780	0.002	0.08	0.280	0.001	0.03	0
8	397	0.01	0.00001	0%	0.000	0%	0.000	0%	0.000	100%	0.009	2.120	0.002	0.04	1.340	0.001	0.03	9
9	135	0.00	0.00000	0%	0.000	0%	0.000	0%	0.000	100%	0.003	2.120	0.001	0.01	1.340	0.000	0.01	3
Total	70,937	1.63	0.003		0.000		0.355		0.208		1.065		0.231	6.470		0.136	4.039	1,081

## CURRENT SITE DRAINAGE

NO OFFSITE FLOWS ENTER THE SITE. THE SITE IS BOUNDED BY DEVELOPED STREETS AND A BUILDING WAREHOUSE TO THE SOUTH. THE PROPERTY DRAINS TO PRINCETON DRIVE FROM THE EAST AND SOUTH SIDES; TO THE NORTH SIDE TO COMANCHE ROAD AND TO THE WEST TO THE 1-25 FRONTAGE ROAD. THE ENTIRE SITE SHEET FLOWS TO THESE DISCHARGE LOCATIONS WITH NO DRAINAGE INFRASTRUCTURE INSTALLED. THE PEAK DISCHARGE CALCULATED FOR THE SITE MATCHES THE APPROVED PEAK DISCHARGE PRESENTED IN THE 1995 DRAINAGE REPORT FOR THE PARCEL OF 6.6 CFS FOR THE 100-YEAR 6 HOUR EVENT.

Excess Precip	vitation, E (in.)		Peak Discharge (cfs/acre)				
Zone 2	100-Year	10-Year	Zone 2	100-Year	10-Year		
Ea	0.53	0.13	Qa	1.56	0.38		
Eb	0.78	0.28	Qb	2.28	0.95		
Ec	1.13	0.52	Qc	3.14	1.71		
Ed	2.12	1.34	Qd	4.70	3.14		

)

Pipe Capac	city						
Pipe	D	Slope	Area	R	Q Provided	Velocity	<b>Q</b> Required
	(in)	(%)	(ft^2)		(cfs)	(ft/s)	(cfs)
PVC	4	1.00	0.09	0.083	0.23	2.58	~
PVC	6	1.00	0.20	0.125	0.66	3.39	
HDPE	8	1.50	0.35	0.167	1.48	4.25	1.45
HDPE	12	1.40	0.79	0.250	4.23	5,38	2.44
HDPE	12	1.85	0.79	0.250	4.86	6.19	2.87

 $\frac{\text{Manning's Equation:}}{Q = 1.49/n * A * R'(2/3) * S'(1/2)}$  A = Area R = D/4 S = Slope  $n = 0.011 \quad PVC$   $n = 0.013 \quad HDPE$ 

Water Quality Volume - "First Flush Pond" - Redevelopment Site

Total Impervious Area =

Retainage depth =  $0.28^{\circ}$ 

Retention Volume =

## CAUTION

ΣArea in "Treatment D"

=0.0233 x area CF

foot

0.0233

ALL EXISTING UTILITIES SHOWN WERE OBTAINED FROM RESEARCH, AS-BUILTS, SURVEYS OR INFORMATION PROVIDED BY OTHERS. IT SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR TO CONDUCT ALL NECESSARY FIELD INVESTIGATIONS PRIOR TO AND INCLUDING ANY EXCAVATION, TO DETERMINE THE ACTUAL LOCATION OF UTILITIES AND OTHER IMPROVEMENTS, PRIOR TO STARTING THE WORK. ANY CHANGES FROM THIS PLAN SHALL BE COORDINATED WITH AND APPROVED BY THE ENGINEER.

![](_page_47_Figure_15.jpeg)