CITY OF ALBUQUERQUE



April 10, 2015

Eugenio Valdez, P.E. Wilson & Company, Inc. 4900 Lang Ave. NE Albuquerque, NM 87109

Re: El Dorado High School

Drainage Master Plan (G22D004) Engineer's Stamp Date 1-16-2015

Dear Mr. Valdez,

Based upon the information provided in your submittal received 1-16-15, the above referenced submittal is approved. It is our understanding that the improvements to this site have already been made, so a Grading and Paving Permit are not necessary.

In should be noted that NOAH Atlas 14 Precipitation Frequency estimates were used as opposed to that shown in the DPM Table A.2. (based on NOAH Atlas 2). As such, the flowrates were about 15% less than that of the original Drainage Master Plan for this site. Future improvements should be based on those values used in the DPM.

Albuquerque If you have any questions, you can contact me at 924-3695.

New Mexico 87103 Sincerely,

www.cabq.gov

Rita Harmon, P.E.

Senior Engineer, Planning Dept. Development and Building Services

Orig: Drainage file

c.pdf via Email: Recipient, Monica Ortiz,

ELDORADO HIGH SCHOOL DRAINAGE MASTER PLAN

January 2015



Prepared For:

APS Facilities Planning & Construction
City of Albuquerque

Prepared By:

Wilson & Company
4900 Lang Avenue NE
Albuquerque, NM 87109

Project # 12-600-025-00

ELDORADO HIGH SCHOOL DRAINAGE MASTER PLAN

JANUARY 2015

I, Eugenio Valdez, P.E., do hereby certify that this report was prepared under my direction and review and that I am a duly registered Professional Engineer under the laws of the State of New Mexico.

Eugenio Valdez, P.E. NMPE No. 18404	
ACCEPTED BY:	
City of Albuquerque	Date



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Eldorado High School Drainage Master Plan

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Appendix B Hydraulic Calculations, AHYMO model results and NOAA Atlas 14 Storm

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1 Introduction

Eldorado High School is located in the city of Albuquerque. Established in 1970, the High School has approximately 2,400 students. The Albuquerque Public Schools Facilities Department is currently developing Master Plans for each of the schools within the District. Plans for Eldorado High School include asphalt pavement, concrete removal and replacement, analysis of existing storm drainage system and expansion and repair of the Math, Humanities, and Gymnasium Buildings.

The urban campus, in addition to core buildings and vehicle parking lots, includes three baseball fields, football field, soccer field, and a paved band practice area.

1.1 Purpose

The purpose of this report is to evaluate existing on-site drainage conditions and recommend drainage patterns and concepts for drainage system infrastructure improvements required for the campus. At the time of this analysis, specific details regarding the phasing of the various elements of the proposed redevelopment are not known. Thus, this document provides drainage planning required for the final full build-out condition.

It is anticipated that detailed design of each of the individual recommended drainage improvements will be completed in tandem with subsequent phases of improvements, including paving and building renovations.

1.2 Existing Plans and Reports

The following previous reports and plans were used to provide data and site conditions in support of the hydrologic and hydraulic analyses:

"Eldorado High School Additions and Renovations, Building A- Music Building/PAC," Alliance Fire Protection, Inc., Albuquerque, NM, 2009.

"As-Built Drawing for PAC Addition," Wilson & Company, Albuquerque, NM, June 2009.

"Eldorado High School Reroofing Project – Lecture Hall, Upper and Lower Roof," Allison Engineering, Inc., Albuquerque, NM, July 2008.

"Albuquerque Public Schools Eldorado High School, Additions and Renovations, Building B-Gymnasium," Weller Architects, Albuquerque, NM, December 2007.

"Albuquerque Public Schools Eldorado High School, Additions and Renovations, Music Building/PAC/Restrooms," Weller Architects, Albuquerque, NM, December 2007.

"Courtyard Sanitary Sewer Replacement, Eldorado High School," Jeff Mortensen & Associates, Inc., Albuquerque, NM, April 2000.

"Eldorado High School Track and Field Improvements," Wilson & Company, Albuquerque, NM, July 1999.



Eldorado High School Drainage Master Plan

"Drainage Management Report, Eldorado High School Science Building," SMPC Architects, Albuquerque, NM, October 1997.

"Eldorado High School Science Building," SMPC Architects and Bohannon-Huston, Albuquerque, NM, October 1997.

"Eldorado High School Master Drainage Plan," SMPC Architects, Albuquerque, NM, July 1997.

"Eldorado High School Soccer Field," Dennis C. Wilkinson & Associates, P.A., November 1995.

"Construction Plans for Eldorado High School 1992 Site Improvements," Jeff Mortensen & Associates, Inc., Albuquerque, NM, March 1992.

The plans and reports listed above provided information regarding existing drainage infrastructure, grading and drainage assumptions, and boundary information that served as the basis for the development of the proposed Drainage Master Plan. A surveyed topographic information was used to supplement LIDAR generated on-site contour data provided by the city of Albuquerque, to more closely reflect current grading conditions. It should be noted that only the LIDAR contour data is shown on the drainage maps included in this report.

1.3 Site Location

Eldorado High School is located on approximately 55 acres of land in the northeast section of Albuquerque (see Figure 1, Vicinity Map). The physical address of the High School is 11300 Montgomery Boulevard NE. The lot is triangular, with Montgomery Boulevard crossing on the north side of campus, Juan Tabo Boulevard on the west, and Eagle Trail and the city of Albuquerque Embudito Arroyo Channel forming the diagonal on the south and east side of the property. As an additional reference, this site can also be found within Zone G-22 on the Albuquerque Zone Atlas Map.



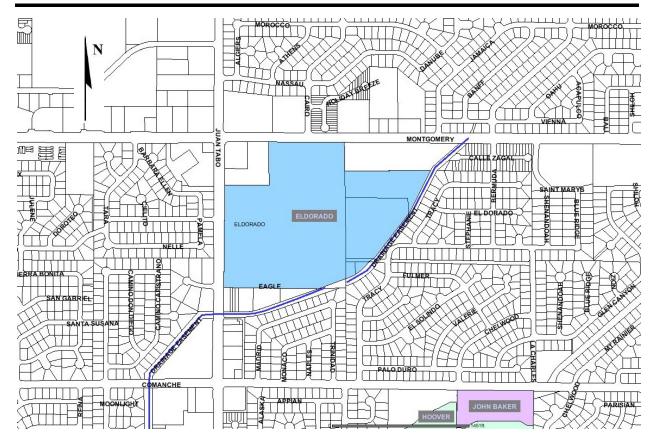


Figure 1: Vicinity Map

No portion of the existing site is located within a FEMA designated flood hazard zone as illustrated on FEMA Flood Insurance Rate Map (FIRM) Map Number 35001C0144G, revised September 26, 2008. The map indicates the presence of a Zone A floodplain along the diagonal on the south and east side of campus. This floodplain is associated with the Embudito Arroyo Channel. A copy of the FIRM map is included as Appendix A of this report.

1.4 Planning History

The existing drainage plans and reports, as outlined in Section 1.2, were used to identify the locations of storm drain inlets and grates, roof drains and downspouts, and existing drainage swales and channels. Multiple site visits were made to verify the location, size, and condition of the referenced drainage structures.

2 Hydrology

The Embudito Arroyo is located on the southeast side of the Eldorado High School campus. This project area lies within Precipitation Zone 4 as defined in Section 22.2, Hydrology, of the Development Process Manual (DPM) for the city of Albuquerque and the Albuquerque Metropolitan Arroyo Flood Control Authority (AMAFCA). Precipitation for the purposes of this study was determined using NOAA Atlas 14. Basin peak flows and volumes for the studied



Eldorado High School Drainage Master Plan

area were computed using the Arid Lands Hydrologic Model (AHYMO-S4). The AHYMO model results for both the existing and proposed conditions are included as Appendix B.

2.1 Methodology

The AHYMO Computer Program follows the procedures outlined in Chapter 22 of the DPM, dated July 1997. The program's input parameters were created by AMAFCA, in conjunction with the city of Albuquerque.

The Upland/Lag Time procedure, used in this model run, is based on the NRCS Upland Method for sub-basins shorter than 4,000 feet. The Muskingum-Cunge Method is used to route the calculated hydrographs through the channel reaches.

2.2 Design Storm Precipitation

The principle design storm used for the analysis of the existing and proposed drainage system is the 100-Year, 6-hour event. The principle storm was utilized in calculating peak runoff while the 100-Year, 24-hour event storm was utilized in determining runoff volumes for design of detention ponds. NOAA Atlas 14 shows that precipitation depths near the Eldorado campus are P_{60} =1.87 inches, P_{360} =2.51 inches, and P_{1440} =3.08 inches. NOAA Atlas 14 data is included in Appendix B.

2.3 Land Treatments

Four land treatments are defined by the DPM. Table A-4 of Section 22.2 of the DPM describes land contributions for each treatment. The following sections describe how the percentages of land treatments were determined for use in the current analysis.

2.3.1 Existing Land Treatment

Existing on-site land treatments were delineated using 2012 aerial photography acquired from the Bernalillo County Website, 2010 LIDAR contour data, and historical construction and survey drawings. Soil information for the site was obtained from the NRCS Web Soil Survey. A copy of the soils report is included as Appendix C.

2.3.2 Proposed Land Treatment

The Eldorado High School Master Site Priority Plan (Figure 2) illustrates the proposed location and approximate sizes of future buildings, parking lots, and landscaped areas. These were included in the proposed model where estimating runoff potential. Although all proposed improvements will not be constructed in 2013-2015, the Master Plan was used for proposed land treatments. Figure 3 illustrates which proposed improvements will be constructed in 2013-2015 and which are Master Plan improvements. Land use assumptions have been divided into two categories: treatment C and treatment D.

Treatment C, as defined in Chapter 22.2 of the DPM, refers to areas containing soil compacted by human activity, with minimal vegetation, unpaved parking, roads, and trails. It also refers to steep slopes with minimal desert landscaping.



Eldorado High School Drainage Master Plan

Treatment D is defined as impervious areas, including pavement and roofs. For the purpose of the Eldorado site, this treatment was used primarily within the central campus and paved areas. It also includes the concrete conveyance channel.

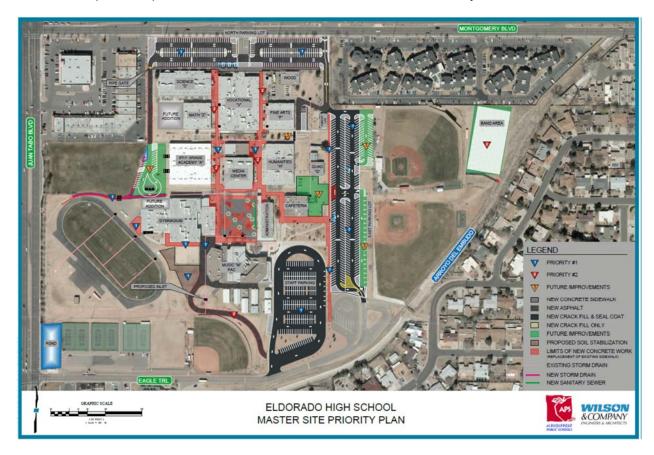


Figure 2: Master Site Priority Plan



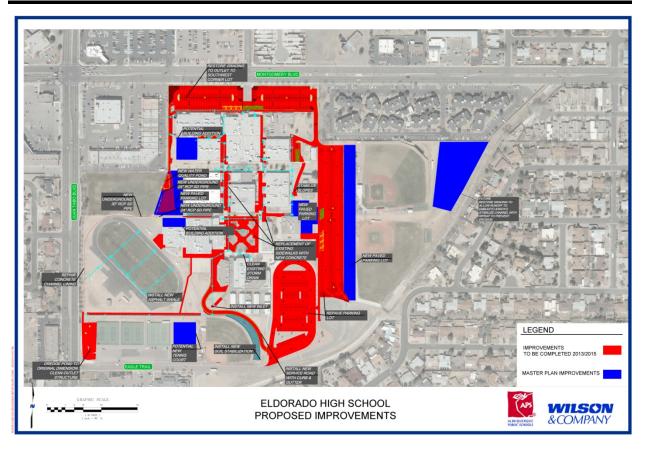


Figure 3: Proposed Improvements

2.4 Time of Concentration

In accordance with DPM Chapter 22, Equation B-9, the time to peak (t_p) is equal to $\frac{2}{3}$ of the time of concentration (t_c) . Based on the small sub-basin size, the times of concentration for the existing and proposed conditions in the on-site hydrologic analysis have been estimated to be 12 minutes or less. Thus, in accordance with the DPM, minimum time-to-peak values of 0.1333 hours were used in the AHYMO model.

2.5 Peak Discharge Rates

Peak discharge rates for existing and proposed conditions were calculated using the AHYMO computer program as outlined in the DPM. Soils report data obtained from the NRCS Web Soil Survey indicated that the primary soils in and around the subject site are classified as Hydrologic Soil Group B or the Embudo-Tijeras Complex (EtC). Bulking factors were not considered in this analysis due to the fact that the campus is not subject to off-site or undeveloped runoff. The soils are described in the Soil Survey as well-drained and having a moderately low runoff potential. Peak discharge rates for the existing and proposed conditions are presented in Tables 1 through 6 in Section 4 of this report.



3 Hydraulics

Basic hydraulic capacity calculations were performed on the existing storm drain system using basic hydraulic equations. Outlet structure calculation spreadsheets can be found in Appendix B.

4 Hydrologic and Hydraulic Analysis

4.1 Existing Site Description

As illustrated in Figure 9, Existing Conditions Basin Map, the existing campus is almost completely developed. The playing fields and the transition areas from the campus to the track and lower baseball fields are pervious and only partially landscaped. The east campus baseball fields, track, and soccer fields are well-vegetated and level. The main campus is primarily impervious with concrete pads throughout, sidewalks and concrete walkways between buildings, and asphalt paved parking.

Existing on-site topography slopes generally from the northeast to the southwest. There are steep slopes on the west and southwest side of the cluster of academic buildings. Several slopes have been stabilized with asphalt and wire-wrapped riprap where there is evidence of surface runoff. The west side of the 9th Grade Academy is used as an informal parking area and has no landscaping or slope stabilization. This area and the slope on the west side of the Gymnasium are reported to carry sediment onto the track. There are some informal retaining walls that have been stacked, but not anchored, on the northeast and east sides of the track to minimize transport of sediment onto the track surface and field areas.

The existing drainage system includes both surface and storm drain discharge. The storm drain system was designed to overflow to the lower sections of the campus, primarily towards a concrete lined channel located on the west side of the campus and the southwest corner of the site. The surface flow is carried over asphalt and riprap swales between the Science Building and 9th Grade Academy, located south of the Academy, and south of the Gymnasium. The storm drain system collects flow at inlets throughout the campus and discharges to the surface between the Gymnasium and the 9th Grade Academy, and south of the track. A separate storm drain system carries flow from the central area of the campus and north side of tennis courts to an existing 12-inch city storm sewer pipe within Juan Tabo Boulevard.

4.2 Existing Conditions Analysis

The following sections discuss existing site drainage patterns and define drainage issues that have been identified through analysis and multiple site inspections. Figure 9 outlines the existing drainage patterns, analysis basins, analysis points, and flow rates associated with the existing conditions. Peak flow rates, volumes, and basin areas are also provided in Table 1.



Eldorado High School Drainage Master Plan

For the purposes of discussion, the site has been subdivided into four regions which include the pond system, Juan Tabo city storm drain system, surface flow into the Embudito Arroyo system, and surface flow into Eagle Trail city storm drain system, shown on Figure 10.

4.2.1 Pond System

The basins flowing into the pond system include the north parking lot (Basin 103), academic buildings (Basin 104), half the soccer field (Basin 102B), track (Basin 101A), area surrounding the track to the south (Basin 101B), tennis courts (Basin 109A), and the parking lot near tennis courts (Basin 109B), and the primary detention pond (Basin 112). The total watershed for this area encompasses approximately 22 acres. Runoff from this area is discharged into the detention pond.

Surface runoff produced within Basins 103 and 104 is conveyed through concrete swales, curb and gutter sections and existing underground storm drain pipes then into a concrete channel which discharges into the detention pond. This pond collects flow indirectly from the central campus, the north parking area, the soccer field, and the track.

The south side of the soccer field, Basin 102B, slopes towards the southwest and into the concrete drainage ditch leading to the detention pond. It appears that the field may drain into other sections of the channel on the south side but the well-vegetated area is not showing signs of erosion. On the east side of the soccer field there is a 30-inch culvert under an access walkway. Analysis of the culvert section indicates that it has sufficient capacity to convey storm water generated in Basins 103 and 104 to the north and east. This culvert has minimal sediment.

The existing rough concrete channel extends along the south and east side of the soccer field, then west of the track into the detention pond. The channel is trapezoidal and is approximately 5 feet wide and 2 feet deep. It is finished in rough concrete and inset with rocks. Installed in 1992, it has several sections that appear to have been repaired or replaced. Other sections are cracked and have weeds growing through them.

Basin 101A includes the track and a sloped area to the east of the track below the Gymnasium. This area was renovated in 1999 to include six 12-inch inlets. Flows from these inlets is conveyed under the track and discharge into the concrete channel that discharges into the detention pond through a 36-inch RCP (Reinforced Concrete Pipe). The slope to the east of the track shows minor erosion. Bricks have been stacked in several areas to impede the sediment, but the informal retaining wall has collapsed in certain sections.

Basin 109A contributes a small amount of flow to the pond on the north side of the tennis courts. Basin 109B drains directly into the pond through a concrete run-down structure.



The detention pond is located within Basin 112. The pond is partially vegetated, with a large tree in the center, and has accumulated sediment over time. The estimated existing residual volume is 1.14 acre-feet, indicating approximately 0.10 acre-feet of sediment in the pond. Flows discharge into the pond from the existing concrete channel that transitions the flow into a 36-inch RCP, a concrete rundown on the northeast corner, and a concrete run-down from the parking lot near the tennis courts. The raised 4 foot by 4 foot outlet structure includes a 36-inch RCP that is connected to the Juan Tabo city storm drain system(See Figure 4 and 5).

According to the July 1997 Eldorado High School Master Drainage Plan, prepared by Bohannan Huston, the peak outlet discharge from the pond is to be 92.1 cfs if an existing 24" CMP located in Basin 102B was upsized. As mentioned above there is currently a 30"-culvert and analysis of the culvert section indicates that it has sufficient capacity to convey storm water generated in Basins 103 and 104. Field survey indicates the top elevation of the outlet structure is 5697.05 ft with the pipe invert at 5688.58 ft. Currently, the weep holes are clogged with gravel and need to be cleaned (See Figure 5). The pond also has an emergency spillway that out-falls to Eagle Trail. The emergency spillway crest elevation is 5699.5 ft. Since the weep holes are currently clogged, only 2 holes at the top were modeled to outflow.



Figure 4: Pond Outlet Structure looking South-West



Figure 6: Pond Outlet Structure



Figure 5: Weep Hole



4.2.2 Juan Tabo

The Juan Tabo system can be separated into surface runoff and storm drain runoff. The surface runoff comes from the north part of the soccer fields (Basin 102A) and the storm drain flow originates from the campus/courtyard. Roof drains and walkway runoff is captured throughout the campus and are tied into existing 8-inch and 12-inch RCP. The total area encompasses approximately 1 acres for surface runoff and 4 acres toward the storm drain.

Storm water captured in the central system is conveyed and discharged to the city storm drain along Juan Tabo Boulevard.

Irregular maintenance is evident throughout campus as inlets are full of leaves, trash, and sediment. Several places through the central concrete walkways show evidence of water damage and ponding.

The storm drain system within Basin 105 is part of the original storm drain system constructed during the original construction of the campus. Based on the area draining to this system, it is evident that it is undersized. Therefore, excess surface flow is conveyed south of the basketball court, down a partially stabilized slope, and into the lower baseball field and Eagle Trail. This is one area that contributes substantial sediment deposition and shows evidence of significant erosion.

4.2.3 Embudito Arroyo system

The Embudito Arroyo system includes the parking lots (Basins 106 and 107), the lower baseball diamond and portables (108A), the east baseball fields (Basin 110) and the band area (Basin 111). The watershed has total drainage area of 21 acres. All basins discharge directly into the Embudito Arroyo. All basins with the exception of Basin 108A, are paved and flows discharge across Eagle Trail and into the Embudito Arroyo. There is a shallow concrete swale that diverts flow from the Eagle Trail through a parking lot and into the Embudito Arroyo for all basins except for Basin 111, which discharges directly into the arroyo through an earthen swale.

The northeast portion of Basin 108A includes a steep, unstabilized slope than is significantly eroded and rilled. The sediment deposited in the lower portion is likely to wash onto Eagle Trail. There is an outlet on the south side of Basin 108A that is damaged, filled with weeds, and located at a higher grade than the actual field. It appears that the majority of the flow at this point comes from the unpaved entrance just west of the staff parking entrance.

The east parking lot, Basin 110, discharges to the east of the bus lot. This bus area is graded almost a foot higher than the east parking lot. The turnaround area on the north end creates a small ponding area.

Basin 110 consist of the two primary baseball diamonds and Basins 111 is the band practice area. While this area is vegetated and permeable, the grading allows ponding to occur on the southern field around the backstop. The upper (northern) field drains



into the lower, carrying sediment. There is a concrete berm around the southwest portion of the field that controls runoff from the lower field. However, there is also a drainage swale on the west side that should carry flow from the parking area to Eagle Trail.

The band practice area is paved and graded to discharge to the Embudito Arroyo. The transition outlet is not stabilized but there is an obvious swale and some riprap to indicate that the water flows to the Channel.

4.2.4 Eagle Trail city storm drain system

The city storm drain system on Eagle Trail includes runoff from area east of the track and the softball practice area just east of the tennis courts (Basin 108B). The total area encompasses approximately 5 acres. This area drains onto Eagle Trail and enters into the Juan Tabo storm drain through curb inlets.

4.2.5 Existing Conditions Hydrologic Analysis Summaries

The AHYMO model was developed based on the general land use and topographic characteristics of each of the sub-basins. Flow was routed through the existing hydraulic structures and either to the pond, the existing city storm drain system, or the Embudito Arroyo. Each of the structures was evaluated to verify that the rated capacity was sufficient to accommodate the calculated flow rates. The storm drain, channel, and pond were determined to have adequate capacity for the 100-year storm event. The sole exception was the courtyard area, where the current storm drain pipe is undersized and does not have the capacity to convey the flows generated from the surrounding structures and concrete walkways.

Table 1 summarizes the assumptions for land use, sub-basin areas, peak flow rates, and runoff volumes associated with the 14 analyzed sub-basins.

Table 1: Existing Sub-Basin Peak Discharge and Volumes

Sub-Basin	Area	Land Treatment Percentage (%)		Q _{100 6} (cfs)	V _{100,24} (ac-ft)
	(Acres)	С	D	,	,
101A	3.46	65.8%	34.2%	12.69	0.491
101B	4.64	80.2%	19.8%	16.13	0.562
102	2.60	100.0%	0.0%	8.38	0.242
103	4.04	5.0%	95.0%	17.97	0.924
104	8.36	14.2%	85.8%	35.94	1.809
105	3.62	13.7%	86.3%	15.70	0.783
106	3.85	8.9%	91.1%	16.90	0.857
107	3.75	14.7%	85.3%	16.20	0.805
108A	4.03	65.4%	34.6%	14.79	0.574
108B	1.25	58.8%	41.2%	4.71	0.190
109A	1.30	15.2%	84.8%	5.61	0.277



Sub-Basin	Area	Land Treatment Percentage (%)		Q _{100,6} (cfs)	V _{100,24} (ac-ft)
	(Acres)	С	D		
109B	0.90	0%	100%	4.06	0.212
110	9.39	93.6%	6.4%	31.02	0.959
111	1.59	33.3%	66.7%	6.51	0.300
112	0.34	83.5%	16.5%	1.19	0.039

Table 2 summarizes the contributing peak flow rates and runoff volumes at 11 Points.

Table 2: Existing Analysis Point Peak Discharge and Volumes

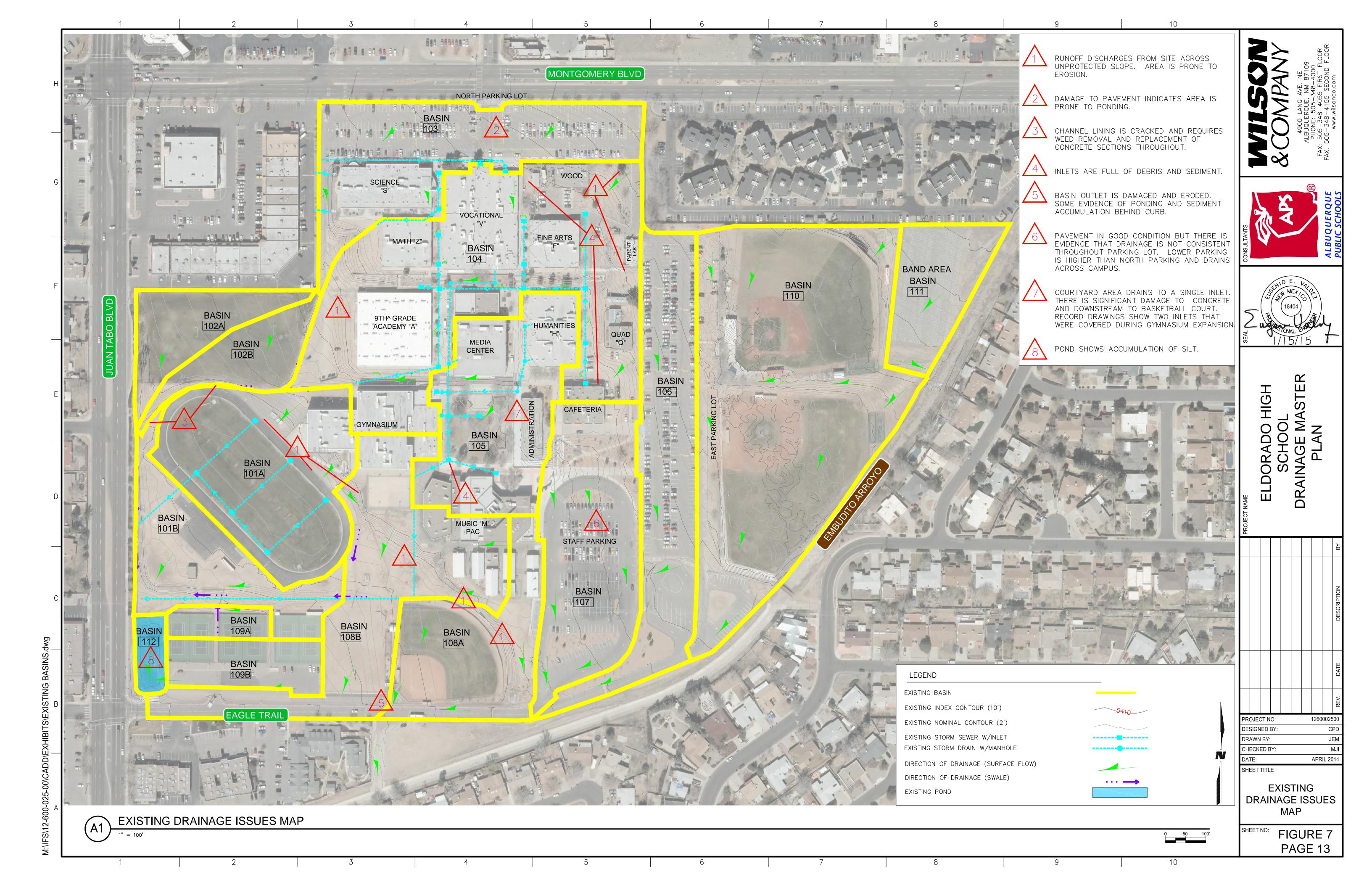
Analysis Point	Q _{100,6} (cfs)	V _{100,24} (ac-ft)
AP-1	70.28	4.140
AP-2	53.25	2.734
AP-3	56.93	2.842
AP-4	69.56	3.738
AP-5	13.60	0.766
AP-6	63.45	2.623
AP-7	73.49	3.017
AP-8	77.37	4.140
AP-9	6.37	0.296
AP-10	17.27	0.707
AP-11	4.29	0.126

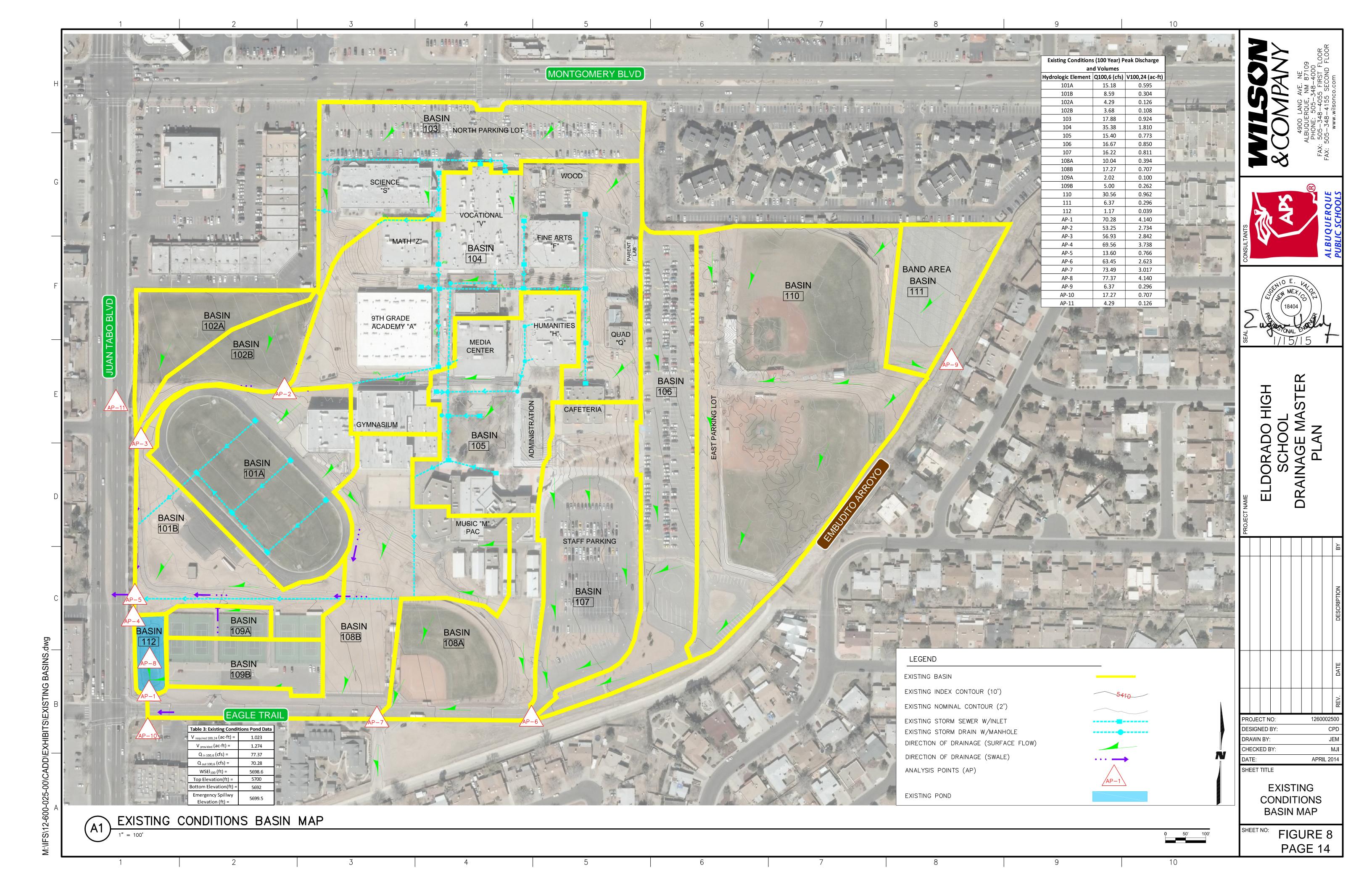
Table 3 summarizes the existing conditions pond.

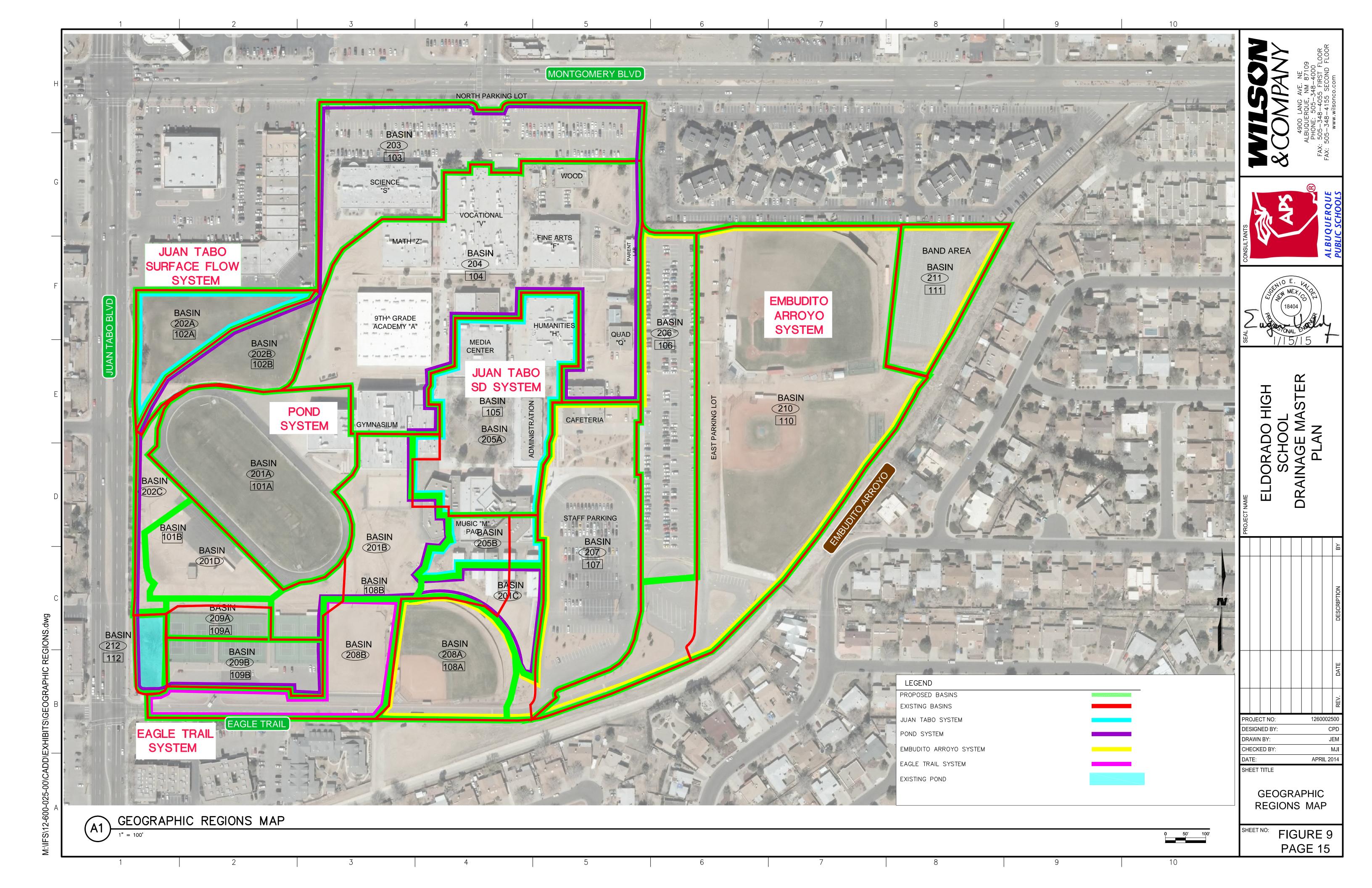
Table 3: Existing Conditions Pond Data

V _{required 100,24} (ac-ft) =	1.023	
V provided (ac-ft) =	1.274	
Q in 100,6 (cfs) =	77.37	
Q _{out 100,6} (cfs) =	70.28	
WSEI ₁₀₀ (ft) =	5698.6	
Top Elevation(ft) =	5700	
Bottom Elevation(ft) =	5692	
Emergency Spillway Elevation (ft) =	5699.5	
Outfall Box Top Elevation (ft) =	5697.05	
Outfall Box Bottom Elevation/ 36"	5688.58	
RCP Outfall Pipe Invert (ft) =	3008.38	









4.3 Water Quality Treatment

At the time of this report, the city of Albuquerque is in the process of adopting new standards for water quality treatment for new and redevelopment projects. Based on discussions with city development services, the new standard includes extended detention times for storage ponds, as well as sediment control.

The proposed drainage improvements and the improvements to the parking areas included in the Master Site Priority Plan take these new standards into consideration.

The water quality pond proposed for the new parking area to the west of the 9th Grade Academy incorporates an interceptor pond that is designed to allow both sedimentation and evaporation of parking lot runoff. Various improvements throughout the system incorporate both slope stabilization and optimization of existing hydraulic systems to minimize sediment transport both to the pond and the city storm drains and inlets.

A proposed water quality manhole will be included for Basin 206 and discharge into the Embudito Arroyo. A 24-inch ADA pipe and inlet are proposed.

4.4 Proposed Site Description

The proposed site improvements in this Drainage Master Plan are limited to the boundaries of the existing campus. The Master Site Priority Plan proposed several improvements to key areas including pavement replacement and repair. These improvements, particularly the paving, contribute to additional surface runoff by increasing impermeable surface areas, minimizing the sedimentation, and better directing flow into the existing storm drain system. The primary improvements proposed in this Drainage Plan include repair and replacement of existing structures and slope stabilization. Proposed improvements are separated into those improvements to be completed in 2013-2015, and Master Plan improvements to be completed in the future.

4.5 Proposed Drainage Improvements

Proposed drainage improvements and drainage patterns are shown in Figures 7 and 8. The primary components of the proposed plan are listed below:

Improvements to be completed in 2013-2015

- Restore grading on north student parking lot and west service road and repave to prevent ponding
- Repair concrete channel and replace approximately 300 feet of channel with 30-inch RCP
- Construct new service road with curb and gutter
- Construct new inlet
- Clean inlets in courtyard area and upsize existing drainage storm drain pipes
- Construct a new water quality pond and new underground 24" RCP
- Dredge pond to original dimensions and clean outlet structure
- Stabilize slopes around cafeteria and parent lab



- Reseal staff parking lot and east student parking lot
- Replacement of existing concrete sidewalks with new concrete
- Construct a new inlet and water quality manhole

Master Plan Improvements to be completed in the future

- Add staff parking lot at cafeteria
- Pave parking lot on east side
- Soil stabilization near south baseball field
- Building additions and potential artificial turf athletic field
- Pave parking lot west of the 9th Grade Academy
- Restore grading in band area to allow runoff to Embudito Arroyo and stabilize channel with riprap to prevent erosion

4.6 Proposed Drainage Improvements and Analysis Details

The following sections provide detailed discussion of the proposed drainage patterns and drainage improvements for Eldorado High School. Figure 11 shows the analysis basins, design points, and flow rates for the proposed conditions. Figure 12 illustrates the location of various improvements throughout the campus. Peak flow rates, volumes, and basin areas are provided in Table 4.

4.6.1 Pond System

The basins flowing into the pond system include the north parking lot (Basin 203), academic buildings (Basin 204), half the soccer field (Basin 202B), track and field and surrounding areas (Basin 201A, 201C), tennis courts (Basin 209A), and the parking lot near tennis courts (Basin 209B), and the primary detention pond (Basin 212) and the overflow from track and field (Basin 201B and 201D). It also includes the proposed water quality pond downstream of Basin 203.

Improvements to be completed in 2013-2015

In Basin 203, the repaving and regrading of the north parking lot will prevent ponding and subsequent damage to the asphalt. No additional drainage improvements are recommended for that area.

The primary pond (Basin 212) cross-section, as determined by the field survey, is irregular and shows evidence of accumulated sediment. The outlet structure has accumulated debris. It is recommended that the pond be dredged and cleaned of sediment and accumulated debris. The outlet structure should also be cleaned of accumulated debris and repaired as needed.

The existing concrete channel, one of the primary storm water conveyance to the existing detention pond, requires repair and reconstruction in sections. In order to protect the track from erosion and deposition of sediment, and allow access to the soccer field, it is recommended that the portion of the channel on the south side of the soccer field be converted to 30-inch culvert pipe. For maintenance reasons,



Eldorado High School Drainage Master Plan

approximately 350 linear feet of concrete pipe should be installed before a manhole to allow cleaning by a vactor truck or water jet when required.

The proposed water quality detention pond will collect roof runoff from the 9th Grade Academy as well as a portion of the runoff from Basins 203 and 204. The water quality detention pond will accept drainage runoff on the west side of Basin 203 through a curb and gutter section and asphalt paved service road including a concrete channel.

Master Plan Improvements to be completed in the future

The area west of the 9th Grade Academy within Basin 204 is currently a dirt lot with steep slopes that allows sediment into the channel and onto the track. Paving this lot will reduce sediment transport and optimize the capacity of the existing hydraulic structures.

4.6.2 Juan Tabo city storm drain system

Basins 205A and 205B (courtyard), Basins 201B and 201D (areas surrounding track) and Basin 201C (northeast of baseball field) all contribute flows into the city storm drain system in Juan Tabo.

Improvements to be completed in 2013-2015

The courtyard (Basin 205A) concrete paving is not level and is cracked in multiple areas. While the expanding tree roots may be a primary contributing factor to the concrete damage, ponding water also may contribute to the cracking and damage to the concrete. Draining the water away from the central structure will help preserve the integrity of the concrete surface. This area is not ADA-compliant because the uneven surface poses a trip hazard. Therefore, the existing concrete surface area should be reconstructed. In addition, it is recommended to use tree wells to absorb excess runoff. The 12-inch storm drain from the courtyard connecting to the Juan Tabo storm drain will be upsized to a 30-inch pipe to accommodate all courtyard flows and the additional runoff from Basin 205 B, 201B and 201C.

The area encompassed by Basin 201C is identified in proposed Master Site Priority Plan and includes a walkway for ADA access to the PAC from Eagle Trail and access to the south baseball field. The upstream side of this walkway, with appropriate curb and gutter, would serve to prevent erosion from the slope that bisects Basin 208A. Flows will discharge west toward a proposed asphalt drainage swale. The proposed asphalt swale will be the main conveyance structure for flows discharging from Basins 201C, 201B and 201D.

In Basin 201B, the slope from the gymnasium to the tennis courts requires stabilization. An asphalt swale will be constructed to reduce sediment transport and direct runoff from north to south to the main drainage swale running east west.

Basin 201D will include an asphalt rundown to provide the basin an outlet to the main conveyance structure and will prevent erosion along the downstream side slopes.



The 12-inch storm drain along the south end of the basins will be upsized to a 30-inch pipe and will run under the asphalt swale. At the termination of the swale an area inlet will be constructed. All flows will converge at this location. The inlet will also act as a junction box which includes the existing 12-inch storm drain to the west and a proposed 30-inch culvert to the south. The existing 12-inch storm drain will reduce the total flow discharging to the Juan Tabo system to the existing allowable flow rate. As the hydraulic head increases the water surface will rise and flow will then discharge into the proposed 30-inch culvert and flow south into the detention pond in Basin 212.

Master Plan Improvements to be completed in the future

In Basin 201B, the slope upstream of the track, on the east side, requires sediment control. A geotextile used in conjunction with some desert landscaping will reduce the sediment transport from the area south of the basketball courts. Terracing would also retain sediment and soil and reduce the velocity of the surface runoff. The inlets at the track are limited in capacity and should be cleaned to maximize the storm water conveyance.

4.6.3 Embudito Arroyo system

The basins flowing into the Embudito Arroyo system include the student parking lot (Basin 206), the staff parking lot (Basin 207), the southern softball field (Basin 208A), the east baseball fields (Basin 210) and the band area (Basin 211).

Improvements to be completed in 2013-2015

An SO-19 (Special order 19) is proposed to convey runoff from basin 206 into the Embudito Arroyo. Currently, runoff from basin 206 is conveyed to basin 207 by way of a low lying sidewalk ramp that provides pedestrian access between the east student parking lot and the staff/visitor parking lot. This leads to localized ponding and hinders pedestrian sidewalk access during storm events. Basin 207 currently discharges into the south parking lot access road. The access road conveys runoff to Eagle Trail road and concrete channel rundown connected to the Embudito Arroyo. Proposed improvements to convey runoff from basin 206 will include a double 'D' inlet constructed in a sump condition. Approximately 330 LF of 24" dia. RCP (Reinforced Concrete Pipe) will connect the inlet to the Embudito Arroyo south of the inlet location. Pipe penetration into the Embudito Arroyo will provide a suitable outfall for the storm drain pipe. A water quality manhole structure will be provided between the inlet and the outfall location to maximize pollutant removal from entering into the Embuditio Arroyo. Proposed improvements will discharge runoff from basin 206 into the Embudito Arroyo approximately 740 ft. upstream from the current discharge point. Existing features such as asphalt, curb and gutter, landscape gravel, and fencing will be removed, salvaged when possible, and reinstalled to replicate existing conditions. This configuration provides a low impact economical solution to mitigate ponding and flooding between the pedestrian sidewalk and parking lots.

Master Plan Improvements to be completed in the future



Basin 210, the east baseball fields, would require substantial re-grading and restoration to improve drainage. Since this a largely a pervious area, this is not considered a priority for repair or rehabilitation.

There is a large, unpaved area that is bordered on the west by Basin 206 and on the east by Basin 210. Master Plan improvements include paving this area which would maximize conveyance capacity from Basin 210 and reduce sediment transport to Eagle Trail.

Basin 211, the band practice area, is proposed for repaving. Drainage improvements in the future should prevent upland drainage runoff into the baseball fields.

4.6.4 Eagle Trail city storm drain system

Basin 208B flows into Eagle Trail and into the city storm drain system.

Improvements to be completed in 2013-2015

There are no improvements to be completed in 2013-2015.

Master Plan Improvements to be completed in the future

The softball practice area may be developed to include an artificial turf athletic field.

4.6.5 Proposed Conditions Hydrologic Analysis Summaries

Table 4 summarizes the assumptions for land use, watershed areas, peak flow rates, and runoff volumes associated with the 16 analyzed sub-basins. Table 5 summarizes the contributing peak flow rates and runoff volumes at 13 design points.

Table 4: Proposed Sub-Basin Peak Discharge and Volumes

Cub Basin	Araa (Aaraa)	Land Treatment		O (efc)	\/ /aaf+\
Sub-Basili	Area (Acres)	С	D	Q _{100,6} (CIS)	V _{100,24} (ac-ft)
201A	4.2	64.7%	35.3%	15.30	0.596
201B	3.2	70.8%	29.2%	11.52	0.431
201C	0.9	25.0%	75.0%	3.76	0.179
201D	1.2	74.4%	25.6%	4.33	0.157
202A	1.3	100.0%	0.0%	4.34	0.125
202B	1.2	100.0%	0.0%	3.93	0.113
202C	0.7	92.0%	8.0%	2.14	0.067
203	4.0	1.0%	99.0%	18.12	0.943
204	8.3	13.3%	86.7%	35.79	1.801
205A	3.6	13.4%	86.6%	15.81	0.789
205B	0.8	10.0%	90.0%	3.38	0.170
206	2.8	0.0%	100.0%	12.40	0.648
207	3.9	14.1%	85.9%	16.89	0.841
208A	1.9	89.6%	10.4%	5.69	0.183
208B	1.9	62.1%	37.9%	6.90	0.273



Cula Dania	Aros (Asros)	Land Treatment		O (afa)	\/
Sub-Basin	Area (Acres)	С	D	Q _{100,6} (CIS)	V _{100,24} (ac-ft)
209A	0.6	33.4%	66.7%	2.36	0.108
209B	1.1	0.0%	100.0%	4.91	0.256
210	10.4	85.1%	14.9%	36.60	1.192
211	1.6	33.3%	66.7%	6.54	0.301
212	0.3	25.0%	75.0%	1.15	0.041

Table 5: Proposed Design Point Peak Discharge and Volumes

Analysis Point	Q _{100,6} (cfs)	V _{100,24} (ac-ft)
AP-1	87.57	4.802
AP-2	53.97	2.745
AP-3	57.10	2.858
AP-4	73.86	3.521
AP-5	5.48	0.860
AP-6	52.49	2.033
AP-7	58.19	2.215
AP-8	114.16	4.792
AP-9	6.54	0.301
AP-10	6.90	0.273
AP-11	4.34	0.125
AP-12	33.27	0.860
AP-13	12.40	0.648

Table 6 summarizes the proposed conditions pond.

Table 6: Proposed Conditions Pond Data

V _{required 100,24} (ac-ft) =	0.773
V provided (ac-ft) =	1.274
Q in 100,6 (cfs) =	114.16
Q _{out 100,6} (cfs) =	87.57
WSEI ₁₀₀ (ft) =	5697.5
Top Elevation(ft) =	5700
Bottom Elevation(ft) =	5692
Emergency Spillway Elevation (ft) =	5699.5
Outfall Box Top Elevation (ft) =	5697.05
Outfall Box Bottom Elevation/ 36" RCP Outfall Pipe Invert (ft) =	5688.58

Basin runoff has been increased slightly from the existing conditions due to an increase in Land Treatment D in Basins 201B, 203, 204, 205B, 206, 208B, and 210.



Table 7: Comparison of Analysis Point Peak Discharges

Analysis Point	Existing Q _{100,6} (cfs)	Proposed Q _{100,6} (cfs)	ΔQ _{100,6} (cfs)
AP-1	70.3	87.57	+17.3
AP-2	53.3	54.0	+0.7
AP-3	56.9	57.1	+0.2
AP-4	69.6	73.9	+4.30
AP-5	13.6	5.5	-8.1
AP-6	63.5	52.5	-11.0
AP-7	73.5	58.2	-15.3
AP-8	77.4	114.2	+36.8
AP-9	6.4	6.5	+0.1
AP-10	17.3	6.9	-10.4
AP-11	4.3	4.3	+0.0
AP-12	n/a	33.3	
AP-13	n/a	12.4	

Table 7 shows the comparison of the analysis points from the existing and proposed peak discharge. The proposed conditions have generally increased by 0 to 36.8 cfs. There is a significant increase in runoff at AP-8, flow into the pond, which increased the outlet from the pond at AP-1. The increase in runoff for proposed conditions is due to the fact that additional areas were routed to the pond instead of directly to the Eagle Trail Road.

Proposed improvements are designed to optimize the existing storm drain system, and reduce sediment transport onto campus and adjacent roadways.

5 Summary and Conclusions

The overall existing drainage conditions at the Eldorado High School campus are satisfactory, with the exception of the pond outlet structure which needs to be cleaned to function properly. In order for the outlet structure to function properly, the weep holes in the structure need to be cleaned of gravel. The pond sediment will be removed from all sides of the structure and 6-inch diameter gravel will be enclosed around the structure as designed by Bohannan Huston in the July 1997 Eldorado High School Master Drainage Plan. The current system has adequate capacity to accommodate the 100-Year storm event if properly maintained. Table 8 shows the comparison of the July 1997 Eldorado High School Master Drainage Plan prepared by Bohannan Huston allowable discharges and the proposed discharge calculated by this drainage report. The overall peak discharge flowrate is reduced in all systems and is below the allowable discharge rates set forth in the July 1997 Eldorado High School Master Drainage Plan.



Table 8: Allowable flow Comparison

Discharge Point	1997 Eldorado Master Drainage Plan Q _{100,6} (cfs)	Proposed Q _{100,6} (cfs)	ΔQ _{100,6} (cfs)
Detention Pond	92.1	87.6	-4.5
Embudito Arroyo	78.9	70.6	-8.3
Juan Tabo	8	9.9	+1.9
Eagle Trail Road	71.8	6.9	-64.9

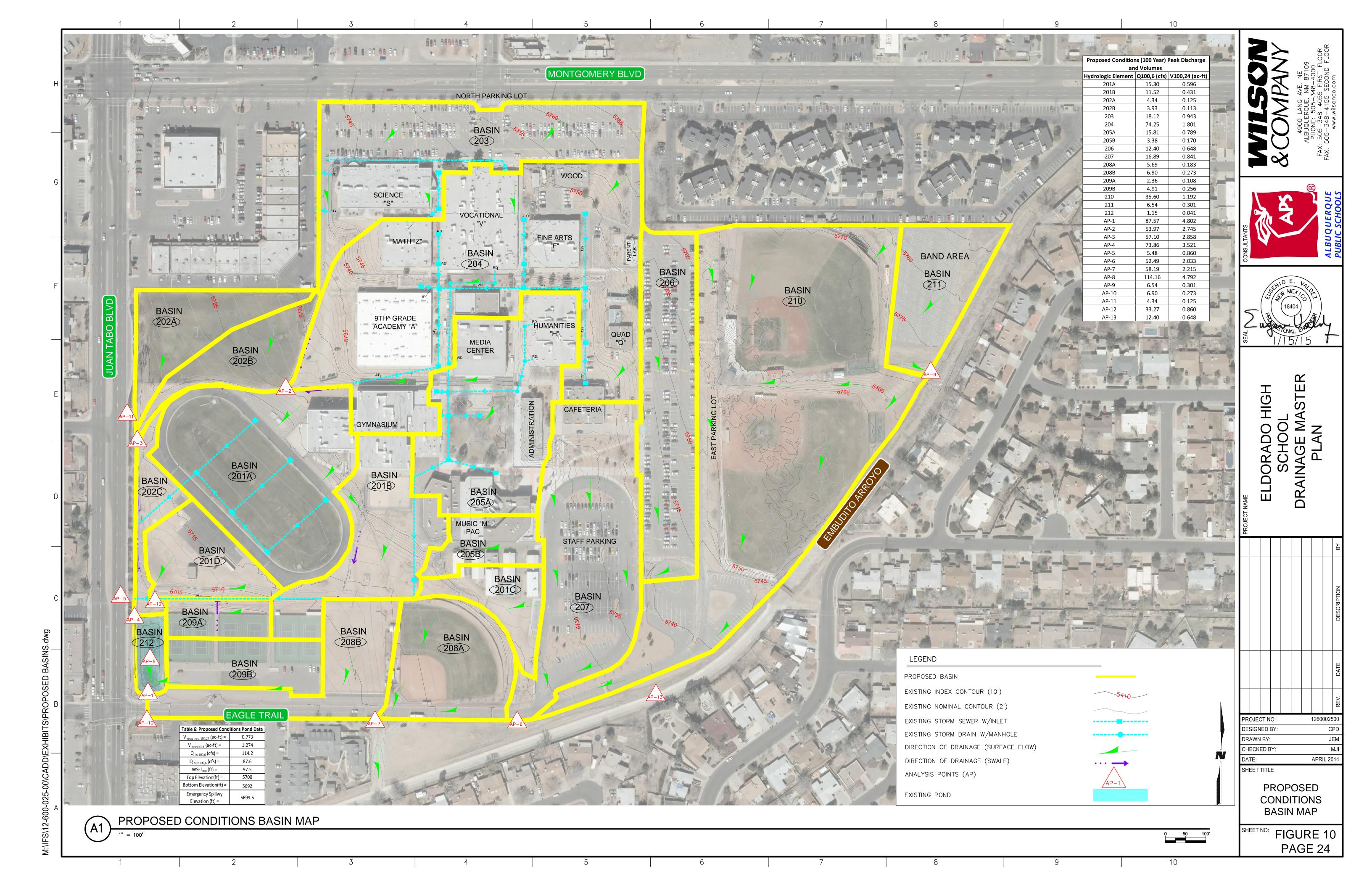
Construction of the improvements proposed in this plan will mitigate drainage issues currently present on the site. Deferred maintenance and sediment accumulation have created these drainage issues. Slope stabilization and repair of the existing structures will optimize the capacity of the existing system by removing or reducing the sediment that clogs the storm drain inlets and piping, and will maximize the capacity of the storm drain.

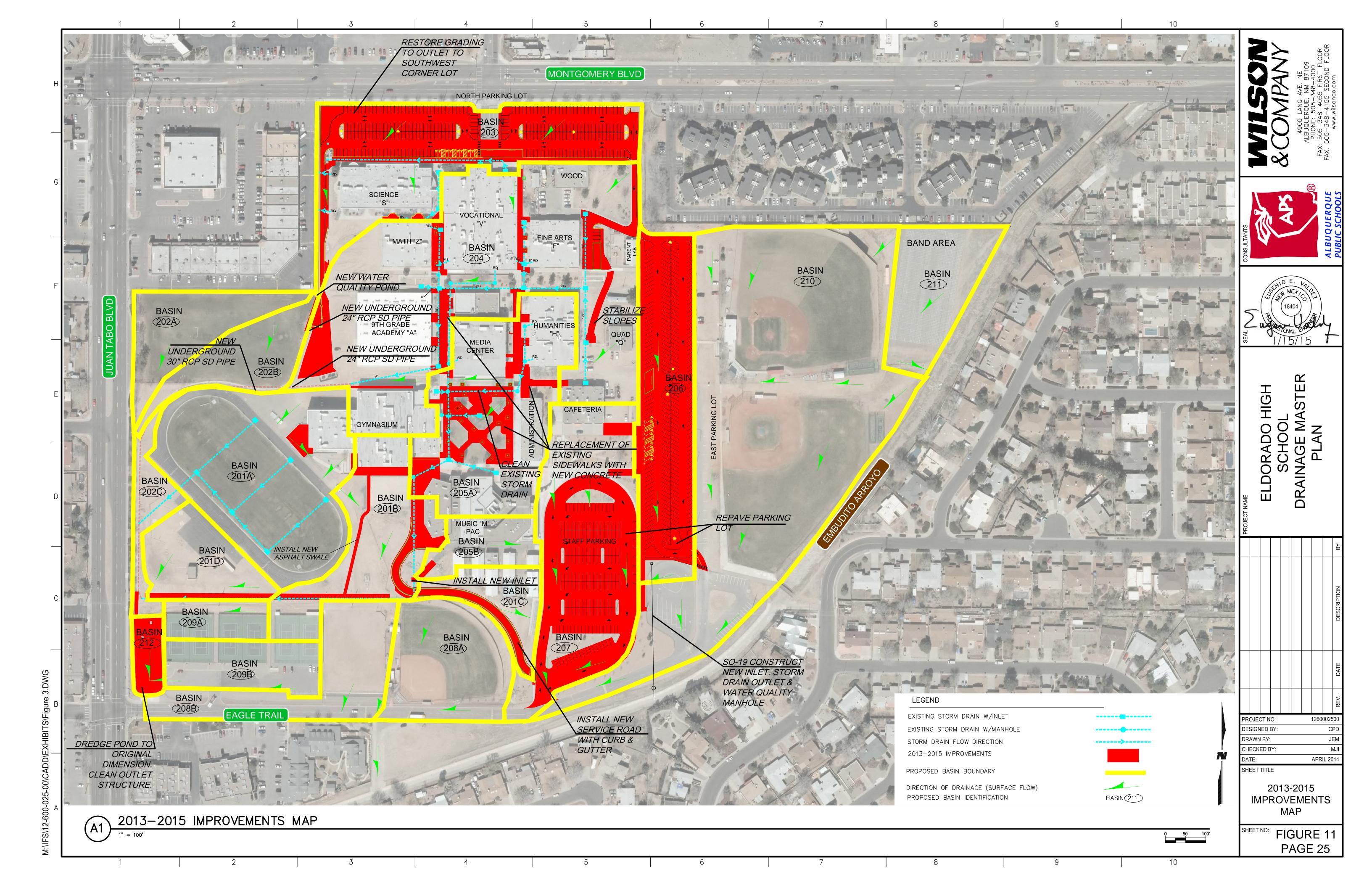
The primary components of the Drainage Master Plan include:

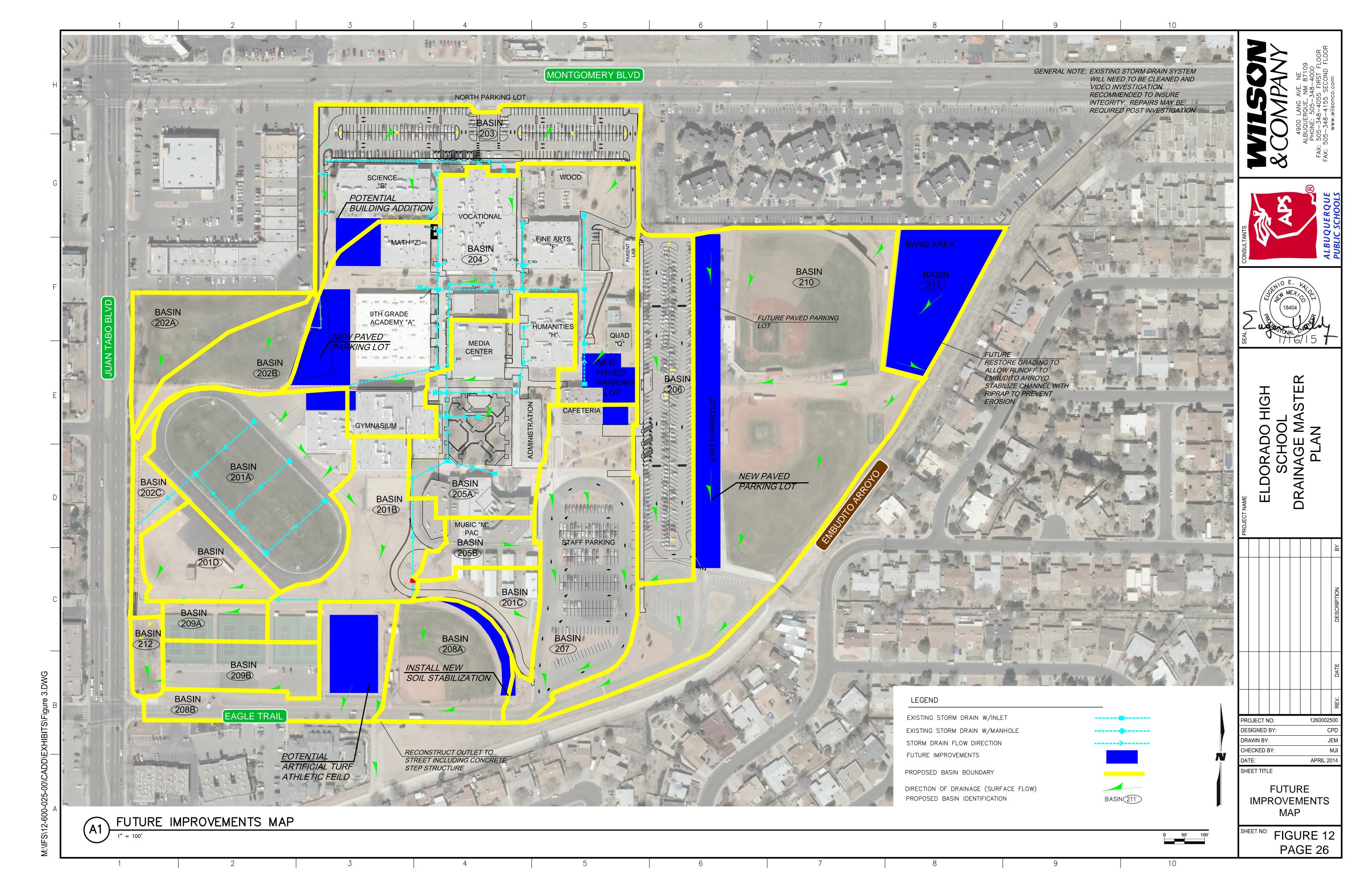
- Modification of the Outlet Structure; excavate around the structure and install 6"-12" wire enclosed riprap to allow water to drain to the outlet
- Repair and replacement of sections of the primary conveyance channel
- Removal of sediment from the detention pond and storm drain system
- Stabilization of slopes to minimize sediment transport and erosion
- Installation of inlets in the courtyard and lower areas to intercept surface flow
- Repaving and re-grading areas to conform to existing drainage patterns

These improvements are an investment that will extend the life of the storm water system and protect valuable capital assets for the Albuquerque Public Schools.

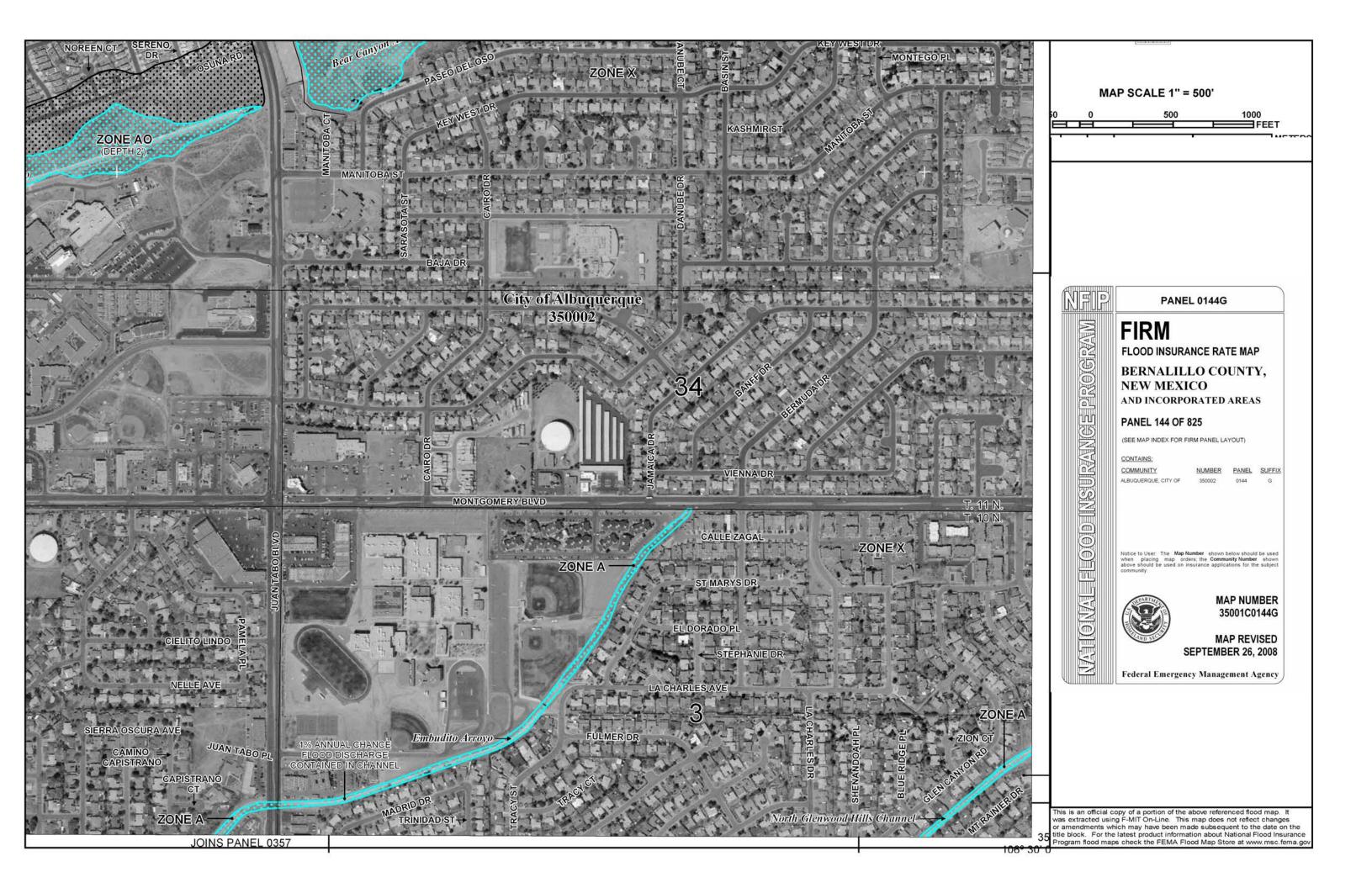








APPENDIX A



APPENDIX B

Project: Project No: Eldorado HS 1260002500

Existing Conditions Outlet Structure Orfice Outflow

Top of Structure Cd

5697.05 ft

0.67

g	32.	2 ft/sec^2													
Bottom Orifices		Row 1 Orifices			Row 2 Orifices			Row 3 Orifices			Row 4 Orifices			Total Flow	
Inlet Dia.	3 in.		Inlet Dia.	3 in.		Inlet Dia.	3 in.		Inlet Dia.	3 in.		Inlet Dia.	3 in.		from
Inlet Area	t Area 0.1963 sq ft		Inlet Area	0.1963 sq ft		Inlet Area			Inlet Area	0.1963 sq ft		Inlet Area	rea 0.1963 sq ft		Low Flow
Invert Elev	v 5689.3833 ft.		Invert Elev	v 5690.88 ft.		Invert Elev	ert Elev 5692.38 ft.		Invert Elev	ert Elev 5693.88 ft.		Invert Elev	/ 5695.4 ft.		Riser
# of Inlets	0		# of Inlets	0)	# of Inlets	0		# of Inlets	nlets 0		# of Inlets	2		Orifices
WSEL (ft)	Q (cfs)	Q row (cfs)	WSEL (ft)	Q (cfs)	Q row (cfs)	WSEL (ft)	Q (cfs)	Q row (cfs)	WSEL (ft)	Q (cfs)	Q row (cfs)	WSEL (ft)	Q (cfs)	Q row (cfs)	
5688.58	0.0	0.0	5688.58	0.0	0.0	5688.58	0.0	0.0	5688.58	0.0	0.0	5688.58	0.0	0.0	0.0
5689	0.0	0.0	5689	0.0	0.0	5689	0.0	0.0	5689	0.0	0.0	5689	0.0	0.0	0.0
5690	0.7	0.0	5690	0.0	0.0	5690	0.0	0.0	5690	0.0	0.0	5690	0.0	0.0	0.0
5691	1.3	0.0	5691	0.0	0.0	5691	0.0	0.0	5691	0.0	0.0	5691	0.0	0.0	0.0
5692	1.7	0.0	5692	1.0	0.0	5692	0.0	0.0	5692	0.0	0.0	5692	0.0	0.0	0.0
5693	2.0	0.0	5693	1.5	0.0	5693	0.7	0.0	5693	0.0	0.0	5693	0.0	0.0	0.0
5694	2.2	0.0	5694	1.8	0.0	5694	1.3	0.0	5694	0.0	0.0	5694	0.0	0.0	0.0
5695	2.5	0.0	5695	2.1	0.0	5695	1.7	0.0	5695	1.0	0.0	5695	0.0	0.0	0.0
5696	2.7	0.0	5696	2.3	0.0	5696	2.0	0.0	5696	1.5	0.0	5696	0.7	1.5	1.5
5697	2.9	0.0	5697	2.6	0.0	5697	2.2	0.0	5697	1.8	0.0	5697	1.3	2.6	2.6
5698	3.1	0.0	5698	2.8	0.0	5698	2.5	0.0	5698	2.1	0.0	5698	1.7	3.3	3.3
5699	3.2	0.0	5699	3.0	0.0	5699	2.7	0.0	5699	2.3	0.0	5699	2.0	3.9	3.9
5699.5	3.3	0.0	5699.5	3.1	0.0	5699.5	2.8	0.0	5699.5	2.5	0.0	5699.5	2.1	4.2	4.2
5700	3.4	0.0	5700	3.1	0.0	5700	2.9	0.0	5700	2.6	0.0	5700	2.2	4.5	4.5

Project: Project No: Eldorado HS 1260002500

Proposed Conditions Outlet Structure Orfice Outflow

 $Q = C_d A \sqrt{2gh}$

Top of Structure **5697.05** ft 0.67

Cd 32.2 ft/sec^2

9	32.2	2 It/sec^2													
Bottom Orifices		Row 1 Orifices			Row 2 Orifices			Row 3 Orifices			Row 4 Orifices			Total Flow	
Inlet Dia.	Dia. 3 in.		Inlet Dia. 3 in.		Inlet Dia.	3 in.		Inlet Dia.	3 in.		Inlet Dia.	3 in.		from	
Inlet Area	0.1963	3 sq ft	Inlet Area	0.1963	sq ft	Inlet Area	0.1963	sq ft	Inlet Area	0.1963	sq ft	Inlet Area	0.1963	sq ft	Low Flow
Invert Elev	lev 5689.3833 ft.		Invert Elev	5690.88	ft.	Invert Elev	5692.38	5692.38 ft.		5693.88 ft.		5693.88 ft. Invert Elev		ft.	Riser
# of Inlets	6	5	# of Inlets	6		# of Inlets	6		# of Inlets	6		# of Inlets	8		Orifices
1440EL (%)	0 (()			0 (()			0 (()		o=: //:\	0 (()		o=. (0)	0 (()		
WSEL (ft)	Q (cfs)	Q row (cfs)	` '	Q (cfs)	Q row (cfs)	` '	Q (cfs)	Q row (cfs)	WSEL (ft)	Q (cfs)	Q row (cfs)	` '	. ,	Q row (cfs)	
5688.58	0.0	0.0	5688.58	0.0	0.0	5688.58	0.0	0.0	5688.58	0.0	0.0	5688.58	0.0	0.0	0.0
5689	0.0	0.0	5689	0.0	0.0	5689	0.0	0.0	5689	0.0	0.0	5689	0.0	0.0	0.0
5690	0.7	4.4	5690	0.0	0.0	5690	0.0	0.0	5690	0.0	0.0	5690	0.0	0.0	4.4
5691	1.3	7.7	5691	0.0	0.0	5691	0.0	0.0	5691	0.0	0.0	5691	0.0	0.0	7.7
5692	1.7	9.9	5692	1.0	6.3	5692	0.0	0.0	5692	0.0	0.0	5692	0.0	0.0	16.2
5693	2.0	11.8	5693	1.5	8.9	5693	0.7	4.4	5693	0.0	0.0	5693	0.0	0.0	25.1
5694	2.2	13.4	5694	1.8	10.9	5694	1.3	7.7	5694	0.0	0.0	5694	0.0	0.0	32.0
5695	2.5	14.8	5695	2.1	12.6	5695	1.7	9.9	5695	1.0	6.3	5695	0.0	0.0	43.6
5696	2.7	16.1	5696	2.3	14.1	5696	2.0	11.8	5696	1.5	8.9	5696	0.7	5.9	56.7
5697	2.9	17.3	5697	2.6	15.4	5697	2.2	13.4	5697	1.8	10.9	5697	1.3	10.3	67.2
5698	3.1	18.4	5698	2.8	16.7	5698	2.5	14.8	5698	2.1	12.6	5698	1.7	13.3	75.7
5699	3.2	19.4	5699	3.0	17.8	5699	2.7	16.1	5699	2.3	14.1	5699	2.0	15.7	83.1
5699.5	3.3	19.9	5699.5	3.1	18.4	5699.5	2.8	16.7	5699.5	2.5	14.8	5699.5	2.1	16.8	86.5
5700	3.4	20.4	5700	3.1	18.9	5700	2.9	17.3	5700	2.6	15.4	5700	2.2	17.8	89.8

Project: Eldorado HS Project No: 1260002500

Existing Conditions Outlet Structure Total Outflow

$$Q = C_w \cdot L \cdot h^{1.5}$$

$$Q = C_d A \sqrt{2gh}$$
 Invert (ft) = 5688.58 Riser Width 4 Diameter (in) = 36

Riser Width 4 Diameter (in) = 36Riser Length 4 Area (sq ft) = 7.07Riser Area 16

 $\begin{array}{ccc} \text{Cw} & \text{2.9} & \text{L= 12' for weir equation} \\ \text{Cd} & \text{0.60} & \end{array}$

 $g (ft/sec^2) = 32.2$

g (11/360 Z) =	UZ.Z				
	Weir Flow (Top of structure)	Orifice Flow (36" RCP Outflow Pipe)	Flow Used	Total Flow Riser Orfices	Total Flow
WSEL (ft)	Q (cfs)	Q (cfs)	Q (cfs)	Q (cfs)	Q (cfs)
5692	0.0	0.0	0.0	0.0	0.0
5693	0.0	0.0	0.0	0.0	0.0
5694	0.0	0.0	0.0	0.0	0.0
5695	0.0	0.0	0.0	0.0	0.0
5696	0.0	0.0	0.0	1.5	1.5
5697	0.0	0.0	0.0	2.6	2.6
5698	32.2	95.8	32.2	3.3	35.5
5699	94.8	101.7	94.8	3.9	98.7
5699.5	133.5	104.5	104.5	4.2	108.7
5700	176.3	107.2	107.2	4.5	111.6

Project: Eldorado HS Project No: 1260002500

Proposed Conditions Outlet Structure Total Outflow

$$Q = C_w \cdot L \cdot h^{1.5}$$

 $Q = C_d A \sqrt{2gh}$

Top of Riser Elev (ft) = 5697.05

Riser Width 4
Riser Length 4
Riser Area 10

Riser Area 16 Cw 2.9 Cd 0.60 g (ft/sec^2) = 32.2

$\mathcal{L} = \mathcal{L}_d \Pi \sqrt{2} \delta$	511
Invert (ft) =	5688.58
Diameter (in) -	36

Diameter (in) =	36
Area (sq ft) =	7.07

		Orifice Flow		Total	
	Weir Flow (Top of	(36" RCP	Flow Used	Flow	Total
	structure)	Outflow	1 10W 03ea	Riser	Flow
		Pipe)		Orfices	
WSEL (ft)	Q (cfs)	Q (cfs)	Q (cfs)	Q (cfs)	Q (cfs)
5688.58	0.0	0.0	0.0	0.00	0.0
5689	0.0	0.0	0.0	0.00	0.0
5690	0.0	0.0	0.0	4.42	4.4
5691	0.0	0.0	0.0	7.70	7.7
5692	0.0	0.0	0.0	16.23	16.2
5693	0.0	0.0	0.0	25.09	25.1
5694	0.0	0.0	0.0	31.96	32.0
5695	0.0	0.0	0.0	43.59	43.6
5696	0.0	0.0	0.0	56.71	56.7
5697	0.0	0.0	0.0	67.20	67.2
5698	32.2	95.8	32.2	75.66	107.9
5699	94.8	101.7	94.8	83.08	177.8
5699.5	133.5	104.5	104.5	86.52	191.0
5700	176.3	107.2	107.2	89.80	197.0

Project:Eldorado HSProject No:1260002500

Emergency Spillway Peak Discharge

Flow Across Trapezoidal Weir NRCS, TR-39

$$H_{ec} = \frac{(3b + 5zd_{c,q})d_{c,q}}{2b + 4zd_{c,q}}$$

Equation 6

 $\frac{Q_{c,d}^2}{g} = \frac{[(b+zd_{c,q})d_{c,q}]^3}{b+2zd_{c,q}}$

Equation 4

 $\begin{array}{ccc} \text{Crest Elevation} & 5699.5 \text{ ft} \\ \text{Side Slope, z} & 0.10326 \text{ ft/ft} \\ \text{Crest Width, b} & 47.16 \text{ ft} \\ \text{Energy Head, H}_{\text{ec}} & 0.5 \\ & 5700 \\ \text{Gravitational Constant, g} & 32.2 \\ \end{array}$

Determine Quadratic Equation from Equation 6 Determine critical depth from Quadratic Equation

A	0.5163
В	141.48
C	-47.16
Critical Depth, d _{c,q}	0.333

Determine peak discharge through spillway

Q 51

1006E_010715.txt

```
*S
      ALBUQUERQUE PUBLIC SCHOOLS
*s
*S
      ELDORADO HIGH SCHOOL DRAINAGE ANALYSIS USE THE IA/INF METHOD TO COMPUTE THE RUNOFF
*S
      FILE: 1006E_010715.txt
*S
      EXISTING CONDITIONS
*s
      DATE: JAN 2015
*s
*s
*S
      100 YEAR 6 HOUR STORM - EXISTING RUNOFF ANALYSIS
*s
      RAINFALL FROM NOAA ATLAS 14, VOLUME 1, VERSION 4
  ***********************************
                TIME=0.0 PUNCH CODE=0 PRINT CODE=0
START
                ALBUQUERQUE
LOCATION
**************************************
RAINFALL
                 TYPE=-1
                 QUARTER=1.12
                             ONE= 1.87 IN
                 SIX= 2.51 IN DAY= 3.08 IN
                                         DT = 0.05 HR
*S
*********************************
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                NK=3 ISLOPE=0
LENGTH=100 FT
                              SLOPE=0.040
                 LENGTH=250 FT
                              SLOPE=0.040
                                         K = 2.0
                 LENGTH=150 FT SLOPE=0.040 K=3.0
                 KN=0.021 CENTROID DIST=250 FT
                ID=1 HYD NO=101A DA= 0.0065594 SQ MI
PER A=0 PER B=0 PER C=65.78 PER D=34.22
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                ID=1 CODE=1
*S ROUTE 101A IN 10-INCH STORM DRAIN
COMPUTE RATING CURVE CID=1 VS No=1 CODE=-1 SLP=0.03
DIA=0.83 FT N=0.025
ROUTE MCUNGE
                 ID=2 HYD NO=101A.R INFLOW ID=1
                DT=0.0 L=700 FT NS=0 SLOPE=0.03
PRINT HYD
                ID=2 CODE=1
*************************
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                 NK=3 ISLOPE=0
                                         K = 0.7
                 LENGTH=100 FT
                              SLOPE=0.040
                 LENGTH=750 FT
                              SLOPE=0.040
                                          K = 2.0
                 LENGTH=150 FT
                              SLOPE=0.040
                                          K = 3.0
                 KN=0.021 CENTROID DIST=500 FT
                ID=3 HYD NO=101B DA= 0.0039166 SQ MI
PER A=0 PER B=0 PER C=80.18 PER D=19.82
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                ID=3 CODE=1
*******************
             **** SUB-BASIN 102A **** (AREA=1.35 ACRES)
***************
             **** AP-11
COMPUTE LT TP
                LCODE=1 UPLAND/LAG TIME METHOD
                 NK=3 ISLOPE=0
                                         K = 0.7
                 LENGTH=100 FT
                              SLOPE=0.015
                 LENGTH=400 FT
                              SLOPE=0.015
                                          K = 2.0
                 LENGTH=100 FT
                              SLOPE=0.015
                                          K = 3.0
                 KN=0.025 CENTROID DIST=300 FT
                TD=7 HYD NO=102A DA= 0.0021153 SQ MI
PER A=0 PER B=0 PER C=100 PER D=0
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                ID=7 CODE=1
**** SUB-BASIN 102B **** (AREA=1.16 ACRES)
**************
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                NK=3 ISLOPE=0
                 LENGTH=100 FT
                              SLOPE=0.015
                 LENGTH=400 FT
                              SLOPE=0.015
                                         K = 2.0
```

1006E_010715.txt LENGTH=100 FT SLOPE=0.015 K=3.0

KN=0.025 CENTROID DIST=300 FT ID=39 HYD NO=102B DA= 0.0018130 SQ MI PER A=0 PER B=0 PER C=100 PER D=0 TP=0.133333 MASSRAIN=-1 COMPUTE NM HYD

PRINT HYD ID=39 CODE=1

COMPUTE LT TP LCODE=1 UPLAND/LAG TIME METHOD

NK=3 ISLOPE=0

LENGTH=100 FT SLOPE=0.055K=2.0 LENGTH=875 FT SLOPE=0.055SLOPE=0.055 LENGTH=300 FT

ELENGTH-300 FT SLOTE-0.037 R-3.0 KN=0.021 CENTROID DIST=638 FT ID=8 HYD NO=103 DA= 0.0063226 SQ MI PER A=0 PER B=0 PER C=4.96 PER D=95.04 TP=0.133333 MASSRAIN=-1 COMPUTE NM HYD

ID=8 CODE=1 PRINT HYD

**** SUB-BASIN 104 **** (AREA=8.36 ACRES)

COMPUTE LT TP LCODE=1 UPLAND/LAG TIME METHOD

NK=3 ISLOPE=0 LENGTH=100 FT SLOPE=0.034 LENGTH=850 FT SLOPE=0.034 K = 2.0LENGTH=2550 FT SLOPE=0.034 KN=0.021 CENTROID DIST=1750 FT

TD=10 HYD NO=104 DA= 0.0130650 SQ MI PER A=0 PER B=0 PER C=13.30 PER D=86.70 TP=0.0 MASSRAIN=-1 ID=10 CODE=1 COMPUTE NM HYD

PRINT HYD

**** AP-2(ADD BASINS 103 AND 104)

ADD HYD ID=14 HYD NO=AP-2 ID I=8 ID II=10

ID=14 CODE=5

*S ROUTE BASINS 103 AND 104 IN CHANNEL

COMPUTE RATING CURVE CID=1 VS No=1 CODE=-1 SLP=0.03 DIA=2.0 FT N=0.025 ROUTE MCUNGE ID=9 HYD NO=103.R INFLOW ID=14

DT=0.0 L=178 FT NS=0 SLOPE=0.03

PRINT HYD ID=9 CODE=1

**** AP-3(ADD BASINS 103 AND 104 AND 102B) =AP-3 ID I=9 ID II=39 CODE=5 ADD HYD ID=16 HYD NO=AP-3

PRINT HYD ID=16

COMPUTE RATING CURVE CID=1 VS NO=1 NO SEGS=1

MIN ELEV=0 MAX ELEV=1.3 CH SLOPE=0.027 FP SLOPE=0.027 N=0.017 DIST=7.09

DIST ELEV

DIST ELEV 2.46 0.0 7.09 1.83 1.83

0.0 1.83 2.46 0.0 4.63 0.0 7.09 1.83 ID=17 HYD NO=AP-3.R INFLOW ID=16 DT=0.0 L=450 FT NS=0 SLOPE=0.027 ROUTE MCUNGE

PRINT HYD ID=17 CODE=1

*

**** (ADD BASINS 103 AND 104 AND 102B AND 101A)

ID=18 HYD NO=18 ID I=17 ID II=2 ID=18 CODE=5 ADD HYD

PRINT HYD

**** AP-4(ADD BASINS 103 AND 104 AND 102B AND 101A AND 101B.CHANNEL)*S =AP-4 ID I=18 ID II=3 CODE=5

ADD HYD ID=19 HYD NO=AP-4

PRINT HYD ID=19

COMPUTE LT TP LCODE=1 UPLAND/LAG TIME METHOD

NK=3 ISLOPE=0

LENGTH=100 FT SLOPE=0.032 K=1.0

```
1006E_010715.txt
                              SLOPE=0.032 K=2.0
SLOPE=0.032 K=3.0
                  LENGTH=850 FT
                  LENGTH=750 FT
                                            K = 3.0
                 KN=0.021 CENTROID DIST=850 FT
ID=21 HYD NO=105 DA= 0.0055891 SQ MI
PER A=0 PER B=0 PER C=13.52 PER D=86.48
COMPUTE NM HYD
                  TP=0.133333
                             MASSRAIN=-1
                 ID=21 CODE=1
PRTNT HYD
*ROUTE SUB-BASINS 105 TO JUAN TABO THROUGH 12-INCH STORM DRAIN
*S **** AP-5
COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.017
                   DIA=1.0 FT N=0.011

ID=22 HYD NO=AP-5 INFLOW ID=21

DT=0.0 L=895 FT NS=0 SLOPE=0.017
ROUTE MCUNGE
PRINT HYD
                   ID=22 CODE=1
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                 NK=3 ISLOPE=0
                  LENGTH=100 FT
                               SLOPE=0.036
                                            K = 2.0
                  LENGTH=500 FT
                               SLOPE=0.036
                              SLOPE=0.036
                  LENGTH=850 FT
                                           K = 3.0
                 KN=0.021 CENTROID DIST=1450 FT
ID=24 HYD NO=106 DA= 0.0059657 SQ MI
PER A=0 PER B=0 PER C=8.94 PER D=91.06
COMPUTE NM HYD
                 TP=0.133333
                             MASSRAIN=-1
PRINT HYD
                 ID=24 CODE=1
**************************************
             **** SUB-BASIN 107 **** (AREA=3.78 ACRES)
*********
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                 NK=3 ISLOPE=0
LENGTH=100 FT
                               SLOPE=0.040
                                           K=1.0
                  LENGTH=360 FT
                               SLOPE=0.040
                                           K = 2.0
                 LENGTH=360 FT SLOPE=0.040 K=3.0
                  KN=0.021 CENTROID DIST=820 FT
                 TD=25 HYD NO=107 DA= 0.0059095 SQ MI
PER A=0 PER B=0 PER C=14.75 PER D=85.25
COMPUTE NM HYD
                 TP=0.133333 MASSRAIN=-1
PRINT HYD
                 ID=25 CODE=1
*************************
             **** SUB-BASIN 108A **** (AREA=2.77 ACRES)
***********
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                 NK=3 ISLOPE=0
                  LENGTH=100 FT
                                SLOPE=0.05
                 SLOPE=0.05 K=2.0

LINGIH=350 FT SLOPE=0.05 K=3.0

KN=0.025 CENTROID DIST=500 FT

ID=26 HYD NO=108A PA
                 ID=26 HYD NO=108A DA= 0.0043302 SQ MI
PER A=0 PER B=0 PER C=65.43 PER D=34.57
COMPUTE NM HYD
                 TP=0.133333
                             MASSRAIN=-1
PRINT HYD
                 ID=26 CODE=1
**** SUB-BASIN 108B **** (AREA=4.66 ACRES)
**** AP-10
*5
                 LCODE=1 UPLAND/LAG TIME METHOD
COMPUTE LT TP
                 NK=3 ISLOPE=0
                  LENGTH=100 FT
                                SLOPE=0.035
                                            K = 0.7
                  LENGTH=450 FT
                               SLOPE=0.035
                                           K = 2.0
                  LENGTH=350 FT
                               SLOPE=0.035
                 KN=0.021 CENTROID DIST=450 FT
                 TD=27  HYD NO=108B  DA= 0.0072807 SQ MI
PER A=0  PER B=0  PER C=58.81  PER D=41.19
TP=0.133333  MASSRAIN=-1
COMPUTE NM HYD
                 ID=27 CODE=1
PRINT HYD
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                 NK=3 ISLOPE=0
```

```
1006E_010715.txt
                                  SLOPE=0.014 K=1.0
                   LENGTH=100 FT
                   LENGTH=100 FT SLOPE=0.014 K=1.0
LENGTH=275 FT SLOPE=0.014 K=2.0
LENGTH=225 FT SLOPE=0.014 K=3.0
                   KN=0.021 CENTROID DIST=300 FT
                   ID=28 HYD NO=109A DA= 0.0007330 SQ MI
PER A=0 PER B=0 PER C=15.22 PER D=84.78
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                   ID=28 CODE=1
               **** ADD BASINS 103 AND 104 AND 102 AND 101A AND 101B.CHANNEL AND **** 109A AND 101B.SWALE)
*S
               ID=30 HYD NO=30 ID I=19 ID II=28
ADD HYD
PRINT HYD
                       ID=30 CODE=5
********************
               **** SUB-BASIN 109B **** (AREA=1.11 ACRES)
COMPUTE LT TP
                   LCODE=1 UPLAND/LAG TIME METHOD
                   NK=3 ISLOPE=0
                   LENGTH=100 FT
                                   SLOPE=0.024
                   LENGTH=225 FT
                                   SLOPE=0.024 K=2.0
                   LENGTH=175 FT SLOPE=0.024
                                                K = 3.0
                   KN=0.021 CENTROID DIST=250 FT
                   TD=31 HYD NO=109B DA= 0.0017420 SQ MI
PER A=0 PER B=0 PER C=0 PER D=100
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
                   ID=31 CODE=1
PRINT HYD
*
               **** ADD BASINS 103 AND 104 AND 102B AND 101A AND 101B.CHANNEL AND **** 109A AND 101B.SWALE AND 109B)
*S
*S
                                     ID I=30 ID II=31
ADD HYD
               ID=32 HYD NO=32
PRINT HYD
                       ID=32
                              CODE=5
COMPUTE LT TP
                   LCODE=1 UPLAND/LAG TIME METHOD
                   NK=3 ISLOPE=0
                   LENGTH=100 FT SLOPE=0.040 K=0.7

LENGTH=650 FT SLOPE=0.040 K=2.0

LENGTH=1275 FT SLOPE=0.040 K=3.0
                   KN=0.025 CENTROID DIST=1012 FT

ID=34 HYD NO=110 DA= 0.0147070 SQ MI

PER A=0 PER B=0 PER C=93.60 PER D=6.40
COMPUTE NM HYD
                   TP=0.133333 MASSRAIN=-1
PRINT HYD
                   ID=34 CODE=1
**** SUB-BASIN 111 **** (AREA=1.57 ACRES)
               **** AP-9
*S
COMPUTE LT TP
                  LCODE=1 UPLAND/LAG TIME METHOD
                   NK=3 ISLOPE=0
                   LENGTH=100 FT
                                   SLOPE=0.030 K=1.0
                   LENGTH=400 FT
                                   SLOPE=0.030
                                                K = 2.0
                   LENGTH=100 FT SLOPE=0.030
                                                K = 3.0
                   KN=0.021 CENTROID DIST=300 FT
ID=35 HYD NO=111 DA= 0.0024568 SQ MI
PER A=0 PER B=0 PER C=33.26 PER D=66.74
COMPUTE NM HYD
                   TP=0.133333 MASSRAIN=-1
ID=35 CODE=1
PRINT HYD
               **** (ADD 110 AND 106)
               ID=36 HYD_NO=36
ADD HYD
                                       ID I=34 ID II=24
                       ID=36 CODE=5
PRINT HYD
               **** AP-6
ADD HYD
               ID=37 HYD NO=AP-6
                                       ID I=36 ID II=25
PRINT HYD
                       ID=37 CODE=5
               **** AP-7
*5
               ID=38 HYD_NO=AP-7
ADD HYD
                                       ID I=37 ID II=26
PRINT HYD
                       ID=38 CODE=5
```

Page 4

```
ID=40 HYD NO=112 DA= 0.0005390 SQ MI
PER A=0 PER B=0 PER C=85.1 PER D=14.9
TP=0.133333 MASSRAIN=-1
ID=40 CODE=1
COMPUTE NM HYD
PRINT HYD
              **** AP-8

**** ADD BASINS 103 AND 104 AND 102 AND 101A AND 101B.CHANNEL AND 109A AND 101B.SWALE AND 109B AND 112

ID=41 HYD NO=AP-8 ID I=32 ID II=40

ID=41 CODE=5
*S
*S
*S
ADD HYD
PRINT HYD
**** AP-1/POND
                    ID=33 HYD NO=AP-1/POND INFLOW=41 CODE=1
OUTFLOW (CFS) STORAGE (AC-FT) ELEV (FT)
ROUTE RESERVOIR
                    0.0
                                  0.0000
                                                  5692
                    1.5
                                  0.4501
                                                  5696
                                  0.6518
                                                  5697
                    35.5
98.7
                                  0.8809
                                                  5698
                                  1.1384
                                                  5699
                    108.7
                                  1.2744
                                                  5699.5
                   PRINT HYD
                                       ID=33 CODE=1
FINISH
```

1006E_010715.SUM

1

RUN DATE (MON/DAY/YR)

AHYMO PROGRAM SUMMARY TABLE (AHYMO-S4) - Ver. S4.01a, Rel: 01a RUN DATE =01/13/2015
INPUT FILE = 025-00\AE_DATA\CALCS\Hydrology\AHYMO\Resubmittal Calcs_1214\1006E_010715.txt USER NO.= WilsonCoanMsiteA96476897

	COMMAND IDE	HYDROGRAPH ENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	DISC	HARGE	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = NOTATION
	*S *S *S *S *S *S *S	USE THE I FILE: 100 EXISTING DATE: JAN	HIGH S A/INF 06E_010 CONDIT I 2015	CHOOL DI METHOD 7 1715.txt TONS	RAINAGE ANA TO COMPUTE	THE RUN		*****				
	*S *S *S *S				- EXISTING AS 14, VOLU							
0.0	*S ***********************************	******		·******	******	******	******	*****				TIME=
2.5	RAINFALL TYPE= 1 10	NOAA 14	, LEBO	QUENQUE								RAIN6=
34.7	*S *S COMPUTE NM HYD 22	101A	*** SU -	B-BASIN 1	101A **** 0.00656		.20 ACRES) 15.18	0.527	1.50649	1.500	3.616	PER IMP=
0.2	*S ROUTE 101A IN ROUTE MCUNGE	10-INCH STOR 101A.R	M DRAI	:N 2	0.00656		12.89	0.524	1.49686	1.700	3.071	CCODE =
19.8	*S COMPUTE NM HYD 32	101B	-	3	101B **** 0.00392	•	8.59	0.280	1.34255	1.500	3.428	PER IMP=
0.0	*S *S COMPUTE NM HYD		**** SU **** AP -		102A **** 0.00212	(AREA=1	35 ACRES) 4.29	0.126	1.11690	1.500	3.167	PER IMP=
0.0	*S COMPUTE NM HYD	102в [*]	*** SU -	B-BASIN 39	102B **** 0.00181	(AREA=1	16 ACRES) 3.68	0.108	1.11690	1.500	3.168	PER IMP=
95.0	*S COMPUTE NM HYD	103.00	*** SU -	B-BASIN 8	103 **** (05 ACRES) 17.88	0.741	2.19893	1.500	4.418	PER IMP=
86.	*S COMPUTE NM HYD	104.00	*** SU -	B-BASIN 10	104 **** (36 ACRES) 35.38	1.466	2.10398	1.500	4.231	PER IMP=
	*S ADD HYD *S ROUTE BASINS 1	AP-2	8&10	14	0.01939		53.25	2.208	2.13491	1.500	4.292	
0.0	ROUTE MCUNGE	103.R	14	9	0.01939		53.25	2.208	2.13491	1.500	4.292	CCODE =
0.2	*S ADD HYD ROUTE MCUNGE	AP-3 AP-3.R			0.02120 0.02120		AND 102B) 56.93 56.55	2.316 2.316	2.04785 2.04799	1.500 1.500	4.196 4.168	CCODE =
V	*S ADD HYD *S	18.00 4(ADD BAS	17& 2 SINS 10	18 3 AND 10	0.02776 04 AND 102E	B AND 10	102B AND 1 61.25 1A AND 101B	2.839 .CHANNEL)	1.91771	1.550	3.447	
	ADD HYD *S COMPUTE NM HYD	AP-4 * 105.00	18& 3 **** SU -	19 B-BASIN 21	0.03168 105 **** (0.00559	(AREA=3.	69.56 58 ACRES) 15.40	3.120 0.626	1.84659 2.10147	1.550 1.500	3.431 4.306	PER IMP=

1006E_010715.SUM

2

				10	006E_010715.SUM					
86.48 *S	4	**** AF								
ROUTE MCUNGE	AP-5			0.00559	13.60	0.619	2.07822	1.650	3.803	CCODE =
*S COMPUTE NM HYD 91.06	106.00	**** Sl -	JB-BASIN 24	106 **** 0.00597	(AREA=3.82 ACRES) 16.67	0.685	2.15362	1.500	4.366	PER IMP=
91.00 *S Ŷ	×	**** Sl	JB-BASIN	107 ****	(AREA=3.78 ACRES)					
	HYDROGRAPH DENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 2
COMPUTE NM HYD 85.25	107.00	-	25	0.00591	16.22	0.658	2.08747	1.500	4.289	PER IMP=
*S COMPUTE NM HYD 34.57	108A	**** Sl -		108A **** 0.00433	(AREA=2.77 ACRES) 10.04	0.349	1.51048	1.500	3.622	PER IMP=
*S *S		**** SU		108в ****	(AREA=4.66 ACRES)					
COMPUTE NM HYD	108в	-	27	0.00728	17.27	0.616	1.58585	1.500	3.707	PER IMP=
*S COMPUTE NM HYD 84.78		**** Sl -		109A **** 0.00073	(AREA=0.47 ACRES) 2.02	0.081	2.08212	1.500	4.312	PER IMP=
*S *S	**** 109A AND	101B.	SWALE)		ND 101A AND 101B.C					
ADD HYD *S	*		JB-BASIN	0.03241 109B ****	(AREA=1.11 ACRES)		1.85191	1.550	3.446	
COMPUTE NM HYD	109B		-	0.00174		0.210	2.25540	1.500	4.487	PER IMP=
*S *S ADD HYD	**** 109A AND		SWALE AN		ND 101A AND 101B.C 76.23	3.411	1.87248	1.550	3.488	
*S COMPUTE NM HYD	110.00	**** Sl	JB-BASIN 34	110 **** 0.01471	(AREA=9.41 ACRES)	0.933	1.18976	1.500		PER IMP=
6.40 *S	110.00		31	0.01171	30.30	0.333	1.10570	1.500	3.217	TER IM -
*S *S	4	**** SU **** AF	JB-BASIN P-9	111 ****	(AREA=1.57 ACRES)					
COMPUTE NM HYD	111.00			0.00246	6.37	0.246	1.87674	1.500	4.051	PER IMP=
*S ADD HYD *S	36.00	**** (<i>A</i> 34&24 **** AF		0.02067	47.23	1.618	1.46789	1.500	3.570	
ADD HYD *S	AP-6	36&25 **** AF	37	0.02658	63.45	2.276	1.60562	1.500	3.730	
ADD HYD *S	AP-7	37&26	38	0.03091 112 ****	73.49 (AREA=0.34 ACRES)	2.625	1.59228	1.500	3.715	
COMPUTE NM HYD 14.90	112.00	-	40	0.00054	1.17	0.037	1.28654	1.500	3.402	PER IMP=
*S *S *S	ADD BASIN	**** AF NS 103 ND 101E	AND 104	AND 102 AI AND 109B AI	ND 101A AND 101B.C	HANNEL AND				
ADD HYD *S *S	AP-8	32&40 **** PC		0.03469	77.37	3.448	1.86337	1.550	3.485	
ROUTE RESERVOIR			33 33	0.03469	70.28	3.448	1.86337	1.600	3.166	AC-FT=
FINISH										

10024E_010715.txt

```
*S
       ALBUQUERQUE PUBLIC SCHOOLS
*s
*S
       ELDORADO HIGH SCHOOL DRAINAGE ANALYSIS USE THE IA/INF METHOD TO COMPUTE THE RUNOFF
*S
       FILE: 10024E_010715.txt
*S
       EXISTING CONDITIONS
*s
      DATE: JAN 2015
*s
*s
       100 YEAR 24 HOUR STORM - EXISTING RUNOFF ANALYSIS RAINFALL FROM NOAA ATLAS 14, VOLUME 1, VERSION 4
*S
*s
  ***********************************
                 TIME=0.0 PUNCH CODE=0 PRINT CODE=0
START
                ALBUQUERQUE
LOCATION
**************************************
RAINFALL
                 TYPE=-2
                 QUARTER=1.12
                              ONE= 1.87 IN
                 SIX= 2.51 IN DAY= 3.08 IN
                                          DT = 0.05 HR
*S
*********************************
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                 NK=3 ISLOPE=0
LENGTH=100 FT
                               SLOPE=0.040
                 LENGTH=250 FT
                              SLOPE=0.040
                                          K = 2.0
                 LENGTH=150 FT SLOPE=0.040 K=3.0
                 KN=0.021 CENTROID DIST=250 FT
                 ID=1 HYD NO=101A DA= 0.0065594 SQ MI
PER A=0 PER B=0 PER C=65.78 PER D=34.22
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                 ID=1 CODE=1
*S ROUTE 101A IN 10-INCH STORM DRAIN
COMPUTE RATING CURVE CID=1 VS No=1 CODE=-1 SLP=0.03
DIA=0.83 FT N=0.025
ROUTE MCUNGE
                 ID=2 HYD NO=101A.R INFLOW ID=1
                 DT=0.0 L=700 FT NS=0 SLOPE=0.03
PRINT HYD
                 ID=2 CODE=1
*************************
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                 NK=3 ISLOPE=0
                                          K = 0.7
                 LENGTH=100 FT
                               SLOPE=0.040
                 LENGTH=750 FT
                              SLOPE=0.040
                                          K = 2.0
                 LENGTH=150 FT
                              SLOPE=0.040
                                          K = 3.0
                 KN=0.021 CENTROID DIST=500 FT
                 ID=3 HYD NO=101B DA= 0.0039166 SQ MI
PER A=0 PER B=0 PER C=80.18 PER D=19.82
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                 ID=3 CODE=1
*******************
             **** SUB-BASIN 102A **** (AREA=1.35 ACRES)
***************
              **** AP-11
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                 NK=3 ISLOPE=0
                                          K = 0.7
                 LENGTH=100 FT
                               SLOPE=0.015
                 LENGTH=400 FT
                              SLOPE=0.015
                                          K = 2.0
                 LENGTH=100 FT
                              SLOPE=0.015
                                          K = 3.0
                 KN=0.025 CENTROID DIST=300 FT
                 TD=7 HYD NO=102A DA= 0.0021153 SQ MI
PER A=0 PER B=0 PER C=100 PER D=0
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                 ID=7 CODE=1
**** SUB-BASIN 102B **** (AREA=1.16 ACRES)
**************
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                 NK=3 ISLOPE=0
                 LENGTH=100 FT
                              SLOPE=0.015
                 LENGTH=400 FT
                              SLOPE=0.015
                                          K = 2.0
```

10024E_010715.txt LENGTH=100 FT SLOPE=0.015 K=3.0 KN=0.025 CENTROID DIST=300 FT ID=39 HYD NO=102B DA= 0.0018130 SQ MI PER A=0 PER B=0 PER C=100 PER D=0 TP=0.133333 MASSRAIN=-1 COMPUTE NM HYD PRINT HYD ID=39 CODE=1 ************************************** COMPUTE LT TP LCODE=1 UPLAND/LAG TIME METHOD NK=3 ISLOPE=0 LENGTH=100 FT SLOPE=0.055K=2.0 LENGTH=875 FT SLOPE=0.055SLOPE=0.055 LENGTH=300 FT ELENGTH-300 FT SLOTE-0.037 R-3.0 KN=0.021 CENTROID DIST=638 FT ID=8 HYD NO=103 DA= 0.0063226 SQ MI PER A=0 PER B=0 PER C=4.96 PER D=95.04 TP=0.133333 MASSRAIN=-1 COMPUTE NM HYD ID=8 CODE=1 PRINT HYD ******************* **** SUB-BASIN 104 **** (AREA=8.36 ACRES) COMPUTE LT TP LCODE=1 UPLAND/LAG TIME METHOD NK=3 ISLOPE=0 LENGTH=100 FT SLOPE=0.034 LENGTH=850 FT SLOPE=0.034 K = 2.0LENGTH=2550 FT SLOPE=0.034 KN=0.021 CENTROID DIST=1750 FT TD=10 HYD NO=104 DA= 0.0130650 SQ MI PER A=0 PER B=0 PER C=13.30 PER D=86.70 TP=0.0 MASSRAIN=-1 ID=10 CODE=1 COMPUTE NM HYD PRINT HYD **** AP-2(ADD BASINS 103 AND 104) ADD HYD ID=14 HYD NO=AP-2 ID I=8 ID II=10 PRINT HYD ID=14 CODE=5 *S ROUTE BASINS 103 AND 104 IN CHANNEL COMPUTE RATING CURVE CID=1 VS No=1 CODE=-1 SLP=0.03 DIA=2.0 FT N=0.025 ROUTE MCUNGE ID=9 HYD NO=103.R INFLOW ID=14 DT=0.0 L=178 FT NS=0 SLOPE=0.03 PRINT HYD ID=9 CODE=1 **** AP-3(ADD BASINS 103 AND 104 AND 102B) =AP-3 ID I=9 ID II=39 CODE=5 ADD HYD ID=16 HYD NO=AP-3 PRINT HYD ID=16 COMPUTE RATING CURVE CID=1 VS NO=1 NO SEGS=1 MIN ELEV=0 MAX ELEV=1.3 CH SLOPE=0.027 FP SLOPE=0.027 N=0.017 DIST=7.09 N=0.017DIST ELEV 2.46 0.0 7.09 1.83 DIST ELEV 1.83 0.0 1.83 2.46 0.0 4.63 0.0 7.09 1.83 ID=17 HYD NO=AP-3.R INFLOW ID=16 DT=0.0 L=450 FT NS=0 SLOPE=0.027 ROUTE MCUNGE PRINT HYD ID=17 CODE=1

* **** (ADD BASINS 103 AND 104 AND 102B AND 101A) ID=18 HYD NO=18 ID I=17 ID II=2 ID=18 CODE=5 ADD HYD PRINT HYD

**** AP-4(ADD BASINS 103 AND 104 AND 102B AND 101A AND 101B.CHANNEL)*S =AP-4 ID I=18 ID II=3 CODE=5 ADD HYD ID=19 HYD NO=AP-4

PRINT HYD ID=19

COMPUTE LT TP LCODE=1 UPLAND/LAG TIME METHOD NK=3 ISLOPE=0

LENGTH=100 FT SLOPE=0.032 K=1.0

```
10024E_010715.txt
                              SLOPE=0.032 K=2.0
SLOPE=0.032 K=3.0
                  LENGTH=850 FT
                  LENGTH=750 FT
                                            K = 3.0
                 KN=0.021 CENTROID DIST=850 FT
ID=21 HYD NO=105 DA= 0.0055891 SQ MI
PER A=0 PER B=0 PER C=13.52 PER D=86.48
COMPUTE NM HYD
                  TP=0.133333
                             MASSRAIN=-1
                 ID=21 CODE=1
PRTNT HYD
*ROUTE SUB-BASINS 105 TO JUAN TABO THROUGH 12-INCH STORM DRAIN
*S **** AP-5
COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.017
                   DIA=1.0 FT N=0.011

ID=22 HYD NO=AP-5 INFLOW ID=21

DT=0.0 L=895 FT NS=0 SLOPE=0.017
ROUTE MCUNGE
PRINT HYD
                   ID=22 CODE=1
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                 NK=3 ISLOPE=0
                  LENGTH=100 FT
                               SLOPE=0.036
                                            K = 2.0
                  LENGTH=500 FT
                               SLOPE=0.036
                              SLOPE=0.036
                  LENGTH=850 FT
                                           K = 3.0
                 KN=0.021 CENTROID DIST=1450 FT
ID=24 HYD NO=106 DA= 0.0059657 SQ MI
PER A=0 PER B=0 PER C=8.94 PER D=91.06
COMPUTE NM HYD
                 TP=0.133333
                             MASSRAIN=-1
PRINT HYD
                 ID=24 CODE=1
**************************************
             **** SUB-BASIN 107 **** (AREA=3.78 ACRES)
*********
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                 NK=3 ISLOPE=0
LENGTH=100 FT
                               SLOPE=0.040
                                           K=1.0
                  LENGTH=360 FT
                               SLOPE=0.040
                                           K = 2.0
                 LENGTH=360 FT SLOPE=0.040 K=3.0
                  KN=0.021 CENTROID DIST=820 FT
                 TD=25 HYD NO=107 DA= 0.0059095 SQ MI
PER A=0 PER B=0 PER C=14.75 PER D=85.25
COMPUTE NM HYD
                 TP=0.133333 MASSRAIN=-1
PRINT HYD
                 ID=25 CODE=1
*************************
             **** SUB-BASIN 108A **** (AREA=2.77 ACRES)
***********
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                 NK=3 ISLOPE=0
                  LENGTH=100 FT
                                SLOPE=0.05
                 SLOPE=0.05 K=2.0

LINGIH=350 FT SLOPE=0.05 K=3.0

KN=0.025 CENTROID DIST=500 FT

ID=26 HYD NO=108A PA
                 ID=26 HYD NO=108A DA= 0.0043302 SQ MI
PER A=0 PER B=0 PER C=65.43 PER D=34.57
COMPUTE NM HYD
                 TP=0.133333
                             MASSRAIN=-1
PRINT HYD
                 ID=26 CODE=1
**** SUB-BASIN 108B **** (AREA=4.66 ACRES)
**** AP-10
*5
                 LCODE=1 UPLAND/LAG TIME METHOD
COMPUTE LT TP
                 NK=3 ISLOPE=0
                  LENGTH=100 FT
                                SLOPE=0.035
                                            K = 0.7
                  LENGTH=450 FT
                               SLOPE=0.035
                                           K = 2.0
                  LENGTH=350 FT
                               SLOPE=0.035
                 KN=0.021 CENTROID DIST=450 FT
                 TD=27  HYD NO=108B  DA= 0.0072807 SQ MI
PER A=0  PER B=0  PER C=58.81  PER D=41.19
TP=0.133333  MASSRAIN=-1
COMPUTE NM HYD
                 ID=27 CODE=1
PRINT HYD
COMPUTE LT TP
                 LCODE=1 UPLAND/LAG TIME METHOD
                 NK=3 ISLOPE=0
```

```
10024E_010715.txt
                   LENGTH=100 FT SLOPE=0.014 K=1.0

LENGTH=275 FT SLOPE=0.014 K=2.0

LENGTH=225 FT SLOPE=0.014 K=3.0
                   KN=0.021 CENTROID DIST=300 FT
                  ID=28 HYD NO=109A DA= 0.0007330 SQ MI
PER A=0 PER B=0 PER C=15.22 PER D=84.78
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                  ID=28 CODE=1
               **** ADD BASINS 103 AND 104 AND 102 AND 101A AND 101B.CHANNEL AND **** 109A AND 101B.SWALE)
*S
               ID=30 HYD NO=30 ID I=19 ID II=28
ADD HYD
PRINT HYD
                      ID=30 CODE=5
********************
              **** SUB-BASIN 109B **** (AREA=1.11 ACRES)
COMPUTE LT TP
                  LCODE=1 UPLAND/LAG TIME METHOD
                  NK=3 ISLOPE=0
                   LENGTH=100 FT
                                  SLOPE=0.024
                   LENGTH=225 FT
                                  SLOPE=0.024 K=2.0
                   LENGTH=175 FT SLOPE=0.024
                                               K = 3.0
                   KN=0.021 CENTROID DIST=250 FT
                  TD=31 HYD NO=109B DA= 0.0017420 SQ MI
PER A=0 PER B=0 PER C=0 PER D=100
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
                   ID=31 CODE=1
PRINT HYD
*
               **** ADD BASINS 103 AND 104 AND 102B AND 101A AND 101B.CHANNEL AND **** 109A AND 101B.SWALE AND 109B)
*S
*S
                                    ID I=30 ID II=31
ADD HYD
               ID=32 HYD NO=32
PRINT HYD
                      ID=32
                             CODE=5
COMPUTE LT TP
                   LCODE=1 UPLAND/LAG TIME METHOD
                   NK=3 ISLOPE=0
                   LENGTH=100 FT SLOPE=0.040 K=0.7

LENGTH=650 FT SLOPE=0.040 K=2.0

LENGTH=1275 FT SLOPE=0.040 K=3.0
                  KN=0.025 CENTROID DIST=1012 FT

ID=34 HYD NO=110 DA= 0.0147070 SQ MI

PER A=0 PER B=0 PER C=93.60 PER D=6.40
COMPUTE NM HYD
                   TP=0.133333 MASSRAIN=-1
PRINT HYD
                  ID=34 CODE=1
**** SUB-BASIN 111 **** (AREA=1.57 ACRES)
               **** AP-9
*S
COMPUTE LT TP
                  LCODE=1 UPLAND/LAG TIME METHOD
                   NK=3 ISLOPE=0
                   LENGTH=100 FT
                                  SLOPE=0.030 K=1.0
                   LENGTH=400 FT
                                  SLOPE=0.030
                                              K = 2.0
                   LENGTH=100 FT SLOPE=0.030
                                               K = 3.0
                  KN=0.021 CENTROID DIST=300 FT
ID=35 HYD NO=111 DA= 0.0024568 SQ MI
PER A=0 PER B=0 PER C=33.26 PER D=66.74
COMPUTE NM HYD
                  TP=0.133333 MASSRAIN=-1
ID=35 CODE=1
PRINT HYD
               **** (ADD 110 AND 106)
               ID=36 HYD_NO=36
ADD HYD
                                     ID I=34 ID II=24
                      ID=36 CODE=5
PRINT HYD
               **** AP-6
ADD HYD
               ID=37 HYD NO=AP-6
                                     ID I=36 ID II=25
PRINT HYD
                      ID=37 CODE=5
               **** AP-7
*5
               ID=38 HYD_NO=AP-7
ADD HYD
                                     ID I=37 ID II=26
PRINT HYD
                      ID=38 CODE=5
```

```
ID=40 HYD NO=112 DA= 0.0005390 SQ MI
PER A=0 PER B=0 PER C=85.1 PER D=14.9
TP=0.133333 MASSRAIN=-1
ID=40 CODE=1
COMPUTE NM HYD
PRINT HYD
              **** AP-8

**** ADD BASINS 103 AND 104 AND 102 AND 101A AND 101B.CHANNEL AND 109A AND 101B.SWALE AND 109B AND 112

ID=41 HYD NO=AP-8 ID I=32 ID II=40

ID=41 CODE=5
*S
*S
*S
ADD HYD
PRINT HYD
**** AP-1/POND
                    ID=33 HYD NO=AP-1/POND INFLOW=41 CODE=1
OUTFLOW (CFS) STORAGE (AC-FT) ELEV (FT)
ROUTE RESERVOIR
                    0.0
                                  0.0000
                                                  5692
                    1.5
                                  0.4501
                                                  5696
                                  0.6518
                                                  5697
                    35.5
98.7
                                  0.8809
                                                  5698
                                  1.1384
                                                  5699
                    108.7
                                  1.2744
                                                  5699.5
                   PRINT HYD
                                       ID=33 CODE=1
FINISH
```

1

10024E_010715.SUM - Ver. S4.01a, Rel: 01a RUN DATE (MON/DAY/YR) AHYMO PROGRAM SUMMARY TABLE (AHYMO-S4) =01/13/2015

<pre>INPUT FILE = 25-00\AE_DATA\CALCS\Hydrology\AHYMO\Resubmittal</pre>	Calcs_1214\10024E_010715.txt USER NO.=
WilsonCoANMSiteA96476897	

	COMMAND ID	HYDROGRAPH ENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	DISC	HARGE	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = NOTATION	1
	*S *S *S *S *S *S *S	USE THE I FILE: 100 EXISTING DATE: JAN	HIGH S A/INF 24E_01 CONDIT 2015	SCHOOL DR METHOD T 10715.txt FIONS	AINAGE ANA O COMPUTE	THE RUN		*****					
	*S *S *S *S	RAINFALL	FROM N	NOAA ATLA	- EXISTING S 14, VOLU	JME 1, V	ERSION 4						
0.00		*****			******	******	*****	*****				TIME=	
3.08		2 NOAA 14	ALBU	JQUERQUE								RAIN24=	
34.7	*S *S COMPUTE NM HYD	101A	*** SI -	JB-BASIN 1	101A **** 0.00656		.20 ACRES) 15.18	0.595	1.70143	1.500	3.616	PER IMP=	
0.2	*S ROUTE 101A IN ROUTE MCUNGE	10-INCH STOR 101A.R	M DRAI	IN 2	0.00656		12.89	0.592	1.69180	1.700	3.071	CCODE =	
19.8	*S COMPUTE NM HYD 82	101B [*]	*** St -	JB-BASIN 3	101B **** 0.00392	(AREA=2	8.51 ACRES) 8.59	0.304	1.45545	1.500	3.428	PER IMP=	
0.00	*S *S COMPUTE NM HYD		*** SU *** AF -		102A **** 0.00212	(AREA=1	35 ACRES) 4.29	0.126	1.11690	1.500	3.167	PER IMP=	
0.00	*S COMPUTE NM HYD	102B	*** SI -	JB-BASIN 39	102B **** 0.00181	(AREA=1	16 ACRES) 3.68	0.108	1.11690	1.500	3.168	PER IMP=	
95.0	*S COMPUTE NM HYD	103.00	*** SI -	JB-BASIN 8	103 **** (0.00632		05 ACRES) 17.88	0.924	2.74032	1.500	4.418	PER IMP=	
86.7		104.00	-	10	104 **** (0.01307		35.38	1.810	2.59786	1.500	4.231	PER IMP=	
	*S ADD HYD *S ROUTE BASINS	AP-2 103 AND 104 I	8&10 N CHAN	14 NNEL	0.01939		53.25	2.734	2.64428	1.500	4.292		
0.0	ROUTE MCUNGE *S					AND 104	53.25 AND 102B)	2.734	2.64428	1.500		CCODE =	
0.2	ADD HYD ROUTE MCUNGE	AP-3.R	16	17	0.02120 0.02120		56.93 56.55	2.842 2.842	2.51366 2.51380	1.500 1.500	4.196 4.168	CCODE =	
	*S ADD HYD *S	18.00 4(ADD BAS	17& 2 INS 10	18 03 AND 10	0.02776 4 AND 102E	B AND 10	0 102B AND 1 61.25 01A AND 101B	3.434 .CHANNEL)	2.31951	1.550	3.447		
	ADD HYD *S COMPUTE NM HYD		18& 3 *** St -		0.03168 105 **** (0.00559	AREA=3.	69.56 58 ACRES) 15.40	3.738 0.773	2.21267	1.550 1.500	3.4314.306	PER IMP=	
							. 1						

10024E_010715.SUM

		10024E_	010715.SUM				
86.48 *S	**** AP-5						
ROUTE MCUNGE	AP-5 21 22	0.00559	13.60	0.766	2.57083	1.650	3.803 CCODE =
*S COMPUTE NM HYD 91.06	**** SUB-B/ 106.00 - 24	ASIN 106 **** (AREA= 0.00597	=3.82 ACRES) 16.67	0.850	2.67233	1.500	4.366 PER IMP=
*S	**** SUB-B	ASIN 107 **** (AREA=	=3.78 ACRES)				
ç COMMAND ID	FROM TO HYDROGRAPH ID ID ENTIFICATION NO. NO		PEAK ISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PAGE = 2 PER ACRE NOTATION
COMPUTE NM HYD	107.00 - 25	0.00591	16.22	0.811	2.57309	1.500	4.289 PER IMP=
85.25 *S COMPUTE NM HYD 34.57	**** SUB-B/ 108A - 26	ASIN 108A **** (AREA 0.00433	A=2.77 ACRES) 10.04	0.394	1.70740	1.500	3.622 PER IMP=
*S *S *S	**** SUB-B/ **** AP-10	ASIN 108B **** (AREA	A=4.66 ACRES))			
COMPUTE NM HYD	108B - 27	0.00728	17.27	0.707	1.82048	1.500	3.707 PER IMP=
*S COMPUTE NM HYD 84.78	**** SUB-B/ 109A - 28	ASIN 109A **** (AREA 0.00073	A=0.47 ACRES) 2.02	0.100	2.56506	1.500	4.312 PER IMP=
*S *S	ADD BASINS 103 AND **** 109A AND 101B.SWA	104 AND 102 AND 101	LA AND 101B.	CHANNEL AND			
ADD HYD *S	30.00 19&28 30	0.03241 ASIN 109B **** (AREA	71.49	3.838	2.22063	1.550	3.446
COMPUTE NM HYD 100.00	109в - 31	0.00174	5.00	0.262	2.82504	1.500	4.487 PER IMP=
*S	DD BASINS 103 AND 3	LO4 AND 102B AND 101	LA AND 101B.	CHANNEL AND			
ADD HYD *S	32.00 30&31 32		76.23 =9 41 ACRES)	4.101	2.25145	1.550	3.488
COMPUTE NM HYD	110.00 - 34		30.56	0.962	1.22622	1.500	3.247 PER IMP=
*S *S	**** SUB-B	ASIN 111 **** (AREA=	=1.57 ACRES)				
*S COMPUTE NM HYD	**** AP-9 111.00 - 35	0.00246	6.37	0.296	2.25691	1.500	4.051 PER IMP=
66.74 *S		L10 AND 106)					
ADD HYD *S	36.00 34&24 36 **** AP-6	0.02067	47.23	1.812	1.64351	1.500	3.570
ADD HYD *S	AP-6 36&25 37 *** AP-7	0.02658	63.45	2.623	1.85015	1.500	3.730
ADD HYD *S	AP-7 37&26 38	0.03091 ASIN 112 **** (AREA=	73.49 -0.34 ACRES)	3.017	1.83015	1.500	3.715
COMPUTE NM HYD	112.00 - 40	0.00054	1.17	0.039	1.37141	1.500	3.402 PER IMP=
*S *S *S	*** AP-8 ADD BASINS 103 AND 1094 AND 1018 SW	104 AND 102 AND 101 ALE AND 109B AND 112	LA AND 101B.C	CHANNEL AND			
ADD HYD *S *S	AP-8 32&40 41 **** POND **** AP-1/	0.03469	77.37	4.140	2.23767	1.550	3.485
ROUTE RESERVOIR	AP-1/POND 41 33		70.28	4.140	2.23767	1.600	3.166 AC-FT=
FINISH							

```
*S
       ALBUQUERQUE PUBLIC SCHOOLS
*s
*S
       ELDORADO HIGH SCHOOL DRAINAGE ANALYSIS USE THE IA/INF METHOD TO COMPUTE THE RUNOFF
*S
       FILE: 1006P.txt
*S
       PROPOSED CONDITIONS
*s
       DATE: JAN. 2015
*s
*s
*S
       100 YEAR 6 HOUR STORM - PROPOSED RUNOFF ANALYSIS
*s
       RAINFALL FROM NOAA ATLAS 14, VOLUME 1, VERSION 5, WEB
  ***********************************
START
                 TIME=0.0 PUNCH CODE=0 PRINT CODE=0
LOCATION
                 ALBUQUERQUE
**************************************
RAINFALL
                 TYPE=-1
                 QUARTER=1.12
                              ONE= 1.87 IN
                 SIX= 2.51 IN DAY= 3.08 IN
                                          DT = 0.0333 HR
**** SUB-BASIN 201A **** (AREA=4.2 ACRES)
ID=1 HYD NO=201A DA= 0.0065 SQ MI
PER A=0 PER B=0 PER C=64.7 PER D=35.3
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                 ID=1 CODE=1
*************************
ID=2 HYD NO=201B DA= 0.0050 SQ MI
PER A=0 PER B=0 PER C=70.8 PER D=29.20
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                 ID=2 CODE=1
********************
ID=3 HYD NO=201C DA= 0.0014 SQ MI
PER A=0 PER B=0 PER C=25 PER D=75
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                 ID=3 CODE=1
********************
             **** SUB-BASIN 201D **** (AREA=1.2 ACRES)
ID=4 HYD NO=201D DA= 0.0019 SQ MI
PER A=0 PER B=0 PER C=74.4 PER D=25.6
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                 ID=4 CODE=1
*ROUTE SUB-BASIN 201C THROUGH SWALE
COMPUTE RATING CURVE CID=1 VS NO=1 NO SEGS=1
MIN ELEV=0 MAX ELEV=1.3
                   CH SLOPE=0.027 FP SLOPE=0.027
N=0.017 DIST=11
                   N=0.017
                   DIST ELEV
0.0 0.5
10.5 0.0
                             DIST ELEV
0.5 0.0
                       0.0 11.0 U.5
HYD NO=201C.SWALE INFLOW ID=3
ROUTE MCUNGE
                   ID=5
                   DT=0.0 L=300 FT NS=0 SLOPE=0.027 ID=5 CODE=1
PRINT HYD
             **** (ADD 201C.SWALE AND 201B)
*5
                   HYD NO=201B.1 ID I=5 ID II=2
ID=6 CODE=5
ADD HYD
             ID=6
PRINT HYD
*ROUTE 201B.1 THROUGH SWALE COMPUTE RATING CURVE CID=1 VS_NO=1 NO SEGS=1
                   MIN ELEV=0 MAX ELEV=1.3
                   CH SLOPE=0.030 FP SLOPE=0.030
                                DIST=11
                   N=0.017
                  DIST ELEV DIST ELEV

0.0 0.5 0.5 0.0

10.5 0.0 11.0 0.5

ID=7 HYD NO=201B.SWALE INFLOW ID=6
ROUTE MCUNGE
                   DT=0.0 L=300 FT NS=0 SLOPE=0.030
```

```
PRINT HYD
                  ID=7 CODE=1
             **** (ADD 201B.SWALE AND 201D)
*5
ADD HYD
             ID=8
                    HYD NO=201D.1 ID I=7 ID II=4 ID=8 CODE=5
PRINT HYD
**************************************
ID=9 HYD NO=205A DA= 0.0057 SQ MI
PER A=0 PER B=0 PER C=13.4 PER D=86.6
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                 ID=9 CODE=1
**************************************
ID=3 HYD NO=205B DA= 0.0012 SQ MI
PER A=0 PER B=0 PER C=10 PER D=90
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                 ID=3 CODE=1
*
             **** (ADD BASINS 205A AND 205B)
                   HYD NO=205.1
                                ID I=9 ID II=3
ADD HYD
             TD=6
*ROUTE SUB-BASINS 205A AND 205B TOWARD JUAN TABO THROUGH 30-INCH STORM DRAIN
COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.017 DIA=2.5 FT N=0.011
                  ID=9 HYD NO=205.1R INFLOW ID=6
DT=0.0 L=660 FT NS=0 SLOPE=0.017
ROUTE MCUNGE
PRINT HYD
                  ID=9 CODE=1
             **** (ADD 201D.1 AND 205.1R)
ID=3 HYD NO=201D.2 ID I=8 ID II=9
*s
ADD HYD
PRINT HYD
                    ID=3 CODE=1
*S DIVIDE 201D.2 BY A RATING CURVE (TYPE D INLET 12" ORIFICE TO JT AND 30" OVERFLOW TO POND)
                              ID I=6 HYD NO=AP-5
ID II=8 HYD NO=AP-12:DPOND.1
DIVIDE HYD
                 ID=3 CODE=999
                 TOTAL FLOW
                               DIVIDED FLOW
                   3.56
37.44
                                  3.56
                                  5.40
                    45.71
                                  5.90
                   52.59
                                  6.30
             **** (AP-5 JUAN TABO)
PRINT HYD
                ID=6 CODE=5
             **** (AP-12:DPOND.1)
PRINT HYD
                ID=8 CODE=5
**************************************
**** AP-11
*S
                 ID=9 HYD NO=AP-11 DA= 0.0021 SQ MI PER A=0 PER B=0 PER C=100 PER D=0 TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                 ID=9
                     CODE=1
************************************
             **** SUB-BASIN 202B **** (AREA=1.2 ACRES)
COMPUTE NM HYD
                 ID=3 HYD NO=202B DA= 0.0019 SQ MI
                 PER A=0 PER B=0 PER C=100 PER D=0
TP=0.133333 MASSRAIN=-1
PRINT HYD
                 ID=3
                      CODE=1
*************************
ID=10 HYD NO=202C DA= 0.0010 SQ MI PER A=0 PER B=0 PER C=92 PER D=8
COMPUTE NM HYD
                 TP=0.133333 MASSRAIN=-1
```

```
PRINT HYD
                    ID=10 CODE=1
**************************
               **** SUB-BASIN 203 **** (AREA=4.0 ACRES)
*************************************
                    COMPUTE NM HYD
PRINT HYD
                    ID=11 CODE=1
*ROUTE THE TOTAL FLOW THROUGH THE WATER QUALITY POND
                     ID=12 HYD NO=WQ.POND INFLOW=11 CODE=1
OUTFLOW (CFS) STORAGE (AC-FT) ELEV (FT)
0.00 0.0000 5728
ROUTE RESERVOIR
                      0.00
7.030
                                     0.0097
                                                       5729
                      24.12
                                     0.0296
PRINT HYD
                      ID=12 CODE=1
*******************
              **** SUB-BASIN 204 **** (AREA=8.3 ACRES)
COMPUTE LT TP
                    LCODE=1 UPLAND/LAG TIME METHOD
                    NK=3 ISLOPE=0
LENGTH=100 FT
                                    SLOPE=0.034
                    LENGTH=850 FT SLOPE=0.034 K=2.0
LENGTH=2550 FT SLOPE=0.034 K=3.0
KN=0.021 CENTROID DIST=1750 FT
                    LENGTH=850 FT
                                    SLOPE=0.034
                                                  K = 2.0
                   ID=11 HYD NO=204 DA= 0.0130 SQ MI
PER A=0 PER B=0 PER C=13.3 PER D=86.7
TP=0.0 MASSRAIN=-1
ID=11 CODE=1
COMPUTE NM HYD
PRINT HYD
**********************
               **** (AP-2: ADD WQ.POND AND BASIN 204)
ID=13 HYD NO=AP-2 ID I=11 ID II=12
ID=13 CODE=5
ADD HYD
PRINT HYD
                **** ROUTE AP-2
COMPUTE RATING CURVE CID=1 VS NO=1 NO SEGS=1
MIN ELEV=0 MAX ELEV=1.3
CH SLOPE=0.027 FP SLOPE=0.027
N=0.017 DIST=7.09
                      N=0.017 DIST=7.09
DIST ELEV DIST ELEV
0.0 1.83 2.46 0.0
4.63 0.0 7.09 1.83
ID=11 HYD NO=AP-2.R INFLOW ID=13
DT=0.0 L=400 FT NS=0 SLOPE=0.027
ID=11 CODE=1
ROUTE MCUNGE
PRINT HYD
                **** (AP-3: ADD AP-2.R AND BASIN 202B)
ID=12 HYD NO=AP-3 ID I=11 ID II=3
ADD HYD
PRINT HYD
                        ID=12 CODE=5
                ADD HYD
PRINT HYD
                **** (ROUTE 201A.1)
COMPUTE RATING CURVE CID=1 VS NO=1 NO SEGS=1
                      MIN ELEV=0 MAX ELEV=1.3
                      CH SLOPE=0.027 FP SLOPE=0.027
N=0.017 DIST=7.09
                      N=0.017 DIST=7.09

DIST ELEV DIST ELEV

0.0 1.83 2.46 0.0

4.63 0.0 7.09 1.83

ID=1 HYD NO=201A.1.R INFLOW ID=2

DT=0.0 L=450 FT NS=0 SLOPE=0.027
ROUTE MCUNGE
PRINT HYD
                      ID=1 CODE=1
*s
                **** (AP-4: ADD 201A.1.R AND BASIN 202C)
ADD HYD
                ID=2 HYD_NO=AP-4:DPOND.2 ID I=1 ID II=10
PRINT HYD
                        ID=2
                                CODE=5
*******************
```

```
**** AP-13
*S
               ID=1    HYD NO=AP-13    DA= 0.0043 SQ MI
PER A=0    PER B=0    PER C=0.0    PER D=100.0
TP=0.133333    MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
               ID=1 CODE=1
ID=3      HYD NO=207      DA= 0.0061 SQ MI
PER A=0      PER B=0      PER C=14.1      PER D=85.9
TP=0.133333      MASSRAIN=-1
COMPUTE NM HYD
               ID=3 CODE=1
PRINT HYD
**************************************
            **** SUB-BASIN 208A **** (AREA=1.9 ACRES)
               ID=4 HYD NO=208A DA= 0.0026448 SQ MI
COMPUTE NM HYD
               PER A=0 PER B=0 PER C=89.69 PER D=10.4
TP=0.133333 MASSRAIN=-1
PRINT HYD
               ID=4 CODE=1
**************************************
ID=5  HYD NO=210  DA= 0.0163 SQ MI
PER A=0  PER B=0  PER C=85.1  PER D=14.9
TP=0.133333  MASSRAIN=-1
COMPUTE NM HYD
               ID=5 CODE=1
PRINT HYD
**** SUB-BASIN 211 **** (AREA=1.6 ACRES)
**** AP-9
*S
               ID=7 HYD NO=AP-9 DA= 0.0025SQ MI
COMPUTE NM HYD
               PER A=0 PER B=0 PER C=33.3 PER D=66.7
TP=0.133333 MASSRAIN=-1
ID=7 CODE=1
PRINT HYD
            **** (AP-6: ADD 210 AND 207)
            ID=10 HYD NO=AP-6 ID I=5 ID II=3 ID=10 CODE=5
ADD HYD
PRINT HYD
            ADD HYD
PRINT HYD
*****************
            **** SUB-BASIN 208B **** (AREA=1.1 ACRES)
********
            **** AP-10
               ID=13 HYD NO=AP-10 DA= 0.0029 SQ MI
PER A=0 PER B=0 PER C=62.1 PER D=37.9
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
               ID=13 CODE=1
********************
            **** SUB-BASIN 209A **** (AREA=1.1 ACRES)
330-03310 203A (ARCA-1:1 ACRC3)
               ID=4 HYD NO=209A DA= 0.0009 SQ MI
PER A=0 PER B=0 PER C=33.3 PER D=66.7
TP=0.133333 MASSRAIN=-1
ID=4 CODE=1
COMPUTE NM HYD
PRINT HYD
**************************************
ID=10 HYD NO=209B DA= 0.0017 SQ MI PER A=0 PER B=0 PER C=0 PER D=100 TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
               ID=10 CODE=1
```

```
ID=11   HYD NO=212   DA= 0.0005 SQ MI
PER A=0   PER B=0   PER C=75 PER D=25
TP=0.13333   MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                ID=11 CODE=1
             **** (ADD BASINS 209A AND 209B)
ID=12 HYD NO=DPOND.3 ID I=4 ID II=10
*S
ADD HYD
                    ID=12 CODE=5
PRINT HYD
             **** (ADD BASIN 212 AND DPOND.3) ID=4 HYD NO=DPOND.3.0
*S
                   HYD NO=DPOND.3.0 ID I=11 ID II=12 ID=4 CODE=5
ADD HYD
PRINT HYD
             **** (ADD AP-12 AND AP-4)
*S
ADD HYD
             ID=10`
                   HYD NO=DPOND.N ID I=8 ID II=2
                    ID=10 CODE=5
PRINT HYD
             *S
ADD HYD
PRINT HYD
**** POND ****
**********************
*
             **** AP-1:POND OUTLET
                ID=4 HYD NO=AP-1:POND OUTLET INFLOW=2 CODE=1
OUTFLOW (CFS) STORAGE (AC-FT) ELEV (FT)
0.0 0.0000 56988.58
ROUTE RESERVOIR
                               0.0001
                  4.4
                                             5690
                               0.0001
                                             5691
                  16.2
                               0.0001
                                             5692
                               0.041
                                             5693
                  32.0
                               0.136
                                             5694
                  43.6
                               0.275
                                             5695
                  56.7
                               0.450
                                             5696
                  67.2
                               0.651
                                             5697
                  107.9
177.8
                               0.880
                                             5698
                               1.138
                                             5699
                  191.0
                               1.274
                                             5699.5
PRINT HYD
                  ID=4 CODE=1
FINISH
```

USER NO.=

1

- Ver. S4.01a, Rel: 01a RUN DATE (MON/DAY/YR)

AHYMO PROGRAM SUMMARY TABLE (AHYMO-S4) - Ver. S4.01a, R =01/13/2015
INPUT FILE = C:\Users\EEValdez\Desktop\AHYMO\Resubmittal Calcs_1214\1006P.txt
AHYMO_Temp_User:20122010

ATTMO_TCIIIP_03CT .20	0122010										
COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	DISC	EAK CHARGE CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = NOTATION
-		`HIGH S IA/INF 06P.txt CONDIT N. 2015	CHOOL DE METHOD 1 : IONS	RAINAGE ANA FO COMPUTE	THE RUI		*****				
*S *S *S 100 YEAR 6 HOUR STORM - PROPOSED RUNOFF ANALYSIS *S RAINFALL FROM NOAA ATLAS 14, VOLUME 1, VERSION 5, WEB *S *S *S ****************************											
*S ********* START 0.00	*****	*****	*****	******	*****	*****	****				TIME=
LOCATION RAINFALL TYPE 2.510 *S	E= 1 NOAA 14	ALBU	QUERQUE								RAIN6=
*S COMPUTE NM HYI 35.30		**** SU -	B-BASIN 1	201A **** 0.00650	(AREA=4	4.2 ACRES) 15.30	0.526	1.51797	1.532	3.677	PER IMP=
*S COMPUTE NM HYI 29.20		**** SU -	B-BASIN 2	201B **** 0.00500	(AREA=	3.2 ACRES) 11.52	0.386	1.44865	1.532	3.600	PER IMP=
*S COMPUTE NM HYI 75.00			B-BASIN 3	201C **** 0.00140	(AREA=0	0.9 ACRES) 3.76	0.147	1.96914	1.532	4.202	PER IMP=
*S COMPUTE NM HYI 25.60		**** SU -	B-BASIN 4	201D **** 0.00190	(AREA=1	1.2 ACRES) 4.33	0.143	1.40774	1.532	3.563	PER IMP=
ROUTE MCUNGE 0.1	201C.SWALE	3	5	0.00140		3.76	0.147	1.96909	1.565	4.197	CCODE =
*S ADD HYD ROUTE MCUNGE 0.2		**** (A 5& 2 6	DD 201C. 6 7	0.00640 0.00640	201B)	15.27 15.26	0.533 0.533	1.56238 1.56251	1.532 1.532	3.728 3.726	CCODE =
*S ADD HYD *S	201D.1	7& 4	8	.SWALE AND 0.00830 205A ****		19.59 3.6 ACRES)	0.676	1.52699	1.532	3.688	
COMPUTE NM HYI 86.60 *S			9	0.00570 205B ****	(ADEA-(15.81	0.639	2.10097	1.532	4.335	PER IMP=
COMPUTE NM HYI	о 205в	-	3	0.00120		3.38	0.137	2.13961	1.532	4.398	PER IMP=
*S ADD HYD *S	205.10		DD BASIN 6	NS 205A AND 0.00690	205B)	19.19	0.776	2.10762	1.532	4.346	
ROUTE MCUNGE 0.1	205.1R		9	0.00690		19.15	0.775	2.10661	1.532	4.337	CCODE =
*S ADD HYD *S DIVIDE 2010 DIVIDE HYD	201D.2 D.2 BY A RATING AP-5	8& 9	3	.1 AND 205. 0.01520 INLET 12" 0.00613	-	38.75 E TO JT AND 5.48	1.451 30" OVERF 0.585	1.79008 1.79008	1.532 1.532	3.983 1.397	
*S	AP-12:DPOND.	and	8	0.00907 202A ****	(AREA=1	33.27	0.866	1.79008	1.532	5.731	

**	د بدید			1000P.SUM				
*S COMPUTE NM HYD 0.00	AP-11	** AP-11 - 9	0.00210	4.34	0.125	1.11681	1.532	3.227 PER IMP=
*S COMPUTE NM HYD	*** 202B	** SUB-BASII	N 202B **** 0.00190	(AREA=1.2 ACRES) 3.93	0.113	1.11681	1.532	3.228 PER IMP=
0.00 *S	***	** SUB-BASI	N 202C ****	(AREA=0.7 ACRES)				
° COMMAND II	HYDROGRAPH	FROM TO ID ID NO. NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PAGE = 2 PER ACRE NOTATION
COMPUTE NM HYD	202C	- 10	0.00100	2.14	0.064	1.20772	1.532	3.350 PER IMP=
8.00 *S COMPUTE NM HYD 99.00	203.00	** SUB-BASII - 11	N 203 **** (0.00630	(AREA=4.0 ACRES) 18.12	0.753	2.24189	1.499	4.493 PER IMP=
ROUTE RESERVOIR 0.023	WQ.POND	11 12	0.00630	18.18	0.753	2.24184	1.532	4.510 AC-FT=
*S COMPUTE NM HYD 86.70	204.00	- 11	0.01300	(AREA=8.3 ACRES) 35.79	1.457	2.10210	1.532	4.301 PER IMP=
*S ADD HYD	AP-2 11	L&12 13	0.01930	AND BASIN 204) 53.97	2.211	2.14770	1.532	4.369
*S ROUTE MCUNGE	*** AP-2.R	** ROUTE AP 13 11	0.01930	53.41	2.209	2.14627	1.565	4.324 CCODE =
0.1 *S ADD HYD *S	AP-3 11	L& 3 12	0.02120	ND BASIN 202B) 57.10	2.322	2.05398	1.565	4.209
ADD HYD *S	201A.1 12		3 AND BASIN 0.02770	71.94	2.849	1.92819	1.532	4.058
ROUTE MCUNGE	201A.1.R	2 1	0.02770	71.84	2.847	1.92697	1.565	4.052 CCODE =
*S ADD HYD *S *S	AP-4:DPOND.2 1	L&10 2	0.02870	AND BASIN 202C) 73.86 (AREA=2.8 ACRES)	2.911	1.90188	1.565	4.021
COMPUTE NM HYD	AP-13	- 1	0.00430	12.40	0.517	2.25325	1.499	4.506 PER IMP=
*S COMPUTE NM HYD 85.90		** SUB-BASII - 3	N 207 **** (0.00610	(AREA=3.9 ACRES) 16.89	0.681	2.09301	1.532	4.325 PER IMP=
*S COMPUTE NM HYD 10.39	208A	- 4	0.00264	(AREA=1.9 ACRES) 5.69	0.174	1.23489	1.532	3.364 PER IMP=
*S COMPUTE NM HYD 14.90	210.00		N 210 **** (0.01630	(AREA=10.4 ACRES) 35.60	1.118	1.28614	1.532	3.413 PER IMP=
*S *S *S	***	** AP-9		(AREA=1.6 ACRES)	0.350	1 07403	1 522	4 006 050 700
COMPUTE NM HYD	AP-9	- 7	0.00250	6.54	0.250	1.87482	1.532	4.086 PER IMP=
*S ADD HYD *S	AP-6 5	5& 3 10	DD 210 AND 2 0.02240		1.799	1.50584	1.532	3.661
ADD HYD *S *S	AP-7 10 ***)& 4 3	0.02504	58.19 (AREA=1.1 ACRES)	1.973	1.47722	1.532	3.630
COMPUTE NM HYD	AP-10	- 13	0.00290	6.90	0.239	1.54752	1.532	3.715 PER IMP=
*S COMPUTE NM HYD		** SUB-BASII - 4	N 209A **** 0.00090	(AREA=1.1 ACRES) 2.36	0.090	1.87482	1.532	4.105 PER IMP=
				Page 2				

66.70										
*S	*	*** SU	JB-BASIN	209B **** (AREA=1.1 ACRES)					
COMPUTE NM HY	D 209B	-	10	0.00170	4.91	0.204	2.25325	1.499	4.511 P	ER IMP=
100.00										
*S	*	*** SU	JB-BASIN	212 **** (A	REA=0.3 ACRES)					
COMPUTE NM HY	D 212.00	-	11	0.00050	1.15	0.037	1.40092	1.532	3.597 P	ER IMP=
25.00										
*S	*	*** (A	ADD BASI	NS 209A AND	209в)					
ADD HYD	DPOND.3			0.00260	7.27	0.294	2.12206	1.532	4.369	
*S			ADD BASI	N 212 AND DF						
ADD HYD	DPOND.3.0		4	0.00310	8.42	0.332	2.00569	1.532	4.245	
*S				2 AND AP-4)						
ADD HYD	DPOND.N			0.03777	106.36	3.777	1.87503	1.565	4.400	
*S				D DPOND.3.0						
ADD HYD				0.04087	114.16	4.109	1.88494	1.565	4.364	
*S	*	*** PC)ND ****							
₽										
		FROM	TO		PEAK	RUNOFF		TIME TO	CFS	PAGE = 3
	HYDROGRAPH	ID	ID	AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER	
COMMAND	IDENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATION
			_							
*S			P-1:POND				4 00405	4 665	2 242	
ROUTE RESERVO	IR AP-1:POND	2	4	0.04087	87.57	4.109	1.88495	1.665	3.348 A	C-FT=
0.766										
FINISH										

```
*S
      ALBUQUERQUE PUBLIC SCHOOLS
*s
*S
       ELDORADO HIGH SCHOOL DRAINAGE ANALYSIS
       USE THE IA/INF METHOD TO COMPUTE THE RUNOFF
*S
       FILE: 10024P txt
*S
       PROPOSED CONDITIONS
*s
      DATE: JAN. 2015
*s
*s
*S
       100 YEAR 24 HOUR STORM - PROPOSED RUNOFF ANALYSIS
       RAINFALL FROM NOAA ATLAS 14, VOLUME 1, VERSION 5, WEB
*s
  ***********************************
START
                 TIME=0.0 PUNCH CODE=0 PRINT CODE=0
LOCATION
                ALBUQUERQUE
**************************************
RAINFALL
                 TYPE=-2
                 QUARTER=1.12
                              ONE= 1.87 IN
                 SIX= 2.51 IN DAY= 3.08 IN
                                         DT = 0.05 HR
**** SUB-BASIN 201A **** (AREA=4.2 ACRES)
ID=1 HYD NO=201A DA= 0.0065 SQ MI
PER A=0 PER B=0 PER C=64.7 PER D=35.3
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                ID=1 CODE=1
*************************
ID=2 HYD NO=201B DA= 0.0050 SQ MI
PER A=0 PER B=0 PER C=70.8 PER D=29.20
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                ID=2 CODE=1
********************
ID=3 HYD NO=201C DA= 0.0014 SQ MI
PER A=0 PER B=0 PER C=25 PER D=75
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                ID=3 CODE=1
********************
             **** SUB-BASIN 201D **** (AREA=1.2 ACRES)
ID=4 HYD NO=201D DA= 0.0019 SQ MI
PER A=0 PER B=0 PER C=74.4 PER D=25.6
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                ID=4 CODE=1
*ROUTE SUB-BASIN 201C THROUGH SWALE
COMPUTE RATING CURVE CID=1 VS NO=1 NO SEGS=1
MIN ELEV=0 MAX ELEV=1.3
                  CH SLOPE=0.027 FP SLOPE=0.027
N=0.017 DIST=11
                  N=0.017
                  DIST ELEV
0.0 0.5
10.5 0.0
                            DIST ELEV
0.5 0.0
                      0.0 11.0 U.5
HYD NO=201C.SWALE INFLOW ID=3
ROUTE MCUNGE
                  ID=5
                  DT=0.0 L=300 FT NS=0 SLOPE=0.027 ID=5 CODE=1
PRINT HYD
             **** (ADD 201C.SWALE AND 201B)
*5
                   HYD NO=201B.1 ID I=5 ID II=2 ID=6 CODE=5
ADD HYD
             ID=6
PRINT HYD
*ROUTE 201B.1 THROUGH SWALE COMPUTE RATING CURVE CID=1 VS_NO=1 NO SEGS=1
                  MIN ELEV=0 MAX ELEV=1.3
                  CH SLOPE=0.030 FP SLOPE=0.030
                               DIST=11
                  N=0.017
                  DIST ELEV DIST ELEV

0.0 0.5 0.5 0.0

10.5 0.0 11.0 0.5

ID=7 HYD NO=201B.SWALE INFLOW ID=6
ROUTE MCUNGE
                  DT=0.0 L=300 FT NS=0 SLOPE=0.030
```

```
ID=7 CODE=1
PRINT HYD
              **** (ADD 201B.SWALE AND 201D)
*5
ADD HYD
              ID=8
                    HYD NO=201D.1 ID I=7 ID II=4 ID=8 CODE=5
PRINT HYD
**************************************
ID=9 HYD NO=205A DA= 0.0057 SQ MI
PER A=0 PER B=0 PER C=13.4 PER D=86.6
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                 ID=9 CODE=1
**************************************
             **** SUB-BASIN 205B **** (AREA=0.8 ACRES)
*******
                 ID=3 HYD NO=205B DA= 0.0012 SQ MI
PER A=0 PER B=0 PER C=10 PER D=90
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                 ID=3 CODE=1
*
              **** (ADD BASINS 205A AND 205B)
                   HYD NO=205.1
                                 ID I=9 ID II=3
ADD HYD
             TD=6
*ROUTE SUB-BASINS 205A AND 205B TOWARD JUAN TABO THROUGH 30-INCH STORM DRAIN
COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.017 DIA=2.5 FT N=0.011
                   ID=9 HYD NO=205.1R INFLOW ID=6
DT=0.0 L=660 FT NS=0 SLOPE=0.017
ROUTE MCUNGE
PRINT HYD
                   ID=9 CODE=1
             **** (ADD 201D.1 AND 205.1R)
ID=3 HYD NO=201D.2 ID I=8 ID II=9
*s
ADD HYD
PRINT HYD
                    ID=3 CODE=1
*S DIVIDE 201D.2 BY A RATING CURVE (TYPE D INLET 12" ORIFICE TO JT AND 30" OVERFLOW TO POND)
                               ID I=6 HYD NO=AP-5
ID II=8 HYD NO=AP-12:DPOND.1
DIVIDE HYD
                 ID=3 CODE=999
                 TOTAL FLOW
                               DIVIDED FLOW
                    3.56
37.44
                                   3.56
                                   5.40
                    45.71
                                   5.90
                    52.59
                                   6.30
              **** (AP-5 JUAN TABO)
PRINT HYD
                 ID=6 CODE=5
              **** (AP-12:DPOND.1)
PRINT HYD
                 ID=8 CODE=5
**************************************
**** AP-11
*S
                 ID=9 HYD NO=AP-11 DA= 0.0021 SQ MI PER A=0 PER B=0 PER C=100 PER D=0 TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                 ID=9 CODE=1
************************************
             **** SUB-BASIN 202B **** (AREA=1.2 ACRES)
COMPUTE NM HYD
                 ID=3 HYD NO=202B DA= 0.0019 SQ MI
                 PER A=0 PER B=0 PER C=100 PER D=0
TP=0.133333 MASSRAIN=-1
PRINT HYD
                 ID=3
                      CODE=1
*************************
ID=10 HYD NO=202C DA= 0.0010 SQ MI PER A=0 PER B=0 PER C=92 PER D=8
COMPUTE NM HYD
                 TP=0.133333 MASSRAIN=-1
```

```
PRINT HYD
                    ID=10 CODE=1
**************************
               **** SUB-BASIN 203 **** (AREA=4.0 ACRES)
*************************************
                    COMPUTE NM HYD
PRINT HYD
                    ID=11 CODE=1
*ROUTE THE TOTAL FLOW THROUGH THE WATER QUALITY POND
                     ID=12 HYD NO=WQ.POND INFLOW=11 CODE=1
OUTFLOW (CFS) STORAGE (AC-FT) ELEV (FT)
0.00 0.0000 5728
ROUTE RESERVOIR
                      0.00
7.030
                                     0.0097
                                                       5729
                      24.12
                                     0.0296
PRINT HYD
                      ID=12 CODE=1
*******************
              **** SUB-BASIN 204 **** (AREA=8.3 ACRES)
COMPUTE LT TP
                    LCODE=1 UPLAND/LAG TIME METHOD
                    NK=3 ISLOPE=0
LENGTH=100 FT
                                    SLOPE=0.034
                    LENGTH=850 FT SLOPE=0.034 K=2.0
LENGTH=2550 FT SLOPE=0.034 K=3.0
KN=0.021 CENTROID DIST=1750 FT
                    LENGTH=850 FT
                                    SLOPE=0.034
                                                  K = 2.0
                   ID=11 HYD NO=204 DA= 0.0130 SQ MI
PER A=0 PER B=0 PER C=13.3 PER D=86.7
TP=0.0 MASSRAIN=-1
ID=11 CODE=1
COMPUTE NM HYD
PRINT HYD
**********************
               **** (AP-2: ADD WQ.POND AND BASIN 204)
ID=13 HYD NO=AP-2 ID I=11 ID II=12
ID=13 CODE=5
ADD HYD
PRINT HYD
                **** ROUTE AP-2
COMPUTE RATING CURVE CID=1 VS NO=1 NO SEGS=1
MIN ELEV=0 MAX ELEV=1.3
CH SLOPE=0.027 FP SLOPE=0.027
N=0.017 DIST=7.09
                      N=0.017 DIST=7.09
DIST ELEV DIST ELEV
0.0 1.83 2.46 0.0
4.63 0.0 7.09 1.83
ID=11 HYD NO=AP-2.R INFLOW ID=13
DT=0.0 L=400 FT NS=0 SLOPE=0.027
ID=11 CODE=1
ROUTE MCUNGE
PRINT HYD
                **** (AP-3: ADD AP-2.R AND BASIN 202B)
ID=12 HYD NO=AP-3 ID I=11 ID II=3
ADD HYD
PRINT HYD
                        ID=12 CODE=5
                ADD HYD
PRINT HYD
                **** (ROUTE 201A.1)
COMPUTE RATING CURVE CID=1 VS NO=1 NO SEGS=1
                      MIN ELEV=0 MAX ELEV=1.3
                      CH SLOPE=0.027 FP SLOPE=0.027
N=0.017 DIST=7.09
                      N=0.017 DIST=7.09

DIST ELEV DIST ELEV

0.0 1.83 2.46 0.0

4.63 0.0 7.09 1.83

ID=1 HYD NO=201A.1.R INFLOW ID=2

DT=0.0 L=450 FT NS=0 SLOPE=0.027
ROUTE MCUNGE
PRINT HYD
                      ID=1 CODE=1
*s
                **** (AP-4: ADD 201A.1.R AND BASIN 202C)
ADD HYD
                ID=2 HYD_NO=AP-4:DPOND.2 ID I=1 ID II=10
PRINT HYD
                        ID=2
                                CODE=5
********************
```

```
**** AP-13
*S
               ID=1    HYD NO=AP-13    DA= 0.0043 SQ MI
PER A=0    PER B=0    PER C=0.0    PER D=100.0
TP=0.133333    MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
               ID=1 CODE=1
ID=3      HYD NO=207      DA= 0.0061 SQ MI
PER A=0      PER B=0      PER C=14.1      PER D=85.9
TP=0.133333      MASSRAIN=-1
COMPUTE NM HYD
               ID=3 CODE=1
PRINT HYD
**************************************
            **** SUB-BASIN 208A **** (AREA=1.9 ACRES)
               ID=4 HYD NO=208A DA= 0.0026448 SQ MI
COMPUTE NM HYD
               PER A=0 PER B=0 PER C=89.69 PER D=10.4
TP=0.133333 MASSRAIN=-1
PRINT HYD
               ID=4 CODE=1
**************************************
ID=5  HYD NO=210  DA= 0.0163 SQ MI
PER A=0  PER B=0  PER C=85.1  PER D=14.9
TP=0.133333  MASSRAIN=-1
COMPUTE NM HYD
               ID=5 CODE=1
PRINT HYD
**** SUB-BASIN 211 **** (AREA=1.6 ACRES)
**** AP-9
*S
               ID=7 HYD NO=AP-9 DA= 0.0025SQ MI
COMPUTE NM HYD
               PER A=0 PER B=0 PER C=33.3 PER D=66.7
TP=0.133333 MASSRAIN=-1
ID=7 CODE=1
PRINT HYD
            **** (AP-6: ADD 210 AND 207)
            ID=10 HYD NO=AP-6 ID I=5 ID II=3 ID=10 CODE=5
ADD HYD
PRINT HYD
            ADD HYD
PRINT HYD
*****************
            **** SUB-BASIN 208B **** (AREA=1.1 ACRES)
********
            **** AP-10
               ID=13 HYD NO=AP-10 DA= 0.0029 SQ MI
PER A=0 PER B=0 PER C=62.1 PER D=37.9
TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
               ID=13 CODE=1
********************
            **** SUB-BASIN 209A **** (AREA=1.1 ACRES)
330-03310 203A (ARCA-1:1 ACRC3)
               ID=4 HYD NO=209A DA= 0.0009 SQ MI
PER A=0 PER B=0 PER C=33.3 PER D=66.7
TP=0.133333 MASSRAIN=-1
ID=4 CODE=1
COMPUTE NM HYD
PRINT HYD
**************************************
ID=10 HYD NO=209B DA= 0.0017 SQ MI PER A=0 PER B=0 PER C=0 PER D=100 TP=0.133333 MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
               ID=10 CODE=1
```

```
ID=11   HYD NO=212   DA= 0.0005 SQ MI
PER A=0   PER B=0   PER C=75 PER D=25
TP=0.13333   MASSRAIN=-1
COMPUTE NM HYD
PRINT HYD
                ID=11 CODE=1
             **** (ADD BASINS 209A AND 209B)
ID=12 HYD NO=DPOND.3 ID I=4 ID II=10
*S
ADD HYD
                    ID=12 CODE=5
PRINT HYD
             **** (ADD BASIN 212 AND DPOND.3) ID=4 HYD NO=DPOND.3.0
*S
                   HYD NO=DPOND.3.0 ID I=11 ID II=12 ID=4 CODE=5
ADD HYD
PRINT HYD
             **** (ADD AP-12 AND AP-4)
*S
ADD HYD
             ID=10`
                   HYD NO=DPOND.N ID I=8 ID II=2
                    ID=10 CODE=5
PRINT HYD
             *S
ADD HYD
PRINT HYD
**** POND ****
**********************
*
             **** AP-1:POND OUTLET
                ID=4 HYD NO=AP-1:POND OUTLET INFLOW=2 CODE=1
OUTFLOW (CFS) STORAGE (AC-FT) ELEV (FT)
0.0 0.0000 56988.58
ROUTE RESERVOIR
                               0.0001
                  4.4
                                             5690
                               0.0001
                                             5691
                  16.2
                               0.0001
                                             5692
                               0.041
                                             5693
                  32.0
                               0.136
                                             5694
                  43.6
                               0.275
                                             5695
                  56.7
                               0.450
                                             5696
                  67.2
                               0.651
                                             5697
                  107.9
177.8
                               0.880
                                             5698
                               1.138
                                             5699
                  191.0
                               1.274
                                             5699.5
PRINT HYD
                  ID=4 CODE=1
FINISH
```

1

RUN DATE (MON/DAY/YR)

AHYMO PROGRAM SUMMARY TABLE (AHYMO-S4) - Ver. S4.01a, Rel: 01a RUN DATE =01/13/2015
INPUT FILE = 2-600-025-00\AE_DATA\CALCS\Hydrology\AHYMO\Resubmittal Calcs_1214\10024P.txt USER NO.= WilsonCoanMsiteA96476897

	COMMAND II	HYDROGRAPH DENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	DISC	EAK CHARGE CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = NOTATION
	*S *S *S *S *S *S *S *S *S *S *S *S *S *	USE THE I FILE: 100 PROPOSED DATE: JAN	HIGH S A/INF 24P.tx CONDIT . 2015	SCHOOL DF METHOD T Kt FIONS S******	RAINAGE ANA TO COMPUTE	THE RUN	****	****				
	*S *S *S *****************************	RAINFALL	FROM N	NOAA ATLA	AS 14, VOLU	JME 1, \	VERSION 5, V				-	ΓIME=
0.00)											I TME=
	LOCATION RAINFALL TYPE=	2 NOAA 14	ALBU	JQUERQUE							F	RAIN24=
3.08	80 *s											
35.3	*S COMPUTE NM HYD	201A	*** SU -	JB-BASIN 1	201A **** 0.00650	(AREA=4	4.2 ACRES) 15.10	0.596	1.71987	1.500	3.630 F	PER IMP=
29.2	*S COMPUTE NM HYD	201B	*** SU -	JB-BASIN 2	201B **** 0.00500	(AREA=	3.2 ACRES) 11.36	0.431	1.61568	1.500	3.551 F	PER IMP=
75.0		201c	-	3	201C **** 0.00140		3.73	0.179	2.39801	1.500	4.168 F	PER IMP=
25.6	*S COMPUTE NM HYD SO	201D	*** SU -	JB-BASIN 4	201D **** 0.00190	(AREA=1	1.2 ACRES) 4.27	0.157	1.55418	1.500	3.511 F	PER IMP=
0.2	ROUTE MCUNGE	201C.SWALE	3	5	0.00140		3.68	0.179	2.39854	1.550	4.104 (CCODE =
	*S ADD HYD ROUTE MCUNGE	201B.1 201B.SWALE		ADD 201C. 6 7	SWALE AND 0.00640 0.00640	201B)	15.03 14.92	0.610 0.610	1.78677 1.78712	1.500 1.550	3.670 3.642 (CCODE =
	*S ADD HYD *S	201D.1	7& 4	8	SWALE AND 0.00830 205A ****	_	19.07	0.767	1.73368	1.500	3.589	
0.0	COMPUTE NM HYD	205A	-	9	0.00570	(ARLA	15.71	0.789	2.59615	1.500	4.307 F	PER IMP=
90.0	*S COMPUTE NM HYD	205в [*]	*** SU -	JB-BASIN 3	205B **** 0.00120	(AREA=0	0.8 ACRES) 3.36	0.170	2.65423	1.500	4.370 F	PER IMP=
	*S ADD HYD *S	205.10		ADD BASIN 6	NS 205A AND 0.00690	205B)	19.07	0.959	2.60616	1.500	4.318	
0.2	ROUTE MCUNGE	205.1R	6	9	0.00690		18.86	0.959	2.60640	1.500	4.270	CCODE =
	*S ADD HYD *S DIVIDE 2010.2 DIVIDE HYD	201D.2	8& 9 CURVE 3	3	1 AND 205 0.01520 INLET 12" 0.00758 0.00762	•	37.92 E TO JT AND 5.43 32.49	1.727 30" OVERF 0.860 0.866	2.12980 2.12980 2.12980	1.500 1.500 1.500	3.898 1.120 6.659	
	*S				202A ****	(AREA=1		0.000	2.12900	1.300	0.033	

**	بالد مالد مالد			10024P.SUM				
*S COMPUTE NM HYD 0.00		* AP-11 - 9	0.00210	4.26	0.125	1.11690	1.500	3.167 PER IMP=
*S COMPUTE NM HYD	*** 202B	* SUB-BAS	SIN 202B **** 0.00190	(AREA=1.2 ACRES) 3.85	0.113	1.11690	1.500	3.168 PER IMP=
0.00 *S	***	* SUB-BAS	SIN 202C ****	(AREA=0.7 ACRES)				
ç COMMAND I	HYDROGRAPH	ROM TO ID ID NO. NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PAGE = 2 PER ACRE NOTATION
COMPUTE NM HYD	202C	- 10	0.00100	2.11	0.067	1.25355	1.500	3.291 PER IMP=
*S COMPUTE NM HYD 99.00	203.00	* SUB-BAS - 11	SIN 203 **** 0.00630	(AREA=4.0 ACRES) 18.02	0.943	2.80796	1.500	4.470 PER IMP=
ROUTE RESERVOIR 0.022	WQ.POND	11 12	0.00630	17.58	0.943	2.80791	1.550	4.361 AC-FT=
*S COMPUTE NM HYD 86.70	204.00	- 11	0.01300		1.801	2.59786	1.500	4.231 PER IMP=
*S ADD HYD	AP-2 11	.&12 13	0.01930	AND BASIN 204) 52.66	2.745	2.66641	1.500	4.263
*S ROUTE MCUNGE 0.0	AP-2.R	** ROUTE A 13 11	AP-2 0.01930	52.66	2.745	2.66641	1.500	4.263 CCODE =
*S ADD HYD *S	AP-3 11	. & 3 12	ADD AP-2.R A 0.02120 P-3 AND BASIN		2.858	2.52753	1.500	4.165
ADD HYD *S	201A.1 12		0.02770		3.454	2.33800	1.500	4.040
ROUTE MCUNGE	201A.1.R	2 1	0.02770	71.62	3.454	2.33800	1.500	4.040 CCODE =
*S ADD HYD *S *S	AP-4:DPOND.2 1	.&10 2	0.02870	AND BASIN 202C) 73.72 (AREA=2.8 ACRES)	3.521	2.30008	1.500	4.014
COMPUTE NM HYD		- 1	0.00430	12.34	0.648	2.82504	1.500	4.482 PER IMP=
*S COMPUTE NM HYD 85.90		* SUB-BAS	SIN 207 **** 0.00610	(AREA=3.9 ACRES) 16.78	0.841	2.58419	1.500	4.298 PER IMP=
*S COMPUTE NM HYD 10.39	*** 208A	* SUB-BAS - 4	5IN 208A **** 0.00264	(AREA=1.9 ACRES) 5.60	0.183	1.29439	1.500	3.308 PER IMP=
*S COMPUTE NM HYD 14.90		* SUB-BAS - 5	SIN 210 **** 0.01630	(AREA=10.4 ACRES) 35.04	1.192	1.37141	1.500	3.359 PER IMP=
*S *S *S	***	* AP-9		(AREA=1.6 ACRES)	0.201	2 25622	1 500	4 050
COMPUTE NM HYD 66.70	AP-9	,	0.00250		0.301	2.25623	1.500	4.050 PER IMP=
*S ADD HYD *S	AP-6 5	6& 3 10	ADD 210 AND 0.02240 ADD AP-6 AND	51.82	2.033	1.70165	1.500	3.614
ADD HYD *S	AP-7 10 ***)& 4 3 ** SUB-BAS	0.02504		2.215	1.65864	1.500	3.582
*S COMPUTE NM HYD 37.90	AP-10	* AP-10 - 13	0.00290	6.81	0.273	1.76429	1.500	3.669 PER IMP=
*S COMPUTE NM HYD		* SUB-BAS - 4	SIN 209A **** 0.00090	(AREA=1.1 ACRES) 2.34	0.108	2.25623	1.500	4.068 PER IMP=
				Page 2				

66.70										
*S	*	*** Sl	JB-BASIN	209B **** ((AREA=1.1 ACRES)					
COMPUTE NM HY	D 209B	-	10	0.00170	4.88	0.256	2.82504	1.500	4.487 P	ER IMP=
100.00										
*S	*	*** SU	JB-BASIN	212 **** (A	REA=0.3 ACRES)					
COMPUTE NM HY	D 212.00	-	11	0.00050	1.13	0.041	1.54393	1.500	3.537 P	ER IMP=
25.00										
*S	*	*** (A	NDD BASI	NS 209A AND	209в)					
ADD HYD	DPOND.3			0.00260	7.22	0.364	2.62790	1.500	4.342	
*S			NDD BASI	N 212 AND DP						
ADD HYD	DPOND.3.0		4	0.00310	8.36	0.406	2.45301	1.500	4.212	
*S				2 AND AP-4)						
ADD HYD	DPOND.N			0.03632	106.21	4.387	2.26434	1.500	4.569	
*S					AND DPOND.N)					
ADD HYD		4&10	2	0.03942	114.57	4.792	2.27918	1.500	4.541	
*S	*	*** PC	ND ****							
4										_
		FROM	TO		PEAK	RUNOFF		TIME TO	CFS	PAGE = 3
	HYDROGRAPH	ID	ID	AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER	
COMMAND	IDENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATION
*S		***_AF	-1:POND							
ROUTE RESERVO	IR AP-1:POND	2	4	0.03942	88.93	4.802	2.28384	1.600	3.524 A	C-FT=
0.773										
FINISH										



NOAA Atlas 14, Volume 1, Version 5 Location name: Albuquerque, New Mexico, US* Latitude: 35.1286°, Longitude: -106.5108° Elevation: 5751 ft* * source: Google Maps



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PI	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹										
Duration				Avera	ige recurren	ce interval (y	years)				
Duration	1	2	5	10	25	50	100	200	500	1000	
5-min	0.181 (0.153-0.214)	0.234 (0.198-0.278)	0.314 (0.265-0.373)	0.376 (0.316-0.444)	0.460 (0.385-0.544)	0.526 (0.439-0.621)	0.595 (0.493-0.702)	0.667 (0.550-0.787)	0.766 (0.625-0.903)	0.844 (0.685-0.996)	
10-min	0.276 (0.233-0.326)	0.357 (0.301–0.423)	0.479 (0.404-0.567)	0.572 (0.481-0.677)	0.700 (0.587–0.828)	0.800 (0.668-0.945)	0.906 (0.750-1.07)	1.02 (0.836-1.20)	1.17 (0.951–1.37)	1.29 (1.04–1.52)	
15-min	0.342 (0.289-0.404)	0.442 (0.373-0.524)	0.593 (0.500-0.703)	0.709 (0.596-0.838)	0.868 (0.727-1.03)	0.992 (0.828-1.17)	1.12 (0.930–1.33)	1.26 (1.04–1.49)	1.45 (1.18–1.70)	1.59 (1.29–1.88)	
30-min	0.461 (0.390-0.544)	0.596 (0.503-0.705)	0.799 (0.674-0.947)	0.955 (0.803-1.13)	1.17 (0.980-1.38)	1.34 (1.12–1.58)	1.51 (1.25–1.78)	1.70 (1.40–2.00)	1.95 (1.59–2.30)	2.15 (1.74-2.53)	
60-min	0.570 (0.482-0.673)	0.737 (0.622-0.873)	0.989 (0.834-1.17)	1.18 (0.993–1.40)	1.45 (1.21–1.71)	1.65 (1.38–1.95)	1.87 (1.55–2.21)	2.10 (1.73–2.47)	2.41 (1.96-2.84)	2.66 (2.15–3.13)	
2-hr	0.687 (0.568-0.848)	0.880 (0.728-1.09)	1.16 (0.960–1.44)	1.39 (1.14–1.71)	1.70 (1.39–2.09)	1.96 (1.59–2.39)	2.22 (1.79–2.71)	2.50 (2.00-3.04)	2.89 (2.29-3.52)	3.20 (2.52–3.91)	
3-hr	0.734 (0.612-0.901)	0.933 (0.775-1.15)	1.22 (1.02-1.49)	1.45 (1.20–1.77)	1.77 (1.45–2.16)	2.02 (1.66-2.47)	2.30 (1.87-2.79)	2.58 (2.08-3.14)	2.98 (2.38–3.61)	3.31 (2.62–4.01)	
6-hr	0.856 (0.720-1.05)	1.08 (0.909–1.32)	1.39 (1.17–1.69)	1.64 (1.37–1.99)	1.97 (1.64-2.39)	2.23 (1.85–2.70)	2.51 (2.07–3.04)	2.79 (2.29–3.37)	3.19 (2.59–3.84)	3.50 (2.83-4.23)	
12-hr	0.969 (0.829-1.14)	1.22 (1.04–1.44)	1.55 (1.32–1.82)	1.81 (1.54–2.12)	2.15 (1.82-2.53)	2.42 (2.04–2.84)	2.71 (2.27–3.17)	2.99 (2.49–3.51)	3.38 (2.80-3.97)	3.70 (3.03-4.34)	
24-hr	1.13 (0.984–1.31)	1.42 (1.23–1.64)	1.78 (1.55–2.06)	2.07 (1.80-2.40)	2.46 (2.12–2.85)	2.76 (2.38–3.20)	3.08 (2.64-3.56)	3.40 (2.90-3.93)	3.84 (3.25-4.43)	4.18 (3.52-4.84)	
2-day	1.22 (1.06–1.40)	1.53 (1.34–1.76)	1.93 (1.69–2.22)	2.25 (1.96–2.58)	2.68 (2.33–3.07)	3.02 (2.61–3.45)	3.37 (2.90–3.86)	3.73 (3.19–4.27)	4.21 (3.58–4.84)	4.60 (3.88-5.29)	
3-day	1.36 (1.21–1.52)	1.70 (1.52–1.90)	2.12 (1.89–2.37)	2.45 (2.19–2.74)	2.91 (2.58-3.25)	3.26 (2.89–3.64)	3.62 (3.19–4.04)	3.99 (3.50-4.46)	4.48 (3.91–5.02)	4.87 (4.23–5.47)	
4-day	1.49 (1.36–1.63)	1.86 (1.70–2.04)	2.30 (2.10-2.52)	2.65 (2.42–2.90)	3.13 (2.84-3.42)	3.50 (3.17–3.82)	3.87 (3.49–4.23)	4.25 (3.82-4.64)	4.75 (4.25–5.21)	5.14 (4.57–5.64)	
7-day	1.73 (1.59–1.89)	2.16 (1.98–2.36)	2.66 (2.43–2.90)	3.04 (2.78-3.32)	3.56 (3.25–3.88)	3.96 (3.60-4.31)	4.36 (3.95–4.75)	4.76 (4.30–5.19)	5.28 (4.75-5.77)	5.68 (5.08-6.22)	
10-day	1.94 (1.79–2.11)	2.42 (2.23–2.64)	2.99 (2.75–3.25)	3.44 (3.16-3.74)	4.04 (3.70-4.39)	4.50 (4.10–4.89)	4.97 (4.51–5.40)	5.43 (4.92–5.91)	6.05 (5.45-6.60)	6.52 (5.85–7.12)	
20-day	2.54 (2.33–2.76)	3.16 (2.90-3.45)	3.86 (3.55-4.21)	4.40 (4.03-4.79)	5.09 (4.65-5.54)	5.60 (5.11–6.09)	6.10 (5.55-6.63)	6.58 (5.97–7.16)	7.21 (6.51–7.86)	7.66 (6.90-8.37)	
30-day	3.08 (2.83-3.34)	3.84 (3.52-4.17)	4.66 (4.27–5.05)	5.27 (4.82-5.72)	6.05 (5.53-6.56)	6.61 (6.03-7.17)	7.16 (6.52–7.77)	7.69 (6.98-8.34)	8.35 (7.55-9.07)	8.83 (7.96–9.61)	
45-day	3.77 (3.47-4.08)	4.68 (4.32–5.07)	5.62 (5.17-6.09)	6.30 (5.79–6.83)	7.15 (6.56–7.76)	7.76 (7.10–8.42)	8.33 (7.61–9.04)	8.87 (8.09-9.64)	9.54 (8.66–10.4)	10.0 (9.06–10.9)	
60-day	4.34 (4.00-4.70)	5.39 (4.97–5.85)	6.48 (5.97–7.02)	7.26 (6.69–7.87)	8.22 (7.56-8.92)	8.89 (8.17-9.65)	9.53 (8.74–10.4)	10.1 (9.27-11.0)	10.9 (9.91–11.8)	11.4 (10.4–12.4)	

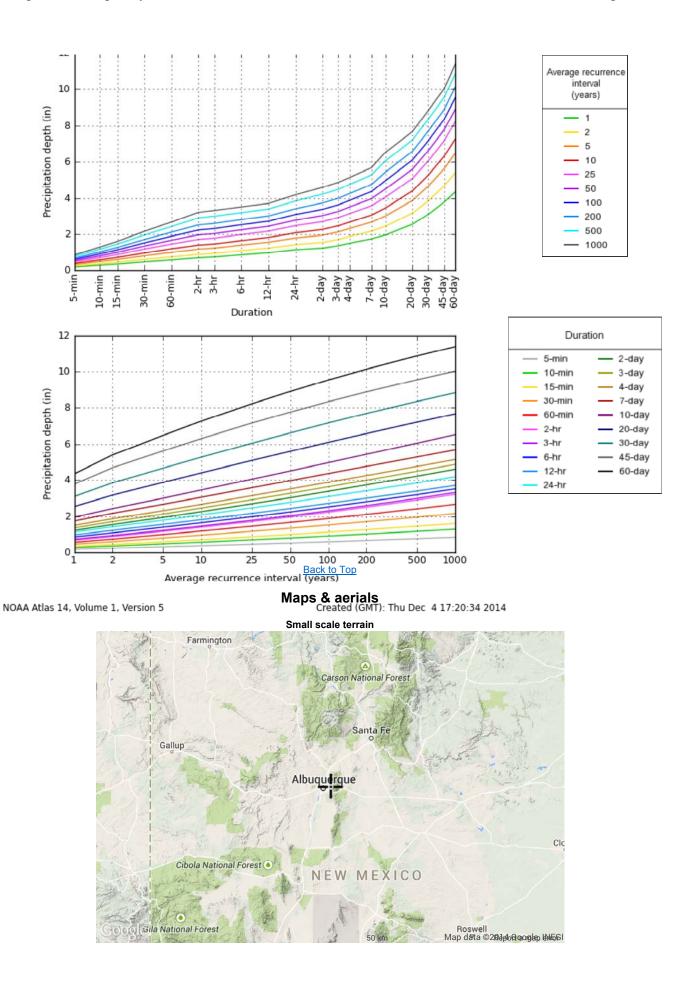
Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

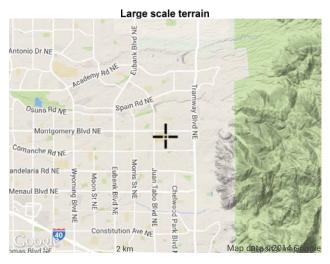
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

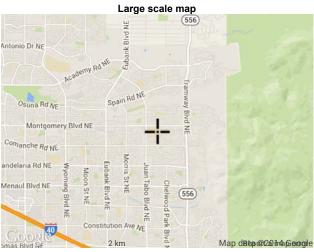
Please refer to NOAA Atlas 14 document for more information.

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PF graphical









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<u>US Department of Commerce</u> <u>National Oceanic and Atmospheric Administration</u> National Weather Service Office of Hydrologic Development 1325 East West Highway Silver Spring, MD 20910

Questions?: HDSC.Questions@noaa.gov

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APPENDIX C



Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants Custom Soil Resource
Report for
Bernalillo County and Parts
of Sandoval and Valencia
Counties, New Mexico
Eldorado HS



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://soils.usda.gov/sqi/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (http://offices.sc.egov.usda.gov/locator/app? agency=nrcs) or your NRCS State Soil Scientist (http://soils.usda.gov/contact/state_offices/).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Soil Data Mart Web site or the NRCS Web Soil Survey. The Soil Data Mart is the data storage site for the official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil scientists classified and named the soils in the survey area, they compared the

individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Units

Special Point Features

 \odot Blowout

Borrow Pit \bowtie

Clay Spot

Closed Depression

Gravel Pit ×

Gravelly Spot

Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water ⊚

Perennial Water

Rock Outcrop

Saline Spot

Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

E Spoil Area

Stony Spot

Very Stony Spot



Wet Spot

Other

Special Line Features

2

Gully

Short Steep Slope

11 Other

Political Features

Cities

Water Features

Streams and Canals

Transportation



Interstate Highways



US Routes



Major Roads



Local Roads

MAP INFORMATION

Map Scale: 1:6,410 if printed on A size (8.5" × 11") sheet.

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for accurate map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL: http://websoilsurvey.nrcs.usda.gov Coordinate System: UTM Zone 13N NAD83

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Bernalillo County and Parts of Sandoval and

Valencia Counties, New Mexico Survey Area Data: Version 9, Dec 9, 2008

Date(s) aerial images were photographed: Data not available.

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Bernalillo County and Parts of Sandoval and Valencia Counties, New Mexico (NM600)			
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
EmB	Embudo gravelly fine sandy loam, 0 to 5 percent slopes	37.8	24.6%
EtC	Embudo-Tijeras complex, 0 to 9 percent slopes	70.4	45.7%
ТдВ	Tijeras gravelly fine sandy loam, 1 to 5 percent slopes	45.8	29.7%
Totals for Area of Interest		154.0	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments

on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Bernalillo County and Parts of Sandoval and Valencia Counties, New Mexico

EmB—Embudo gravelly fine sandy loam, 0 to 5 percent slopes

Map Unit Setting

Landscape: Valleys

Elevation: 4,850 to 6,500 feet

Mean annual precipitation: 7 to 10 inches

Mean annual air temperature: 58 to 60 degrees F

Frost-free period: 170 to 195 days

Map Unit Composition

Embudo and similar soils: 85 percent

Description of Embudo

Setting

Landform: Terraces

Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Alluvium derived from igneous and sedimentary rock

Properties and qualities

Slope: 0 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: Rare Frequency of ponding: None

Calcium carbonate, maximum content: 5 percent Maximum salinity: Nonsaline (0.0 to 2.0 mmhos/cm)

Sodium adsorption ratio, maximum: 2.0

Available water capacity: Low (about 3.4 inches)

Interpretive groups

Farmland classification: Not prime farmland

Land capability (nonirrigated): 7e

Hydrologic Soil Group: B

Ecological site: Sandy (R042XA051NM)

Typical profile

0 to 4 inches: Gravelly fine sandy loam 4 to 20 inches: Gravelly sandy loam

20 to 60 inches: Stratified very gravelly loamy coarse sand to extremely gravelly

loamy sand

EtC—Embudo-Tijeras complex, 0 to 9 percent slopes

Map Unit Setting

Landscape: Uplands, valleys Elevation: 4,850 to 6,500 feet

Mean annual precipitation: 7 to 10 inches Mean annual air temperature: 58 to 60 degrees F

Frost-free period: 170 to 195 days

Map Unit Composition

Embudo and similar soils: 50 percent Tijeras and similar soils: 35 percent

Description of Embudo

Setting

Landform: Terraces

Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Alluvium derived from igneous and sedimentary rock

Properties and qualities

Slope: 0 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: Rare Frequency of ponding: None

Calcium carbonate, maximum content: 7 percent Maximum salinity: Nonsaline (0.0 to 2.0 mmhos/cm)

Sodium adsorption ratio, maximum: 2.0

Available water capacity: Low (about 3.4 inches)

Interpretive groups

Farmland classification: Not prime farmland

Land capability (nonirrigated): 7e

Hydrologic Soil Group: B

Ecological site: Sandy (R042XA051NM)

Typical profile

0 to 4 inches: Gravelly fine sandy loam 4 to 20 inches: Gravelly sandy loam

20 to 60 inches: Stratified gravelly loamy coarse sand to very gravelly loamy sand

Description of Tijeras

Setting

Landform: Fan remnants
Down-slope shape: Linear
Across-slope shape: Linear

Parent material: Alluvium derived from igneous and sedimentary rock

Properties and qualities

Slope: 1 to 9 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 2.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 5 percent Maximum salinity: Nonsaline (0.0 to 2.0 mmhos/cm)

Sodium adsorption ratio, maximum: 2.0

Available water capacity: Low (about 5.2 inches)

Interpretive groups

Farmland classification: Not prime farmland

Land capability (nonirrigated): 7c

Hydrologic Soil Group: B

Ecological site: Sandy (R042XA051NM)

Typical profile

0 to 4 inches: Gravelly fine sandy loam 4 to 14 inches: Sandy clay loam 14 to 19 inches: Gravelly sandy loam

19 to 60 inches: Stratified very gravelly sand to very gravelly sandy loam

TgB—Tijeras gravelly fine sandy loam, 1 to 5 percent slopes

Map Unit Setting

Landscape: Uplands

Elevation: 5,000 to 6,500 feet

Mean annual precipitation: 7 to 10 inches

Mean annual air temperature: 58 to 60 degrees F

Frost-free period: 170 to 195 days

Map Unit Composition

Tijeras and similar soils: 80 percent

Description of Tijeras

Setting

Landform: Fan remnants, alluvial fans Landform position (three-dimensional): Rise

Down-slope shape: Convex, linear Across-slope shape: Convex, linear

Parent material: Alluvium derived from igneous and sedimentary rock

Properties and qualities

Slope: 1 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 2.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 10 percent Maximum salinity: Nonsaline (0.0 to 2.0 mmhos/cm)

Sodium adsorption ratio, maximum: 2.0

Available water capacity: Low (about 5.8 inches)

Interpretive groups

Farmland classification: Not prime farmland

Land capability (nonirrigated): 7c

Hydrologic Soil Group: B

Ecological site: Sandy (R042XA051NM)

Typical profile

0 to 6 inches: Gravelly fine sandy loam 6 to 19 inches: Sandy clay loam 19 to 60 inches: Gravelly sandy loam

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