

HCI ENGINEERING

A division of
HABERER CARPENTRY INC.

February 22, 2017

Attn: City of Albuquerque, Hydrology Department
600 2nd Street NW
Albuquerque, NM 87102

Re: 15_39 Taco Bell at Heritage Marketplace (Project File: H09D026) Drainage Calculations

To whom it may concern,

Please see the attached drainage calculations. These calculations were used to determine the runoff values for the existing and proposed site, required and proposed pond storage volumes, design the outlet structures and size the associated storm pipes. Please see below for a list of the included documents.

Sincerely,

Lance VanDemark, PE 21777
The Vertex Companies, Inc.

Attachments:

DPM Weighted E Method
Pond Volume Calculations
Water Quality (First Flush) Basin Volume Calculations
Pond 1 Outlet Structure – Water Quality Capture Volume Orifice Plate Design
Pond 1 Outlet Structure – Restrictor Plate Sizing
Pond 1 Outlet Structure – Weir and Orifice Design
Pond 2 Outlet Structure – Water Quality Capture Volume Orifice Plate Design
Pond 2 Outlet Structure – Restrictor Plate Sizing
Pond 2 Outlet Structure – Weir and Orifice Design
12" Dia. Pipe Sizing
18" Dia. Pipe Sizing

Basin Descriptions															100-Year, 6-Hour			10-Year, 6-Hour			2-Year, 6-Hour		
Basin	Area (sf)	Area (acres)	Treatment A			Treatment B			Treatment C			Treatment D			Weighted E (ac-ft)	Volume (ac-ft)	Flow cfs	Weighted E (ac-ft)	Volume (ac-ft)	Flow cfs	Weighted E (ac-ft)	Volume (ac-ft)	Flow cfs
			(sf)	(acres)	%	(sf)	(acres)	%	(sf)	(acres)	%	(sf)	(acres)	%									
B2-A	17083	0.392	0	0	0%	0	0	0%	3765	0.086	22%	13318	0.306	78%	1.754	0.057	1.584	1.064	0.035	1.012	0.175	0.006	0.557
B2-B	2454	0.056	0	0	0%	0	0	0%	1660	0.038	68%	794	0.018	32%	1.307	0.006	0.189	0.699	0.023	0.109	0.112	0.004	0.049
B2-C	3568	0.082	0	0	0%	0	0	0%	1393	0.032	39%	2175	0.050	61%	1.587	0.011	0.310	0.928	0.030	0.192	0.152	0.005	0.099
B2-D	11300	0.259	0	0	0%	0	0	0%	1506	0.035	13%	9794	0.225	87%	1.839	0.040	1.082	1.133	0.037	0.701	0.187	0.006	0.396
B2-E	2440	0.056	0	0	0%	0	0	0%	817	0.019	33%	1623	0.037	67%	1.642	0.008	0.217	0.972	0.032	0.136	0.160	0.005	0.072
B2-F	1526	0.035	0	0	0%	0	0	0%	1526	0.035	100%	0	0.000	0%	0.990	0.003	0.101	0.440	0.014	0.052	0.064	0.002	0.016
OS-1	8659	0.199	0	0	0%	0	0	0%	0	0.000	0%	8659	0.199	100%	1.970	0.033	0.869	1.240	0.041	0.574	0.205	0.007	0.336
TOTAL	38371	0.881	0	0	0%	0	0	0%	10667	0.245	28%	27704	0.636	72%	1.698	0.125	3.482	1.018	0.033	2.203	0.168	0.005	1.190
EXISTING	38371	0.881	0	0	0%	0	0	0%	38371	0.881	100%	0	0.000	0%	0.990	0.073	2.528	0.440	0.014	1.313	0.064	0.002	0.414

Zone 1 - Excess Precipitation, E (inches) 6-Hour Storm

Treatment	100-Yr	10-Yr	2-Yr
A	0.44	0.08	0
B	0.67	0.22	0.01
C	0.99	0.44	0.12
D	1.97	1.24	0.72

Zone 1 - Peak Discharge (CFS/Acre)

Treatment	100-Yr	10-Yr	2-Yr
A	1.29	0.24	0
B	2.03	0.76	0.03
C	2.87	1.49	0.47
D	4.37	2.89	1.69

Equations

Weighted E = Ea*Aa + Eb*Ab + Ec*Ac + Ed*Ad / (Aa + Ab + Ac + Ad)

Volume = Weighted E * (Aa + Ab + Ac + Ad)

Flow = Qa*Aa + Qb*Ab + Qc*Ac + Qd*Ad

Basin	First Flush Volume (cf)
B2-A	377
B2-B	22
B2-C	62
B2-D	277
B2-E	46
B2-F	0
Total Req'd	785

First Flush Volume =
(0.44"-0.1")*Type D Area

Pond 1 Volume Calculations				
Elevation (feet)	Area (sf)	Cumulative Vol. (cf)	Cumulative Vol. (acre-ft)	Retained 1st Flush Vol. (cf)
5174.00	22	11	0.000	
5174.25	49	20	0.000	
5174.50	80	36	0.001	
5174.75	130	61	0.001	
5175.00	187	101	0.002	
5175.25	250	157	0.004	
5175.50	320	228	0.005	
5175.75	396	318	0.007	318
5176.00	476	427	0.010	
5176.25	559	556	0.013	
5176.50	649	707	0.016	
5176.75	743	881	0.020	
5177.00	834	1078	0.025	
5177.25	917	1297	0.030	
5177.50	996	1536	0.035	
5177.75	1073	1795	0.041	Minor 2-yr WSEL
5178.00	1143	2072	0.048	5178.10
5178.25	1208	2366	0.054	
5178.50	1275	2676	0.061	Major 100-yr WSEL
5178.75	1366	3006	0.069	5178.93
5179.00	1385	3350	0.077	
5179.25	1430	3702	0.085	

Pond 2 Volume Calculations				
Elevation (feet)	Area (sf)	Cumulative Vol. (cf)	Cumulative Vol. (acre-ft)	Retained 1st Flush Vol. (cf)
5173.00	109	21	0.000	
5173.25	287	69	0.002	
5173.50	450	160	0.004	
5173.75	532	281	0.006	281
5174.00	570	419	0.010	
5174.25	594	570	0.013	
5174.50	618	721	0.017	
5174.75	642	879	0.020	
5175.00	665	1042	0.024	
5175.25	688	1211	0.028	
5175.50	710	1386	0.032	
5175.75	731	1566	0.036	
5176.00	752	1752	0.040	Minor 2-yr WSEL
5176.25	772	1942	0.045	5176.39
5176.50	792	2138	0.049	Major 100-yr WSEL
5176.75	811	2338	0.054	5176.63
5177.00	830	2543	0.058	

Water Quality Basin B2-B Volume Calculations				
Elevation (feet)	Area (sf)	Cumulative Vol. (cf)	Cumulative Vol. (acre-ft)	Retained 1st Flush Vol. (cf)
5179.75	342	46	0.001	
5180.00	498	149	0.003	149

Water Quality Basin B2-C Volume Calculations				
Elevation (feet)	Area (sf)	Cumulative Vol. (cf)	Cumulative Vol. (acre-ft)	Retained 1st Flush Vol. (cf)
5181.00	166	28	0.001	
5181.25	365	92	0.002	92

Total Pond Volume	
6245 sf	0.143 acre-ft

Total Retention Volume	
840 > 785 Req'd	

DETENTION VOLUME BY THE MODIFIED FAA METHOD

Project: 15_39 Taco Bell Heritage

Basin ID: Pond 1

(For catchments less than 160 acres only. For larger catchments, use hydrograph routing method)
(NOTE: for catchments larger than 90 acres, CUHP hydrograph and routing are recommended)

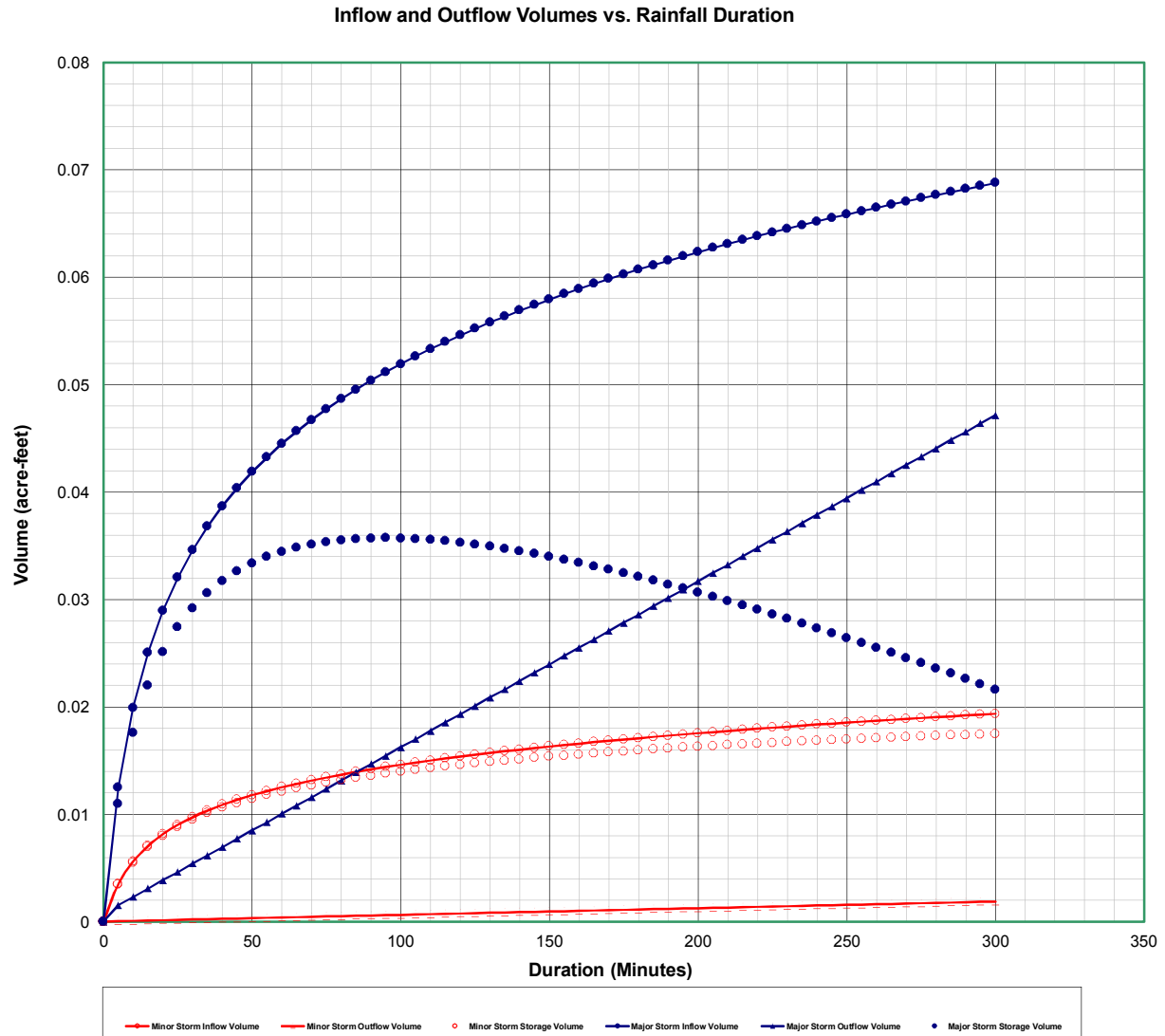
Determination of MINOR Detention Volume Using Modified FAA Method							Determination of MAJOR Detention Volume Using Modified FAA Method						
Design Information (Input): Catchment Drainage Imperviousness $I_p = 74.95$ percent Catchment Drainage Area $A = 0.449$ acres Predevelopment NRCS Soil Group Type = A A, B, C, or D Return Period for Detention Control $T = 2$ years (2, 5, 10, 25, 50, or 100) Time of Concentration of Watershed $T_c = 5$ minutes Allowable Unit Release Rate $q = 0.02$ cfs/acre One-hour Precipitation $P_1 = 0.72$ inches Design Rainfall IDF Formula $i = C_1 \cdot P_1 / (C_2 + T_c)^{C_3}$ Coefficient One $C_1 = 28.50$ Coefficient Two $C_2 = 10$ Coefficient Three $C_3 = 0.789$							Design Information (Input): Catchment Drainage Imperviousness $I_p = 74.95$ percent Catchment Drainage Area $A = 0.449$ acres Predevelopment NRCS Soil Group Type = A A, B, C, or D Return Period for Detention Control $T = 100$ years (2, 5, 10, 25, 50, or 100) Time of Concentration of Watershed $T_c = 5$ minutes Allowable Unit Release Rate $q = 0.50$ cfs/acre One-hour Precipitation $P_1 = 1.97$ inches Design Rainfall IDF Formula $i = C_1 \cdot P_1 / (C_2 + T_c)^{C_3}$ Coefficient One $C_1 = 28.50$ Coefficient Two $C_2 = 10$ Coefficient Three $C_3 = 0.789$						
Determination of Average Outflow from the Basin (Calculated): Runoff Coefficient $C = 0.47$ Inflow Peak Runoff $Q_{p-in} = 0.51$ cfs Allowable Peak Outflow Rate $Q_{p-out} = 0.01$ cfs Mod. FAA Minor Storage Volume = 761 cubic feet Mod. FAA Minor Storage Volume = 0.017 acre-ft							Determination of Average Outflow from the Basin (Calculated): Runoff Coefficient $C = 0.61$ Inflow Peak Runoff $Q_{p-in} = 1.82$ cfs Allowable Peak Outflow Rate $Q_{p-out} = 0.22$ cfs Mod. FAA Major Storage Volume = 1,555 cubic feet Mod. FAA Major Storage Volume = 0.036 acre-ft						
5 <- Enter Rainfall Duration Incremental Increase Value Here (e.g. 5 for 5-Minutes)													
Rainfall Duration minutes (input)	Rainfall Intensity inches / hr (output)	Inflow Volume acre-feet (output)	Adjustment Factor "m" (output)	Average Outflow cfs (output)	Outflow Volume acre-feet (output)	Storage Volume acre-feet (output)	Rainfall Duration minutes (input)	Rainfall Intensity inches / hr (output)	Inflow Volume acre-feet (output)	Adjustment Factor "m" (output)	Average Outflow cfs (output)	Outflow Volume acre-feet (output)	Storage Volume acre-feet (output)
0	0.00	0.000	0.00	0.00	0.000	0.000	0	0.00	0.000	0.00	0.00	0.000	0.000
5	2.42	0.004	1.00	0.01	0.000	0.003	5	6.63	0.013	1.00	0.22	0.002	0.011
10	1.93	0.006	0.75	0.01	0.000	0.006	10	5.28	0.020	0.75	0.17	0.002	0.018
15	1.62	0.007	0.67	0.01	0.000	0.007	15	4.43	0.025	0.67	0.15	0.003	0.022
20	1.40	0.008	0.63	0.01	0.000	0.008	20	3.84	0.029	0.63	0.14	0.004	0.025
25	1.24	0.009	0.60	0.01	0.000	0.009	25	3.40	0.032	0.60	0.13	0.005	0.027
30	1.12	0.010	0.58	0.01	0.000	0.010	30	3.06	0.035	0.58	0.13	0.005	0.029
35	1.02	0.010	0.57	0.01	0.000	0.010	35	2.79	0.037	0.57	0.13	0.006	0.031
40	0.94	0.011	0.56	0.01	0.000	0.011	40	2.56	0.039	0.56	0.13	0.007	0.032
45	0.87	0.011	0.56	0.00	0.000	0.011	45	2.38	0.040	0.56	0.12	0.008	0.033
50	0.81	0.012	0.55	0.00	0.000	0.011	50	2.22	0.042	0.55	0.12	0.009	0.033
55	0.76	0.012	0.55	0.00	0.000	0.012	55	2.08	0.043	0.55	0.12	0.009	0.034
60	0.72	0.013	0.54	0.00	0.000	0.012	60	1.97	0.044	0.54	0.12	0.010	0.034
65	0.68	0.013	0.54	0.00	0.000	0.012	65	1.86	0.046	0.54	0.12	0.011	0.035
70	0.65	0.013	0.54	0.00	0.000	0.013	70	1.77	0.047	0.54	0.12	0.012	0.035
75	0.62	0.013	0.53	0.00	0.000	0.013	75	1.69	0.048	0.53	0.12	0.012	0.035
80	0.59	0.014	0.53	0.00	0.001	0.013	80	1.61	0.049	0.53	0.12	0.013	0.036
85	0.56	0.014	0.53	0.00	0.001	0.013	85	1.54	0.050	0.53	0.12	0.014	0.036
90	0.54	0.014	0.53	0.00	0.001	0.014	90	1.48	0.050	0.53	0.12	0.015	0.036
95	0.52	0.014	0.53	0.00	0.001	0.014	95	1.43	0.051	0.53	0.12	0.015	0.036
100	0.50	0.015	0.53	0.00	0.001	0.014	100	1.38	0.052	0.53	0.12	0.016	0.036
105	0.49	0.015	0.52	0.00	0.001	0.014	105	1.33	0.053	0.52	0.12	0.017	0.036
110	0.47	0.015	0.52	0.00	0.001	0.014	110	1.28	0.053	0.52	0.12	0.018	0.036
115	0.45	0.015	0.52	0.00	0.001	0.014	115	1.24	0.054	0.52	0.12	0.019	0.035
120	0.44	0.015	0.52	0.00	0.001	0.015	120	1.21	0.055	0.52	0.12	0.019	0.035
125	0.43	0.016	0.52	0.00	0.001	0.015	125	1.17	0.055	0.52	0.12	0.020	0.035
130	0.42	0.016	0.52	0.00	0.001	0.015	130	1.14	0.056	0.52	0.12	0.021	0.035
135	0.40	0.016	0.52	0.00	0.001	0.015	135	1.11	0.056	0.52	0.12	0.022	0.035
140	0.39	0.016	0.52	0.00	0.001	0.015	140	1.08	0.057	0.52	0.12	0.022	0.034
145	0.38	0.016	0.52	0.00	0.001	0.015	145	1.05	0.057	0.52	0.12	0.023	0.034
150	0.37	0.016	0.52	0.00	0.001	0.015	150	1.02	0.058	0.52	0.12	0.024	0.034
155	0.37	0.016	0.52	0.00	0.001	0.015	155	1.00	0.058	0.52	0.12	0.025	0.034
160	0.36	0.017	0.52	0.00	0.001	0.016	160	0.98	0.059	0.52	0.12	0.026	0.033
165	0.35	0.017	0.52	0.00	0.001	0.016	165	0.95	0.059	0.52	0.12	0.026	0.033
170	0.34	0.017	0.51	0.00	0.001	0.016	170	0.93	0.060	0.51	0.12	0.027	0.033
175	0.33	0.017	0.51	0.00	0.001	0.016	175	0.91	0.060	0.51	0.12	0.028	0.032
180	0.33	0.017	0.51	0.00	0.001	0.016	180	0.89	0.061	0.51	0.12	0.029	0.032
185	0.32	0.017	0.51	0.00	0.001	0.016	185	0.88	0.061	0.51	0.12	0.029	0.032
190	0.31	0.017	0.51	0.00	0.001	0.016	190	0.86	0.062	0.51	0.12	0.030	0.031
195	0.31	0.017	0.51	0.00	0.001	0.016	195	0.84	0.062	0.51	0.12	0.031	0.031
200	0.30	0.018	0.51	0.00	0.001	0.016	200	0.83	0.062	0.51	0.12	0.032	0.031
205	0.30	0.018	0.51	0.00	0.001	0.016	205	0.81	0.063	0.51	0.11	0.032	0.030
210	0.29	0.018	0.51	0.00	0.001	0.016	210	0.80	0.063	0.51	0.11	0.033	0.030
215	0.29	0.018	0.51	0.00	0.001	0.017	215	0.78	0.063	0.51	0.11	0.034	0.029
220	0.28	0.018	0.51	0.00	0.001	0.017	220	0.77	0.064	0.51	0.11	0.035	0.029
225	0.28	0.018	0.51	0.00	0.001	0.017	225	0.76	0.064	0.51	0.11	0.036	0.029
230	0.27	0.018	0.51	0.00	0.001	0.017	230	0.74	0.065	0.51	0.11	0.036	0.028
235	0.27	0.018	0.51	0.00	0.001	0.017	235	0.73	0.065	0.51	0.11	0.037	0.028
240	0.26	0.018	0.51	0.00	0.002	0.017	240	0.72	0.065	0.51	0.11	0.038	0.027
245	0.26	0.018	0.51	0.00	0.002	0.017	245	0.71	0.066	0.51	0.11	0.039	0.027
250	0.26	0.019	0.51	0.00	0.002	0.017	250	0.70	0.066	0.51	0.11	0.039	0.026
255	0.25	0.019	0.51	0.00	0.002	0.017	255	0.69	0.066	0.51	0.11	0.040	0.026
260	0.25	0.019	0.51	0.00	0.002	0.017	260	0.68	0.066	0.51	0.11	0.041	0.025
265	0.24	0.019	0.51	0.00	0.002	0.017	265	0.67	0.067	0.51	0.11	0.042	0.025
270	0.24	0.019	0.51	0.00	0.002	0.017	270	0.66	0.067	0.51	0.11	0.043	0.025
275	0.24	0.019	0.51	0.00	0.002	0.017	275	0.65	0.067	0.51	0.11	0.043	0.024
280	0.23	0.019	0.51	0.00	0.002	0.017	280	0.64	0.068	0.51	0.11	0.044	0.024
285	0.23	0.019	0.51	0.00	0.002	0.017	285	0.63	0.068	0.51	0.11	0.045	0.023
290	0.23	0.019	0.51	0.00	0.002	0.017	290	0.62	0.068	0.51	0.11	0.046	0.023
295	0.22	0.019	0.51	0.00	0.002	0.017	295	0.62	0.068	0.51	0.11	0.046	0.022
300	0.22	0.019	0.51	0.00	0.002	0.017	300	0.61	0.069	0.51	0.11	0.047	0.022
Mod. FAA Minor Storage Volume (cubic ft.) = 761 Mod. FAA Minor Storage Volume (acre-ft.) = 0.0175							Mod. FAA Major Storage Volume (cubic ft.) = 1,555 Mod. FAA Major Storage Volume (acre-ft.) = 0.0357						

UDFCD DETENTION BASIN VOLUME ESTIMATING WORKBOOK Version 2.34, Released November 2013

DETENTION VOLUME BY THE MODIFIED FAA METHOD

Project: 15_39 Taco Bell Heritage

Basin ID: Pond 1



DETENTION VOLUME BY THE FULL SPECTRUM METHOD

Project: Taco Bell Heritage
Basin ID: Pond 1

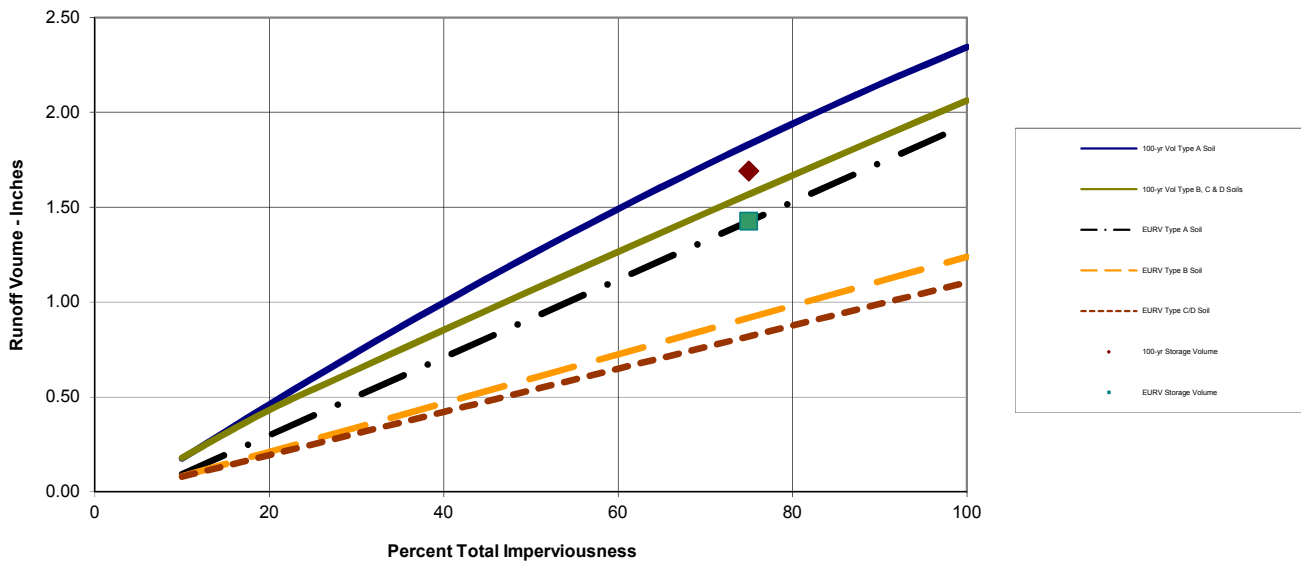
* User input data
shown in blue.

Area of Watershed (acres)	0.45	
Subwatershed Imperviousness	75.0%	
Level of Minimizing Directly Connected Impervious Area (MDCIA)	2	2
Effective Imperviousness ¹	68.7%	
Hydrologic Soil Type	Percentage of Area	Area (acres)
Type A	100.0%	0.5
Type B		0.0
Type C or D		0.0

Recommended Horton's Equation Parameters for CUHP		
Infiltration (inches per hour)		Decay Coefficient-- α
Initial-- f_i	Final-- f_o	
5	1.0	0.0007
Detention Volumes ^{2,5}		Maximum Allowable Release Rate, cfs ³
(watershed inches)	(acre-feet)	
1.43	0.05	Design Outlet to Empty EURV in 72 Hours
1.69	0.06	0.23

Excess Urban Runoff Volume⁴

100-year Detention Volume Including WQCV⁵



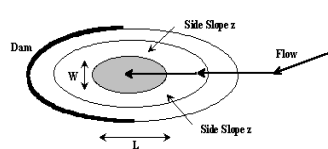
Notes:

- 1) Effective imperviousness is based on Figure ND-1 of the Urban Storm Drainage Criteria Manual (USDCM).
- 2) Results shown reflect runoff reduction from Level 1 or 2 MDCIA and are plotted at the watershed's total imperviousness value; the impact of MDCIA is reflected by the results being below the curves.
- 3) Maximum allowable release rates for 100-year event are based on Table SO-1. Outlet for the Excess Urban Runoff Volume (EURV) to be designed to empty out the EURV in 72 hours. Outlet design is similar to one for the WQCV outlet of an extended detention basin (i.e., perforated plate with a micro-pool) and extends to top of EURV water surface elevation.
- 4) EURV approximates the difference between developed and pre-developed runoff volume.
- 5) 100-yr detention volume includes EURV. No need to add more volume for WQCV or EURV

STAGE-STORAGE SIZING FOR DETENTION BASINS

Project: Taco Bell Heritage

Basin ID: Pond 1



Design Information (Input):

Width of Basin Bottom, W	=		ft
Length of Basin Bottom, L	=		ft
Dam Side-slope (H:V), Z_d	=		ft/ft

Right Triangle		OR...
Isosceles Triangle		OR...
Rectangle		OR...
Circle / Ellipse		OR...
Irregular		(Use Override values in cells G32:G52)

MINOR	MAJOR
0.02	0.04

acre-ft.

		acre-ft.
--	--	----------

0.05	0.06	acre-ft.
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Stage-Storage Relationship:

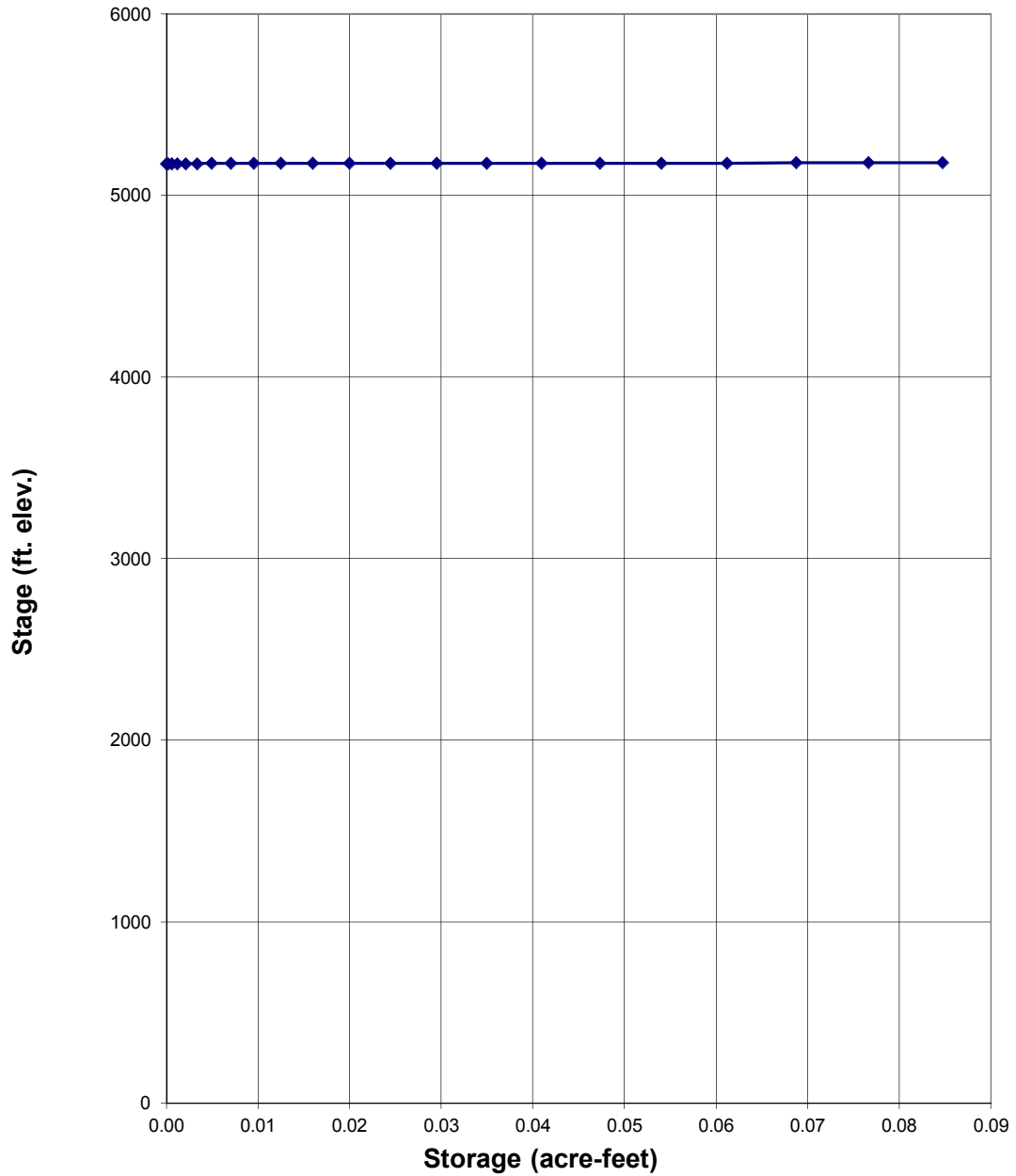
[illegible]

STAGE-STORAGE SIZING FOR DETENTION BASINS

Project: _____

Basin ID: _____

STAGE-STORAGE CURVE FOR THE POND



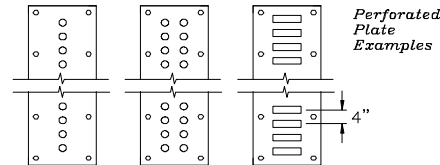
STAGE-DISCHARGE SIZING OF THE WATER QUALITY CAPTURE VOLUME (WQCV) OUTLET	
1	1
2	2
3	3
4	4
5	5
6	6
7	7
8	8
9	9
10	10
11	11
12	12
13	13
14	14
15	15
16	16
17	17
18	18
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97	97
98	98
99	99
100	100

Basin ID: Pond 1

WQCV Design Volume (Input):			
Catchment Imperviousness, I_a	=	75.0	percent
Catchment Area, A	=	0.45	acres
Depth at WQCV outlet above lowest perforation, H	=	1.1	feet
Vertical distance between rows, h	=	12.00	inches
Number of rows, N_L	=	2.00	
Orifice discharge coefficient, C_o	=	0.61	
Slope of Basin Trickle Channel, S	=	0.020	ft / ft
Time to Drain the Pond	=	72	hours

Height of slot, $H =$ inches
Width of slot, $W =$ inches

Percent Soil Type A =	100	%
Percent Soil Type B =		%
Percent Soil Type C/D =		%



Excess Urban Runoff Volume (From 'Full-Spectrum Sheet')	1.425 watershed inches
	N/A
Excess Urban Runoff Volume (From 'Full-Spectrum Sheet')	0.053 acre-feet
Outlet area per row, Ao =	0.32 square inches
Total opening area at each row based on user-input above, Ao =	6.28 square inches
Total opening area at each row based on user-input above, Ao =	0.044 square feet

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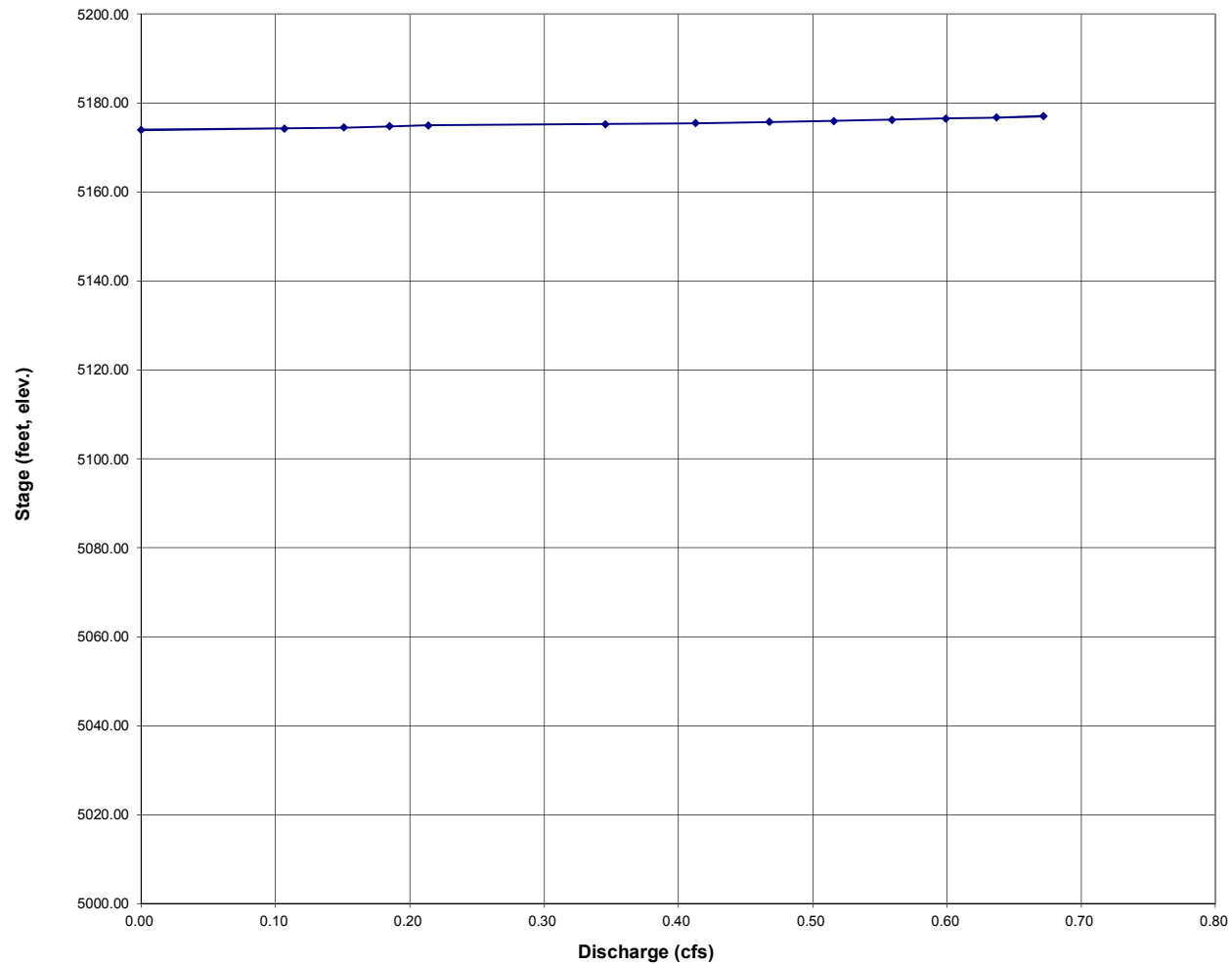
STAGE-DISCHARGE SIZING OF THE WATER QUALITY CAPTURE VOLUME (WQCV) OUTLET

Worksheet Protected

Project: **Taco Bell Heritage**

Basin ID: **Pond 1**

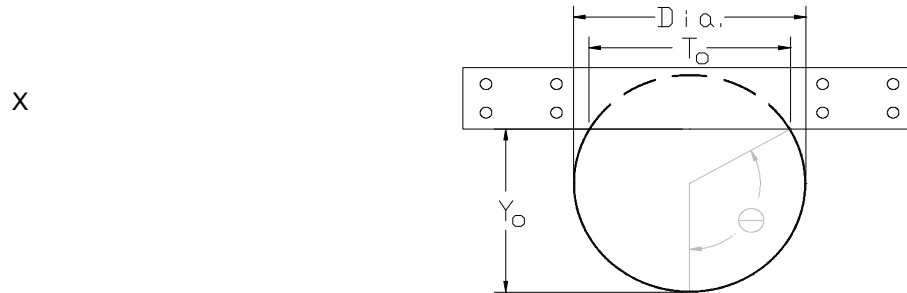
STAGE-DISCHARGE CURVE FOR THE WQCV OUTLET STRUCTURE



RESTRICTOR PLATE SIZING FOR CIRCULAR VERTICAL

Project: Taco Bell Heritage

Basin ID: Pond 1



Sizing the Restrictor Plate for Circular Vertical Orifices or Pipes (Input)

Water Surface Elevation at Design Depth

Pipe/Vertical Orifice Entrance Invert Elevation

Required Peak Flow through Orifice at Design Depth

Pipe/Vertical Orifice Diameter (inches)

Orifice Coefficient

Elev: WS =

Elev: Invert =

Q =

Dia =

C_o =

Full-flow Capacity (Calculated)

Full-flow area

Half Central Angle in Radians

Full-flow capacity

A_f =

Theta =

Q_f =

Percent of Design Flow =

Calculation of Orifice Flow Condition

Half Central Angle (0<Theta<3.1416)

Flow area

Top width of Orifice (inches)

Height from Invert of Orifice to Bottom of Plate (feet)

Elevation of Bottom of Plate

Resultant Peak Flow Through Orifice at Design Depth

Theta =

A_o =

T_o =

Y_o =

Elev Plate Bottom Edge =

Q_o =

Width of Equivalent Rectangular Vertical Orifice

Equivalent Width =

L ORIFICES

#1 Vertical Orifice	#2 Vertical Orifice	
5,175.75		feet
5,172.00		feet
0.60		cfs
12.0		inches
0.65		

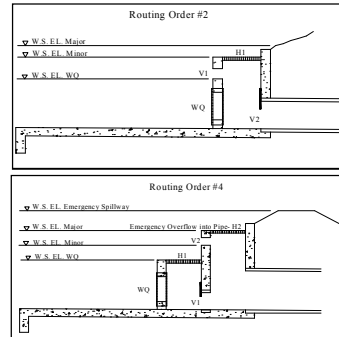
0.79		sq ft
3.14		rad
7.4		cfs
1232%		

0.74		rad
0.06		sq ft
8.07		inches
0.13		feet
5,172.13		feet
0.6		cfs

0.46		feet
-------------	--	-------------

STAGE-DISCHARGE SIZING OF THE WEIRS AND ORIFICES (INLET CONTROL)	
--	--

Project: Taco Bell Heritage
Basin ID: Pond 1



Routing 3: Single Stage - Water flows through WQCV plate and #1 horizontal opening into #1 vertical opening. This flow will be applied to culvert sheet (#2 vertical & horizontal openings is not used).

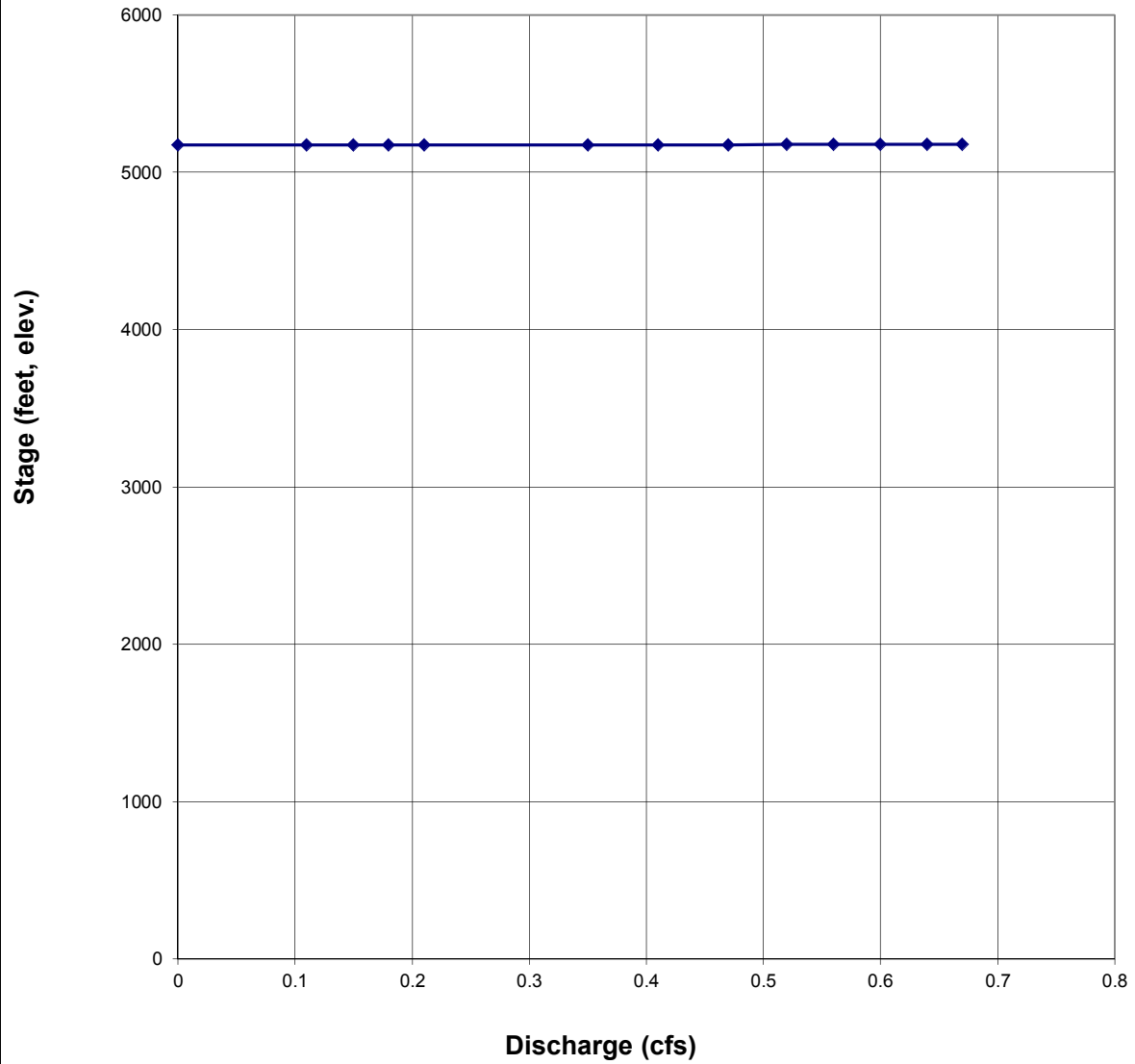
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STAGE-DISCHARGE SIZING OF THE WEIRS AND ORIFICES (INLET CONTROL)

Project: Taco Bell Heritage

Basin ID: Pond 1

STAGE-DISCHARGE CURVE FOR THE OUTLET STRUCTURE



DETENTION VOLUME BY THE MODIFIED FAA METHOD

Project: 15_39 Taco Bell Heritage

Basin ID: Pond 2

(For catchments less than 160 acres only. For larger catchments, use hydrograph routing method)
(NOTE: for catchments larger than 90 acres, CUHP hydrograph and routing are recommended)

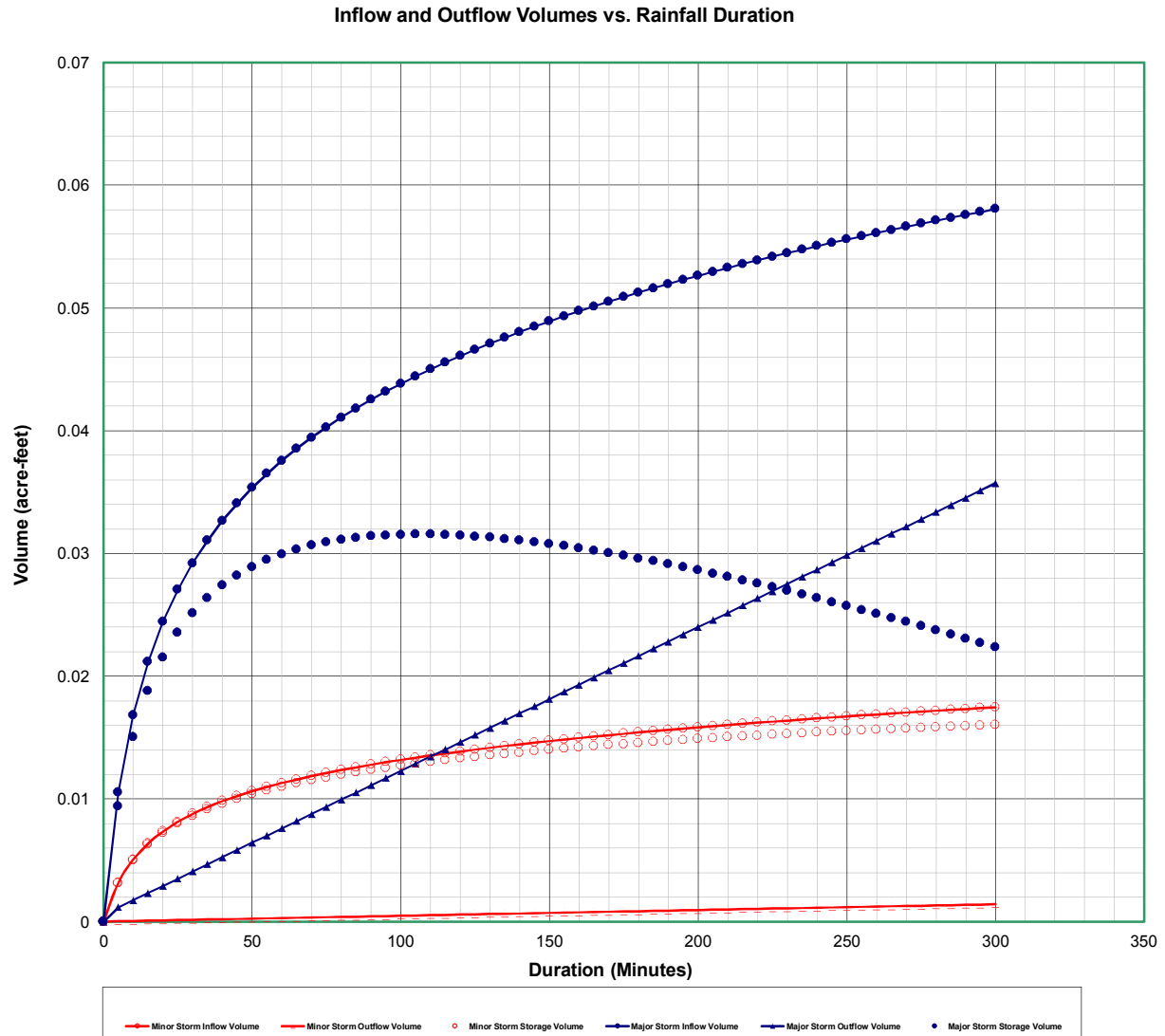
Determination of MINOR Detention Volume Using Modified FAA Method							Determination of MAJOR Detention Volume Using Modified FAA Method						
Design Information (Input): Catchment Drainage Imperviousness $I_p = 81.90$ percent Catchment Drainage Area $A = 0.340$ acres Predevelopment NRCS Soil Group Type = A A, B, C, or D Return Period for Detention Control $T = 2$ years (2, 5, 10, 25, 50, or 100) Time of Concentration of Watershed $T_c = 5$ minutes Allowable Unit Release Rate $q = 0.02$ cfs/acre One-hour Precipitation $P_1 = 0.72$ inches Design Rainfall IDF Formula $i = C_1 \cdot P_1 / (C_2 + T_c)^{C_3}$ Coefficient One $C_1 = 28.50$ Coefficient Two $C_2 = 10$ Coefficient Three $C_3 = 0.789$							Design Information (Input): Catchment Drainage Imperviousness $I_p = 81.90$ percent Catchment Drainage Area $A = 0.340$ acres Predevelopment NRCS Soil Group Type = A A, B, C, or D Return Period for Detention Control $T = 100$ years (2, 5, 10, 25, 50, or 100) Time of Concentration of Watershed $T_c = 5$ minutes Allowable Unit Release Rate $q = 0.50$ cfs/acre One-hour Precipitation $P_1 = 1.97$ inches Design Rainfall IDF Formula $i = C_1 \cdot P_1 / (C_2 + T_c)^{C_3}$ Coefficient One $C_1 = 28.50$ Coefficient Two $C_2 = 10$ Coefficient Three $C_3 = 0.789$						
Determination of Average Outflow from the Basin (Calculated): Runoff Coefficient $C = 0.56$ Inflow Peak Runoff $Q_{p-in} = 0.46$ cfs Allowable Peak Outflow Rate $Q_{p-out} = 0.01$ cfs Mod. FAA Minor Storage Volume = 699 cubic feet Mod. FAA Minor Storage Volume = 0.016 acre-ft							Determination of Average Outflow from the Basin (Calculated): Runoff Coefficient $C = 0.68$ Inflow Peak Runoff $Q_{p-in} = 1.53$ cfs Allowable Peak Outflow Rate $Q_{p-out} = 0.17$ cfs Mod. FAA Major Storage Volume = 1,374 cubic feet Mod. FAA Major Storage Volume = 0.032 acre-ft						
5 <- Enter Rainfall Duration Incremental Increase Value Here (e.g. 5 for 5-Minutes)													
Rainfall Duration minutes (input)	Rainfall Intensity inches / hr (output)	Inflow Volume acre-feet (output)	Adjustment Factor "m" (output)	Average Outflow cfs (output)	Outflow Volume acre-feet (output)	Storage Volume acre-feet (output)	Rainfall Duration minutes (input)	Rainfall Intensity inches / hr (output)	Inflow Volume acre-feet (output)	Adjustment Factor "m" (output)	Average Outflow cfs (output)	Outflow Volume acre-feet (output)	Storage Volume acre-feet (output)
0	0.00	0.000	0.00	0.00	0.000	0.000	0	0.00	0.000	0.00	0.00	0.000	0.000
5	2.42	0.003	1.00	0.01	0.000	0.003	5	6.63	0.011	1.00	0.17	0.001	0.009
10	1.93	0.005	0.75	0.01	0.000	0.005	10	5.28	0.017	0.75	0.13	0.002	0.015
15	1.62	0.006	0.67	0.00	0.000	0.006	15	4.43	0.021	0.67	0.11	0.002	0.019
20	1.40	0.007	0.63	0.00	0.000	0.007	20	3.84	0.024	0.63	0.11	0.003	0.022
25	1.24	0.008	0.60	0.00	0.000	0.008	25	3.40	0.027	0.60	0.10	0.004	0.024
30	1.12	0.009	0.58	0.00	0.000	0.009	30	3.06	0.029	0.58	0.10	0.004	0.025
35	1.02	0.009	0.57	0.00	0.000	0.009	35	2.79	0.031	0.57	0.10	0.005	0.026
40	0.94	0.010	0.56	0.00	0.000	0.010	40	2.56	0.033	0.56	0.10	0.005	0.027
45	0.87	0.010	0.56	0.00	0.000	0.010	45	2.38	0.034	0.56	0.09	0.006	0.028
50	0.81	0.011	0.55	0.00	0.000	0.010	50	2.22	0.035	0.55	0.09	0.006	0.029
55	0.76	0.011	0.55	0.00	0.000	0.011	55	2.08	0.037	0.55	0.09	0.007	0.029
60	0.72	0.011	0.54	0.00	0.000	0.011	60	1.97	0.038	0.54	0.09	0.008	0.030
65	0.68	0.012	0.54	0.00	0.000	0.011	65	1.86	0.039	0.54	0.09	0.008	0.030
70	0.65	0.012	0.54	0.00	0.000	0.012	70	1.77	0.039	0.54	0.09	0.009	0.031
75	0.62	0.012	0.53	0.00	0.000	0.012	75	1.69	0.040	0.53	0.09	0.009	0.031
80	0.59	0.012	0.53	0.00	0.000	0.012	80	1.61	0.041	0.53	0.09	0.010	0.031
85	0.56	0.013	0.53	0.00	0.000	0.012	85	1.54	0.042	0.53	0.09	0.011	0.031
90	0.54	0.013	0.53	0.00	0.000	0.012	90	1.48	0.043	0.53	0.09	0.011	0.031
95	0.52	0.013	0.53	0.00	0.000	0.013	95	1.43	0.043	0.53	0.09	0.012	0.031
100	0.50	0.013	0.53	0.00	0.000	0.013	100	1.38	0.044	0.53	0.09	0.012	0.032
105	0.49	0.013	0.52	0.00	0.001	0.013	105	1.33	0.044	0.52	0.09	0.013	0.032
110	0.47	0.014	0.52	0.00	0.001	0.013	110	1.28	0.045	0.52	0.09	0.013	0.032
115	0.45	0.014	0.52	0.00	0.001	0.013	115	1.24	0.046	0.52	0.09	0.014	0.032
120	0.44	0.014	0.52	0.00	0.001	0.013	120	1.21	0.046	0.52	0.09	0.015	0.031
125	0.43	0.014	0.52	0.00	0.001	0.013	125	1.17	0.047	0.52	0.09	0.015	0.031
130	0.42	0.014	0.52	0.00	0.001	0.014	130	1.14	0.047	0.52	0.09	0.016	0.031
135	0.40	0.014	0.52	0.00	0.001	0.014	135	1.11	0.048	0.52	0.09	0.016	0.031
140	0.39	0.014	0.52	0.00	0.001	0.014	140	1.08	0.048	0.52	0.09	0.017	0.031
145	0.38	0.015	0.52	0.00	0.001	0.014	145	1.05	0.048	0.52	0.09	0.018	0.031
150	0.37	0.015	0.52	0.00	0.001	0.014	150	1.02	0.049	0.52	0.09	0.018	0.031
155	0.37	0.015	0.52	0.00	0.001	0.014	155	1.00	0.049	0.52	0.09	0.019	0.031
160	0.36	0.015	0.52	0.00	0.001	0.014	160	0.98	0.050	0.52	0.09	0.019	0.030
165	0.35	0.015	0.52	0.00	0.001	0.014	165	0.95	0.050	0.52	0.09	0.020	0.030
170	0.34	0.015	0.51	0.00	0.001	0.014	170	0.93	0.051	0.51	0.09	0.020	0.030
175	0.33	0.015	0.51	0.00	0.001	0.014	175	0.91	0.051	0.51	0.09	0.021	0.030
180	0.33	0.015	0.51	0.00	0.001	0.015	180	0.89	0.051	0.51	0.09	0.022	0.030
185	0.32	0.016	0.51	0.00	0.001	0.015	185	0.88	0.052	0.51	0.09	0.022	0.029
190	0.31	0.016	0.51	0.00	0.001	0.015	190	0.86	0.052	0.51	0.09	0.023	0.029
195	0.31	0.016	0.51	0.00	0.001	0.015	195	0.84	0.052	0.51	0.09	0.023	0.029
200	0.30	0.016	0.51	0.00	0.001	0.015	200	0.83	0.053	0.51	0.09	0.024	0.029
205	0.30	0.016	0.51	0.00	0.001	0.015	205	0.81	0.053	0.51	0.09	0.025	0.028
210	0.29	0.016	0.51	0.00	0.001	0.015	210	0.80	0.053	0.51	0.09	0.025	0.028
215	0.29	0.016	0.51	0.00	0.001	0.015	215	0.78	0.054	0.51	0.09	0.026	0.028
220	0.28	0.016	0.51	0.00	0.001	0.015	220	0.77	0.054	0.51	0.09	0.026	0.028
225	0.28	0.016	0.51	0.00	0.001	0.015	225	0.76	0.054	0.51	0.09	0.027	0.027
230	0.27	0.016	0.51	0.00	0.001	0.015	230	0.74	0.054	0.51	0.09	0.028	0.027
235	0.27	0.016	0.51	0.00	0.001	0.015	235	0.73	0.055	0.51	0.09	0.028	0.027
240	0.26	0.017	0.51	0.00	0.001	0.015	240	0.72	0.055	0.51	0.09	0.029	0.026
245	0.26	0.017	0.51	0.00	0.001	0.015	245	0.71	0.055	0.51	0.09	0.029	0.026
250	0.26	0.017	0.51	0.00	0.001	0.016	250	0.70	0.056	0.51	0.09	0.030	0.026
255	0.25	0.017	0.51	0.00	0.001	0.016	255	0.69	0.056	0.51	0.09	0.030	0.025
260	0.25	0.017	0.51	0.00	0.001	0.016	260	0.68	0.056	0.51	0.09	0.031	0.025
265	0.24	0.017	0.51	0.00	0.001	0.016	265	0.67	0.056	0.51	0.09	0.032	0.025
270	0.24	0.017	0.51	0.00	0.001	0.016	270	0.66	0.057	0.51	0.09	0.032	0.024
275	0.24	0.017	0.51	0.00	0.001	0.016	275	0.65	0.057	0.51	0.09	0.033	0.024
280	0.23	0.017	0.51	0.00	0.001	0.016	280	0.64	0.057	0.51	0.09	0.033	0.024
285	0.23	0.017	0.51	0.00	0.001	0.016	285	0.63	0.057	0.51	0.09	0.034	0.023
290	0.23	0.017	0.51	0.00	0.001	0.016	290	0.62	0.058	0.51	0.09	0.035	0.023
295	0.22	0.017	0.51	0.00	0.001	0.016	295	0.62	0.058	0.51	0.09	0.035	0.023
300	0.22	0.017	0.51	0.00	0.001	0.016	300	0.61	0.058	0.51	0.09	0.036	0.022
Mod. FAA Minor Storage Volume (cubic ft.) = 699 Mod. FAA Minor Storage Volume (acre-ft.) = 0.0160							Mod. FAA Major Storage Volume (cubic ft.) = 1,374 Mod. FAA Major Storage Volume (acre-ft.) = 0.0315						

UDFCD DETENTION BASIN VOLUME ESTIMATING WORKBOOK Version 2.34, Released November 2013

DETENTION VOLUME BY THE MODIFIED FAA METHOD

Project: 15_39 Taco Bell Heritage

Basin ID: Pond 2



DETENTION VOLUME BY THE FULL SPECTRUM METHOD

Project: Taco Bell Heritage
Basin ID: Pond 2

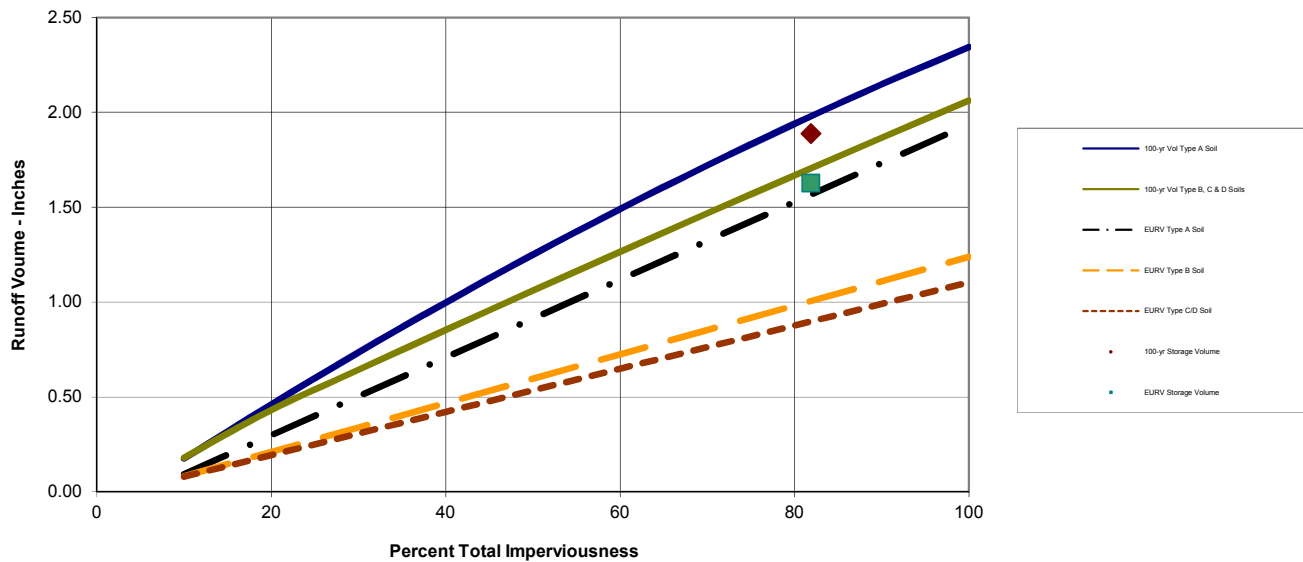
* User input data
shown in blue.

Area of Watershed (acres)	0.34	
Subwatershed Imperviousness	81.9%	
Level of Minimizing Directly Connected Impervious Area (MDCIA)	2	2
Effective Imperviousness ¹	77.6%	
Hydrologic Soil Type	Percentage of Area	Area (acres)
Type A	100.0%	0.3
Type B		0.0
Type C or D		0.0

Recommended Horton's Equation Parameters for CUHP		
Infiltration (inches per hour)		Decay Coefficient-- α
Initial-- f_i	Final-- f_o	
5	1.0	0.0007
Detention Volumes ^{2,5}		Maximum Allowable Release Rate, cfs ³
(watershed inches)	(acre-feet)	
1.63	0.05	Design Outlet to Empty EURV in 72 Hours
1.89	0.05	0.17

Excess Urban Runoff Volume⁴

100-year Detention Volume Including WQCV⁵

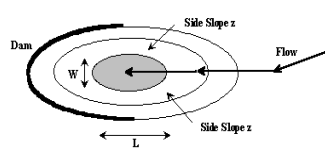


Notes:

- 1) Effective imperviousness is based on Figure ND-1 of the Urban Storm Drainage Criteria Manual (USDCM).
- 2) Results shown reflect runoff reduction from Level 1 or 2 MDCIA and are plotted at the watershed's total imperviousness value; the impact of MDCIA is reflected by the results being below the curves.
- 3) Maximum allowable release rates for 100-year event are based on Table SO-1. Outlet for the Excess Urban Runoff Volume (EURV) to be designed to empty out the EURV in 72 hours. Outlet design is similar to one for the WQCV outlet of an extended detention basin (i.e., perforated plate with a micro-pool) and extends to top of EURV water surface elevation.
- 4) EURV approximates the difference between developed and pre-developed runoff volume.
- 5) 100-yr detention volume includes EURV. No need to add more volume for WQCV or EURV

STAGE-STORAGE SIZING FOR DETENTION BASINS

Project: Taco Bell Heritage
Basin ID: Pond 2



Design Information (Input):		Check Basin Shape	
Width of Basin Bottom, W	=	Right Triangle	OR...
Length of Basin Bottom, L	=	Isosceles Triangle	OR...
Dam Side-slope (H:V), Z_d	=	Rectangle	OR...
		Circle / Ellipse	OR...
		Irregular	(Use Override values in cells G32:G52)

Check Basin Shape		
Right Triangle		OR...
Isosceles Triangle		OR...
Rectangle		OR...
Circle / Ellipse		OR...
Irregular		(Use Override values in cells G32:G52)

MINOR	MAJOR	
0.02	0.03	acre-ft.
		acre-ft.
0.05	0.05	acre-ft.

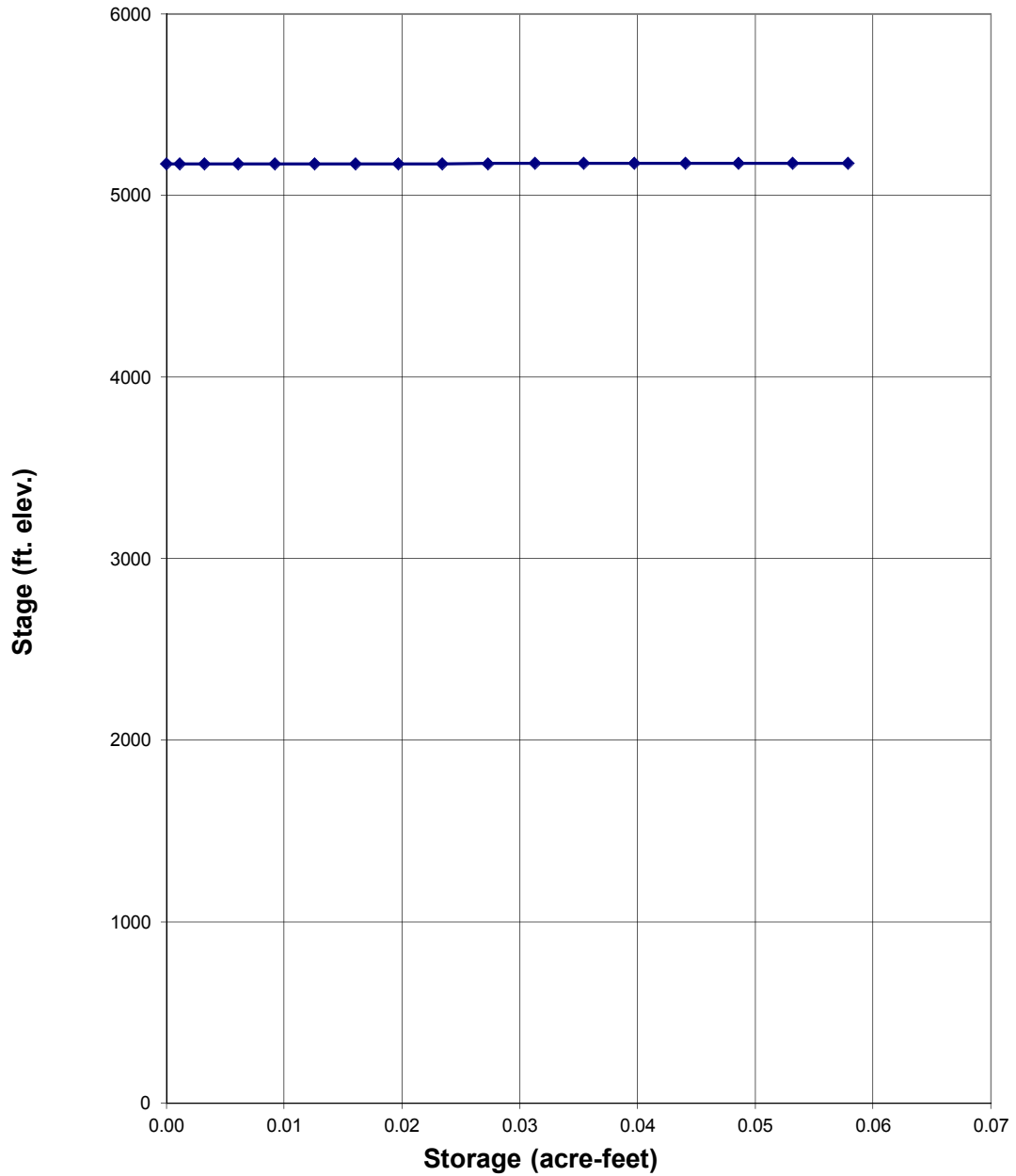
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STAGE-STORAGE SIZING FOR DETENTION BASINS

Project: _____

Basin ID: _____

STAGE-STORAGE CURVE FOR THE POND



STAGE-DISCHARGE SIZING OF THE WATER QUALITY CAPTURE VOLUME (WQCV) OUTLET	
--	--

Project: **Taco Bell Heritage**

Basin ID: Pond 2

WQCV Design Volume (Input): _____

Diameter of holes, $D = 2.000$ inches
 Number of holes per row, $N = 2$
OR
 Height of slot, $H =$ inches
 Width of slot, $W =$ inches

Height of slot, $H =$ inches
Width of slot, $W =$ inches

Watershed Design Information (Input):

Perforated Plate Examples

Outlet Design Information (Output):

Excess Urban Runoff Volume (From 'Full-Spectrum Sheet')	1.627 watershed inches
	N/A
Excess Urban Runoff Volume (From 'Full-Spectrum Sheet')	0.046 acre-feet
Outlet area per row, Ao =	0.28 square inches
Total opening area at each row based on user-input above, Ao =	6.28 square inches
Total opening area at each row based on user-input above, Ao =	0.044 square feet

[illegible]

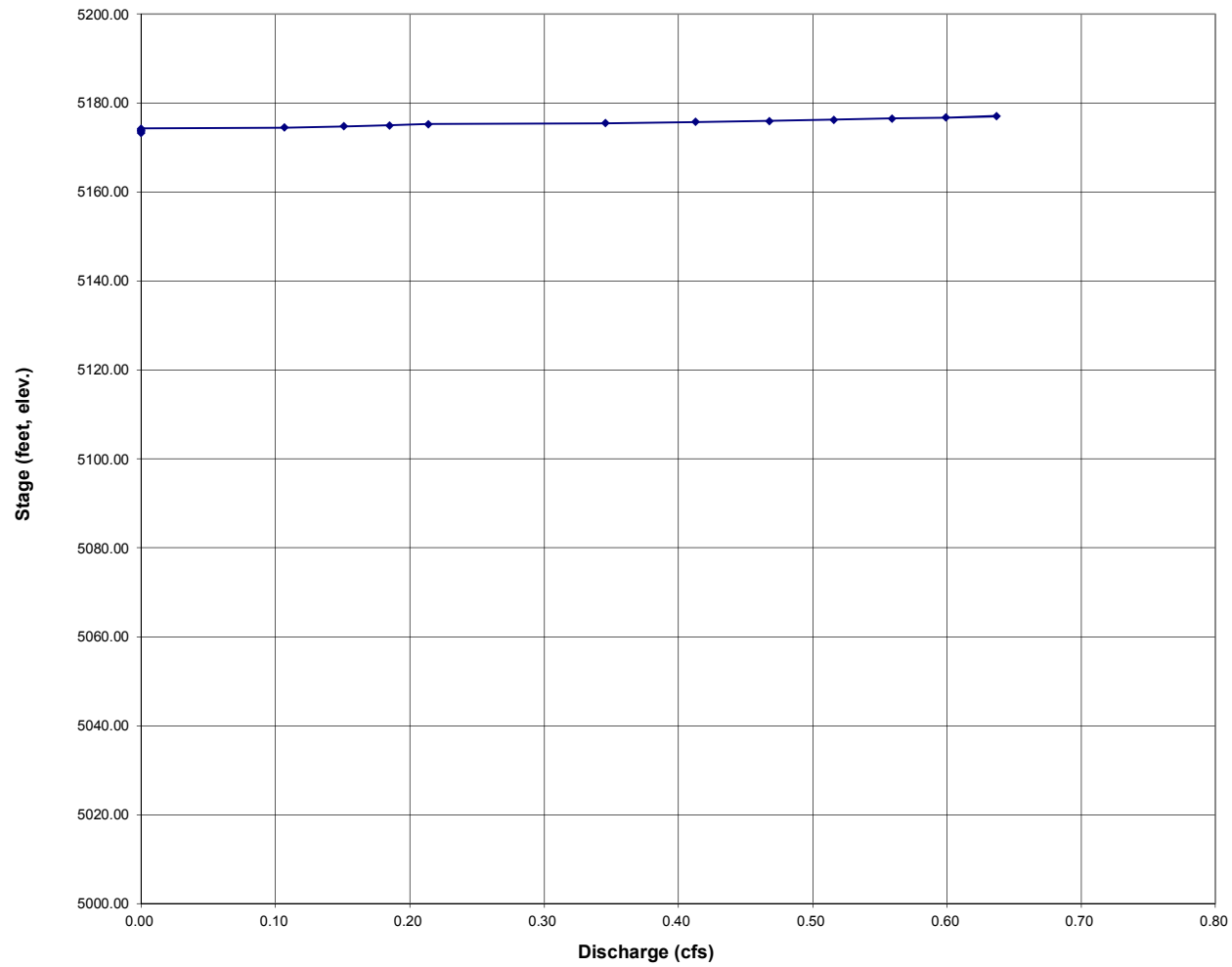
STAGE-DISCHARGE SIZING OF THE WATER QUALITY CAPTURE VOLUME (WQCV) OUTLET

Worksheet Protected

Project: **Taco Bell Heritage**

Basin ID: **Pond 2**

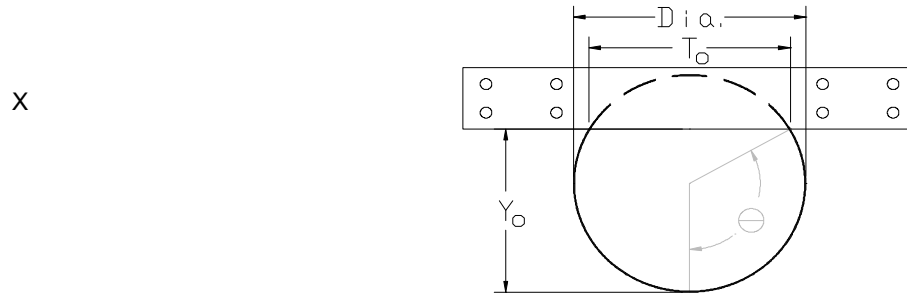
STAGE-DISCHARGE CURVE FOR THE WQCV OUTLET STRUCTURE



RESTRICTOR PLATE SIZING FOR CIRCULAR VERTICAL

Project: Taco Bell Heritage

Basin ID: Pond 2



Sizing the Restrictor Plate for Circular Vertical Orifices or Pipes (Input)

Water Surface Elevation at Design Depth

Elev: WS =

Pipe/Vertical Orifice Entrance Invert Elevation

Elev: Invert =

Required Peak Flow through Orifice at Design Depth

Q =

Pipe/Vertical Orifice Diameter (inches)

Dia =

Orifice Coefficient

C_o =

Full-flow Capacity (Calculated)

Full-flow area

A_f =

Half Central Angle in Radians

Theta =

Full-flow capacity

Q_f =

Percent of Design Flow =

Calculation of Orifice Flow Condition

Half Central Angle ($0 < \text{Theta} < 3.1416$)

Theta =

Flow area

A_o =

Top width of Orifice (inches)

T_o =

Height from Invert of Orifice to Bottom of Plate (feet)

Y_o =

Elevation of Bottom of Plate

Elev Plate Bottom Edge =

Resultant Peak Flow Through Orifice at Design Depth

Q_o =

Width of Equivalent Rectangular Vertical Orifice

Equivalent Width =

L ORIFICES

#1 Vertical Orifice	#2 Vertical Orifice	
5,173.75		feet
5,170.95		feet
0.50		cfs
12.0		inches
0.65		

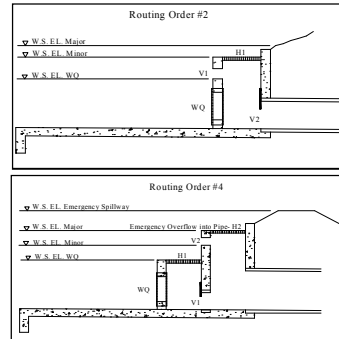
0.79		sq ft
3.14		rad
6.2		cfs
1242%		

0.73		rad
0.06		sq ft
7.99		inches
0.13		feet
5,171.08		feet
0.5		cfs

0.46		feet
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STAGE-DISCHARGE SIZING OF THE WEIRS AND ORIFICES (INLET CONTROL)	
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Project: Taco Bell Heritage
Basin ID: Pond 2



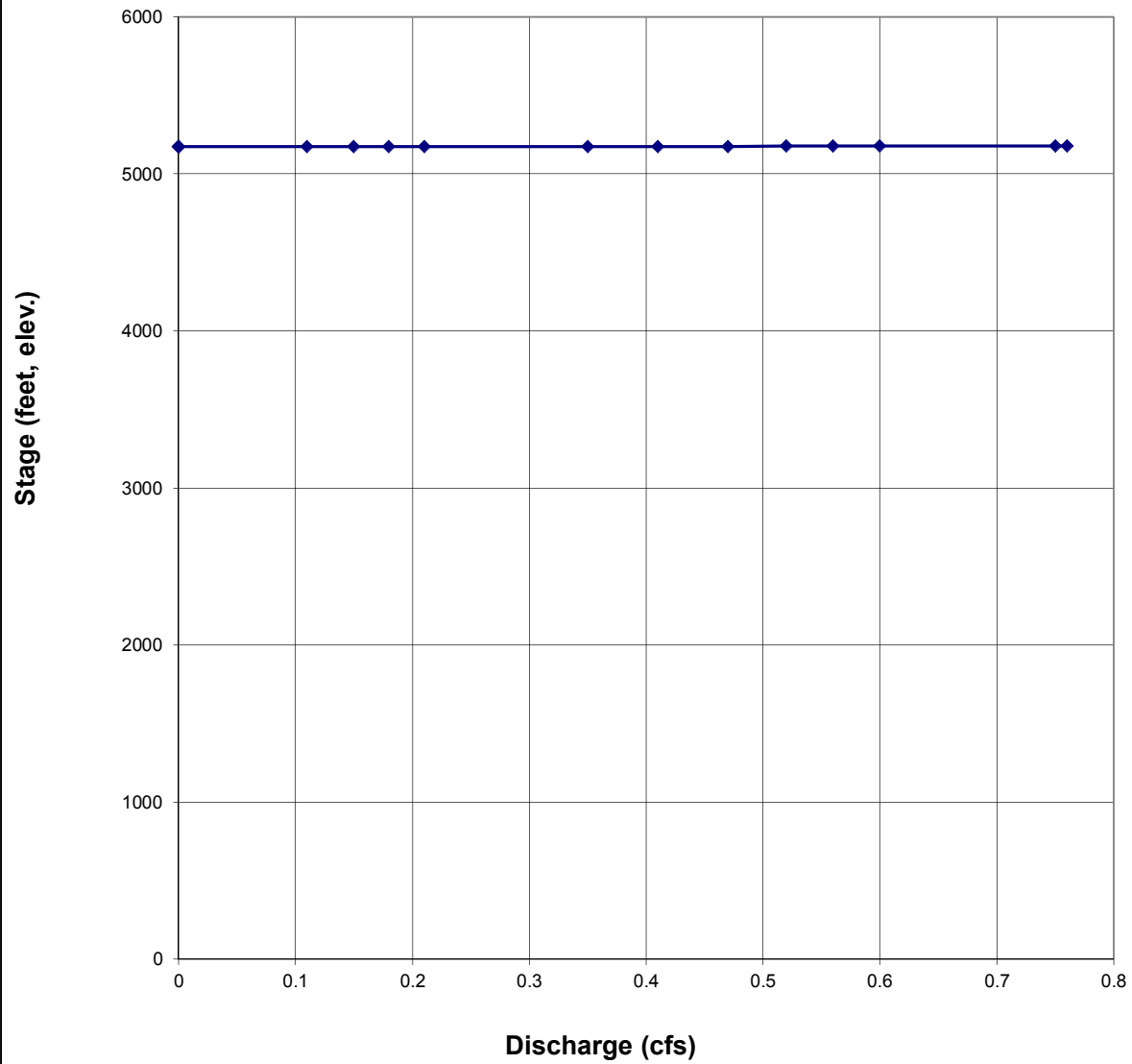
Routing 3: Single Stage - Water flows through WQCV plate and #1 horizontal opening into #1 vertical opening. This flow will be applied to culvert sheet (#2 vertical & horizontal openings is not used).

[illegible]

STAGE-DISCHARGE SIZING OF THE WEIRS AND ORIFICES (INLET CONTROL)

Project: Taco Bell Heritage
Basin ID: Pond 2

STAGE-DISCHARGE CURVE FOR THE OUTLET STRUCTURE



Channel Report

12 in. Pipe @ 0.50%

Circular

Diameter (ft) = 1.00

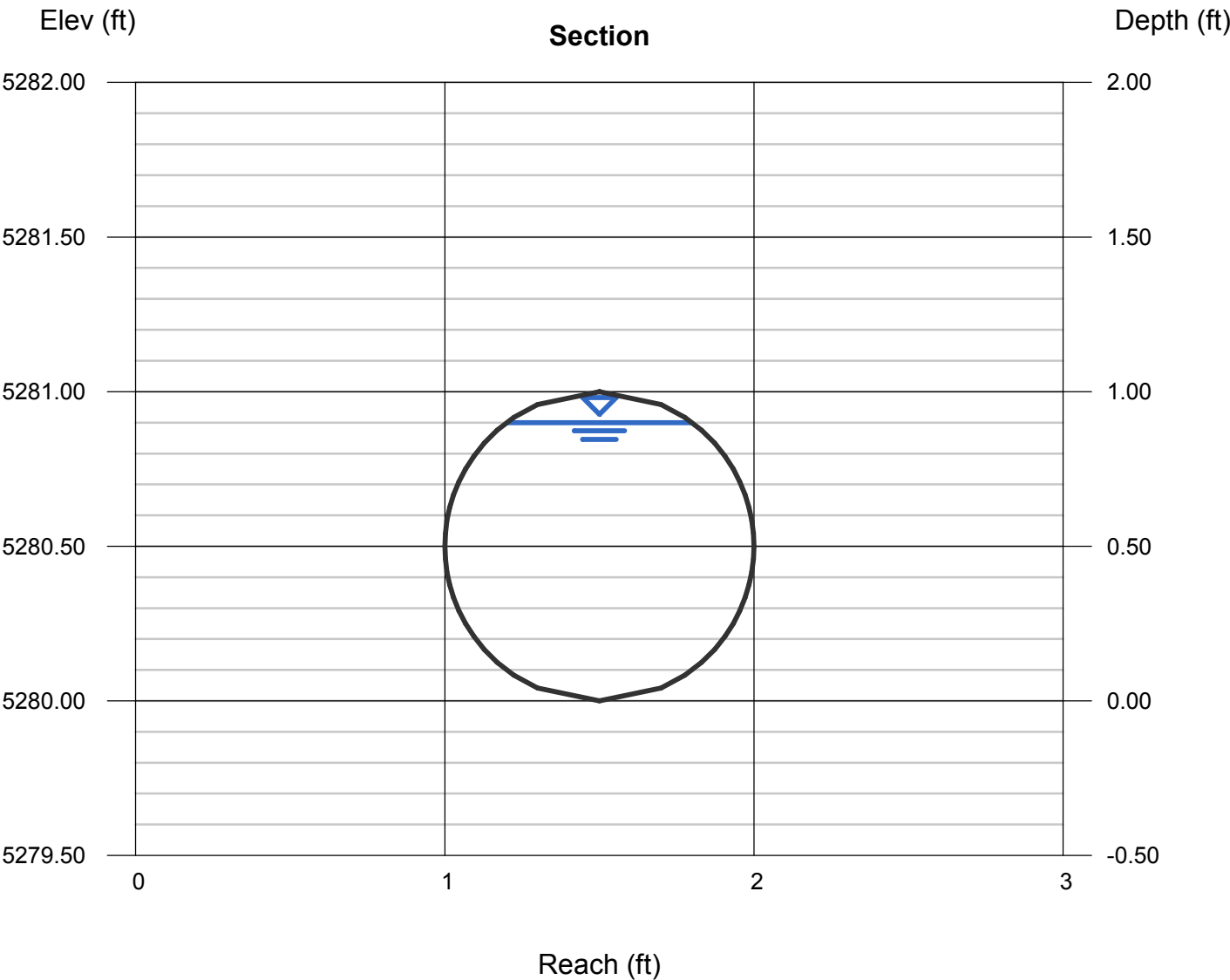
Invert Elev (ft) = 5280.00
Slope (%) = 0.50
N-Value = 0.013

Calculations

Compute by: Q vs Depth
No. Increments = 10

Highlighted

Depth (ft) = 0.90
Q (cfs) = 2.685
Area (sqft) = 0.74
Velocity (ft/s) = 3.60
Wetted Perim (ft) = 2.50
Crit Depth, Yc (ft) = 0.71
Top Width (ft) = 0.60
EGL (ft) = 1.10



Channel Report

18 in. Pipe @ 8.00%

Circular

Diameter (ft) = 1.50

Invert Elev (ft) = 5280.00

Slope (%) = 8.00

N-Value = 0.013

Calculations

Compute by: Q vs Depth

No. Increments = 10

Highlighted

Depth (ft) = 1.35

Q (cfs) = 31.67

Area (sqft) = 1.68

Velocity (ft/s) = 18.89

Wetted Perim (ft) = 3.75

Crit Depth, Yc (ft) = 1.50

Top Width (ft) = 0.90

EGL (ft) = 6.90

