# CITY OF ALBUQUERQUE

*Planning Department* David Campbell, Director



Mayor Timothy M. Keller

June 20, 2019

David Soule, P.E. Rio Grande Engineering PO Box 93924 Albuquerque, NM 87199

### RE: 10101 Norman NE Grading and Drainage Plan Engineer's Stamp Date: 6/13/19 Drainage File: E10D063

Dear Mr. Soule:

Based on the submittal received on 6/14/19, the grading and drainage plan is approved for Grading Permit and Building Permit. As a reminder, if the project total area of disturbance (including the staging area and any work within the adjacent Right-of-Way) is 1 acre or more, then an Erosion and Sediment Control (ESC) Plan and Owner's certified Notice of Intent (NOI) is required to be submitted to the Stormwater Quality Engineer (Curtis Cherne, PE, ccherne@cabq.gov, 924-3420) 14 days prior to any earth disturbance.
 Albuquerque
 Prior to Certificate of Occupancy (For Information):

 Engineer's Certification, per the DPM Chapter 22.7: Engineer's Certification Checklist For Non-Subdivision is required.

www.cabq.gov

2. A Bernalillo County Recorded Private Facility Drainage Covenant is required for the stormwater quality ponds. The original notarized form, exhibit A (legible on 8.5x11 paper), and recording fee (\$25, payable to Bernalillo County) must be turned into DRC (4th, Plaza del Sol) for routing. Please contact Charlotte LaBadie (clabadie@cabq.gov, 924-3996) or Madeline Carruthers (mtafoya@cabq.gov, 924-3997) regarding the routing and recording process for covenants. The routing and recording process for covenants can take a month or longer; Hydrology recommends beginning this process as soon as possible as to not delay approval for certificate of occupancy.

If you have any questions, please contact me at 924-3695 or dpeterson@cabq.gov.

Sincerely,

Dana Peterson, P.E. Senior Engineer, Planning Dept. Development Review Services

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# City of Albuquerque

Planning Department Development & Building Services Division

DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 6/2018)

Project Title: 10101 Norman	Building Permit	#:	Hydrol	ogy File #:
DRB#:	_ EPC#:		Work	Order#:
Legal Description: LOT 44 BLOCK	125 SNOW HE	IGHTS		
City Address: Norman		••••••••••••••••••••••••••••••••••••••		
			_Contact:	
Address:				
Phone#:				
Other Contact: RIO GRANDE ENGINE	CERING		_Contact:	DAVID SOULE
Address: PO BOX 93924 ALB NM				
Phone#: 505.321.9099	<b>Fax#:</b> 505.872.	0999	_E-mail:d	avid@riograndeengineering.com
TYPE OF DEVELOPMENT: PLAT				
Check all that Apply:				
DEPARTMENT: <u> </u>		TYPE OF APPROV BUILDING PER CERTIFICATE	RMIT APPF	
TYPE OF SUBMITTAL:        ENGINEER/ARCHITECT CERTIFICATION        PAD CERTIFICATION        CONCEPTUAL G & D PLAN         X       GRADING PLAN        DRAINAGE REPORT        DRAINAGE MASTER PLAN        FLOODPLAIN DEVELOPMENT PERMIT A        ELEVATION CERTIFICATE        CLOMR/LOMR        TRAFFIC CIRCULATION LAYOUT (TCL)        TRAFFIC IMPACT STUDY (TIS)        STREET LIGHT LAYOUT        OTHER (SPECIFY)        Yes       X        Yes       X	APPLIC	FINAL PLAT A	R SUB'D A R BLDG. I APPROVAL OF FINAN PERMIT A PERMIT APPR VAL IIT APPRC D CERTIF APPROVAL DEVELOPI	APPROVAL PERMIT APPROVAL L VCIAL GUARANTEE APPROVAL ROVAL OVAL DVAL ICATION
DATE SUBMITTED:				
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DRAINAGE REPORT

For

# Norman Apartment

# Albuquerque, New Mexico

Prepared by

Rio Grande Engineering PO Box 93924 Albuquerque, New Mexico 87199

June 2019



David Soule P.E. No. 14522

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### Appendix

Site Hydrology/ AHYMO MODEL
Map Pocket
Site Grading and Drainage Plan

### PURPOSE

The purpose of this report is to provide the Drainage Management Plan for the infill development of an existing lot between Snow Heights and Indian School east of Eubank. This plan was prepared in accordance with the City of Albuquerque design regulations, utilizing the City of Albuquerque's Development Process Manual drainage guidelines. This report will demonstrate that the grading does not adversely affect the surrounding properties, nor the upstream or downstream facilities.

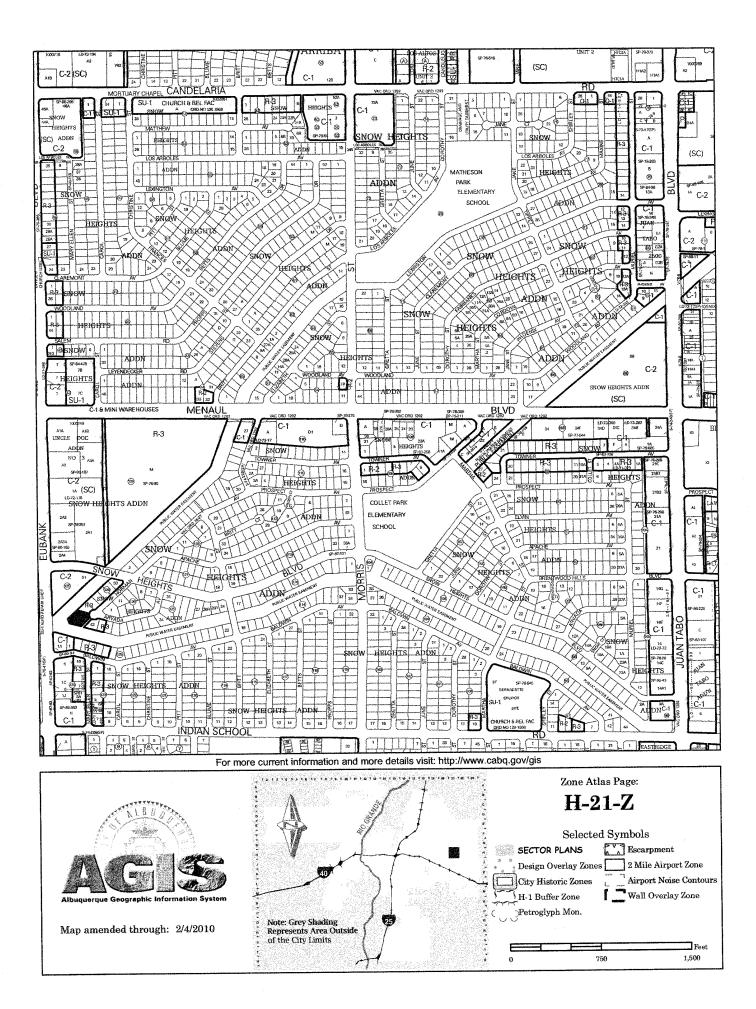
### INTRODUCTION

The subject of this report, as shown on the Exhibit A, is a 0.39-acre parcel of land located at 10101 Norman NE in north east Albuquerque. The legal description of this site is lot 44 Block 125 Snow heights Addition. As shown on FIRM map35001C0356HG, the entire property is located within Flood Zone X. This site is surrounded by fully developed parcels. The site is bound by two city maintained drainage channels. This site is an existing developed site within fully developed areas. Based on the site location and the adjacent drainage infrastructure this development must maintain existing drainage patterns and match existing conditions as closely as possible.

### **EXISTING CONDITIONS**

The site is currently developed as a single family residential lot. The site is not in native condition. Due to curb and gutter and adjacent drainage infrastructure, this lot is not impacted by upland flow. The site currently discharges 1.07 cfs to thru the rear wall to the adjacent channels. The discharge leaves the site thru a series of turned blocks within the perimeter wall.

3



### **PROPOSED CONDITIONS**

The proposed improvements consist of a two unit townhouse building and associated parking area. The site will be graded to accommodate the new building while maintaining the existing drainage patterns. As shown on the grading plan, the site will be graded to contain two basins. The site was modeled utilizing NOAA atlas rainfall data and AHMYO, located appendix B. The northern basin contains the northern half of the new units and a portion of the existing building. This basin generates 0.50 cfs. The flow drains through a water quality/detention basin at the northwest corner of the site. The pond discharges to the existing drainage rights of way via the existing turned blocks in the wall. The required first flush volume of 44 cf is retained onsite. The southern basin contains the remaining portion of the lot. This basin generates 0.85 cfs. The basin discharges to a new 6" pipe connected to an existing concrete channel. The parking area serves as a detention basin and the peak routed flow leaving this basin 0.43 cfs. An emergency overflow for this basin is provided by a turned block. The combined proposed peak flow leaving the site will be 0.82 cfs. The required first flush volume of 142 cf is retained onsite.

### SUMMARY AND RECOMMENDATIONS

This project is an infill project within a completely developed area of North Albuquerque. The site is currently undeveloped. The site currently discharges 1.07 cfs to the adjacent drainage right of way. The site is not impacted by upland flows. The proposed drainage plan will maintain the existing drainage patterns and reduce the peak flow to 0.82 cfs to pass through the site. The first flush volumes are retained onsite. since this site work area encompasses less than 1 acre, a NPDES permit and Erosion and Sediment Control Plan may not be required prior to any construction activity.

5

### APPENDIX A

## SITE HYDROLOGY / AHYMO MODEL



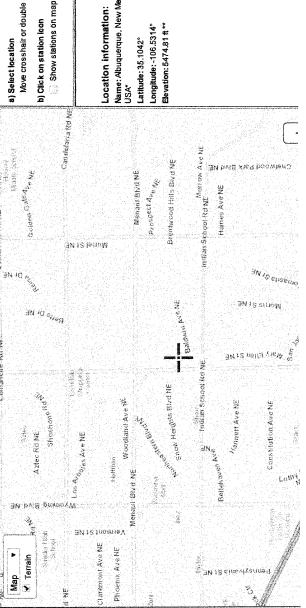
Organization

NWS O ANNOAA Go Search

# NOAA ATLAS 14 POINT PRECIPITATION FREQUENCY ESTIMATES: NM

General Information Progress Reports

1-0-174 BARB	
Progress Reports	Data description
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anajar Tarto Setters	b) By station (list of NM stations):   Select station *
Tokas prosentina Estas antra metra	c) By address Search Q
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Contact Us

Precipitation Frequency Tata Server

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# POINT PRECIPITATION FREQUENCY (PF) ESTIMATES WITH 90% CONFIDENCE INTERVALS AND SUPPLEMENTARY INFORMATION NOAA Atlas 14, Volume 1, Version 5

PF tabular

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PP graphicat

Supplementary manuation

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Print page

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				~	Average recurrence interval (years)	ce interval (years)				
<u> </u>	-	2	5	10	25	50	100	200	500	1000
~	0.179	0.232	0.310	0.371	0.455	0.520	0.589	0.661	0.758	0.836
	(0.152-0.211)	(0.198-0.274)	(0.262-0.367)	(0.313-0.438)	(0.382-0.536)	(0.434-0.612)	(0.488-0.692)	(0.544-0.776)	(0.619-0.892)	(0.679-0.983)
<u> </u>	0.272	0.352	0.473	0.565	0.692	0.791	0.896	1.00	1.15	1.27
)) 10-min	(0.231-0.321)	(0.298-0.416)	(0.399-0.558)	(0.476-0.666)	(0.581-0.815)	(0.661-0.832)	(0.743-1.05)	(0.829-1.18)	(0.942-1.36)	(1.03-1.50)
	0.338	0.437	0.586	0.701	0.858	0.981	1.11	1.26	1.43	1.58
15-min (	(0.286-0.398)	(0.369-0.516)	(0.485-0.692)	(0.590-0.826)	(0.720-1.01)	(0.820-1.16)	(0:921-1.31)	(1.03-1.47)	(1.17-1.68)	(1.28-1.86)
	0.455	0.588	0.789	0.944	1.16	1.32	1.50	1,68	1.93	2.12
30-min    (	(0.385-0.536)	(0.497-0.695)	(0.667-0.932)	(0.794-1.11)	(0.970-1.36)	(1.10-1.56)	(1.24-1.76)	(1.38-1.97)	(1.57-2.27)	(1.72-2.50)
	0.663	0.727	0.976	1.17	1.43	1,64	1,85	2.08	2.38	2.63
60-min	(0.477-0.663)	(0.615-0.860)	(0.825-1.15)	(0.983-1.38)	(1.20-1.68)	(1.37-1.93)	(1.54-2.18)	(1.71-2.44)	(1.95-2.80)	(2.13-3.09)
IL_	0.668	0.857	1.13	1.35	1.66	1,91	2.17	2.44	2.82	3.13
2-hr	(0.557-0.817)	(0.714-1.05)	(0,842-1.38)	(1.12-1.64)	(1.36-2.01)	(1.56-2.31)	(1.76-2.62)	(1.97-2.94)	(2.25-3.40)	(2.48-3.78)
	0.713	0.907	1.19	1.41	1.72	1.97	2.24	2.52	2.91	3.23
3tr	(0.598-0.866)	(0.758-1.10)	(0.994-1.44)	(1.18-1.70)	(1.42-2.08)	(1.62-2.38)	(1,83-2,69)	(2.04-3.03)	(2.34-3.49)	(2.57-3.88)
	0.631	1.05	1.35	1.59	1.92	2.17	2.44	2.72	3.10	3.42
2-5-	(0.703-1.00)	(0.888-1.27)	(1.14-1.63)	(1.34-1.91)	(1.60-2.30)	(1.81-2.60)	(2.02-2.92)	(2.24-3.25)	(2.54-3.70)	(2.77-4.08)
	0.926	1.17	1.48	1.73	2.06	2,32	2.59	2.87	3.24	3.55
12-br	(0.795-1.08)	(1.00-1.37)	(1.26-1.73)	(1.47-2.02)	(1.75-2.40)	(1.96-2.70)	(2.18-3.01)	(2.39-3.34)	(2.68-3.78)	(2.91-4.14)
	1.07	1.34	1.68	1.95	2.32	2.60	2.90	3.20	3.61	3.93
24-hr	(0.932-1.24)	(1.17-1.55)	(1.46-1.94)	(1.70-2.25)	(2.01-2.68)	(2.25-3.00)	(2.49-3.34)	(2.74-3.68)	(3.07-4.15)	(3.32-4.52)
	1.14	1.43	1.80	2.08	2.48	2.78	3.10	3.43	3.86	4.21
2-day	(0.983-1.30)	(1.25-1.63)	(1.57-2.05)	(1.82-2.38)	(2.15-2.83)	(2.41-3.18)	(2.67-3.54)	(2.94-3.92)	(3.29-4.43)	(3.57-4.83)
	1.25	1.56	1.94	2.24	2.65	2,96	3.28	3.61	4.04	4.38
3-day	(1.12-1.40)	(1.40-1.74)	(1.74-2.17)	(2.00-2.50)	(2.36-2.96)	(2.63-3.31)	(2.90-3.66)	(3.18-4.03)	(3.54-4.53)	(3.82-4.91)
	1.36	1.69	2.09	2.40	2.82	3,14	3.46	3.79	4.22	4.56
4-day	(1.25-1.49)	(1.55-1.85)	(1.91-2.28)	(2.19-2.62)	(2.56-3.08)	(2.85-3.43)	(3.13-3.78)	(3.42-4.14)	(3.79-4.62)	(4.07-5.00)
	1.57	1.95	2,38	2.72	3.18	3.51	3,85	4.19	4.62	4.95
7-day	(1.44-1.71)	(1.79-2.12)	(2.19-2.60)	(2.49-2.97)	(2.90-3.45)	(3.21-3.82)	(3.51-4.19)	(3.80-4.55)	(4.18-5.04)	(4.46-5.40)
	1.74	2.17	2.67	3.06	3.58	3.97	4.37	4.76	5.28	5.67
10-day	(1.61-1.90)	(1.99-2.36)	(2.45-2.90)	(2.81-3.32)	(3.28-3.88)	(3.63-4.30)	(3.98-4.73)	(4.32-5.16)	(4.77-5.73)	(5.10-6.16)
20-day	2.23	2.78	3.39	3.84	4.43	4.86 (4.45.5.28)	<b>5.28</b> (4 82-5 74)	5.68 (5.17-6.17)	6.19 (5.82-6.73)	6.56 (5.94-7.15)
	(2.05-2.43)	(cn:c-cc:z)	(0.11-0.00)	(0.33-4.10)	(20'1-00'4)		(- ··· - ···)	1	(n 10 40.0)	(A1.1 A1A)

30-day	<b>2.69</b> (2.47-2.92)	<b>3.35</b> (3.07-3.63)	<b>4.04</b> (3.71-4.38)	<b>4.56</b> (4.18-4.94)	<b>5.22</b> (4.78-5.64)	<b>5.69</b> (5.20-6.14)	<b>6.14</b> (5.60-6.63)	<b>6.57</b> (5.98-7.10)	<b>7.09</b> (6.44-7.67)	<b>7.47</b> (6.77-8.09)	
45-day	<b>3.29</b> (3.04-3.56)	<b>4.08</b> (3.77-4.42)	4.50-5.28)	<b>5.46</b> (5.03-5.90)	<b>6.17</b> (5.67-6.67)	<b>6.66</b> (6.12-7.20)	<b>7.12</b> (6.54-7.70)	<b>7.54</b> (6.91-8.15)	<b>8.04</b> (7.35-8.70)	<b>8.37</b> (7,65-9.07)	
0-day	<b>3.79</b> (3.50-4.11)	<b>4.70</b> (4.34-5.09)	<b>5.62</b> (5.19-6.09)	<b>6.29</b> (5.80-6.81)	<b>7.09</b> (6.54-7.68)	<b>7.65</b> (7.05-8.28)	<b>8.17</b> (7.52-8.85)	<b>8.64</b> (7,95-9.38)	<b>9.21</b> (8.45-10.00)	<b>9.58</b> (8.80-10.4)	
Precipita	ation frequency (F	requency (PF) estimates in this table are based on	s table are based o	in frequency analysis	of partial dur	ation series (PDS).					

Number in performance of the performance of the performance of the second s

Hease refer to NOAA Atlas 14 document for more information.

Estimates from the table in CSV format: Precipitation frequency estimates **v** Submit

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1325 East West Highway		
Silver Spring, MD 20910		
Page Author: HDSC webmaster		
Page last modified: April 21, 2017		

### FIRST FLUSH VOLUMES

### NORTH BASIN

REQUIRED=1550X.034/12=44 CU. FT PROVIDED=60 CU.FT

SOUTH BASIN= 5024 SF x0.34/12=142 CU FT PROVIDED=144 CU.FT

# **VOLUME CALCULATIONS**

pond b

OUTLET@73

outlet at 74

	ACTUAL ELEV.	DEPTH (FT)	AREA SF	VOLUME PER UNIT	VOLUME CUMULATIVI	VOLUME AC-FT	Q (CFS)
	73.00	0.00	30.00	0	0	0.000	0.00
r	74.00	0.00	1106.00	568.00	568	0.001	0.00
	74.50	0.83	1520.00	656.50	1224.5	0.028	0.86
ſ	75.00	1.33	2400.00	980.00	2204.5	0.051	1.09

### Orifice Equation

Q = CA SQRT(2gH)

C =	0.6
Diameter (in)	6
Area (ft^2)=	0.196349541
g =	32.2
H (Ft) =	Depth of water above center of orifice
Q (CFS)=	Flow

pondrout061219.txt

-	ENTION-NORMAN ROUTING
START	TIME=0.0 PUNCH CODE=0
RAINFALL	TYPE=2 QUARTER=0.0 ONE= 1.85 IN SIX=2.44 IN DAY= 2.90 IN DT = 0.05 HR
*Basin EXISTING COMPUTE NM HYD	ID=1 HYD NO=101 DA= .000606348 SQ MI PER A=00 PER B=41 PER C=42 PER D=17 TP=170 MASSRAIN=-1
PRINT HYD	ID=1 CODE=3
*Basin NORTH PROPOS COMPUTE NM HYD	ID=2 HYD NO=102 DA= .000240796 SQ MI
	PER A=00 PER B=23 PER C=39 PER D=38 TP=170 MASSRAIN=-1
PRINT HYD	ID=2 CODE=3
*Basin SOUTH PROPOS COMPUTE NM HYD	
	PER A=00 PER B=10 PER C=25 PER D=65 TP=- 170 MASSRAIN=-1
PRINT HYD	ID=3 CODE=3
* ROUTE THE TOTAL ROUTE RESERVOIR	FLOW THROUGH THE PROPOSED RESERVOIR         ID=4       HYD NO=104       INFLOW=3       CODE=3         OUTFLOW(CFS)       STORAGE(AC-FT)       ELEV(FT)         0.00       0.001       74.00         0.86       0.028       74.50         1.09       0.051       75.00
*TOTAL PROPOSED	
ADD HYD	ID=5 HYD NO=105 ID I=2 ID II=4
PRINT HYD	ID=5 CODE=3

	AHYMO. OUT							
AHYMO PROGRAM (AHY	YMO-54)	- Version: S4.01a - Rel:						
01a RUN DATE (MON START TIME (H	N/DAY/YR) = 06/13/2019 HR:MIN:SEC) = 17:00:38	USER NO.=						
RioGrandeSingleA41963517 INPUT FILE = C:\Documents and Settings\Owner\Desktop\2019								
JOBS\1976-norman\pondrout(	061219.txt							
*S AHYMO – DETENT	TION-NORMAN							
*S POND RC	DUTING							
START TI	IME=0.0 PUNCH CODE=0							

RAINFALL TYPE=2 QUARTER=0.0 ONE= 1.85 IN SIX=2.44 IN DAY= 2.90 IN DT = 0.05 HR

24-HOUR RAINFALL DIST. - BASED ON NOAA ATLAS 14 FOR CONVECTIVE AREAS (NM & AZ) - D1 DT = 0.050000 HOURS END TIME = 0.0123 0.0170 24.000002 HOURS 0.0000 0.0039 0.0080 0.0218 0.0273 0.0350 0.0473 0.0605 0.0742 0.08910.1041 0.1196 0.2083 0.2329 0.1517 0.1883 0.1355 0.1696 0.2596 0.3361 1.4505 0.2955 0.3863 0.4532 0.8606 1.8235 2.0777 2.1833 2.2267 2.2595 2.2877 1.2070 1.7389 1.6425 1.8843 1.9326 2.2110 2.2460 2.2761 2.0339 2.1574 2.2163 2.2506 2.0573 2.1706 2.2216 2.2551 2.0966 1.9747 2.1136 2.1297 2.2054 2.2414 2.2720 2.1997 2.2367 2.2679 2.1938 2.2317 2.2637 2.2839 2.2915 2.2801 2.2952

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80912.81012.81122.81222.81322.8142281632.81732.81832.81932.82022.8212282322.82412.82512.82602.82702.8279282982.83072.83162.83252.83342.8344283612.83702.83792.83882.83962.8405284222.84312.84392.84472.84562.8464284802.84882.84962.85042.85122.8520285362.85432.85512.85592.85662.8574285382.85962.86032.86102.86172.8624286382.86452.86522.86592.86662.8672286382.86922.86992.87052.87112.8718287302.87762.87422.87482.87542.8760287722.87782.87832.87892.87552.8800288112.88162.88272.88272.8837288812.88862.88902.88952.88992.8903289122.89162.89202.89242.89282.8932289402.89442.89482.89512.89552.89582		153 222 289 352 414 472 528 581 631 679 724 766 806

\*Basin EXISTING

COMPUTE NM HYD ID=1 HYD NO=101 DA= .000606348 SQ MI

TP=-.170 MASSRAIN=-1

K = 0.092650HR TP = 0.170000HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428UNIT PEAK = 0.31911CFS UNIT VOLUME = 0.9655B = P60 = 1.8500526.28 AREA = 0.000103 SQ MIIA = 0.10000 INCHES INF = 0.04000INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000 K = 0.150918HRTP = 0.170000HR K/TP RATIO = 0.887754 SHAPE CONSTANT, N = 3.995652 UNIT PEAK = 1.0506 CFS UNIT VOLUME = 0.9888 <sup>т</sup>В = 354.88 P60 = 1.8500AREA = 0.000503 SO MIIA = 0.42410 INCHES INF = 1.03747INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT

= 0.050000

PRINT HYD ID=1 CODE=3

PARTIAL HYDROGRAPH 101.00 TIME FLOW TIME FLOW TIME FLOW TIME FLOW TIME FLOW HRS CFS HRS CFS HRS CFS HRS HRS CFS CFS 0.000 4.050 0.0 8.100 0.0 0.0 16.200 0.0 12.150 0.0 0.150 4.200 0.0 0.0 0.0 8.250 0.0 0.0 16.350 12.300 4.350 0.0 0.300 0.0 8.400 0.0 0.0 12.450 0.0 16.500 4.500 0.450 0.0 0.0 8.550 0.0 16.650 0.0 12,600 0.0 4.650 8.700 0.0 0.600 0.0 0.0

10 750	0.0		AH) 16.800	MO.OL	IT.		
12.750 0.750	0.0	0.0	4.800	0.0	0.0	8.850	0.0
12.900 0.900	0.0	0.0	16.950 4.950	0.0	0.0	9.000	0.0
13.050 1.050	0.0	0.0	17.100 5.100	0.0	0.0	9.150	0.0
13.200 1.200	0.0	0.0	17.250 5.250		0.0	9.300	0.0
13.350 1.350	0.0	0.2	17.400 5.400	0.0	0.0	9.450	0.0
13.500 1.500		1.0	17.550 5.550	0.0	0.0	9.600	0.0
13.650 1.650	0.0	0.9	17.700 5.700	0.0	0.0	9.750	0.0
13.800 1.800	0.0	0.4	17.850 5.850	0.0	0.0	9.900	0.0
13.950 1.950	0.0	0.2	18.000 6.000	0.0	0.0	10.050	0.0
14.100 2.100	0.0	0.1	18.150 6.150		0.0	10.200	0.0
14.250 2.250	.0.0	0.1	18.300 6.300	0.0	0.0	10.350	0.0
14.400 2.400	0.0	0.1	18.450 6.450	0.0	0.0	10.500	0.0
14.550 2.550	0.0	0.0	18.600 6.600	0.0	0.0	10.650	0.0
14.700 2.700	0.0	0.0	18.750 6.750	0.0	00	10.800	00
14.850 2.850	0.0	0.0	18.900 6.900	0.0	0.0	10.950	0.0
15.000 3.000	0.0	0.0	19.050 7.050	0.0	0.0	11.100	0.0
15.150 3.150	0.0	0.0	19.200 7.200	0.0	0.0	11.250	0.0
15.300 3.300	0.0	0.0	19.350 7.350	0.0	0.0	11.400	0.0
15.450 3.450	0.0	0.0	19.500 7.500	0.0	0.0	11.550	0.0
15.600 3.600	0.0	0.0	19.650 7.650	0.0	0.0	11.700	0.0
15.750 3.750	0.0	0.0	19.800 7.800	0.0	<b>O</b> <sub>60</sub> <b>. O</b> <sub>60</sub>	11.850	0.0
15.900 3.900	0.0	0.0	19.950 7.950	0.0	0.0	12.000	0.0

16.050 0.0

RUNOFF VOLUME = 1.25558 INCHES = 0.0406 ACRE-FEET PEAK DISCHARGE RATE = 1.07 CFS AT 1.550 HOURS BASIN AREA = 0.0006 SQ. MI.

\*Basin NORTH PROPOSED

COMPUTE NM HYD ID=2 HYD NO=102 DA= .000240796 SQ MI PER A=00 PER B=23 PER C=39 PER D=38

TP=-.170 MASSRAIN=-1

K = 0.092650 HR TP = 0.170000 HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428 UNIT PEAK = 0.28327 CFS UNIT VOLUME = 0.9587 B = P60 = 1.8500526.28 AREA = 0.000092 SQ MI IA = 0.10000 INCHES INF = 0.04000INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000 K = 0.146886HR TP = 0.170000HR K/TP RATIO = 0.864036 SHAPE CONSTANT, N = 4.113943 UNIT PEAK = 0.31852 CFS UNIT VOLUME = 0.9582 B = P60 = 1.8500362.70 0.000149 SQ MI IA = 0.40565 INCHES INF = 0.98581AREA =

INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=2 CODE=3

PARTIAL HYDROGRAPH 102.00 Page 5

AF	IYMO	.OUT
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TIME	FLO	W	TIME	F	LOW	TIME	FLOW
TIME FI	LOW CF	TIME	FLO HRS	OW	CFS	HRS	CFS
HRS 0.000	CFS 0	.0	c 3,900	FS	0.0	7.800	0.0
11.700 0.150	0.0	.0 .0	0 4.050	0.0	0.0	7.950	0.0
11.850 0.300	0.0	15.75	0 4.200	0.0	0.0	8.100	0.0
12.000 0.450	0.0	15.90	00 4.350	0.0	0.0	8.250	0.0
12.150 0.600			0 4.500		0.0	8.400	0.0
12.300 0.750		16.20		0.0	0.0	8.550	0.0
12.450 0.900			50 4.800	0.0	0.0	8.700	0.0
12.600 1.050		16.50	0 4.950		0.0	8.850	0.0
12.750 1.200	0_0	16.6	50 5.100	0.0	0.0	9.000	0.0
12.900 1.350			5.250		0.0	9.150	0.0
13.050 1.500		16.9	50		.0.0	9.300	0.0
13.200 1.650			)0 5.550	0.0		9.450	0.0
13.350 1.800	0.0		50 5.700			9.600	0.0
13.500 1.950		17.4	5.850	0.0		9,750	0.0
13.650	0.0	17.5	50	0.0	0.0		
2.100		).1 17.7	6.000 00	.0	00	9.900	0.0
2.250 13.950 2.400		).0 17.8	6.150 50 6.300	0.0	0.0	10.050	0.0
14,100				0.0	0.0	10.200	0.0
2.550	0.0		00 6.450 50	0.0	0.0	10.350	0.0
14.250 2.700 14.400	. (		6.600	0.0	0.0	10.500	<b>0</b> -1 <sub>0</sub> <b>-0</b> -1
2.850	0.0	0.0	00 6.750	0.0	0.0	10.650	0.0

			АНУ	MO.OL	JT		
14.550 3.000	0.0	0.0	18.450 6.900	0.0	0.0	10.800	0.0
14.700 3.150	0.0	0.0	18.600 7.050	0.0	0.0	10.950	0.0
14.850 3.300	0.0	0.0	18,750 7.200	0.0	0.0	11.100	0.0
15.000 3.450	0.0	0.0	18.900 7.350	0.0	0.0	11.250	0.0
15.150 3.600	0.0	0.0	19.050 7.500	0.0	0.0	11.400	0.0
15.300 3.750	0.0	0.0	7.650		0.0	11.550	0.0
15.450	0.0						

RUNOFF VOLUME = 1.62552 INCHES = 0.0209 ACRE-FEET PEAK DISCHARGE RATE = 0.50 CFS AT 1.550 HOURS BASIN AREA = 0.0002 SQ. MI.

\*Basin SOUTH PROPOSED

COMPUTE NM HYD	ID=3 HYD	NO=103 DA= .000365552 SQ MI
	PER A=00	PER B=10 PER C=25 PER D=65
	TP=170	MASSRAIN=-1

 $K = 0.092650HR \quad TP = 0.170000HR \quad K/TP \text{ RATIO} = 0.545000$ SHAPE CONSTANT, N = 7.106428 UNIT PEAK = 0.73557 CFS UNIT VOLUME = 0.9858 B = 526.28 P60 = 1.8500 AREA = 0.000238 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.144092HR TP = 0.170000HR K/TP RATIO = 0.847598
SHAPE CONSTANT, N = 4.200762

AHYMO.OUT UNIT PEAK = 0.27722 CFS UNIT VOLUME = 0.9548 B = 368.34 P60 = 1.8500AREA = 0.000128 SQ MI IA = 0.39286 INCHES INF = 0.95000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT

= 0.050000

PRINT HYD ID=3 CODE=3

		P	ARTIAL HYDROG	RAPH 103.00	
TIME	FLOW	TIME	FLOW	TIME	FLOW
TIME F HRS	LOW	TIME FL HRS	OW CFS	HRS	CFS
HRS 0.000	CFS 0.0	HRS C 4.800	FS 0.0	9.600	0.0
14.400 0.150	0.0	19.200 4.950	0.0	9.750	0.0
14.550 0.300	0.0	19.350 5.100	0.0	9.900	0.0
14.700 0.450	0.0	19.500 5.250	0.0	10.050	0.0
14.850 0.600	0.0	5.400	0.0	10.200	0.0
<b>15.000</b> 0.750	0.0	<b>19.800</b> 5.550	0.0	10.350	0.0
15.150 0.900	0.0	19.950 5.700	0.0	10.500	0.0
15.300 1.050	0.0	20.100 5.850	0.0	10.650	0.0
15.450 1.200	0.0 0.1	20.250 6.000	0.0	10.800	0.0
15.600 1.350	0.0	20.400 6.150	0.0	10.950	0.0
15.750 1.500	0.0	20.550 6.300	0.0	11.100	0.0
15.900 1.650	0.0	20.700 6.450	0.0	11.250	0.0
<b>16.050</b> 1.800	0.0	20.850 6.600	0.0	11.400	0.0
16.200 1.950	0.0	21.000 6.750	0.0	11.550	0.0
16.350 2.100	0.0	21.150 6.900	0.0	11.700	0.0

16.500	0.0		21,300	MO.OU 0.0			
16.500 2.250		0.1	7.050		0.0	11.850	0.0
16.650 2.400	0.0	0.0	21.450 7.200	0.0	0.0	12.000	0.0
16.800 2.550	0.0	0.0	21.600 7.350	0.0	0.0	12.150	0.0
16.950 2.700	0.0	0.0	21.750 7.500	0.0	0.0	12.300	0.0
17.100 2.850	0.0	0.0	21.900 7.650	0.0	0.0	12.450	0.0
17.250 3.000	0.0	0.0	22.050 7 <b>.8</b> 00		0.0	12.600	0.0
17.400 3.150	0.0	0.0	22.200 7.950	0.0	0.0	12.750	0.0
17.550 3.300	0.0	0.0	22.350 8.100	0.0	0.0	12.900	0.0
<b>17.700</b> 3.450		0.0	<b>22.500</b> 8.250	-0.0	0.0	13.050	0.0
17.850 3.600	0.0	0.0	22.650 <u>8.400</u>	0.0	0.0	13.200	0.0
18.000 3.750	0.0	0.0	22.800 8.550	0.0	0.0	13.350	0.0
18.150 3.900	0.0	0.0	22.950 8.700		0.0	13.500	0.0
18.300 4.050	0.0	0,0	23.100 8.850		0.0	13.650	0.0
18.450 4.200	0.0	0.0	23.250 9.000			13.800	0.0
18.600 4.350	0.0	0.0	23.400 9.150	0.0	0.0	13.950	0.0
<b>18.750</b> 4.500	0.0	0.0	23.550 9.300	0.0	0.0	14.100	0.0
18.900 4.650	0.0	0.0	23.700 9.450	0.0	0.0	14.250	0.0
19.050	0.0						
RUNOFF	VOLUM		2.07762 INCH	ES	=	0.0405 ACRE-FEE	T

PEAK DISCHARGE RATE = 0.85 CFS AT 1.550 HOURS BASIN AREA = 0.0004 SQ. MI.

AHYMO.OUT. \* ROUTE THE TOTAL FLOW THROUGH THE PROPOSED RESERVOIR

ROUTE RESERVOIR	ID=4 HYD NO=	104 INFLOW=3	CODE=3		
	OUTFLOW(CES)	STORAGE (AC-FT)	ELEV(FT)		
	0.00	0.001	74.00		
	0.86	0.028	74.50		
	1.09	0.051	75.00		

*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
	TIM (HR				FLO FS)			LEV FEE				UME - FT			TFL FS)	OW
	0. 0. 0. 0. 0. 0. 0. 1. 1. 1. 1. 2. 2. 2. 3. 3. 3.	150 3450 79050 5680 91050 5050 5050 5050 5050 5050 5050 50				00002450376281852111111		744.7744.77744.77744.77744.77744.77744.77744.77744.77744.77744.77744.77744.77744.77744.77744.77744.77744.77744.77744.777744.777777	00 00 00 00 00 00 00 00 00 00 00 00 00			.00 .00 .00 .00 .00 .00 .00 .00 .00 .00	111111223844208654322222			00 00 00 00 00 00 00 00 00 00 00 00 00
	33. 34. 44. 4	60 75 90 05 20 35 <b>50</b>		-9	0.0	11111111		74. 74. 74. 74. 74. 74.	01 01 00 00 00 00		000000000000000000000000000000000000000	.00 .00 .00 .00 .00 .00	1 1 1 1 1 1		0. 0. 0. 0. 0.	01 01 01 01 01 01
	4. 4. 5. 5. 5. 5.	80 95 10 25 40 55			0.0 0.0 0.0 0.0 0.0 0.0 0.0	1     1     1     1     1     1     1     1		74. 74. 74. 74. 74. 74. 74.	00 00 00 00 00 00		000000000000000000000000000000000000000	.00 .00 .00 .00 .00 .00 .00	1 1 1 1 1		0. 0. 0. 0. 0. 0.	01 01 01 01 01 01

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	74.00	AHYMO.OUT 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001	$\begin{array}{c} 0.01\\$	
8.55 $0.01$ $74.00$ $0.001$ $0.01$ $8.70$ $0.01$ $74.00$ $0.001$ $0.01$ $9.00$ $0.01$ $74.00$ $0.001$ $0.01$ $9.15$ $0.01$ $74.00$ $0.001$ $0.01$ $9.15$ $0.01$ $74.00$ $0.001$ $0.01$ $9.30$ $0.01$ $74.00$ $0.001$ $0.01$ $9.45$ $0.01$ $74.00$ $0.001$ $0.01$ $9.60$ $0.01$ $74.00$ $0.001$ $0.01$ $9.75$ $0.01$ $74.00$ $0.001$ $0.01$ $9.90$ $0.01$ $74.00$ $0.001$ $0.01$ $9.90$ $0.01$ $74.00$ $0.001$ $0.01$ $10.20$ $0.01$ $74.00$ $0.001$ $0.01$ $10.50$ $0.01$ $74.00$ $0.001$ $0.01$ $10.50$ $0.01$ $74.00$ $0.001$ $0.01$ $10.80$ $0.01$ $74.00$ $0.001$ $0.01$ $11.10$ $0.01$ $74.00$ $0.001$ $0.01$ $11.10$ $0.01$ $74.00$ $0.001$ $0.01$ $11.55$ $0.01$ $74.00$ $0.001$ $0.01$ $11.85$ $0.01$ $74.00$ $0.001$ $0.01$ $11.85$ $0.01$ $74.00$ $0.001$ $0.01$ $11.20$ $0.01$ $74.00$ $0.001$ $0.01$ $11.230$ $0.00$ $74.00$ $0.001$ $0.01$ $12.45$ $0.00$ $74.00$ $0.001$ $0.01$					
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	74.00 7	0.001 0.001	0.01 0.001 0.001 0.	1.75

### 0.050000HRS

\*TOTAL PROPOSED

ADD HYD

ID=5 HYD NO=105 ID I=2 ID II=4

PRINT HYD ID=5 CODE=3

ATEN	11.60	× 0	11.11	<b>-</b>
AH.	YMC		U. I	

				PARTI	EAL HYD	ROGRAPH 105.00	
TIME	1	FLOW	TIME	F	LOW	TIME	FLOW
TIME F HRS	LOW	CFS	TIME F HRS		CFS	HRS	CFS
HRS 0.000	CFS	0.0	HRS 4.800	CFS	0.0	9.600	0.0
14.400 0.150	0.0	0.0	19.200 4.950	0.0	0.0	9.750	0.0
14.550 0.300	0.0	0.0	19.350 5.100	0.0	0.0	9.900	0.0
14.700 0.450	0.0	0.0	19.500 5.250	0.0	0.0	10.050	0.0
14.850 0.600	0.0	0.0	19.650 5.400	0.0	0.0	10.200	0.0
15.000 0.750	0.0	0.0	<b>19.800</b> 5.550	0.0	0.0	10.350	0.0
15.150 0.900	0.0	0.0	19.950 5.700	0.0	00	10.500	0.0
15.300 1.050	0.0	0.0	20.100 5.850	0.0	0.0	10.650	0.0
15.450 1.200	0.0	0.1	20.250 6.000	0.0	0.0	10.800	0.0
15.600 1.350	0.0	0.2	20.400 6.150	0.0	0.0	10.950	0.0
15.750 1.500	0.0	0.7	20.550 6.300	0.0	0.0	11.100	0.0
15.900 1.650	0.0	0.8	20.700 6.450	0.0	0.0	11.250	0.0
16.050 1.800	0.0	0.6	20.850 6.600	0.0	0.0	11.400	0.0
16.200 1.950	0.0	0.5	21.000 6.750	0.0	00	11.550	0.0
16.350 2.100	0.0	0.3	21.150 6.900	0.0	0.0	11.700	0.0
16.500 2.250	0.0	0.3	21.300 7.050	0.0	0.0	11.850	0.0
16.650 2.400	0.0	0.2	21.450 7.200	0.0	0.0	12.000	0.0
16.800 2.550	0.0	0.1	21.600 7.350	0.0	0.0	12.150	0.0
16.950 2.700	0.0	0.1	21.750 7.500	0.0	0.0	12.300	0.0

AHYMO.OUT 17.100 0.0 21.900 0.0										
17.100 2.850	0.0	0.1	7.650	0.0	0.0	12.450	0.0			
17.250 3.000	0.0	0.1	22.050 7.800	0.0	0.0	12.600	0.0			
17.400 3.150			22.200 7.950	0.0	0.0	12.750	0.0			
17.550 3.300	0.0	0.0	22.350 8.100	0.0	0.0	12.900	0.0			
17.700 3.450	0.0	0.0	22.500 8.250	0.0	0.0	13.050	0.0			
17.850 3.600	0.0	0.0	22.650 8.400			13.200	0.0			
18.000 3.750	0.0	0.0	22.800 8.550	0.0	.0.0	13.350	0.0			
18.150 3.900	0.0	0.0	22.950 8.700	0.0	0.0	13.500	0.0			
<b>18.300</b> 4.050	0.0	0.0	23.100 8.850	0.0	0.0	13.650	0.0			
18.450 4.200	0.0	0.0	23.250 9.000	0.0	0.0	13.800	0.0			
18.600 4.350	0.0	0.0	23.400 9.150	0.0	0.0	13.950	0.0			
18.750 4.500	0.0	0.0	23.550 9.300	0.0	0.0	14.100	0.0			
18.900 4.650	0.0	0.0	23.700 9.450	0.0	0.0	14.250	0.0			
19.050	0.0		23.850	0.0						

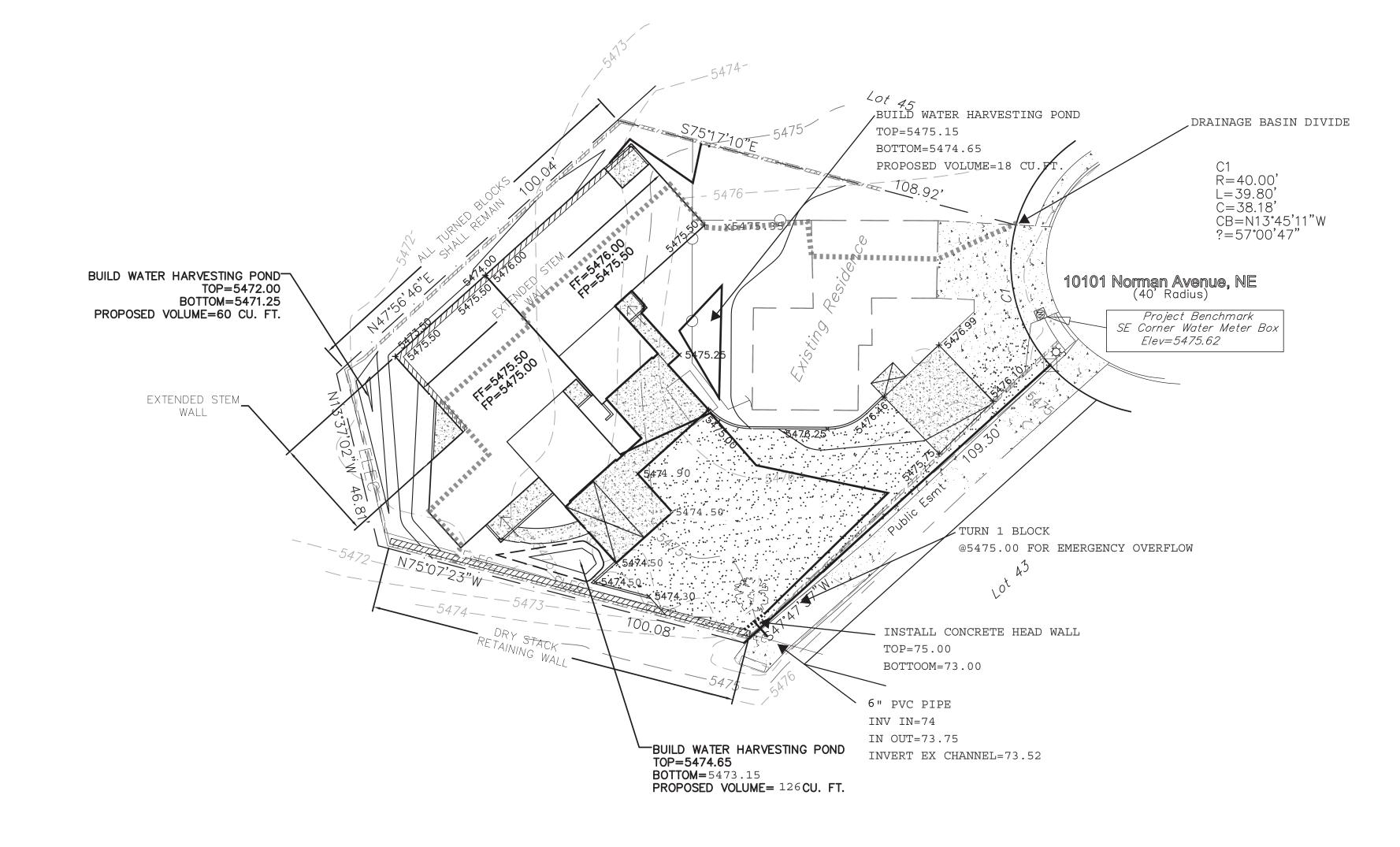
RUNOFF VOLUME = 1.88736 INCHES = 0.0610 ACRE-FEET PEAK DISCHARGE RATE = 0.82 CFS AT 1.600 HOURS BASIN AREA = 0.0006 SQ. MI.

FINISH

NORMAL PROGRAM FINISH

END TIME (HR:MIN:SEC) = 17:00:38

...



CAUTION: EXISTING UTILITIES ARE NOT SHOWN. IT SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR TO CONDUCT ALL NECESSARY FIELD INVESTIGATIONS PRIOR TO ANY EXCAVATION TO DETERMINE THE ACTUAL LOCATION OF UTILITIES & OTHER

IMPROVEMENTS.

EROSION CONTROL NOTES: PERMIT PRIOR TO BEGINNING WORK.

2. CONTRACTOR IS RESPONSIBLE FOR MAINTAINING RUN-OFF ON SITE DURING CONSTRUCTION.

3. CONTRACTOR IS RESPONSIBLE FOR CLEANING ALL SEDIMENT THAT GETS INTO EXISTING RIGHT-OF-WAY.

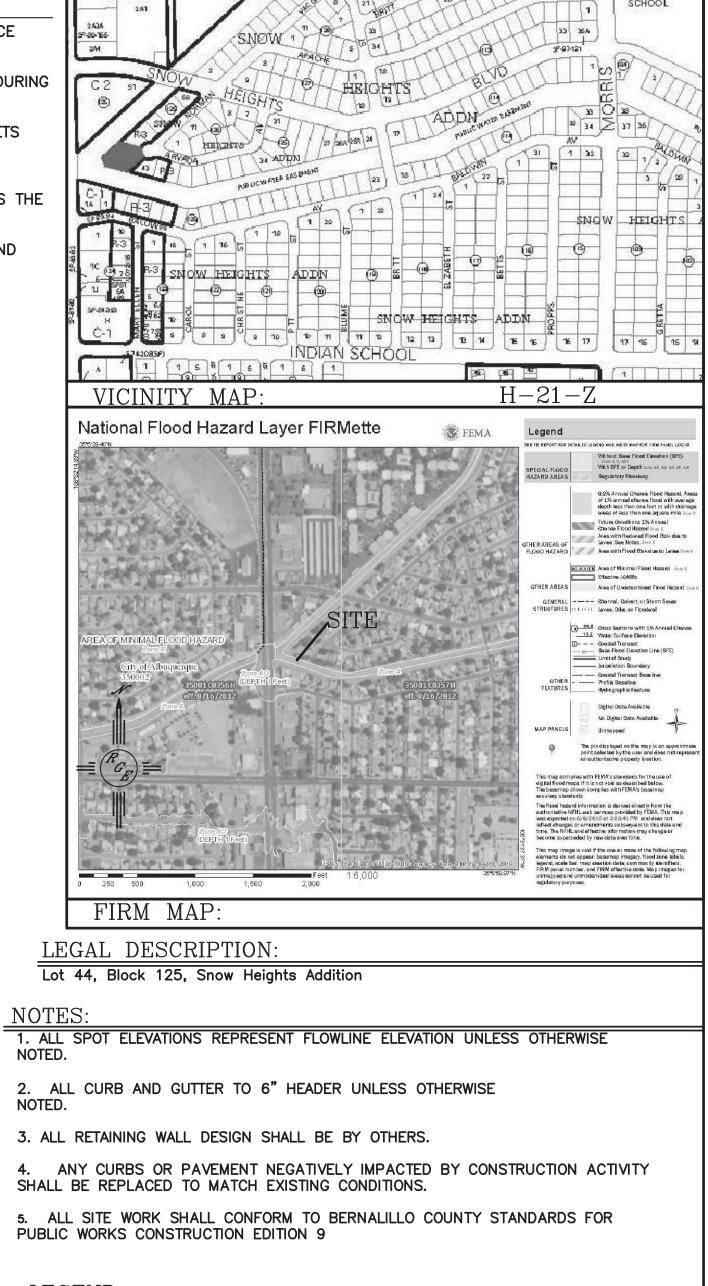
4. REPAIR OF DAMAGED FACILITIES AND CLEANUP OF SEDIMENT ACCUMULATIONS ON ADJACENT PROPERTIES AND IN PUBLIC FACILITIES IS THE RESPONSIBILITY OF THE CONTRACTOR.

5. ALL EXPOSED EARTH SURFACES MUST BE PROTECTED FROM WIND AND WATER EROSION PRIOR TO FINAL ACCEPTANCE OF ANY PROJECT.



1. CONTRACTOR IS RESPONSIBLE FOR OBTAINING A TOPSOIL DISTURBANCE

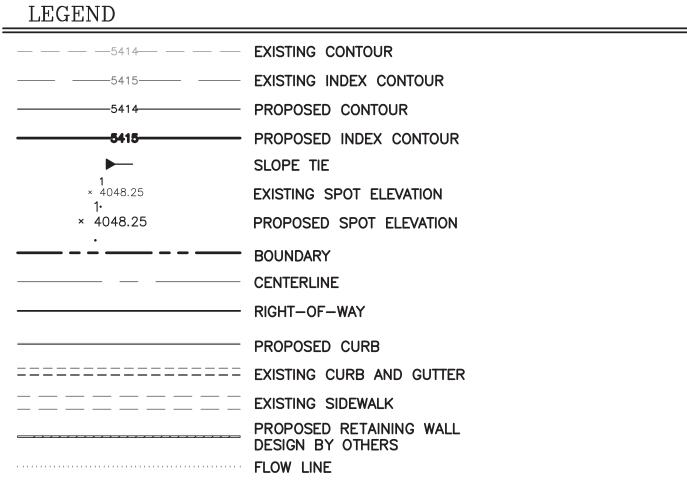
9-18357

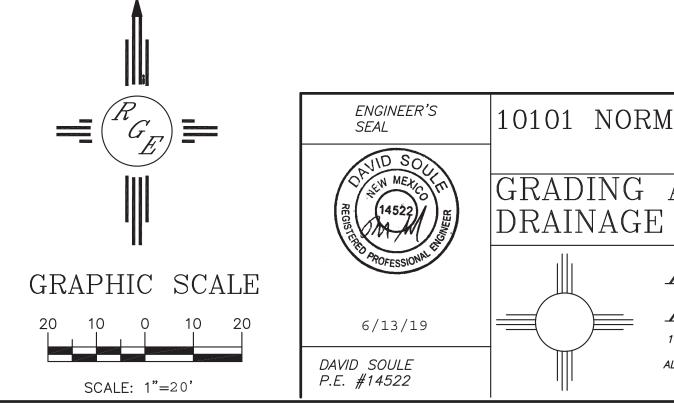


ELEMENTARY

SCHOOL

ADDN





DRAWN 10101 NORMAN <sup>BY</sup> WCWJ DATE 6-11-19 GRADING AND DRAINAGE PLAN 2109054-LAYOUT-6-11-19 SHEET # Rio Grande Engineering 1606 CENTRAL AVENUE SE SUITE 201 ALBUQUERQUE, NM 87106 (505) 872–0999 JOB # 2109054