

CITY OF ALBUQUERQUE



June 28, 2017

Farshad Omidvaran, P.E.
Parsons Brinkerhoff
6100 Uptown Blvd NE
Albuquerque, NM 87110

RE: **ABQ Ride Daytona Transit Facility**
Grading and Drainage Plan (Engineer's Stamp Date: 6/28/17)
Hydrology File: J09D025

Dear Mr. Omidvaran:

Based on the information provided in your submittal received on 6/28/2017, the Grading and Pavement Plan Sheet C-7 with engineer's stamp dated 6/28/2017 and the Proposed Storm Drain Plan Sheet C-9 with engineer's stamp dated 6/14/2017 are approved for Building Permit.

PO Box 1293

The following inconsistencies were noted during the review of the HGL calculations.

Albuquerque

New Mexico 87103

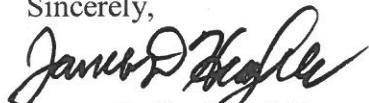
www.cabq.gov

1. HEC-22 (2nd ed) was used which incorrectly applied losses directly to the HGL without calculating the EGL. The COA DPM 22.3.B requires the use of Bernoulli's equation and several other minor losses. If the HEC-22 (3rd Ed) option is used in the current version of StormCAD, the results will be consistent with the DPM. This will increase the HGL at the upstream end by about 3' so the HGL will be more than a foot out of the ground there.
2. Several things can be done to lower the HGL.
 - a. Starting with a lower tail-water elevation. The DPM allows use of the 10-year elevation of Pond 6 to account for the difference in timing of the peak stage in the pond and the peak flow in the pipe. That elevation is not known but it may be assumed to be at least 1' below the crest elevation of the emergency overflow spillway which is at 5182.6. So a reasonable starting elevation would be 5181.6.(1.4' lower)
 - b. The peak flow rate in Daytona Street can be reduced to 195.86 cfs per Amole Hubble DMP (0.9' less HL)
 - c. The onsite peak flow rate can be reduced to 80 cfs since about 20% of basin U201 goes to a different storm drain.

When all of these changes are combined the resulting HGL will probably be below the surface, so the design will be in compliance with City Code 14-5-2-12(G).

If you have any questions, please contact me at 924-3986 or jhughes@cabq.gov.

Sincerely,



James D. Hughes, P.E.

Principal Engineer, Planning Dept.
Development Review Services



City of Albuquerque

Planning Department
Development & Building Services Division

DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 11/2016)

Project Title: ABQ Ride Daytona Design **Building Permit #:** BP-2017-19346 **Hydrology File #:** J09D025

DRB#: _____ **EPC#:** _____ **Work Order#:** _____

Legal Description: Lot A, West Side Transit Facility

City Address: 8001 Daytona Road NW, Albuquerque, NM 87121

Applicant: Daytona Transit Facility (COA) **Contact:** Nolan Meadows

Address: 8001 Daytona Place, NM, Albuquerque, NM 87121

Phone#: 505-239-9924 **Fax#:** _____ **E-mail:** nmeadows@cabq.gov

Other Contact: WSP|Parsons Brinckerhoff **Contact:** Jim Buckman

Address: 6100 Uptown Blvd. NE Suite 600, Albuquerque, NM 87110

Phone#: 505-878-6577 **Fax#:** _____ **E-mail:** Buckman@pbworld.com

Check all that Apply:

DEPARTMENT:

HYDROLOGY/ DRAINAGE
 TRAFFIC/ TRANSPORTATION

TYPE OF SUBMITTAL:

ENGINEER/ARCHITECT CERTIFICATION

CONCEPTUAL G & D PLAN

GRADING PLAN

DRAINAGE MASTER PLAN

DRAINAGE REPORT

CLOMR/LOMR

TRAFFIC CIRCULATION LAYOUT (TCL)

TRAFFIC IMPACT STUDY (TIS)

OTHER (SPECIFY) _____

PRE-DESIGN MEETING?

TYPE OF APPROVAL/ACCEPTANCE SOUGHT:

BUILDING PERMIT APPROVAL

CERTIFICATE OF OCCUPANCY

PRELIMINARY PLAT APPROVAL

SITE PLAN FOR SUB'D APPROVAL

SITE PLAN FOR BLDG. PERMIT APPROVAL

FINAL PLAT APPROVAL

SIA/ RELEASE OF FINANCIAL GUARANTEE

FOUNDATION PERMIT APPROVAL

GRADING PERMIT APPROVAL

SO-19 APPROVAL

PAVING PERMIT APPROVAL

GRADING/ PAD CERTIFICATION

WORK ORDER APPROVAL

CLOMR/LOMR

IS THIS A RESUBMITTAL?: Yes No

OTHER (SPECIFY) _____

DATE SUBMITTED: 07/03/2017

By: *Lanham O'Neal* for Jim Buckman

COA STAFF:

ELECTRONIC SUBMITTAL RECEIVED: _____

FEE PAID: _____



June 30, 2017

James Hughes, PE
Principal Engineer, Planning Dept.
Development Review SErvices
City of Albuquerque
PO Box 1293
Albuquerque, NM 87103

Re: ABQ Ride Daytona Transit Facility
Grading and Drainage Plan
Hydrology File J09D025

Dear Mr. Hughes:

We have addressed the comments provided in your letters dated June 26 and June 28, 2017. We disagree that the current storm drain layout will not provide for adequate drainage for the site. Our responses are listed below.

1. The depressed landscape areas are being built per the construction plans, sheet C-6, attached, and sheet C-11, which was provided with the original submittal.
2. Wall details are included for your reference, sheets S-1 and S-4, showing turned blocks to pass drainage.
3. A memo describing the drainage analysis for the site is attached, for your review. This includes the information requested, per the City of Albuquerque DPM Chapter 22.
4. The stormwater treatment system is designed to treat 25 cfs. This flow rate was determined in coordination with DMD and ABQ Ride staff, and approximately represents a 1-year storm. The "Stormwater Pollution Prevention Plan for the Daytona Maintenance Facility" (September 2015) recommends to "Select and evaluate the appropriate storm water control or combination of controls (treatment train) to improve storm water quality." The proposed system meets this requirement. Typical details from three manufacturers are attached.

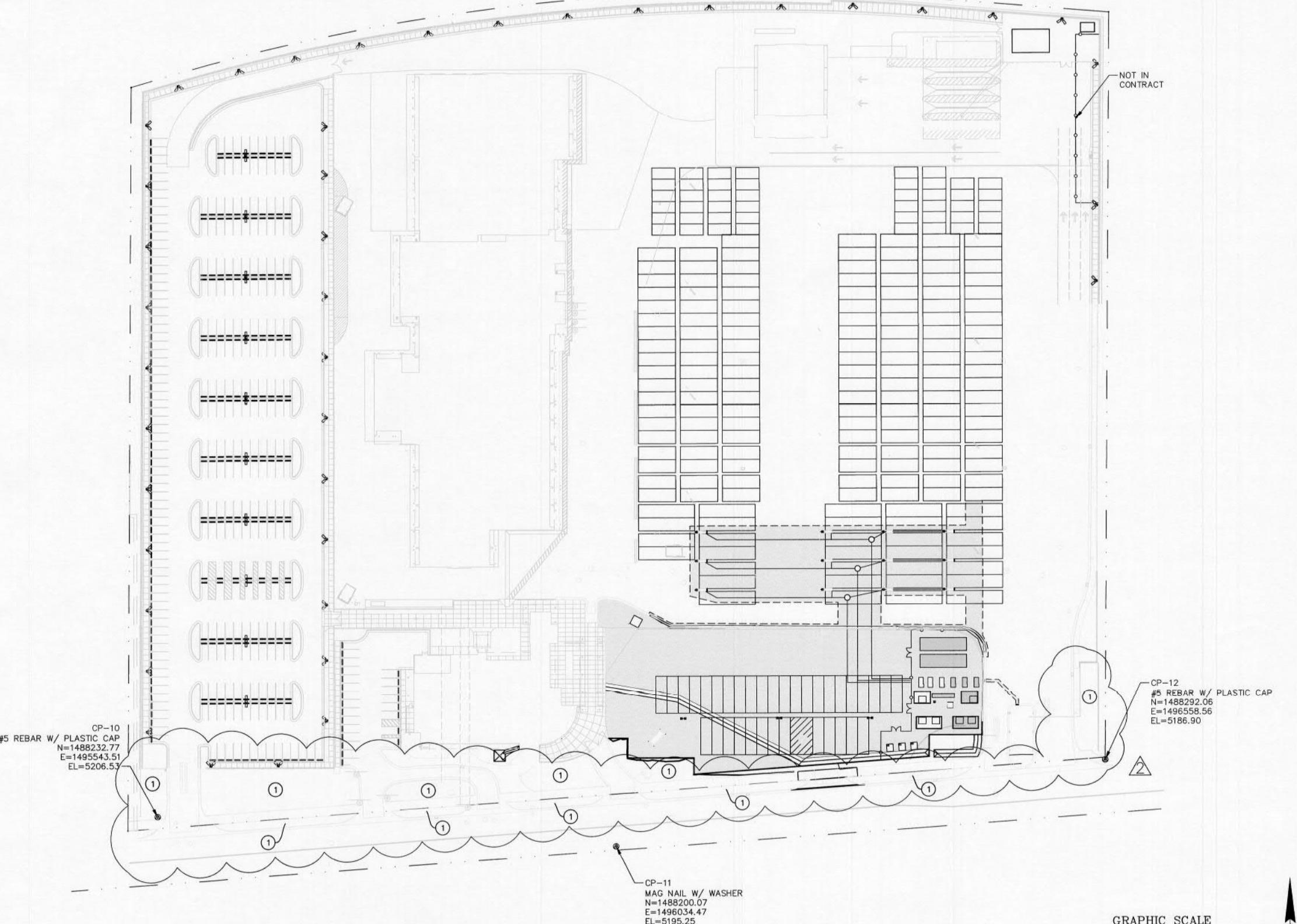
Kind regards,

Jim Buckman, PE

Attachments
cc: Bruce Rizzieri
Nolan Meadows

WSP USA
Suite 700
6100 Uptown Boulevard NE
Albuquerque, NM 87110

Tel.: +1 505 881-5357
Fax: +1 505 881-7602
wsp.com



LEGEND		AS BUILT INFORMATION	
	PROPOSED PAVED AREA		PROPOSED SAW CUT LINE
	PROPOSED VALLEY GUTTER		PROPOSED CHAIN LINK FENCE
	PROPOSED DOUBLE GATES		PROPOSED CMU WALL
	PROPOSED PARKING SPACE STRIPING		PROPOSED ELECTRICAL CHARGING STATION
	LUMINARE		KEYED NOTES:
			1. GRADE LANDSCAPE AREA PER DETAILS ON SHEET C-11.
		BENCH MARKS	
		FIELD NOTES "TRIMBLE VRSNOW RTK NETWORK" WITH CHECKS	
		NO.	BY DATE TO NES CONTROL STATION "NGS Q 424"
		JB	
SURVEY INFORMATION		ENGINEER'S SEAL	
FIELD NOTES		AR	
6/13/17 SITE CONFIGURATION CHANGE		6/28/17 SITE CONFIGURATION CHANGE	
LANDSCAPE GRADING NOTES		LANDSCAPE GRADING NOTES	
NO. DATE		NO. DATE	
REMARKS		REMARKS	
BY		BY	
DESIGNED BY: PB		DESIGNED BY: PB	
DRAWN BY: PB		DRAWN BY: PB	
CHECKED BY: PB		CHECKED BY: PB	
NO. DATE		NO. DATE	
REMARKS		REMARKS	
BY		BY	
CITY OF ALBUQUERQUE		CITY OF ALBUQUERQUE	
TRANSIT DEPARTMENT		TRANSIT DEPARTMENT	
ABQ RIDE		ABQ RIDE	
ABQ RIDE DAYTONA DESIGN		ABQ RIDE DAYTONA DESIGN	
SITE PLAN			
DESIGN REVIEW COMMITTEE	CITY ENGINEER APPROVAL	MO./DAY/YR.	MO./DAY/YR.
Parsons Brinckerhoff			
ABQ RIDE			
CITY OF ALBUQUERQUE			
TRANSIT DEPARTMENT			
ABQ RIDE			
ABQ RIDE DAYTONA DESIGN			
SITE PLAN			
City Project No.	Zone Map No.	Sheet	
COA 5658.05	J-09-Z	C-6	

JAMES H. BUCKMAN
NEW MEXICO
13062
REGISTERED PROFESSIONAL ENGINEER
S-73-11

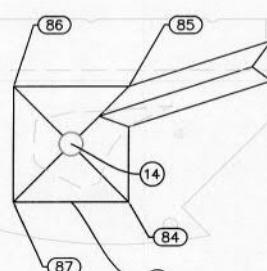
KEYED NOTES:

1. SAW CUT LINE
2. CONCRETE CHARGING STATION ISLAND, SEE DETAIL SHEET C-10.
3. LANDSCAPE AREA, SEE DETAIL SHEET C-11 FOR GRADING TYPICAL.
4. WALL SEE SHEETS S-1 AND S-2.
5. PAVED AREA SEE PAVEMENT SECTION ON DETAIL SHEET C-10.
6. 6' DOUBLE GATE SEE COA STANDARD DWG. 2252.
7. 6' CHAIN LINK FENCE SEE COA STANDARD DWG. 2252.
8. VALLEY GUTTER "TYPE I", SEE SHEET C-10.
9. 4" U SHAPED BOLLARD, SEE DETAIL SHEET C-10.
10. VALLEY GUTTER "TYPE II" SEE DETAIL SHEET C-10.
11. BOLLARD, SEE COA STANDARD DWG. 2370.
12. PROPOSED SIDEWALK SEE COA STANDARD DWG. 2430.
13. PROPOSED CURB AND GUTTER SEE COA STANDARD DWG. 2451A.
14. REMOVE EXISTING GRATE AND REPLACE WITH BEEHIVE GRATE AND FRAME, SEE SHEET C-10.
15. 4" CONCRETE SIDEWALK APRON, SLOPE TO DRAIN.
16. 6" TALL HEADER CURB, SEE COA DWG. 2415, COST INCIDENTAL TO VALLEY GUTTER.



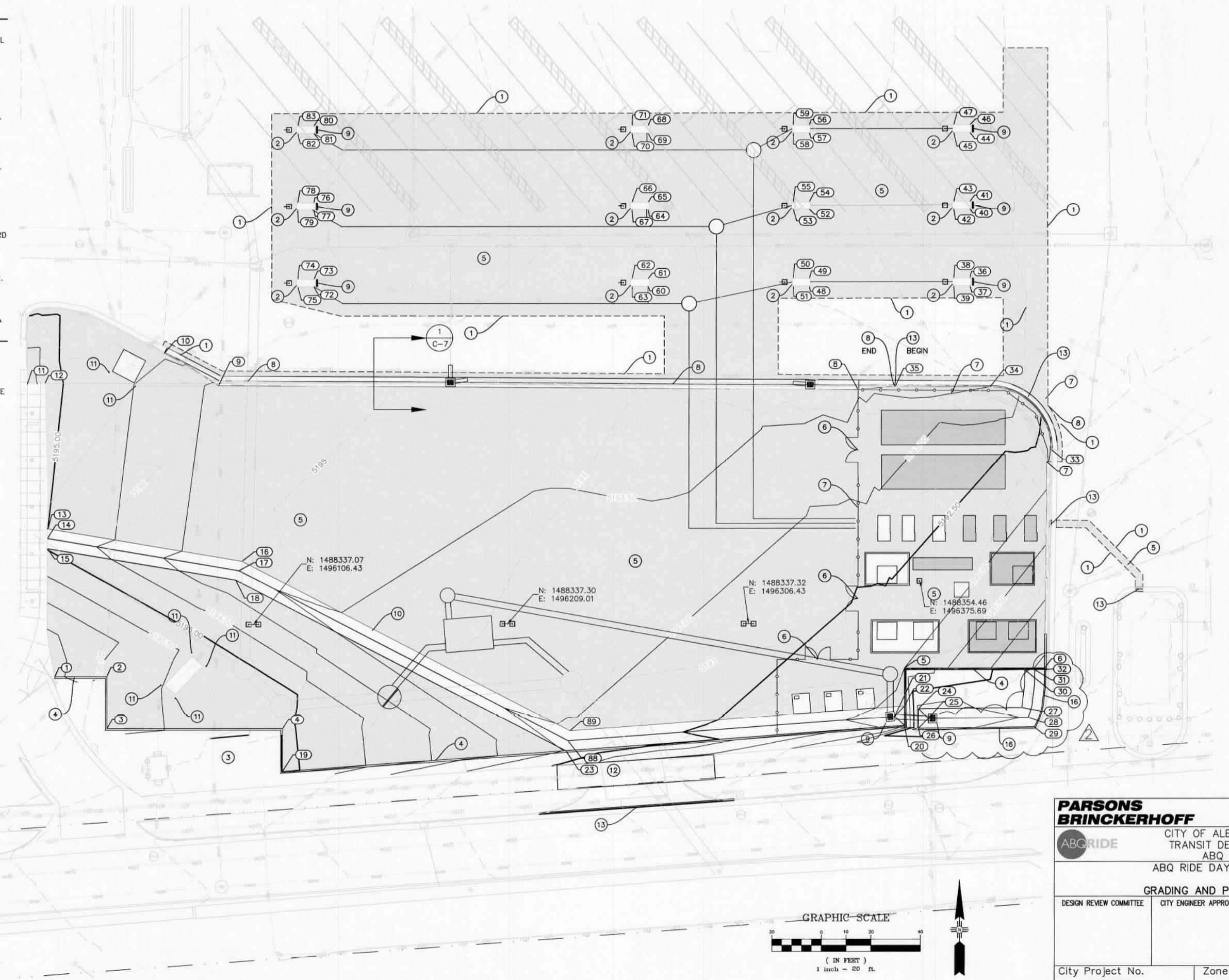
KEYED NOTES:

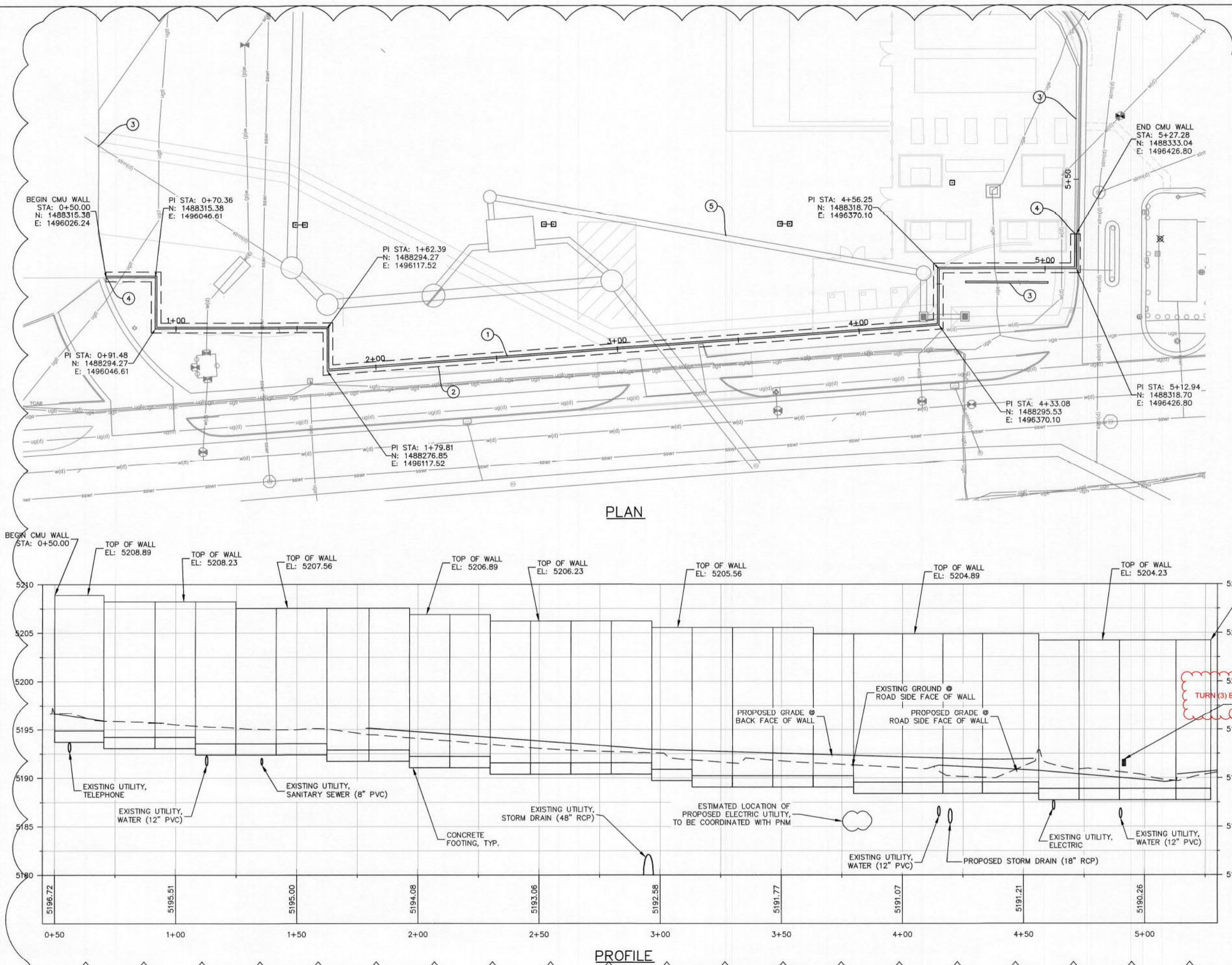
- LIGHT, SEE SHEET E-300.
- LOCATION OF FUTURE ELECTRICAL PAD, TO BE ASPHALT PAVED
- ELECTRICAL PAD
- NEW PAVED AREA
- MAJOR CONTOUR (0.5' INTERVAL)
- MINOR CONTOUR (0.5' INTERVAL)
- - - EXISTING MAJOR CONTOUR (1' INTERVAL)
- - - EXISTING MINOR CONTOUR (1' INTERVAL)



CONCRETE DRAIN DETAIL

SCALE: 1"=10'





KEYED NOTES:

- ① NEW CMU WALL, SEE SHEET S2 FOR DETAILS.
- ② NEW CONCRETE FOOTING, SEE SHEET S2 FOR DETAILS.
- ③ EXISTING CMU WALL TO REMAIN IN PLACE.
- ④ TIE NEW CMU WALL TO EXISTING PILASTER.
- ⑤ PROPOSED STORM DRAIN, SEE CIVIL DRAWINGS

GENERAL NOTES:

1. THE CONTRACTOR SHALL VERIFY EXISTING UTILITY LOCATIONS, INCLUDING DEPTHS, PRIOR TO CONSTRUCTION AND SHALL NOTIFY THE PROJECT MANAGER OF ANY CONFLICTS.

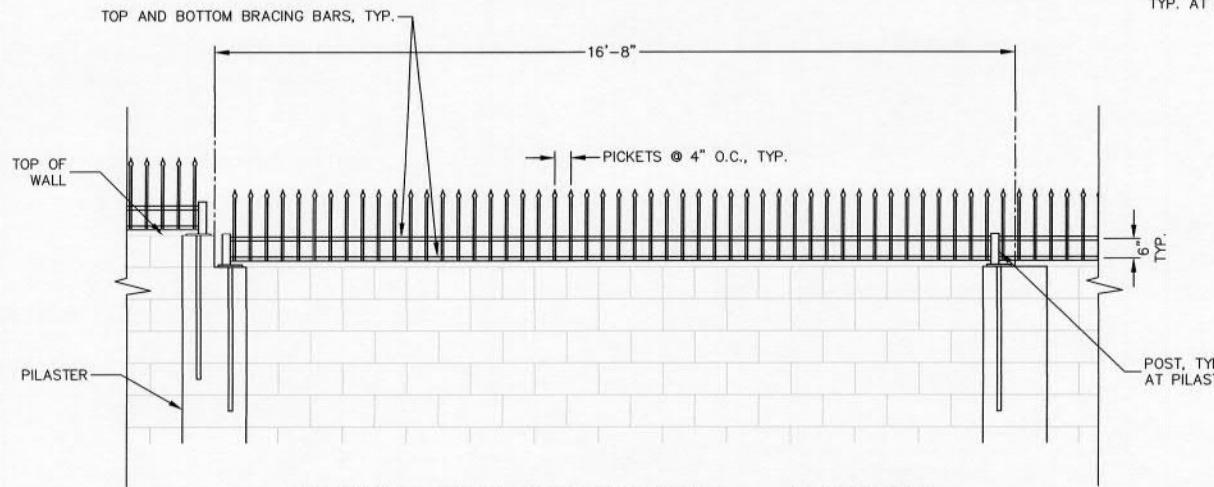
**PARSONS
BRINCKERHOFF**

OF ALBUQUERQUE
SIT DEPARTMENT
ABQ RIDE
E DAYTONA DESIGN

III. PLAN & PROFILE

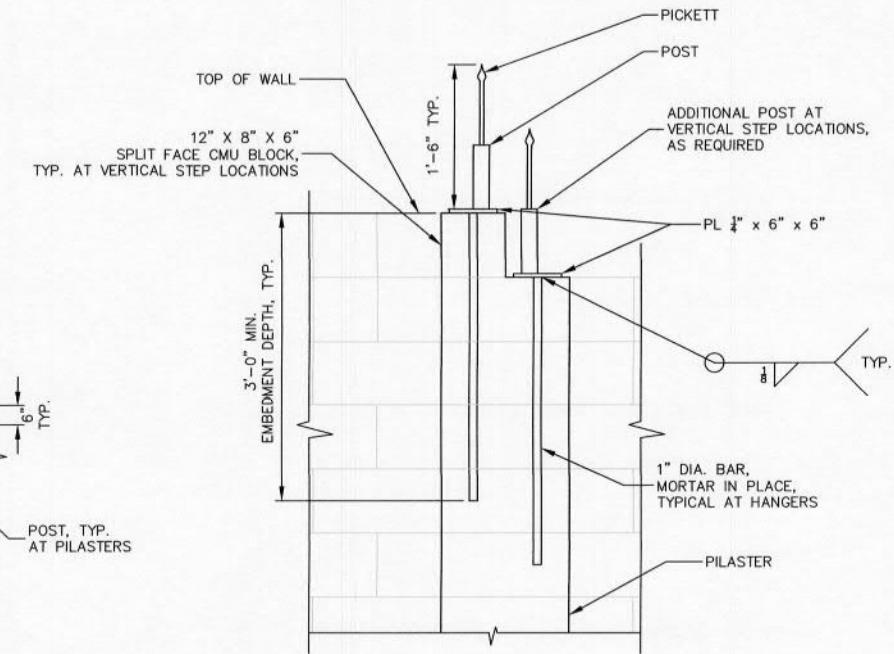
WALL I CAN & PROFILE		MO./DAY/YR.	MO./DAY/YR.
DESIGN REVIEW COMMITTEE	CITY ENGINEER APPROVAL		

City Project No. Zone Map No. Sheet



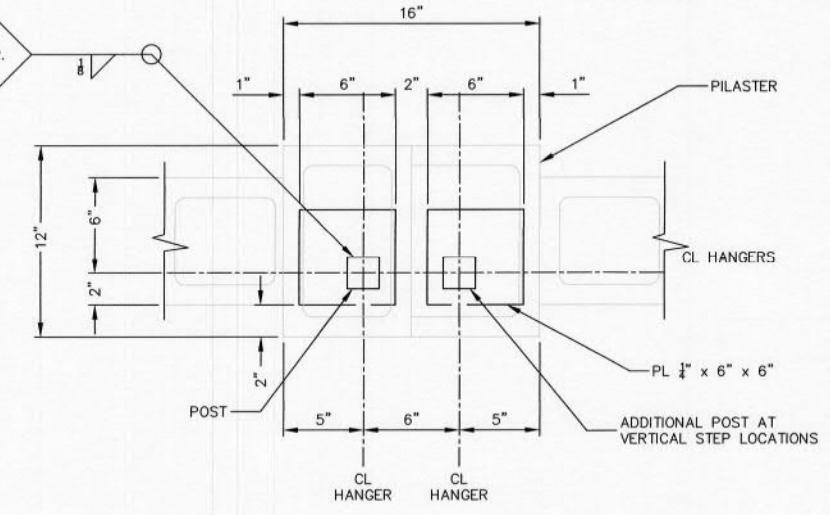
WROUGHT IRON TOPPING DETAIL ~ ELEVATION

SCALE: N.T.



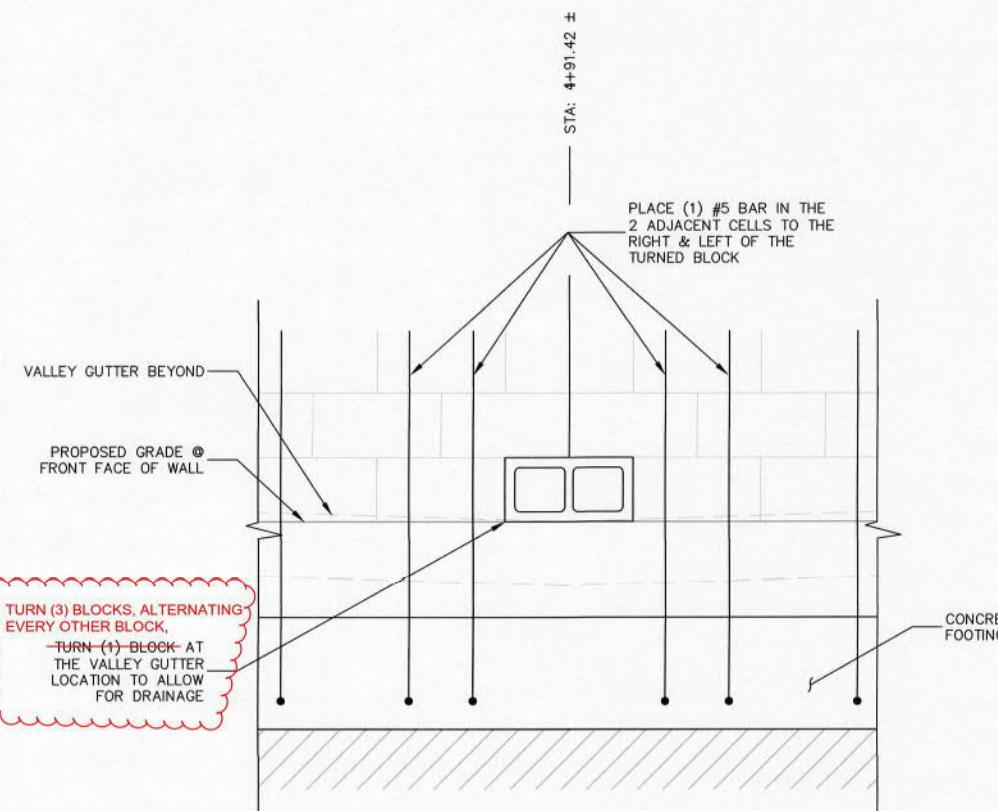
TOPPING INSTALLATION AT PILASTERS ~ SECTION

SCALE: N.T.S.



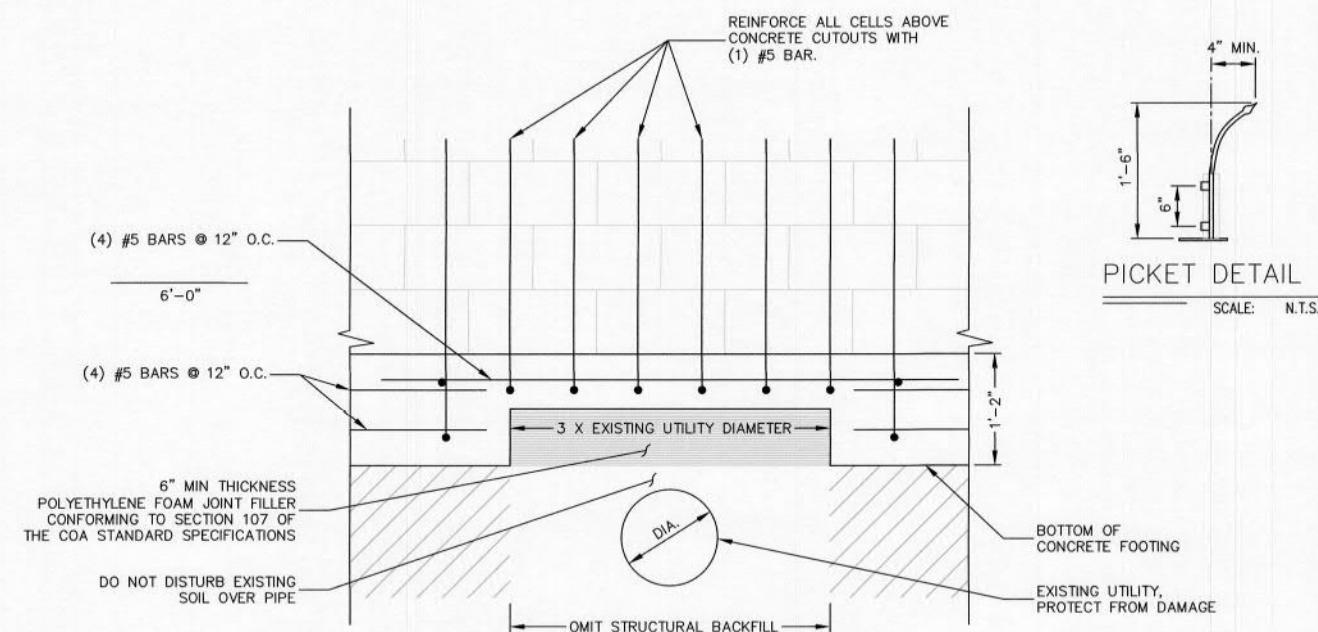
TOPPING PLACEMENT DETAIL ~ PLAN

SCALE: NTS



TURNED BLOCK AT VALLEY GUTTER ~ ELEVATION

SCALE: N.



CONCRETE CUTOUT AT UTILITIES ~ SECTION

SCALE: N.T.S.

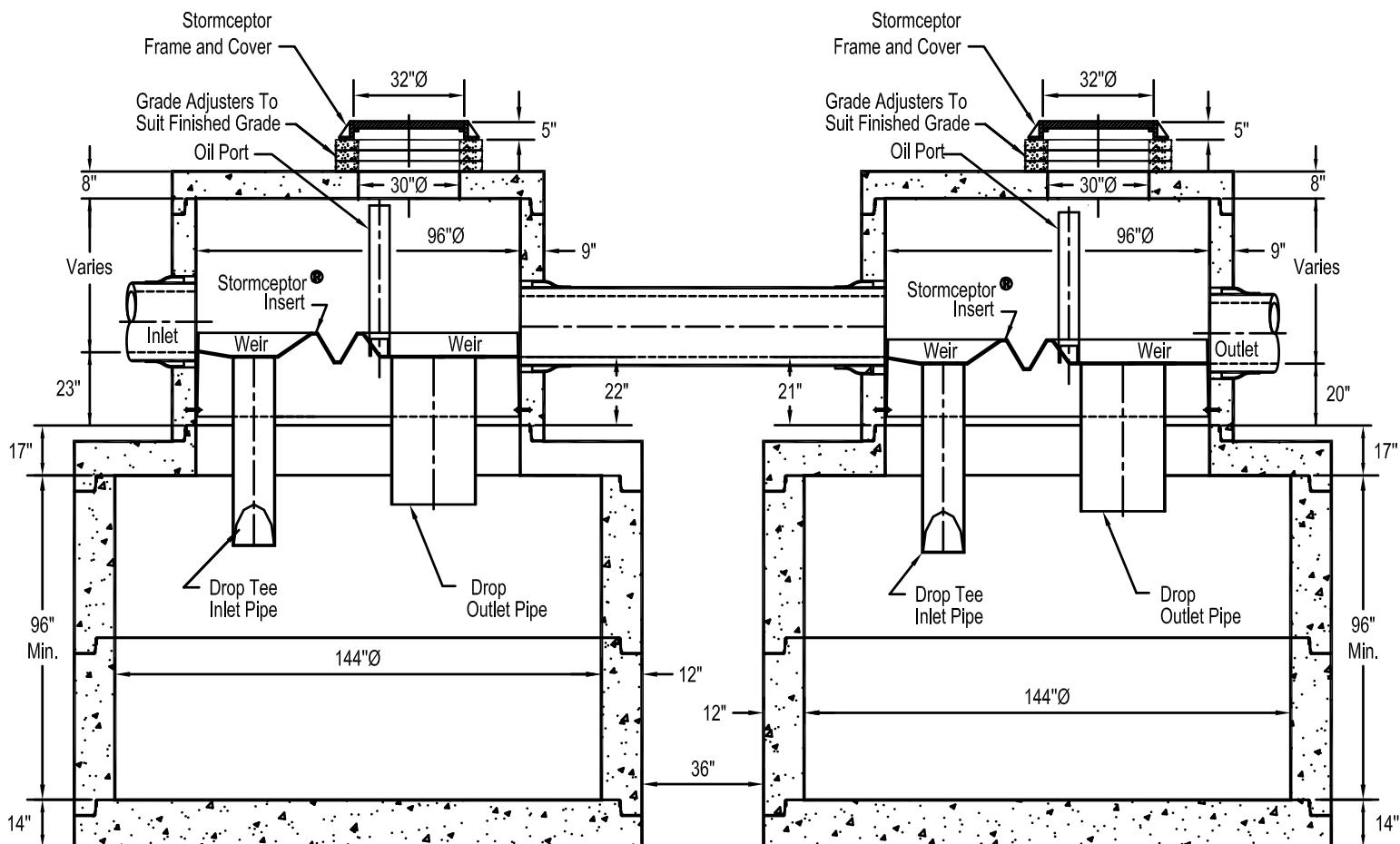
**PARSONS
BRINCKERHOFF**

CITY OF ALBUQUERQUE
TRANSIT DEPARTMENT
ABQ RIDE

WALL DETAILS

WALL DETAILS		MO./DAY/YR.	MO./DAY/YR.
DESIGN REVIEW COMMITTEE	CITY ENGINEER APPROVAL		

**STC 16000s Precast Concrete Stormceptor®
(16000 U.S. Gallon Capacity)**



Section Thru Chambers

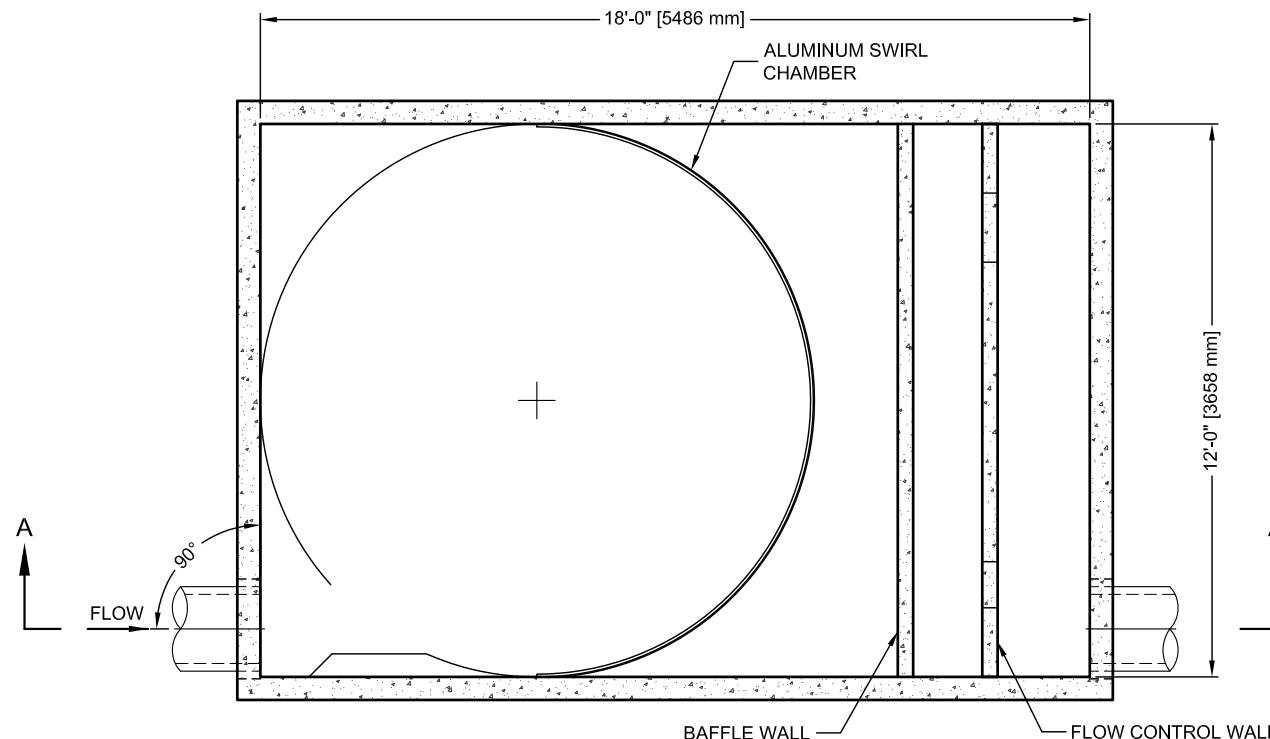
Notes:

1. The Use Of Flexible Connection is Recommended at The Inlet and Outlet Where Applicable.
2. The Cover Should be Positioned Over The Outlet Drop Pipe and The Oil Port.
3. The Stormceptor System is protected by one or more of the following U.S. Patents:
#5753115, #5849181, #6068765, #6371690, #7582216, #7666303.
4. Contact a Concrete Pipe Division representative for further details not listed on this drawing.

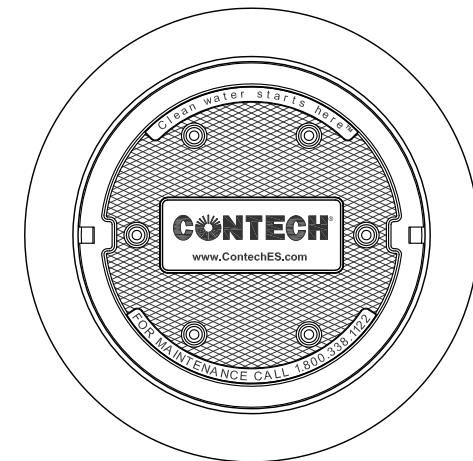
VORTECHS 16000 DESIGN NOTES

VORTECHS 16000 RATED TREATMENT CAPACITY IS 25 CFS, OR PER LOCAL REGULATIONS. IF THE SITE CONDITIONS EXCEED RATED TREATMENT CAPACITY, AN UPSTREAM BYPASS STRUCTURE IS REQUIRED.

THE STANDARD INLET/OUTLET CONFIGURATION IS SHOWN. FOR OTHER CONFIGURATION OPTIONS, PLEASE CONTACT YOUR CONTECH CONSTRUCTION PRODUCTS REPRESENTATIVE. www.ContechES.com

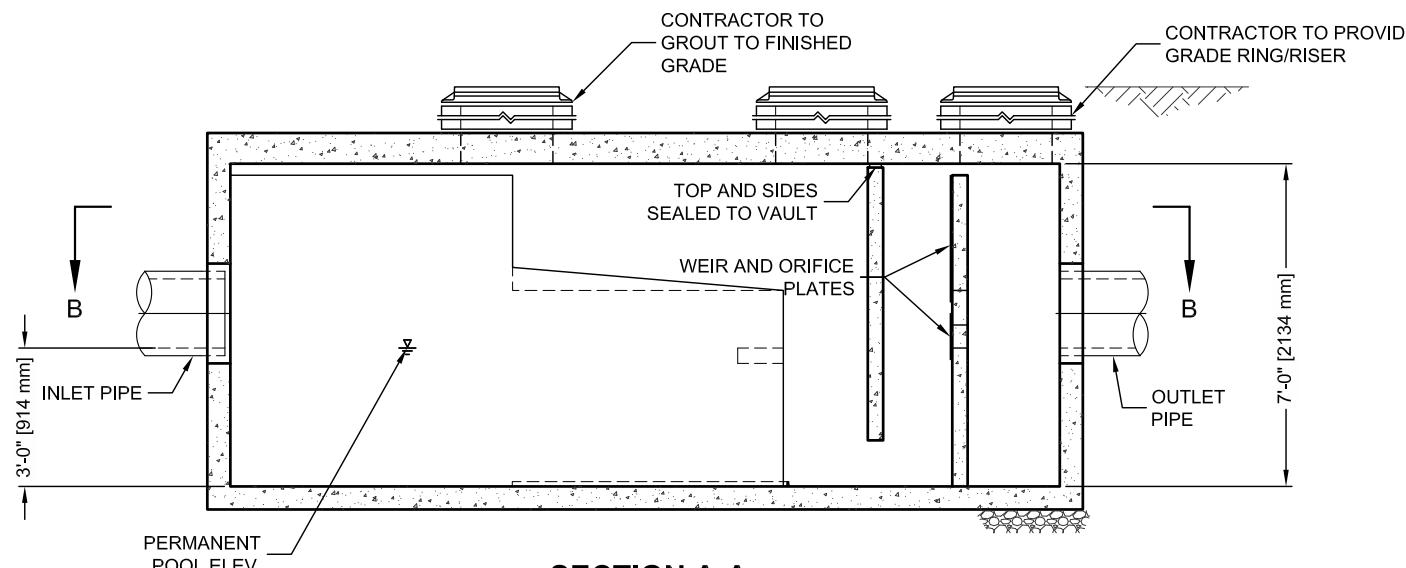


SECTION B-B



FRAME AND COVER
(DIAMETER VARIES)
N.T.S.

SITE SPECIFIC DATA REQUIREMENTS			
STRUCTURE ID	*		
WATER QUALITY FLOW RATE (CFS)	*		
PEAK FLOW RATE (CFS)	*		
RETURN PERIOD OF PEAK FLOW (YRS)	*		
PIPE DATA: I.E.	MATERIAL	DIAMETER	
INLET PIPE 1	*	*	*
INLET PIPE 2	*	*	*
OUTLET PIPE	*	*	*
RIM ELEVATION			*
ANTI-FLOTATION BALLAST	WIDTH	HEIGHT	
	*	*	
NOTES/SPECIAL REQUIREMENTS:			
* PER ENGINEER OF RECORD			



SECTION A-A

GENERAL NOTES

1. CONTECH TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERWISE.
2. DIMENSIONS MARKED WITH () ARE REFERENCE DIMENSIONS. ACTUAL DIMENSIONS MAY VARY.
3. FOR FABRICATION DRAWINGS WITH DETAILED STRUCTURE DIMENSIONS AND WEIGHT, PLEASE CONTACT YOUR CONTECH ENGINEERED SOLUTIONS LLC REPRESENTATIVE. www.ContechES.com
4. VORTECHS WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS DRAWING.
5. STRUCTURE SHALL MEET AASHTO HS20 AND CASTINGS SHALL MEET AASHTO M306 LOAD RATING, ASSUMING GROUNDWATER ELEVATION AT, OR BELOW, THE OUTLET PIPE INVERT ELEVATION. ENGINEER OF RECORD TO CONFIRM ACTUAL GROUNDWATER ELEVATION.
6. INLET PIPE(S) MUST BE PERPENDICULAR TO THE VAULT AND AT THE CORNER TO INTRODUCE THE FLOW TANGENTIALLY TO THE SWIRL CHAMBER. DUAL INLETS NOT TO HAVE OPPOND TANGENTIAL FLOW DIRECTIONS.
7. OUTLET PIPE(S) MUST BE DOWN STREAM OF THE FLOW CONTROL BAFFLE AND MAY BE LOCATED ON THE SIDE OR END OF THE VAULT. THE FLOW CONTROL WALL MAY BE TURNED TO ACCOMODATE OUTLET PIPE KNOCKOUTS ON THE SIDE OF THE VAULT.

INSTALLATION NOTES

- A. ANY SUB-BASE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
- B. CONTRACTOR TO PROVIDE EQUIPMENT WITH SUFFICIENT LIFTING AND REACH CAPACITY TO LIFT AND SET THE VORTECHS STRUCTURE (LIFTING CLUTCHES PROVIDED).
- C. CONTRACTOR TO INSTALL JOINT SEALANT BETWEEN ALL STRUCTURE SECTIONS AND ASSEMBLE STRUCTURE.
- D. CONTRACTOR TO PROVIDE, INSTALL, AND GROUT PIPES. MATCH PIPE INVERTS WITH ELEVATIONS SHOWN.
- E. CONTRACTOR TO TAKE APPROPRIATE MEASURES TO ASSURE UNIT IS WATER TIGHT, HOLDING WATER TO FLOWLINE INVERT MINIMUM. IT IS SUGGESTED THAT ALL JOINTS BELOW PIPE INVERTS ARE GROUTED.

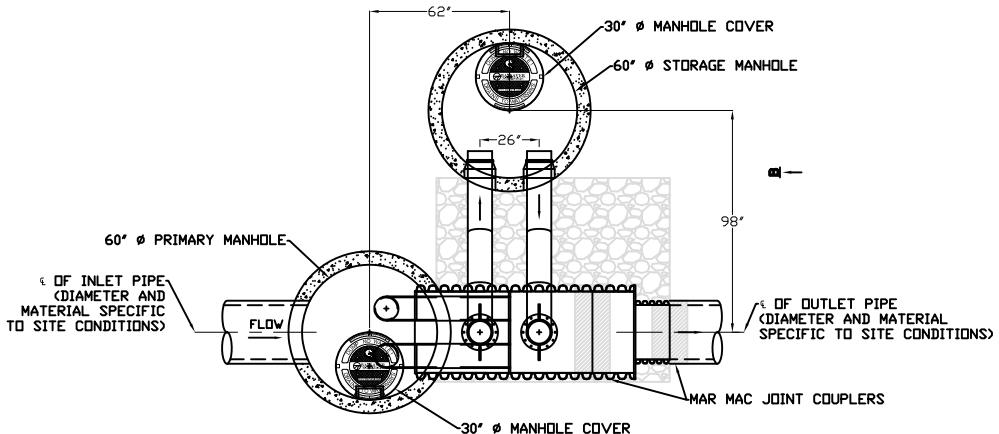


THIS PRODUCT MAY BE PROTECTED BY THE FOLLOWING
U.S. PATENT: 5,759,415; RELATED FOREIGN PATENTS.

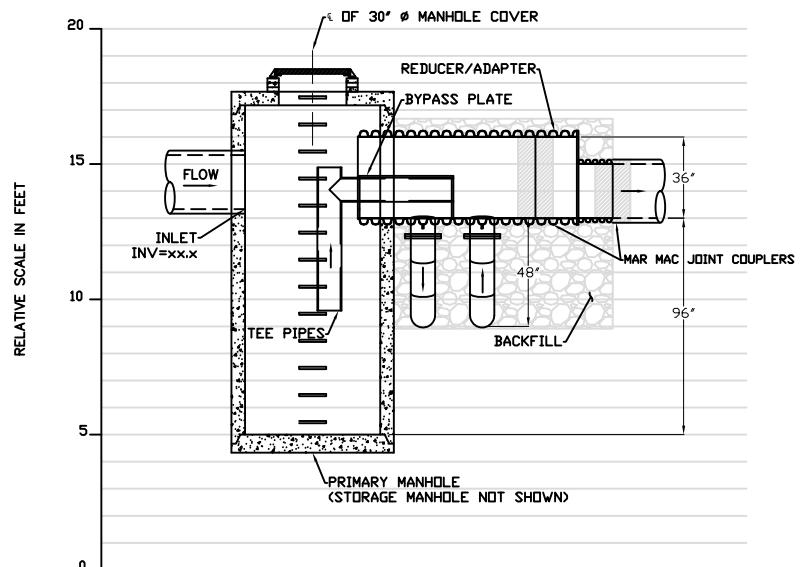
CONTECH
ENGINEERED SOLUTIONS LLC
www.ContechES.com

9025 Centre Pointe Dr., Suite 400, West Chester, OH 45069
800-338-1122 513-645-7000 513-645-7993 FAX

**VORTECHS 16000
STANDARD DETAIL**



PLAN VIEW-BAYSAVER SEPARATION SYSTEM
(LEFT HAND ORIENTATION SHOWN)

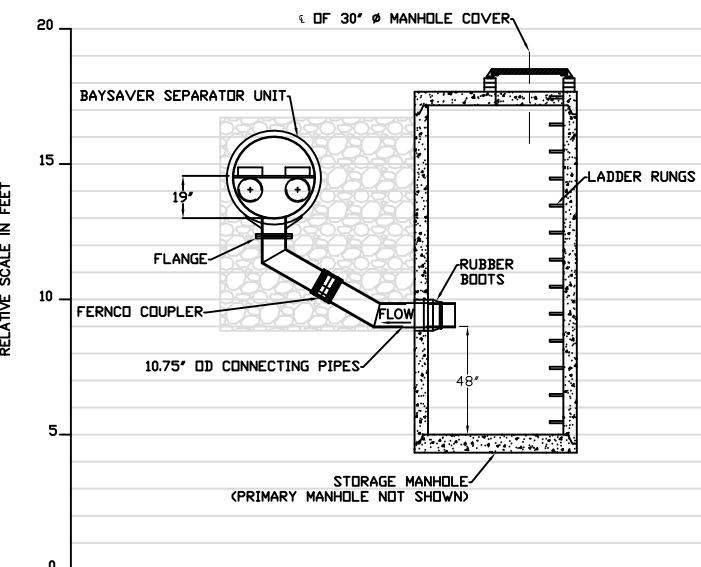


PROFILE VIEW A-A

INLET PIPE INVERT:	xxx
INLET PIPE ID AND MATERIAL:	xxx
OUTLET PIPE INVERT:	xxx
OUTLET PIPE ID AND MATERIAL:	xxx
PRIMARY MANHOLE RIM ELEVATION:	xxx
STORAGE MANHOLE RIM ELEVATION:	xxx
ORIENTATION (RIGHT OR LEFT):	

GENERAL NOTES:

1. MANHOLES SHOWN REPRESENT STANDARD PRECAST STRUCTURES PROVIDED BY OTHERS.
2. SEAL THE CONNECTING PIPES INTO THE STORAGE MANHOLE USING RUBBER BOOTS/GASKETS.
3. THE BAYSAVER SEPARATION SYSTEM INCLUDES THE SEPARATOR UNIT, (2) CONNECTING PIPES, (2) FERNCO COUPLERS, (1) REDUCER ADAPTER, AND (2) MARMAC JOINT COUPLERS.
4. LEFT HAND ORIENTATION SHOWN. FOR RIGHT HAND ORIENTATION ROTATE STORAGE MANHOLE AND CONNECTING PIPES 180°.
5. SEE BAYSAVER SPECIFICATIONS AND INSTALLATION INSTRUCTIONS FOR FURTHER DETAIL.
6. USE NON-SHRINK GROUT TO SEAL THE INLET PIPE AND BAYSEPARATOR IN TO THE PRIMARY MANHOLE.
7. BACKFILL: CLASS I, II OR III BACKFILL SHOULD BE USED TO AN ELEVATION OF AT LEAST 6' OVER THE CROWN OF THE SEPARATOR UNIT.
8. 12' COVER REQUIRED FOR TRAFFIC RATED SURFACE.
9. BAYSEPARATOR IS PROTECTED BY US PATENT NO. 5,746,911



PROFILE VIEW B-B

REV	DESCRIPTION	DATE	APPR	NOTES:



**BAYSAVER
TECHNOLOGIES**
800-229-7283
WWW.BAYSAVER.COM

DESIGNED: TEP	DATE: 5/28/15
DRAWN: EKH	SCALE: N.T.S.
CHECKED: PR	DWG NO: 3K

**3K BAYSEPARATOR™
SYSTEM DETAILS**



MEMO

TO: ABQ Ride

FROM: Farshad Omidvaran, PE

SUBJECT: Daytona Transit Facility, Grading and Drainage, Hydrologic and Hydraulic Analysis, Project #5658.05

DATE: June 30, 2017

INTRODUCTION

WSP was selected by the City of Albuquerque (CoA) ABQ Ride to design improvements to the Daytona Transit Facility as part of City of Albuquerque project 5685.05. A vicinity map for the project area can been seen in Exhibit 1 which has been included as an attachment to this memo. The purpose of the project is to upgrade the site so that it can accommodate electric bus services. For the most part, the site is developed. As part of this project, an unpaved portion of the site, located along the southern border of the property will be regraded and developed.

HYDROLOGY

On-Site

WSP was unable to find the original drainage report for the site and used DPM Chapter 22, Hydrology to estimate the flows generated within the site as follows.

Total area of the site: 19.63 acres. Presently 1.25 acres of this site is unpaved; however, under the proposed conditions the entire site will be paved. Assume land treatment D for the entire site.

The site is in precipitation Zone 1, and since the area is less than 40 acres, Table A-9 (DPM) was used to estimate the Peak Discharge.

Total Site: $Q_{100} = 19.63 * 4.37 = 85.8 \text{ cfs}$

WSP USA
Suite 700
6100 Uptown Boulevard NE
Albuquerque, NM 87110

Tel.: +1 505 881-5357
Fax: +1 505 881-7602
wsp.com



The undeveloped portion of the site: Area = 1.25 acres, all land treatment D, Q100 = 5.5 cfs

The portion of the site that contributes to the openings in the proposed wall:
Area = 0.35 acres, all land treatment D. Q100 = 1.5 cfs

Off-Site Daytona Road Storm Drain System

The "I-40 South and Unser Mini Drainage Management Plan" (I-40 DMP), prepared by Easterling Consultants, dated April 2014, the "Master Drainage Plan for the West Side Transit Facility" (WSTF), prepared by Smith Engineering, dated 2001, and the Amole Hubbell Drainage Master Plan Update (Amole Hubbell) by Wilson, dated May 2013 were used to evaluate the effect of the proposed improvements to the existing downstream storm drain and pond facilities.

Historically, the runoff from the north side of I-40 drained south through tributaries of the Mirehaven Arroyo and reached Daytona Road. However, with the construction of the I-40 diversion channel along the north side of I-40, the offsite flows from north of I-40 are now diverted to the east. The WSTF analysis, which was used for the design and construction of the existing storm drain system under Daytona Road and its downstream ponds, was modeled under the assumption that the land within the contributory drainage basins south of I-40 is fully developed, and the developed basins north of I-40 still drain to the south. The WSTF analysis used the AHYMO computer program. The I-40 DMP reanalyzed the downstream capacity of the ponds based on the assumption that there would be no off-site flow from north of I-40, and that the watershed land use has changed to a commercial/light industrial area as opposed to the medium-high density residential area that was assumed in the WSTF analysis and design.

The key findings from the reports are described below.

I-40 DMP:

Plate 1, Existing Conditions Drainage Basin Map with HEC-HMS Input and Output Summary, April 2014 from the I-40 South and Unser Diversion Mini DMP (copy attached) shows a routed flow at the outfall of the Daytona Storm Drain system of 82.8 cfs. This map identifies the discharge into Pond 6 as AP-3.

WSTF Analysis and Design

The as-built plans for the West Side Transit Facility Phase I, Sheet 18 of 61, show a flow of 243 cfs in the 60" diameter RCP at the outfall of the Daytona Road trunk line into Pond 6.



Amole-Hubbell DMP:

The Amole-Hubbell DMP indicates that a flow of 196 cfs reaches Pond 6 at the outfall of the Daytona Road storm drain trunk line.

A 100-year flow of 260 cfs at the outlet of the Daytona Road storm drain trunk line was used as a conservative basis for the hydraulic analysis.

HYDRAULICS

See the construction plans for COA Project 5658.05, Daytona Operations and Maintenance Facility, prepared by WSP, June 2017 for the proposed improvements to the unpaved portion of the site. The improvements consist of: 1) two valley gutters directing the flows from the new parking area to two drop inlets at the southeast corner of the site; and 2) a 24" diameter RCP carrying the flow from these inlets west to the existing 48" diameter RCP trunk line, via a new stormwater treatment system (STS). To avoid overwhelming the STS, it will be off-line from the existing trunk. A new manhole with a diversion weir will direct part of the flow in the existing 48" diameter RCP to the new STS. High flows will continue to the east in the existing 48" diameter RCP. The diversion weir and STS will be designed to treat a total of approximately 25 cfs.

The eastern part of the property drains towards the east and is directed toward 3 turned blocks in the proposed perimeter wall. From there, valley gutter will carry the flow to a Type D drop inlet with a modified grate. Calculations to show the openings and valley gutter/rundown capacity are included as an attachment to this memo.

A StormCAD model was developed (printouts attached) to ensure that the backwater from the existing storm drain system under Daytona Road does not overflow the storm drain and inlets. A total flow of 260 cfs was used to analyze the trunk line under Daytona Road. The tailwater elevation at the pipe outlet to Pond 6 was set at elevation 5183.2. This elevation was assumed conservatively as the top of the outlet pipe plus a head loss of one times the velocity head. This water surface elevation is above the top of the pond riser, which is at elevation 5181.40.

For the proposed manhole with the diversion weir, the losses for a submerged weir were added to the model. Since StormCAD does not calculate split flow networks, the hydraulic grade lines (HGL's) for the two pipe branches were calculated, and the flows were adjusted until the HGL's converged at the manhole with the diversion weir. The attached StormCAD printouts show the split in the system at MH 3; MH-3A represents the flow through the Stormceptor and MH-3B shows the remainder of the flow through the existing system. MH-

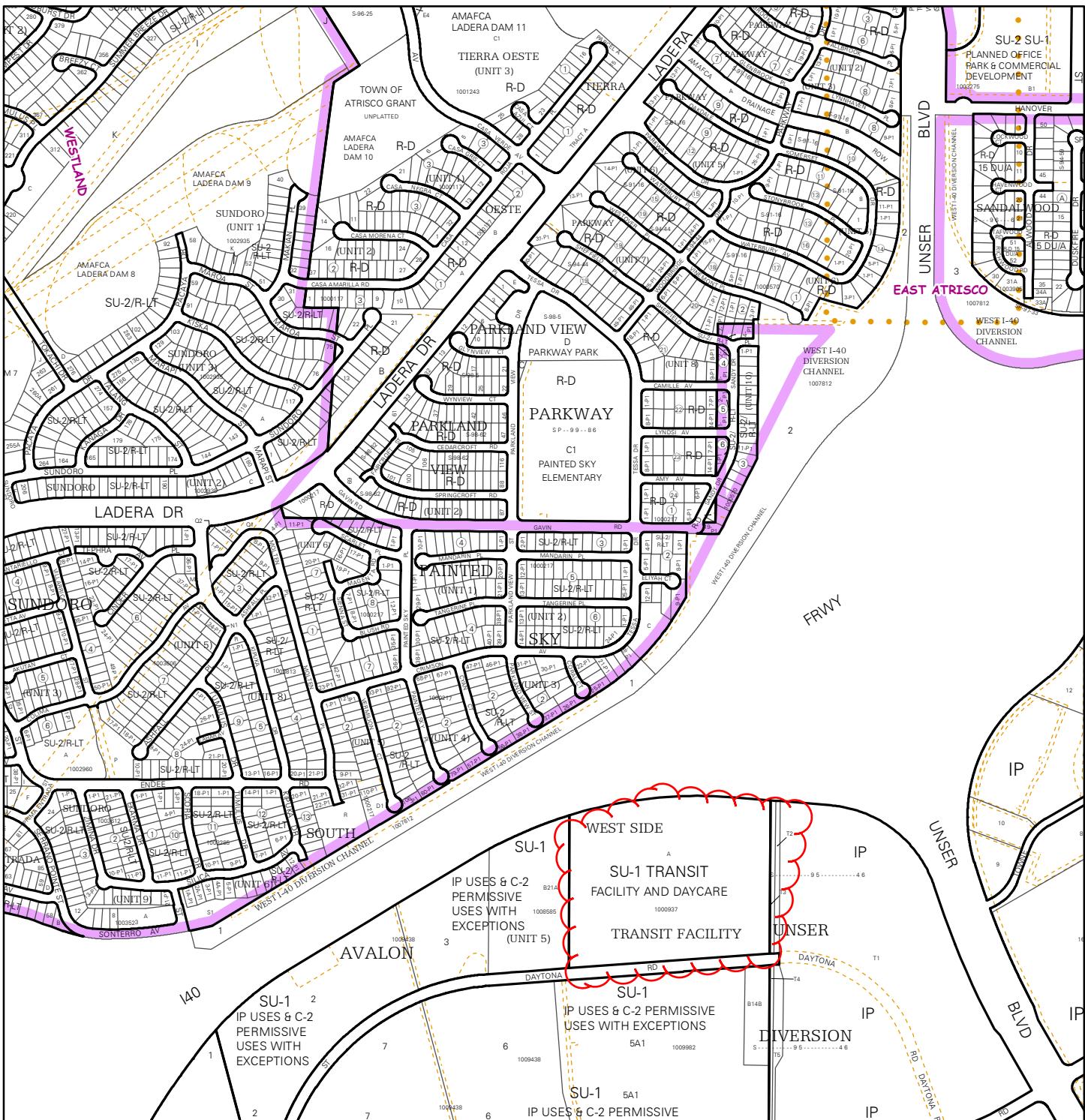


13A and MH-13B in addition to CO-14A and CO-14B represent the same manhole and trunk line upstream of the proposed diversion manhole.

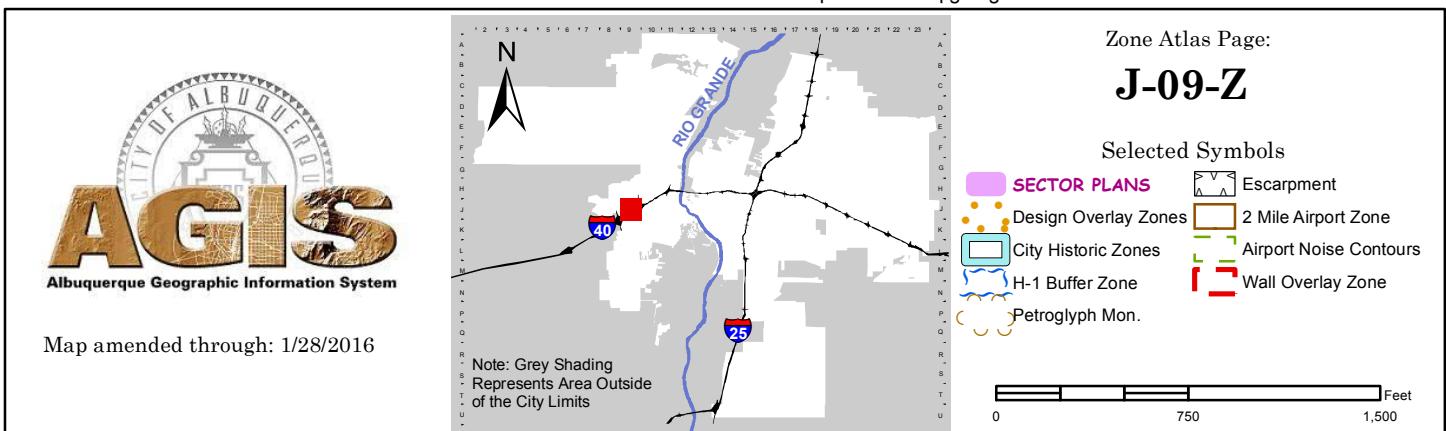
The losses through the oil/water separator were included in the StormCAD model. Because the project is federally funded, bidders were given three different STS options. For this analysis, a Stormceptor 16000 from Rinker Materials was assumed. A "K" value of 1.3 was recommended by the manufacturer to calculate head losses through each manhole.

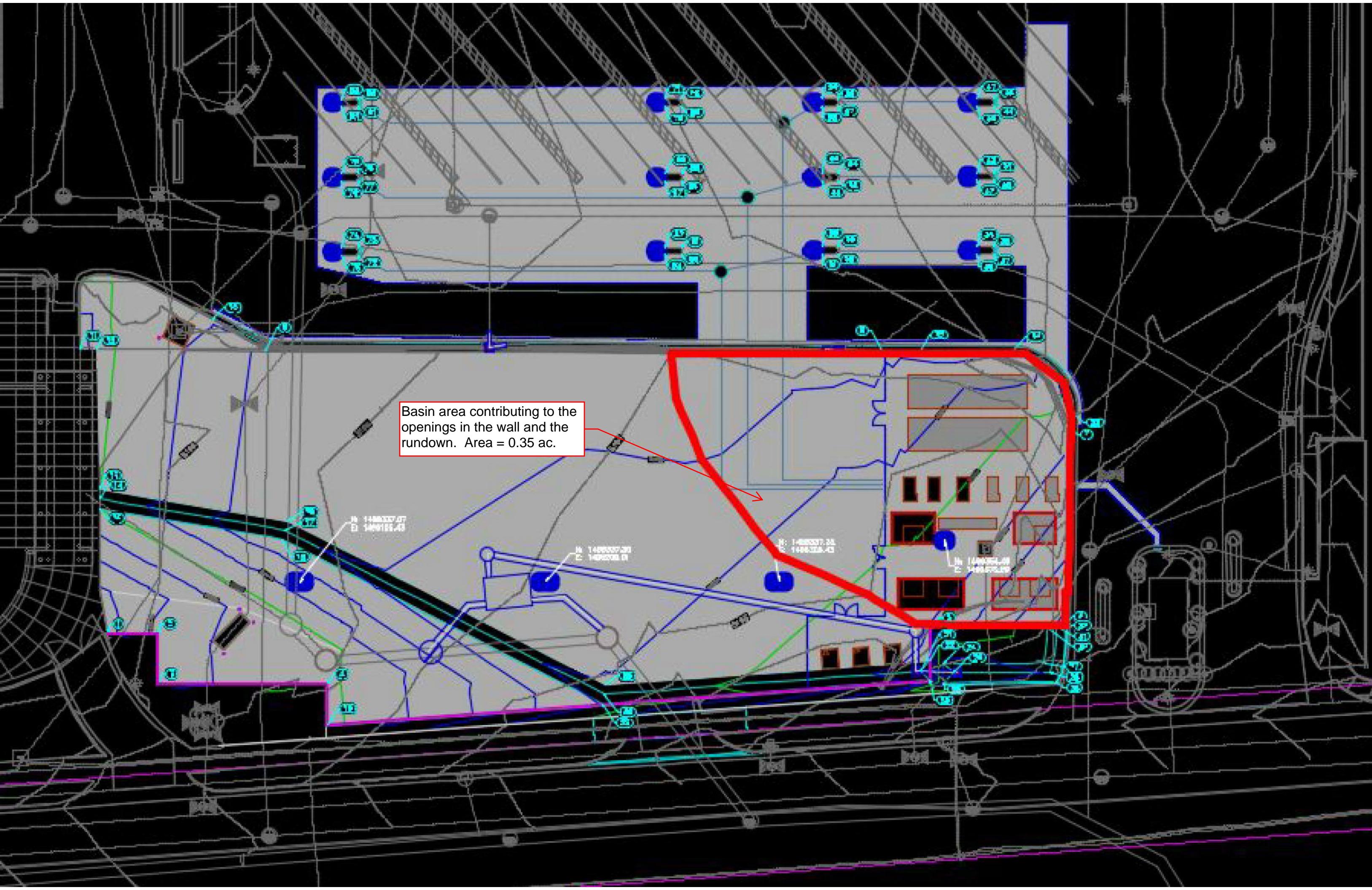
The StormCAD results show that the HGL stays below the ground at the lowest inlet during a 100-year storm. The proposed storm drain system will have adequate capacity for the 100-year design storm in accordance with DPM Chapter 22 criteria, while also providing stormwater treatment and allowing for maintenance by ABQ Ride forces.

Attachments



For more current information and details visit: <http://www.cabq.gov/qis>





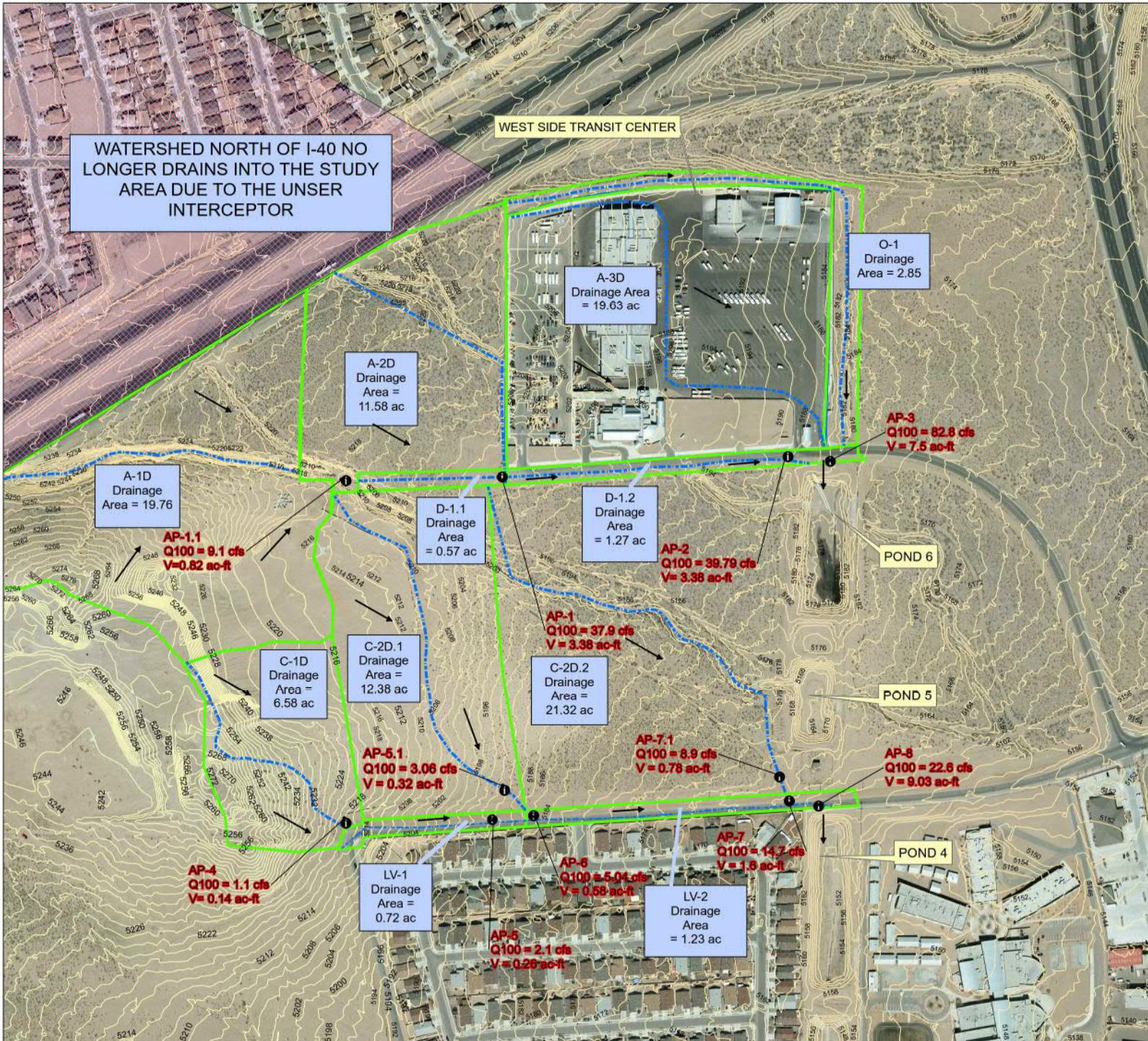
I-40 South and Unser

Mini Drainage Master Plan

Prepared for:
I-40 SOUTH LLC
c/o Tom Keleher
P.O. Box AA
Albuquerque, NM 87103

Prepared by:
Easterling Consultants LLC
3613 NM 528
Suite E-2
Albuquerque, NM 87114

April 2014
Revision #1



LEGEND

- SUBBASIN BOUNDARY
- LONGEST FLOWPATH FOR Tc
- SUBBASIN ID
- ANALYSIS POINT
- FLOW DIRECTION



EXISTING CONDITIONS HEC-HMS INPUT PARAMETERS																									
General Subbasin Data				Time of Concentration (Tc) Data								Lag Time Results													
				Upper Reach or Entire Reach (0 to 400-ft length)								Middle Reach (400 to 1600-ft length)				Lag Time									
Sub-basin	Sub-basin Area	Sub-basin Area	Number of Reaches	L Longest Watercourse	Lc _a Centroid Length	Sc Slope	Kc Composite K	Top Elevation at beginning of water course	Bottom Elevation	Length (L _s)	Slope (S _s)	K _{H1}	K ₁	V _t	Elevation at lower end of water course	Length (L ₂)	Slope (S ₂)	K _{H2}	K ₂	V ₂	Sub-basin				
a	acres	sq mi		ft	ft	ft/ft		ft	ft	ft	ft/ft				ft/sec	(hours)	(minutes)	hours	hours	hours	a				
A-1D	19.758	0.0309	2	1,642	NA	0.0292	1.4457	5258	5252	400	0.0150	1.0	1.22	5210	1,242	0.0338	2.0	3.68	0.15	9	0.18	0.20	0.13	69	A-1D
A-2D	11.581	0.0181	2	988	NA	0.0144	1.2671	5221.19	5210	400	0.0280	1.0	1.67	5207	586	0.0051	2.0	1.43	0.15	9	0.18	0.20	0.13	90	A-2D
A-3D	19.628	0.0307	2	1,630	NA	0.0112	1.5227	5203.2	5193	400	0.0255	1.0	1.60	5185	1,230	0.0065	2.0	1.61	0.21	13	0.28	0.28	0.19	91	A-3D
C-1D	6.581	0.0103	2	832	NA	0.0433	0.9790	5256	5250	400	0.0150	1.0	1.22	5220	432	0.0694	2.0	5.27	0.15	9	0.11	0.20	0.13	63	C-1D
C-2D.1	12.376	0.0193	2	1,261	NA	0.0222	1.4201	5216	5210	400	0.0150	1.0	1.22	5188	861	0.0256	2.0	3.20	0.15	9	0.17	0.20	0.13	65	C-2D.1
C-2D.2	21.324	0.0333	2	1,544	NA	0.0233	1.6145	5206	5192	400	0.0350	1.0	1.87	5170	1,144	0.0192	2.0	2.77	0.15	9	0.17	0.20	0.13	69	C-2D.2
D-1.1	0.556	0.0009	2	460	NA	0.0130	1.0571	5212	5207	400	0.0125	1.0	1.22	5206	60	0.0167	2.0	2.58	0.15	9	0.11	0.20	0.13	82	D-1.1
D-1.2	1.266	0.0020	2	953	NA	0.0210	1.3981	5206	5198	400	0.0200	1.0	1.41	5186	553	0.0217	2.0	2.95	0.15	9	0.13	0.20	0.13	82	D-1.2
LV-1	0.721	0.00113	2	607	NA	0.0478	1.2222	5217	5196	400	0.0525	1.0	2.29	5188	207	0.0386	2.0	3.93	0.15	9	0.06	0.20	0.13	82	LV-1
LV-2	1.225	0.00191	2	967	NA	0.0248	1.4428	5188	5175	400	0.0325	1.0	1.80	5164	567	0.0194	2.0	2.79	0.15	9	0.12	0.20	0.13	82	LV-2
O-1	2.852	0.00446	2	1,870	NA	0.0171	1.4742	5214	5200	400	0.0350	0.7	1.31	5182	1,470	0.0122	2.0	2.21	0.20	12	0.27	0.27	0.18	66	O-1

(a) All measurements were obtained from the Drainage Basin Maps, based on Lidar contour mapping dated 2010.
(b) Obtained from Table I-5 in the DPM, pg. 22-64.
(d) Obtained from Table F-6 in the DPM., pg. 22-64.
(e) V= $10^K S^{0.5}$ - determined from $V=K(S^{100})^{0.5}$
(f) See DPM, pages 22-63 through 22-65 for following formulas:
If L < 4000 ft, then
 $Tc = (L/1 + L/2V + L^3/3)3600 \text{ sec/hour}$
If L is between 4,000 ft and 12,000 ft, then
 $Tc = ((12,000-L)/(72,000^K * S^{0.5})) + ((L-4000)^K(Lc/L)^{0.33} / (552.2 * S^{0.165}))$
If L > 12000 ft, then
 $Tc = (4/3)^{26} K^2 (Lc/(5280^2 * (S^{5200}/0.5)))^{0.33}$
(g) Tc = If Tc is computed to be less than 0.2 hours, then use 0.2 hours DPM pg. 22-37
(h) Tp = $(2/V)Tc$ per DPM pg. 22-36
(i) Sc = $(L^1 S^1 + L^2 S^2 + L^3 S^3)/L$ per DPM pg. 22-65
(j) Kc = $(L/S^{0.5}) / (L_1/(K_1 S^{1.0}) + L_2/(K_2 S^{2.0}) + L_3/(K_3 S^{3.0}))$ per DPM pg. 22-65

Summary of Pond Routings												
Pond	Model Description	Design Volume	100 Yr Peak Storage Volume	100 Yr 24 Hr Inflow Volume	100 Yr 24 Hr Outflow Volume	100 Yr 24 Hr Inflow	100 Yr 24 Hr Outflow	Elevation of Emergency Spillway	100 Yr 24 Hr Peak Water Surface Elevation	Freeboard from Emergency Spillway	Available Storage	Comments
a	a	ac-ft	ac-ft	cfs	cfs	cfs	ft	ft	ft	ft	ac-ft	
Pond 4	Ex Conditions HEC-HMS	8.51	2.42	9.03	9.03	22.6	7.7	5155.1	5148.98	6.1	6.09	Model uses current watershed conditions using latest NOAA 14 100 Yr-24 Hr rainfall depth of 2.52 in. Pond 5 not modeled
Pond 6	Conditions HEC-HMS	9.01	2.98	7.48	7.48	82.8	9.4	5177.9	5174.18	3.7	6.03	

a - All values reported on this table are taken directly from The Master Drainage Plan for the West Side Transit Facility 100 Yr 24 Hr rainfall depth based on latest NOAA Atlas 14 data
b - Freeboard = Elevation of Emergency Spillway - Peak Water Surface Elevation

EX POND 6 RATING CURVE		
Elevation	Storage	Discharge
ft.	ac-ft.	cfs
5170	0	0
5171	0.14	4
5172	0.83	6.2
5173	1.77	7.9
5174	2.79	9.2
5175	3.87	10.4
5176	5.04	11.5
5177	6.27	79.5
5178	7.46	86.1
5179	9.01	93.2

DATA FROM MASTER DRAINAGE PLAN FOR THE WEST SIDE TRANSIT FACILITY

EX POND 4 RATING CURVE		
Elevation	Storage	Discharge
ft.	ac-ft.	cfs
5147	0	0
5148	0.08	0
5149	0.51	3
5150	1.3	5.7
5151	2.29	

WEST SIDE TRANSIT FACILITY

PHASE I

8001 DAYTONA RD. SW
ALBUQUERQUE, NEW MEXICO

SCANNED BY
MESA REPRO

NEW FACILITIES TRANSIT DEPARTMENT

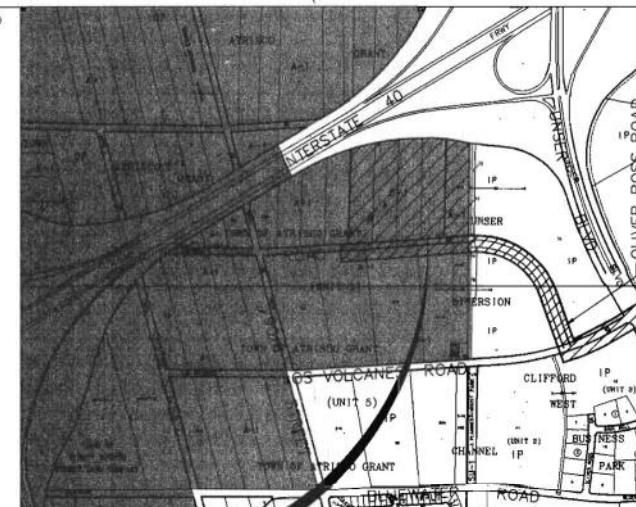
PROJECT NO. 5658.01

SURVEYOR'S CERTIFICATE
I, THOMAS W. PATRICK, A DULY QUALIFIED LICENSED PROFESSIONAL SURVEYOR UNDER THE LAWS OF THE STATE OF NEW MEXICO, DO HEREBY CERTIFY THAT THE AS-BUILT INFORMATION SHOWN ON THESE DRAWINGS WAS OBTAINED FROM FIELD CONSTRUCTION AND "AS-BUILT" SURVEYS PERFORMED IN ACCORDANCE WITH MY SUPERVISION. THAT THE "AS-BUILT" INFORMATION SHOWN IN THESE DRAWINGS (UNLESS OTHERWISE NOTED) WAS ADDED BY ME, OR BY UNDER MY SUPERVISION, AND THAT THIS "AS-BUILT" INFORMATION IS TRUE AND CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF. COMMUNITY SCIENCES CORPORATION IS NOT RESPONSIBLE FOR ANY OF THE DESIGN CONCEPTS, CALCULATIONS, ENGINEERING AND/OR INTENT OF THE RECORD DRAWINGS.



7-26-2001
DATE

VICINITY MAP



VICINITY MAP

NOT TO SCALE
PROPOSED CONSTRUCTION AREA

ZONE MAP NO.

J-9-Z

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DWL ARCHITECTS & PLANNERS, INC.
OF NEW MEXICO
202 CENTRAL AVE., S.E.
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APPROVED FOR CONSTRUCTION

George P. Gee 6/26/02
City Architect Date

Frank J. Aguirre 7/1/02
City Engineer Date

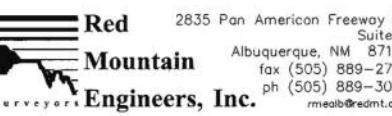
LAST DESIGN UPDATE

00.01

SHEET 01 OF 61

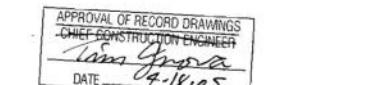


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ph (505) 889-3004
rmeab@redmt.com

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15
26 5658.01 05



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- 04 SI-C-103 LOS VOLCANES RD. P&P: STA 9+00 TO STA 13+60
- 05 SI-C-104 LOS VOLCANES RD. P&P: STA 13+60 TO 18+00
- 06 SI-C-105 OLIVER ROSS DR. PAVING P&P: 10+00 TO STA 14+60
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43B

RECORD DRAWING

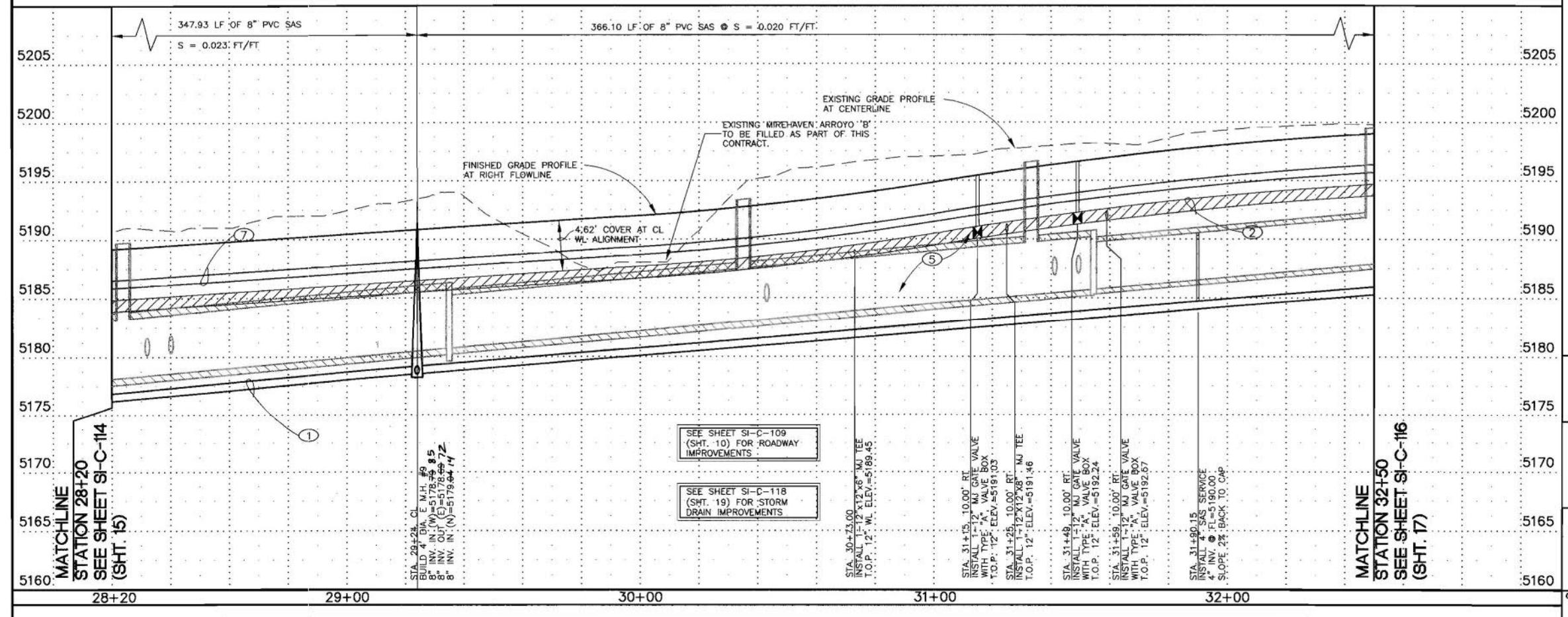
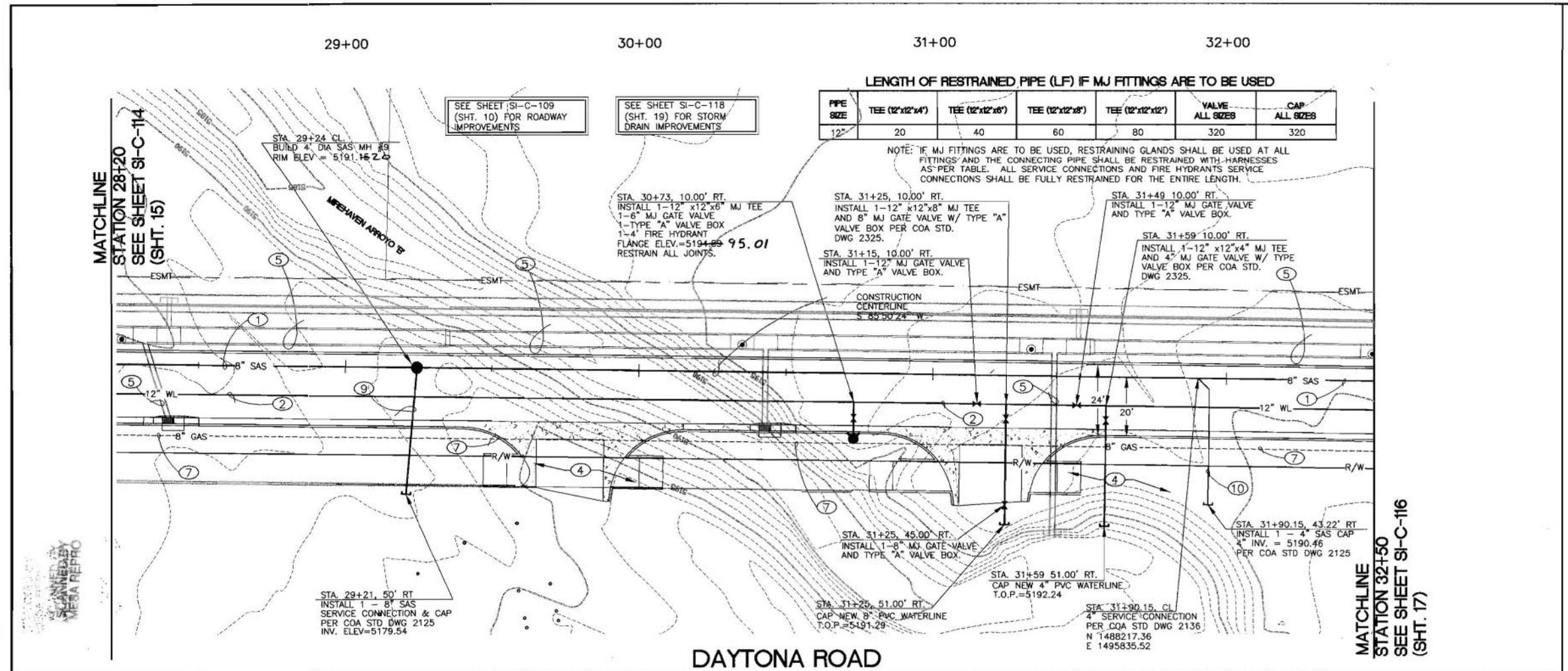
THE FOLLOWING EFFECTS WERE ADDED IN GREEN CHANGE ORDERS
FOR ON-SITE UTILITIES AND WALL MOOS AND PAVING

- 23 A PHASE 1 CHANGE ORDER - WATER
- 23 B PHASE 1 CHANGE ORDER - ONSITE SANITARY SEWER
- 23 C ON-SITE PAVING CO.
- 23 D PHASE 2 CHANGE ORDER - STORM DRAIN
- 23 E CHANGE ORDER - GAS & ELECTRICAL
- 23 F NEW INTERIOR WALL LOCATION SHERH 06103

PATRICK CONLEY of the firm of SMITH ENG. CO.
A Registered Professional Engineer in the State of New Mexico, do hereby certify, to the best of my knowledge and belief, that the infrastructure installed as part of this project has been inspected by me or by a qualified person under my direct supervision and has been constructed in accordance with the plans and specifications, while someone from Smith Engineering Company was onsite, approved by the City Engineer and that the original design intent of the approved plans has been met, except as noted by me on the as-built construction drawings. This Certification is based on site inspections by me or personnel under my direction and survey information provided by THOMAS PATRICK (Surveyor Name) NMPS number 12651 (PS#).

Engineers Seal & Signature

* FOR WORK DONE IN NMHTD RIGHT-OF-WAY



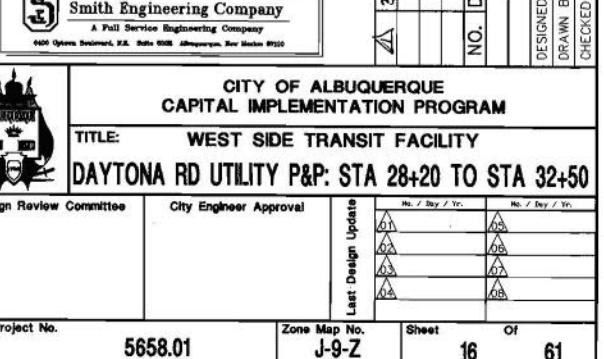
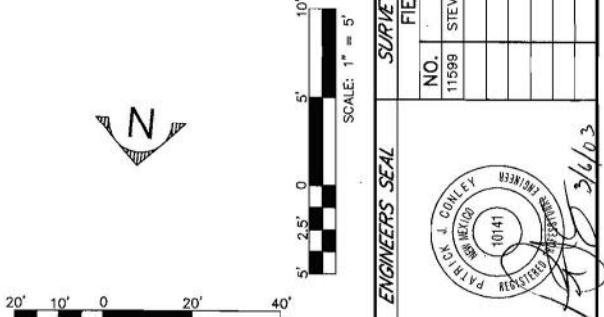
- KEYED NOTES:**
1. NEW 8" PVC SANITARY SEWER LINE.
 2. NEW 12" PVC WATERLINE.
 3. 35'X45' WATER METER ESMT BY PLAT.
 4. 10' S/W ESMT AND P.U.E. BY PLAT.
 5. STORM DRAIN SYSTEM - SEE SHEET SIT-C-118 (SHT. 18) FOR STORM DRAIN PLAN & PROFILES.
 6. NOT USED.
 7. NEW 8" HIGH PRESSURE GAS LINE TO BE INSTALLED BY PNM GAS. MINIMUM OF 3' OF COVER.
 8. FUTURE WATER METER VAULT LOCATION.
 9. CONSTRUCT 45 LF 8" PVC SAS @ S=0.010 FT/FT
 10. INSTALL 4" SAS SERVICE PER COA STD DWG. 2136 "B"

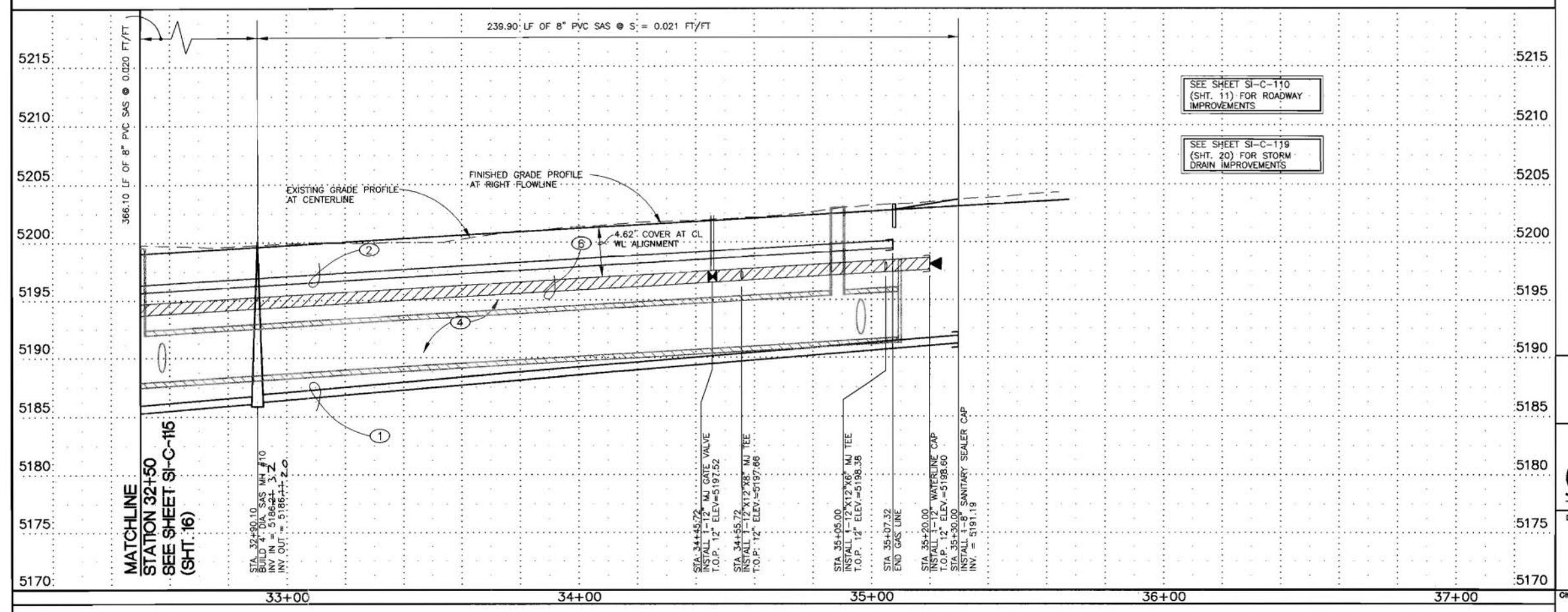
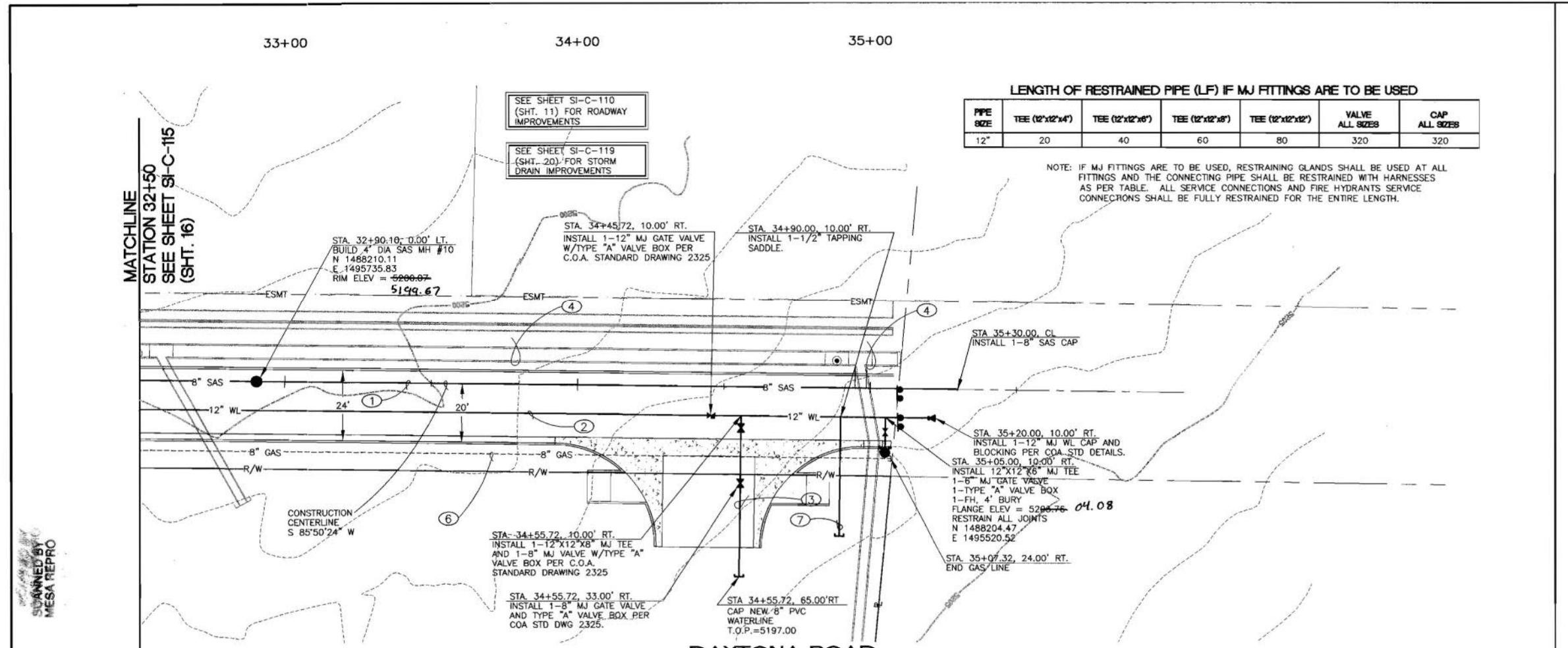
AS BUILT INFORMATION

CONTRACTOR C.C.M. INC.	DATE ISSUED CSC
INSPECTOR BY SEC	DATE ACCEPTED BY CO
DRAWN BY JP	DATE DRAWN BY CO
RECORDED BY JP	DATE RECORDED BY CO
NO.	

BENCH MARKS

A.C.S. CONTROL MONUMENT #10-K'0"	FIELD NOTES	SURVEY INFORMATION
NO. BY DATE	NO. BY DATE	NO. BY DATE
11599 STEVE TOLER 2000 3-1/4" AL. CAP IN CONC. CURB		
S.W. COR. UNSER & LOS VOLCANES		
N 148°05'52.22 : E 35°37'50.04		
DELTA ALPHA = -01627"		
COMBINED FACTOR=0.999675/701 (PROJECT)		
NO.		





KEYED NOTES:

1. NEW 8" PVC SANITARY SEWER LINE.
 2. NEW 12" PVC WATERLINE.
 3. INSTALL 50 LF OF 8" PVC WATERLINE.
 4. STORM DRAIN SYSTEM - SEE SHEET SI-C-119 (SHT. 19) FOR STORM DRAIN PLAN & PROFILES.
 5. NOT USED.
 6. NEW 8" HIGH PRESSURE GAS LINE TO BE INSTALLED BY PNM GAS. MINIMUM OF 3' OF COVER.
 7. INSTALL 1-1/2" TYPE K COPPER IRRIGATION LINE TO 5' BACK OF R/W. CAP LINE.

SURVEY INFORMATION					
BENCH MARKS		FIELD NOTES		A.C.S. CONTROL MONUMENT "10-K10"	
				ELEV. (NGVD 29) = 5,142.79'	
				S.W. COR. UNSER & LOS VOLCANES	
				N 1.487-056-22 : E 357-375-04	
				DELTA ALPHA = -016-27"	
				COMBINED FACTOR=0.999675701 (PROJECT)	
				RECORDED BY DATE NO.	

AS BUILT INFORMATION

ENGINEERS SEAL		CONTRACTOR C.M. INC.	
		WORK BY C.S.C.	
		INSPECTOR BY SEC	
		ACCEPTANCE BY CMA	
		FIELD DRAWINGS BY S.P.S.	
		DATE OF DRAWING	
		MICRO-FILM INFORMATION	
		RECORDED BY DATE	

SCALE: 1" = 5'

L

STRUCTS, INC.
Mexico

AVE. S.E.
URTIADO
MEXICO
87102

12-4159
12-6202
T66.DON

BENEFIT OF THE PUBLIC

NEW MEXICO

PARKS & RECREATION

3/1/13

LBUQUERQUE
ENTATION PROGRAM

TRANSIT FACILITY

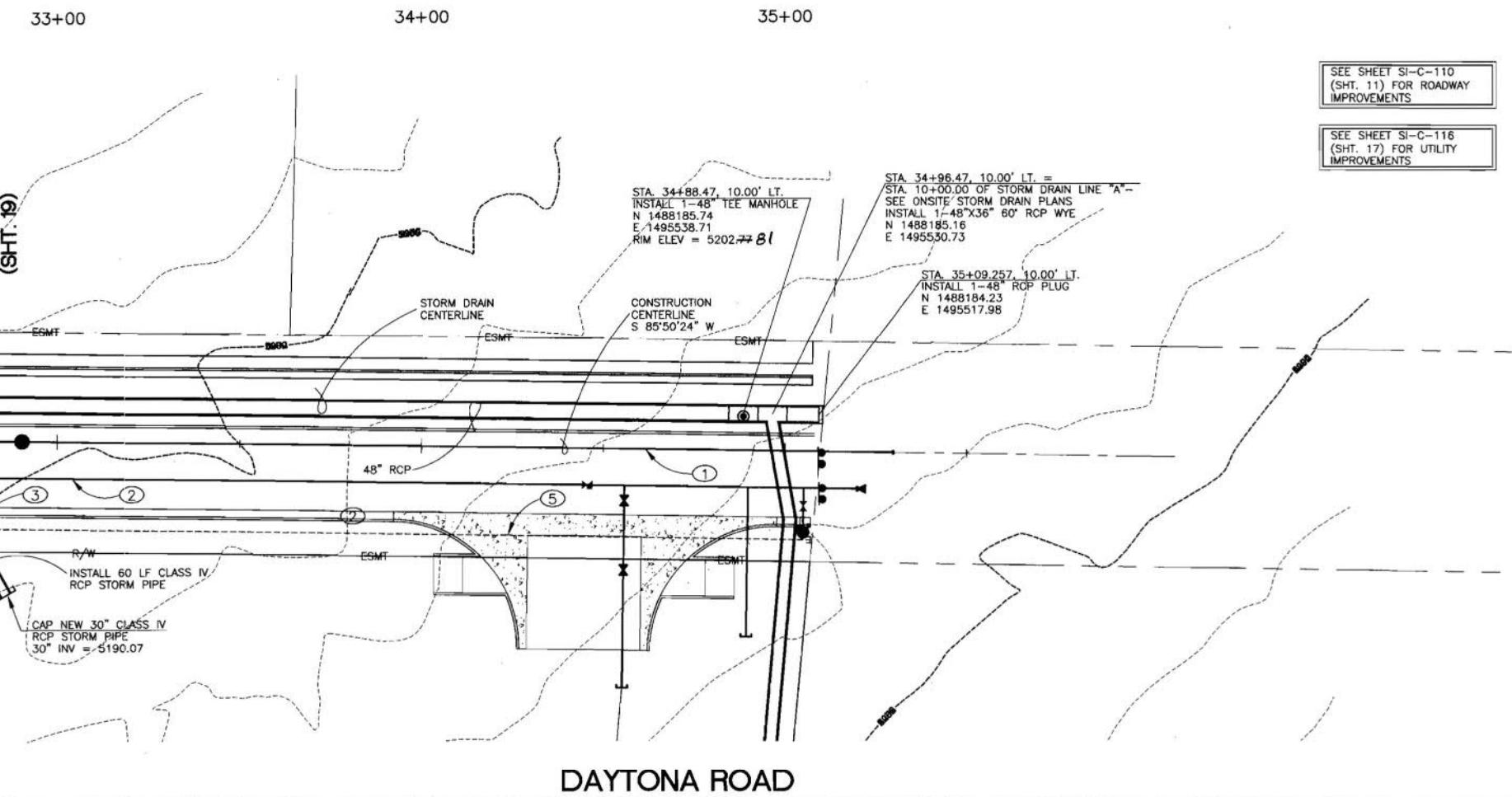
STA 32+50 TO STA 35+12.07

Last Design Update

No. / Day / Yr.	No. / Day / Yr.
01	01
02	02
03	03
04	04
05	05
06	06
07	07
08	08
09	09
10	10
11	11
12	12
13	13
14	14
15	15
16	16
17	17
18	18
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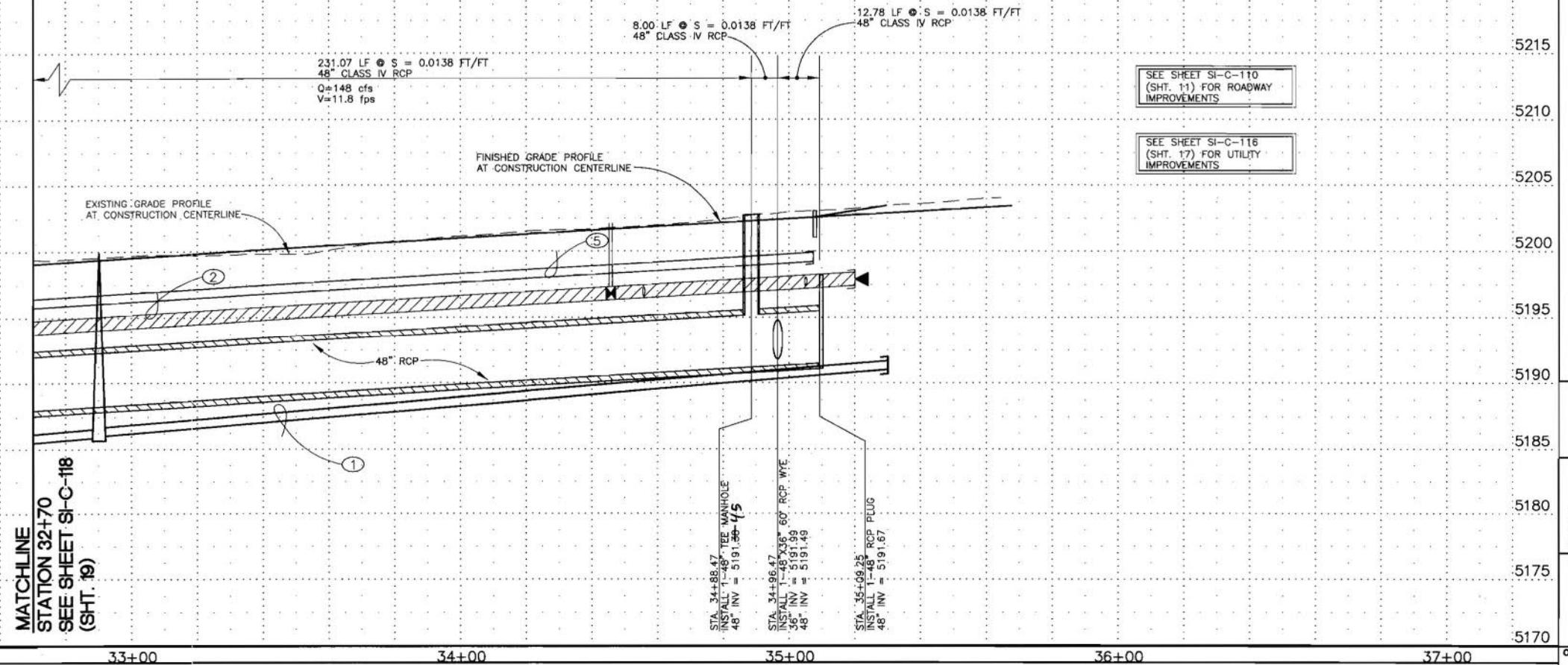
MATCHLINE
STATION 32+70
SEE SHEET SI-C-18
(SHT. 19)

SCANNED BY
WEST SIDE TRANSIT



MATCHLINE
STATION 32+70
SEE SHEET SI-C-18
(SHT. 19)

SCANNED BY
WEST SIDE TRANSIT



KEYED NOTES:

1. NEW 8" PVC SANITARY SEWER LINE - SEE UTILITY PLANS.
2. NEW 12" PVC WATERLINE - SEE UTILITY PLANS.
3. INSTALL 56' LF 30" CL IV RCP STORM DRAIN @ S = 0.020 FT/FT
4. NOT USED.
5. NEW 8" HIGH PRESSURE GAS LINE TO BE INSTALLED BY PNM GAS. MINIMUM OF 3' OF COVER.

AS BUILT INFORMATION		BENCH MARKS	
CONTRACTOR	CSC DATE 2/14	WORK BY	ACCEPTANCE BY SEC DATE 2/14
SUBCONTRACTORS	DATE 2/14	FIELD LOCATION BY DR DATE 2/14	DETERMINATION BY SPB DATE 2/14
DRAWINGS	DATE 2/14	RECORDED BY	MICRO-FILM INFORMATION DATE
	NO.		

SCALE: 1" = 5'

5' 2.5' 0 5' 10'

20' 10' 0 20' 40'

SCALE: 1" = 20'



DWL
ARCHITECTS
& PLANNERS, INC.
OF NEW MEXICO

202 CENTRAL AVE. S.E.
WEST COURTYARD
ALBUQUERQUE, NEW MEXICO
87102

FAX (505) 242-4159
VOICE (505) 242-2292
E-MAIL DWLNH@RTS6.COM

SI-C-119

NO.	DATE	REMARKS	BY
		REVISONS	DESIGN

DESIGNED BY PJC DATE 4/02
DRAWN BY EAD DATE 4/02
CHECKED BY PJC DATE 4/02

100300

Smith Engineering Company
A Full Service Engineering Company
600 Uptown Boulevard, N.E. Suite 2000 Albuquerque, New Mexico 87102

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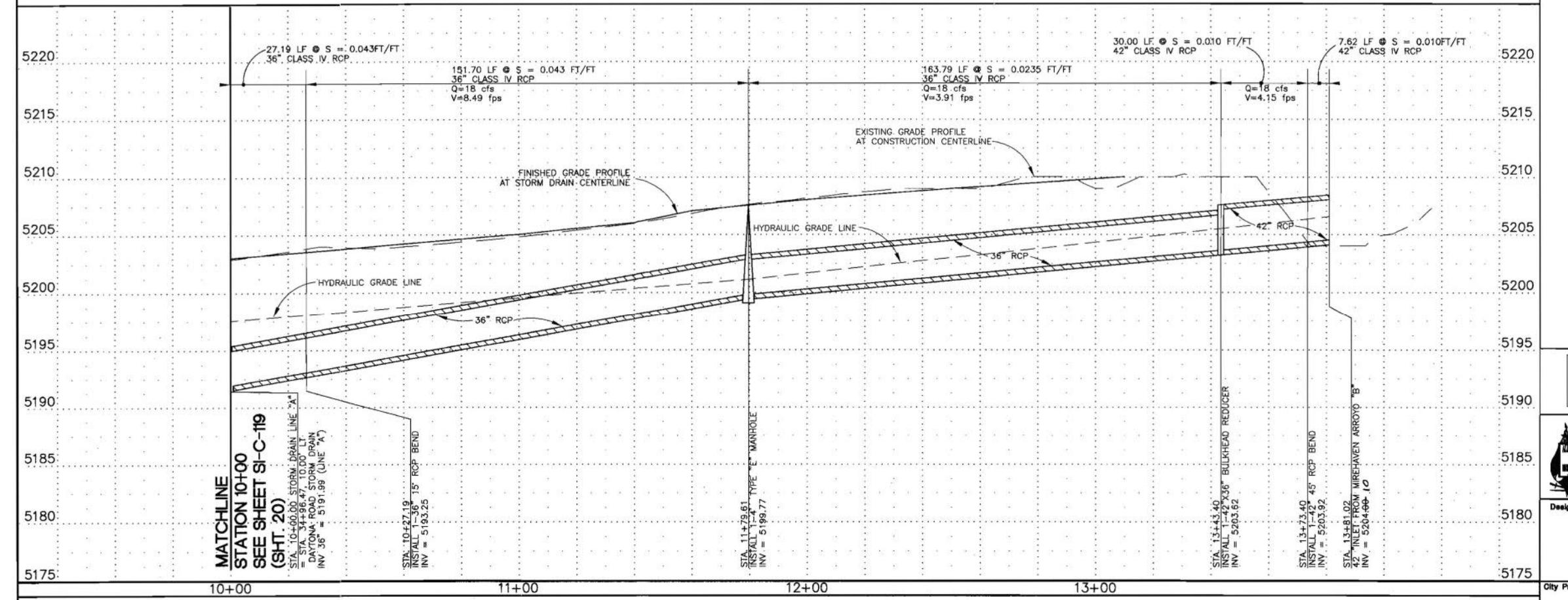
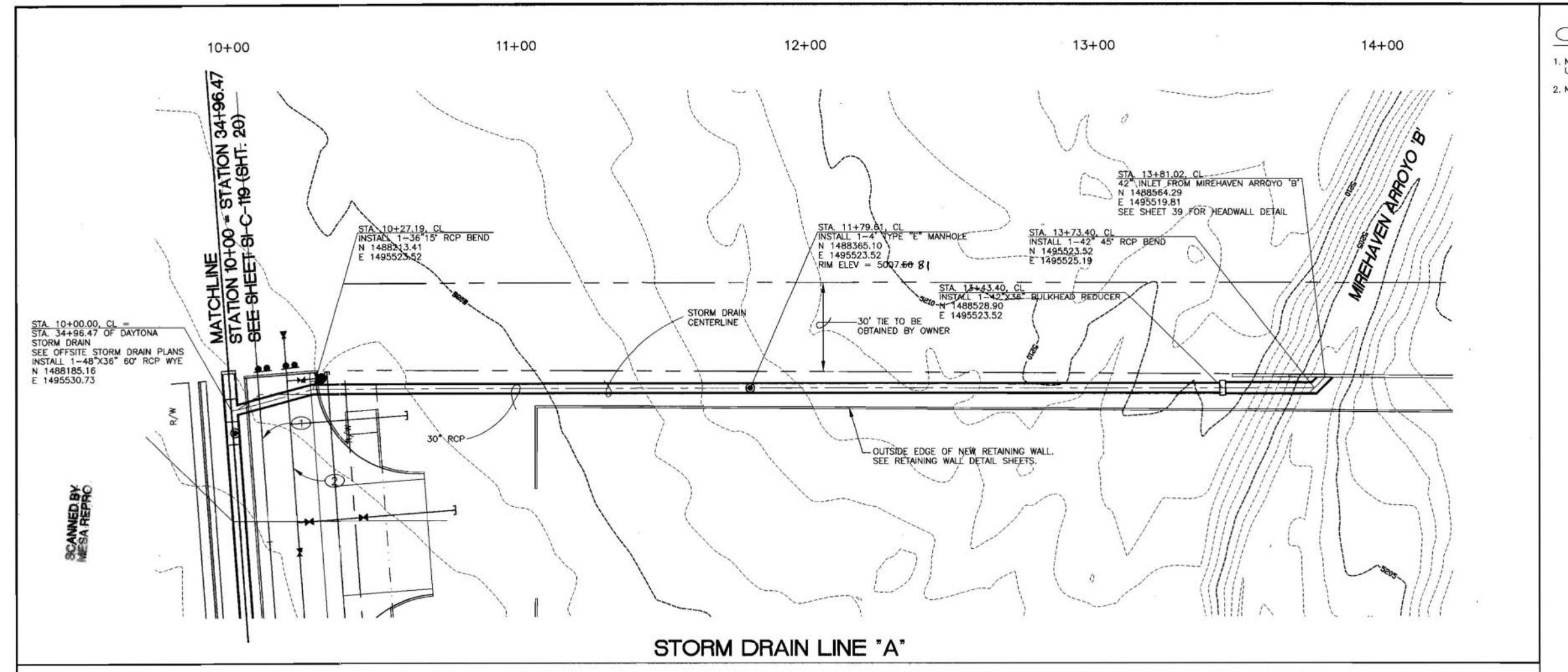
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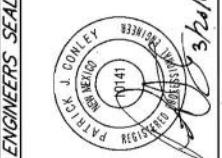
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KEYED NOTES:

- NEW 8" PVC SANITARY SEWER LINE-SEE
UTILITY PLANS.

SURVEY INFORMATION		BENCH MARKS		AS BUILT INFORMATION			
FIELD NOTES	BY	DATE	A.C.S. CONTROL MONUMENT "10-K10"	CONTRACTOR	GC M Inc.	DATE	
NO.			ELEV. (NGVD 29) = 5,142.79'	WORK PERFORMED BY	CSC		
11599	STEVE TOLER	2000	3-1/4" AL. CAP IN CONC. CURB	SHAKEDOWN			
			S.W. COR. UNSER & LOS VOLCANES	ACCEPTANCE BY	SEC.		
			N 1,487.056.22 ; E 357.375.04	FIELD	CDR		
			DELTA ALPHA = -0°16'27"	VERIFICATION BY	CDR		
			COMBINED FACTOR=0.999675701 (PROJECT)	DRAWN BY	CDR		
				CHANGED BY	CDR		
				RECORDED BY	CDR		
				DATE	10/13/04		
				NO.			



W.L.
ARCHITECTS
agent

ARCHITECTS
ENGINEERS, INC.
OF NEW MEXICO

CENTRAL AVE. S.E.
WEST COURTYARD

87102
24.VI

605) 242-6202
VLNM@RT66.COM

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NO.

OF ALBUQUERQUE

TRANSIT FACILITY

P&P: STA 10:00 TO S

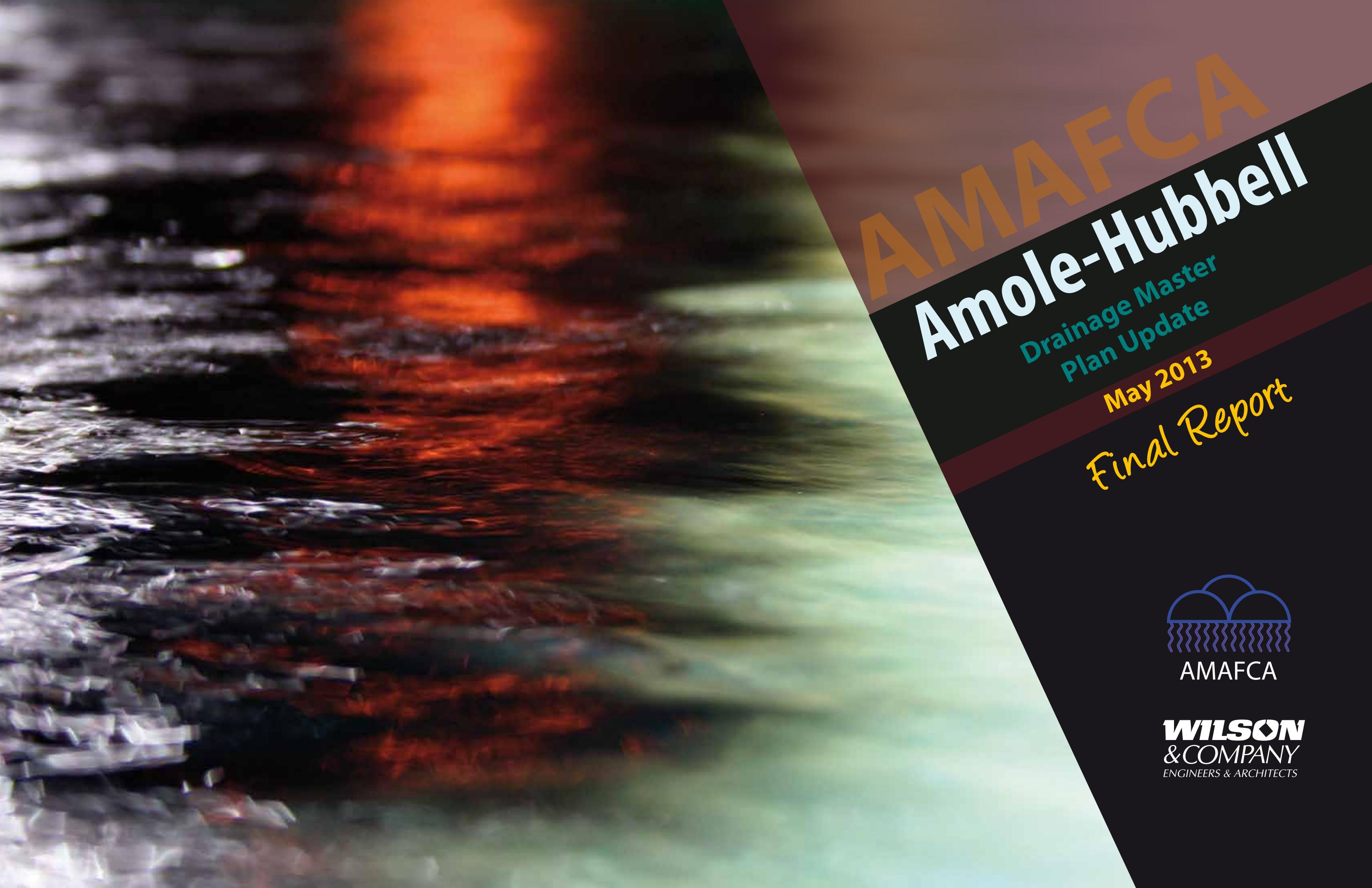
oval Date Mo. / Day / Yr.

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Zone Map No. 1-9-7 Sheet 01

E1 61



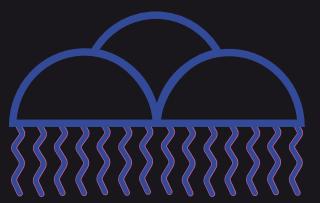
AMAFCA

Amole-Hubbell

Drainage Master
Plan Update

May 2013

Final Report



AMAFCA

WILSON
& COMPANY
ENGINEERS & ARCHITECTS



Figure 3-11: Unser/214 - Proposed Basin Map

Project Daytona
 Subject Turned block capacity

Computed by FHO

Checked by

Date 6-28-17

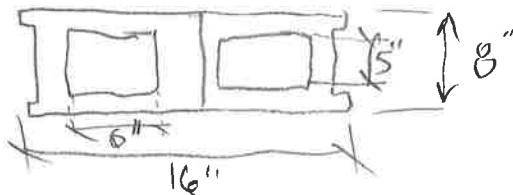
Date

Contributory basin (see map) = 15100 sq. ft. = 0.35 ac.

$$Q_{100} = 0.35(4.37) \quad \text{zone 1, land treatment D}$$

$$\underline{Q_{100} \approx 1.5 \text{ cfs}}$$

Blocks configuration 16" x 8" w/ 2-6" x 5" holes



use Weir equation to

determine capacity of 1 block since the water level should not get that high for Orifice eqn.

assume 4" depth $Q_c = C L (H)^{3/2}$

$$Q_c @ 4" = 3.0 (1)(4^4/12)^{3/2}$$



$$Q_c @ 4" \text{ depth / block} = 0.58 \text{ cfs}$$

use 3 turned blocks, $Q_c @ 4" = 0.58(3) = 1.73 \text{ cfs}$

water depth behind the wall should be slightly less than 4" during the 100-year storm

Since the transformers have a minimum 4" high header curb around them, the 3 turned blocks should work fine.

Project: Daytona
 Subject: Valley Gutter Capacity

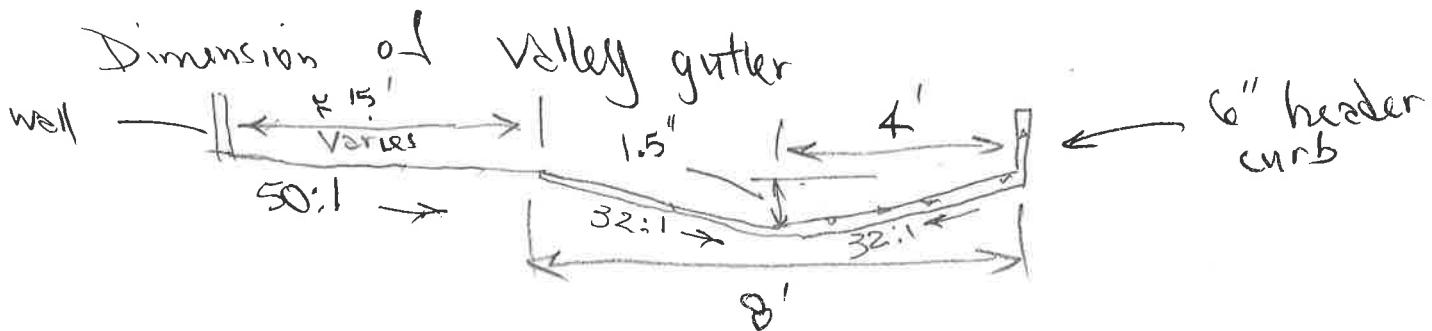
Computed by FHB

Checked by

Date 6-29-17

Date

Determine the capacity of the valley gutter at the SE corner of the property just outside of the proposed wall.



long. slope of valley gutter $\approx 1.5\%$

use FlowMaster to estimate capacity.

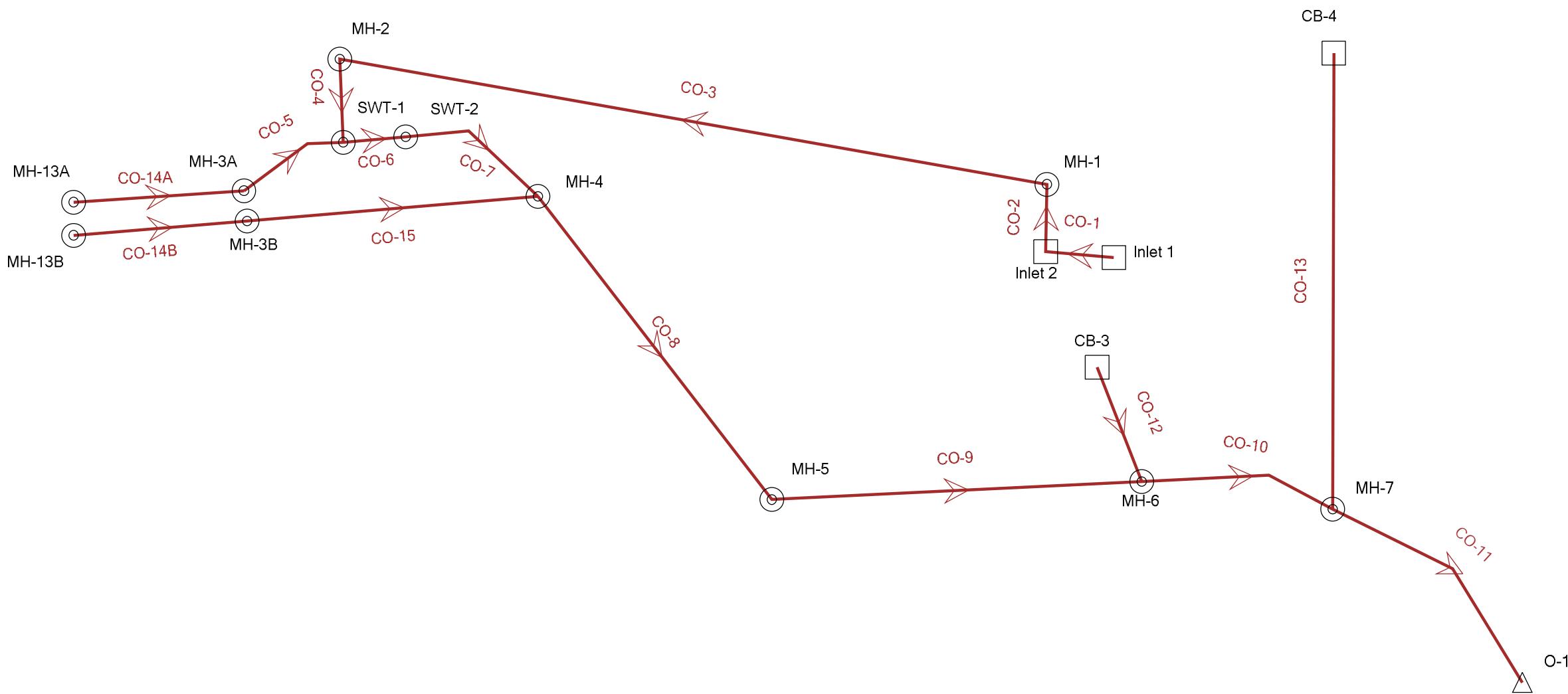
$$Q_{100} = 1.5 \text{ cfs}$$

$$\text{depth of flow } d_{100} = 0.15'$$

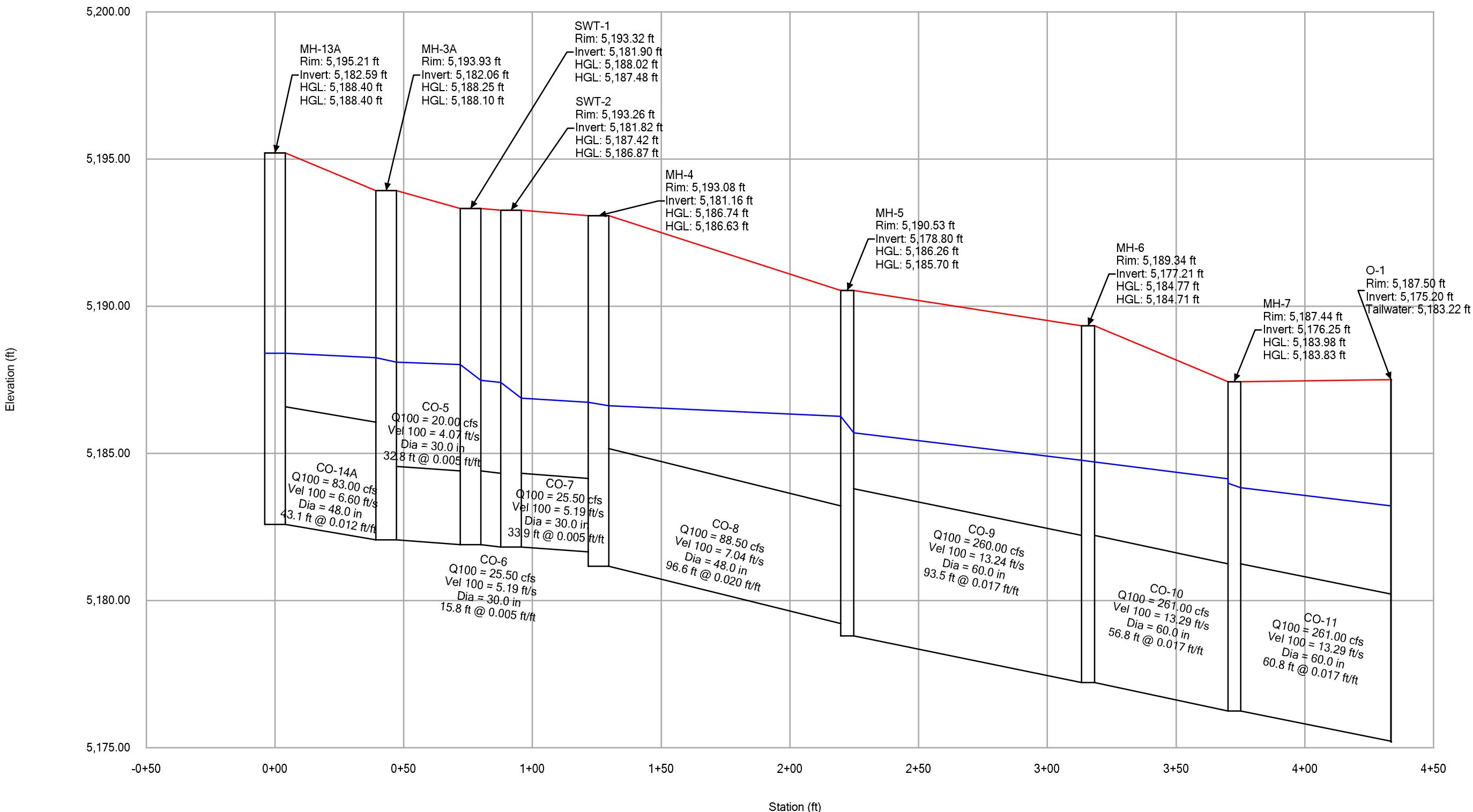
Use the specific energy depth of 0.22' for the worst case condition of if flow comes to a sudden stop; the depth around the curved portion of the valley gutter should be less than the 0.22' or 2.6" (specific energy depth).

Since the transformers are sitting on a pad with a minimum 4" high header curb around them; the runoff should not get on the pads.

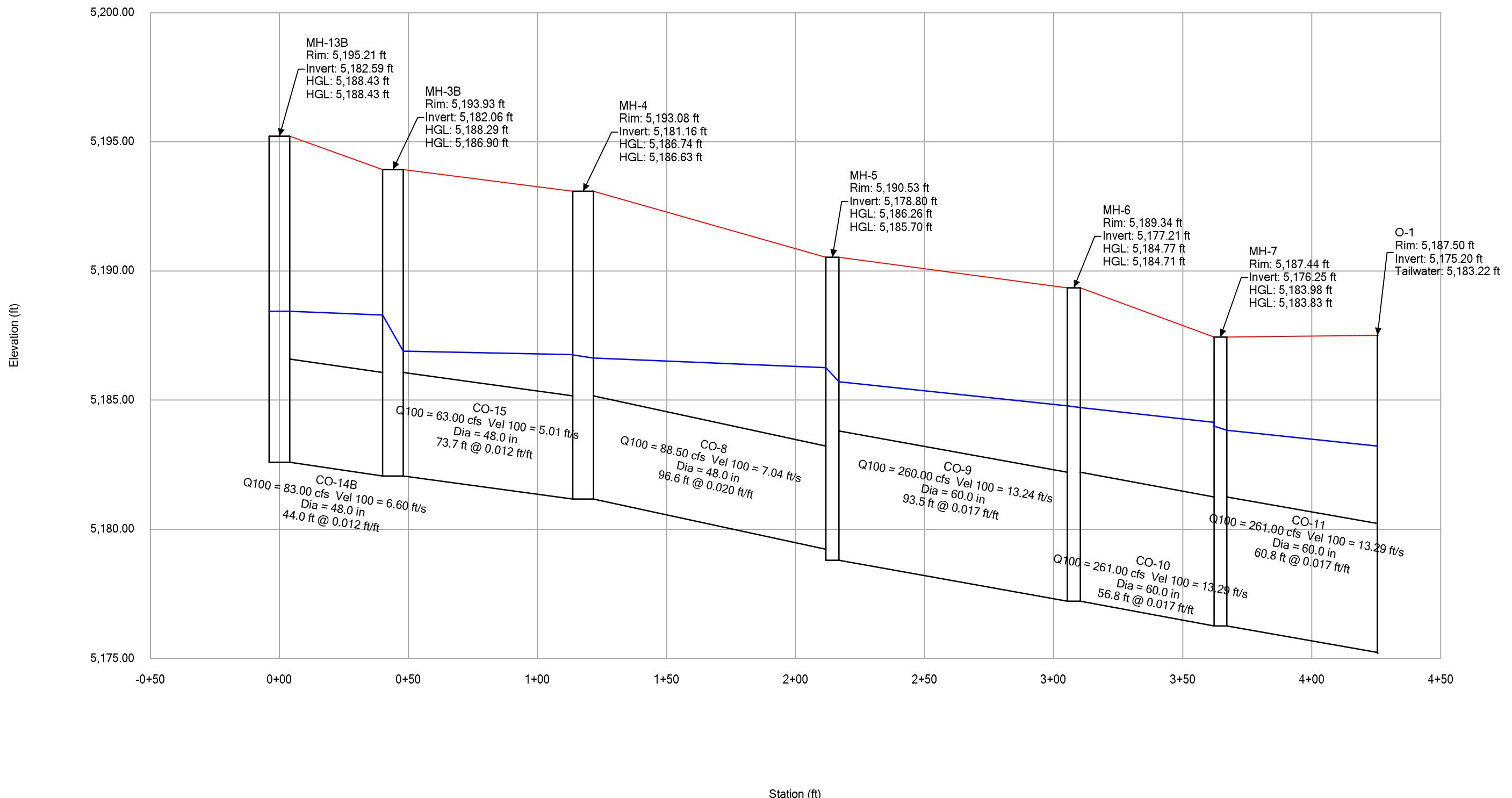
Scenario: Base



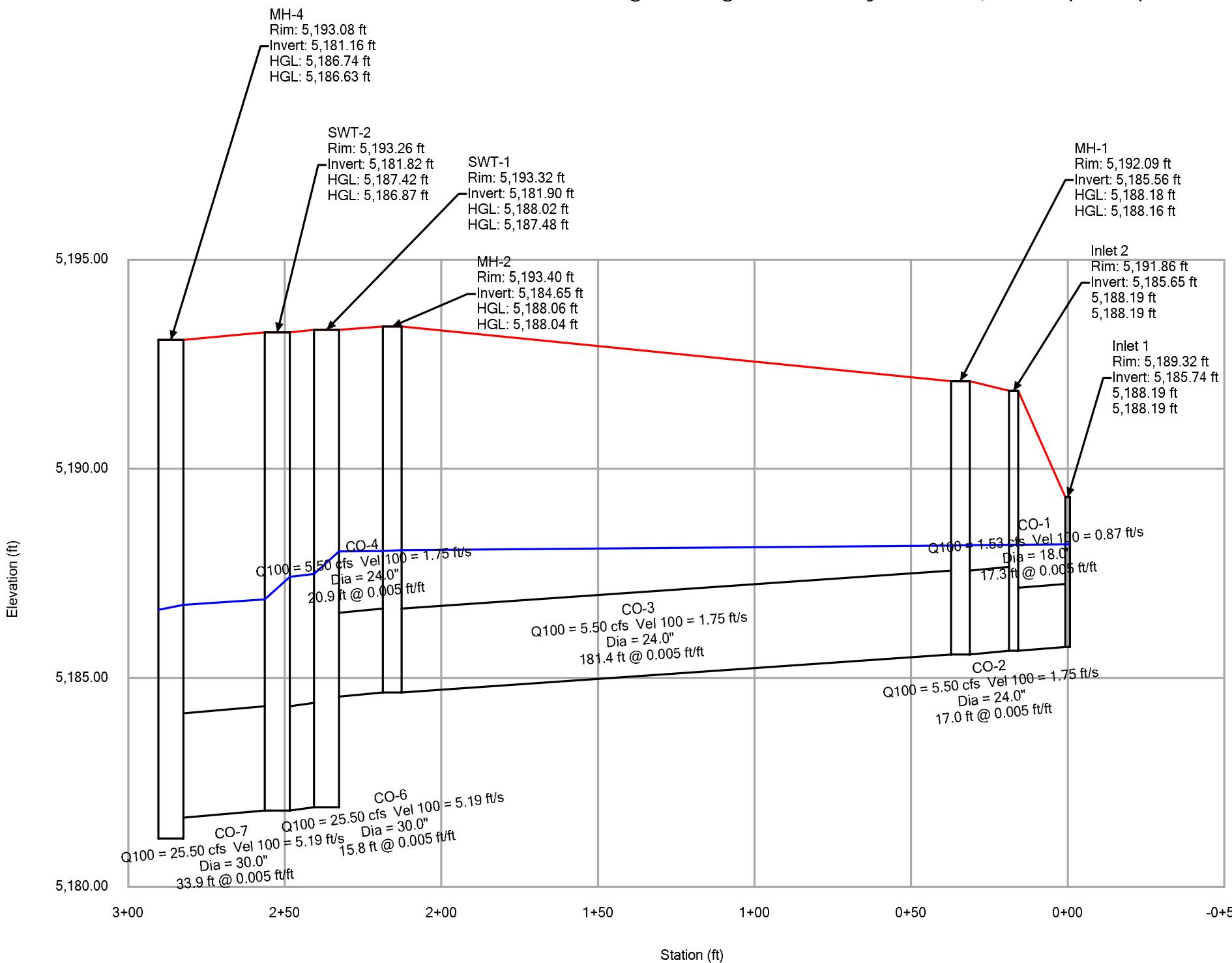
Profile Report
Engineering Profile - TreatmentSys SD (Ex&PropSD Option1.stsw)



Profile Report
Engineering Profile - Existing SD (Ex&PropSD Option1.stsw)



Profile Report
Engineering Profile - Daytona SD (Ex&PropSD Option1.stsw)



DAYTONA - STORM CAD RESULTS

CATCH BASIN SUMMARY								
Label	Elevation (Rim) (ft)	Elevation (Invert) (ft)	Depth (In) (ft)	Hydraulic Grade Line (In) (ft)	Headloss Method	Headloss (ft)	Flow (Known) (cfs)	Inflow (Wet) Collection (cfs)
Inlet 1	5,189.32	5,185.74	2.45	5,188.19	Absolute	0	0	1.53
Inlet 2	5,191.86	5,185.65	2.54	5,188.19	Absolute	0	0	3.97
CB-3	5,188.96	5,177.83	6.96	5,184.79	Absolute	0	0	1
CB-4	5,190.11	5,178.67	5.32	5,183.98	Absolute	0	0	0

DAYTONA - STORM CAD RESULTS

MANHOLE SUMMARY											
Label	Elevation (Rim) (ft)	Elevation (Invert) (ft)	Diameter (in)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	HEC-22 Benching Method	Headloss Method	Headloss Coefficient (Standard)	Headloss (ft)	Flow (Known) (cfs)	Inflow (Wet) Collection
MH-1	5,192.09	5,185.56	72	5,188.18	5,188.16	Half	HEC-22(2nd Ed)		0.01	0	0
MH-2	5,193.40	5,184.65	72	5,188.06	5,188.04	Half	HEC-22(2nd Ed)		0.02	0	0
SWT-1	5,193.32	5,181.90	96	5,188.02	5,187.48		Standard	1.3	0.55	0	0
MH-4	5,193.08	5,181.16	96	5,186.74	5,186.63	Half	HEC-22(2nd Ed)		0.12	0	0
MH-5	5,190.53	5,178.80	60	5,186.26	5,185.70	Half	HEC-22(2nd Ed)		0.56	254.5	0
MH-6	5,189.34	5,177.21	60	5,184.77	5,184.71	Half	HEC-22(2nd Ed)		0.06	0	0
MH-7	5,187.44	5,176.25	60	5,183.98	5,183.83	Half	HEC-22(2nd Ed)		0.15	0	0
MH-3B	5,193.93	5,182.06	96	5,188.29	5,186.90	Half	Absolute		1.39	63	0
MH-3A	5,193.93	5,182.06	96	5,188.25	5,188.10	Half	HEC-22(2nd Ed)		0.15	20	0
SWT-2	5,193.26	5,181.82	96	5,187.42	5,186.87		Standard	1.3	0.55	0	0
MH-13B	5,195.21	5,182.59	96	5,188.43	5,188.43	Half	HEC-22(2nd Ed)		0	83	0
MH-13A	5,195.21	5,182.59	96	5,188.40	5,188.40	Half	HEC-22(2nd Ed)		0	83	0

DAYTONA - STORM CAD RESULTS

CONDUIT SUMMARY								
Label	Diameter (in)	Material	Flow (cfs)	Capacity (Design) (cfs)	Velocity (ft/s)	Manning's n	Slope (Calculated) (ft/ft)	Headloss (ft)
CO-1	18	Concrete	1.53	7.57	0.87	0.013	0.005	0
CO-2	24	Concrete	5.5	16.46	1.75	0.013	0.005	0.01
CO-3	24	Concrete	5.5	16.02	1.75	0.013	0.005	0.11
CO-4	24	Concrete	5.5	15.63	1.75	0.013	0.005	0.01
CO-8	48	Concrete	88.5	203.5	7.04	0.013	0.02	0.37
CO-9	60	Concrete	260	339.55	13.24	0.013	0.017	0.93
CO-12	18	Concrete	1	14.87	0.57	0.013	0.02	0
CO-13	24	Concrete	0	32.82	0	0.013	0.021	0
CO-15	48	Concrete	63	158.72	5.01	0.013	0.012	0.14
CO-6	30	Concrete	25.5	29.19	5.19	0.013	0.005	0.06
CO-14B	48	Concrete	83	157.7	6.6	0.013	0.012	0.15
CO-5	30	Concrete	20	28.65	4.07	0.013	0.005	0.08
CO-7	30	Concrete	25.5	29.04	5.19	0.013	0.005	0.13
CO-10	60	Concrete	261	338.57	13.29	0.013	0.017	0.57
CO-11	60	Concrete	261	338.97	13.29	0.013	0.017	0.61
CO-14A	48	Concrete	83	159.19	6.6	0.013	0.012	0.14

MH 3-B HEADLOSS	
Flow	63 cfs
Velocity	5 ft/s
Weir Equation	
$Q = 3.33 \times 8 \times \text{Head}^{(3/2)}$	
Weir Head	1.775024 ft
Velocity Head	
$\text{Head} = V^2/2g$	
Velocity Head	0.3881988 ft
Headloss	1.39 ft

Project

Daytona

Computed by

Subject

Tailwater elevation for trunkline
at Pond 6

Checked by

Date

Date

Assume the tailwater elevation is at top of the 60" pipe plus the velocity head.

Determine velocity at the outfall (full flow)

$$Q = 260 \text{ cfs}, \text{ 60" diameter}, A = 19.63 \text{ ft}^2$$

$$V = 13.25 \text{ fps}$$

$$\text{use tailwater elev. } = 5' + \frac{(13.25)^2}{\text{Pipe diam. } 2g}$$
$$= 5' + 2.73' = \underline{\underline{7.73'}}$$

Invert of the 60" RCP @ 5175.20

Tailwater elev. @ 5182.93'

The elevation of the spillway (riser structure) in Pond 6 is at: 5181.40

use elev. @ 5183.0 for tail-water @ Pond 6

CONSTRUCTION PLANS FOR

ALBUQUERQUE METROPOLITAN ARROYO FLOOD CONTROL AUTHORITY

UNSER DIVERSION

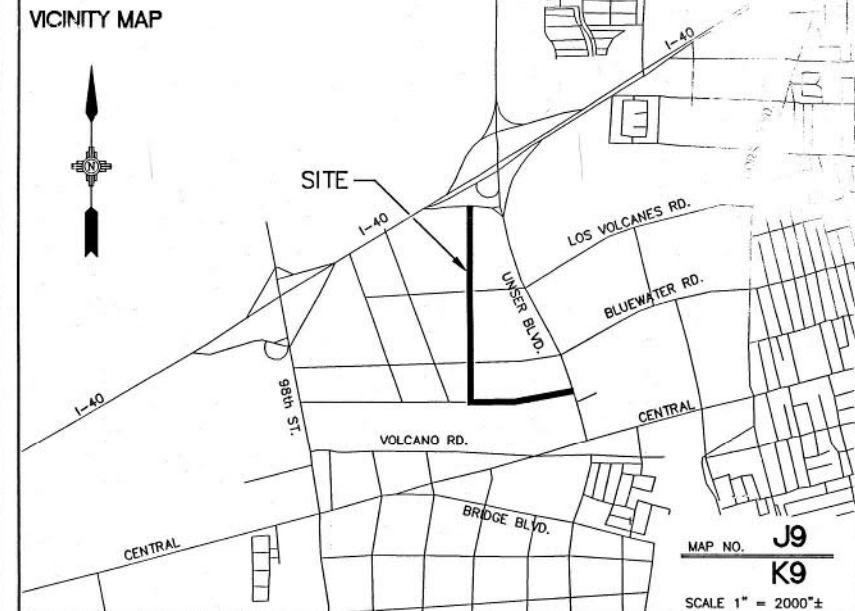
GENERAL NOTES

- ALL WORK DETAILED ON THESE PLANS, EXCEPT AS OTHERWISE STATED OR PROVIDED HEREON WITHIN THE PROJECT CONTRACT DOCUMENTS AND SPECIFICATIONS, SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE NEW MEXICO STATE HIGHWAY DEPARTMENT STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION 1994 EDITION.
- ALL STORM DRAIN CONSTRUCTION AND WORK REQUIRED ON THE WATERLINE OWNED BY THE CITY OF ALBUQUERQUE, EXCEPT WHERE REVISED OR AMENDED BY THESE PLANS AND SPECIFICATIONS, SHALL BE DONE IN ACCORDANCE WITH THE TECHNICAL SPECIFICATIONS, STANDARD DRAWINGS, AND SECTIONS 13 AND 18 OF THE GENERAL CONDITIONS OF THE CITY OF ALBUQUERQUE'S STANDARD SPECIFICATIONS FOR PUBLIC WORKS CONSTRUCTION, 1986 EDITION AS AMENDED THROUGH UPDATE NO. 5.
- TWO (2) WORKING DAYS PRIOR TO ANY EXCAVATION, CONTRACTOR MUST CONTACT ONE CALL SYSTEM, INC., 260-1990, FOR LOCATION OF EXISTING UTILITIES.
- THESE DRAWINGS REFLECT INFORMATION ON UTILITIES GATHERED BY SITE INSPECTION, DISCUSSIONS WITH MUNICIPAL OFFICIALS, AND PREVIOUS CONSTRUCTION DRAWINGS. IT IS POSSIBLE THAT THE EXACT LOCATION OF LINES AND UTILITIES CONVEYED PERTAINS TO THE VICTIMITY OF THE REQUIRED WORK MAY BE DIFFERENT FROM THE LOCATION SHOWN ON THESE DRAWINGS. PRIOR TO CONSTRUCTION, THE CONTRACTOR SHALL EXCAVATE AND VERIFY THE HORIZONTAL AND VERTICAL LOCATIONS OF ALL OBSTRUCTIONS. SHOULD A CONFLICT EXIST, THE CONTRACTOR SHALL NOTIFY THE ENGINEER SO THAT THE CONFLICT CAN BE RESOLVED WITH A MINIMUM AMOUNT OF DELAY.
- ALL GAS, ELECTRIC, TELEPHONE LINES, CABLES, AND APPURTENANCES ENCOUNTERED DURING CONSTRUCTION THAT REQUIRE RELOCATION SHALL BE RELOCATED BY THE RESPECTIVE UTILITY. THE CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATION OF ALL NECESSARY UTILITY RELOCATIONS AND ADJUSTMENTS TO GRADE.
- IT WILL BE THE CONTRACTOR'S RESPONSIBILITY TO PROTECT AND MAINTAIN IN SERVICE ALL EXISTING UTILITIES.
- ALL WORK ON THIS PROJECT SHALL BE PERFORMED IN ACCORDANCE WITH APPLICABLE FEDERAL, STATE, AND LOCAL LAWS, RULES, AND REGULATIONS CONCERNING CONSTRUCTION SAFETY AND HEALTH. THESE DRAWINGS DO NOT INCLUDE NECESSARY COMPONENTS FOR CONSTRUCTION SAFETY WHICH SHALL REMAIN THE CONTRACTOR'S RESPONSIBILITY.
- ALL EXCAVATION/CONSTRUCTION PERMITS WILL BE REQUIRED BEFORE BEGINNING ANY WORK WITHIN THE CITY RIGHT-OF-WAY. AN APPROVED COPY OF THESE PLANS MUST BE SUBMITTED AT THE TIME OF APPLICATION FOR PERMITS.
- THE CONTRACTOR SHALL EXERCISE REASONABLE CARE DURING CONSTRUCTION TO PREVENT THE MOVEMENT OF SEDIMENT FROM THE SITE INTO EXISTING STREETS OR ABUTTING PROPERTY. LOOSE SOIL STOCKPILES DURING CONSTRUCTION ACTIVITIES SHALL BE PROMPTLY CLEANED UP OR PROTECTED FROM BEING CARRIED DOWNSTREAM BY FLOWING WATER.

ABBREVIATIONS

AC	- ASBESTOS CEMENT
ARV	- AIR/VACUUM RELEASE VALVE
B	- BASELINE
BC	- BEGIN CURVE
BCT	- BEGIN CROWN TRANSITION
C	- CONSTRUCT
CAV	- COMBINATION AIR VALVE
CCP	- CONCRETE CYLINDER PIPE
CI	- CAST IRON
CL	- CENTERLINE
COA	- CITY OF ALBUQUERQUE
DD	- DEFLECT DOWN
DIP	- DUCTILE IRON PIPE
DU	- DEFLECT UP
E	- EXISTING
EC	- END CURVE
ECT	- END CROWN TRANSITION
ELEV	- ELEVATION
F-F	- FACE TO FACE
F/F	- FEET/FOOT
FH	- FIRE HYDRANT
FL	- FLOW LINE
FO	- FIBER OPTIC CABLE
G	- GAS
HP	- HIGH PRESSURE
I	- INSTALL
LP	- LIGHT POLE
LT	- LEFT
MH	- MANHOLE
PC	- POINT OF CURVATURE
PCC	- POINT OF COMPOUND CURVATURE
POC	- POINT ON CURVE
PP	- POWER POLE
PRC	- POINT OF REVERSE CURVATURE
PRV	- PRESSURE RELIEF VALVE
PT	- POINT OF TANGENCY
PUE	- PUBLIC UTILITY EASEMENT
R/REL-	- REMOVE & RELOCATE
R/RPLC	- REMOVE & REPLACE
PVC	- POLY VINYL CHLORIDE
R	- REMOVE
REL	- RELOCATE
ROW	- RIGHT-OF-WAY
RT	- RIGHT

SAS	- SANITARY SEWER
SD	- STORM DRAIN
TC	- TOP OF CURB
T	- TELEPHONE
TP	- TOP OF PIPE
TW	- TOP WIDTH
UE	- UNDERGROUND ELECTRIC
VCP	- VITRIFIED CLAY PIPE
VER	- VERIFY LOCATION
W OR WL	- WATERLINE
X	- CROSSING



SHEET INDEX

- COVER PAGE
- KEY MAP, UTILITY CONTACTS AND STOCKPILE SECTIONS
- STORM DRAIN - PLAN AND PROFILE
- STORM DRAIN - PLAN AND PROFILE
- STORM DRAIN/POND CONNECTIONS - PLAN AND PROFILE
- STORM DRAIN/POND CONNECTIONS - PLAN AND PROFILE
- EARTHEN CHANNEL - PLAN AND PROFILE
- POUND 1 - GRADING PLAN
- POUND 2 - GRADING PLAN
- POUND 3 - GRADING PLAN
- POUND 4 - GRADING PLAN
- POUND 5 - GRADING PLAN
- POUND 6 - GRADING PLAN
- OUTLET STRUCTURE - DETAILS AND SECTIONS
- OUTLET STRUCTURE TRASH RACK - DETAILS AND SECTIONS
- RUNDOWN STRUCTURE DETAILS AND SECTIONS
- RUNDOWN STRUCTURE DETAILS AND SECTIONS
- MISCELLANEOUS DETAILS AND SECTIONS
- FENCE DETAILS AND LOW FLOW CHANNEL DETAILS
- PROJECT PLAT

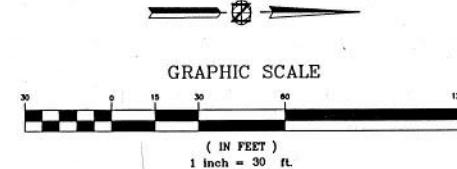
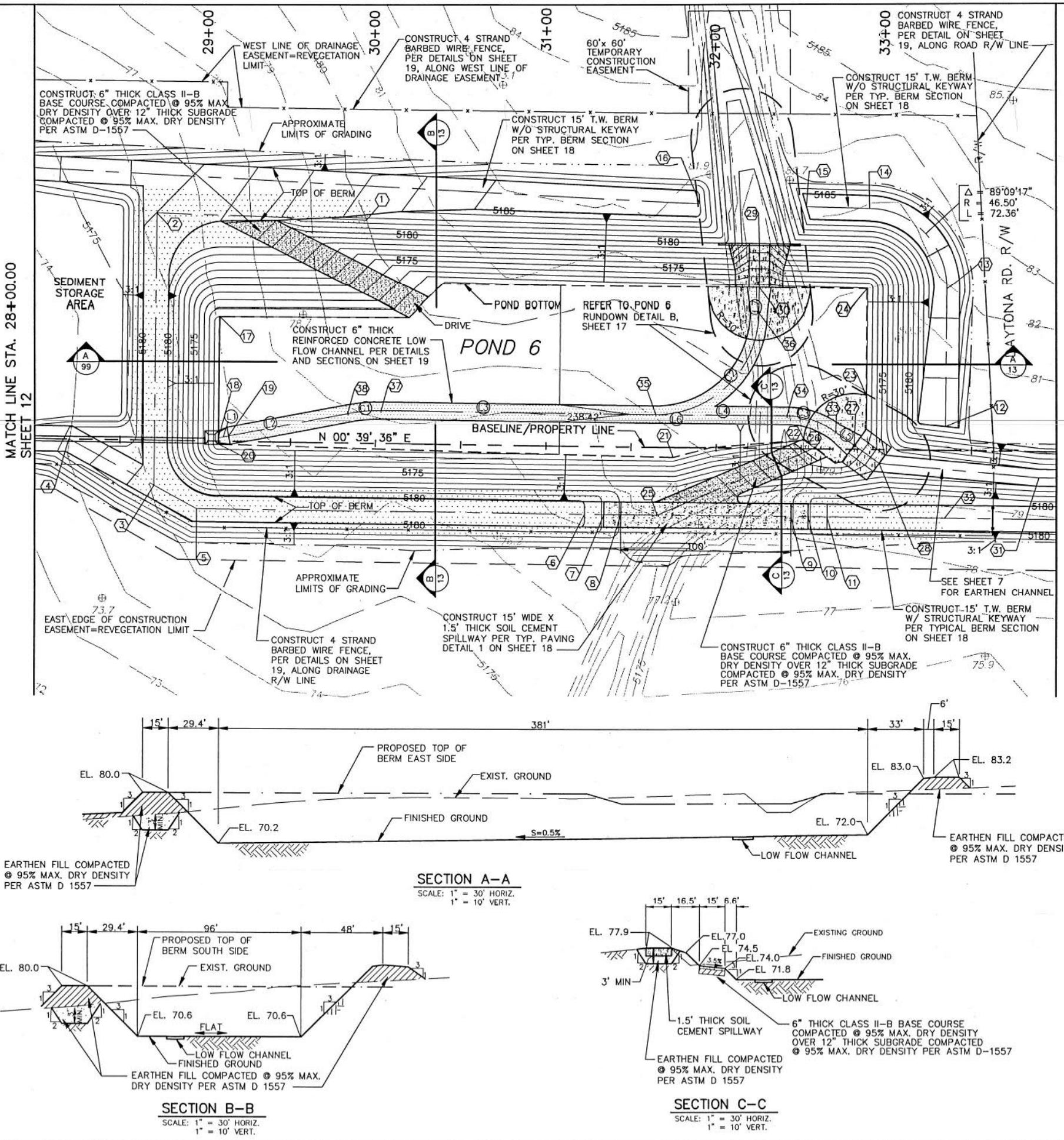
RECORD DRAWING

I, Charles M. Easterling, hereby certify that these drawings have been revised in accordance with the information furnished by Surv-Tek, Inc. to reflect the construction as actually accomplished.

Charles M. Easterling, P.E.
N.M.P.E. No. 6411
Date: 3-8-97

REV.	Sheets	CITY ENGINEER	DATE	USER DEPARTMENT	DATE	USER DEPARTMENT	DATE
APPROVAL OF REVISIONS							

	AMAFCA APPROVED FOR CONSTRUCTION Larry A. Blair Executive Engineer 11/1/96	EASTERLING & ASSOCIATES, INC. CONSULTING ENGINEERS 10131 Coors Rd., NW, Suite H-7/8 ALBUQUERQUE, NEW MEXICO 87114 (505) 898-8021 FAX (505) 898-8501 CITY HYDROLOGY DATE	APPROVED FOR CONSTRUCTION
			SHEET 1 OF 25 PROJECT NUMBER 3324.0



POND 6 POINT DATA					
POINT I.D.	STA.	OFFSET	ELEV.	POINT DESCRIPTION	
NO.		(FT)			
1	29+93.4	129.5' LT	5182.7	¢ N/S KEY WAY @ END OF KEY WAY	
2	28+70.4	131.8' LT	5180.0	¢ N/S KEY WAY AND E/W KEY WAY @ INT.	
3	28+70.3	26.3' RT	5180.0	¢ N/S AND E/W BERMS @ INT.	
4	28+20.0	0.0	5178.1	¢ ACCESS RD/BERM @ ANGLE POINT	
5	28+95.5	40.0' RT	5180.0	¢ BERM @ ANGLE POINT	
6	31+23.2	40.0' RT	5180.0	¢ BERM @ TOP OF SLOPE	
7	31+34.6	40.0' RT	5178.9	¢ SPILLWAY PAVING @ SOUTH EDGE OF PAVING	
8	31+44.6	40.0' RT	5177.9	¢ SPILLWAY PAVING @ TOE OF SLOPE	
9	32+44.6	40.0' RT	5177.9	¢ SPILLWAY PAVING @ TOE OF SLOPE	
10	32+54.6	40.0' RT	5178.9	¢ SPILLWAY PAVING @ NORTH EDGE OF PAVING	
11	32+65.7	40.0' RT	5180.0	¢ BERM @ TOP OF SLOPE	
12	33+34.5	14.0' LT	5182.0	¢ E/W BERM @ TOP OF SLOPE	
13	33+34.6	93.0' LT	5184.4	¢ E/W BERM @ P.T.	
14	32.88.8	139.8' LT	5185.0	¢ N/S BERM @ P.C.	
15	32.51.6	140.3' LT	5185.0	¢ N/S BERM @ TOP OF SLOPE	
16	31+89.0	141.4' LT	5185.0	¢ N/S BERM @ TOP OF SLOPE	
17	29+07.8	72.4' LT	5170.5	S.W. CORNER OF POND BOTTOM	
18	29+07.78	2.00' LT	5169.50	¢ OF LOW FLOW CHANNEL @ FACE OF OUTLET STRUCTURE	
19	29+13.67	3.17' LT	5169.80	¢ OF LOW FLOW CHANNEL @ END OF TRANSITION	
20	29+07.8	2.0' RT	5170.00	S.E. CORNER OF POND BOTTOM	
21	31+74.8	5.9' RT	5171.4	EAST SIDE OF POND BOTTOM @ ANGLE POINT	
22	32+51.3	5.7' LT	5171.8	EAST SIDE OF POND BOTTOM @ EDGE OF SOIL CEM. PAV.	
23	32+87.9	31.5' LT	5172.0	NORTH SIDE OF POND BOTTOM @ EDGE OF SOIL CEM. PAV.	
24	32+87.8	93.0' LT	5172.0	N.W. CORNER OF POND BOTTOM	
25	31+66.0	40.0' RT	5177.9	¢ OF SPILLWAY PAVING AND MAINT. RAMP @ INT.	
26	32+58.0	0.4' LT	5171.9	¢ OF MAINT. ROAD @ BOTTOM OF POND	
27	32+80.0	2.3' LT	5171.80	¢ OF INLET STRUCTURE & ¢ OF LOW FLOW CHANNEL ¢ EDGE OF POND BOTTOM	
28	32+95.8	8.0' RT	5175.0	¢ OF INLET STRUCTURE @ N. EDGE OF PAVING	
29	32+24.3	115.5' LT	5176.7	¢ OF INLET STRUCTURE @ W. EDGE OF PAVING	
30	32+24.32	93.0' LT	5171.70	¢ OF INLET STRUCTURE & LOW FLOW CHANNEL ¢ WEST EDGE OF POND BOTTOM	
31	33+90.0	15.5' RT	5175.8	¢ OF CHANNEL @ ANGLE POINT	
32	33+34.0	40.0' RT	5180.0	¢ OF N/S BERM @ N. END OF N.S. KEYWAY	
33	32+70.21	9.93' LT	5171.60	¢ OF LOW FLOW CHANNEL @ E.C./START OF WIDTH TRANSITION	
34	32+41.50	19.00' LT	5171.45	¢ OF LOW FLOW CHANNEL @ B.C.	
35	31+64.32	19.00' LT	5171.06	INTERSECTION OF LOW FLOW CHANNELS CENTERLINES	
36	32+24.32	79.00' LT	5171.53	¢ OF LOW FLOW CHANNEL @ E.C./START OF WIDTH TRANSITION	
37	30+03.08	19.00' LT	5170.25	¢ OF LOW FLOW CHANNEL @ E.C.	
38	29+83.57	17.08' LT	5170.16	¢ OF LOW FLOW CHANNEL @ B.C.	

CURVE	RADIUS	LENGTH	TANGENT	DELTA
C1	100.00'	19.64'	9.85"	11°15'07"
C2	60.00'	94.25'	60.00"	90°00'00"
C3	50.00'	30.58'	15.79"	35°02'44"

LINE	DIRECTION	DISTANCE
L1	N10°35'31"W	6.00'
L2	N10°35'31"W	71.27'
L3	N00°39'36"E	161.24'
L4	N00°39'36"E	77.18'
L5	N33°52'23"E	13.24'
L6	S00°39'36"W	238.42'
L7	N89°00'24"W	14.00'

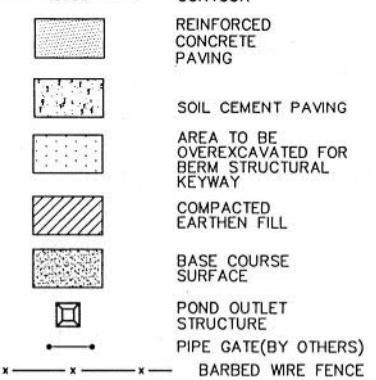
LEGEND

PROPOSED FEATURES

43.9 ♦ SPOT ELEVATION
5135 CONTOUR

Edwin M. Estepes 5-8-97
Edwin M. Estepes, R.P.

Adam Easterling 5-8-97
Charles M. Easterling, P.E. Date:

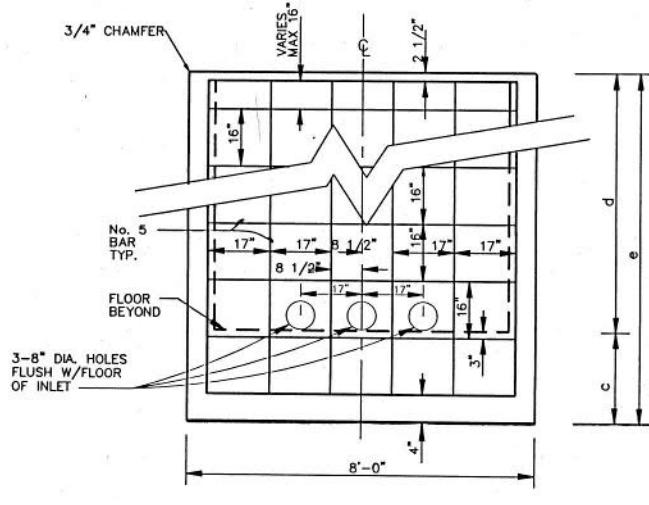


EASTERL & ASSOCIATES, INC.
CONSULTING ENGINEERS
10131 Coors Rd., NW, Suite H-7/8
ALBUQUERQUE, NEW MEXICO 87114
(505) 266-2261 FAX (505) 266-2561

**ALBUQUERQUE METROPOLITAN
ARROYO FLOOD CONTROL
AUTHORITY**

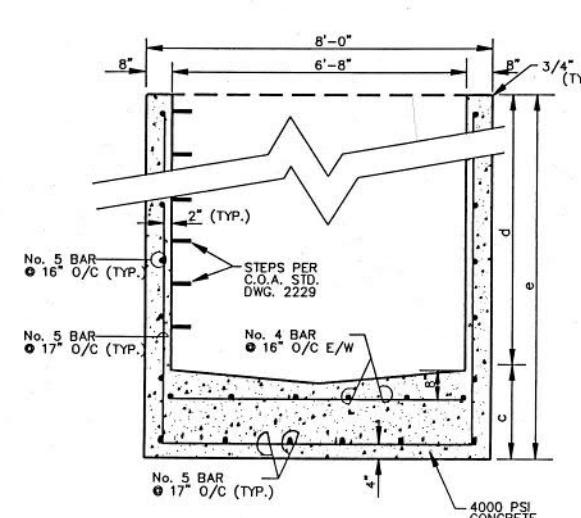
**TITLE: UNSER DIVERSION POND 6
GRADING PLAN AND SECTIONS**

PIPE GATE(BY OTHERS)		APPROVALS			
BARBED WIRE FENCE		APPROVALS			
EXISTING FEATURES		ENGINEER	DATE	ENGINEER	DATE
⊕ 49.8 SPOT ELEVATION		AMAFCA			
— 5150 — CONTOUR					
PROJECT NO		3324.0	MAP NO Z-K9	SHEET 13 OF 25	

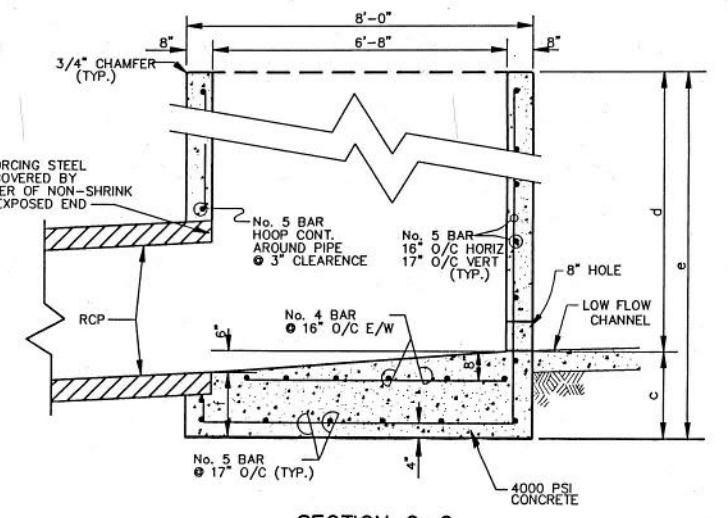


NOTE: ACCURATE PLACEMENT OF REINFORCING STEEL TO THE DIMENSIONS SHOWN IS REQUIRED TO FACILITATE CORING OF HOLES THROUGH THE FRONT WALL OF THE STRUCTURE.

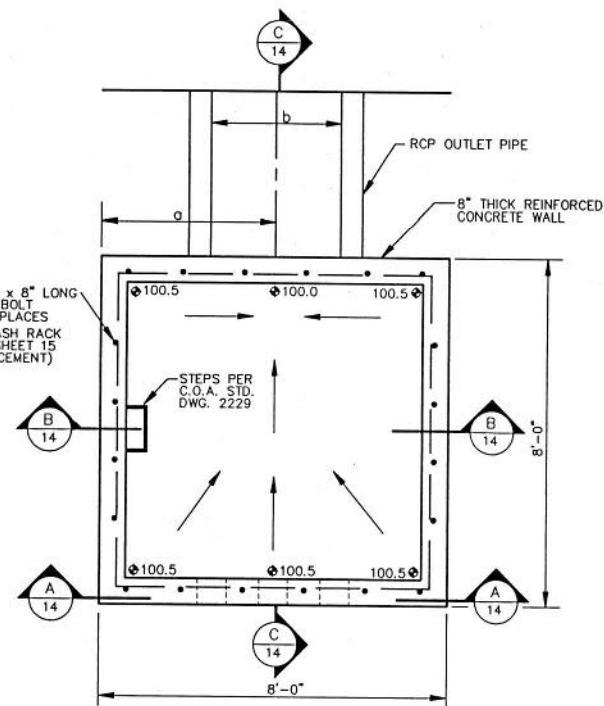
SECTION A-A
NOT TO SCALE



SECTION B-B
NOT TO SCALE



SECTION C-C
NOT TO SCALE



OUTLET STRUCTURE DETAIL - PLAN

The diagram illustrates a rectangular concrete pond structure. The top surface features a triangular roof truss system with a central vent. The left side shows the 'POND BOTTOM' and a 'CONSTRUCT REINFORCED CONCRETE OUTLET STRUCTURE' with three circular components. The right side shows the 'POND SIDE SLOPE'. The bottom front shows the 'BOTTOM OF LOW FLOW CHANNEL' with three '8" DIA. HOLES'. A callout at the top indicates to 'CONSTRUCT WELDED STEEL TRASH RACK PER DETAILS AND SECTIONS ON SHEET 15'.

ISOMETRIC – CONCRETE OUTLET STRUCTURE
NOT TO SCALE

CONCRETE OUTLET STRUCTURE DIMENSIONS							
POND No.	* a	b	c	d	e	f	
1	4'-0"	3'-6"	3'-1"	8'-0"	11'-1"	2'-7"	5141.0
2	4'-0"	4'-0"	2'-11"	7'-4 $\frac{1}{4}$ "	10'-3 $\frac{3}{4}$ "	2'-5"	5144.8
3	4'-0"	3'-6"	2'-5"	5'-0"	7'-5"	1'-11"	5147.5
4	4'-0"	3'-6"	2'-5"	5'- $\frac{1}{4}$ "	7'-6 $\frac{1}{4}$ "	1'-11"	5151.9
5	4'-0"	4'-0"	2'-4"	4'-5"	6'-9"	1'-8"	5164.0
6	2'-0"	3'-0"	2'-9"	6'-6"	9'-3"	2'-3"	5176.0

* THE "a" DIMENSION IS THE DISTANCE FROM THE CENTERLINE OF P TO THE RIGHT OUTSIDE EDGE OF THE OUTLET STRUCTURE.

Add 2.75' for datum
adjustments

RECORD DRAWING

 5-8-97
Charles M. Easterling, P.E.
N.M.D.E. No. G444
Date:

SURVEY INFORMATION		BENCH MARKS		AS BUILT INFORMATION	
FIELD NOTES		STATION NAME: I-40-20A		CONTRACTOR	
NO.	BY	DATE	WORKE BY	DATE	
TOPO	GEO SERVICE	04-93	INSPECTOR'S ACCEPTANCE BY	DATE	
		N.M.S.H.C. BRASS TABLET LOCATED ON THE NORTH SIDE OF U.S. HWY. I-40 AND ABOUT 465' EAST OF UNSER BLVD. OVERPASS		FIELD EVIDENCE BY	
				CHIEF ENGINEER BY	
				CORRECTED BY	
				DATE	
MICRO-FILM INFORMATION					
RECORDED BY _____ DATE _____					
NO. _____					
		NORTHING: 1,490,199.97			
		EASTING: 365,926.16			
		ELEVATION: 5165.89			

A handwritten signature "David L. Miller" is written over a circular professional seal. The seal contains the text "PROFESSIONAL DESIGNER" around the perimeter and "REGISTERED" at the bottom. In the center of the seal is a smaller circle containing the letters "P.D.".

DESIGNED BY ✓
DRAWN BY ✓
CHECKED BY ✓

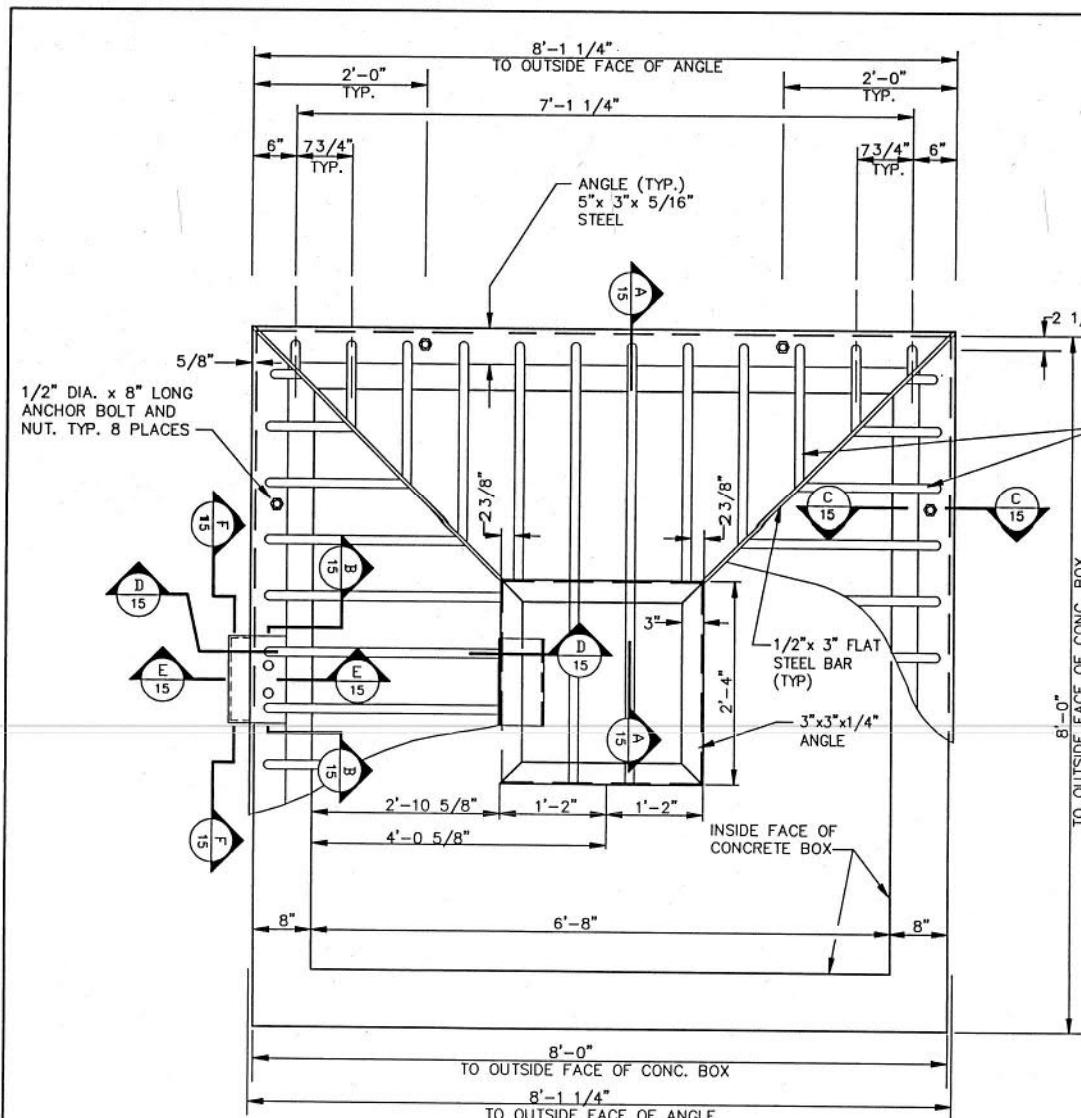
OLITAN
TROL

ALBUQUERQUE METROPOLITAN
ARROYO FLOOD CONTROL
AUTHORITY

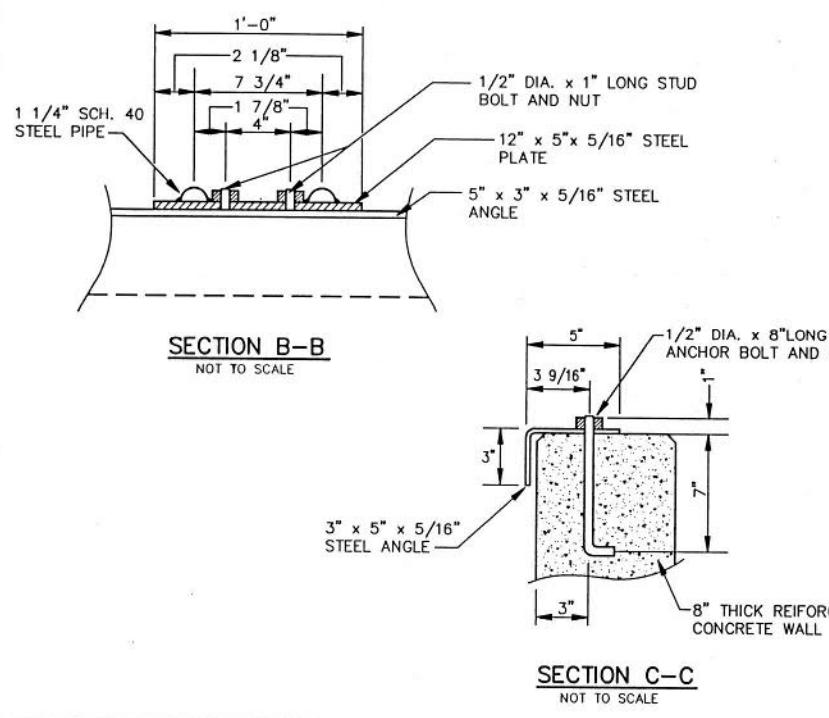
UNSER DIVERSION OUTLET STRUCTURE DETAILS AND SECTIONS

DETAILS AND SECTIONS

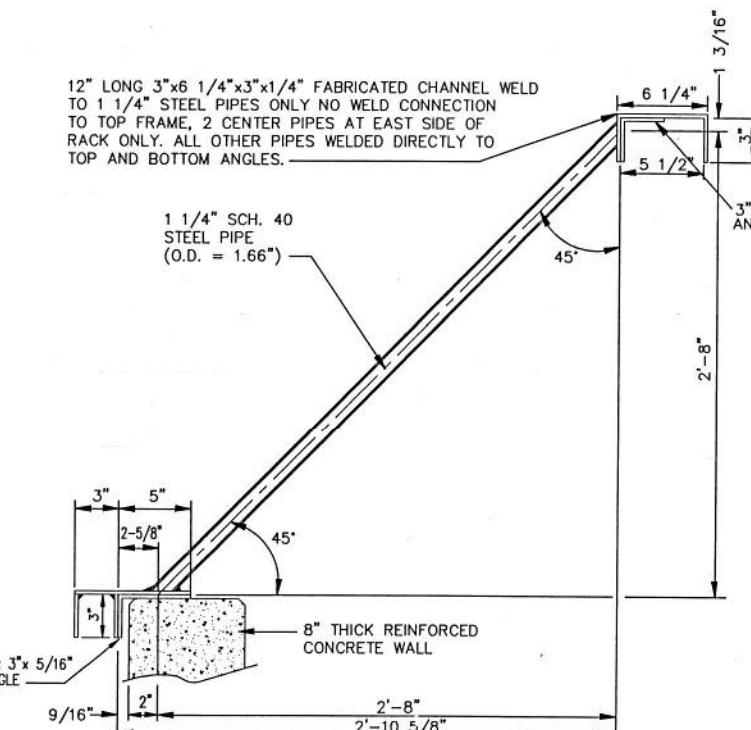
MAP SHEET



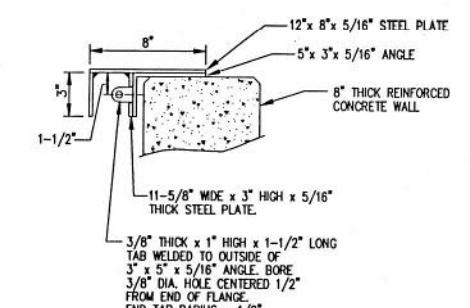
TRASH RACK PLAN



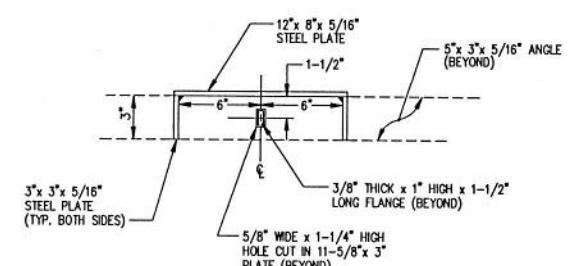
12" LONG 3"x6 1/4"x3"x1/4" FABRICATED CHANNEL WT
TO 1 1/4" STEEL PIPES ONLY NO WELD CONNECTION
TO TOP FRAME, 2 CENTER PIPES AT EAST SIDE OF
RACK ONLY. ALL OTHER PIPES WELDED DIRECTLY TO
TOP AND BOTTOM ANGLES.



SECTION D-D



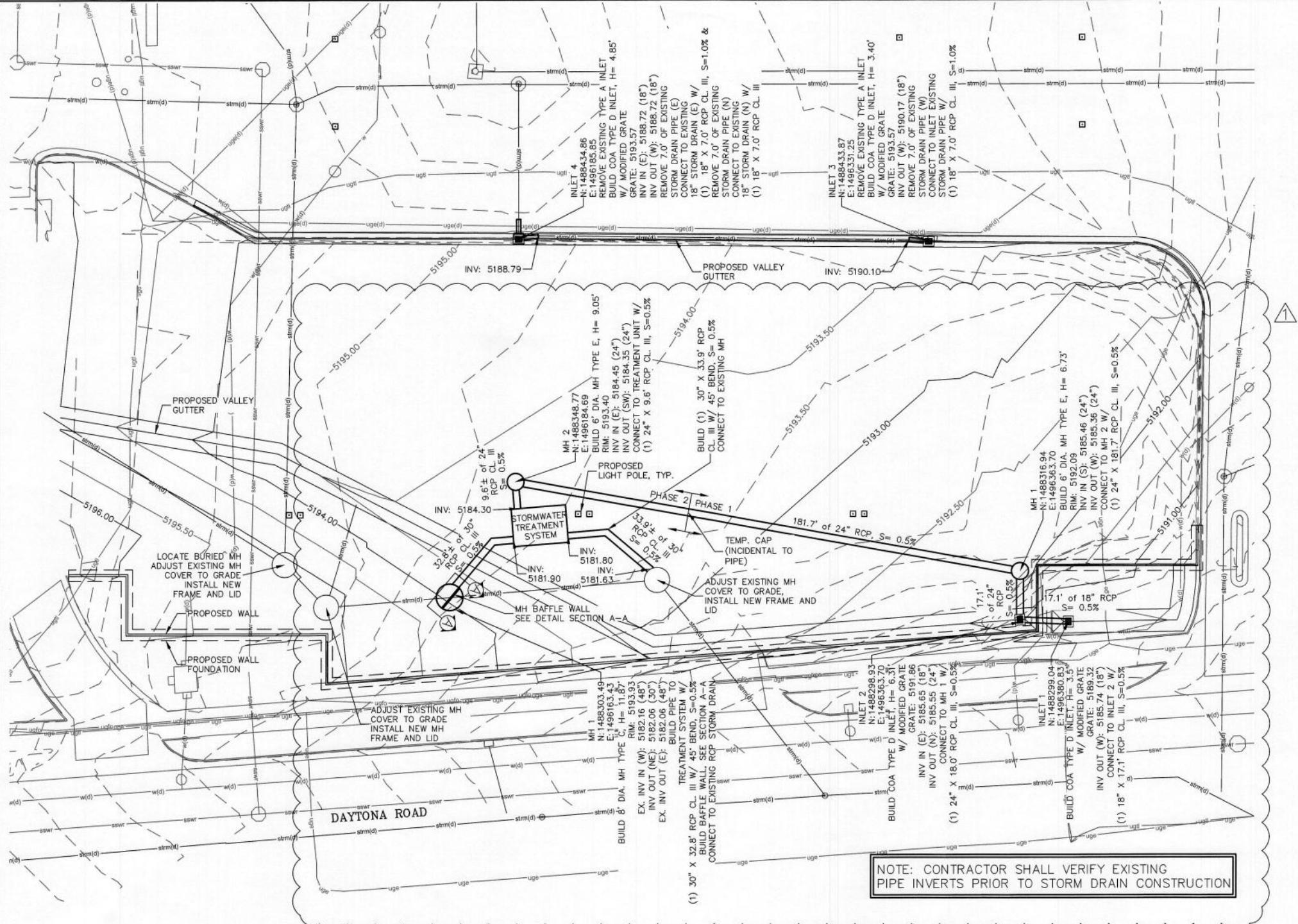
SECTION E-E



SECTION F-F

RECORD DRAWING
I, Charles M. Easterling, hereby certify that these drawings have been revised in accordance with the information furnished by Surv-Tek, Inc. to reflect the construction as actually accomplished.

John E. Easterling 5-8-97
Charles M. Easterling, P.E. Date:
N.M.P.E. No. 6411



GENERAL NOTES:

- PIPE LENGTHS AND SLOPES ARE MEASURED FROM THE CENTER OF MANHOLE TO THE CENTER OF MANHOLE AND FROM THE CENTER OF INLET TO THE CENTER OF INLET.
- SEE SHEET C-10 FOR MODIFIED INLET FRAME AND GRATE DETAILS
- TO CONNECT NEW PIPES AT BENDS, SEE CONCRETE COLLAR DETAIL, SHEET C-11
- FOR MANHOLES, SEE COA DWG. 2101.
- FOR TYPE D INLETS, SEE COA DWG. 2206.
- STORMWATER TREATMENT SYSTEM (STS) SHALL BE A MANUFACTURER DESIGNED STORMWATER POLLUTANTS SEPARATOR SYSTEM WITH A TREATMENT CAPACITY OF AT LEAST 25 CFS AND CAPABLE OF TRAPPING HYDROCARBONS, FLOATABLES, AND 80% OF TOTAL SUSPENDED SOLIDS. PAID FOR UNDER ITEM NO. 915X2, STORMWATER TREATMENT SYSTEM, COMPLETE IN PLACE.

LEGEND:

- strm(d) EXISTING STORM DRAIN SYSTEM
- ssw EXISTING STORM SEWER
- w(d) EXISTING WATER
- uge EXISTING ELECTRIC
- ugf EXISTING FIBER
- ugtl EXISTING TELEPHONE
- PROPOSED INLET
- PROPOSED STORM DRAIN
- EXISTING 0.5' CONTOURS

PROPOSED 0.5' CONTOURS

BUILD 8" WIDE BLOCK OR CONCRETE BAFFLE WALL BETWEEN NEW 30" RCP AND EX. 48" RCP OUTLET. *

* BAFFLE WALL HEIGHT AND LENGTH SHALL BE VERIFIED WITH PROJECT ENGINEER AND STS SUPPLIER PRIOR TO CONSTRUCTION

SECTION A-A
NTS

**PARSONS
BRINCKERHOFF**

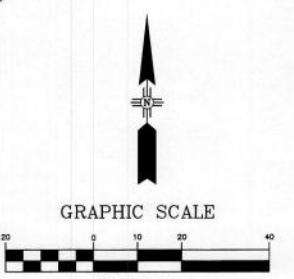
CITY OF ALBUQUERQUE
TRANSIT DEPARTMENT
ABQ RIDE

ABQ RIDE DAYTONA DESIGN

PROPOSED STORM DRAIN PLAN

DESIGN REVIEW COMMITTEE CITY ENGINEER APPROVAL MO./DAY/YR. MO./DAY/YR.

AS BUILT INFORMATION		BENCH MARKS		FIELD NOTES		SURVEY INFORMATION		FIELD NOTES		SURVEY INFORMATION		FIELD NOTES		SURVEY INFORMATION	
NO.	DATE	NO.	DATE	"TRIMBLE VRSnow RTK NETWORK" WITH CHECKS		"TRIMBLE VRSnow RTK NETWORK" WITH CHECKS		NO.	DATE	"TRIMBLE VRSnow RTK NETWORK" WITH CHECKS		NO.	DATE	"TRIMBLE VRSnow RTK NETWORK" WITH CHECKS	
DESIGNED BY:	PB	WORK BY	CONTRACTOR	TO NGS CONTROL STATION "NGS Q 424"		WORK BY	CONTRACTOR	DESIGNED BY:	PB	WORK BY	CONTRACTOR	DESIGNED BY:	PB	WORK BY	CONTRACTOR
DRAWN BY:	PB	INSPECTED BY	MICRO-FILM INFORMATION	RECORDED BY		INSPECTED BY	MICRO-FILM INFORMATION	DRAWN BY:	PB	RECORDED BY		DRAWN BY:	PB	RECORDED BY	
CHECKED BY:	PB	NO.	NO.	NO.		NO.	NO.	NO.	NO.	NO.		NO.	NO.	NO.	

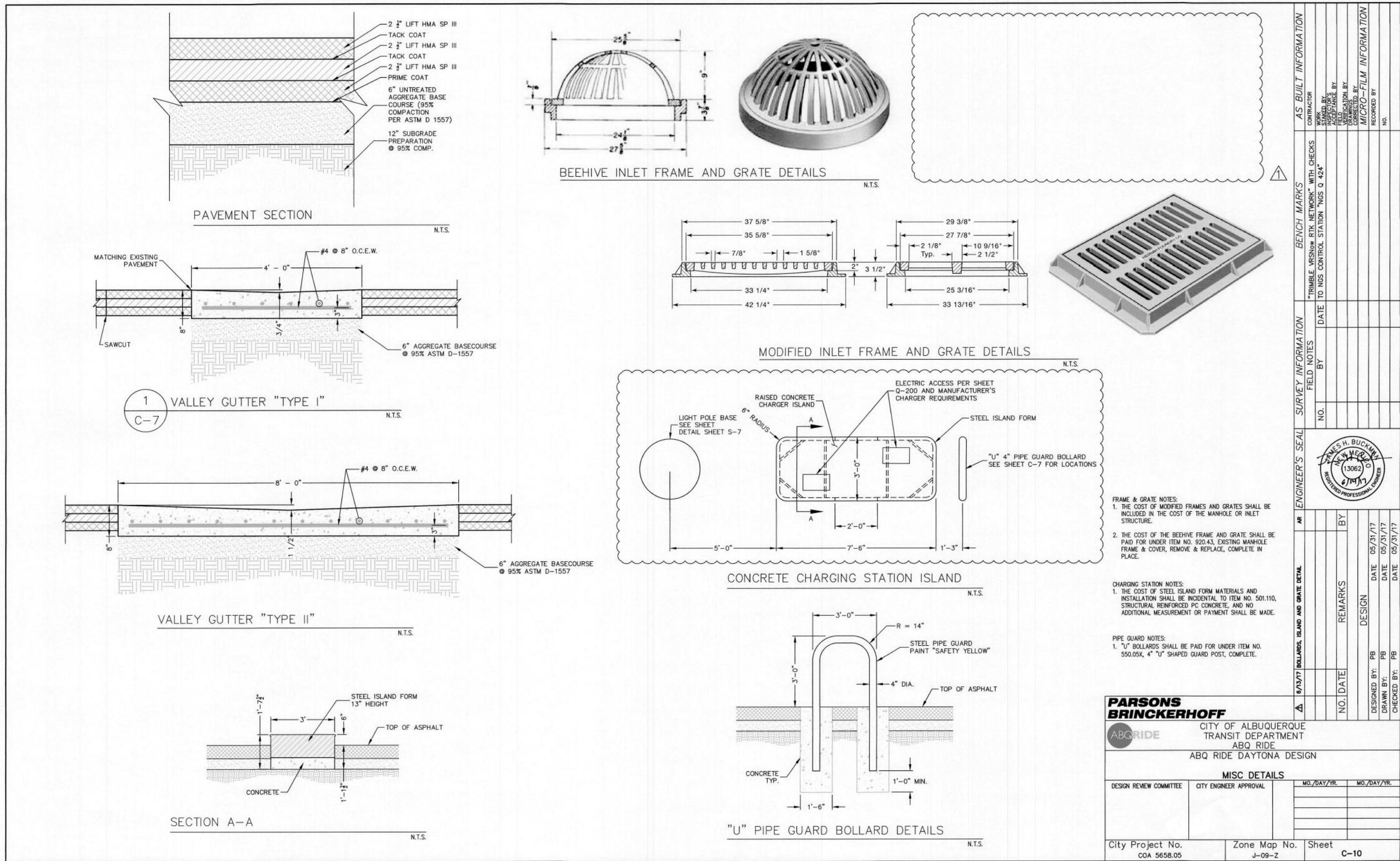


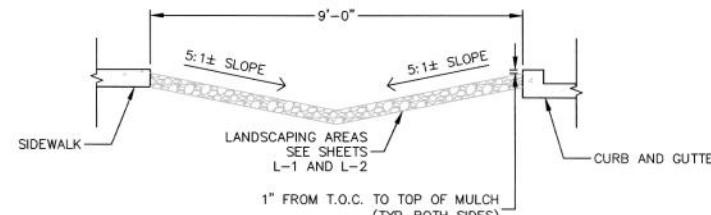
(IN FEET)
1 inch = 20 ft.

City Project No. COA 5658.05

Zone Map No. J-09-Z

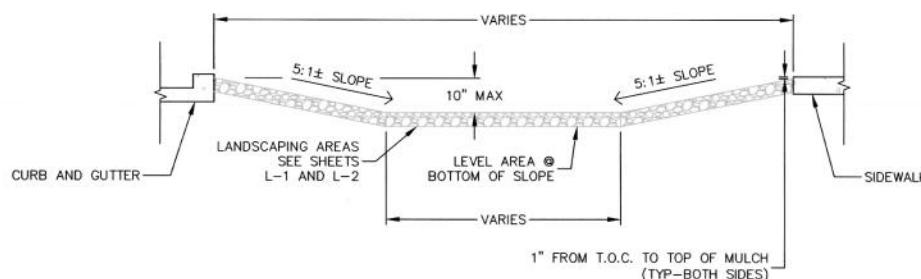
Sheet C-9





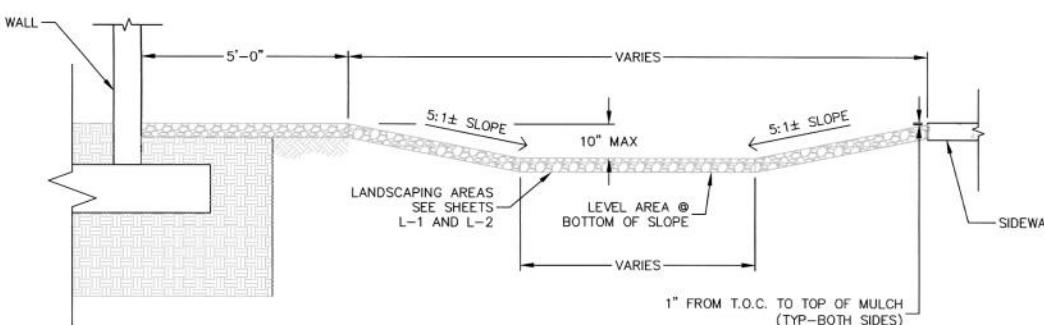
LANDSCAPE AREA SECTION, TYPICAL

N.T.S.



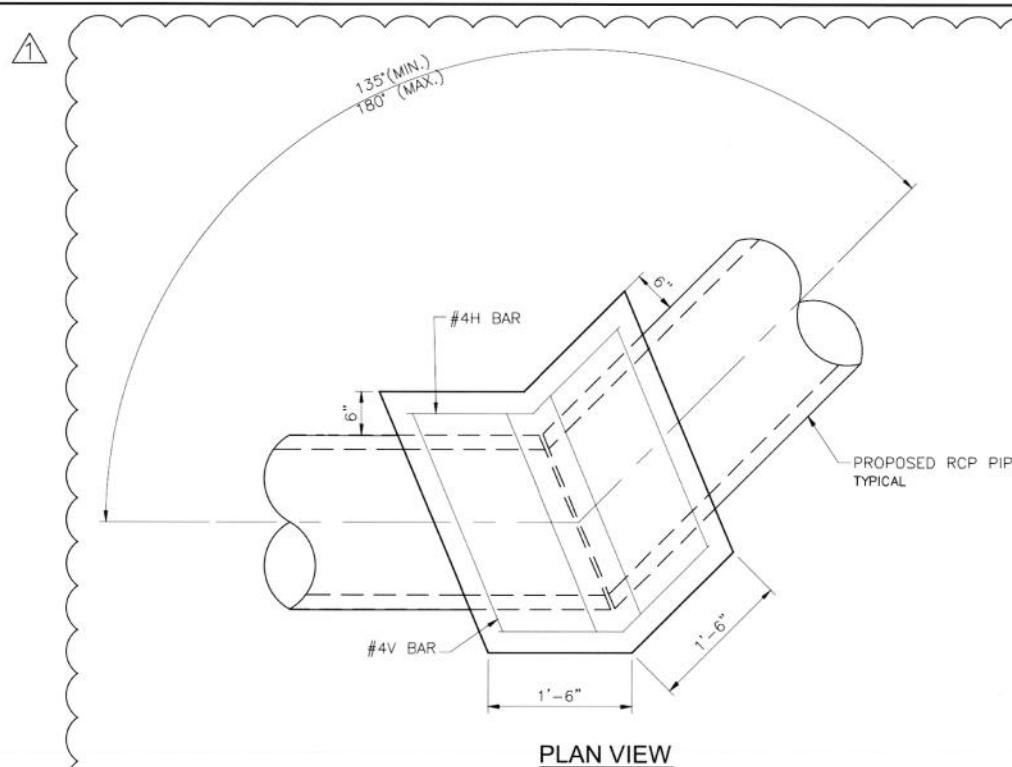
LANDSCAPE AREA SECTION, TYPICAL

N.T.S.

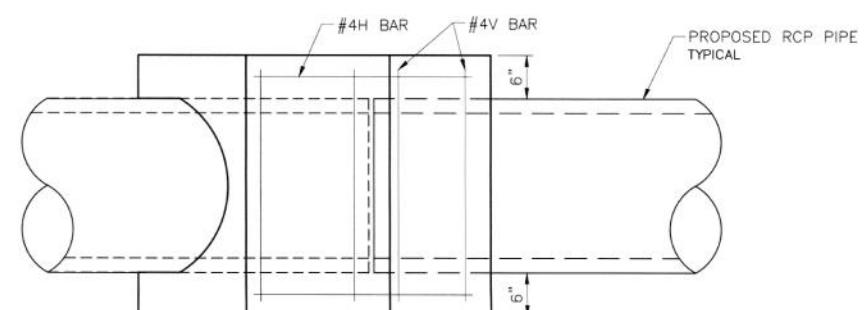


LANDSCAPE AREA SECTION, TYPICAL

N.T.S.

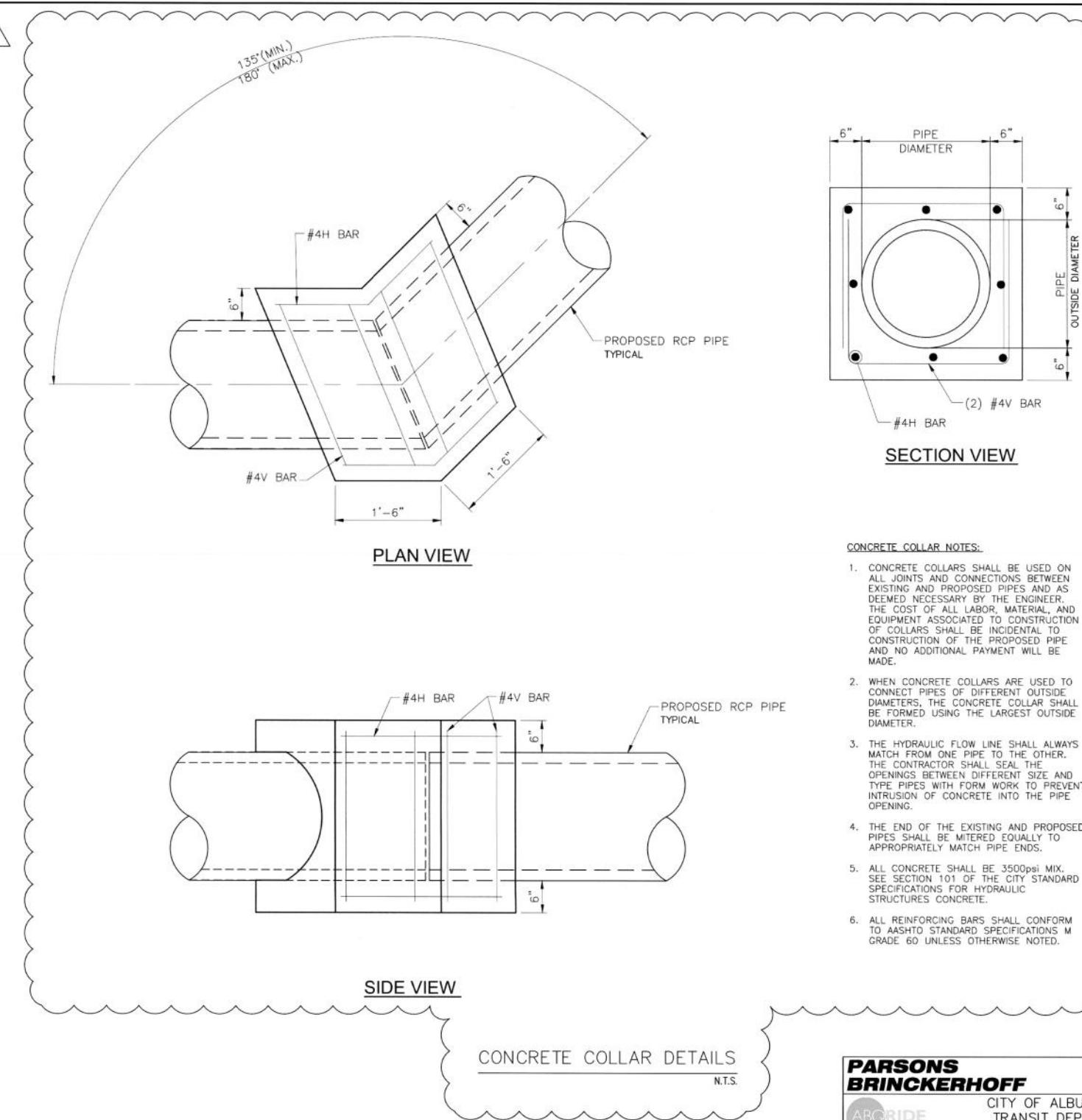


PLAN VIEW



SIDE VIEW

N.T.S.



CONCRETE COLLAR NOTES:

1. CONCRETE COLLARS SHALL BE USED ON ALL JOINTS AND CONNECTIONS BETWEEN EXISTING AND PROPOSED PIPES AND AS DEEMED NECESSARY BY THE ENGINEER. THE COST OF ALL LABOR, MATERIAL, AND EQUIPMENT ASSOCIATED TO CONSTRUCTION OF COLLARS SHALL BE INCIDENTAL TO CONSTRUCTION OF THE PROPOSED PIPE AND NO ADDITIONAL PAYMENT WILL BE MADE.
2. WHEN CONCRETE COLLARS ARE USED TO CONNECT PIPES OF DIFFERENT OUTSIDE DIAMETERS, THE CONCRETE COLLAR SHALL BE FORMED USING THE LARGEST OUTSIDE DIAMETER.
3. THE HYDRAULIC FLOW LINE SHALL ALWAYS MATCH FROM ONE PIPE TO THE OTHER. THE CONTRACTOR SHALL SEAL THE OPENINGS BETWEEN DIFFERENT SIZE AND TYPE PIPES WITH FORM WORK TO PREVENT INTRUSION OF CONCRETE INTO THE PIPE OPENING.
4. THE END OF THE EXISTING AND PROPOSED PIPES SHALL BE MITERED EQUALLY TO APPROPRIATELY MATCH PIPE ENDS.
5. ALL CONCRETE SHALL BE 3500psi MIX. SEE SECTION 101 OF THE CITY STANDARD SPECIFICATIONS FOR HYDRAULIC STRUCTURES CONCRETE.
6. ALL REINFORCING BARS SHALL CONFORM TO AASHTO STANDARD SPECIFICATIONS M GRADE 60 UNLESS OTHERWISE NOTED.

AS BUILT INFORMATION	
CONTRACTOR	TRIMBLE VRSN 2 RTK NETWORK™ WITH CHECKS
STAGED BY	DATE TO NGS CONTROL STATION "NGS Q 424"
ACCURACY BY	
FIELD VERIFICATION BY	
CORRECTED BY	MICRO-FILM INFORMATION
RECORDED BY	NO.



FIELD NOTES	SURVEY INFORMATION	BENCH MARKS
NO.	NO.	NO.

**PARSONS
BRINCKERHOFF**

CITY OF ALBUQUERQUE
TRANSIT DEPARTMENT
ABQ RIDE

ABQ RIDE DAYTONA DESIGN

MISC DETAILS

DESIGN REVIEW COMMITTEE	CITY ENGINEER APPROVAL	MO./DAY/YR.	MO./DAY/YR.

City Project No.
COA 5658.05

Zone Map No.
J-09-Z

Sheet
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