

J11/023

DRAINAGE REPORT
FOR
McDONALD'S RESTAURANT

NOTES:

1. THE SITE IS THE NORTH-WEST CORNER OF
COORS RD & HANOVER RD
2. EXISTING TOPO SHOWN ON ARCHITECTURAL SURVEY
3. PROPOSED STREET IMPROVEMENTS ARE TAKEN FROM
PLANS PREPARED BY LEVERTON-DENNEY & ASSOC.
4. PROPOSED STORM DRAIN SYSTEM TO BE
DESIGNED TO DRAIN 100' LF BEHIND PROPERTY
LINE ALONG COORS AVE; FOR A 25 YR FREQUENCY
AND A RUNOFF FACTOR OF 0.80 - PER LEVERTON
DENNEY.
5. LOT AREA = 0.846 AC.
6. REF: MASTER PLAN OF DRAINAGE, CITY OF
ALBUQUERQUE, NEW MEXICO & ENVIRONS 1963
CHARTS, MAPS & TABLES, PREPARED BY GORDON
HERKENHUFF & ASSOC.

292-1736

DEVELOPED CONDITION

$$A = 0.71 \text{ AC why not } .846$$

$$C = 0.90 \text{ (PAVED PARKING LOT)}$$

USING THE MODIFIED RATIONAL METHOD HYDROGRAPHS

$$Q = C_p C_L A$$

FOR 100 YR RETURN FREQUENCY $C_A = 1.25$ $C \times C_A \times A = 0.8$

$$C_A C \text{ max } 1.0$$

STORM DURATION MIN.	RAINFALL INTENSITY "/HR	PEAK RUNOFF RATE cfs	STORM RUNOFF VOLUME	RELEASE VOLUME CU FT	STORAGE REQ'D. CU FT
		^{3.46}			
10	5.40	4.56 4.32	2592	1140	1452 800
15	4.72	3.79 3.78	3402	1710	1692 1228 1128
20	4.2	3.55 2.98 3.36	4032	2280	1752 Vol. $\leq$ 1226 Req'd
30	3.44	2.91 2.75	4950	3420	1540 1173
40	2.90	2.45 2.32	5568	4560	1008
50	2.52	2.13 2.02	6060	5700	360
60	2.22	1.87 1.78	6408	6840	-432

LENGTH OF FLOW: 378 LF
HEIGHT: 1.7'
SLOPE: 0.449%

ASSUME $V = 38 \text{ FT/MIN ON ASPHALT}$
 $T_c = 378' / 38 \approx 10 \text{ MIN.}$

QUANTITY OF RUNOFF PERMITTED TO
DRAIN TO PROPOSED CATCH BASIN

$$A = 0.59 \text{ AC.}$$

$$T_c = 10 \text{ MIN}$$

$$C = 0.80$$

$$C_{25} = 4.03$$

$$Q_{25} = 0.8 \times 4.03 \times 0.59 = 1.90 \text{ cfs.}$$

P&F DRAINAGE REPORT PREPARED BY LEVERTON.
DENNY - CONVERSATION WITH MR LOU GROSS

Storage

$$(4.56 - 1.9) 60 \frac{11}{2} = 878$$

$$(3.99 - 1.9) 60 (10) = 1254$$

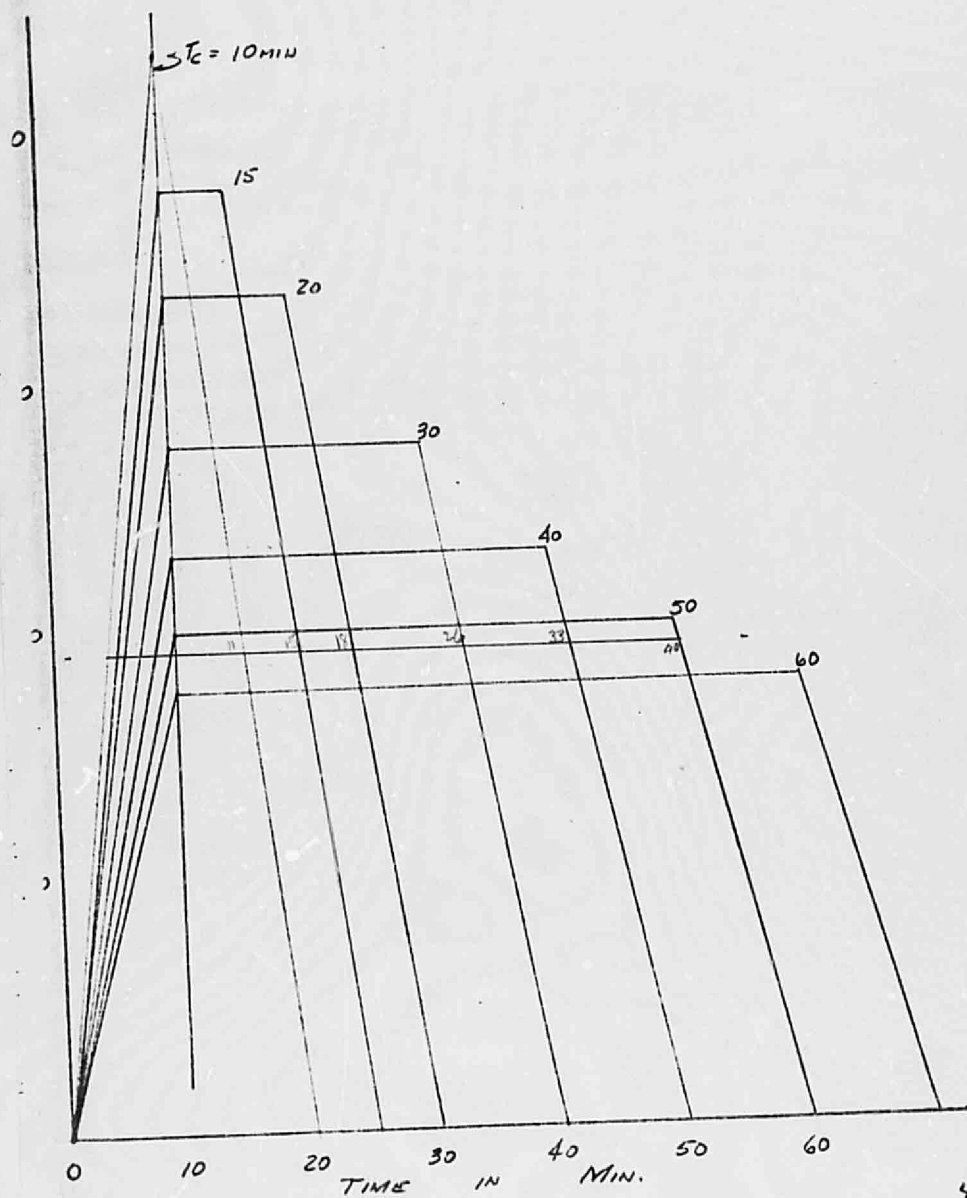
$$(3.55 - 1.9) (60) (14) = 1386$$

$$(2.91 - 1.9) (60) (23) = 1394$$

$$(2.45 - 1.9) (60) (31.5) = 1040$$

$$(2.13 - 1.9) (60) (40.5) = 559$$

MODIFIED RATIONAL METHOD HYDROGRAPH.



STORM RUNOFF VOLUME CALCULATION

10 MIN

$$2 \left[\frac{4.32 \times 10}{2} \right] \times 60 = 2592$$

15 MIN

$$3.78 \times 5 \times 60 + 2 \left[\frac{3.78 \times 10}{2} \right] 60 = 3402$$

$$= 1134 + 2268$$

20 MIN

$$3.36 \times 10 \times 60 + 2 \left[\frac{3.36 \times 10}{2} \right] 60 = 4032$$

$$= 2016 + 2016$$

30 MIN

$$2.75 \times 20 \times 60 + 2 \left[\frac{2.75 \times 10}{2} \right] 60 = 4950$$

$$= 3300 + 1650$$

40 MIN

$$2.32 \times 30 \times 60 + 2 \left[\frac{2.32 \times 10}{2} \right] 60 = 5568$$

$$= 4176 + 1392$$

50 MIN

$$2.02 \times 40 \times 60 + 2 \left[\frac{2.02 \times 10}{2} \right] 60 = 6060$$

$$4848 + 1212$$

60 MIN

$$1.78 \times 50 \times 60 + 2 \left[\frac{1.78 \times 10}{2} \right] 60 = 6408$$

$$5340 + 1068$$

WIER CALCULATION

$$Q \cong 1.9 \text{ cfs} \quad Q = CLH^{3/2}$$

$$Q = 2.8 \times 2 \times 0.5^{3/2} = 1.98 \text{ cfs}$$

OK. USE 2' CURB OPENING.

$$C = 2.8 \text{ (KING'S HANDS)} \\ L = 2.0' \\ H = 0.5' \text{ (6" CURB)}$$

5/6

STORAGE VOLUME CALCULATION

AREA BEHIND CURB OPENING,
BUT NOT OVER TOP OF CURB ELEVATION

$$\text{AREA} = 14.5 \text{ IN. SQ} = 5800 \text{ SQ FT}$$

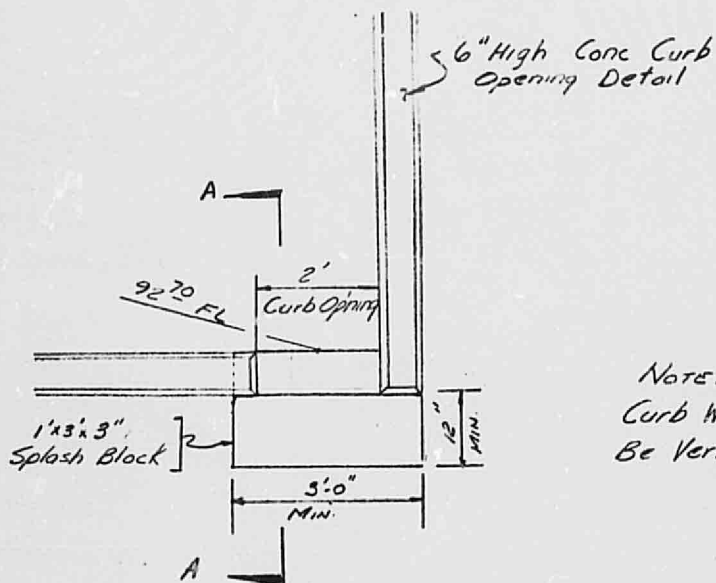
$$\text{AVERAGE DEPTH} = 0.3'$$

$$\text{VOLUME} = 1740 \text{ CU. FT.}$$

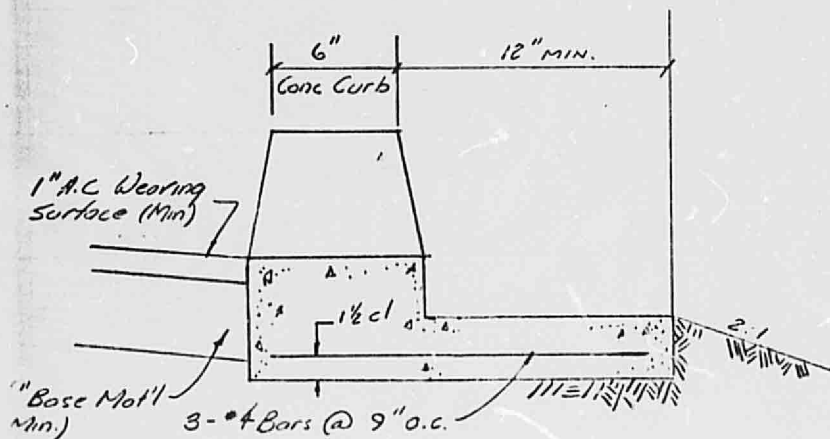
$$\text{VOLUME REQ'D} = 1752 \text{ CU FT. (SEE HYDROGRAPH TABLE)}$$

FOR ADDED PROTECTION, CONST
POND AFTER CURB OPENING.

$$\text{VOLUME} = 15' \times 15' \times 2' = 450 \text{ CU FT.} \quad \therefore \text{OK}$$



NOTE:
Curb Walls May
Be Vertical



SECTION "A-A"