DRAINAGE REPORT

Bureau of Reclamation & Social Security Administration Building Located at 555 Broadway NE

April 11, 2002

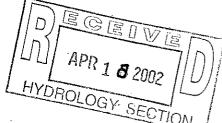
Prepared For:

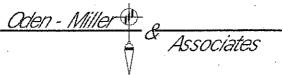
AARDEX Corporation

12340 West Alameda Parkway, Suite 220 Lakewood, Colorado 80228-2841



Prepared By:





P.O. Box 1976 Moriarty, NM 87035 (505) 832-1425

DRAINAGE AND TRANSPORTATION INFORMATION SHEET

(REV. 1/11/2002)

•		(J-14/D143)
	Bureau of Reclamation & Social	
	Security Administration Building	
PROJE	:CI IIILE: located at 555 Broadway N.E.	ZONE MAP/DRG. FILE #: J-14-Z
DRB #:	EPC#:	WORK ORDER#:
		WOTIK OT DEITH.
LEGAL	DESCRIPTION: Parcel 1 - Marquette Subdivision	•
CITY A	DDRESS: 555 Broadway Blvd. N.E.	
•		3
ENGINE	ERING FIRM: Oden-Miller & Associates	Courter Verlyn Miller
Litairi	ADDRESS: P.O. Boy 1976	CONTACT: Verlyn Miller PHONE: 832-1425
•	ADDRESS: P.O. Box 1976	PHONE: 632~1425
	CITY, STATE: Moriarty, NM 87035	ZIP CODE: <u>87035</u>
OWNER	Aardex Corporation	Don Wooles
OANIACI	ADDRESS: 12340 West Alameda Parkway, Suite 220	CONTACT: Ben Weeks PHONE: 303-987-9000
		PHONE: 303-987-9000
	CITY, STATE: Lakewood, CO	ZIP CODE: 80228-2841
40010		
ARCHIT	ECI;	_ CONTACT:
	ADDRESS;	PHONE:
1	CITY, STATE:	ZIP CODE:
SURVE	YOR: Clint Sherrill & Associates ADDRESS 730 San Mateo S.E.	CONTACT: Clint Sherrill PHONE: 505-256-7364
	ADDRESS 730 San Mateo S.E.	PHONE: 505-256-7364
	CITY, STATE: Albuquerque, NM	ZIP CODE: 87108
•		ZII CODE. 07100
CONTR	ACTOR:	_ CONTACT:
	ADDRESS:	PHONE.
	CITY, STATE:	PHONE: ZIP CODE:
		ZIP CODE;
•		
CHECK	TYPE OF SUBMITTAL: CHE	OVER OR A PER PARTY OF THE PART
	<u>~</u>	CK TYPE OF APPROVAL SOUGHT:
	DD UNIO E DI AU	SIA / FINANCIAL GUARANTEE RELEASE
	OON OF THE COLUMN AS A SECOND	PRELIMINARY PLAT APPROVAL
v	CONCEPTUAL GRADING & DRAINAGE PLAN	S. DEV. PLAN FOR SUB'D, APPROVAL
	GRADING PLAN	S. DEV. PLAN FOR BLDG. PERMIT APPROVAL
	EROSION CONTROL PLAN ENGINEER'S CERTIFICATION (HYDROLOGY)	_ SECTOR PLAN APPROVAL
	ENGINEER'S CERTIFICATION (HYDROLOGY)	FINAL PLAT APPROVAL
	CLOMPLOME	FOUNDATION PERMIT APPROVAL
	TRAFFIC CIRCULATION LAYOUT (TCL) ENGINEERS CERTIFICATION (TCL)	BUILDING PERMIT APPROVAL
	ENGINEERS CERTIFICATION (TCL)	CERTIFICATE OF OCCUPANCY (PERM.)
		CERTIFICATE OF OCCUPANCY (TEMP.)
		_ GRADING PERMIT APPROVAL
	·	PAVING PERMIT APPROVAL
		WORK ORDER APPROVAL
	·	
	· · · · · · · · · · · · · · · · · · ·	OTHER (SPECIFY)
		So-19 D) 医医医DV 图 D)
WASA	PRE-DESIGN CONFERENCE ATTENDED:	
Y.	YES	[[]]] ADD
_A	NO	* APR 1 3 2002 U)
	COPY PROVIDED	
	OOL LE HOAIDED.	HYDROLOGY SECTION
	, ·	L HYDROLOGY SECTION
	/	1 1
DATE	UDWITTED HORD 1/2 2	
$\cup A : \vdash S$	UBMITTED: APRIL 16, 2002 BY:	

Requests for approvals of Site Development Plans and/or Subdivision Plats shall be accompanied by a drainage submittal. The particular nature, location and scope of the proposed development defines the degree of drainage detail. One or more of the following levels of submittal may be required based on the following:

- 1. Conceptual Grading and Drainage Plan: Required for approval of Site Development Plans greater than five
- 2. Drainage Plans: Required for building permits, grading permits, paving permits and site plans less than five (5)
- 3. Drainage Report: Required for subdivisions containing more than ten (10) lots or constituting five (5) acres or

TABLE OF CONTENTS

1.0 PURPOSE & SCOPE	. 1
2.0 EXISTING CONDITIONS	. 1
3.0 PROPOSED CONDITIONS	1
4.0 HYDROLOGY	2
5.0 HYDRAULICS	3
6.0 CONCLUSION	. 3
LIST OF TABLES	
TABLE 4-1 RAINFALL DEPTHS	2
TABLE 4-2 HYDROLOGIC SUMMARY OF RESULTS	2
APPENDICES	
APPENDIX A HYDROLOGY SPREADSHEETS	6
APPENDIX R HVDR ALII IC CALCULATIONS	7

1.0 PURPOSE & SCOPE

The purpose of this report is to provide a hydrologic analysis of existing and post-developed conditions, demonstrate existing and post-developed drainage patterns, and to develop a grading & drainage plan for the management of post-developed flows.

2.0 EXISTING CONDITIONS

The subject site is located at 555 Broadway NE at the corner of Broadway and Marquette (see Figure 2-1). The proposed site currently consists of 3.27 acres of undeveloped land. The site was previous occupied by the Coca-Cola Bottling Company Facility. The site is currently surrounded on all four sides by curb & guttered streets with an old perimeter sidewalk. Off-site drainage does not appear to adversely impact the site due to the presence of curb and guttered streets and sloping topography adjacent to the site.

The ground cover on-site consists of bare ground with little or no vegetation. Under existing conditions, the site may be classified under Land Treatment C as per the City of Albuquerque DPM, Section 22.2.

3.0 PROPOSED CONDITIONS

The proposed development will consist of a two story commercial building with over 50,000 sf of space. The building will be used by the Bureau of Reclamation and the Social Security Administration. The site also consists of asphalt paved parking areas, sidewalks and numerous landscaped areas.

As per previous meetings with the City of Albuquerque Hydrology Section, it was determined that no on-site retention or detention ponding would be required by this project. It was determined that the "free release" of storm water runoff would be allowed based on the following conditions:

1) Post-developed flows would be dispersed to both Roma Avenue (north) and Marquette Avenue (south) so that the numerous curb inlets in the area could collect the runoff. The entire site would not discharge to one point on the property.

2) Verify that the storm sewer system in Commercial and John Street connected to the 72-inch main in Lomas Boulevard.

In order to satisfy the first requirement, the site was divided into five on-site drainage basins, A – D (see Figure 3-1), in order to disperse the flows to various locations. To further ensure that the capacities of drop inlets in Marquette, Commercial and Roma were not exceeded, the drainage plan includes two on-site drop inlets, which will collect runoff from Basins C & D. Runoff from Basins C & D will be collected by two Type D Drainage Inlets on-site and discharged directly into the storm sewer system in Commercial Street via a 12-inch RCP storm drain pipe.

To satisfy the second condition, as-built plans were obtained from the Records Department and the City to verify that the existing storm sewer system in Commercial and John Streets does in fact connect to the 72-inch main storm sewer line in Lomas Boulevard. A full size print of the as-built plan and profile sheet has been included as an attachment to the grading and drainage plan for the City's reference.

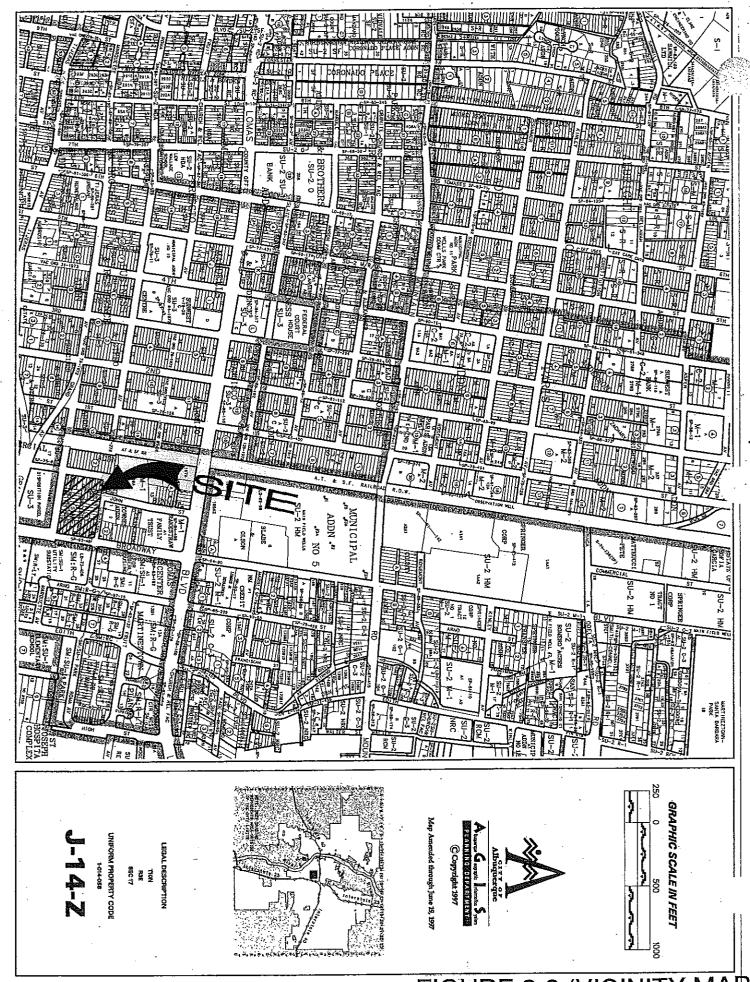
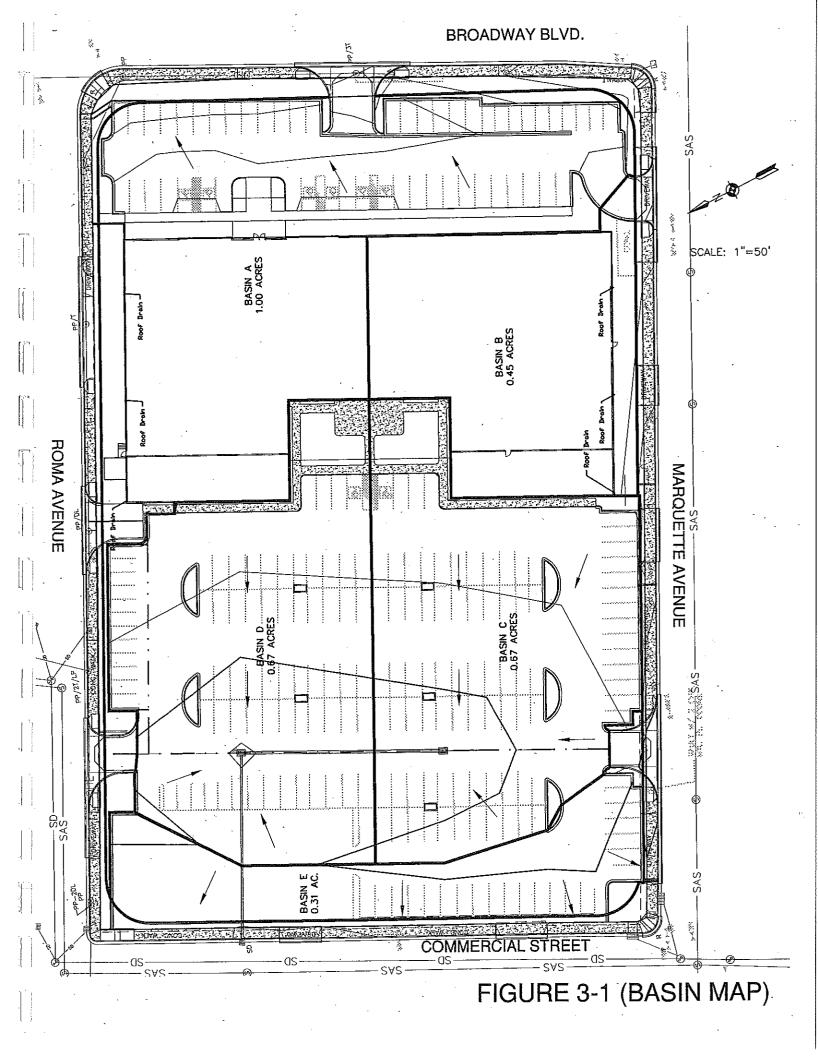


FIGURE 2-2 (VICINITY MAP)



Other proposed drainage improvements on-site include splash blocks at roof drains to dissipate the energy in the runoff before discharge and to minimize potential erosion to landscaped areas. A minimum water block height of6-inches has been provided at all driveway entrances in order to maintain curb height and prevent runoff from entering the site. In order to ensure proper parking lot drainage, care has been taken to maintain a 1.5% slope or better in all paved parking lot areas. Concrete valley gutter is specified in areas where longitudinal slopes are 1% or less.

4.0 HYDROLOGY

The hydrologic calculations in this section will quantify the storm water runoff from the site basins for the 10-year, 24-hour and 100-year, 24-hour storm events. The methodology used is per "Section 22.2, Part A, Development Process Manual, Volume 2" dated January 1993. The subject site lies within Precipitation Zone 2 as per Table A-1. The 10-year and 100-year rainfall depths are outlined in Table 4-1.

TABLE 4-1 Rainfall Depths

1	0-Year Even	ıt	16	00-Year Eve	nt
1-Hour	6-Hour	24-Hour	1-Hour	6-Hour	24-Hour
1.34 in	1.57 in	1.83 in	2.01 in	2.35 in	2.75 in

The time of concentration for all basins in this analysis are considered to be a minimum value of 12 minutes. As such, Tables A-8 and A-9 in the DPM are used to compute volumetric runoff and peak discharge values for the 10-year and 100-year events. A detailed hydrology spreadsheet is included in Appendix A, which indicates the total area of each basin, the total acreage for each land treatment category per basin and the computed discharge values. A spreadsheet is provided for both the 10-year and 100-year events. A summary of the results of this analysis is provided in Table 4-2.

TABLE 4-2
Hydrologic Summary of Results

Basin #	Basin Area (acres)	V _{10yr-24hr} (acre-feet)	Q _{10-yr} (cfs)	V _{100yr-24hr} (acre-feet)	Q 100-yr (cfs)
EXISTING	CONDITIONS				
Site	3.10	0.134	5.3	0.292	9.7
PROPOSED	CONDITIONS	3			sald A
A	1.00	0.120	2.9	0.193	4.4
В	0.45	0.055	1.3	0.087	2.0
C	0.67	0.085	. 2.0	0.135	3.1
D	0.67	0.086	2.0	0.136	3,1
Е	.0.31	0.040	1.0	0.064	1,4

5.0 HYDRAULICS

Hydraulic calculations are provided in Appendix B for all proposed hydraulic structures on-site including drainage inlets and storm sewer pipes. The DPM hydraulic charts are used to determine the drainage inlet capacities and a computer program will be used to verify the capacity of proposed storm sewer pipes.

6.0 CONCLUSION

The requirements as set forth by the City's Hydrology Section in the pre-design meeting for this project have been satisfied. When this site is developed and the grading and drainage improvement are implemented as shown on the grading and drainage plan, the impacts to downstream facilities should be minimal. When this site is fully developed, approximately 14 cfs will be generated during the 100-year event. Approximately 6.2 cfs (44%) of this runoff will be collected on-site and will not surface discharge to adjacent roadways. As a result, 7.78 cfs will discharge from the site during the 100-year event, which is less than the 9.7 cfs that is currently discharged under existing conditions.

APPENDIX A

Hydrology Spreadsheets

HYDROLOGY - 100-YEAR EVENT

Percipita	Percipitation Zone 2				-	P(100-6) = 2.35"		P(100-24) = 2.75"	75"
1	Basin	La	and Treatm	Land Treatment Factors					~
Basin	Area	Α	œ	C	D	⊞	V ₍₁₀₀₋₆₎	V(100-24)	Q ₍₁₀₀₎
	(Ac)		(Acres)		c c c c c c c c c c c c c c c c c c c	(in)	(af)	· (af)	(cfs)
Existing	Existing Conditions	1		,		. ,		,	,
Site	3.10	0.00	0.00	3.10	0.00	1.13	0.292	0.292	9.7
Propose	Proposed Conditions		-					•	
A	1.00	0.00	0.12	0.00	0.88	1.96	0:163	0.193	4.4
Φ.	0.45	0.00	0.05	0.00	0.40	1.97	0.074	0.087	2.0
С	0.67	.000	0.04	0.00	0.63	2.04	0.114	0.135	3.1
ם	0.67	00.0	0.03	0.00	0.64	2.06	0.115	0.136	3.1
Ш	0.31	00.0	0.01	0.00	0.30	2.08	0.054	0.064	1.4

HYDROLOGY - 10-YEAR EVENT

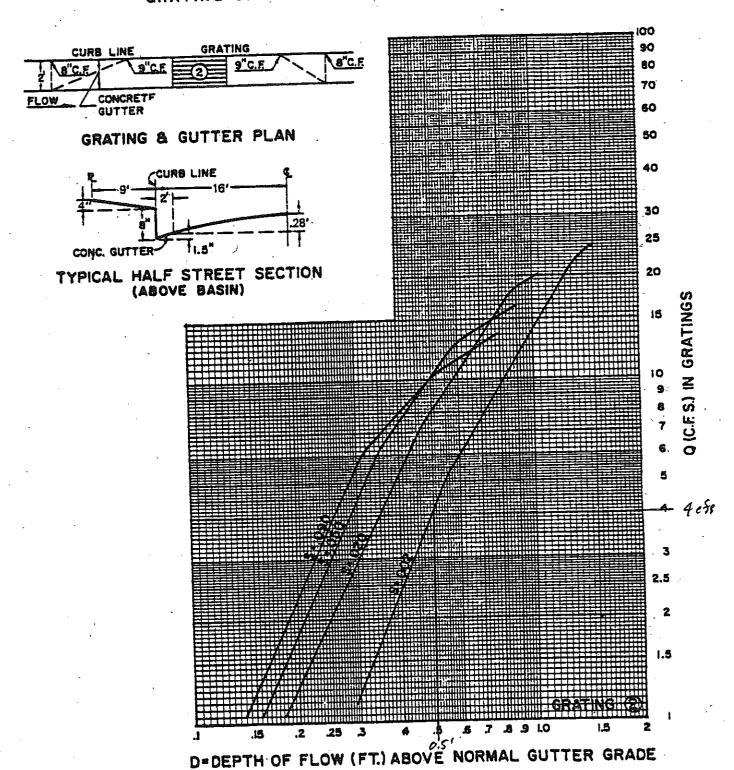
Percipitat	Percipitation Zone 2	-				P(10-6) = 1.57"	·	P(10-24) = 1.83"	-
	Basin		Land Treatment Factors	ent Factors	•	•			,
Basin	Area	A	В	C	ם	Εw	V(100-6)	V(100-24)	Q ₍₁₀₀₎
	(Ac)		(Acres)			(in)	(af)	(af)	(cfs)
Existing (Existing Conditions								
Site	3.10	0.00	0.00	3.10	0.00	0.52	0.134	0.134	5.3
Proposed	Proposed Conditions			٠.	•				
Α	1.00	0.00	0.12	0.00	0.88	1.21	0.101	0.120	2.9
ѿ	0.45	0.00	0.05	0.00	0.40	1.22	0.046	0.055	1.3
C	0.67	0.00	0.04	0.00	0.63	1.28	0.071	0.085	2.0
ס	0.67	0.00	0.03	0.00	0.64	1.29	0.072	0.086	2.0
m	0.31	0.00	0.01	0.00	0.30	1.31	0.034	0.040	1.0
						-			

APPENDIX B

Hydraulic Calculations

MORARTY, N BUS: (505)8 FAX: (505)8	ASSOCIATES SUIVEYOIS, ENGINEERS & PLANNERS SHET INDIBER: WAM 9/9/05 COCHERCY SUIVEYOIS, ENGINEERS & PLANNERS COCHERCY BY CHECKED B
	TNUES: Q100 = 3.1 cfs (BOTH BASTN C 6D) GRATE ELEN (BASTN C) = \$4,92 } AHN = HIGH POTH PLEN = \$4,96 } FROM PLATE 22.3 D-5 -> QCAR = 4 cfs > ANALYSES IS CONSERVATIVE -> ASSUMED CONSTRUCTION SUPE OF 0,002 FE/FE AT GRATE SHATE IS ACTUALY IN SUMP CONSTRUCT NA NO MEED TO RIN HEZ- 12 ANALYSIS. TBOTHER THEFS C +> D BASTN C -> Q100 = 3.1 cfs
	GRATE ELEV (BASINC) = \$4.42 } AHW = HIGH POOT BEV, = \$4.96 } FROM PLATE 22,3 D-S -> Read = 4cfs > AWAYSES IS CONSERVATIONE > ASSUMED LONGITUDENAL SLOPE OF O. D. D. FELFE AT GRATE. SHATE IS ACTUALY IN SUMP CONDITION. NO MEED TO PLOY HEC-12 ANALYSIS. BASEN C > \$100 = 3,1 cfs
	GRATE ELEV (BASINC) = \$4.42 } AHW = HIGH POOT BEV, = \$4.96 } FROM PLATE 22,3 D-S -> Read = 4cfs > AWAYSES IS CONSERVATIONE > ASSUMED LONGITUDENAL SLOPE OF O. D. D. FELFE AT GRATE. SHATE IS ACTUALY IN SUMP CONDITION. NO MEED TO PLOY HEC-12 ANALYSIS. BASEN C > \$100 = 3,1 cfs
	GRATE ELEV (BASINC) = \$4.42 } AHW = HIGH POOT BEV, = \$4.96 } FROM PLATE 22,3 D-S -> Read = 4cfs > AWAYSES IS CONSERVATIONE > ASSUMED LONGITUDENAL SLOPE OF O. D. D. FELFE AT GRATE. SHATE IS ACTUALY IN SUMP CONDITION. NO MEED TO PLOY HEC-12 ANALYSIS. BASEN C > \$100 = 3,1 cfs
	FROM PLATE 223 D-5 -> PROPE = 4cfs > ANALYSES IS CONSERVATIVE -> ASSUMED LONGITUDENAL SUPE OF OLOGI FELLE AT BRATE, SHATE IS ACTUALY IN SUMP CONDITION, NO MEED TO ROW HEC-12 ANALYSIS. BASEN C -> PROPE = 3, 1 cfs
	FROM PLATE 223 D-5 -> PROPE = 4cfs > ANALYSES IS CONSERVATIVE -> ASSUMED LONGITUDENAL SUPE OF OLOGI FELLE AT BRATE, SHATE IS ACTUALY IN SUMP CONDITION, NO MEED TO ROW HEC-12 ANALYSIS. BASEN C -> PROPE = 3, 1 cfs
720	FROM PLATE 22,3 D-5 -> QCAR = ACFS > ANALYSES IS CONSERVATIVE -> ASSUMED CONSETTUDENAL SLOPE OF OLOS FELFE AT GRATE, SPATE IS ACTUALY IN SUMP CONDITION, NO MEED TO RIN HEC-12 ANALYSIS. TOBOLISEM INDISC +> D BASIN C -> Q100 = 3,1 Cfs
	AWAYYSTS IS CONSERVATIVE > ASSUMED CONSITIONAL SLOPE OF DISCONDING AT GRATE, SPATE IS ACTUALY IN SUMP CONDITION, NO MED TO RIN HEZ-12 ANALYSIS. I BOWEN INTS C + D BASTN C -> Q100 = 3, 1 cfs
720	AWAYYSTS IS CONSERVATIVE > ASSUMED CONSITIONAL SLOPE OF DISCONDING AT GRATE, SPATE IS ACTUALY IN SUMP CONDITION, NO MED TO RIN HEZ-12 ANALYSIS. I BOWEN INTS C + D BASTN C -> Q100 = 3, 1 cfs
	LONGSTVOTMAL SLOPE OF 0.002 FE/FE AT GRATE, GRATE IS ACTUALLY IN SUMP CONDITION, NO MEED TO RIM HEC-12 ANALYSIS. TBOTHEN INETS C + D BASEN C -> Q100 = 3,1 cfs
72	LONGSTVOTMAL SLOPE OF 0.002 FE/FE AT GRATE, GRATE IS ACTUALLY IN SUMP CONDITION, NO MEED TO RIM HEC-12 ANALYSIS. TBOTHEN INETS C + D BASEN C -> Q100 = 3,1 cfs
	AT GRATE, GRATE IS ACTUALLY IN SUMP CONDITION, NO MEED TO RIN HEC-12 ANALYSIS. TO BETWEEN INCTS C & D BASTN C -> Q100 = 3,1 cfs
722	SUMP CONDITION, NO MED TO RING HEC-12 ANALYSTS. THE BETWEN IMETS C & D BASTN C => Q100 = 3,1 cfs
720	$\frac{\mathcal{H}_{C}-\mathcal{I}_{C}}{\mathcal{H}_{C}} = \frac{\mathcal{H}_{C}}{\mathcal{H}_{C}} = \frac{\mathcal{H}_{C}} = \frac{\mathcal{H}_{C}}{\mathcal{H}_{C}} = \frac{\mathcal{H}_{C}}{\mathcal{H}_{C}} = \mathcal{H$
720	$2DES$: I BETWEEN TIMETS $C \rightarrow D$ $BASTAN C \rightarrow Q_{100} = 3.1 cfs$
720	I BETWEEN INTO C + D BASTN C -> Q100 = 3,1 cfs
72	I BETWEEN INTO C + D BASTN C -> Q100 = 3,1 cfs
7-22	I BETWEEN INTO C + D BASTN C -> Q100 = 3,1 cfs
	BASTN 4 -> Q100 = 3,1 cfs
	BASTN 4 -> Q100 = 3,1 cfs
	BASTN 4 -> Q100 = 3,1 cfs
	
	I I I I I I I I I I I I I I I I I I I
	50 = 0.00\$ ft/ft , n = 0.01 (PLASTER)
	D= 12" - SEE FLOW MASTER OUT
	Qcan = 3,52 cts > 3.1 cts,
	I. Berneen INLETS D + EXIST, DI
	┡ ┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼
	BASIN C 6 D 7 Q160 = 3.1 (2) = 6.2
	50=0.005 ft/st, n=0.01 (PLASTIC)
	D= 16" -> SEE FLOW MASHER OUTP
	THE REPORT OF THE PROPERTY OF
	Que = 7,59 cfs > 6,2cfs, 1.

GRATING CAPACITIES FOR TYPE "A" , "C" and "D"



Worksheet Worksheet for Circular Channel

Project Description	
Project File	c:\haestad\fmw\aardex.fm2
Worksheet	Basin C Drop Inlet
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Discharge

Input Data		
Mannings Coefficient	0.010	
Channel Slope	0.0050	00 ft/ft
Depth	1.00	ft
Diameter	12.00	in

Results		٠
Discharge	3.27	cfs
Flow Area	0.79	ft².
Wetted Perimeter	3.14	ft
Top Width	0.3e-7	ft
Critical Depth	0.77	ft
Percent Full	100.00	
Critical Slope	0.00558	9 ft/ft
Velocity	4.17	ft/s
Velocity Head	0.27	ft
Specific Energy	1.27	ft
Froude Number	0.14e-3	
Maximum Discharge	3.52	cfs
Full Flow Capacity	3.27	cfs
Full Flow Slope	0.00500	0 ft/ft
Flow is subcritical.		

Worksheet Worksheet for Circular Channel

Project Description	
Project File	c:\haestad\fmw\aardex.fm2
Worksheet	Basin D Drop Inlet
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Discharge

Input Data		
Mannings Coefficient	0.010	•
Channel Slope	0.0050	00 ft/ft
Depth	1.33	ft
Diameter	16.00	in

Results		
Discharge	7.20	cfs
Flow Area	1.40	ft²
Wetted Perimeter	4.06	ft
Top Width	0.13	ft
Critical Depth	1.07	ft
Percent Full	99.75	•
Critical Slope	0.005455 ft/ft	
Velocity	5.16	ft/s
Velocity Head	0.41	ft
Specific Energy	1.74	ft
Froude Number	0.28	
Maximum Discharge	7.59	cfs
Full Flow Capacity	7.05	cfs
Full Flow Slope	0.005217 ft/ft	
Flow is subcritical.		