

City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

January 16, 2004

Shahab Biazar PE Advanced Engineering and Consulting 10205 Snowflake Ct NW Albuquerque, NM 87114

Re: West Bluff Mobile Home Park Grading Certification Engineer's Stamp dated 10-11-03 (K9/D24)

Dear Mr. Biazar,

Based upon the information provided in your submittal dated 1-15-03, the above referenced certification is approved for Release of Financial Guarantee.

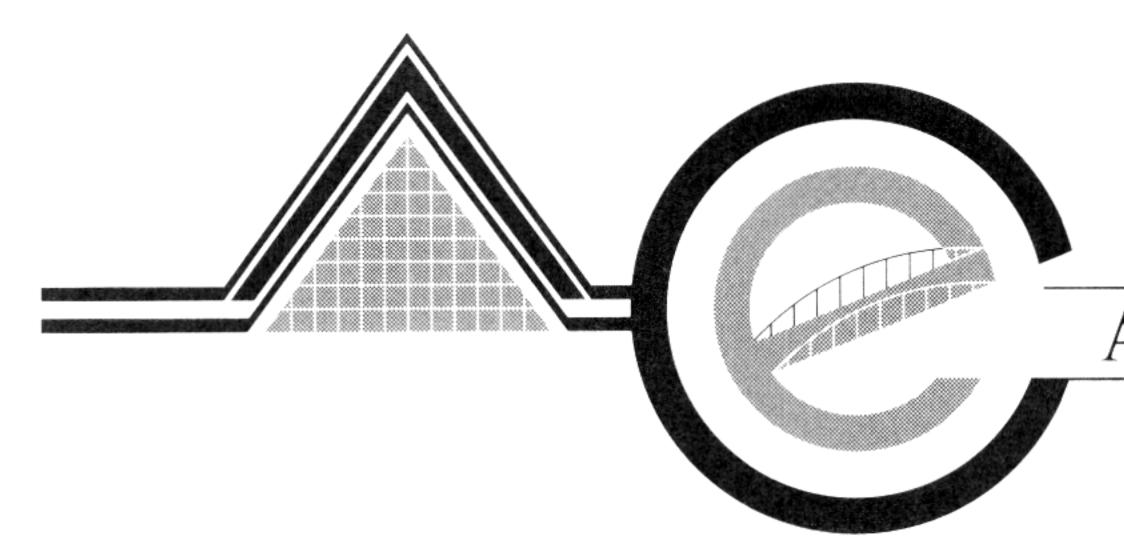
If you have any questions, you can contact me at 924-3986.

Sincerely,

Bradley L. Bingham, PE

Sr. Engineer, Planning Dept. Development and Building

C: Arlene Portillo, CPN 707881 file



ADVANCED ENGINEERING and CONSULTING, LLC

Consulting
Design
Development
Management
Inspection

January 12, 2004

Mr. Bradley L. Bingham, P.E. Sr. Engineer, Planing Dept. Development and Building Services 600 Second Street NW Albuquerque, New Mexico 87102

RE: GRADING AND PAD CERTIFICATION AND FINANCIAL GUARANTEE RELEASE, WEST PLATEAU MOBILE HOME SUBDIVISION (K9 / D24), CITY PROJECT # 707881

Dear Mr. Bingham:

This submittal is for grading plan/pad certification. All the improvements for the above-mentioned project has been completed last year. The storm sewer piping and pavements have been inspected and approved by the City last year as well. Attached please find the as-built grades on the grading plan and as-built plans for the storm sewer pipe construction. We are asking for the Financial Guarantee Release and Grading/Pad Certification Approval.

Please contact me if there are any questions or concerns regarding this submittal.

Sincerely yours,

Shahab Biazar, P.E.



City of Albuquerque P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

April 30, 2003

Shahab Biazar PE Advanced Engineering and Consulting 10205 Snowflake Ct NW Albuquerque, NM 87114

Re: West Bluff Mobile Home Park Grading and Drainage Plan Engineer's Stamp dated 3-28-03 (K9/D24)

Dear Mr. Biazar,

Based upon the information provided in your submittal dated 3-28-03, the above referenced plan is approved as amended. This is now the plan that must be certified for release of financial guarantee.

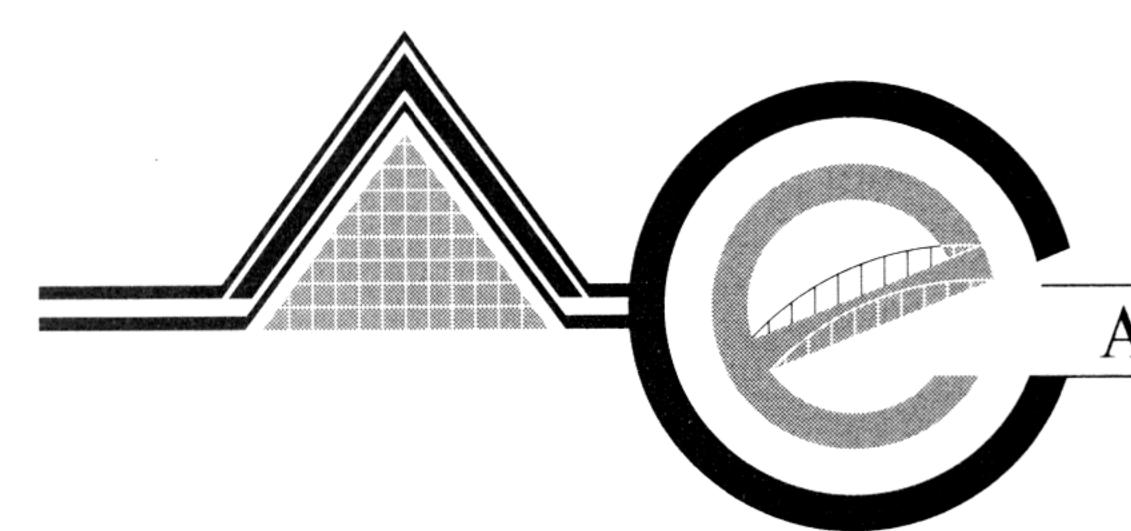
If you have any questions, you can contact me at 924-3986.

Sincerely,

Bradley L. Bingham, PE

Sr. Engineer, Planning Dept. Development and Building

C: file



ADVANCED ENGINEERING and CONSULTING, LLC

Consulting
Design
Development
Management
Inspection
Surveying

March 28, 2003

Mr. Bradley L. Bingham, P.E. Sr. Engineer, PWD
Development and Building Services
600 Second Street NW
Albuquerque, New Mexico 87102

RE: GRADING PLAN MODIFICATION FOR WEST PLATEAU MOBILE HOME SUBDIVISION (K9 / D24)

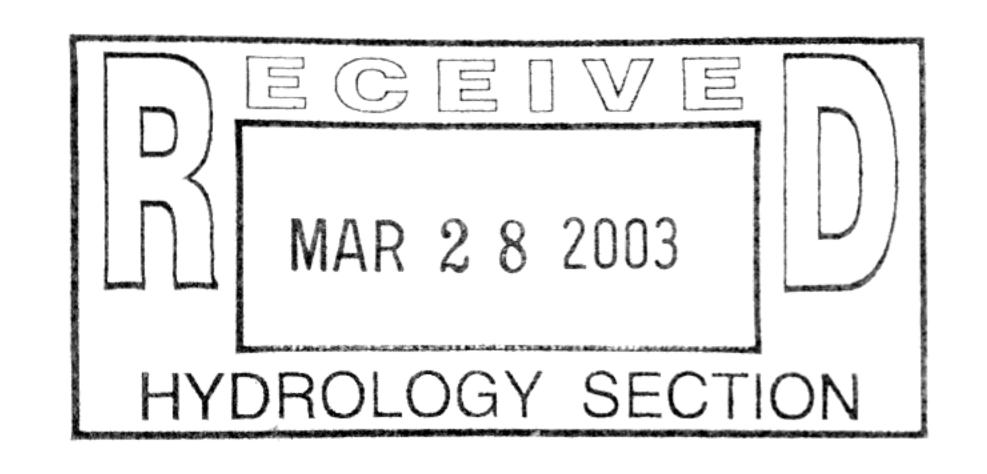
Dear Mr. Bingham:

This letter is to request the approval on the revised grading plan. The grading plan has previously been approved. The grades were changed to reduce some of the retaining walls. Lots 1 through 15 will slope to the back of the lot (15' from the rear of the lot) in order to eliminate and reduce some of the retaining wall along 90th Street. Only 15' rear portion of the lot will drain to the back and the remaining portion of the lot will continue to drain to the front of the lot. The ponding requirement for the back drainage is only 35 cfs and ponding capacity (up to 18" water depth) is 135 CF. See attached calculation for ponding requirement. Some of the grades on the north side of the project were also modified to eliminate some of the retaining walls. See the revised grading plan for changes.

Please contact me if there are any questions or concerns regarding this submittal.

Sincerely yours,

Shahab Biazar, P.E.



VOLUME CALCULATIONS FOR 10-DAY STORM

REAR LOT PONDING VOLUME REQUIREMENT (UNDER PROPOSED CONDITIONS)

DRAINAGE BASINS

| SUB-BASIN | AREA (SF) | AREA (AC-FT) | AREA (MI ²) |
|-----------|-----------|--------------|-------------------------|
| BASIN | 600.00 | 0.01377 | 0.000022 |

$$E = \underline{EA(AA) + EB(AB) + EC(AC) + ED(AD)}$$

$$AA + AB + AC + AD$$

$$V-360 = E(AA + AB + AC + AD)$$

$$V-10 \text{ Day} = V-360 + AD (P-10 \text{ Day} - P-360) / 12 in/ft$$

EA = 0.44

EB = 0.67

EC = 0.99

ED = 1.97

AA = 0.00%

AB = 100.00%

AC = 0.00%

AD = 0.00%

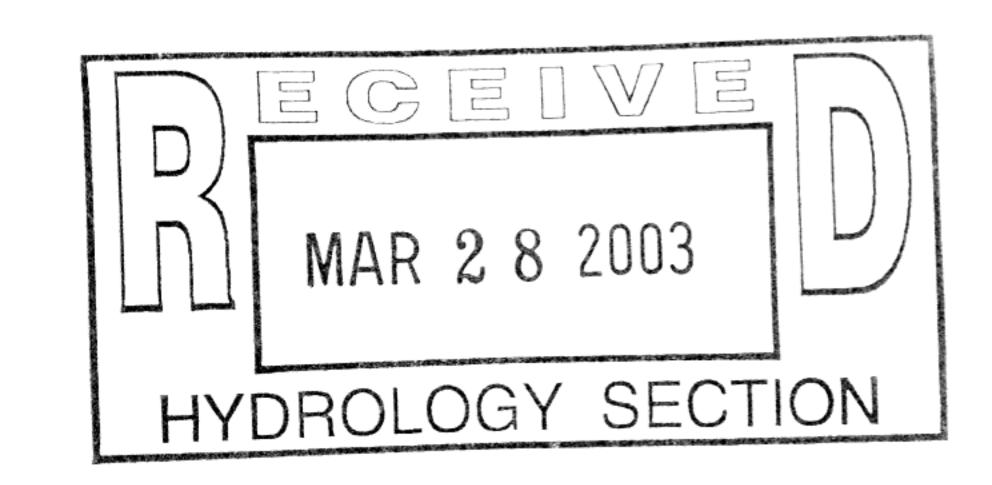
P-60 = 1.87

P-360 = 2.20

P-1440 = 2.66

P-10 Day = 3.67

| $\mathbf{E} =$ | 0.6700 | IN |
|----------------|--------|---------------|
| V-360 = | 0.0008 | AC-FT |
| AD = | 0.0000 | AC |
| V-10 Day = | 0.0008 | AC-FT |
| V-10 DAY = | 33.50 | \mathbf{CF} |





City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

March 14, 2003

Shahab Biazar PE Advanced Engineering and Consulting 10205 Snowflake Ct NW Albuquerque, NM 87114

Re: West Bluff Mobile Home Park Drainage Report

Engineer's Stamp dated 10-9-02 and letter of acceptance (K9/D24)

Dear Mr. Biazar,

Based upon the information provided in your submittal dated 2-20-03, the above referenced report is approved for Site Development Plan for Building Permit and Preliminary Plat action by the DRB.

If you have any questions, you can contact me at 924-3986.

Sincerely,

Bradley L. Bingham, PE

Sr. Engineer, Planning Dept.

Development and Building

C: file

City of Albuquerque Planning Department

Certificate of Work Order Completion October 22, 2002

City Engineer 600 Second St. Plaza Del Sol Albuquerque, NM 87102

Los Volcanos Mobile Home Park, Project No. 6608.81 Re:

Dear Sir:

This is to certify that Project No. 6608.81 has been completed according to approved plans and construction specifications. Please be advised this Certificate of Work-Order Completion does not constitute acceptance of the city infrastructure until all requirements of the subdivision improvements agreement have been satisfied and a Certificate of Completion and Acceptance is issued by the City Engineer.

48'FF arterial paving, curb and gutter and 6' sidewalk (on the both sides of the street) for 90th Street from Volcano, NW (south property line) to NE

30' FE arterial paving (24' permanent and 6' of temporary), curb and gutter and 6' sidewalk (on the east side of the street only) for Volcano from corner of Tract 6. east property line to 90th Street(north property line)

30' FE arterial paving (24' permanent and 6' of temporary), curb and gutter and 6' sidewalk (on the north side of the street only) for 90th Street from NE corner of Tract 6 to east property line.

WATER:

8", waterline for Volcano, NW from east property line to 90th Street (west property line)

SANITARY SEWER:

8" sewer line for 90th Street from Volcano NW (south property line) to NE corner of Tract 6

8" sewer line for Volcano NW from east property line to 90th Street (west property line)

STORM SEWER:

54" storm sewer RCP for 90th Street from NE corner of Tract 6 to North property line (existing RCP)

54" storm sewer RCP for 90th Street from NE corner of Tract 6 to Volcano NW (south property line)

54" storm sewer RCP for Volcano NW from 90th Street (manhole) to existing stub (to the west of 90th Street± 50")

60" storm sewer RCP for Volcano NW from East property line to 90 Street (east property line)

PRIVATE ROAD IMPROVEMENTS

28' FF residential paving, curb and gutter and 4' sidewalk (on both sides of the street) for Merida Street from East property line to 90th Street (west property line)

28' FF residential paving, curb and gutter and 4' sidewalk (on both sides of the street) for Monterrer Ct from Mazatlan Street to West property line (90th Street)

28' FF residential paving, curb and gutter and 4' sidewalk (on both sides of the street) for Matamoros Ct. from Mazatlan Street to West property line (90th Street)

28' FF residential paving, curb and gutter and 4' sidewalk (on both sides of the street) for Manzanillo Ct from Mazatlan Street to West property line (90th Street)

28' FF residential paving, curb and gutter and 4' sidewalk (on both sides of the street) for Mazatlan Street from Volcano NW to Merida Street.

PRIVATE UTILITY IMPROVEMENTS

Water

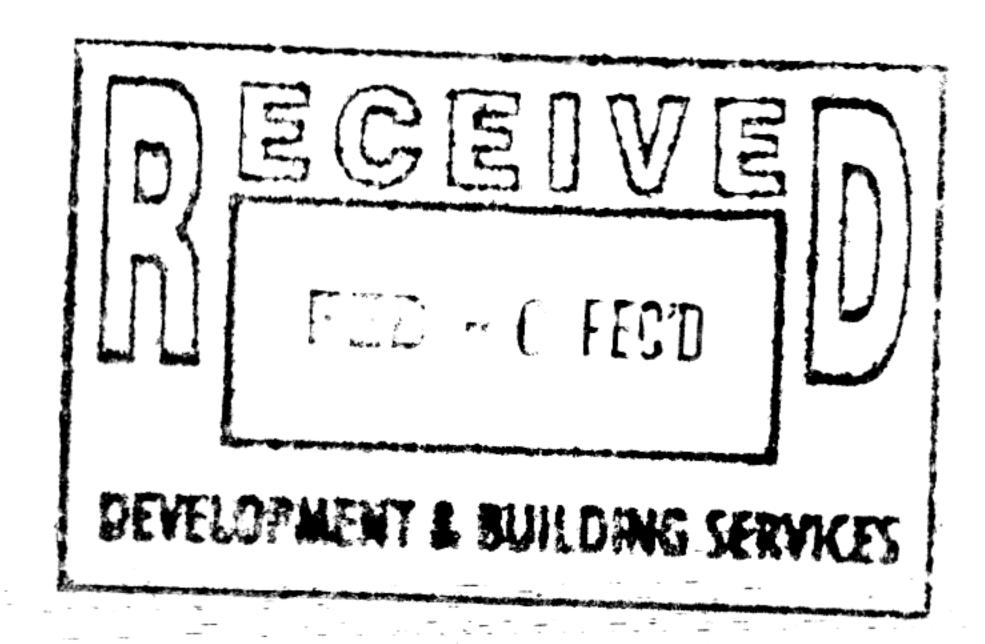
6" waterline for Merida Street from East property line to 90th Street (West Property line)

6" waterline for Monterrer Ct from Mazatlan St to West property line (90th Street)

6" waterline for Matamoros Ct from Mazatlan St. to West property line (90th Street)

6" waterline for Manzanillo Ct from Mazatlan St. to West property line (90th Street)

8" waterline for Mazatlan St from Volcano NW to Merida Street.



Los Volcanos MHP
Project NO.-6608.81
Page 2

Sanitary Sewer

8" sewer line for Merida Street from East property line to 90th Street (West property line)

8" sewer line for Monterrer Ct from Mazatlan Street to West property line (90th Street)

8" sewer line for Matamoros Ct from Mazatlan St. to West property line (90th Street)

8" sewer line for Manzanillo Ct from Mazatlan St. to West property line (90th Street)

8" sewer line for Mazatlan St from Volcano NW to Merida Street.

The contractor's correction period will begin October 22, 2002 and is effective for a period of one (1) year.

Kevin Broderick

Development & Bldg Services

Planning Department

Advanced Engineering
Albuquerque Excavators
Master Scheduler
Project Administrator
Martin Barker, Materials Testing Lab
Orvis Bartow, Water Systems
Dave Harmon, Traffic Engineering, PWD
Josie Jaramillo, New Meter Sales, PWD
George King, Maps & Records, PWD

Project No. 6608.81 Warranty:Contract



City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

November 7, 2002

Shahab Biazar PE Advanced Engineering and Consulting 10205 Snowflake Ct NW Albuquerque, NM 87114

Re: West Bluff Home Park Drainage Report
Engineer's Stamp dated 10-9-02 (K9/D24)

Dear Mr. Biazar,

Based upon the information provided in your submittal dated 10-9-02, the above referenced report cannot be approved for Site Development Plan for Building Permit, Preliminary Plat or Building Permit until the following comments are addressed.

• Please provide all as-built drawings to ascertain that the storm drain in 90th is active. That is, I need to see the drawings, or the Letter of Acceptance of the section of storm drain in 90th between Volcano and Central.

If you have any questions, you can contact me at 924-3986.

Sincerely,

Bradley L. Bingham, PE

Sr. Engineer, Planning Dept.

Development and Building

C: file

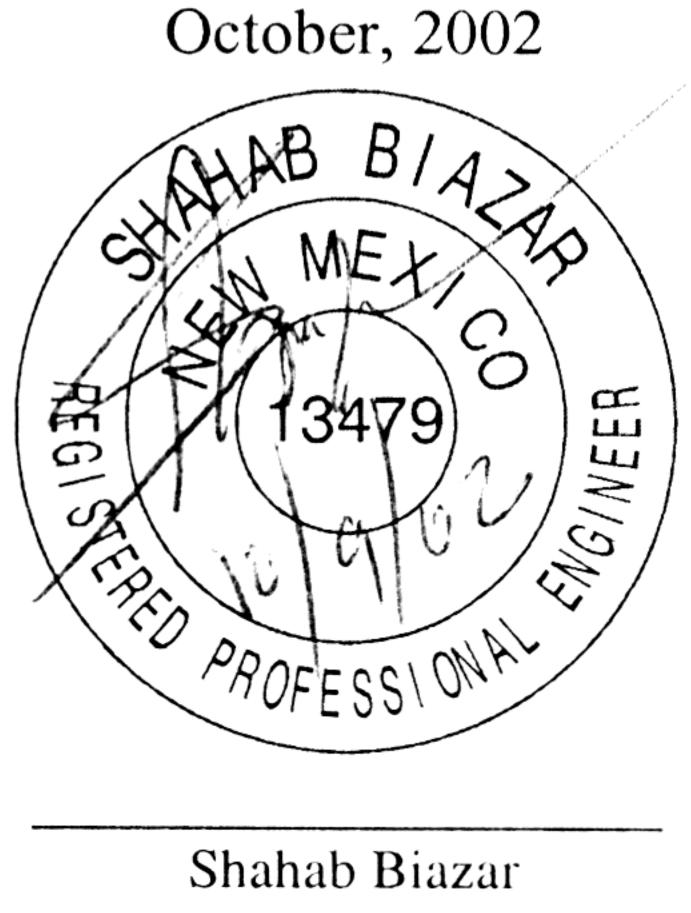
DRAINAGE REPORT FOR

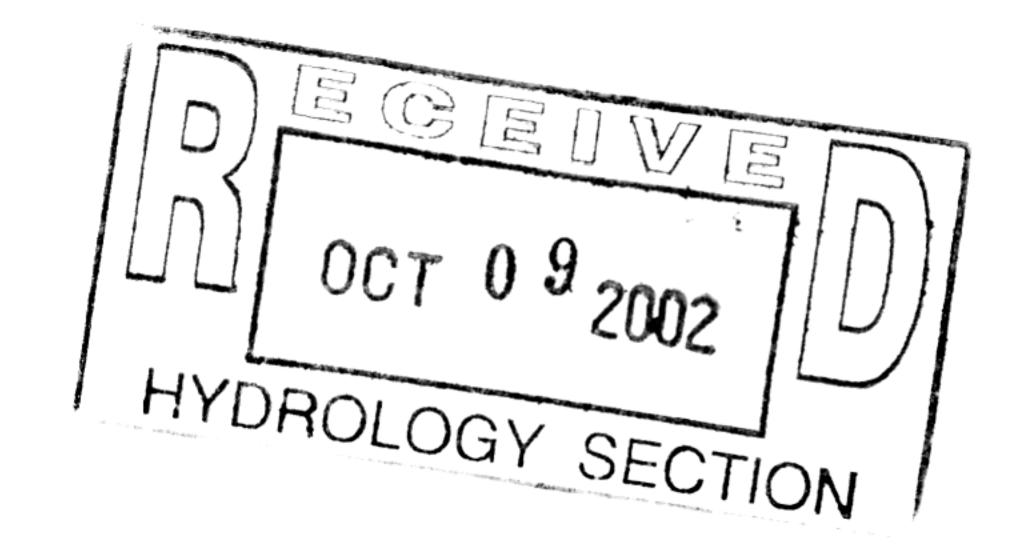
WEST BLUFF Mobile Home Subdivision

Prepared by:

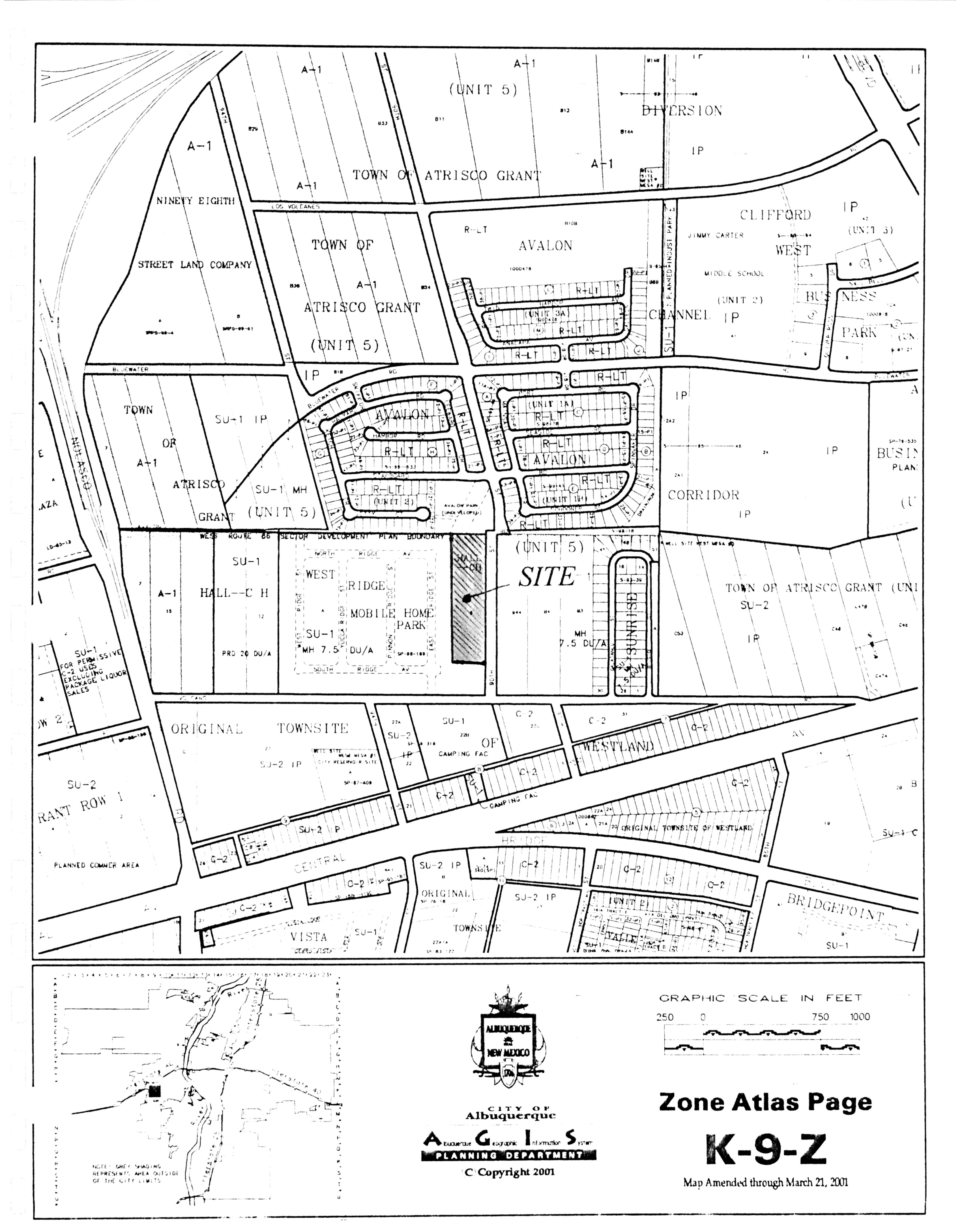


10205 Snowflake Ct. NW Albuquerque, New Mexico 87114





PE NO. 13479



Location

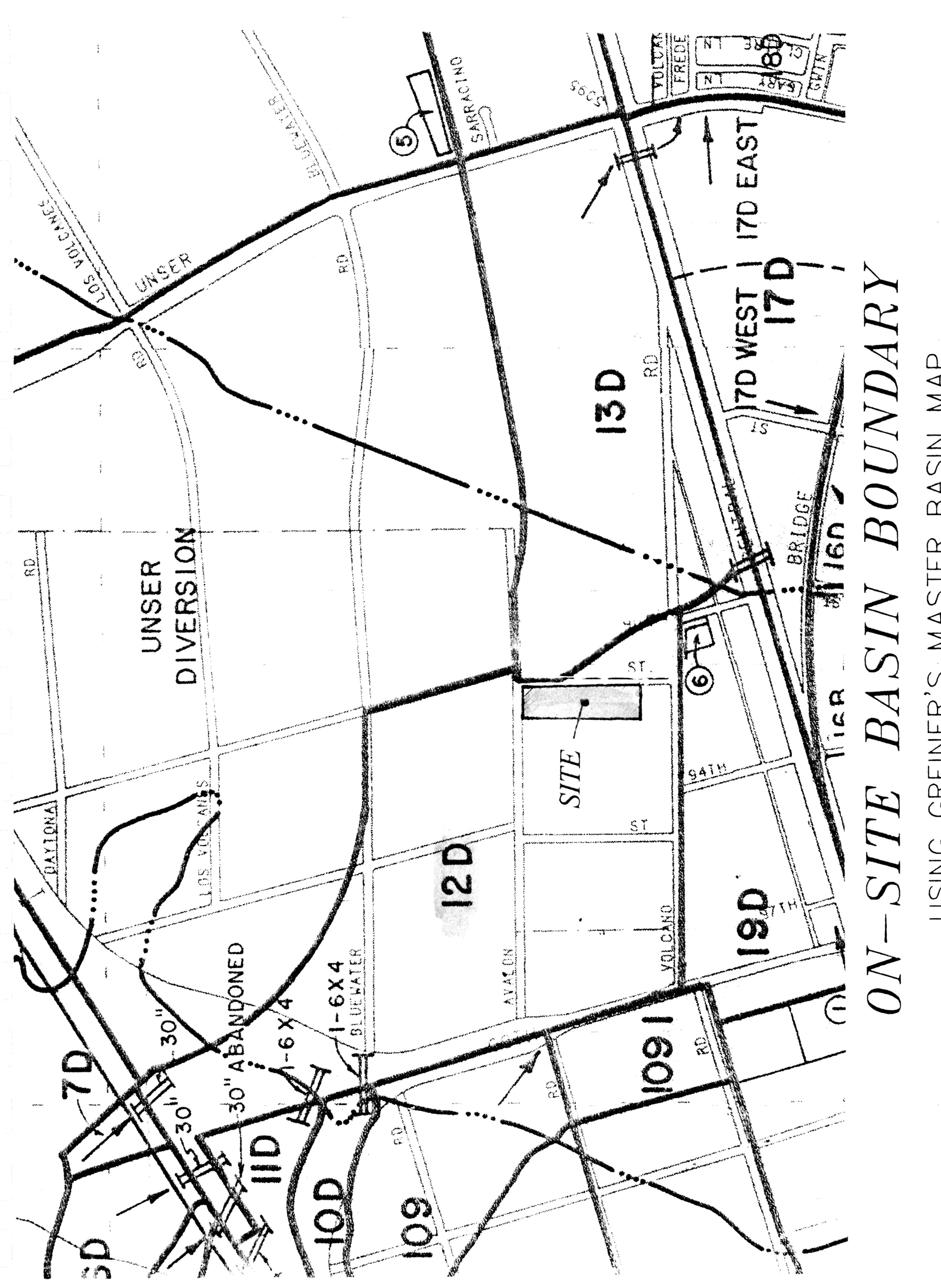
West Bluff Mobile Home Subdivision Tract 6, Lands of C.H. Hall, is located on 90th Street North of Volcano Rd. The site contains ±4.00 acres. See attached vicinity map for location.

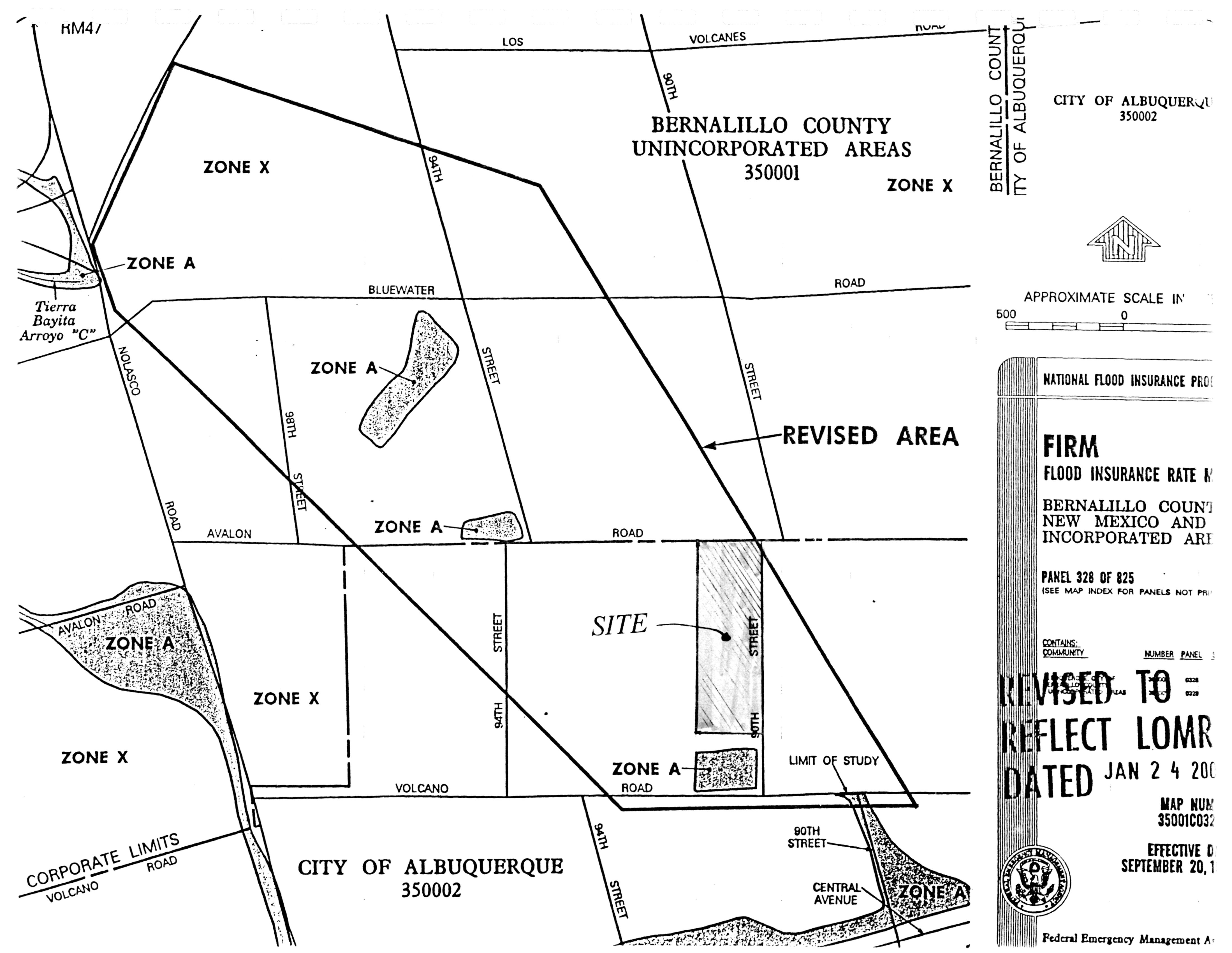
Purpose

Advanced Engineering and Consulting, LLC on behalf of the owners has prepared this grading and drainage solution for the proposed site. This grading and drainage plan is prepared in order to obtain site plan for subdivision approval, preliminary and final plat approval as well as grading and drainage approval and building permit approval for this site.

Existing Drainage Conditions

This site falls within the Master Drainage Basin for the Amole Del Norte (AND) system Diversion Facility prepared by Greiner. The site is part of Basin 12D of Master Drainage Basin. See attached exhibit for the location of the site in relationship to the Master Plan. The site drains to 90th Street and the to Volcano Road and then it is intercepted by existing inlets and discharged into the storm sewer system on Volcano Road. There are no offsite runoff that enters the site. There is an existing mobile home park to the west and to the south. The runoff from the MH park drains to the existing storm sewer system within the mobile home park itself. The runoff to the north drains east to an existing pond and then discharges to the storm sewer pipe in 90th Street. To the east, 90th Street, intercepts the runoff and no offsite enters the site from the east. According to the revised flood plain map 35001C0328 D dated January 24, 2000 the site does not fall within a 100-year floodplain.





Proposed Conditions and On-Site/Offsite Drainage Management Plan

Based on the West Ridge Mobile Home Park Drainage Report (City Drainage Number K9/D6) an allowable discharge rate of 2.05 cfs per acre was determined for Basin 12D of the Master Drainage Plan prepared by Greiner. Therefore, the runoff from this site will be detained in the street and then discharge at a flow rate of 7.94 cfs which is less than allowable discharge of (3.99 ac X 2.05 cfs/ac) 8.18 cfs. The storm sewer system is designed to detail the runoff using a 12" RCP discharge pipe. The runoff on site will be intercepted by 2 Single-A and then discharged into the existing 54" RCP on 90th Street. The runoff will be ponded on site (within the street limits) but not exceeding the top of curb elevation. According to the master drainage plan the runoff has to be retained on-site until the main storm sewer is extended in Broadway. Ultimately the site will be able to free discharge into the storm sewer system. Storm sewer pipes—shown on site are for future discharge of the runoff into the main storm sewer pipe within the right of way. See grading and drainage plan for storm sewer locations.

Calculations

City of Albuquerque, Development Process Manuel, Section 22.2, Hydrology Section, revised January 1993, was used for the runoff calculations. The site falls under Zone 2 based on Figure A-1 of page A-1. The street flow capacity calculation was preformed for West Bluff Street using the flow number from the entire runoff on site for 4" and 8" curb height. The runoff for both cases does not exceed the top of curb elevation. The two storm sewer inlets (Single-A) will have a drainage capacity of 60.90 cfs (under ponding conditions) and the total on site runoff is 14.36 cfs.

RUNOFF CALCULATIONS

The site is @ Zone 1

LAND TREATMENT

Based on the historical conditions:

A=100.00%

Based on the developed conditions:

 $D = 7 \sqrt{(N^2+5N)}$, Where N=units/acre, N≤6 (From DPM Section 22.2-Hydrology, Page A5, Table A-5)

N = 29/4.00 = 7.25 > 6, Therefore use the following treatments

A=0.0%, B=20%, C=20%, D=60%

DEPTH (INCHES) @ 100-YEAR STORM

 $P_{60} = 1.87$ inches

 $P_{360} = 2.20 \text{ inches}$

 $P_{1440} = 2.66 \text{ inches}$

DEPTH (INCHES) @ 10-YEAR STORM

 $P_{60} = 1.87 \times 0.667$ = 1.25 inches

 $P_{360} = 1.47$

 $P_{1440} = 1.77$

See the summary output from AHYMO calculations.

Also see the following summary tables.

RUNOFF CALCULATION RESULTS

| BASIN | AREA (SF) | AREA (AC) | AREA (MI ²) |
|---------|-----------|-----------|-------------------------|
| ON-SITE | 173801.20 | 3.9899 | 0.006234 |

PROPOSED

| BASIN | Q-100 | Q-10 | | [REA] | MEN | Γ |
|---------|-------|-----------|-----|-------|------|-----|
| | CFS | CFS A, B, | | C, | D | |
| ON-SITE | 14.36 | 8.66 | 0%, | 20%, | 20%, | 60% |

EXISTING

| BASIN | Q-100 | | TREATMENT |
|---------|-------|------|------------------|
| | CFS | CFS | A, B, C, D |
| ON-SITE | 5.18 | 0.98 | 100%, 0%, 0%, 0% |

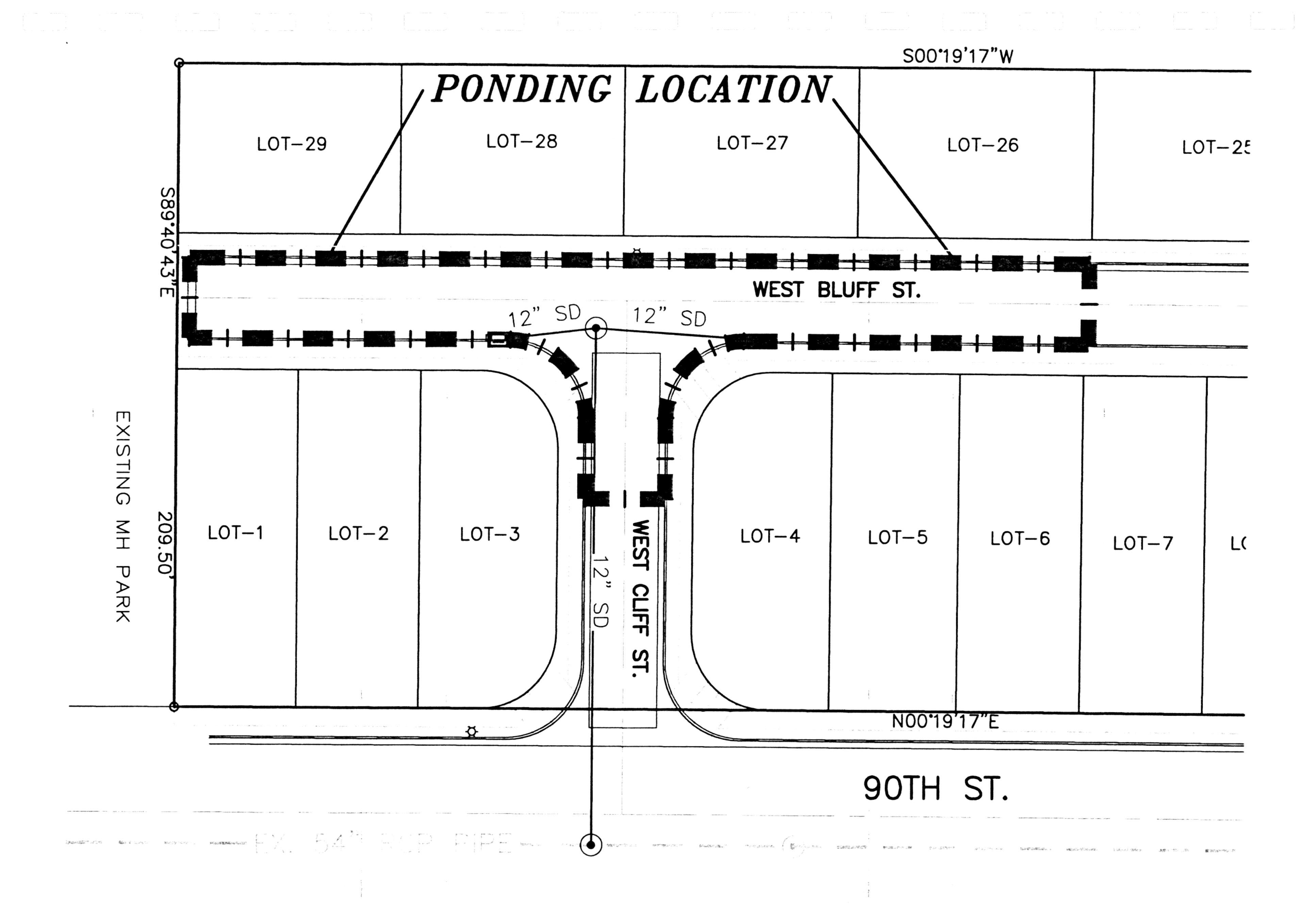
transfer of the state of the st

INPUT FILE

| | INPULFILE |
|-----------------------------|--|
| * ZONE 1 | |
| | *********** |
| | 6-HR STORM (UNDER EXISTING CONDITIONS) * |
| * | ****************** |
| START | |
| RAINFALL | TIME=0.0 TYPE-1 DATM OURDED O O TM |
| I/WIIII. WIII | TYPE=1 RAIN QUARTER=0.0 IN RAIN ONE=1.87 IN RAIN SIX=2.20 IN |
| | RAIN DAY=2.66 IN DT=0.03333 HR |
| * ON-SITE | Idiin Dri-2.00 in Di-0.05555 in |
| COMPUTE NM HYD | ID=1 HYD NO=101.0 AREA=0.006234 SQ MI |
| | PER A=100.00 PER B=0.00 PER C=0.00 PER D=0.00 |
| | TP=0.1333 HR MASS RAINFALL=-1 |
| | |
| ****** | **************** |
| * 10-YEAR, | 6-HR STORM (UNDER EXISTING CONDITIONS) * |
| ****** | ****************** |
| START | TIME=0.0 |
| RAINFALL | TYPE=1 RAIN QUARTER=0.0 IN |
| | RAIN ONE=1.25 IN RAIN SIX=1.47 IN |
| + ON COUTT | RAIN DAY=1.77 IN DT=0.03333 HR |
| * ON-STIE COMPUTE NM HYD | TD-1 HVD NO-111 O ADEA O OOCO24 GO MT |
| COMPOIE MM HID | ID=1 HYD NO=111.0 AREA=0.006234 SQ MI PER A=100.00 PER B=0.00 PER C=0.00 PER D=0.00 |
| | TP=0.1333 HR MASS RAINFALL=-1 |
| | TI-0.IJJJ IIK MADD KATMIATIL-I |
| ********** | ********************** |
| * 100-YEAR, | 6-HR STORM (UNDER PROPOSED CONDITIONS) * |
| | ************ |
| * | |
| START | TIME=0.0 |
| RAINFALL | TYPE=1 RAIN QUARTER=0.0 IN |
| | RAIN ONE=1.87 IN RAIN SIX=2.20 IN |
| d. 017 0.7 mm | RAIN DAY=2.66 IN DT=0.03333 HR |
| * ON-SITE | TD 1 TTTTD 170 101 1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 |
| COMPUTE NM HYD | ID=1 HYD NO=101.1 AREA=0.006234 SQ MI |
| | PER A=0.00 PER B=20.00 PER C=20.00 PER D=60.00 |
| | TP=0.1333 HR MASS RAINFALL=-1 |
| *********** | ************** |
| | 6-HR STORM (UNDER PROPOSED CONDITIONS) * |
| | ************************************** |
| START | TIME = 0.0 |
| RAINFALL | TYPE=1 RAIN QUARTER=0.0 IN |
| | RAIN ONE=1.25 IN RAIN SIX=1.47 IN |
| | RAIN DAY=1.77 IN DT=0.03333 HR |
| * ON-SITE | |
| COMPUTE NM HYD | ID=1 HYD NO=111.1 AREA=0.006234 SQ MI |
| | PER A=0.00 PER B=20.00 PER C=20.00 PER D=60.00 |
| | TP=0.1333 HR MASS RAINFALL=-1 |
| * | |
| FINISH | |

SUMMARY OUTPUT FILE

| AHYMO PROGRAINPUT FILE = | M SUMMARY TABLE 200226 | (AHYMO | _97) - | | - | VERSION: 1 | 1997.02d | RUN DATE USER NO.= | • | /YR) =07/2 9702c01000 | • |
|--------------------------------|------------------------------|--------|-----------------|-----------------|----------------------------|-----------------------------|--------------------|----------------------------|--------------------|------------------------------------|----------------------------|
| COMMAND | HYDROGRAPI IDENTIFICATION | | TO ID NO. | AREA (SQ MI) | PEAK DISCHARGE (CFS) | RUNOFF VOLUME (AC-FT) | RUNOFF (INCHES) | TIME TO PEAK (HOURS) | CFS PER ACRE | PAGE = | |
| COMPUTE NM H START | PE= 1 YD 101.0 PE= 1 |) – | 1 | .00623 | 5.18 | .146 | .43925 | 1.533 | 1.298 | TIME= RAIN6= PER IMP= TIME= RAIN6= | .00 2.200 .00 .00 |
| COMPUTE NM H START | |) – | 1 | .00623 | .98 | .027 | .08264 | 1.533 | .246 | PER IMP= TIME= RAIN6= | .00 |
| COMPUTE NM H START RAINFALL TY | YD 101.1 PE= 1 |) – | 1 | .00623 | 14.36 | .501 | 1.50556 | 1.500 | 3.600 | PER IMP= TIME= RAIN6= | 60.00 .00 1.470 |
| COMPUTE NM H FINISH | YD 111.1 |) – | 1 | .00623 | 8.66 | .289 | .86984 | 1.500 | 2.170 | PER IMP= | 60.00 |



PONDING LOCATION

VOLUME CALCULATIONS

DETENTION POND

Ab - Bottom Of The Pond Surface Area

At - Top Of The Pond Surface Area

D - Water Depth

Dt - Total Pond Depth

C - Change In Surface Area / Water Depth

Volume = $Ab * D + 0.5 * C * D^2$

$$C = (At - Ab) / Dt$$

Ab = 13.59 At = 8,153.15 Dt = 1.00 C = 8139.56

| ACTUAL | DEPTH | VOLUME | Q |
|---------|-------|---------|-------|
| ELEV. | (FT) | (AC-FT) | (CFS) |
| 5160.09 | 0.00 | 0 | 0.00 |
| 5161.09 | 1.00 | 0.0003 | 2.67 |
| 5162.09 | 2.00 | 0.0006 | 4.63 |
| 5163.09 | 3.00 | 0.0009 | 5.98 |
| 5164.09 | 4.00 | 0.0012 | 7.07 |
| 5164.19 | 4.10 | 0.0022 | 7.18 |
| 5164.29 | 4.20 | 0.0050 | 7.27 |
| 5164.39 | 4.30 | 0.0098 | 7.37 |
| 5164.49 | 4.40 | 0.0163 | 7.47 |
| 5164.59 | 4.50 | 0.0248 | 7.56 |
| 5164.69 | 4.60 | 0.0351 | 7.66 |
| 5164.79 | 4.70 | 0.0472 | 7.75 |
| 5164.89 | 4.80 | 0.0613 | 7.84 |
| 5164.99 | 4.90 | 0.0772 | 7.93 |
| 5165.09 | 5.00 | 0.0950 | 8.02 |

Orifice Equation Q = CA SQRT(2gH)

C = 0.6Diameter (in) 12
Area (ft^2)= 0.79 g = 32.2

H(Ft) = Depth of water above center of orifice

Q(CFS)=Flow

INPUT FILE

| * | | | |
|---------------------|---------------------|-------------------|-----------------|
| * PONDING CONDITION | IS | | |
| * | | | |
| ***** | ***** | ***** | ******* |
| * 100-YEAR, | 6-HR STORM (UNDE | R PROPOSED CONDIT | 'IONS) * |
| ***** | ***** | ***** | **** |
| * | | | |
| START | TIME=0.0 | | |
| RAINFALL | TYPE=1 RAIN QUAR' | TER=0.0 IN | |
| | RAIN ONE=1.87 IN | RAIN SIX=2.20 IN | [|
| | RAIN DAY=2.66 IN | DT=0.03333 HR | |
| * ON-SITE | | | |
| COMPUTE NM HYD | ID=1 HYD $NO=101$. | 1 AREA=0.006234 S | QMI |
| | PER A=0.00 PER B | =20.00 PER C=20.0 | 0 PER D=60.00 |
| | TP=0.1333 HR MAS | S RAINFALL=-1 | |
| ***** | **** | ***** | **** |
| * | PONDING CONDITION | | * |
| ****** | **** | ***** | **** |
| * | | | |
| ROUTE RESERVOIR | | .1 INFLOW ID=1 CC | |
| | OUTFLOW(CFS) | STORAGE (AC-FT) | |
| | 0.00 | 0.0000 | 5160.09 |
| | 2.67 | 0.0003 | 5161.09 |
| | 4.63 | 0.0006 | 5162.09 |
| | 5.98 | 0.0009 | 5163.09 |
| | 7.07 | 0.0012 | 5164.09 |
| | 7.18 | 0.0022 | 5164.19 |
| | 7.27 | 0.0050 | 5164.29 |
| | 7.37 | 0.0098 | 5164.39 |
| | 7.47 | 0.0163 | 5164.49 |
| | 7.56 | 0.0248 | 5164.59 |
| | 7.66 | 0.0351 | 5164.69 |
| | 7.75 | 0.0472 | 5164.79 |
| | 7.84 7.93 | 0.0613 | 5164.89 |
| | 7.93 8.02 | 0.0772 | 5164.99 |
| * | 0.02 | 0.0950 | 5165.09 |
| ·· *********** | **** | ***** | **** |
| * | | , | |
| FINISH | | | |

AHYMO OUTPUT FILE (PONDING @ THE INLET)

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AHYMO PROGRAM (AHYMO 97) -- Version: 1997.02d (MON/DAY/YR) = 09/26/2002START TIME (HR:MIN:SEC) = 11:18:41USER NO. = AHYMO-I-9702c01000R31-AH INPUT FILE = 2226-PDPONDING CONDITIONS *************** 100-YEAR, 6-HR STORM (UNDER PROPOSED CONDITIONS) ***************** START TIME=0.0RAINFALL TYPE=1 RAIN QUARTER=0.0 IN RAIN ONE=1.87 IN RAIN SIX=2.20 IN RAIN DAY=2.66 IN DT=0.03333 HR COMPUTED 6-HOUR RAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2 - PEAK AT 1.40 HR. DT =.033330 HOURS END TIME = 5.999400 HOURS .0000 .0016 .0033 .0050 .0067 .0085 .0103 .0122 .0141 .0160 .0180 .0201 .0222 .0243 .0266 .0289 .0312 .0337 .0362 .0388 .0415 .0443 .0472 .0502 .0534 .0567 .0601 .0637 .0675 .0715 .0758 .0924 .0809 .0865 .1050 .1334 .2398 .1771 .3254 .5814 .4379 .7600 .9780 1.2649 1.1804 1.4575 1.3363 1.3997 1.5106 1.5600 1.6061 1.6493 1.6900 1.7284 1.7646 1.7989 1.8314 1.8623 1.8915 1.9193 1.9456 1.9518 1.9576 1.9630 1.9682 1.9732 1.9780 1.9825 1.9869 1.9912 1.9953 1.9993 2.0031 2.0104 2.0068 2.0140 2.0174 2.0240 2.0207 2.0272 2.0303 2.0333 2.0363 2.0392 2.0448 2.0475 2.0502 2.0528 2.0605 2.0629 2.0653 2.0677 2.0700 2.0723 2.0746 2.0768 2.0790 2.0812 2.0833 2.0855 2.0875 2.0896 2.0916 2.0936 2.0956 2.0976 2.0995 2.1014 2.1033 2.1088 2.1106 2.1051 2.1070 2.1124 2.1141 2.1159 2.1176 2.1193 2.1210 2.1227 2.1244 2.1260 2.1276 2.1292 2.1308 2.1324 2.1355 2.1340 2.1371 2.1386 2.1416 2.1401 2.1431 2.1446 2.1460 2.1475 2.1489 2.1518 2.1504 2.1532 2.1573 2.1546 2.1560 2.1587 2.1627 2.1640 2.1600 2.1614 2.1654 2.1667 2.1680 2.1692 2.1705 2.1718 2.1731 2.1743 2.1756 2.1768 2.1804 2.1817 2.1792 2.1829 2.1840 2.1780 2.1852 2.1887 2.1899 2.1876 2.1864 2.1910 2.1922 2.1933 2.1944 2.1956 2.1967 2.1978 2.1989 2.2000 * ON-SITE COMPUTE NM HYD ID=1 HYD NO=101.1 AREA=0.006234 SQ MI PER A=0.00 PER B=20.00 PER C=20.00 PER D=60.00 TP=0.1333 HR MASS RAINFALL=-1 K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420 UNIT PEAK = 14.767 CFS UNIT VOLUME = .9987 B = 526.28 P60 = 1.8700AREA =.003740 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033330

K = .118429HR TP = .133300HR K/TP RATIO = .888442 SHAPE CONSTANT, N = 3.992480

UNIT PEAK = 6.6347 CFS UNIT VOLUME = .9984 B = 354.67 P60 = 1.8700

AREA = .002494 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033330

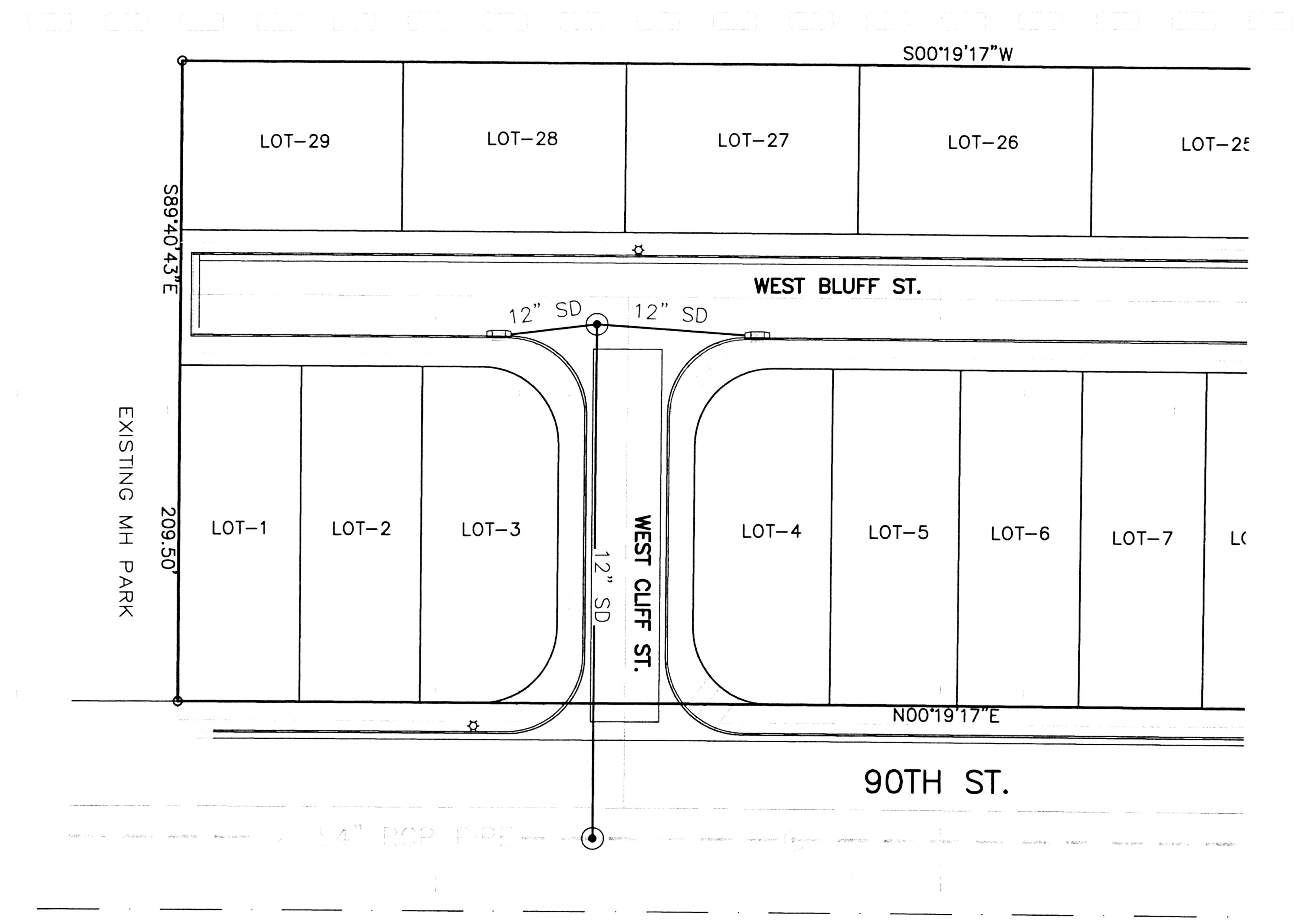
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PONDING CONDITION
****************
                    ID=10 HYD NO=501.1 INFLOW ID=1 CODE=24
ROUTE RESERVOIR
                    OUTFLOW (CFS)
                                      STORAGE (AC-FT)
                                                      ELEVATION (FT)
                        0.00
                                                        5160.09
                                           0.0000
                        2.67
                                           0.0003
                                                        5161.09
                        4.63
                                           0.0006
                                                        5162.09
                        5.98
                                           0.0009
                                                        5163.09
                        7.07
                                           0.0012
                                                        5164.09
                        7.18
                                           0.0022
                                                        5164.19
                        7.27
                                           0.0050
                                                        5164.29
                        7.37
                                           0.0098
                                                        5164.39
                        7.47
                                           0.0163
                                                        5164.49
                        7.56
                                           0.0248
                                                        5164.59
                        7.66
                                           0.0351
                                                        5164.69
                        7.75
                                           0.0472
                                                        5164.79
                        7.84
                                           0.0613
                                                        5164.89
                        7.93
                                           0.0772
                                                        5164.99
                        8.02
                                           0.0950
                                                        5165.09
                                  VOLUME
    TIME
              INFLOW
                        ELEV
                                            OUTFLOW
    (HRS)
              (CFS)
                        (FEET)
                                  (AC-FT)
                                            (CFS)
      .00
                 .00
                       5160.09
                                     .000
                                                .00
      .80
                       5160.09
                                     .000
                 .00
                                                .00
     1.60
               10.19
                       5164.98
                                     .075
                                               7.92
     2.40
                 .56
                       5160.31
                                     .000
                                                .59
     3.20
                       5160.13
                 .10
                                     .000
                                                .10
                                     .000
     4.00
                       5160.11
                                                .06
                 .06
                                     .000
     4.80
                       5160.11
                 .06
                                                .06
                                     .000
     5.60
                       5160.12
                                                .07
                 .07
                       5160.09
     6.40
                                     .000
                 .01
                                                .01
 PEAK DISCHARGE =
                       7.943 CFS -
                                     PEAK OCCURS AT HOUR
                                                            1.67
MAXIMUM WATER SURFACE ELEVATION =
                                       5165.004
MAXIMUM STORAGE =
                                            INCREMENTAL TIME=
                           .0797 AC-FT
                                                                   .033330HRS
FINISH
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NORMAL PROGRAM FINISH

END TIME (HR:MIN:SEC) = 11:18:41

SUMMARY OUTPUT FILE

| AHYMO PROGRAM SUMMARY TABLE INPUT FILE = 2226-PD | (AHYMO_97) - | | - | VERSION: 199 | 7.02d U | | (MON/DAY/YR) =09/ AHYMO-I-9702c0100 | • |
|--|-----------------------|-----------------|----------------------------|-----------------------------|--------------------|----------------------|---|-------------------------------|
| HYDROGRAPH COMMAND IDENTIFICATION | FROM TO ID ID NO. NO. | AREA (SQ MI) | PEAK DISCHARGE (CFS) | RUNOFF VOLUME (AC-FT) | RUNOFF (INCHES) | TIME TO PEAK (HOURS) | CFS PAGE PER ACRE NOTAT | |
| START RAINFALL TYPE= 1 COMPUTE NM HYD 101.10 ROUTE RESERVOIR 501.10 FINISH | - 1 1 1 10 | .00623 | 14.36 | .501 | 1.50556 1.50551 | 1.500 | TIME= RAIN6= 3.600 PER IMP= 1.991 AC-FT= | .00 2.200 60.00 .080 |



STORM SEWER LOCATION

STORM DROP INLET DRAINAGE CAPACITY

Single 'A' (in ponding conditions)

Area at the grate:

$$L = 44 3/8" - 2(6"_{ends}) - 7(\frac{1}{2})$$

$$= 28 7/8"$$

$$= 2.41'$$

$$W = 25 \frac{1}{2}$$
" - 13($\frac{1}{2}$ " middle bars)
= 19"
= 1.58'

Area =
$$2.41' \times 1.58'$$

= 3.81 ft^2

$$= 3.81 - 3.81 (0.5_{\text{clogging factor}})$$

= 1.91 ft² at the grate

Area at the throat:

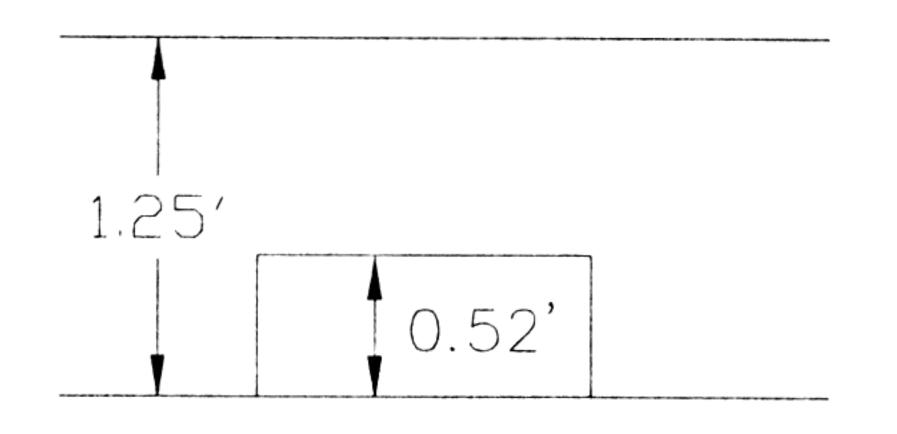
$$L = 7.45'$$

$$H = 10 \frac{3}{4}$$
" - 4 $\frac{1}{2}$ "
= 6 $\frac{1}{4}$ "
= 0.5208'

Area =
$$7.45' \times 0.5208'$$

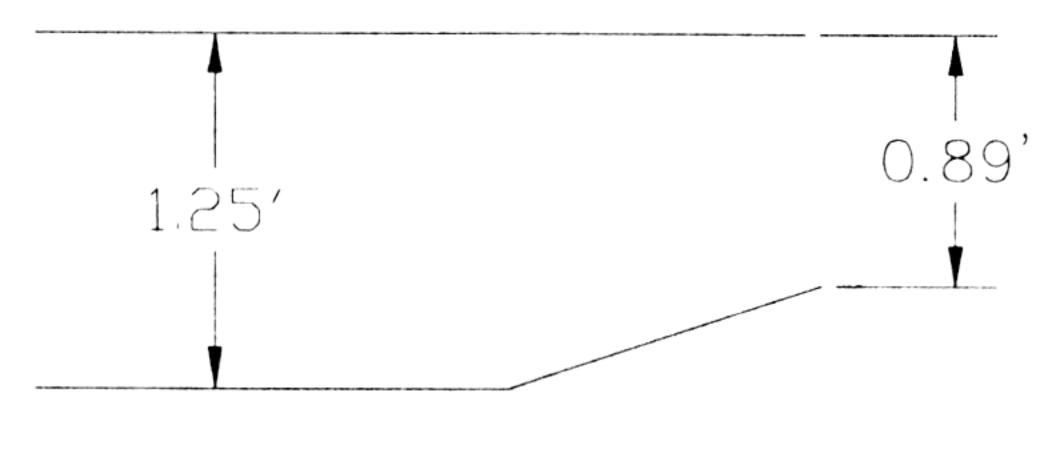
= 3.88 ft^2 at the throat

THROAT



H=1.25 Q= $CA\sqrt{2gH}$ Q=0.60(3.88) $\sqrt{2(32.2)(1.25)}$ Q=20.89 CFS

GRATE



H=(1.25+0.89)/2=1.08 $Q=CA\sqrt{2gH}$ $Q=0.60(1.91)\sqrt{2(32.2)(1.08)}$ Q=9.56 CFS

Q = 20.89 + 9.56 = 30.45 CFS

Total on site runoff is only 14.36 cfs and we will have two single A on site.

FINDING STREET CAPACITY - 26 F-F CROSS-SECTION FOR 4" CURB

Q = 1.49/n A R^(2/3) S^ $\frac{1}{2}$ n = 0.017 SLOPE = STREET SLOPE R^2/3 = (A/P)^2/3 D2 = HYDRAULIC DEPTH AFTER HYDRAULIC JUMP = D1/2 [SQRT (1 + 8Fr²) - 1]

HALF STREET CALCULATIONS

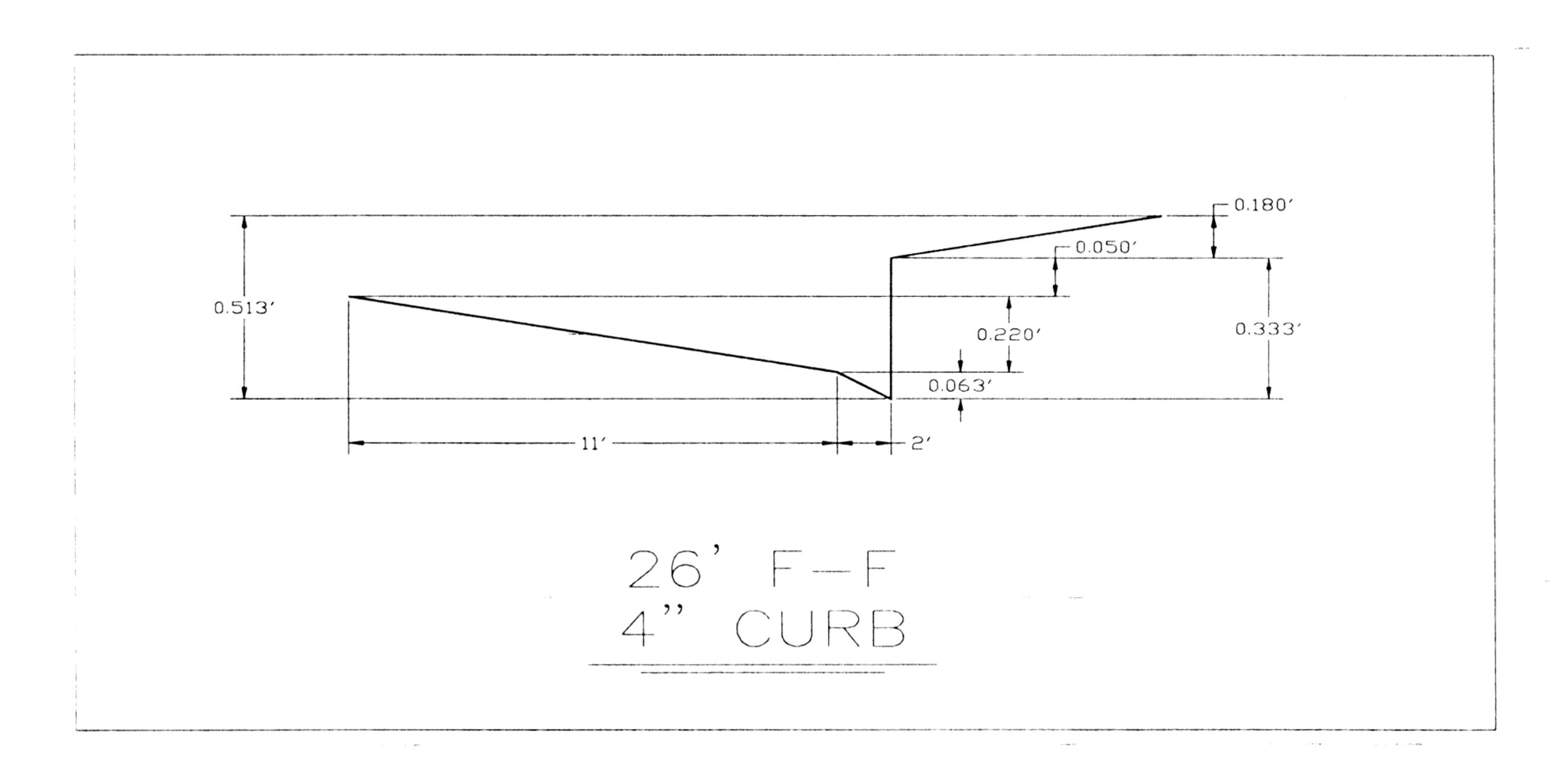
@Y < 0.0625A1 = $\frac{1}{2}$ Y (Y/0.03125) = 16Y² P1 = SQRT[Y² + (Y/0.03125)²] + Y = SQRT(1025 Y²) + Y

@ 0.0625 < Y < 0.2825 & Y1 = Y - 0.0625A2 = A1 + ½Y1 (Y1/0.02) + 2Y1 = A1 + 25Y1² + 2Y1 P2 = P1 + SQRT[Y1² + (Y1/0.02)²] + Y1 = P1 + SQRT(2501 Y²) + Y1

@ 0.2825 < Y < 0.333 & Y2 = Y - 0.2825A3 = A2 + 13Y2 P3 = P2 + Y2

@ 0.333 < Y < 0.513 & Y3 = Y - 0.333A4 = A3 + 13Y3 + ½Y3[Y3/(0.02)] = A3 + 13 Y3 + 25 Y3² P4 = P3 + SQRT(Y3² + [Y3/(0.02)]²) = P3 + SQRT(2501 Y3²)

SEE THE FOLLOWING SHEET FOR CALCULAITON



26 F-F STREET CROSS-SECTION (4" CURB)

FINDING STREET CAPACITY

 $Q = 1.49 / n A (A/P)^{2/3} S^{1/2}$

0.017

SLOPE = 0.01370

HALF STREET CALCULATIONS

FULL STREET FLOW

@Y > 0.0625

 $A1 = \frac{1}{2} Y (Y/0.03125) = 16Y^2$

 $P1 = SQRT[Y^2 + (Y/0.03125)^2] + Y = SQRT(1025 Y^2) +$

| Y (FT) | Α | Р | (A/P) ² /3 | Q | 2Q | V | Fr | D*V | D2 |
|--------|--------|--------|-----------------------|------|------|------|------|---------|------|
| 0.0250 | 0.0100 | 0.8254 | 0.0528 | 0.01 | 0.01 | 0.54 | 0.60 | 0.01349 | 0.01 |
| 0.0500 | 0.0400 | 1.6508 | 0.0837 | 0.03 | 0.07 | 0.86 | 0.68 | 0.04284 | 0.03 |
| 0.0625 | 0.0625 | 2.0635 | 0.0972 | 0.06 | 0.12 | 0.99 | 0.03 | 0.06213 | 0.00 |

@ 0.0625 < Y < 0.2825 & Y1 = Y - 0.0625

 $A2 = A1 + \frac{1}{2}Y1 (Y1/0.02) + 2Y1 = A1 + 25Y1^2 + 2Y1$

 $P2 = P1 + SQRT[Y1^2 + (Y1/0.02)^2] + Y1 = P1 + SQRT(2501 Y^2) + Y1$

| 0.1000 | 0.1727 | 3.9764 | 0.1235 | 0.22 | 0.44 | 1.26 | 0.70 | 0.1264 | 0.06 |
|--------|--------|---------|--------|------|------|------|------|--------|------|
| 0.1500 | 0.4289 | 6.5269 | 0.1628 | 0.71 | 1.43 | 1.67 | 0.76 | 0.2499 | 0.10 |
| 0.2000 | 0.8102 | 9.0774 | 0.1997 | 1.66 | 3.31 | 2.04 | 0.81 | 0.4087 | 0.15 |
| 0.2500 | 1.3164 | 11.6279 | 0.2340 | 3.15 | 6.30 | 2.39 | 0.84 | 0.5986 | 0.20 |
| 0.2825 | 1.7125 | 13.2857 | 0.2552 | 4.47 | 8.94 | 2.61 | 0.87 | 0.7375 | 0.23 |

@ 0.2825 < Y < 0.333 & Y2 = Y - 0.2825

A3 = A2 + 13Y2

P3 = P2 + Y2

| 0.3000 | 1.9400 | 13.3032 | 0.2771 | 5.50 | 11.00 | 2.83 | 0.91 | 0.8504 | 0.26 |
|--------|--------|---------|--------|------|-------|------|------|--------|------|
| 0.3100 | 2.0700 | 13.3132 | 0.2892 | 6.12 | 12.25 | 2.96 | 0.94 | 0.9171 | 0.28 |
| 0.3260 | 2.2780 | 13.3292 | 0.3080 | 7.18 | 14.36 | 3.15 | 0.97 | 1.0272 | 0.31 |
| 0.3333 | 2.3729 | 13.3365 | 0.3163 | 7.68 | 15.36 | 3.24 | 0.99 | 1.0788 | 0.33 |

@ 0.333 < Y < 0.513 & Y3 = Y - 0.333

 $A4 = A3 + 13Y2 + \frac{1}{2}Y2[Y3/(0.02)] = A3 + 13Y3 + 25Y3^2$

 $P4 = P3 + SQRT(Y3^2 + [Y3/(0.02)]^2) = P3 + SQRT(2501 Y3^2)$

| 0.4000 | 3.4179 | 16.6721 | 0.3477 | 12.16 | 24.32 | 3.56 | 0.99 | 1.4229 | 0.40 |
|--------|--------|---------|--------|-------|-------|------|------|--------|------|
| 0.4500 | 4.3472 | 19.1726 | 0.3718 | 16.54 | 33.08 | 3.80 | 1.00 | 1.7120 | 0.45 |
| 0.5000 | 5.4014 | 21.6731 | 0.3960 | 21.89 | 43.77 | 4.05 | 1.01 | 2.0259 | 0.51 |
| 0.5130 | 5.6960 | 22.3233 | 0.4023 | 23.44 | 46.89 | 4.12 | 1.01 | 2.1115 | 0.52 |

FINDING STREET CAPACITY - 26 F-F CROSS-SECTION FOR 8" CURB

Q = 1.49/n A R^{$^{^{^{^{\prime}}}$}(2/3) S^{$^{^{^{\prime}}}$}/
n = 0.017 SLOPE = STREET SLOPE R^{$^{^{^{\prime}}}$}2/3 = (A/P) $^{^{^{^{\prime}}}}$ 2/3 D2 = WATER DEPTH AFTER HYDRAULIC JUMP = D1/2 [SQRT (1 + 8Fr^{$^{^{\prime}}$}) - 1]

HALF STREET CALCULATIONS

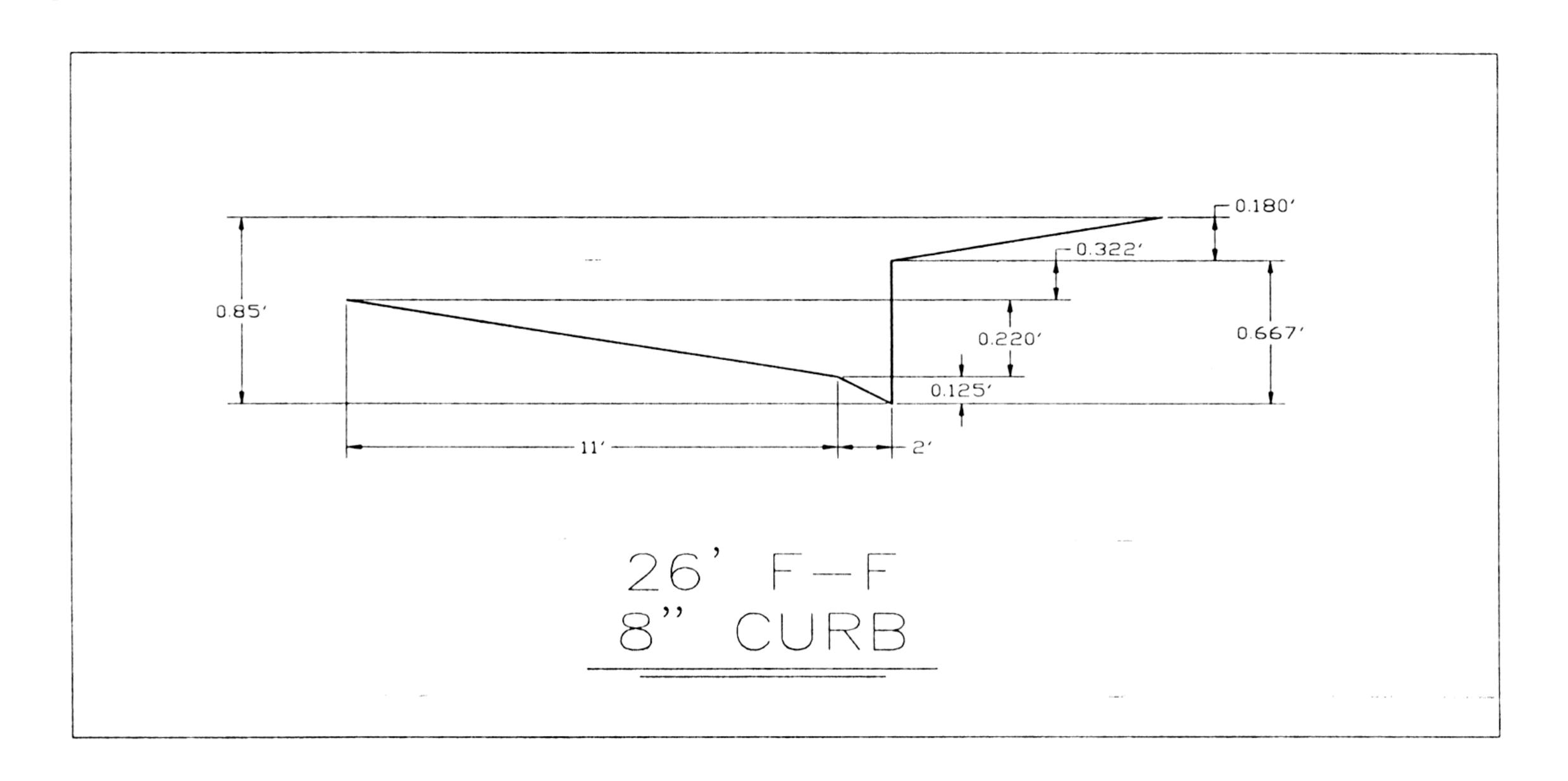
@Y < 0.125 A1 = $\frac{1}{2}$ Y (Y/0.0625) = 8Y² P1 = SQRT[Y² + (Y/0.0625)²] + Y = SQRT(257 Y²) + Y

@ 0.125 < Y < 0.345 & Y1 = Y - 0.125A2 = A1 + ½Y1 (Y1/0.02) + 2Y1 = A1 + 25Y1² + 2Y1 P2 = P1 + SQRT[Y1² + (Y1/0.02)²] + Y1 = P1 + SQRT(2501 Y1²) + Y1

@ 0.345 < Y < 0.667 & Y2 = Y - 0.345A3 = A2 + 13Y2 + ½Y2[Y2/(0.02)] = A2 + 13 Y2 P3 = P2 + SQRT(Y2² + [Y2/(0.02)]²) = P2 + Y2

@ 0.667 < Y < 0.847 & Y3 = Y - 0.667 $A4 = A3 + 13Y3 + \frac{1}{2}Y3[Y3/(0.02)] = A3 + 13 Y3 + 25 Y3^2$ $P4 = P3 + SQRT(Y3^2 + [Y3/(0.02)]^2) = P3 + SQRT(2501 Y3^2)$

SEE THE FOLLOWING SHEET FOR CALCULAITON



26 F-F STREET CROSS-SECTION (8" CURB)

FINDING STREET CAPACITY

 $Q = 1.49 / n A (A/P)^{2/3} S^{1/2}$

n =

0.017

SLOPE =

0.8467

22.8011

10.6125

0.0137

| HALF STREET CALCULATION | | | | FŲLL STREET FLOW | | | | | |
|------------------------------|-------------------|-----------------------------|-------------------|-----------------------------|--------|---------|------|----------|------|
| @Y < 0.125 | | _ | **** | | | | | | |
| $A1 = \frac{1}{2} Y (Y / 0)$ | • | | | | | | | | |
| $P1 = SQRT[Y^2]$ | + (Y / 0.0625 | $\frac{(s)^2}{2} + Y = SQR$ | $(T(257 Y^2) + Y$ | | 4 | | | | |
| Y (F I) | Α | P | (A/P)^2/3 | Q | 2Q | V | Fr | D*V | D2 |
| 0.0250 | 0.0050 | 0.4258 | 0.0517 | 0.00 | 0.01 | 0.53 | 0.59 | 0.013215 | 0.01 |
| 0.0500 | 0.0200 | 0.8516 | 0.0820 | 0.02 | 0.03 | 0.84 | 0.66 | 0.041954 | 0.03 |
| 0.1250 | 0.1250 | 2.1289 | 0.1511 | 0.19 | 0.39 | 1.55 | 0.04 | 0.193201 | 0.00 |
| @ 0.125 < Y < | 0.345 & Y | '1 = Y - 0.125 | | | | | | | |
| $A2 = A1 + \frac{1}{2} Y'$ | • | | | | | | | | |
| P2 = P1 + SQR | $RT[Y1^2 + (Y1)]$ | $(0.01)^2 + Y1$ | = P1 + SQRT | (2501 Y1 ²) + ` | Y1 | N 77-91 | | | -41 |
| 0.2000 | 0.4156 | 6.0797 | 0.1672 | 0.71 | 1.42 | 1.71 | 0.67 | 0.342118 | 0.12 |
| 0.2500 | 0.7656 | 8.6302 | 0.1989 | 1.56 | 3.12 | 2.04 | 0.72 | 0.508786 | 0.16 |
| 0.3000 | 1.2406 | 11.1807 | 0.2309 | 2.93 | 5.86 | 2.36 | 0.76 | 0.708762 | 0.21 |
| 0.3450 | 1.7750 | 13.4761 | 0.2589 | 4.70 | 9.40 | 2.65 | 0.79 | 0.913774 | 0.25 |
| @ 0.345 < Y < | 0.6667 & | Y2 = Y - 0.385 | 5 | | | | | | |
| A3 = A2 + 16 Y | ' 2 | | | | | | | | |
| P3 = P2 + Y2 | | | | | | | | | |
| 0.3500 | 1.8550 | 13.4811 | 0.2665 | 5.06 | 10.12 | 2.73 | 0.81 | 0.95443 | 0.26 |
| 0.3773 | 2.2910 | 13.5084 | 0.3064 | 7.18 | 14.36 | 3.13 | 0.90 | 1.182609 | 0.33 |
| 0.5000 | 4.2550 | 13.6311 | 0.4602 | 20.03 | 40.07 | 4.71 | 1.17 | 2.354033 | 0.62 |
| 0.6667 | 6.9217 | 13.7978 | 0.6313 | 44.71 | 89.42 | 6.46 | 1.39 | 4.306368 | 1.02 |
| @ 0.6667 < Y < | < 0.8467 & | Y3 = Y - 0.66 | 367 | | | | | | |
| A4 = A3 + 16 Y | | | | 5 Y3 ² | | | | | |
| P4 = P3 + SQR | | • | | | | | | | |
| 0.7000 | 7.4828 | 15.4646 | 0.6163 | 47.19 | 94.37 | 6.31 | 1.33 | 4.414119 | 1.01 |
| 0.7500 | 8.4286 | 17.9651 | 0.6038 | 52.07 | 104.14 | 6.18 | 1.26 | 4.633137 | 1.01 |
| 0.8000 | 9.4994 | 20.4656 | 0.5995 | 58.27 | 116.53 | 6.13 | 1.21 | 4.90684 | 1.02 |
| 0.8467 | 10 6125 | 22 9011 | 0.6006 | 6F 21 | 120.40 | C 1 1 | 4.40 | T.00001 | 1.02 |

65.21

130.42

6.14

4.90684 5.202761

1.18

1.05

0.6006