CITY OF ALBUQUERQUE



October 30, 2014

Vince Carrica, P.E. Tierra West, LLC 5571 Midway Park Pl NE Albuquerque, NM 87109

Re: FedEx Ground ABQ Drainage Report and Grading Plan and Drainage Plan Engineer's Stamp Date 10-20-14 (K09D026A)

Dear Mr. Carrica,

Based upon the information provided in your submittal received 10-22-14, the above referenced report and plan is approved for Building Permit. Please attach a copy of this approved plan to the Building Permit construction sets prior to sign-off by Hydrology

Prior to Certificate of Occupancy release, Engineer Certification per the DPM checklist will be required and the following comments will need to be addressed.

PO Box 1293

1. Provide a private drainage easement with the maintenance defined for the pond northwest of Daytona. The format should follow the one already provided for the desiltation pond west of the Fed Ex site.

Albuquerque

- 2. An easement for Floodway and Storm Drainage Works is on the east side of Tract 5-A of Avalon Subdivision Unit 5. The platting action through DRB should be complete prior to the Engineer Certification for this site.
- 3. Provide an Elevation Certificate for the work in the Floodplain.

New Mexico 87103 Please contact me at 924-3994 if you have any questions.

www.cabq.gov

Sincerely,

Amy L. D. Niese, P.E. Senior Engineer, Hydrology

Planning Department

C: e-mail

Revised G&D 10-20-14 JN: 2013075

City of Albuquerque

Planning Department

Development & Building Services Division

DRAINAGE AND TRANSPORTATION INFORMATION SHEET

(REV 02/2013)

Project Title: FedEx Ground		City Drainage #:
DRB#:	EPC#: 14EPC-40012 (Project#1	009982Work Order#:
Legal Description: A portion of Tract	of Atrisco Grant Unit 5	
City Address:		
Engineering Firm: Tierra West, LLC		Contact: Vince Carrica
Address: 5571 Midway Park Place		
Phone#: 505-858-3100	Fax#: <u>505-858-1118</u>	E-mail: vcarrica@tierrawestllc.com
Owner: I-40 South, LLC c/o Thorn	nas Keleher	Contact: Thomas Keleher
Address: P.O. Box AA, Albuquerqu	ie, NM 87103	
Phone#: 505-346-4646	Fax#:	E-mail: tfk@keleher-law.com
Architect: Castle Design Group		Contact: Larry L. Christian
Address: 3801 Kirby Drtive, Suite 60	00, Houston, TX 77098	
Phone#: 713-664-7974	Fax#:	E-mail: lchristian@castledesigngroup.com
Surveyor: Precision Surveys		Contact: Larry Medrano
Address: 5571 Midway Park Place	NE Albuquerque NM 87109	
Phone#:	Fax#:	E-mail:
Contractor: W&G Construction Con	npany	Contact: Chris White
Address: 470 Central Road, Frederi		Cili is Willie
Phone#: 5403682688	Fax#:	E-mail: cwhite@wandgconstruction.com
TYPE OF SUBMITTAL:	CHECK TYPE OF AP	PROVAL/ACCEPTANCE SOUGHT:
DRAINAGE REPORT		ARANTEE RELEASE
DRAINAGE PLAN 1st SUBMITTAL	PRELIMINARY PLA	· · · · · · · · · · · · · · · · · · ·
X DRAINAGE PLAN RESUBMITTAL	S. DEV. PLAN FOR S	
CONCEPTUAL G & D PLAN		PERMIT APPROVAL
GRADING PLAN	SECTOR PLAN APPI	
EROSION & SEDIMENT CONTROL PL		
ENGINEER'S CERT (HYDROLOGY)	AN (ESC) FINAL PLAT APPRO CERTIFICATE OF Q	HOUTERNO PERNOVIE
CLOMR/LOMR	CERTIFICATE OF O	COUPANCY (TCL TEMP)
TRAFFIC CIRCULATION LAYOUT (TO	CL) FOUNDATION PERM	COUPANCY (TCL TEMP)
ENGINEER'S CERT (TCL)	X BUILDING PERMIT	APPROVAL
ENGINEER'S CERT (DRB SITE PLAN)		AND DEVELOPMENT SPC PIORPROVAL
ENGINEER'S CERT (ESC)	PAVING PERMIT AF	
SO-19	WORK ORDER APPR	
OTHER (SPECIFY)	GRADING CERTIFIC	
WAS A PRE-DESIGN CONFERENCE ATTER	NDED: Yes No	Copy Provided
DATE SUBMITTED: 09/19/2014 Revised	1 10-20-14 By: Vince Carrica	

Requests for approvals of Site Development Plans and/or Subdivision Plats shall be accompanied by a drainage submittal. The particular nature, location, and scope to the proposed development defines the degree of drainage detail. One or more of the following levels of submittal may be required based on the following

- 1. Conceptual Grading and Drainage Plan: Required for approval of Site Development Plans greater than five (5) acres and Sector Plans
- 2. Drainage Plans: Required for building permits, grading permits, paving permits and site plans less than five (5) acres
- 3. Drainage Report: Required for subdivision containing more than ten (10) lots or constituting five (5) acres or more
- 4. Erosion and Sediment Control Plan: Required for any new development and redevelopment site with 1-acre or more of land disturbing area, including project less than 1-acre than are part of a larger common plan of development

lierrawestllc.com



TIERRA WEST, LLC

October 20, 2014

Ms. Amy L. D. Niese, P.E. Senior Engineer, Hydrology Planning Department PO Box 1293 Albuquerque, NM 87103

RE: FedEx Ground ABQ Drainage Report and Grading Plan and Drainage Plan Engineer's Stamp Date 9-12-14 (K09D026A)

Dear Ms. Niese:

Per correspondence from your office dated October 06, 2014, please find the following responses addressing the drainage comments listed below:

1. On sheet G-6, a desiltation pond is shown northwest of Daytona. Provide rip-rap on the upward slope from the bottom of the pond elevation to the top of pond. Include a top of pond elevation. Show existing contour elevations that the pond is tying into. What is the top of pond elevation? Provide a swale from the top of pond to the concrete pad for the 24 inch storm pipe. Ultimately, the 24 inch storm pipe will receive 48 cfs. The pipe is at a 20% slope. Reduce the slope and provide the HGL for the proposed 24 inch and 36 inch pipe n Daytona. Also provide the HGL for the storm drain in Los Volcanes. The ROW for Daytona begins to curve near the pond. Show the correct ROW.

Response: Rip rap, contour elevations, top of pond elevation and a swale have been added to the pond layout. The slope of the 24" lateral pipe has been reduced to 6%. P&P sheets from the work order set are attached for reference with HGL information for both Los Volcanes and Daytona storm drains. The right of way for Daytona is updated on the plan.

 Provide a private drainage easement with the maintenance defined for the pond northwest of Daytona prior to the Grading and Drainage Certification of the Fed Ex Grading and Drainage Plan. The format should follow the one already provided for the desiltation pond west of the Fed Ex site.

Response: A private drainage easement similar to the easement will be provided for the Daytona desiltation pond prior to grading and drainage certification. The format will follow the easement provided for the drainage easement west of the FedEx site.

3. For the pond north of Los Volcanes, provide enough distance for the slope so that it is actually 3:1 as called out on the plan.

Response: The pond limits have been revised to show the required 3:1 slope distances.

4. Show the storm drainage on the master drainage plan so it is easier to follow the report. Two pipe #20 references are shown. The one by the inlet should be #22 not #20.

Response: The storm drains have been added to the basin map for clarity and the pipe run numbers have been corrected.

5. In the Storm Drainage Table the basins for Pipe #18 should not include C1D1 and D2D2 for the Interim Condition. The flow stated for Pipe #18 is correct. Pipes #19 and #20 should not include basin LV5 in them because the water goes in the inlet further down at Pipe #22. Pipes #19 and #20 should total to 85.72 cfs instead of 87.00 cfs. The flow for Pipe #22 is stated as 8.48, but the basins referenced add to 7.99 cfs. The basins for Pipe #23 add to 93.71, but the total in the table is 89.86 cfs. AHYMO states 89.04 cfs is going into pond, but the basins (including surface flow) are 87.17 cfs. Please correct all discrepancies. There is no discussion of the storm drain sizing in the tables for the 24 and 36 inch storm drains in Daytona. Include that.

Response: The noted changes have been made to the drainage table.

Under Interim Drainage Conditions, the report states 16.1 cfs drains to the desiltation pond north of Los Volcanes. The amount is 28.34 cfs for the summation of the drainage basins referenced. Please revise.

Response: The report has been revised with noted change.

7. Provide a detail (width and size) for the rip-rap along the east and south sides of the parking lot.

Response: A detail has been added to sheet GR-4.

8. Where the 18 inch storm drains connect to the storm pipe north of the building, what are the inverts?

Response: Noted inverts have been added to sheet GR-3.

9. Inlet (2) is supposed to be a double inlet per your letter. Call it out as such on the grading plate.

Response: Inlet (2) is now shown on the plans as a double inlet.

10. An easement for Floodway and Storm Drainage Works is on the east side of Tract 5-A of Avalon Subdivision Unit 5. The platting action through DRB should be complete prior to the Certificate of Occupancy for this site.

Response: The plat was submitted and approved by DRB. We are seeking signatures from dry utility companies prior to recording the plat showing the vacation of the drainage easement along the east side of the FedEx property.

If you have any questions or need additional information regarding this response, please do not hesitate to contact me.

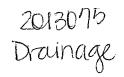
Sincerely.

Vincent Carrica, P.E.

Enclosure/s

JN: 2013075.20

VPC/sc Z:\2013\2013\075 Daytona Blvd Distribution Center\Working Documents\2013\075.20 14-10-21 Final FedEx Ground Response Letter - Amy L. D. Niese.docx



City of Albuquerque

Planning Department

Development & Building Services Division

DRAINAGE AND TRANSPORTATION INFORMATION SHEET
(REV 02/2013)

Project Title: FedEx Ground		City Drainage#:
DRB#: EPC#: 14	EPC-40012 (Project#1009982)work	Order#:
Legal Description: A portion of Tract 12, Tract 13	and Tract 14A, Town of Atrisco (Grant Unit 5
City Address:		
Engineering Firm: Tierra West, LLC	Contac	et: Vince Carrica
Address: 5571 Midway Park Place NE Albuqu	erque NM 87109	- Inde Carrio
Phone#: 505-858-3100 Fax#: 505		: vcarrica@tierrawestllc.com
Owner: I-40 South, LLC c/o Thomas Keleher		t: Thomas Keleher
Address: P.O. Box AA, Albuquerque, NM 871	03	
Phone#: 505-346-4646 Fax#:	E-mail	tfk@keleher-law.com
Architect: Castle Design Group	Contac	t: Larry L. Christian
Address: 3801 Kirby Drtive, Suite 600, Houston	, TX 77098	
Phone#: 713-664-7974 Fax#:	E-mail	lchristian@castledesigngroup.com
Surveyor: Precision Surveys	Contac	t: Larry Medrano
Address: 5571 Midway Park Place NE Albuqu		
Phone#: Fax#:	E-mail	
Contractor: W&G Construction Company	Contac	t:Chris White
Address: 470 Central Road, Fredericksburg, V.		
Phone#: 5403682688 Fax#:	E-mail	cwhite@wandgconstruction.com
TYPE OF SUBMITTAL:	CHECK TYPE OF APPROVAL/ACC	EPTANCE SOUGHT:
DRAINAGE REPORT	SIA/FINANCIAL GUARANTEE REL	EASE
DRAINAGE PLAN 1st SUBMITTAL	PRELIMINARY PLAT APPROVAL	
X DRAINAGE PLAN RESUBMITTAL	S. DEV. PLAN FOR SUB'D APPROV	AL
CONCEPTUAL G & D PLAN	S. DEV. FOR BLDG. PERMIT APPRO	OVAL DE QE IVED
GRADING PLAN	SECTOR PLAN APPROVAL	MEGEIVEN
EROSION & SEDIMENT CONTROL PLAN (ESC)	FINAL PLAT APPROVAL	
ENGINEER'S CERT (HYDROLOGY)	CERTIFICATE OF OCCUPANCY (PE	ERM)
CLOMR/LOMR	CERTIFICATE OF OCCUPANCY (TO	CL TEMPOLI
TRAFFIC CIRCULATION LAYOUT (TCL)	FOUNDATION PERMIT APPROVAL	LAND DEVELOPMENT SECTION
ENGINEER'S CERT (TCL)	X BUILDING PERMIT APPROVAL	FAMD DE AFFOR MENT DES LIGHT
ENGINEER'S CERT (DRB SITE PLAN)	GRADING PERMIT APPROVAL	SO-19 APPROVAL
ENGINEER'S CERT (ESC)	PAVING PERMIT APPROVAL	ESC PERMIT APPROVAL
SO-19	WORK ORDER APPROVAL	ESC CERT. ACCEPTANCE
OTHER (SPECIFY)	GRADING CERTIFICATION	OTHER (SPECIFY)
WAS A PRE-DESIGN CONFERENCE ATTENDED:	Yes No Copy Provi	ded
DATE SUBMITTED: 09/09/2014 KEUISE \$\ 10 \ 20/14	By: Vince Carrica	

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DRAINAGE REPORT

For

FEDEX GROUND ABQ ALBUQUERQUE, NEW MEXICO

Prepared by

Tierra West, LLC 5571 Midway Park Place NE Albuquerque, New Mexico 87109

Prepared for

W&G Construction Company 470 Central Rd. Fredericksburg, VA 22401

October 09, 2014

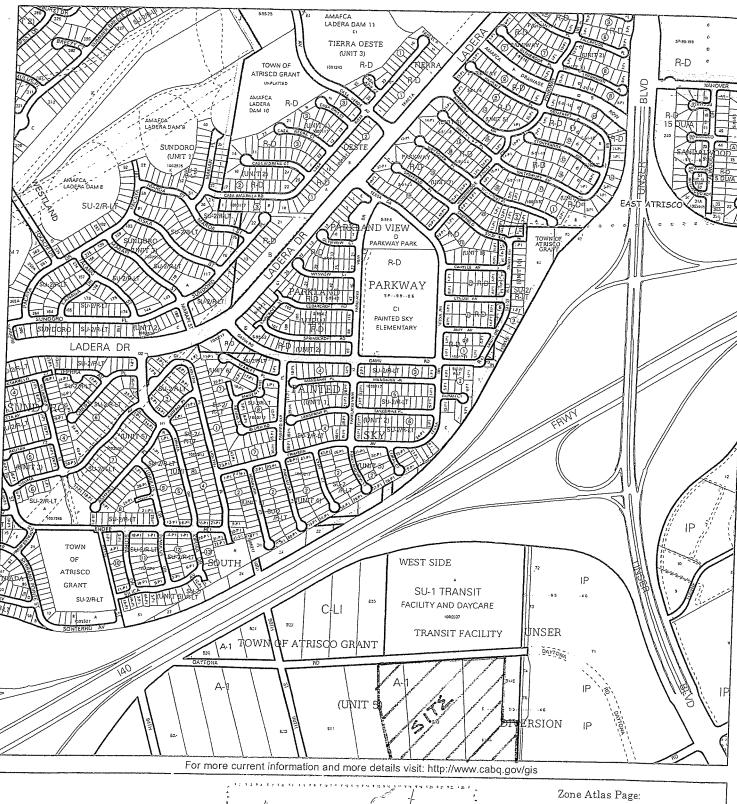
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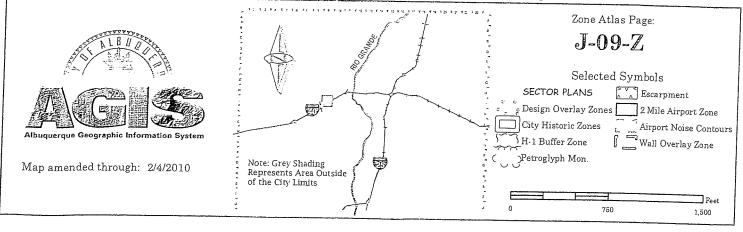
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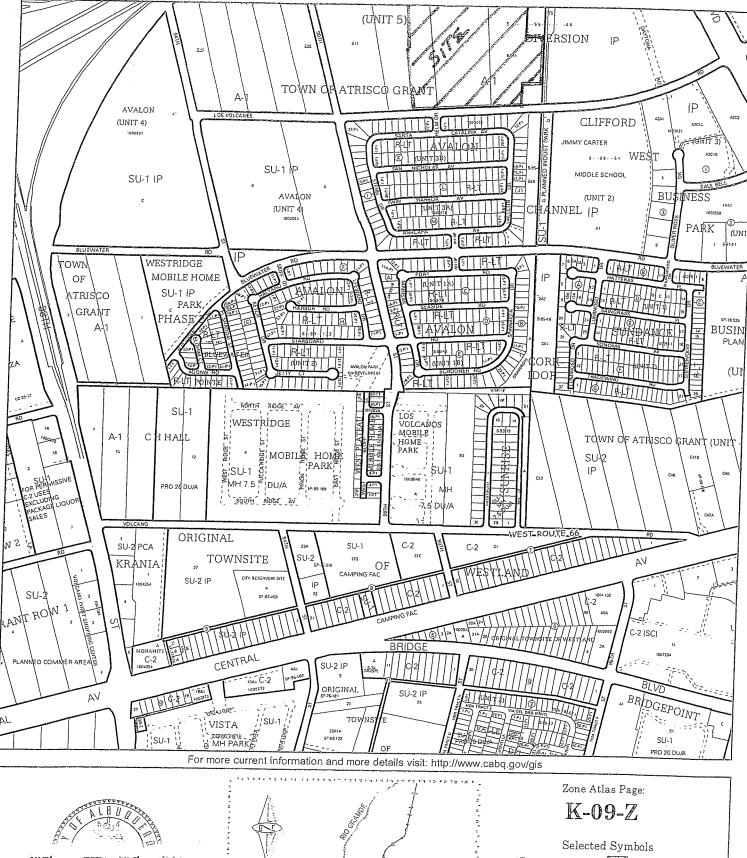
Vincent Carrica, PE # 16212

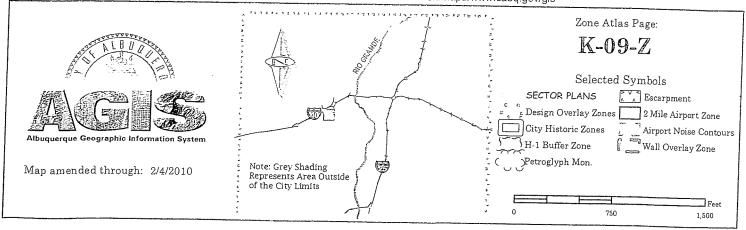
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Basin Map Developed Conditions	MAP POCKET









LOCATION

The proposed commercial development, FedEx Ground ABQ, is comprised of approximately 21.86 acres zoned SU-1 For IP and C-2 Uses and is located in the City of Albuquerque, in Bernalillo County. The site is bordered by Daytona Road to the north, Los Volcanes Road to the south, undeveloped property to the west and storm drain ponds and undeveloped property to the east. An existing ABCWUA water well facility exists adjacent to the southeast corner of the site. The subject property is currently undeveloped with an existing arroyo bisecting the site from northwest to south east.

This report represents a drainage management and grading plan for approval by the City of Albuquerque, for Site Plan for Building Permit submittal.

DRAINAGE BASIN DESIGNATION

The drainage basins for proposed conditions are as indicated on the BASIN MAP included in this report. On-site basins are designated as "A-xx". Off-site upstream basins are designated as "C-xDx". Basins within Daytona right-of-way are designated as "D-1x". Basins within Los Volcanes right-of-way are designated as "LV-x".

EXISTING DRAINGE CONDITIONS

The site is currently undeveloped and drains from northwest to southeast with an existing slope ranging between two to five percent. The northernmost portion of the site is captured in the Mirehaven Arroyo and drains into the temporary Pond 5 of the Unser Diversion Pond system. The remaining southern portion of the site currently drains via surface flow to Los Volcanes Road and into the existing Pond 4 of the Unser Diversion Pond system via curb inlets and storm drain pipes located at the low point in Los Volcanes Road.

FIRM MAP AND SOIL CONDITIONS

The FedEx Ground Albuquerque is currently partially located in a designated Flood Hazard Zone AO per FEMA – (Firm Map 35001C0328H – See Attached Map). Per the USDA Soil Conservation Services (SCS), the soils type for this site is Bluepoint Loamy fine sand and

Pajarito loamy fine sand and consists largely of undulating excessively drained soils at 1 to 9 percent slopes. Runoff is medium, the hazard of soil blowing is moderate and the hazard of water erosion is slight.

DESIGN-CRITERIA

The drainage plan presented in this report was prepared in accordance with the City of Albuquerque Drainage Ordinances and Chapter 22 of the Development Process Manual DPM. The hydrological analysis is based on the 100-year frequency, 6-hour duration storm, as Represented in Section 22, Part A, Hydrology, of the Development Process Manual. Storage detention ponds are sized for the 100-year, 24-hour storm and ultimately will drain in less than 24 hours.

Rainfall intensities per this report are as follows:

FREQ	ZONE	P60	P360	P1440
100YR	1	1.87	2.20	2.66

Land Treatments:

Proposed Subdivision:

The proposed commercial developed land use values were calculated as follows:

Commercial

A = 0% (Under fully developed conditions, no undisturbed naturally vegetated areas will remain.)

B = 0 % (Under fully developed conditions, no irrigated lawns will be provided)

C = Varies 25% to 100% depending on individual basin which will be landscaped to varying degrees with gravel and Xeriscaping

D= Varies 70% to 100% depending on individual basin which will be paved or covered by buildings

INTERIM DRAINGE CONDITIONS

The current landowner worked with AMAFCA to cut off flows to the Mirehaven Arroyo from the north side of Interstate-40, which will now be routed in the North I-40 Diversion system. This diversion greatly reduces flows that impact this site. AMAFCA will also cause to have a LOMR completed and submitted to FEMA to adjust the flood plain from what is currently mapped. This adjustment to the flood plain will show the proposed site as being removed from the flood plain.

The existing Mirehaven Arroyo that traverses the site from northwest to northeast will be filled in order to construct the proposed improvements including a building, drive aisles and parking facilities. An updated master drainage plan for the area is being prepared by Easterling Consultants, LLC for the City.

Under Interim conditions all upland basins designated as "C-xDx" will remain undeveloped. Basin C-3D will continue to drain to Daytona right-of-way where it will be routed through a desilting pond, captured in a storm drain that will be extended from in front of the existing Bruckner's facility and conveyed east to Pond 6 of the Unser Diversion Pond system. Basins C-1D2, C-2D1 and C-4D (approximately 28.34 cfs) will drain to a proposed desilting pond and into a storm drain lateral that will direct the flows into the proposed Los Volcanes storm drain that will run east and connect into an existing 48" storm drain and into Pond 4 of the Unser Diversion Pond System. The desilting pond and storm drain lateral are intended to be temporary until such time as the applicable basins are develop where at that point the lateral can be used for a future storm drain curb drop inlet outfall.

Basins C-1D1 and C-2D2 (approximately 5.2 cfs) will continue to drain into the Los Volcanes right-of-way where they will surface flow along with Basin LV-1 thru LV-5 down the roadway to proposed and existing curb drop inlets and into Pond 4 of the Unser Diversion Pond system.

Also under interim drainage conditions, the FedEx Ground site will be developed including all on-site basins designated as "A-xx" along with the north half of Los Volcanes Rd

and the south half of Daytona Rd along the frontage of the FedEx property. All on-site basins with the exception of Basins A-16 and A-17 will drain to an on-site detention pond formerly designated as Pond 5 of the Unser Diversion Pond system. The out flow of this on-site detention pond will be tied to the existing storm drain line that caries flows to Pond 4 of the Unser Diversion Pond system. Basins A-16 and A-17 will drain to an area Inlet (12) that will be tied to the proposed storm drain in Los Volcanes which will be tied to the existing storm drain that runs into Pond 4 of the Unser Diversion Pond system.

Former Pond 5 of the Unser Diversion System will be a private pond, which will act as a detention pond with an outfall to the Unser Diversion System of less than 10 cfs maximum. An emergency overflow structure exists and will remain on the pond. The overflow directs flows in excess of the pond's capacity to the east along the arroyo's historic route.

The drainage plan for routing flows from the site and from the upland basins is per the I-40 South and Unser Mini Drainage Master Plan prepared by Easterling Consultants LLC as Revision #1 dated April 2014. The existing outlet structure in Pond 5 will be revised to include a ported outlet riser that will restrict the flow rate out of the pond to less than 10 cfs for the 100-year, 24-hour design storm. The proposed maximum flow rate out of Pond 5 will be far less than the allowable flow rate as provided for in the Daytona Road Storm Drain Master Plan prepared for the West Side Transit Facility by Smith Engineering, February 2001. The proposed Pond 5 volume will be 5.66 ac-ft. The required volume at a maximum 10 cfs outflow is 2.39 ac-ft. The bottom of the pond will be one foot lower than the outfall invert to account for the first flush volume and any future sediment build up. Minor on-site ponding is provided in addition to this main detention pond. This minor ponding volume was not included in the calculations for required volumes and outflow from the main pond.

ULTIMATE DRAINAGE CONDITIONS

Under ultimate drainage conditions the on-site drainage basins will continue to drain as described above. Pond 5 will be a private detention pond and will continue to outfall to the existing storm drain culvert that ties Pond 6 to Pond 4 of the Unser Diversion Pond system. The upland off-site basins designated as "C-xDx" will be developed. Basins C-3D and C-4D will drain to Daytona and will be conveyed east to Pond 6 of the Unser Diversion Pond system. Basins C-1D1, C-1D2, C-2D1 and C-2D2 will drain south to Los Volcanes where the proposed

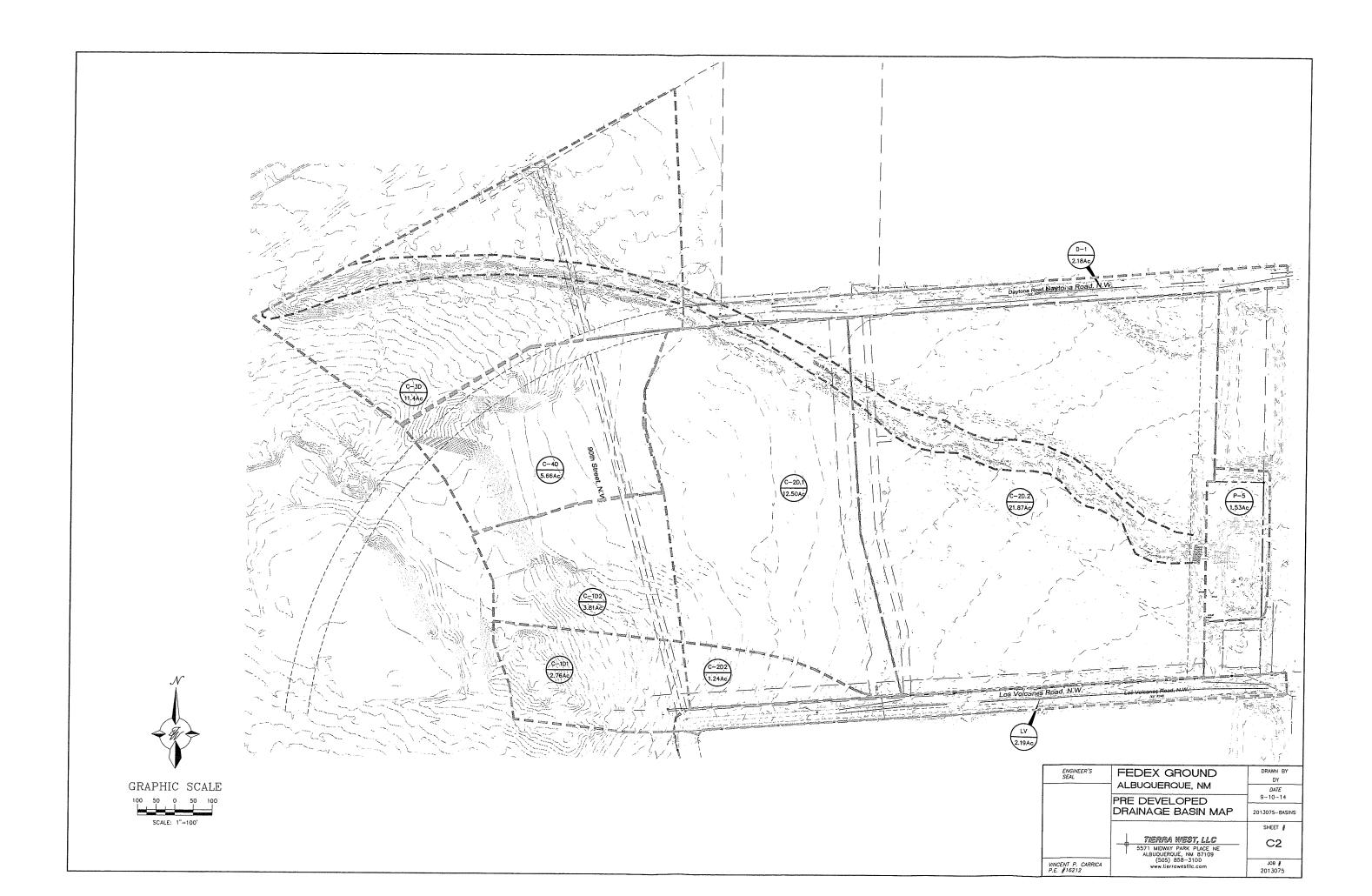
storm drain that is constructed under interim conditions will be extended west to accept the developed flows (approximately 85.7 cfs). These flows will be conveyed to Pond 4 of the Unser Diversion Pond system.

Basins D-1A, D-1B and D-1C will drain to existing or proposed drop inlets in Daytona Road and will be conveyed to Pond 6 of the Unser Diversion Pond system. Basins LV-1 through LV-5 will continue to drain down Los Volcanes either as surface flow in the roadway or be intercepted by existing and proposed drop inlets, eventually being routed into Pond 4 of the Unser Diversion Pond system.

A LOMR will be completed to adjust the flood plain and FEMA maps from what is currently mapped. This adjustment to the flood plain will show the proposed site as well as the parcels to the west as having been removed from the flood plain.

SUMMARY

The proposed grading and drainage plan for the FedEx Ground Albuquerque site provides the grading and drainage elements which are capable of safely passing the 100-year storm and meet the COA DPM requirements. Development of the site will take place after the flows into the Mirehaven Arroyo from north of Interstate-40 were cut off, greatly reducing the upland flows from west of the site and effectively removing the site from the existing flood plain. The remaining upland flows and onsite developed flows will be routed via surface flow and underground storm drains to the existing detention pond which in turn is tied to the Unser Diversion Pond system. The proposed drainage plan for developed conditions follows the I-40 South and Unser Mini Drainage Master Plan.



FEDEX GROUND ALBUQUERQUE

		Inte	rim Post D	eveloped .	FedEX Gro	und Drain	age Calci	ulations					
					and Upstream								
	1	This table i	s based on the	COA DPM Se	tion 22.2, Zone	:[1			·- T	r	Т	T	7
BASIN	Area	Area		Land Treatm	ent Percenlages		Q(100)	Q(100)	WTE	V(100) ₃₆₀	V(100) ₁₄₄₀	V(100) _{10day}	Comments
	(SQ. FT)	(AC.)	Α	В	С] D	(cts/ac.)	(CFS)	(inches)	(CF)	(CF)	(CF)	
C-1D1	120225	2.76	100.0%	0.004									To Los Voicanes and Por
C-ID1	120225	2./6	100.0%	0.0%	0.0%	0.0%	1.29	3.56	0.44	4408	4408	20438	(Public)
					1								To Temp Swale, Los Volcanes and Pond 4
C-1D2	165963	3.81	100.0%	0.0%	0.0%	0.0%	1.29	4.91	0.44	6085	6085	28214	(Public)
													To Temp Swale, Los
C-2D.1	544591	12.50	100.0%	0.0%	0.0%	0.0%	1.29	16.13	0.44	19968	10000	00500	Volcanes and Pond 4
	 		100.070	0.070	0.076	0.078	1.23	10.13	0.44	19968	19968	92580	(Public) To Los Voicanes and Por
C-2D.2	54001	1.24	100.0%	0.0%	0.0%	0.0%	1.29	1.60	0.44	1980	1980	9180	(Public)
0.00	407404	44.44	100.00/										To Daytona and Pond
C-3D	497104	11.41	100.0%	0.0%	0.0%	0.0%	1.29	14.72	0.44	18227	18227	84508	(Pubilc)
	1		1			i					İ		To Temp Swale, Los
C-4D	246344	5 .66	100.0%	0.0%	0.0%	0.0%	1.29	7.30	0.44	9033	9033	41878	Volcanes and Pond 4 (Public)
D-1A	45518	1.04	0.0%	0.0%	10.0%	90.0%	4.22	4.41	1.87	7101	9968	13170	To Pond 6 (Public)
D-1B	29635	0.68	0.0%	0.0%	10.0%	90.0%	4.22	2.87	1.87	4623	6490	8574	To Pond 6 (Public)
D-1C	7360	0.17	0.0%	50.0%	10.0%	40.0%	3.05	0.52	1.22	749	956	1731	To Pond 6 (Public)
D-1D	12710	0.29	0.0%	90.0%	10.0%	0.0%	2.11	0.62	0.70	744	744	2438	To Pond 4 (Public)
A-1	19495	0.45	0.0%	0.0%	100.0%	0.0%	2.87	1.28	0.99	1608	1608	4208	To Pond 5 (Private)
A-2	126940	2.91	0.0%	0.0%	25.0%	75.0%	4.00	11.64	1.73	18248	24912	35173	To Pond 5 (Private)
A-3	35097	0.81	0.0%	0.0%	0.0%	100.0%	4.37	3.52	1.97	5762	8219	10441	To Pond 5 (Private)
A-4	94094	2.16	0.0%	0.0%	25.0%	75.0%	4.00	8.63	1.73	13526	18466	26072	To Pond 5 (Private)
A-5	46006	1.06	0.0%	0.0%	0.0%	100.0%	4.37	4.62	1.97	7553	10773	13687	To Pond 5 (Private)
A-6	22899	0.53	0.0%	0.0%	0.0%	100.0%	4.37	2.30	1.97	3759	5362	6812	To Pond 5 (Private)
A-7	22898	0.53	0.0%	0.0%	0.0%	100.0%	4.37	2.30	1.97	3759	5362	6812	To Pond 5 (Private)
A-8	22896	0.53	0.0%	0.0%	0.0%	100.0%	4.37	2.30	1.97	3759	5361	6812	To Pond 5 (Private)
A-9	20854	0.48	0.0%	0.0%	0.0%	100.0%	4.37	2.09	1.97	3424	4883	6204	To Pond 5 (Private)
A-10	6239 0	1.43	0.0%	0.0%	10.0%	90.0%	4.22	6.04	1.87	9733	13663	18052	To Pond 5 (Private)
A-11	129032	2.96	0.0%	0.0%	25.0%	75.0%	4.00	11.83	1.73	18548	25323	35753	To Pond 5 (Private)
A-12	67194	1.54	0.0%	0.0%	90.0%	10.0%	3.02	4.66	1.09	6092	6563	15051	To Pond 5 (Private)
A-13	30790	0.71	0.0%	0.0%	25.0%	75.0%	4.00	2.82	1.73	4426	6043	8531	To Pond 5 (Private)
A-14	18000	0.41	0.0%	0.0%	100.0%	0.0%	2.87	1.19	0.99	1485	1485	3885	To Pond 5 (Private)
A-15	195109	4.48	0.0%	0.0%	30.0%	70.0%	3.92	17.56	1.68	27250	36811	53265	To Pond 5 (Private)
A-16	49958	1.15	0.0%	0.0%	100.0%	0.0%	2.87	3.29	0.99	4122	4122	10783	To Los Volcanes and Pone (Public)
A-17	8538	0.20	0.0%	0.0%	100.0%	0.0%	2.87	0.56	0.99	704	704	1843	To Los Volcanes and Pon (Public)
P-5	66622	1.53	0.0%	0.0%	100.0%	0.0%	2.87	4.39	0.99	5496	5496	14379	To Pond 5 (Private)
LV-1	29565	0.68	0.0%	0.0%	10.0%	90.0%	4.22	2.86	1.87	4612	6475	8554	To Pond 4 (Public)
LV-2	31842	0.73	0.0%	0.0%	10.0%	90.0%	4.22	3.08	1.87	4967	6973	9213	To Pond 4 (Public)
LV-3	13271	0.30	0.0%	0.0%	10.0%	90.0%	4.22	1.29	1.87	2070	2906	3840	To Pond 4 (Public)
LV-4	7680	0.18	0.0%	50.0%	10.0%	40.0%	3.05	0.54	1.22	782	997	1806	To Pond 4 (Public)
LV-5	13253	0.30	0.0%	90.0%	10.0%	0.0%	2.11	0.64	0.70	775	775	2542	To Pond 4 (Public)
TOTAL	2857874	65.61						156.07		225380	281142	606430	

		Ultin		Developed				ulations					
		T =		edEx Develope			loped						
	+		is based on the	COA DPM Sec	tion 22.2, Zone	: 1							7
BASIN	Area	Area			ent Percentages		Q(100)	Q(100)	WTE	V(100) ₃₆₀	V(100) ₁₄₄₀	V(100) _{10day}	Comments
	(SQ. FT)	(AC.)	A	В	С	D	(cfs/ac.)	(CFS)	(inches)	(CF)	(CF)	(CF)	
C-1D1	120225	2.76	0.0%	0.0%	10.0%	00.00/	400	44.05					To Los Volcanes and Pon
0.01	120225	2.70	0.078	0.0 /8	10.0%	90.0%	4.22	11.65	1.87	18755	26329	34785	(Public)
C-1D2	165963	3.81	0.0%	0.0%	10.0%	90.0%	4.22	16.08	1.87	25890	36346	48019	To Los Voicanes and Pon (Public)
								·				40075	To Los Volcanes and Pon
C-2D.1	544591	12.50	0.0%	0.0%	10.0%	90.0%	4.22	52.76	1.87	84956	119265	157568	(Public)
C-2D.2	54001	1.24	0.0%	0.0%	10.0%	90.0%	4.22	<i>5.00</i>	4.00	2424			To Los Volcanes and Pon
	0.001	1.27	0.078	0.078	10.076	90.0%	4.22	5.23	1.87	8424	11826	15624	(Public)
C-3D	497104	11.41	0.0%	0.0%	10.0%	90.0%	4.22	48.16	1.87	77548	108866	143829	To Daytona and Pond 6 (Public)
						1			1.07		700000	143023	To Daytona and Pond 6
C-4D	246344	5.66	0.0%	0.0%	10.0%	90.0%	4.22	23.87	1.87	38430	53949	71276	(Public)
D-tA	45518	1.04	0.0%	0.0%	10.0%	90.0%	4.22	4.41	1.87	7101	9968	13170	To Pond 6 (Public)
D-1B	29635	0.68	0.0%	0.0%	10.0%	90.0%	4.22	2.87	1.87	4623	6490	8574	To Pond 6 (Public)
D-tC	7360	0.17	0.0%	0.0%	10.0%	90.0%	4.22	0.71	1.87	1148	1612	2129	To Pond 6 (Public)
D-1D	12710	0.29	0.0%	0.0%	10.0%	90.0%	4.22	1.23	1.87	1983	2783	3677	To Pond 6 (Public)
A-1	19495	0.45	0.0%	0.0%	100.0%	0.0%	2.87	1.28	0.99	1608	1608	4208	To Pond 5 (Private)
A-2	126940	2.91	0.0%	0.0%	25.0%	75.0%	4.00	11.64	1.73	18248	24912	35173	To Pond 5 (Private)
A-3	35097	0.81	0.0%	0.0%	0.0%	100.0%	4.37	3.52	1.97	5762	8219	10441	To Pond 5 (Private)
A-4	94094	2.16	0.0%	0.0%	25.0%	75.0%	4.00	8.63	1.73	13526	18466	26072	To Pond 5 (Private)
A-5	46006	1.06	0.0%	0.0%	0.0%	100.0%	4.37	4.62	1.97	7553	10773	13687	To Pond 5 (Private)
A-6	22899	0.53	0.0%	0.0%	0.0%	100.0%	4.37	2.30	1.97	3759	5362	6812	To Pond 5 (Private)
A-7	22898	0.53	0.0%	0.0%	0.0%	100.0%	4.37	2.30	1.97	3759	5362	6812	To Pond 5 (Private)
A-8	22896	0.53	0.0%	0.0%	0.0%	100.0%	4.37	2.30	1.97	3759	5361	6812	To Pond 5 (Private)
A-9	20854	0.48	0.0%	0.0%	0.0%	100.0%	4.37	2.09	1.97	3424	4883	6204	To Pond 5 (Private)
A-10	62390	1.43	0.0%	0.0%	10.0%	90.0%	4.22	6.04	1.87	9733	13663	18052	To Pond 5 (Private)
A-11	129032	2.96	0.0%	0.0%	25.0%	75.0%	4.00	11.83	1.73	18548	25323	35753	To Pond 5 (Private)
A-12	67194	1.54	0.0%	0.0%	90.0%	10.0%	3.02	4.66	1.09	6092	6563	15051	To Pond 5 (Private)
A-13	30790	0.71	0.0%	0.0%	25.0%	75.0%	4.00	2.82	1.73	4426	6043	8531	To Pond 5 (Private)
A-14	18000	0.41	0.0%	0.0%	100.0%	0.0%	2.87	1.19	0.99	1485	1485	3885	To Pond 5 (Private)
A-15	195109	4.48	0.0%	0.0%	30.0%	70.0%	3.92	17.56	1.68	27250	36811	53265	To Pond 5 (Private)
	4 9 958	4.45	0.004	0.00/	400.00/								To Los Volcanes and Pond
A-16	49958	1.15	0.0%	0.0%	100.0%	0.0%	2.87	3.29	0.99	4122	4122	10783	(Public)
A-17	8538	0.20	0.0%	0.0%	100.0%	0.0%	2.87	0.56	0.99	704	704	4040	To Los Volcanes and Pond
P-5	66622	1.53	0.0%	0.0%	100.0%	0.0%	2.87	4.39	0.99	704 5496		1843	(Public)
LV-1	29565	0.68	0.0%	0.0%	10.0%	90.0%	4.22	2.86	1.87	5496 4612	5496	14379	To Pond 5 (Private)
LV-2	31842	0.73	0.0%	0.0%	10.0%	90.0%	4.22	3.08	1.87	4612 4967	6475	8554	To Pond 4 (Public)
LV-3	13271	0.30	0.0%	0.0%	10.0%	90.0%	4.22	1.29	1.87		6973	9213	To Pond 4 (Public)
LV-4	7680	0.18	0.0%	0.0%	10.0%	90.0%	4.22	0.74	1.87	2070	2906	3840	To Pond 4 (Public)
LV-5	13253	0.30	0.0%	0.0%	10.0%	90.0%	4.22	1.28	1.87	1198 2067	1682	2222	To Pond 4 (Public)
OTAL	2857874	65.61	0.070	0.078	10.076	30.0 /0	4.22	267.25	1.87	2067 423028	2902 583530	3835 804078	To Pond 4 (Public)

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					STORM DRAIN PIPES	
\vdash	Н		Actual	Pipe	Contributing	
Pipe Size	S	Capacity	Flow	Length	Basins	Commonts
#		cfs	cfs	Ħ		COLLINGING
1 18	3 1.07	11.71	1.28	140.00	A-1	
2 18	3 1.10	11.88	11.64	85.00	A-2	
3 24		18.84	12.92	260.00	A-1. A-2	
4 18	3 4.25	10.75	8.63	102.00	A-4	TOTAL
5 12	1.00	3.57	3.52	101.00	A-3	Transfer Avenue Transfer Trans
9 30		34.41	25.07	70.00	A-1, A-2, A-3, A-4	1000
7 30		34.41	30.90	80.00	A-1, A-2, A-3, A-4, A-5, Part A-10	
8 30		34.41	34.41	80.00	A-1, A-2, A-3, A-4, A-5, Part A-10, A-6	The state of the s
98 6	09.0	55.48	37.92	80.00	A-1, A-2, A-3, A-4, A-5, Part A-10, A-6, A-7	TOTAL
10 36	09:0	55.48	41.43	80.00	A-1, A-2, A-3, A-4, A-5, Part A-10, A-6, A-7, A-8	THE PERSON NAMED IN COLUMN NAM
11 36		55.48	44.73	25.00	A-1, A-2, A-3, A-4, A-5, Part A-10, A-6, A-7, A-8, A-9	
12 36		84.59	44.73	130.00	A-1, A-2, A-3, A-4, A-5, Part A-10, A-6, A-7, A-8, A-9	
13 18		18.26	16.49	110.00	A-11, A-12	- Control of the Cont
14 36	3 10.73	234.60	61.22	115.00	A-1, A-2, A-3, A-4, A-5, A-10, A-6, A-7, A-8, A-9, A-11, A-12	
15 24	09:0	18.84	17.56	40.00	A-15	THE PARTY OF THE P
16 24	09:0	18.84	17.56	330.00	A-15	
17 24	7.34	65.88	17.56	155.00	A-15	- Address
18 30		59.88	28.34	40.00	C-2D.1, C-1D2, C-4D	Interim Conditions
19 30		87.24	85.72	400.00	C-1D1, C-2D.1, C-1D2, C-2D2	Ultimate Conditions
		87.20	85.72	400.00	C-1D1, C-2D.1, C-1D2, C-2D2	Ultimate Conditions
		43.47	3.85	15.00	A-16, A-17	
22 18	3 23.00	59.43	7.99	5.00	A-16, A-17, 1/2 LV	***************************************
		100.88	93.71	179.00	C-1D1, C-2D.1, C-1D2, C-2D2, A-16, A-17, LV-5, LV-1	Ultimate Conditions
24 36	1.06	68.86	48.16	144.00	C-3D	
25 24	00.9	55.56	48.16	52.00	C-3D	AND THE PARTY OF T
						The state of the s
Pipe capacities are based on gravity flow using man	re based on gr	avity flow us		y's equation	ning's equation with n=0.013	

Worksheet for Irregular Section - Full Width

Project Description

Friction Method

Manning Formula

Solve For

Discharge

Input Data

Channel Slope

0.01470 ft/ft <

Normal Depth

0.57 ft

Section Definitions

Station (ft)		Elevation (ft)	
	0+00		100.67
	0+00		100.00
	0+02		100.13
	0+20		- 100.48
	0+38		100.13
	0+40		100.00
	0+40	•	100.67

Roughness Segment Definitions

Ending Station

Roughness Coefficient

(0+00, 100.67)

(0+40, 100.67)

0.016

Options

Current Roughness Weighted

Method

Pavlovskii's Method

Open Channel Weighting Method

Pavlovskii's Method

Closed Channel Weighting Method

Pavlovskii's Method

Results

Discharge

56.63 Hy/s - 2 Section QCAP = 28.31CFS

Elevation Range

100.00 to 100.67 ft

Flow Area Wetted Perimeter

11.66 41.15 ft 2720518 =xm0 5

Hydraulic Radius Top Width

0.28 ft

40.00 ft

Worksheet for Irregular Section - Full Width

Results			
Normal Depth		0.57	ft
Critical Depth		0.67	ft
Critical Slope		0.00531	ft/ft
Velocity		4.86	ft/s
Velocity Head		0.37	ft
Specific Energy		0.94	ft
Froude Number		1.59	
Flow Type	Supercritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Downstream Velocity		Infinity	ft/s
Upstream Velocity		Infinity	ft/s
Normal Depth		0.57	ft
Critical Depth		0.67	ft
Channel Slope		0.01470	ft/ft
Critical Slope		0.00531	ft/ft

Worksheet for Irregular Section - Full Width Project Description Friction Method Manning Formula Solve For Discharge Input Data Channel Slope 0.05190 ft/ft 4-Normal Depth 0.47 ft Section Definitions Station (ft) Elevation (ft) 0+00 100.67 0+00 100.00 0+02 100.13 0+20 100.48 0+38 100.13 0+40 100.00 0+40 100.67 Roughness Segment Definitions Start Station **Ending Station** Roughness Coefficient (0+00, 100.67) (0+40, 100.67) 0.016 **Options** Current Roughness vveignted Pavlovskii's Method Open Channel Weighting Method Pavlovskii's Method Closed Channel Weighting Method Pavlovskii's Method Results 53.96 H3/s - 2 Section QCAP = 26.98 cfs Discharge Elevation Range 100.00 to 100.67 ft Z Qmxx = 8 ito cfs Flow Area 7.67 Wetted Perimeter 39.94 Hydraulic Radius 0.19

38.99

Top Width

Worksheet for Irregular Section - Full Width

Results			
Normal Depth		0.47	ft
Critical Depth		0.66	ft
Critical Slope		0.00536	ft/ft
Velocity		7.04	ft/s
Velocity Head		0.77	ft
Specific Energy		1.24	ft
Froude Number		2.80	
Flow Type	Supercritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description	u		
Profile Headloss	•	0.00	ft
Downstream Velocity		Infinity	ft/s
Upstream Velocity		Infinity	ft/s
Normal Depth		0.47	ft
Critical Depth		0.66	ft
Channel Slope		0.05190	ft/ft
Critical Slope		0.00536	ft/ft

LOS VOLCANES STREET CAPACITY

Worksheet for Irregular Section - Full Width Project Description Friction Method Manning Formula Solve For Discharge Input Data Channel Slope 0.02440 ft/ft Normal Depth 0.52 ft Section Definitions Station (ft) Elevation (ft) 0+00 100.67 0+00 100.00 0+02 100.13 0+20 100.48 0+38 100.13 0+40 100.00 0+40 100.67 Roughness Segment Definitions Start Station **Ending Station** Roughness Coefficient (0+00, 100.67) (0+40, 100.67)0.016 **Options** Current Rougnness vveignted Pavlovskii's Method Method Open Channel Weighting Method Pavlovskii's Method Closed Channel Weighting Method Pavlovskii's Method Results 53.41 Ha/s = 26,7Defs Discharge Elevation Range 100.00 to 100.67 ft ≥ Qmax = 8,70 cfs Flow Area 9.66 ft2 Wetted Perimeter 41.05 ft

0.24

40.00 ft

Hydraulic Radius

Top Width

Worksheet for Irregular Section - Full Width

Results			
Normal Depth		0.52	ft
Critical Depth		0.66	ft
Critical Slope		0.00537	ft/ft
Velocity		5.53	ft/s
Velocity Head		0.48	ft
Specific Energy		1.00	ft
Froude Number		1.98	
Flow Type	Supercritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Downstream Velocity	•	Infinity	ft/s
Upstream Velocity		Infinity	ft/s
Normal Depth		0.52	ft
Critical Depth		0.66	ft
Channel Slope		0.02440	ft/ft
Critical Slope		0.00537	ft/ft

DAYTONA STREET CAPACITY

Works	sheet for Irregular S	ection - Full	Width
Project Description			
Friction Method Solve For	Manning Formula Discharge		
Input Data			
Channel Slope Normal Depth Section Definitions		4050 ft/ft 4 0.49 ft	
Station (ft)	Elevation (ft)		
	0+00	100.67	
	0+00	100.00	
	0+02	100.13	
	0+20	100.48	
	0+38	100.13	
	0+40	100.00	
	0+40	100.67	
Roughness Segment Definitions			
Start Station	Ending Station		Roughness Coefficient
(0+00, 1	00.67) (0+40, 100.67)	0.016
Options			
Surrent Roughness Weighted	Pavlovskii's Method		
Method Dpen Channel Weighting Method	Pavlovskii's Method		
Closed Channel Weighting Method	Pavlovskii's Method		
Results			
Discharge	55	5.22 ft³/s	- 2 Section Que 77 LISE
Elevation Range	100.00 to 100.67 ft	-	- 2 Section QCAP= 27.61cf Z Q MAX = 2.87cfs
Flow Area	8	3.46 ft²	= X MAX = C. 101C+2

40.99 ft

0.21 ft

40.00 ft

Wetted Perimeter

Hydraulic Radius

Top Width

Worksheet for Irregular Section - Full Width

Results			
Normal Depth		0.49	ft
Critical Depth		0.67	ft
Critical Slope		0.00534	ft/ft
Velocity		6.53	ft/s
Velocity Head		0.66	ft
Specific Energy		1.15	ft
Froude Number		2.50	
Flow Type	Supercritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Downstream Velocity		Infinity	ft/s
Upstream Velocity		Infinity	ft/s
Normal Depth		0.49	ft
Critical Depth		0.67	ft
Channel Slope		0.04050	ft/ft
Critical Slope		0.00534	ft/ft

LOS VOLCANZS @ DI #14

Worksheet for Irregular Section - Half Width

Project Description

Friction Method

Manning Formula

Solve For

Normal Depth

Input Data

Channel Slope

0.01470 ft/ft

Discharge

8.70 ft3/s = BASINS: C-IDI, C-ZD.Z & LV-5 UNDEU. LV-1 Developed

Section Definitions

Cocion Delinitions

Station (ft) Elevation (ft)

0+00 100.67 0+00 100.00 0+02 100.13 0+20 100.48

Roughness Segment Definitions

Start Station

Ending Station

Roughness Coefficient

(0+00, 100.67)

(0+20, 100.48)

0.016

Options

Current Roughness Weighted

Pavlovskii's Method

Method
Open Channel Weighting Method

Pavlovskii's Method

Closed Channel Weighting Method

Pavlovskii's Method

Results

Normal Depth

0.40 ft 4

Elevation Range

100.00 to 100.67 ft

4

Flow Area Wetted Perimeter 2.63

Hydraulic Radius

16.46 ft

Top Width

Normal Depth

16.05 ft

Normal Depth Critical Depth 0.40 ft

Critical Slope

0.45 ft 4 0.00672 ft/ft

Worksheet for Irregular Section - Half Width				
Results				
Velocity		3.31	ft/s	
Velocity Head		0.17	ft	
Specific Energy		0.57	ft	
Froude Number		1.44		
Flow Type	Supercritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Downstream Velocity		Infinity	ft/s	
Upstream Velocity		Infinity	·ft/s	
Normal Depth	_	0.40	ft	•
Critical Depth	-	0.45	ft	
Channel Slope		0.01470	ft/ft	
Critical Slope		0.00672	ft/ft	

Cross Section for Irregular Section - Half Width

Project Description

Friction Method

Manning Formula

Solve For

Normal Depth

Input Data

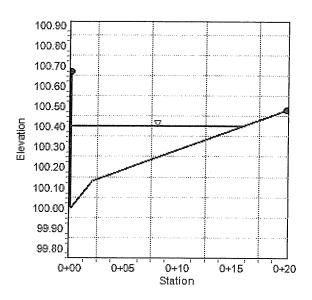
Discharge

Channel Slope Normal Depth 0.01470 ft/ft

0.40 ft

8.70 ft³/s

Cross Section Image



Worksheet for Irregular Section - Half Width

Project Description

Friction Method

Manning Formula

Solve For

Normal Depth

Input Data

Channel Slope

0.01470 ft/ft

Discharge

Section Definitions

3.67 ANS E BASINS: CIDI, C-ZD.Z & LY-5 UNDEL LV-1 DevelopED

LESS FLOW TO INLET #14

Station (ft)

Elevation (ft)

0+00	100.67
0+00	100.00
0+02	100.13
0+20	100.48

Roughness Segment Definitions

Start Station

Ending Station

Roughness Coefficient

(0+00, 100.67)

(0+20, 100.48)

0.016

Options

Current Roughness vveighted

Pavlovskii's Method

Open Channel Weighting Method

Pavlovskii's Method

Closed Channel Weighting Method

Pavlovskii's Method

Results

Normal Depth

Elevation Range

100.00 to 100.67 ft

1.37 11.71

0.31

Flow Area Wetted Perimeter Hydraulic Radius

0.12 ft

Top Width Normal Depth

11.39 ft 0.31

Critical Depth Critical Slope

0.34 0.00753 ft/ft

Worksheet for Irregular Section - Half Width

Results			
Velocity		2.69	ft/s
Velocity Head		0.11	ft
Specific Energy		0.42	ft
Froude Number		1.37	
Flow Type	Supercritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Downstream Velocity		Infinity	ft/s
Upstream Velocity		Infinity	ft/s
Normal Depth		0.31	ft
Critical Depth		0.34	ft
Channel Slope		0.01470	ft/ft
Critical Slope		0.00753	ft/ft

Worksheet for Irregular Section - Half Width

Project Description

Friction Method

Manning Formula

Solve For

Normal Depth

Input Data

Channel Slope

0.01570 ft/ft

Discharge

2.87 ft3/s = D-18 Developes

Section Definitions

Station (ft)

Elevation (ft)

0+00 100.67 0+00 100.00 0+02 100.13 0+20 100.48

Roughness Segment Definitions

Start Station

Ending Station

Roughness Coefficient

(0+00, 100.67)

(0+20, 100.48)

0.016

Options

Current Rougnness vveighted

Method

Pavlovskii's Method

Open Channel Weighting Method

Pavlovskii's Method

Closed Channel Weighting Method

Pavlovskii's Method

Results

Normal Depth	
Elevation Range	

100.00 to 100.67 ft



Flow Area Wetted Perimeter

1.10 ft²

Wetted Perimeter Hydraulic Radius 10.45 ft

0.29

Top Width
Normal Depth

10.16 ft

Normal Depth Critical Depth 0.29 ft 0.32 ft **◄**—

Critical Slope

0.00778 ft/ft

Worksheet for Irregular Section - Half Width 2.60 ft/s 0.11 ft 0.39 ft 1.39 Supercritical 0.00 ft 0.00 ft

GVF Output Data

Results Velocity

Velocity Head

Specific Energy

Froude Number

GVF Input Data

Downstream Depth

Number Of Steps

Flow Type

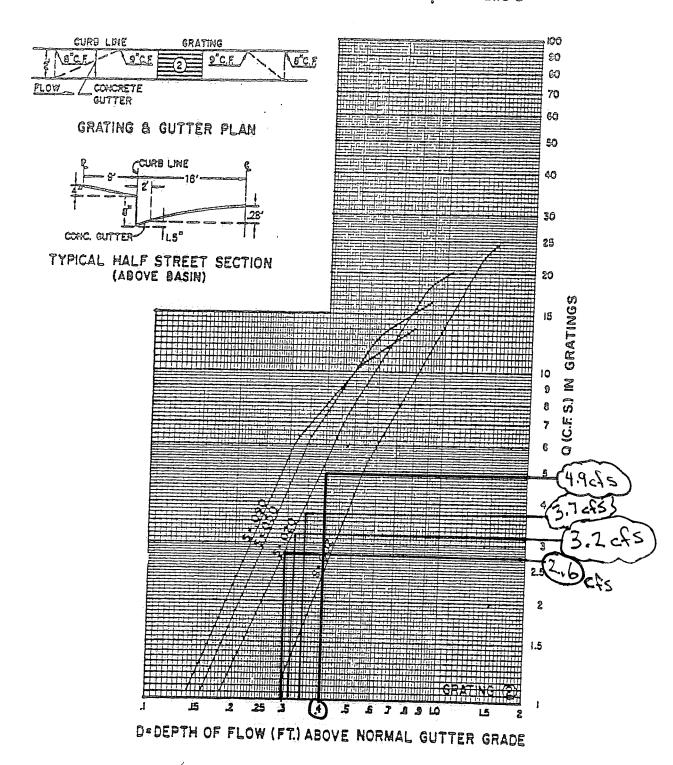
Length

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.29	ft
Critical Depth	0.32	ft
Channel Slope	0.01570	ft/ft
Critical Slope	0.00778	ft/ft

	Project FEDEX GROUND ALF	Date
	Project No. No. CAPACITY Meeting Purpose Attendees	Sheet Noof
TIERRA WEST, L	<u>LC</u>	
LESS BEARING	PER COASTA DW9 #2220,5 RATE = {25,11/12}(40,11/12) = BARS = (0.5,11/12)(3,33 ft)	6.945f
	GEATE AREA OPENING 50%	OPEN ARRA = 4,695A Closerus FACTOR = 2,355A
OK, FACE EQUATION:	SEGRATE AREA OPENING FOR DO	UBL2 6 11N/EL = 7170 S+
C=0.67 9=32.2 Ft/sec ² A = 2.35 Pt ² (20	GDATEC = 41705+	
h = he gat of w		
BASIN A-Z AREA = 2.91 AC Q. N = 11.14 CSC	< 0 = 17.87 cf.	

Chapter 22 - Drainage, Flood Control and Erosion Control

GRATING CAPACITIES FOR TYPE "A" , "C" and "D"



FEDEX GROUND ABOL LOS VOLCAMES RD. SLOPE = 1.47%

PLATE 22.3 D-5

VOLUME CALCULATIONS

Pond 5 - Proposed Conditions

ACTUAL	DEPTH	VOLUME	Q
ELEV.	(FT)	(AC-FT)	(CFS)
59.00	0	0	0.000
60.00	1.00	0.2646	2.745
65.00	6.00	2.1906	8.002
70.00	11.00	5.2846	10.979
70.50	11.50	5.6666	11.233

Emergency Overflow

Orifice Equation

Q = CA SQRT(2gH)

C =

0.6

Diameter (in)

8 Two Each

Area (ft^2)= 0.34906585

g =

32.2

H(Ft) =

Depth of water above center of orifice

Q(CFS) = Flow

FedEx Ground, Albuquerque

Pond #5 Detention Pond Volume Calculation

Elev	Area	Elev	Avg			
		Change	Area	Volume	Cumulative	Volume
	SF	FT	SF	CU.FT.	CU.FT.	ACRE-FT
5159	10648					
5160	12400	1	11524	11524	11524	0.264555
5165	21160	5	16780	83900	95424	2.190634
5170	32750	5	26955	134775	230199	5.284642
5170.5	33800	0.5	33275	16637.5	246836.5	5.666586

```
hymo .txt
   ***********************
             FEDEX GROUND ALBUQUERQUE, NM
  ***********************
  * 100-YEAR, 24-HR STORM (UNDER PROPOSED CONDITIONS) W/ routing * *****************************
  START
                      TIME=0.0
  ⊹
  RAINFALL
                      TYPE=2 RAIN QUARTER=0.0 IN
                      RAIN ONE=1.87 IN RAIN SIX=2.20 IN
                      RAIN DAY=2.66 IN DT=0.05 HR
  *DEVELOPED CONDITIONS
  *BASIN A1
  COMPUTE NM HYD
                      ID=1 HYD NO=100.1 AREA=0.00070 SQ MI
                      PER A=0.00 PER B=0.00 PER C=100.0 PER D=0.00
                     TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD
                     ID=1 CODE=1
 *BASIN A2
 COMPUTE NM HYD
                     ID=2 HYD NO=100.2 AREA=0.00363 SQ MI
                     PER A=0.00 PER B=0.00 PER C=25.0 PER D=75.00
                     TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD
                     ID=2 CODE=1
 *BASIN A3
 COMPUTE NM HYD
                     ID=3 HYD NO=100.3 AREA=0.00126 SQ MI
                     PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00
                     TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD
                     ID=3 CODE=1
 *
 *BASIN A4
 COMPUTE NM HYD
                    ID=4 HYD NO=100.4 AREA=0.00389 SO MI
                    PER A=0.00 PER B=0.00 PER C=25.0 PER D=75.00
                    TP=-0.1333 HR MASS RAINFALL=-1
PRINT HYD
                    ID=4 CODE=1
*BASIN A5
COMPUTE NM HYD
                    ID=5 HYD NO=100.5 AREA=0.00165 SQ MI
                    PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00
                    TP=-0.1333 HR MASS RAINFALL=-1
PRINT HYD
                    ID=5 CODE=1
*BASIN A6
COMPUTE NM HYD
                    ID=6 HYD NO=100.6 AREA=0.00082 SQ MI
                    PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00
                    TP=-0.1333 HR MASS RAINFALL=-1
PRINT HYD
                    ID=6 CODE=1
*BASIN A7
COMPUTE NM HYD
                   ID=7 HYD NO=100.7 AREA=0.00082 SQ MI
                   PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00
                   TP=-0.1333 HR MASS RAINFALL=-1
                                      Page 1
```

```
hymo .txt
 COMPUTE NM HYD
                        ID=16 HYD NO=100.16 AREA=0.00239 SQ MI
                         PER A=0.00 PER B=0.00 PER C=100.0 PER D=0.00
                        TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD
                        ID=16 CODE=1
 *
 ADD HYD
                        ID=50 HYD NO=100.5 ID=1 ID=2
 ADD HYD
                        ID=50 HYD NO=100.6 ID=50 ID=3
 ADD HYD
                        ID=50 HYD NO=100.8 ID=50 ID=4
 ADD HYD
                        ID=50 HYD NO=100.9 ID=50 ID=5
 ADD HYD
                        ID=50 HYD NO=100.10 ID=50 ID=6
 ADD HYD
                        ID=50 HYD NO=100.11 ID=50 ID=7
                       ID=50 HYD NO=100.12 ID=50 ID=8
ID=50 HYD NO=100.13 ID=50 ID=9
ID=50 HYD NO=100.14 ID=50 ID=10
ID=50 HYD NO=100.15 ID=50 ID=11
 ADD HYD
 ADD HYD
 ADD HYD
 ADD HYD
 ADD HYD
                       ID=50 HYD NO=100.16 ID=50 ID=12
ADD HYD
                       ID=50 HYD NO=100.17 ID=50 ID=13
ADD HYD
                       ID=50 HYD NO=100.18 ID=50 ID=14
ADD HYD
                       ID=50 HYD NO=100.19 ID=50 ID=15
ADD HYD
                       ID=50 HYD NO=100.20 ID=50 ID=16
PRINT HYD
                       ID=50 CODE=1
*ROUTE THROUGH DETENTION POND NO 1
ROUTE RESERVOIR
                       ID=55 HYD NO=200.1 INFLOW ID=50 CODE=24
                       OUTFLOW (CFS) STORAGE(AC-FT) ELEVATION(FT)
                       0.0
                                        0.0
                                                              59.00
                       2.745
                                        0.2646
                                                              60.00
                       8.002
                                        2.1906
                                                              65.00
                       10.979
                                        5.2846
                                                              70.00
                       11.233
                                        5.6666
                                                             70.50
PRINT HYD
                      ID=55 CODE=1
*
FINISH
```

```
hymo .txt
  ******************
            FEDEX GROUND ALBUQUERQUE, NM
  **********************
  ^{*} 100-YEAR, 24-HR STORM (UNDER PROPOSED CONDITIONS) W/ routing ^{*}
  *******************
  START
                     TIME=0.0
  ⊹
                     TYPE=2 RAIN QUARTER=0.0 IN
  RAINFALL
                     RAIN ONE=1.87 IN RAIN SIX=2.20 IN
                     RAIN DAY=2.66 IN DT=0.05 HR
  *DEVELOPED CONDITIONS
  *BASIN A1
 COMPUTE NM HYD
                     ID=1 HYD NO=100.1 AREA=0.00070 SQ MI
                    PER A=0.00 PER B=0.00 PER C=100.0 PER D=0.00
                    TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD
                    ID=1 CODE=1
 *BASIN A2
 COMPUTE NM HYD
                    ID=2 HYD NO=100.2 AREA=0.00363 SO MI
                    PER A=0.00 PER B=0.00 PER C=25.0 PER D=75.00
                    TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD
                    ID=2 CODE=1
 *BASIN A3
 COMPUTE NM HYD
                    ID=3 HYD NO=100.3 AREA=0.00126 SQ MI
                    PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00
                    TP=-0.1333 HR MASS RAINFALL=-1
                    ID=3 CODE=1
 PRINT HYD
 六
 *BASIN A4
                   ID=4 HYD NO=100.4 AREA=0.00389 SQ MI
 COMPUTE NM HYD
                   PER A=0.00 PER B=0.00 PER C=25.0 PER D=75.00
                   TP=-0.1333 HR MASS RAINFALL=-1
PRINT HYD
                   ID=4 CODE=1
*BASIN A5
COMPUTE NM HYD
                   ID=5 HYD NO=100.5 AREA=0.00165 SQ MI
                   PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00
                   TP=-0.1333 HR MASS RAINFALL=-1
PRINT HYD
                   ID=5 CODE=1
*BASIN A6
                   ID=6 HYD NO=100.6 AREA=0.00082 SQ MI
COMPUTE NM HYD
                   PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00
                   TP=-0.1333 HR MASS RAINFALL=-1
                   ID=6 CODE=1
PRINT HYD
*BASIN A7
COMPUTE NM HYD
                   ID=7 HYD NO=100.7 AREA=0.00082 SQ MI
                   PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00
                  TP=-0.1333 HR MASS RAINFALL=-1
                                    Page 1
```

*

hymo .txt PRINT HYD ID=7 CODE=1 *BASIN A8 COMPUTE NM HYD ID=8 HYD NO=100.8 AREA=0.00082 SQ MI PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00 TP=-0.1333 HR MASS RAINFALL=-1 PRINT HYD ID=8 CODE=1 *BASIN A9 ID=9 HYD NO=100.9 AREA=0.00075 SQ MI COMPUTE NM HYD PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00 TP=-0.1333 HR MASS RAINFALL=-1 PRINT HYD ID=9 CODE=1 *BASIN A10 COMPUTE NM HYD ID=10 HYD NO=100.10 AREA=0.00224 SQ MI PER A=0.00 PER B=0.00 PER C=10.0 PER D=90.00 TP=-0.1333 HR MASS RAINFALL=-1 ID=10 CODE=1 PRINT HYD *BASIN All COMPUTE NM HYD ID=11 HYD NO=100.11 AREA=0.00433 SQ MI PER A=0.00 PER B=0.00 PER C=25.0 PER D=75.00 TP=-0.1333 HR MASS RAINFALL=-1 PRINT HYD ID=11 CODE=1 *BASIN A12 ID=12 HYD NO=100.12 AREA=0.00241 SQ MI COMPUTE NM HYD PER A=0.00 PER B=0.00 PER C=90.0 PER D=10.00 TP=-0.1333 HR MASS RAINFALL=-1 PRINT HYD ID=12 CODE=1 *BASIN A13 COMPUTE NM HYD ID=13 HYD NO=100.13 AREA=0.00110 SQ MI PER A=0.00 PER B=0.00 PER C=25.0 PER D=75.00 TP=-0.1333 HR MASS RAINFALL=-1 ID=13 CODE=1 PRINT HYD *BASIN A14 COMPUTE NM HYD ID=14 HYD NO=100.14 AREA=0.00065 SQ MI PER A=0.00 PER B=0.00 PER C=100.0 PER D=0.00 TP=-0.1333 HR MASS RAINFALL=-1 ID=14 CODE=1 PRINT HYD *BASIN A15 COMPUTE NM HYD ID=15 HYD NO=100.15 AREA=0.00700 SQ MI PER A=0.00 PER B=0.00 PER C=30.0 PER D=70.00 TP=-0.1333 HR MASS RAINFALL=-1 PRINT HYD ID=15 CODE=1

*BASIN P5

```
hymo .txt
 COMPUTE NM HYD
                       ID=16 HYD NO=100.16 AREA=0.00239 SQ MI
                       PER A=0.00 PER B=0.00 PER C=100.0 PER D=0.00
                       TP=-0.1333 HR MASS RAINFALL=-1
 PRINT HYD
                       ID=16 CODE=1
 *
 ADD HYD
                       ID=50 HYD NO=100.5 ID=1 ID=2
 ADD HYD
                      ID=50 HYD NO=100.6 ID=50 ID=3
 ADD HYD
                      ID=50 HYD NO=100.8 ID=50 ID=4
 ADD HYD
                      ID=50 HYD NO=100.9 ID=50 ID=5
                      ID=50 HYD NO=100.10 ID=50 ID=6 ID=50 HYD NO=100.11 ID=50 ID=7
 ADD HYD
 ADD HYD
 ADD HYD
                      ID=50 HYD NO=100.12 ID=50 ID=8
 ADD HYD
                      ID=50 HYD NO=100.13 ID=50 ID=9
ADD HYD
                      ID=50 HYD NO=100.14 ID=50 ID=10
ADD HYD
                      ID=50 HYD NO=100.15 ID=50 ID=11
ADD HYD
                      ID=50 HYD NO=100.16 ID=50 ID=12
ADD HYD
                      ID=50 HYD NO=100.17 ID=50 ID=13
ADD HYD
                      ID=50 HYD NO=100.18 ID=50 ID=14
                      ID=50 HYD NO=100.19 ID=50 ID=15
ADD HYD
ADD HYD
                      ID=50 HYD NO=100.20 ID=50 ID=16
PRINT HYD
                      ID=50 CODE=1
*ROUTE THROUGH DETENTION POND NO 1
ROUTE RESERVOIR
                     ID=55 HYD NO=200.1 INFLOW ID=50 CODE=24
                     OUTFLOW (CFS) STORAGE(AC-FT) ELEVATION(FT)
                     0.0
                                     0.0
                                                          59.00
                     2.745
                                     0.2646
                                                          60.00
                     8.002
                                     2.1906
                                                          65.00
                     10.979
                                     5.2846
                                                          70.00
                     11.233
                                     5.6666
                                                          70.50
PRINT HYD
                     ID=55 CODE=1
FINISH
```

				ages.
-				

AHYMO PROGRAM (AHYMO-S4)

```
- Version: S4.01a - Rel: 01a
               RUN DATE (MON/DAY/YR) = 06/25/2014
               START TIME (HR:MIN:SEC) = 15:34:11
                                                        USER NO.=
 AHYMO_Temp_User:20122010
               INPUT FILE = C:\Users\vince.TWLLC\Desktop\hymo .txt
     *******************
     * 100-YEAR, 24-HR STORM (UNDER PROPOSED CONDITIONS) W/ routing * *****************************
    START
                          TIME=0.0
    RAINFALL
                          TYPE=2 RAIN QUARTER=0.0 IN
                         RAIN ONE=1.87 IN RAIN SIX=2.20 IN RAIN DAY=2.66 IN DT=0.05 HR
                    24-HOUR RAINFALL DIST. - BASED ON NOAA ATLAS 14 FOR CONVECTIVE
AREAS (NM & AZ) - D1
                           0.050000 HOURS
                    DT =
                                                  END TIME =
                                                                 24.000002 HOURS
                      0.0000
                              0.0022
                                       0.0045
                                               0.0069
                                                        0.0096
                                                                0.0123
                                                                         0.0154
                      0.0197
                              0.0264
                                       0.0336
                                               0.0412
                                                        0.0494
                                                                 0.0578
                                                                         0.0664
                              0.0844
                      0.0753
                                       0.0946
                                               0.1052
                                                        0.1168
                                                                0.1387
                                                                         0.1657
                      0.2020
                              0.2430
                                       0.2937
                                               0.3614
                                                        0.4375
                                                                0.5689
                                                                         0.7733
                      1.1234
                              1.3695
                                       1.5635
                                               1.6610
                                                        1.7465
                                                                1.8079
                                                                         1.8568
                      1.8994
                              1.9306
                                       1.9592
                                               1.9828
                                                        1.9979
                                                                2.0087
                                                                         2.0183
                              2.0352
                      2.0273
                                       2.0426
                                               2.0499
                                                        2.0568
                                                                2.0625
                                                                         2.0659
                                       2.0754
                      2.0692
                              2.0724
                                               2.0784
                                                        2.0813
                                                                2.0842
                                                                         2.0870
                      2.0896
                              2.0923
                                               2.0974
                                       2.0949
                                                        2.0999
                                                                2.1023
                                                                         2.1046
                      2.1069
                              2.1092
                                      2.1115
                                               2.1136
                                                        2.1158
                                                                2.1179
                                                                         2.1199
                      2.1220
                              2.1240
                                      2.1260
                                               2.1280
                                                       2.1299
                                                                2.1318
                                                                         2.1337
                      2.1356
                              2.1374
                                      2.1392
                                                                2.1446
                                               2.1411
                                                       2.1428
                                                                        2.1463
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                              2.1498
2.1612
                                      2.1514
                                               2.1531
                                                       2.1548
                                                                2.1564
                                                                        2.1580
                     2.1596
                                               2.1643
                                                       2.1658
                                       2.1628
                                                                2.1674
                                                                        2.1689
                     2.1704
                              2.1718
                                      2.1733
                                                       2.1762
2.1859
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2.1845
                                                                2.1776
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                              2.1818
                                      2.1832
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                     2.1899
                              2.1912
                                      2.1925
                                               2.1937
                                                       2.1950
                                                                2.1963
                                                                        2.1975
                     2.1988
                              2.2000
                                      2.2013
                                                       2.2038
                                               2.2026
                                                                2.2051
                                                                        2.2064
                     2.2077
                              2.2089
                                      2.2102
                                               2.2115
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                                                                2.2141
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                                      2.2192
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                                               2.2294
                                                                        2.2332
                     2.2345
                              2.2358
                                      2.2371
                                               2.2383
                                                       2.2396
                                                               2.2409
                                                                        2.2422
                     2.2434
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                                      2.2460
                                                       2.2486
                                               2.2473
                                                               2.2498
                                                                        2.2511
                     2.2524
                              2.2537
                                              2.2562
                                      2.2549
                                                       2.2575
                                                               2.2588
                                                                        2.2601
                     2.2613
                             2.2626
                                      2.2639
                                                       2.2664
                                               2.2652
                                                                2.2677
                                                                        2.2690
                     2.2703
                             2.2716
                                      2.2728
                                               2.2741
                                                       2.2754
                                                               2..2767
                                                                        2.2779
                             2.2805
                     2.2792
                                      2.2818
                                              2.2831
                                                       2.2843
                                                                2.2856
                                                                        2.2869
                     2.2882
                             2.2894
                                      2.2907
                                              2.2920
                                                       2.2933
                                                               2.2946
                                                                        2.2958
                     2.2971
                             2.2984
                                      2.2997
                                              2.3009
                                                       2.3022
                                                               2.3035
                                                                        2.3048
                     2.3061
                             2.3073
                                      2.3086
                                              2.3099
                                                       2.3112
                                                               2.3124
                                                                        2.3137
                     2.3150
                             2.3163
                                      2.3176
                                                               2.3214
                                              2.3188
                                                       2.3201
                                                                        2.3227
                    2.3239
                             2.3252
                                      2.3265
                                              2.3278
                                                       2.3291
                                                               2.3303
                                                                        2.3316
                    2.3329
                             2.3342
2.3431
                                      2.3354
                                              2.3367
                                                       2.3380
                                                               2.3393
                                                                        2.3406
                    2.3418
                                      2.3444
                                              2.3457
                                                       2.3469
                                                               2.3482
                                                                        2.3495
                    2.3508
                             2.3521
                                     2.3533
                                              2.3546
                                                       2.3559
                                                               2.3572
                                                                        2.3584
                    2.3597
                             2.3610
                                     2.3623
                                              2.3636
                                                       2.3648
                                                               2.3661
                                                                        2.3674
                    2.3687
                             2.3699
                                     2.3712
                                              2.3725
                                                      2.3738
                                                               2.3750
                                                                       2.3763
                    2.3776
                             2.3789
                                     2.3802
                                              2.3814
                                                      2.3827
                                                               2.3840
                                                                       2.3853
                    2.3865
                             2.3878
                                     2.3891
                                              2.3904
                                                      2.3917
                                                                       2.3942
                                                               2.3929
                                       Page 1
```

```
AHYMO.OUT
                  2.3980 2.3993 2.4006 2.4019 2.4032 2.4070 2.4083 2.4095 2.4108 2.4121 2.4150 2.4172 2.4185 2.4188 2.4121
 2.3955
          2.3968
 2.4044
          2.4057
                           2.4172
                                     2.4185
                                              2.4198
 2.4134
          2.4147
                   2.4159
                                                       2.4210
 2.4223
          2.4236
                   2.4249
                                     2.4274
2.4364
                            2.4262
                                              2.4287
                                                        2.4300
 2.4313
          2.4325
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                                                        2.4389
 2.4402
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                                     2.4543
                                              2.4555
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         2.4594
                   2.4607
                            2.4619
                                     2.4632
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                                               2.4645
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          2.4683
                  2.4696
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                                               2.4734
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         2.4952
                            2.4977
                                     2.4990
                                              2.5003
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                            2.5067
                                     2.5079
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         2.5399
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                                                        2.5463
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                  2.5501
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2.5565
         2.5578
                  2.5590
                           2.5603
                                     2.5616
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                                     2.5884
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2.6102
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                  2.6127
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                                                       2.6178
2.6191
        2.6204
                                     2.6242
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                            2.6229
                                              2.6255
                                                       2.6268
2.6280
        2.6293
                  2.6306
                           2.6319
                                     2.6332
                                              2.6344
                                                       2.6357
2.6370
        2.6383
                 2.6395
                           2.6408
                                     2.6421
                                              2.6434
                                                       2.6447
2.6459 2.6472 2.6485 2.6498 2.6510
2.6549 2.6562 2.6574 2.6587 2.6600
2.6459
                                    2.6510
                                             2.6523
                                                      2.6536
```

*DEVELOPED CONDITIONS

*

*BASIN A1

COMPUTE NM HYD

ID=1 HYD NO=100.1 AREA=0.00070 SQ MI PER A=0.00 PER B=0.00 PER C=100.0 PER D=0.00 TP=-0.1333 HR MASS RAINFALL=-1

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 100.10

RUNOFF VOLUME = 1.08591 INCHES = 0.0405 ACRE-FEET PEAK DISCHARGE RATE = 1.41 CFS AT 1.500 HOURS BASIN AREA = 0.0007 SQ. MI.

*BASIN A2

COMPUTE NM HYD ID=2 HYD NO=100.2 AREA=0.00363 SQ MI Page 2

AHYMO.OUT PER A=0.00 PER B=0.00 PER C=25.0 PER D=75.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.105867HR TP = 0.133300HR CONSTANT, N = 4.514593K/TP RATIO = 0.794199SHAPE UNIT PEAK = 2.6424CFS UNIT VOLUME = 0.9970B = 388.14 P60 = 1.87000.000908 SQ MI AREA = IA = 0.35000 INCHESINF = 0.83000INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD

ID=2 CODE=1

PARTIAL HYDROGRAPH 100.20

RUNOFF VOLUME = 2.08322 INCHES = 0.4033 ACRE-FEET PEAK DISCHARGE RATE = 9.63 CFS AT 1.500 HOURS BASIN AREA = 0.0036 SQ. MI.

* *BASIN A3

COMPUTE NM HYD

ID=3 HYD NO=100.3 AREA=0.00126 SQ MI PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00 TP=-0.1333 HR MASS RAINFALL=-1

PRINT HYD

ID=3 CODE=1

PARTIAL HYDROGRAPH 100.30

RUNOFF VOLUME = 2.41566 INCHES = 0.1623 ACRE-FEET PEAK DISCHARGE RATE = 3.61 CFS AT 1.500 HOURS BASIN AREA = 0.0013 SQ. MI.

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*BASIN A4

COMPUTE NM HYD

ID=4 HYD NO=100.4 AREA=0.00389 SQ MI PER A=0.00 PER B=0.00 PER C=25.0 PER D=75.00 TP=-0.1333 HR MASS RAINFALL=-1

CONSTANT, N = 4.514593 UNIT PEAK = 2.8317 CFS UNIT VOLUME = 0.9977 B = 388.14 P60 = 1.8700 AREA = 0.000973 SQ MI IA = 0.35000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=4 CODE=1

PARTIAL HYDROGRAPH 100.40

RUNOFF VOLUME = 2.08322 INCHES = 0.4322 ACRE-FEET PEAK DISCHARGE RATE = 10.32 CFS AT 1.500 HOURS BASIN AREA = 0.0039 SQ. MI.

* *BASIN A5

K = 0.072649HRTP = 0.133300HRK/TP RATIO = 0.545000SHAPE CONSTANT, N = 7.106428UNIT PEAK = 6.5143 CFS UNIT VOLUME = 0.9975 B = 526.28 P60 = 1.87000.001650 SQ MI AREA = IA = 0.10000 INCHESINF = 0.04000INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=5 CODE=1

PARTIAL HYDROGRAPH 100.50

RUNOFF VOLUME = 2.41566 INCHES = 0.2126 ACRE-FEET PEAK DISCHARGE RATE = 4.73 CFS AT 1.500 HOURS BASIN AREA = 0.0017 SQ. MI.

*

*BASIN A6

COMPUTE NM HYD

ID=6 HYD NO=100.6 AREA=0.00082 SQ MI PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649 HR TP = 0.133300 HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428

UNIT PEAK = 3.2374 CFS UNIT VOLUME = 0.9959 P60 = 1.8700

B = 526.28

AREA =

AREA = 0.000820 SQ MI

IA = 0.10000 INCHES

INF = 0.04000

INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD

ID=6 CODE=1

PARTIAL HYDROGRAPH 100.60

RUNOFF VOLUME = 2.41566 INCHES = 0.1056 ACRE-FEET PEAK DISCHARGE RATE = 2.35 CFS AT 1.500 HOURS BASIN AREA = 0.0008 SQ. MI.

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*

*BASIN A7

COMPUTE NM HYD

ID=7 HYD NO=100.7 AREA=0.00082 SQ MI PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HRTP = 0.133300HRK/TP RATIO = 0.545000SHAPE CONSTANT, N = 7.106428UNIT PEAK = 3.2374 CFS UNIT VOLUME = 0.9959 526,28 P60 = 1.87000.000820 SQ MI IA = 0.10000 INCHESAREA = INF = 0.04000INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD

ID=7 CODE=1

PARTIAL HYDROGRAPH 100.70

RUNOFF VOLUME = 2.41566 INCHES = 0.1056 ACRE-FEET PEAK DISCHARGE RATE = 2.35 CFS AT 1.500 HOURS BASIN AREA = 0.0008 SQ. MI.

* *BASIN A8

COMPUTE NM HYD

ID=8 HYD NO=100.8 AREA=0.00082 SQ MI PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649 HR TP = 0.133300 HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428

AHYMO, OUT

UNIT PEAK = 3.2374CFS UNIT VOLUME = 0.9959B = 526.28

P60 = 1.8700

AREA =0.000820 SQ MI IA = 0.10000 INCHESINF = 0.04000

INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD

ID=8 CODE=1

PARTIAL HYDROGRAPH 100.80

RUNOFF VOLUME = 2.41566 INCHES 0.1056 ACRE-FEET PEAK DISCHARGE RATE = 2.35 CFS AT 1.500 HOURS BASIN AREA = 0.0008 SQ. MI.

*BASIN A9

COMPUTE NM HYD

ID=9 HYD NO=100.9 AREA=0.00075 SO MI PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HRTP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428UNIT PEAK = 2.9610 CFS UNIT VOLUME = 0.9959 B = 526.28 P60 = 1.8700

AREA =0.000750 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD

ID=9 CODE=1

PARTIAL HYDROGRAPH 100.90

RUNOFF VOLUME = 2.41566 INCHES = PEAK DISCHARGE RATE = 2.15 CFS AT 0.0966 ACRE-FEET 1.500 HOURS BASIN AREA = 0.0008 SQ. MI.

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*BASIN A10

ID=10 HYD NO=100.10 AREA=0.00224 SO MI COMPUTE NM HYD PER A=0.00 PER B=0.00 PER C=10.0 PER D=90.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HRK/TP RATIO = 0.545000SHAPE CONSTANT, N = 7.1064287.9593 CFS UNIT VOLUME = UNIT PEAK = 0.9978 B = 526.28

P60 = 1.87000.002016 SQ MI

IA = 0.10000 INCHESINF = 0.04000

AREA =INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.105867HR TP = 0.133300HR K/TP RATIO = 0.794199 SHAPE CONSTANT, N = 4.514592

UNIT PEAK = 0.65223 CFS UNIT VOLUME = 0.9821 B = 388.14

P60 = 1.8700

 $AREA = 0.000224 \text{ SQ MI} \quad IA = 0.35000 \text{ INCHES} \quad INF = 0.83000$

INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =

PRINT HYD

ID=10 CODE=1

PARTIAL HYDROGRAPH 100.10

RUNOFF VOLUME = 2.28268 INCHES = 0.2727 ACRE-FEET PEAK DISCHARGE RATE = 6.24 CFS AT 1.500 HOURS BASIN AREA = 0.0022 SQ. MI.

*

*BASIN A11

COMPUTE NM HYD

ID=11 HYD NO=100.11 AREA=0.00433 SQ MI PER A=0.00 PER B=0.00 PER C=25.0 PER D=75.00 TP=-0.1333 HR MASS RAINFALL=-1

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.105867HR TP = 0.133300HR K/TP RATIO = 0.794199 SHAPE CONSTANT, N = 4.514593 UNIT PEAK = 3.1520 CFS UNIT VOLUME = 0.9977 B = 388.14 PEAK = 0.001083 SQ MI IA = 0.35000 INCHES INF = 0.83000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =

0.050000

PRINT HYD

ID=11 CODE=1

PARTIAL HYDROGRAPH 100.11

RUNOFF VOLUME = 2.08322 INCHES = 0.4811 ACRE-FEET PEAK DISCHARGE RATE = 11.49 CFS AT 1.500 HOURS BASIN AREA = 0.0043 SQ. MI.

*BASIN A12

COMPUTE NM HYD

ID=12 HYD NO=100.12 AREA=0.00241 SQ MI PER A=0.00 PER B=0.00 PER C=90.0 PER D=10.00 TP=-0.1333 HR MASS RAINFALL=-1 Page 7

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428UNIT PEAK = 0.95148CFS UNIT VOLUME = 0.9891 526.28 P60 = 1.8700AREA = 0.000241 SQ MI 0.10000 INCHES IA =INF = 0.04000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.105867HRTP = 0.133300HRK/TP RATIO = 0.794199SHAPE CONSTANT, N = 4.514593UNIT PEAK = 6.3156 CFS UNIT VOLUME = 0.9999B = 388.14 P60 = 1.87000.002169 SQ MI 0.35000 INCHES AREA =IA =INF = 0.83000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD

ID=12 CODE=1

PARTIAL HYDROGRAPH 100.12

RUNOFF VOLUME = 1.21889 INCHES = 0.1567 ACRE-FEET PEAK DISCHARGE RATE = 5.06 CFS AT 1.500 HOURS BASIN AREA = 0.0024 SQ. MI.

*

*BASIN A13

COMPUTE NM HYD

ID=13 HYD NO=100.13 AREA=0.00110 SQ MI PER A=0.00 PER B=0.00 PER C=25.0 PER D=75.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HRTP = 0.133300HRK/TP RATIO = 0.545000SHAPE CONSTANT, N = 7.106428UNIT PEAK = 3.2571CFS UNIT VOLUME = 0.9959 B =526.28 P60 = 1.8700IA = 0.10000 INCHESAREA = 0.000825 SQ MI INF = INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.105867HRTP = 0.133300HRK/TP RATIO = 0.794199CONSTANT, N = 4.514593UNIT PEAK = 0.80073 CFS UNIT VOLUME = 0.9874 R = 388.14 P60 = 1.8700AREA = 0.000275 SQ MI IA = 0.35000 INCHESINF = INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=13 CODE=1

PARTIAL HYDROGRAPH 100.13

RUNOFF VOLUME = 2.08322 INCHES = 0.1222 ACRE-FEET PEAK DISCHARGE RATE = 2.93 CFS AT 1.500 HOURS BASIN AREA = 0.0011 SQ. MI.

* *BASIN A14

COMPUTE NM HYD

ID=14 HYD NO=100.14 AREA=0.00065 SQ MI PER A=0.00 PER B=0.00 PER C=100.0 PER D=0.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.105867HRTP = 0.133300HRK/TP RATIO = 0.794199SHAPE CONSTANT, N = 4.514592UNIT PEAK = 1.8926 CFS UNIT VOLUME = 0.9952388.14 P60 = 1.87000.000650 SQ MI AREA = IA = 0.35000 INCHESINF = 0.83000INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=14 CODE=1

PARTIAL HYDROGRAPH 100.14

RUNOFF VOLUME = 1.08591 INCHES = 0.0376 ACRE-FEET PEAK DISCHARGE RATE = 1.31 CFS AT 1.500 HOURS BASIN AREA = 0.0007 SQ. MI.

*
*BASIN A15

COMPUTE NM HYD

ID=15 HYD NO=100.15 AREA=0.00700 SQ MI PER A=0.00 PER B=0.00 PER C=30.0 PER D=70.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HRTP = 0.133300HRK/TP RATIO = 0.545000SHAPE CONSTANT, N = 7.106428UNIT PEAK = 19.345 CFS UNIT VOLUME = 0.9986 526,28 P60 = 1.8700AREA = 0.004900 SQ MI IA =0.10000 INCHES INF = 0.04000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.105867HRTP = 0.133300HRK/TP RATIO = 0.794199SHAPE CONSTANT, N = 4.514592UNIT PEAK = 6.1147CFS UNIT VOLUME = 0.9999388.14 P60 = 1.8700AREA = 0.002100 SQ MI IA = 0.35000 INCHESINF = 0.83000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =0.050000

PRINT HYD ID=15 CODE=1

PARTIAL HYDROGRAPH 100.15

RUNOFF VOLUME = 2.01673 INCHES = 0.7529 ACRE-FEET PEAK DISCHARGE RATE = 18.26 CFS AT 1.500 HOURS BASIN AREA = 0.0070 SQ. MI.

*

*BASIN P5

COMPUTE NM HYD

ID=16 HYD NO=100.16 AREA=0.00239 SQ MI PER A=0.00 PER B=0.00 PER C=100.0 PER D=0.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.105867HR TP = 0.133300HR K/TP RATIO = 0.794199 SHAPE CONSTANT, N = 4.514592 UNIT PEAK = 6.9591 CFS UNIT VOLUME = 0.9999 B = 388.14 P60 = 1.8700

AREA = 0.002390 SQ MI IA = 0.35000 INCHES INF = 0.83000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ARSTRACTION/INETLIBRATION NUMBER METHOD. DE

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD

ID=16 CODE=1

PARTIAL HYDROGRAPH 100.16

RUNOFF VOLUME = 1.08591 INCHES = 0.1384 ACRE-FEET PEAK DISCHARGE RATE = 4.81 CFS AT 1.500 HOURS BASIN AREA = 0.0024 SQ. MI.

* ADD HYD ID=50 HYD NO=100.5 ID=1 ID=2 ADD HYD ID=50 HYD NO=100.6 ID=50 ID=3 ID=50 HYD NO=100.8 ID=50 ID=4 ADD HYD ADD HYD ID=50 HYD NO=100.9 ID=50 ID=5 ADD HYD ID=50 HYD NO=100.10 ID=50 ID=6 ADD HYD ID=50 HYD NO=100.11 ID=50 TD=7 ADD HYD ID=50 HYD NO=100.12 ID=50 ID=8 ID=50 HYD NO=100.13 ID=50 ID=9 ADD HYD ADD HYD ID=50 HYD NO=100.14 ID=50 ID=10 ADD HYD ID=50 HYD NO=100.15 ID=50 ID=11 ID=50 HYD NO=100.16 ID=50 ID=12 ADD HYD ADD HYD ID=50 HYD NO=100.17 ID=50 TD=13 ADD HYD ID=50 HYD NO=100.18 ID=50 ID=14

Page 10

AHYMO.OUT ADD HYD

ID=50 HYD NO=100.19 ID=50 ID=15

ADD HYD

ID=50 HYD NO=100.20 ID=50 ID=16

PRINT HYD

ID=50 CODE=1

PARTIAL HYDROGRAPH 100.20

RUNOFF VOLUME = 1.97292 INCHES = 3.6259 ACRE-FEET
PEAK DISCHARGE RATE = 89.04 CFS AT 1.500 HOURS BASIN AREA = 0.0345 SQ. MI.

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*ROUTE THROUGH D	ETENTION POND NO	0 1			
ROUTE RESERVOIR	ID=55 HYD NO	0=200.1	LINFLOW	ID=50	CODE=24
	OUTFLOW	(CF5)	STORAGE(AC-FT)	ELEVATION

W	0.0	STORAGE(AC-FT) ELEVAT 0.0	TION(FT) 59.00
	2.745	0.2646	60.00
	8.002	2.1906	65.00
	10.979	5.2846	70.00
	11.233	5.6666	70.50

TIME	INFLOW	ELEV	VOLUME	OUTFLOW
(HRS)	(CFS)	(FEET)	(AC-FT)	(CFS)
0.00 1.20 2.40 3.60 4.80 6.00 7.20 8.40 9.60 10.80 12.00 14.40 15.60 16.80 19.20 20.40 21.60 22.80 24.00 25.20 26.40 27.60 28.80 30.00	0.00 10.40 2.77 0.13 0.20 0.35 0.38 0.38 0.38 0.38 0.38 0.38 0.38 0.38	59.00 59.41 65.18 63.54 62.12 61.06 69.62 59.31 59.16 59.14 59.14 59.14 59.14 59.14 59.14 59.14 59.14 59.14 59.14 59.14 59.14 59.14 59.06 59.00 59.00 59.00	0.000 0.110 2.303 1.630 1.081 0.674 0.371 0.163 0.082 0.053 0.042 0.037 0.037 0.037 0.037 0.037 0.037 0.037 0.037 0.037 0.037 0.037 0.037 0.037 0.037 0.037	0.00 1.14 8.11 6.47 4.97 3.86 3.03 1.69 0.85 0.44 0.40 0.39 0.38 0.38 0.38 0.38 0.38 0.38 0.38

PEAK DISCHARGE = 8.196 CFS - PEAK OCCURS AT HOUR 2.10

MAXIMUM WATER SURFACE ELEVATION = 65.325

MAXIMUM STORAGE = 2.3919 AC-FT INCREMENTAL TIME= 0.050000HRS

PRINT HYD

ID=55 CODE=1

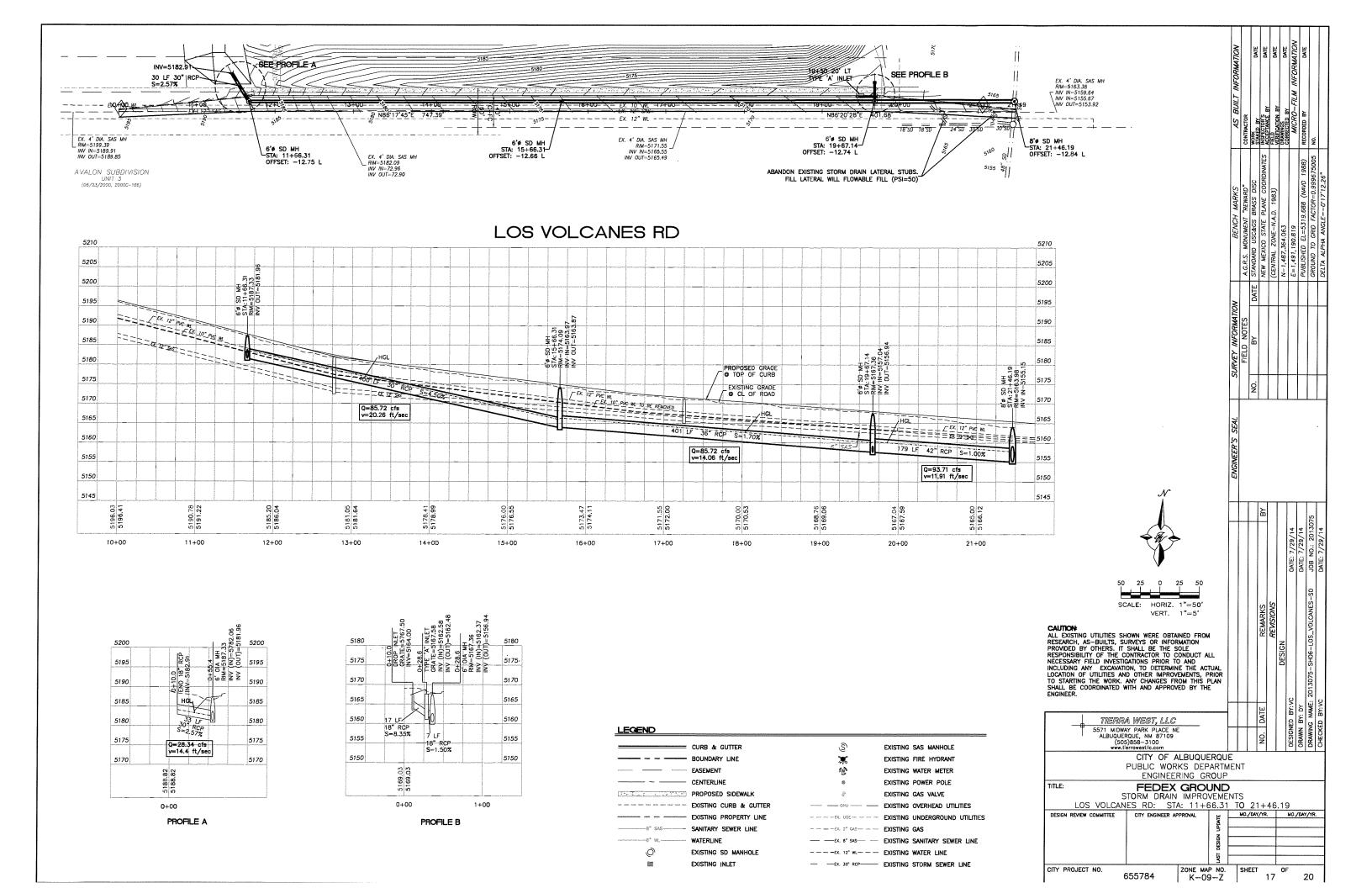
PARTIAL HYDROGRAPH 200.10

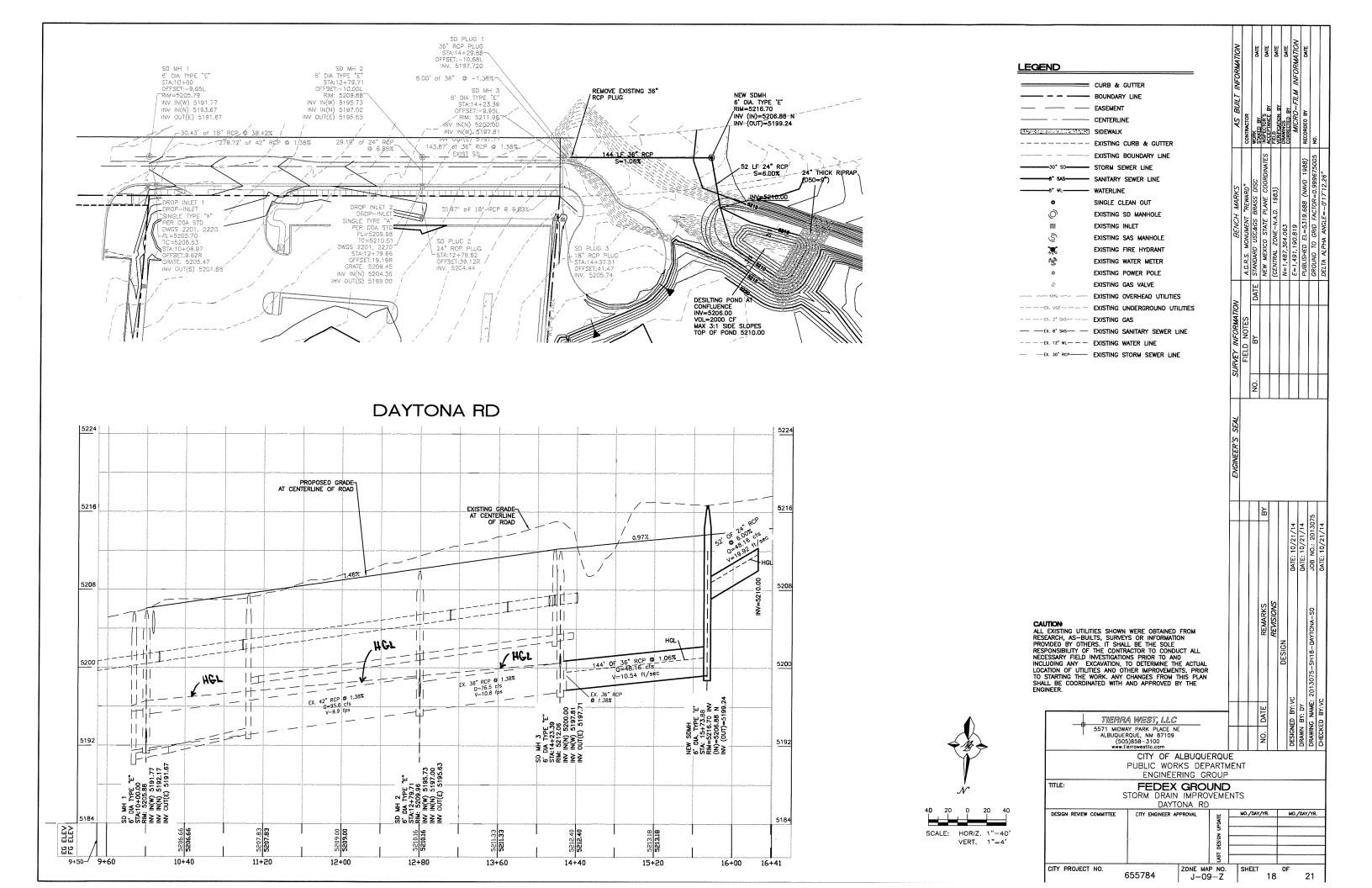
RUNOFF VOLUME = 1.97292 INCHES RUNOFF VOLUME = 1.97292 INCHES = 3.6259 ACRE-FEET
PEAK DISCHARGE RATE = 8.20 CFS AT 2.100 HOURS BASIN AREA = 0.0345 SQ. MI.

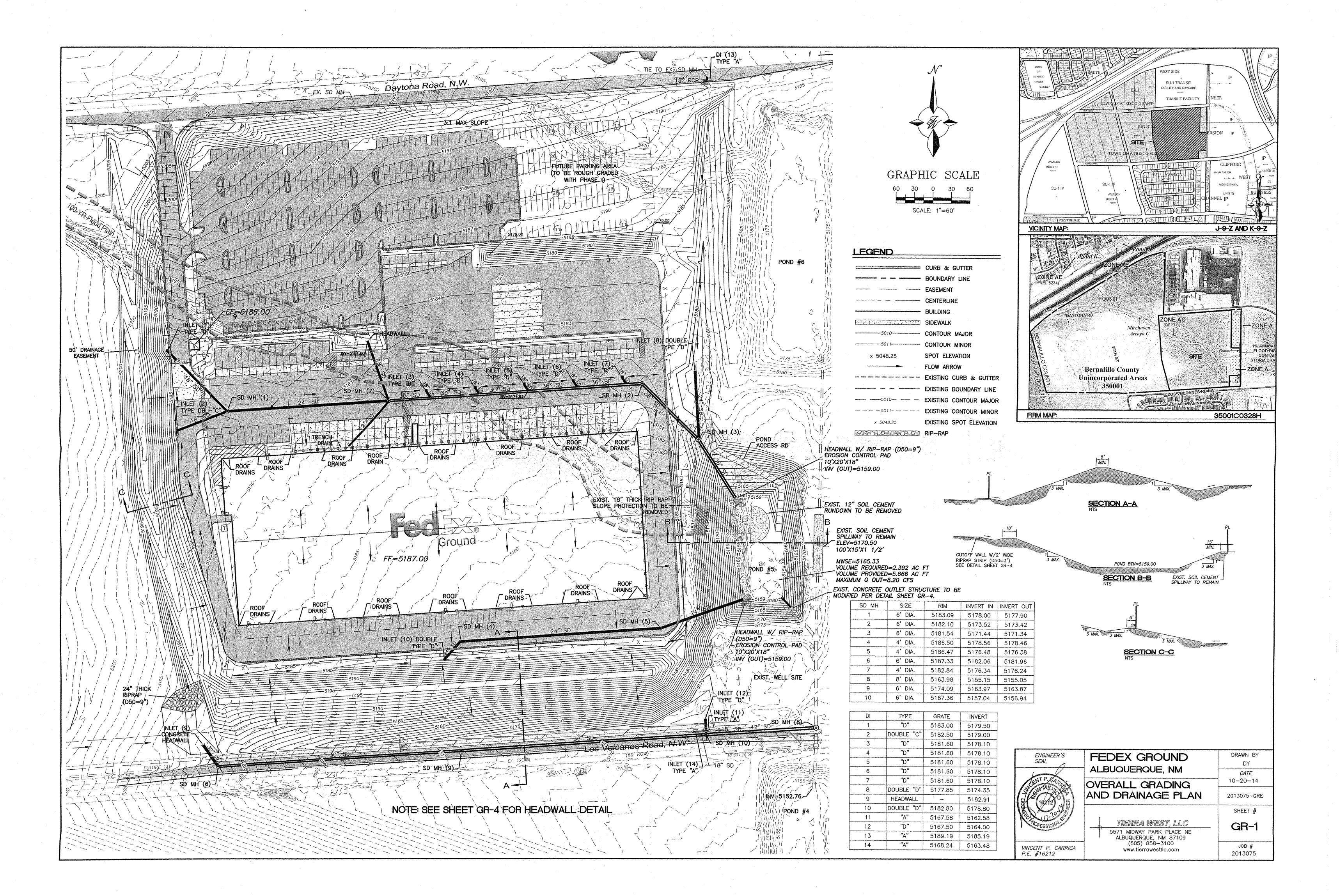
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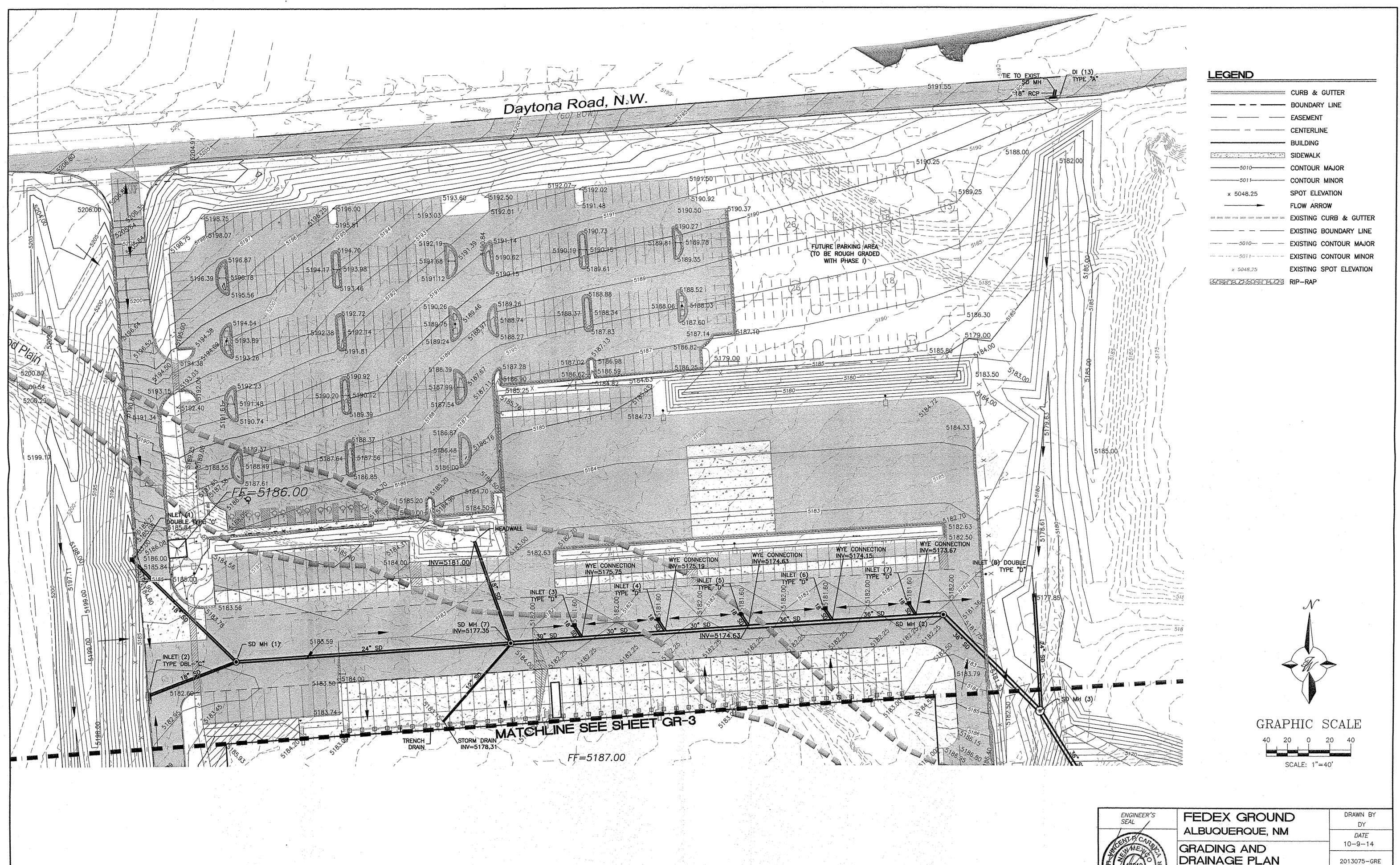
FINISH

NORMAL PROGRAM FINISH END TIME (HR:MIN:SEC) = 15:34:11

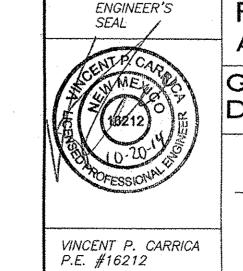








NOTE: SEE ARCHITECTURAL PLANS FOR DETAIL AT STAIRS AND ENTRANCES TO THE BUILDING.

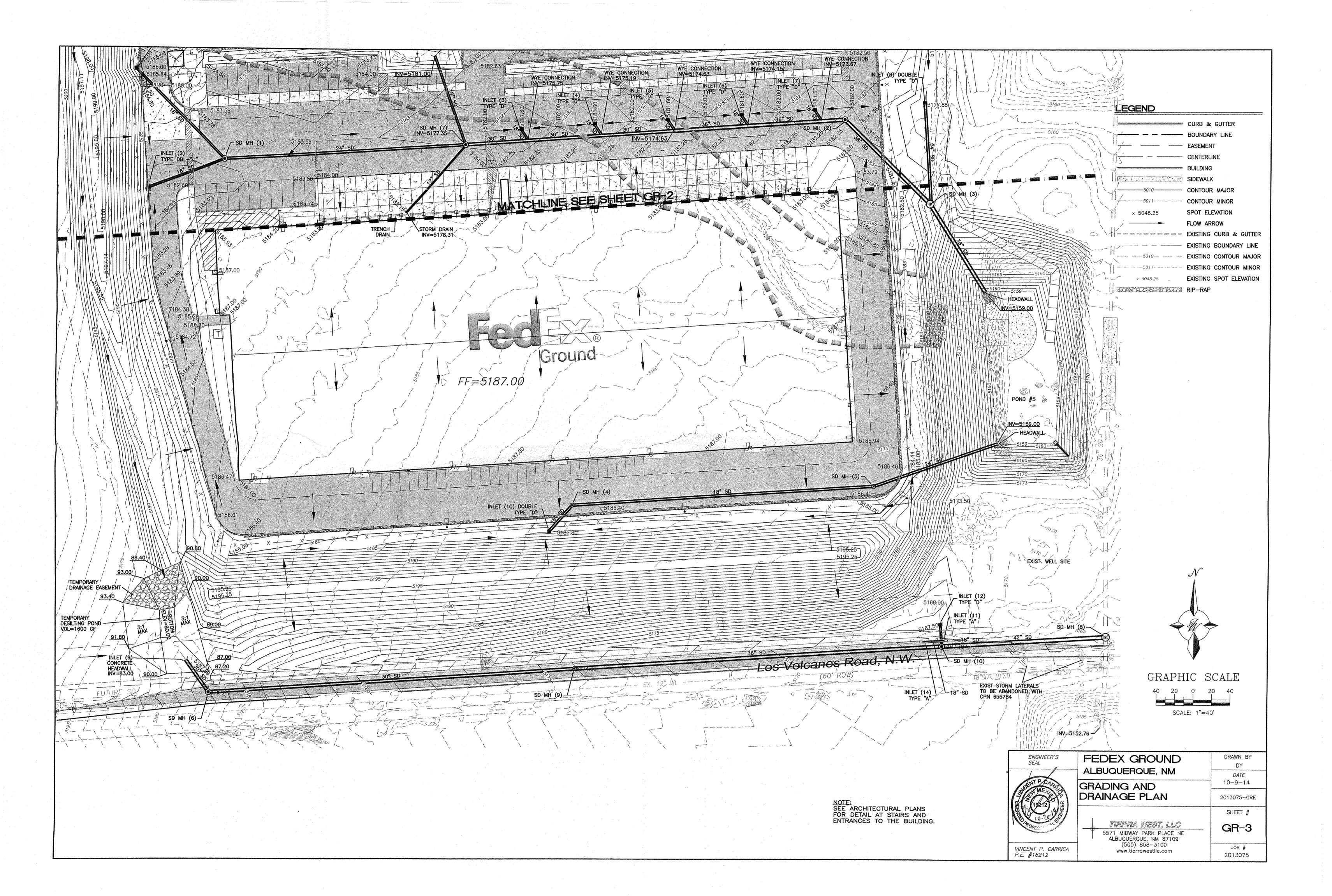


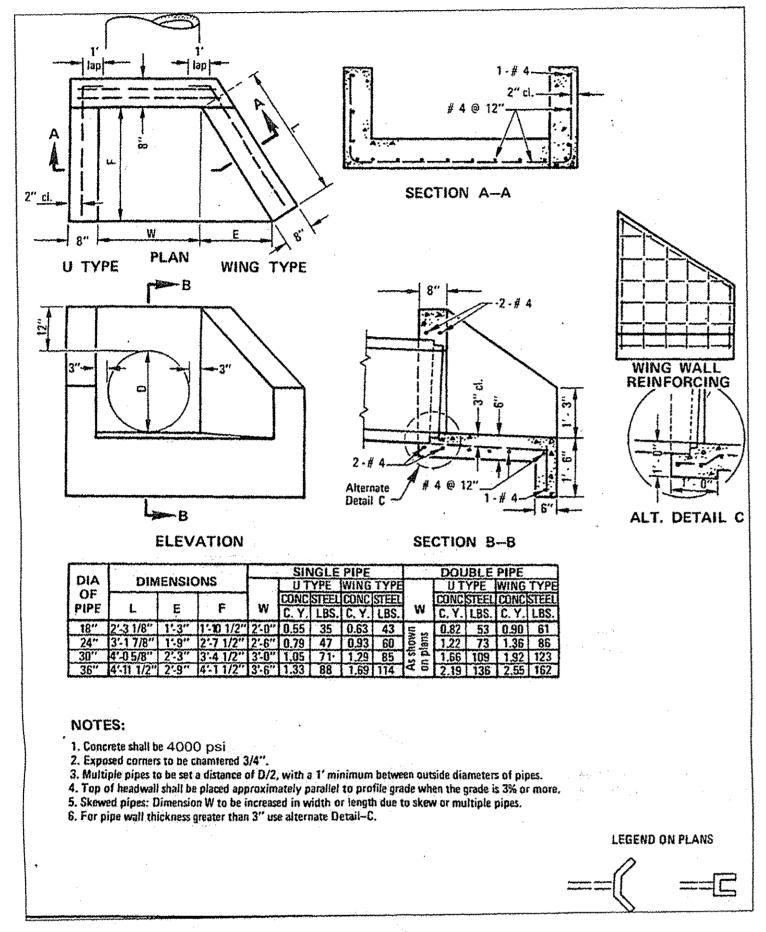
	ALBUQUERQUE,				
	GRADING AND				
	DRAINAGE PLA				

TIERRA WEST, LLC 5571 MIDWAY PARK PLACE NE ALBUQUERQUE, NM 87109 (505) 858-3100 www.tierrawestllc.com

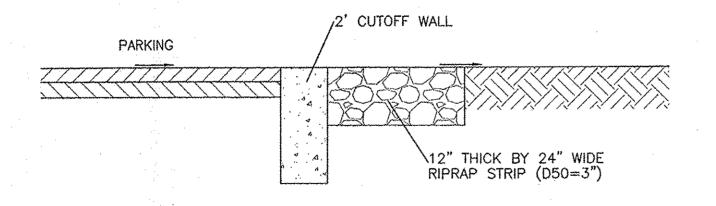
GR-2 JOB # 2013075

SHEET #

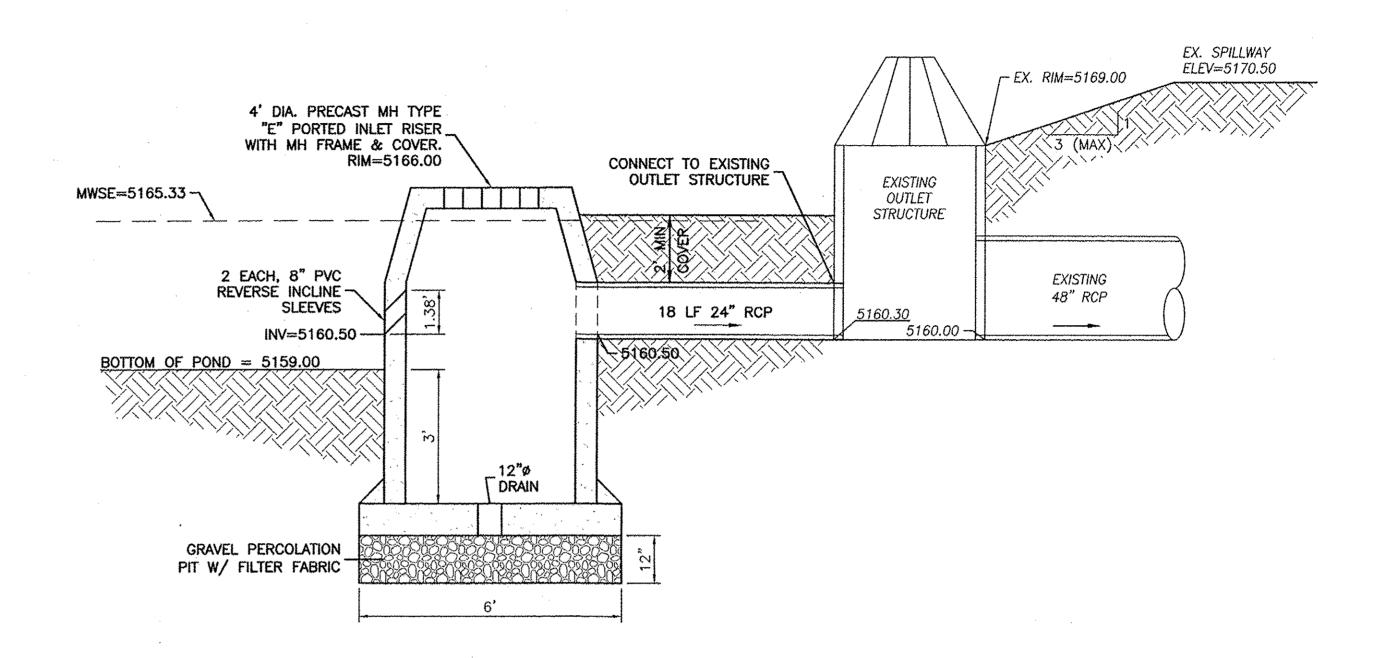




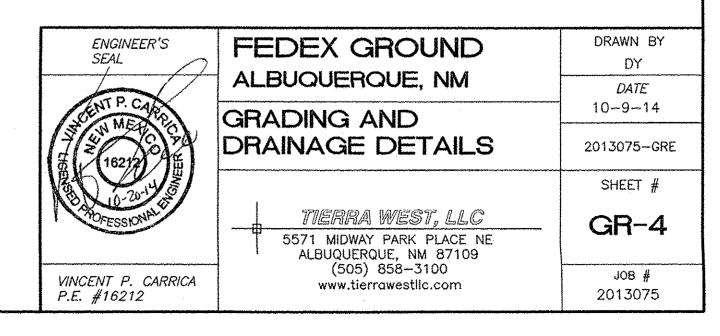
HEADWALL DETAIL
NTS

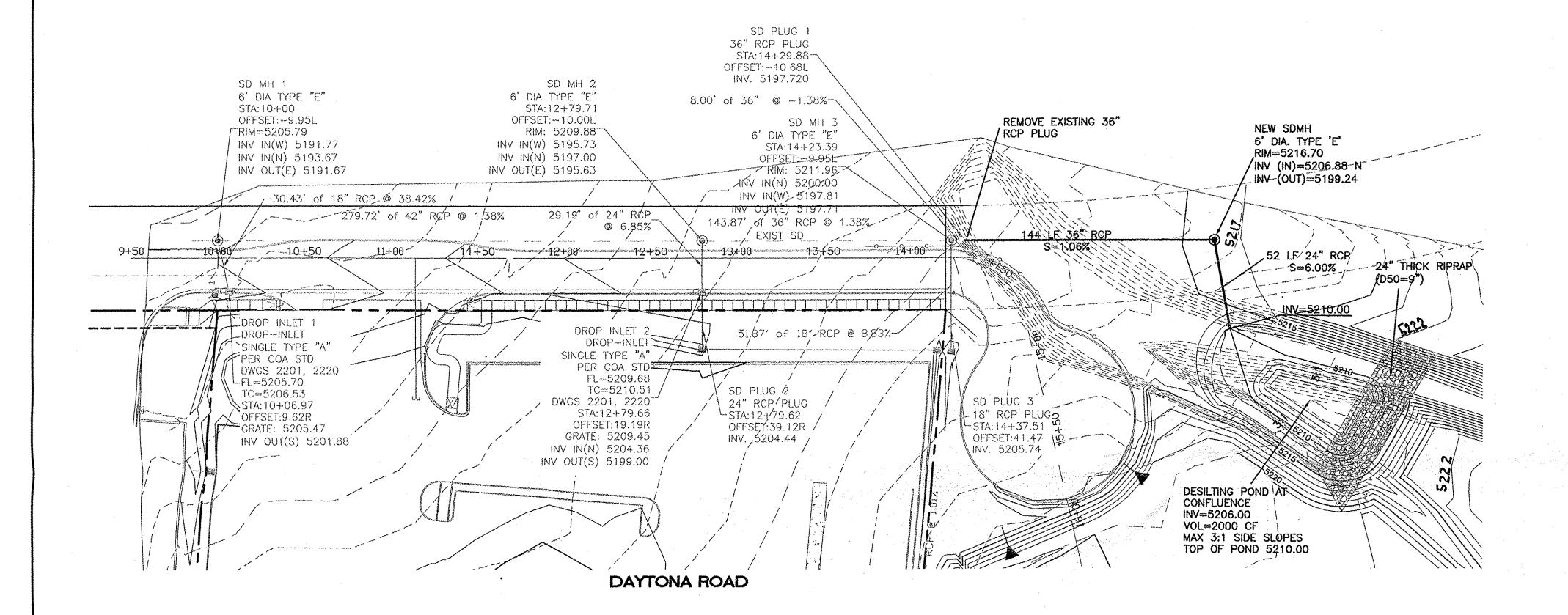


CUTOFF WALL-RIPRAP STRIP DETAIL



POND 5 OUTLET STRUCTURE MODIFICATION DETAIL



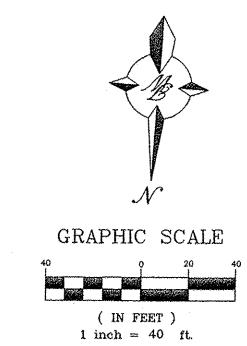


GENERAL NOTES:

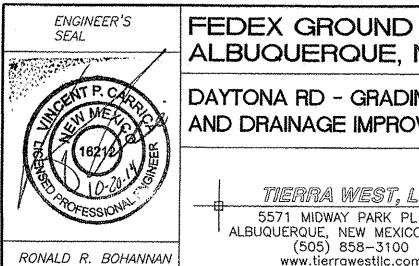
1. BASIS OF STATIONING IS CENTERLINE OF DAYTONA RD.

LEGEND

CURB & GUTTER BOUNDARY LINE ---- EASEMENT CENTERLINE RIGHT-OF-WAY SIDEWALK EXISTING CURB & GUTTER EXISTING BOUNDARY LINE



ALL EXISTING UTILITIES SHOWN WERE OBTAINED FROM RESEARCH, AS-BUILTS, SURVEYS OR INFORMATION PROVIDED BY OTHERS. IT SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR TO CONDUCT ALL NECESSARY FIELD INVESTIGATIONS PRIOR TO AND INCLUDING ANY EXCAVATION, TO DETERMINE THE ACTUAL LOCATION OF UTILITIES AND OTHER IMPROVEMENTS, PRIOR TO STARTING THE WORK. ANY CHANGES FROM THIS PLAN SHALL BE COORDINATED WITH AND APPROVED BY THE ENGINEER.



P.E. #7868

<i>j</i>	ALBUQUERQUE, NM	pm	
	DAYTONA RD - GRADING	<i>DATE</i> 10-20-14	
X	AND DRAINAGE MAPROVEMENTO	<i>DRAWING</i> 2013075—DAYTONA	
		SHEET #	
	l tierra west. llc	OD E	

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GR-5 JOB # www.tierrawestllc.com 2013075

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