

DRAINAGE REPORT
for
CLIFFORD WEST BUSINESS PARK



REV. 3-11-98

SEPTEMBER 1997

DRAINAGE INFORMATION SHEET

K-9/D23

PROJECT TITLE: Clifford West Business Park ZONE ATLAS/DRNG, FILE#: ~~K-9/D23~~

DRB #: 97-138 EPC #: S-97-21 WORK ORDER #: _____

LEGAL DESCRIPTION: ATRISCO BUSINESS PARK, UNIT 2, TRACT K-1 and

CITY ADDRESS: UNSER DIVERSION CHANNEL CORRIDOR J-1, TOWN OF ATRISCO
GRANT

ENGINEERING FIRM: Mark Goodwin + Assoc. PA CONTACT: Diane Hoelzer

ADDRESS: P.O. Box 90606 ABQ 87199 PHONE: 828-2200

OWNER: Grayland Inc. CONTACT: Jack Clifford

ADDRESS: P.O. Box 35640 ABQ 87176 PHONE: 881-0900

ARCHITECT: _____ CONTACT: _____

ADDRESS: _____ PHONE: _____

SURVEYOR: _____ CONTACT: _____

ADDRESS: _____ PHONE: _____

CONTRACTOR: _____ CONTACT: _____

ADDRESS: _____ PHONE: _____

TYPE OF SUBMITTAL:

CHECK TYPE OF APPROVAL SOUGHT:

- ☐ DRAINAGE REPORT
- ☒ DRAINAGE PLAN
- ☐ CONCEPTUAL GRADING & DRAINAGE PLAN
- ☒ GRADING PLAN
- ☐ EROSION CONTROL PLAN
- ☐ ENGINEER'S CERTIFICATION
- ☒ OTHER supplemental information

- ☐ SKETCH PLAT APPROVAL
- ☒ PRELIMINARY PLAT APPROVAL
- ☐ S. DEV. PLAN FOR SUB'D APPROVAL
- ☐ S. DEV. PLAN FOR BLDG PERMIT APPROVAL
- ☐ SECTOR PLAN APPROVAL
- ☐ FINAL PLAT APPROVAL
- ☐ FOUNDATION PERMIT APPROVAL
- ☐ BUILDING PERMIT APPROVAL
- ☐ CERTIFICATION OF OCCUPANCY APPROVAL
- ☐ GRADING PERMIT APPROVAL
- ☐ PAVING PERMIT APPROVAL
- ☐ S.A.D. DRAINAGE REPORT
- ☐ DRAINAGE REQUIREMENTS
- ☐ OTHER _____ (Specify)

PRE-DESIGN MEETING:

- ☐ YES
- ☐ NO
- ☐ COPY PROVIDED

DATE SUBMITTED: _____

BY: Diane Hoelzer

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I. LOCATION AND DESCRIPTION

The proposed Clifford West Business Park , which was part of the larger Atrisco Business Park is comprised of approximately 52.2 acres and is located south of I-25, just west of Unser Blvd. between Los Volcanes Road and Bluewater Road. Proposed development includes the infrastructure to support the individual development of 29 commercial sites.

The topographic relief in the area is in an southeasterly direction at a slope of approximately 2.0 percent.

The FEMA map indicates that a portion of the site is within the 100-year floodplain. Presently AMAFCA is working on a LOMR for the Unser Diversion. The Unser Diversion infrastructure has been built.

II. DRAINAGE DESIGN CRITERIA AND ASSUMPTIONS

The design criteria used in this report was in accordance with Section 22.2 Hydrology of the Development Process Manual, Volume 2, Design Criteria, January 1993 edition. The drainage management plan for this site is based entirely on the previously approved Atrisco Business Park Master Drainage Plan for fully developed conditions dated October 22, 1993. In accordance with that plan the allowable discharge from this site is 56.6 cfs and the 100-year peak discharge from this site is 217.1 cfs. These two values are the basis for all the drainage calculations in this report.

IV. EXISTING DRAINAGE CONDITIONS

Under existing drainage conditions, on-site runoff flows in a southeasterly direction. All of these flows are intercepted by either Unser Blvd. or Bluewater Road. There is an existing swale on this site just north of Bluewater Road that intercepts flows and conveys the runoff to the east toward Unser Blvd. After some ponding the flows spill over into Unser Blvd. at the intersection with Bluewater Road.

Off-site flows along the east and south property line continue in the southeasterly direction, away from the project site. Off-site flows north of the project site flow in a southeasterly direction through the site. All flows west of the site are intercepted by the Unser Diversion facility.

There is an existing storm drain in Unser Blvd. that includes stub-outs in Los Volcanes Road and Bluewater Road and four inlets in the west flowline of Unser Blvd. This system includes two inlets at the intersection of Los Volcanes Rd./Unser Blvd. and four inlets at the intersection of Bluewater Road/Unser Blvd.

V. PROPOSED DRAINAGE CONDITIONS

A. MASTER DRAINAGE PLAN

For this drainage plan the primary drainage requirement is that every individual commercial site will be required to retain a certain amount of their runoff on-site and all runoff from the site must discharge directly into the adjacent storm drain. The allowable discharge from each lot within the project site was calculated based on the approved master drainage plan for Atrisco Business Park and is summarized in a Table in Figure 3 and shown on the grading and drainage plan. Drainage calculations are in the Appendix A Hydrology.

The storm drain in Bluewater Road will be extended west to the Unit 1/3 boundary divide and in Oliver Ross Road and Saul Bell Road within the project site. Storm drain stub-outs will be provided to the property line for each of the 29 lots. Four 18" storm drain laterals will be extended from the existing inlets in Unser Blvd. to the property line to allow direct discharge from the seven properties adjacent to Unser Blvd. The storm drain in

Bluewater will include four stub-outs to the property line to service those lots that drain in a southerly direction.

Street flows in Los Volcanes Road will be intercepted by the existing inlets at the Unser Blvd. Intersection. Street flows in Bluewater Road will be intercepted by the existing inlets at the intersection of Unser Blvd. Street flows in Saul Bell Road will be intercepted by two new inlets located just west of the Unser Blvd. intersection.

Off-site flows originating from the west are intercepted by the Unser Diversion Facility. Off-site flows originating from the north will be intercepted by a temporary drainage swale located within the public right-of-way along the north side of Los Volcanes Road before discharging into the street at the intersection of Unser Blvd. and Los Volcanes Road. The profile for Los Volcanes road is being constructed lower than the surrounding area to help prevent the possibility of offsite flows originating from the north from entering the project site as it is developing.

The Atrisco Business Park Master Plan Fully Developed Conditions exhibit is included in the back pocket of this report to facilitate in the understanding of the big picture for development of the area. Another close up exhibit of the area and the drainage basin areas used in the master plan is included in Appendix A Hydrology.

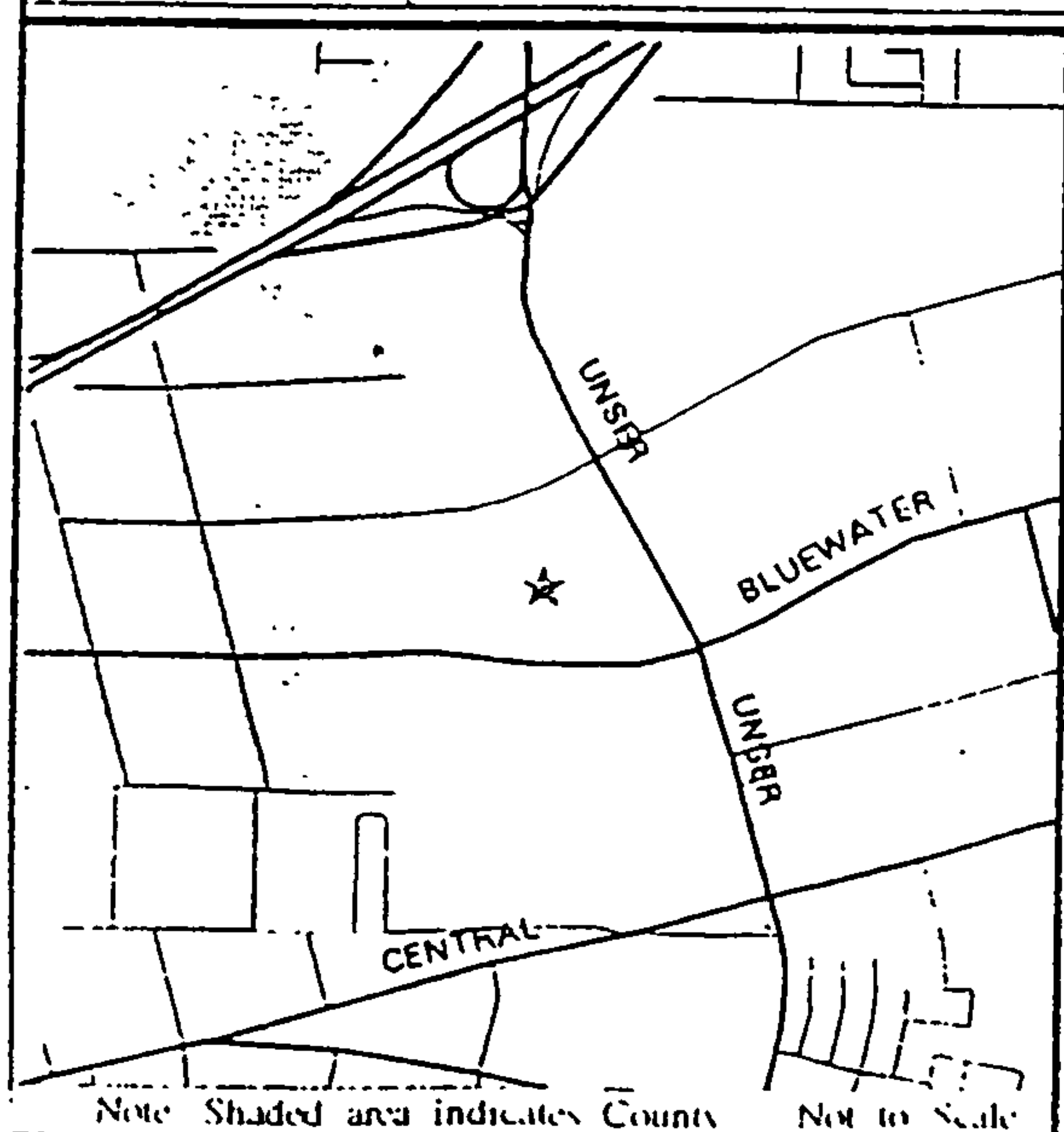
TABLE 1

SUMMARY OF STREET CAPACITY AND INLET CALCULATIONS

Clifford West Industrial Park

LOCATION	LOCATION	WIDTH ft.	SLOPE %	Q cfs	DEPTH ft	Q per INLET cfs	# of INLETS	REMAIN Q (cfs)	ADDITIONAL Q (cfs)
Oliver Ross Rd	@ Bluewater	40' FF	1.54	7.88	0.31	2.50	2	2.88	—
Saul Bell Rd	@ Unser	40' FF	0.60	4.24	0.29	1.65	2	0.94	—
Bluewater	@ Unser	40' FF	2.00	12.81	0.34	3.80	2	5.21	—
Bluewater	@ Unser	40' FF	0.005	5.21	0.32	1.90	2	1.41	—
Bluewater	@ Oliver Ross	40' FF	1.00	5.69	0.30	2.0	1	3.69	—

f:\clifford.wst\condition.tbl



Note: Shaded area indicates County Not to Scale

LAND USE MAP

KEY to Land Use Abbreviations

AGRI Agricultural
 COMM Commercial - Retail, Service, Wholesale
 DRNG Drainage
 EDUC Public or Private School
 GOLF Golf Course
 MED Medical Office or Facility
 MFG Manufacturing or Mining
 MH Mobile Home
 MULT Multi-Family or Group Home
 OFF Office
 ORG Social or Civic Organization
 PARK Park, Recreation or Open Space
 PRKG Parking
 PUBF Public Facility
 RELG Religious Facility
 SF Single Family
 TRAN Transportation Facility
 UTIL Utility
 VAC Vacant Land or Abandoned Bldg
 WH Warehousing & Storage



Scale 1" = 449'

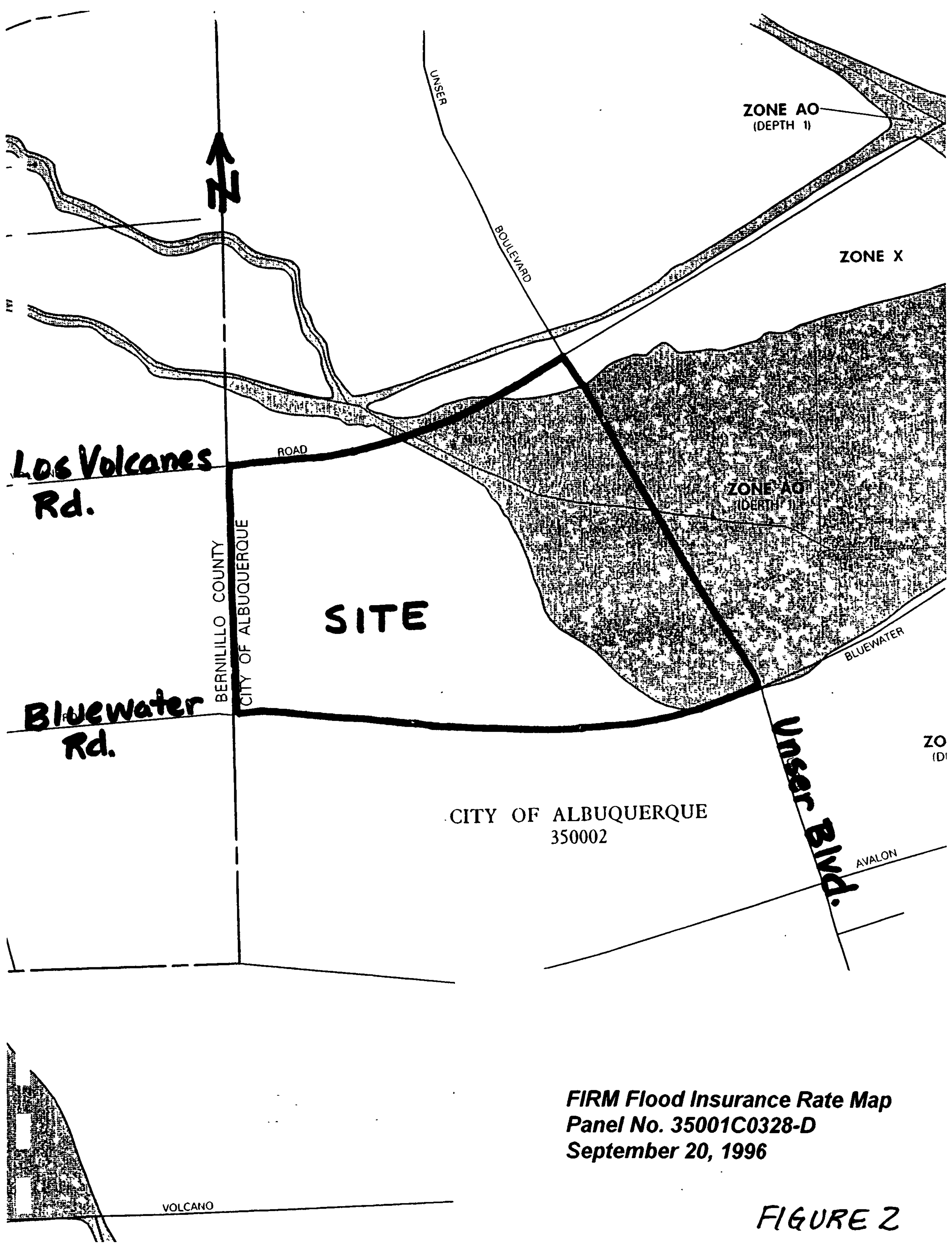
CASE PLANNER

HEARING DATE
1-16-97

MAP NO.
K-9/K-10

FILE NO.
Z-97-11

FIGURE 1



APPENDIX A
HYDROLOGY

Type 'C' Sump Inlets Calculations For Saul Bell Road

Capacity is measured by the weir equation at the lip of the gutter assuming an allowable ponding elevation which is 0.67' (or top of curb elevation). The length of the grate facing the street is 2.95' with a corresponding ponding depth of 0.54' (at top of curb). The side width is 2.0' with a corresponding average ponding depth of 0.604'.

With these values and the using the weir equation, the design capacity for the two type 'C' grates is:

Front: $Q_{cap} = 3.0 \times 2.95' \times (.54')^{1.5} = 3.51 \text{ cfs}$

Sides: $Q_{cap} = 3.0 \times 2.0' \times (.604')^{1.5} \times (2 \text{ sides}) = 5.63 \text{ cfs}$

Design Q_{cap} (per inlet) = 9.14 cfs

Total Design Capacity (2 inlets) **$Q(\text{design}) = 18.28 \text{ cfs}$**

$Q(100 \text{ yr.}) = 4.24 \text{ cfs}$

The storm drain has the capacity to handle twice the 4.24 cfs flow (or 8.48 cfs) and thus an emergency overflow spillway is not necessary.



D. Mark Goodwin & Associates, P.A.
Consulting Engineers and Surveyors

PROJECT _____
SUBJECT Hydrology
BY DLH DATE 9-12-97
CHECKED _____ DATE _____
SHEET _____ OF _____

Summary of Approved Hydrology Criteria For

THE ATRISCO BUSINESS PARK MASTER DRAINAGE PLAN (K10/D23)

APPROVED 10-22-93

POCKET 1 FOR SCHEMATIC.

1. 100 YR. 24 HR. STORM

RAINFALL TYPE 2

$P_1 = 1.87$ $P_6 = 2.20"$ $P_{24} = 2.66"$

$DT = 0.05$

SUBBASIN 170.7 = 55 ACRES $\Rightarrow Q_{max} = 217.1$ CFS

2. FOR SAD 214 REPORT $Q_{max. allowable} = 56.6$ cfs


```

START                                TIME=0.0
*****    CLIFFORD WEST BUSINESS PARK
*****    100-YEAR 6-HOUR STORM EVENT
*****    FILE: CLIFFEX.DAT  JULY 1997 BY:DLH
RAINFALL                                TYPE=1 RAIN QUARTER=0.0 IN
                                           RAIN ONE=1.90 IN RAIN SIX=2.20 IN
                                           RAIN DAY=0.0 IN DT=0.0333 HR

*****
***** NORTH OFFSITE EXISTING CONDITIONS
*****
COMPUTE NM HYD                        ID=1 HYD NO=100.0 AREA=0.02532 SQ MI
                                           PER A=100 PER B=0 PER C=0 PER D=0
                                           TP=0.1333 HR MASS RAINFALL=-1

PRINT HYD                            ID=1 CODE=1
*****
***** LOS VOLCANES PAVED CONDITIONS
*****
COMPUTE NM HYD                        ID=1 HYD NO=100.0 AREA=0.002036 SQ MI
                                           PER A=0 PER B=10 PER C=0 PER D=90
                                           TP=0.1333 HR MASS RAINFALL=-1

PRINT HYD                            ID=1 CODE=1
*****
***** SAUL BELL RD PAVED CONDITIONS
*****
COMPUTE NM HYD                        ID=1 HYD NO=100.0 AREA=0.001572 SQ MI
                                           PER A=0 PER B=10 PER C=0 PER D=90
                                           TP=0.1333 HR MASS RAINFALL=-1

PRINT HYD                            ID=1 CODE=1
*****
***** OLIVER ROSS RD PAVED CONDITIONS
*****
COMPUTE NM HYD                        ID=1 HYD NO=100.0 AREA=0.002928 SQ MI
                                           PER A=0 PER B=10 PER C=0 PER D=90
                                           TP=0.1333 HR MASS RAINFALL=-1

PRINT HYD                            ID=1 CODE=1
*****
***** BLUEWATER PAVED CONDITIONS
*****
COMPUTE NM HYD                        ID=1 HYD NO=100.0 AREA=0.004764 SQ MI
                                           PER A=0 PER B=10 PER C=0 PER D=90
                                           TP=0.1333 HR MASS RAINFALL=-1

PRINT HYD                            ID=1 CODE=1
FINISH

```

RUN DATE (MON/DAY/YR)

USER NO. =

CFS	PAGE = 1	HYDROGRAPH	FROM ID	TO ID	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)
PER ACRE	COMMAND NOTATION	IDENTIFICATION	NO.	NO.					
START TIME= .00 RAINFALL TYPE= 1 RAIN6= 2.200 COMPUTE NM HYD 100.00 - 1 .02532 21.53 .606 .44912 1.532 1.328 PER IMP= .00 COMPUTE NM HYD 100.00 - 1 .00204 5.48 .200 1.83780 1.499 4.209 PER IMP= 90.00 COMPUTE NM HYD 100.00 - 1 .00157 4.24 .154 1.83780 1.499 4.213 PER IMP= 90.00 COMPUTE NM HYD 100.00 - 1 .00293 7.88 .287 1.83780 1.499 4.205 PER IMP= 90.00 COMPUTE NM HYD 100.00 - 1 .00476 12.81 .467 1.83780 1.499 4.202 PER IMP= 90.00 FINISH									

APPENDIX B
STORM DRAIN

9-3-97

If drainage off of each lot requires an 18" SD directly into the main line, there will need to be a manhole at each service storm drain intersection with the main storm drain.

Sherrill
Jung

For Clifford West Business Park
Grading & Drainage Plan

K-9/10

1
0

HYDRAULIC REPORT FOR

CLIFFORD WEST BUS. PARK

@ UNSER AND BLUEWATER

100 YR 6 HR STORM

DMG & ASSOCIATES

MARCH 1998

BY: DLH

1
0

Run date: 03-10-1998
File: CLIFF.ST3

Return Period = 100 Yrs
Rainfall file: Your_County

LINE 1 / Q = 58.0 / HT = 36 / WID = 36 / N = .013 / L = 99 / JLC = .05

EXMH 1 - EXMH 2 / Outfall

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	12.00	36.00	6.41	8.21	13.05	0.00	5.73	7.07
UPSTRM	12.75	36.00	7.86	8.21	13.79	0.00	5.6	7.07

Drainage area (ac) = 0	Slope of invert (%) = 1.465
Runoff coefficient = 0	Slope energy grade line (%) = 0.756
Time of conc (min) = 13	Critical depth (in) = 29.12
Inlet time (min) = 0	Req'd length curb inlet (ft) = 0.0
Intensity (in/hr) = 0.00	Req'd grate area (sf) = 0.0
Cumulative C*A = 0.0	Depth at inlet opening (in) = 0
Flow contrib (cfs) = 58	Confluence angle (deg) = 0
Default Q (cfs) = 58	Natural ground elev (ft) = 16.47
Line capac. (cfs) = 80.7	Line storage (cuft) = 700

LINE 2 / Q = 46.6 / HT = 36 / WID = 36 / N = .013 / L = 299.75 / JLC = .05

EXMH 2 - MH 14 / DNLN = 1

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	12.80	36.00	7.86	6.59	13.48	0.00	5.6	7.07
UPSTRM	14.16	35.67	11.19	6.60	14.84	6.86	6.01	7.06

Drainage area (ac) = 0	Slope of invert (%) = 1.111
Runoff coefficient = 0	Slope energy grade line (%) = 0.455
Time of conc (min) = 11	Critical depth (in) = 26.10
Inlet time (min) = 0	Req'd length curb inlet (ft) = 0.0
Intensity (in/hr) = 0.00	Req'd grate area (sf) = 0.0
Cumulative C*A = 0.0	Depth at inlet opening (in) = 0
Flow contrib (cfs) = 46.5	Confluence angle (deg) = 0
Default Q (cfs) = 46.6	Natural ground elev (ft) = 20.2
Line capac. (cfs) = 70.3	Line storage (cuft) = 2117

LINE 3 / Q = 46.6 / HT = 30 / WID = 30 / N = .013 / L = 244.07 / JLC = .05

MH 14 - MH 13 / DNLN = 2

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	14.20	30.00	11.24	9.50	15.60	0.00	6.46	4.91
UPSTRM	17.35	30.00	13.70	9.49	18.75	0.00	6.75	4.91

Drainage area (ac) = 0	Slope of invert (%) = 1.008
Runoff coefficient = 0	Slope energy grade line (%) = 1.291
Time of conc (min) = 10	Critical depth (in) = 27.45
Inlet time (min) = 0	Req'd length curb inlet (ft) = 0.0
Intensity (in/hr) = 0.00	Req'd grate area (sf) = 0.0
Cumulative C*A = 0.0	Depth at inlet opening (in) = 0
Flow contrib (cfs) = 46.5	Confluence angle (deg) = 0
Default Q (cfs) = 46.6	Natural ground elev (ft) = 22.96
Line capac. (cfs) = 41.2	Line storage (cuft) = 1198

LINE 4 / Q = 42.4 / HT = 30 / WID = 30 / N = .013 / L = 356.84 / JLC = .05

MH 13 - MH 12 / DNLN = 3

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	17.42	30.00	13.75	8.64	18.58	0.00	6.7	4.91
UPSTRM	21.24	30.00	17.35	8.64	22.40	0.00	7.72	4.91

Drainage area (ac) = 0	Slope of invert (%) = 1.009
Runoff coefficient = 0	Slope energy grade line (%) = 1.070
Time of conc (min) = 8	Critical depth (in) = 26.55
Inlet time (min) = 0	Req'd length curb inlet (ft) = 0.0
Intensity (in/hr) = 0.00	Req'd grate area (sf) = 0.0
Cumulative C*A = 0.0	Depth at inlet opening (in) = 0
Flow contrib (cfs) = 42.4	Confluence angle (deg) = 0
Default Q (cfs) = 42.42	Natural ground elev (ft) = 27.58
Line capac. (cfs) = 41.2	Line storage (cuft) = 1751

LINE 5 / Q = 40.1 / HT = 30 / WID = 30 / N = .013 / L = 288.73 / JLC = .1

MH 12 - MH 11 / DNLN = 4

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	21.30	30.00	17.40	8.16	22.33	0.00	7.68	4.91
UPSTRM	24.05	30.00	20.31	8.16	25.09	0.00	7.46	4.91

Drainage area (ac) =	0	Slope of invert (%)	=	1.008
Runoff coefficient =	0	Slope energy grade line (%)	=	0.954
Time of conc (min) =	6	Critical depth (in)	=	25.38
Inlet time (min) =	0	Req'd length curb inlet (ft)	=	0.0
Intensity (in/hr) =	0.00	Req'd grate area (sf)	=	0.0
Cumulative C*A =	0.0	Depth at inlet opening (in)	=	0
Flow contrib (cfs) =	40	Confluence angle (deg)	=	0
Default Q (cfs) =	40.06	Natural ground elev (ft)	=	30.27
Line capac. (cfs) =	41.2	Line storage (cuft)	=	1417

LINE 6 / Q = 20.7 / HT = 24 / WID = 24 / N = .013 / L = 241 / JLC = .05

MH 11-END BLUE / DNLN = 5

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	24.15	24.00	20.81	6.59	24.83	0.00	7.46	3.14
UPSTRM	27.66	19.35	26.00	7.63	28.56	18.97	5.4	2.71

Drainage area (ac) = 0	Slope of invert (%) = 2.154
Runoff coefficient = 0	Slope energy grade line (%) = 1.548
Time of conc (min) = 0	Critical depth (in) = 19.33
Inlet time (min) = 0	Req'd length curb inlet (ft) = 0.0
Intensity (in/hr) = 0.00	Req'd grate area (sf) = 0.0
Cumulative C*A = 0.0	Depth at inlet opening (in) = 0
Flow contrib (cfs) = 20.7	Confluence angle (deg) = 0
Default Q (cfs) = 20.7	Natural ground elev (ft) = 33.4
Line capac. (cfs) = 33.2	Line storage (cuft) = 706

LINE 7 / Q = 19.4 / HT = 24 / WID = 24 / N = .013 / L = 26.45 / JLC = .05

MH 11 - MH 10 / DNLN = 5

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	24.15	24.00	20.81	6.18	24.75	0.00	7.46	3.14
UPSTRM	24.35	24.00	20.94	6.18	24.94	0.00	7.18	3.14

Drainage area (ac) = 0	Slope of invert (%) = 0.491
Runoff coefficient = 0	Slope energy grade line (%) = 0.736
Time of conc (min) = 6	Critical depth (in) = 18.71
Inlet time (min) = 0	Req'd length curb inlet (ft) = 0.0
Intensity (in/hr) = 0.00	Req'd grate area (sf) = 0.0
Cumulative C*A = 0.0	Depth at inlet opening (in) = 0
Flow contrib (cfs) = 19.3	Confluence angle (deg) = -90
Default Q (cfs) = 19.4	Natural ground elev (ft) = 30.13
Line capac. (cfs) = 15.9	Line storage (cuft) = 83

LINE 8 / Q = 12.0 / HT = 24 / WID = 24 / N = .013 / L = 187.14 / JLC = .05

MH 10 - MH 9 / DNLN = 7

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	24.38	24.00	20.99	3.82	24.61	0.00	7.13	3.14
UPSTRM	24.91	24.00	21.97	3.82	25.13	0.00	8.71	3.14

Drainage area (ac)	= 0	Slope of invert (%)	= 0.524
Runoff coefficient	= 0	Slope energy grade line (%)	= 0.282
Time of conc (min)	= 5	Critical depth (in)	= 14.72
Inlet time (min)	= 0	Req'd length curb inlet (ft)	= 0.0
Intensity (in/hr)	= 0.00	Req'd grate area (sf)	= 0.0
Cumulative C*A	= 0.0	Depth at inlet opening (in)	= 0
Flow contrib (cfs)	= 12	Confluence angle (deg)	= 0
Default Q (cfs)	= 12	Natural ground elev (ft)	= 32.69
Line capac. (cfs)	= 16.4	Line storage (cuft)	= 588

LINE 9 / Q = 11.6 / HT = 24 / WID = 24 / N = .013 / L = 135 / JLC = .05

MH 9 - MH 8 / DNLN = 8

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	24.92	24.00	22.02	3.68	25.13	0.00	8.66	3.14
UPSTRM	25.27	24.00	22.69	3.68	25.48	0.00	10.15	3.14

Drainage area (ac) = 0	Slope of invert (%) = 0.496
Runoff coefficient = 0	Slope energy grade line (%) = 0.262
Time of conc (min) = 5	Critical depth (in) = 14.45
Inlet time (min) = 0	Req'd length curb inlet (ft) = 0.0
Intensity (in/hr) = 0.00	Req'd grate area (sf) = 0.0
Cumulative C*A = 0.0	Depth at inlet opening (in) = 0
Flow contrib (cfs) = 11.5	Confluence angle (deg) = 0
Default Q (cfs) = 11.57	Natural ground elev (ft) = 34.85
Line capac. (cfs) = 15.9	Line storage (cuft) = 424

LINE 10 / Q = 11.1 / HT = 24 / WID = 24 / N = .013 / L = 94.2 / JLC = .05

MH 8 - MH 7 / DNLN = 9

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	25.28	24.00	22.74	3.53	25.48	0.00	10.1	3.14
UPSTRM	25.51	24.00	23.21	3.53	25.70	0.00	11.13	3.14

Drainage area (ac) = 0	Slope of invert (%) = 0.499
Runoff coefficient = 0	Slope energy grade line (%) = 0.240
Time of conc (min) = 4	Critical depth (in) = 14.15
Inlet time (min) = 0	Req'd length curb inlet (ft) = 0.0
Intensity (in/hr) = 0.00	Req'd grate area (sf) = 0.0
Cumulative C*A = 0.0	Depth at inlet opening (in) = 0
Flow contrib (cfs) = 11	Confluence angle (deg) = 0
Default Q (cfs) = 11.09	Natural ground elev (ft) = 36.35
Line capac. (cfs) = 16.0	Line storage (cuft) = 296

LINE 11 / Q = 10.0 / HT = 24 / WID = 24 / N = .013 / L = 161.9 / JLC = .1

MH 7 - MH 5 / DNLN = 10

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	25.52	24.00	23.26	3.18	25.68	0.00	11.08	3.14
UPSTRM	25.80	20.73	24.07	3.47	25.98	16.47	12.84	2.88

Drainage area (ac) = 0	Slope of invert (%) = 0.500
Runoff coefficient = 0	Slope energy grade line (%) = 0.191
Time of conc (min) = 3	Critical depth (in) = 13.44
Inlet time (min) = 0	Req'd length curb inlet (ft) = 0.0
Intensity (in/hr) = 0.00	Req'd grate area (sf) = 0.0
Cumulative C*A = 0.0	Depth at inlet opening (in) = 0
Flow contrib (cfs) = 10	Confluence angle (deg) = 0
Default Q (cfs) = 10	Natural ground elev (ft) = 38.92
Line capac. (cfs) = 16.0	Line storage (cuft) = 488

LINE 12 / Q = 4.0 / HT = 18 / WID = 18 / N = .013 / L = 157.3 / JLC = .05

MH 5 - MH 4 / DNLN = 11

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	25.82	14.35	24.62	2.59	25.92	14.01	12.79	1.54
UPSTRM	29.93	9.17	29.17	4.41	30.24	18.00	10.74	0.91

Drainage area (ac) = 0	Slope of invert (%) = 2.893
Runoff coefficient = 0	Slope energy grade line (%) = 2.744
Time of conc (min) = 2	Critical depth (in) = 9.15
Inlet time (min) = 0	Req'd length curb inlet (ft) = 0.0
Intensity (in/hr) = 0.00	Req'd grate area (sf) = 0.0
Cumulative C*A = 0.0	Depth at inlet opening (in) = 0
Flow contrib (cfs) = 3.9	Confluence angle (deg) = 0
Default Q (cfs) = 3.99	Natural ground elev (ft) = 41.42
Line capac. (cfs) = 17.9	Line storage (cuft) = 192

LINE 13 / Q = 3.6 / HT = 18 / WID = 18 / N = .013 / L = 138.81 / JLC = .05

MH 4 - MH 3 / DNLN = 12

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	29.95	8.75	29.22	4.14	30.22	18.00	10.69	0.86
UPSTRM	33.96	8.68	33.24	4.22	34.24	17.99	8.87	0.84

Drainage area (ac) = 0	Slope of invert (%) = 2.896
Runoff coefficient = 0	Slope energy grade line (%) = 2.899
Time of conc (min) = 1	Critical depth (in) = 8.64
Inlet time (min) = 0	Req'd length curb inlet (ft) = 0.0
Intensity (in/hr) = 0.00	Req'd grate area (sf) = 0.0
Cumulative C*A = 0.0	Depth at inlet opening (in) = 0
Flow contrib (cfs) = 3.5	Confluence angle (deg) = 0
Default Q (cfs) = 3.56	Natural ground elev (ft) = 43.62
Line capac. (cfs) = 17.9	Line storage (cuft) = 118

LINE 14 / Q = 2.3 / HT = 18 / WID = 18 / N = .013 / L = 128.4 / JLC = .05

MH 3 - MH 2 / DNLN = 13

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	33.98	8.24	33.29	2.84	34.10	17.95	8.82	0.80
UPSTRM	37.58	6.94	37.00	3.63	37.78	17.52	7.29	0.63

Drainage area (ac) = 0	Slope of invert (%) = 2.889
Runoff coefficient = 0	Slope energy grade line (%) = 2.867
Time of conc (min) = 1	Critical depth (in) = 6.91
Inlet time (min) = 0	Req'd length curb inlet (ft) = 0.0
Intensity (in/hr) = 0.00	Req'd grate area (sf) = 0.0
Cumulative C*A = 0.0	Depth at inlet opening (in) = 0
Flow contrib (cfs) = 2.2	Confluence angle (deg) = 0
Default Q (cfs) = 2.28	Natural ground elev (ft) = 45.8
Line capac. (cfs) = 17.9	Line storage (cuft) = 92

LINE 15 / Q = 1.1 / HT = 18 / WID = 18 / N = .013 / L = 131.4 / JLC = .05

MH 2 - MH 1 / DNLN = 14

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	37.59	6.46	37.05	1.96	37.65	17.34	7.25	0.59
UPSTRM	41.27	4.92	40.85	2.94	41.40	16.04	6.38	0.39

Drainage area (ac) = 0	Slope of invert (%) = 2.892
Runoff coefficient = 0	Slope energy grade line (%) = 2.856
Time of conc (min) = 0	Critical depth (in) = 4.91
Inlet time (min) = 0	Req'd length curb inlet (ft) = 0.0
Intensity (in/hr) = 0.00	Req'd grate area (sf) = 0.0
Cumulative C*A = 0.0	Depth at inlet opening (in) = 0
Flow contrib (cfs) = 1.1	Confluence angle (deg) = 0
Default Q (cfs) = 1.15	Natural ground elev (ft) = 48.73
Line capac. (cfs) = 17.9	Line storage (cuft) = 64

LINE 16 / Q = 5.6 / HT = 18 / WID = 18 / N = .013 / L = 214.9 / JLC = .05

MH 5 - MH 6 / DNLN = 11

	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	25.82	14.35	24.62	3.62	26.02	14.01	12.79	1.54
UPSTRM	26.61	10.91	25.70	4.98	26.99	17.59	10.93	1.12

Drainage area (ac) =	0	Slope of invert (%)	=	0.503
Runoff coefficient =	0	Slope energy grade line (%)	=	0.454
Time of conc (min) =	1	Critical depth (in)	=	10.82
Inlet time (min) =	0	Req'd length curb inlet (ft)	=	0.0
Intensity (in/hr) =	0.00	Req'd grate area (sf)	=	0.0
Cumulative C*A =	0.0	Depth at inlet opening (in)	=	0
Flow contrib (cfs) =	5.5	Confluence angle (deg)	=	-90
Default Q (cfs) =	5.58	Natural ground elev. (ft)	=	38.13
Line capac. (cfs) =	7.4	Line storage (cuft)	=	286

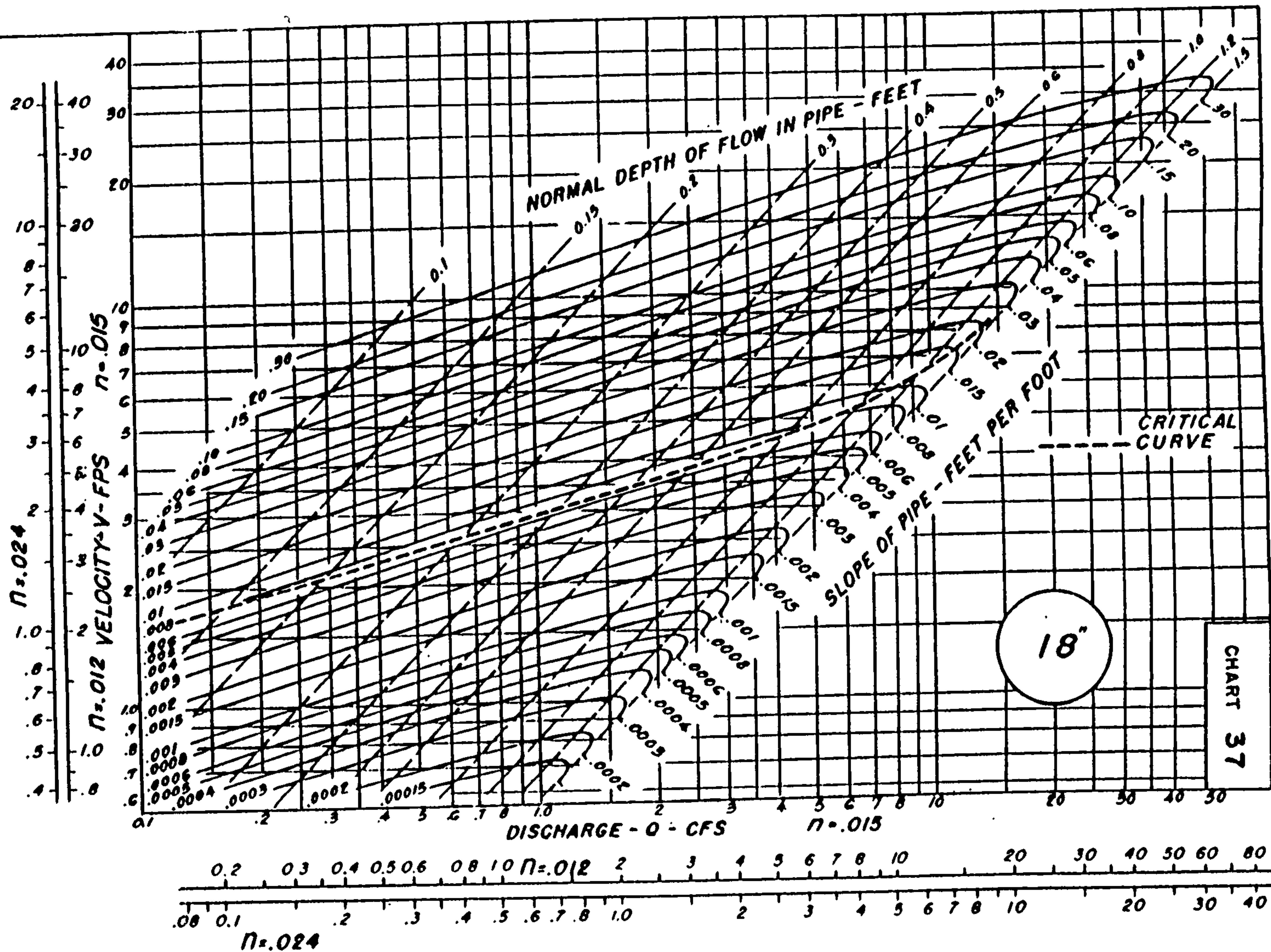
LINE 17 / Q = 4.2 / HT = 18 / WID = 18 / N = .013 / L = 197 / JLC = .05

MH 6 - MH 15 / DNLN = 16

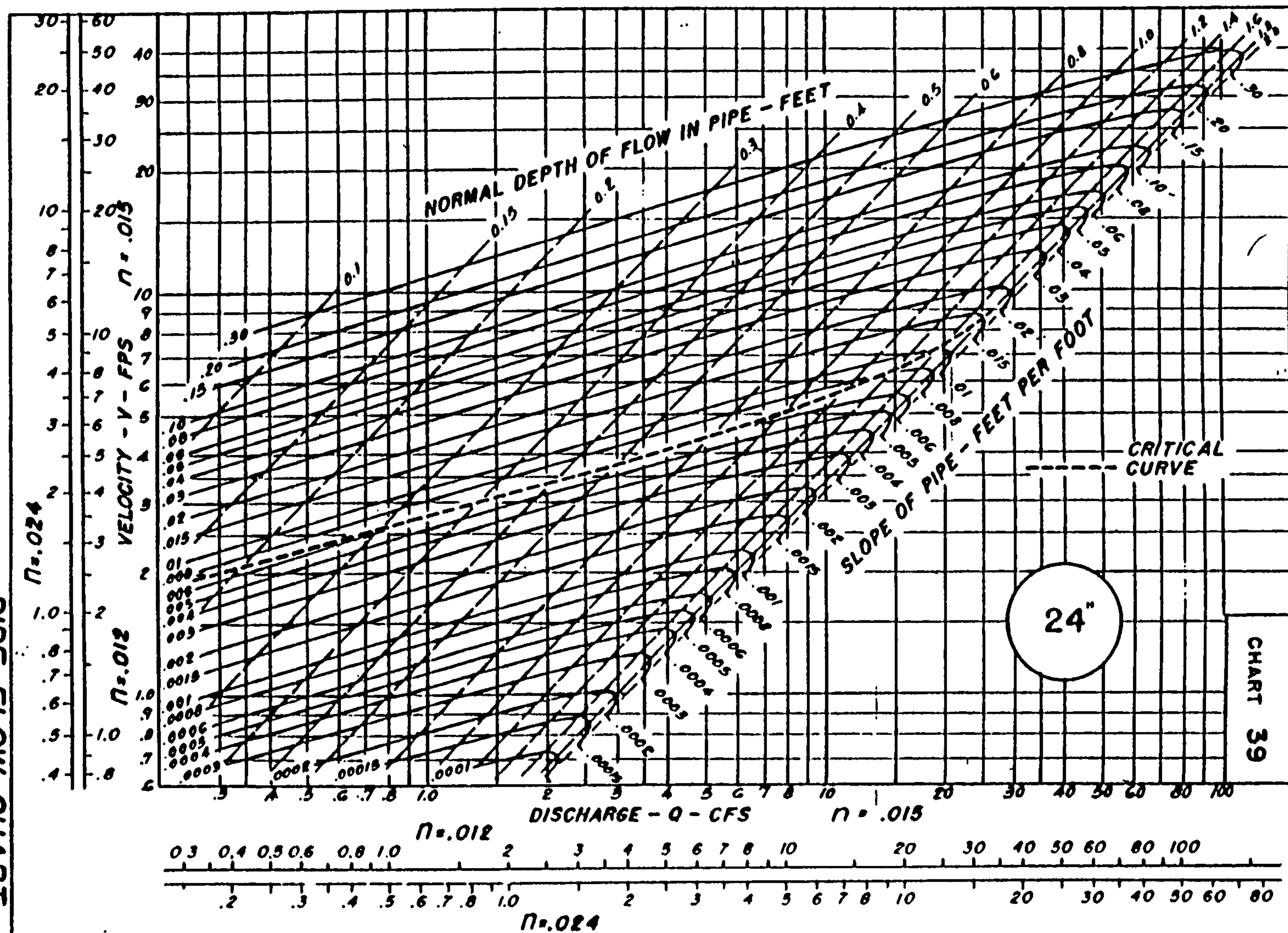
	HGL	DEPTH	INVERT	VEL	EGL	T WID	COVER	AREA
DNSTRM	26.63	10.54	25.75	3.91	26.87	17.71	10.88	1.08
UPSTRM	27.68	9.44	26.88	4.52	28.00	17.98	5	0.94

Drainage area (ac) = 0	Slope of invert (%) = 0.574
Runoff coefficient = 0	Slope energy grade line (%) = 0.567
Time of conc (min) = 0	Critical depth (in) = 9.43
Inlet time (min) = 0	Req'd length curb inlet (ft) = 0.0
Intensity (in/hr) = 0.00	Req'd grate area (sf) = 0.0
Cumulative C*A = 0.0	Depth at inlet opening (in) = 0
Flow contrib (cfs) = 4.2	Confluence angle (deg) = 0
Default Q (cfs) = 4.24	Natural ground elev (ft) = 33.38
Line capac. (cfs) = 8.0	Line storage (cuft) = 199

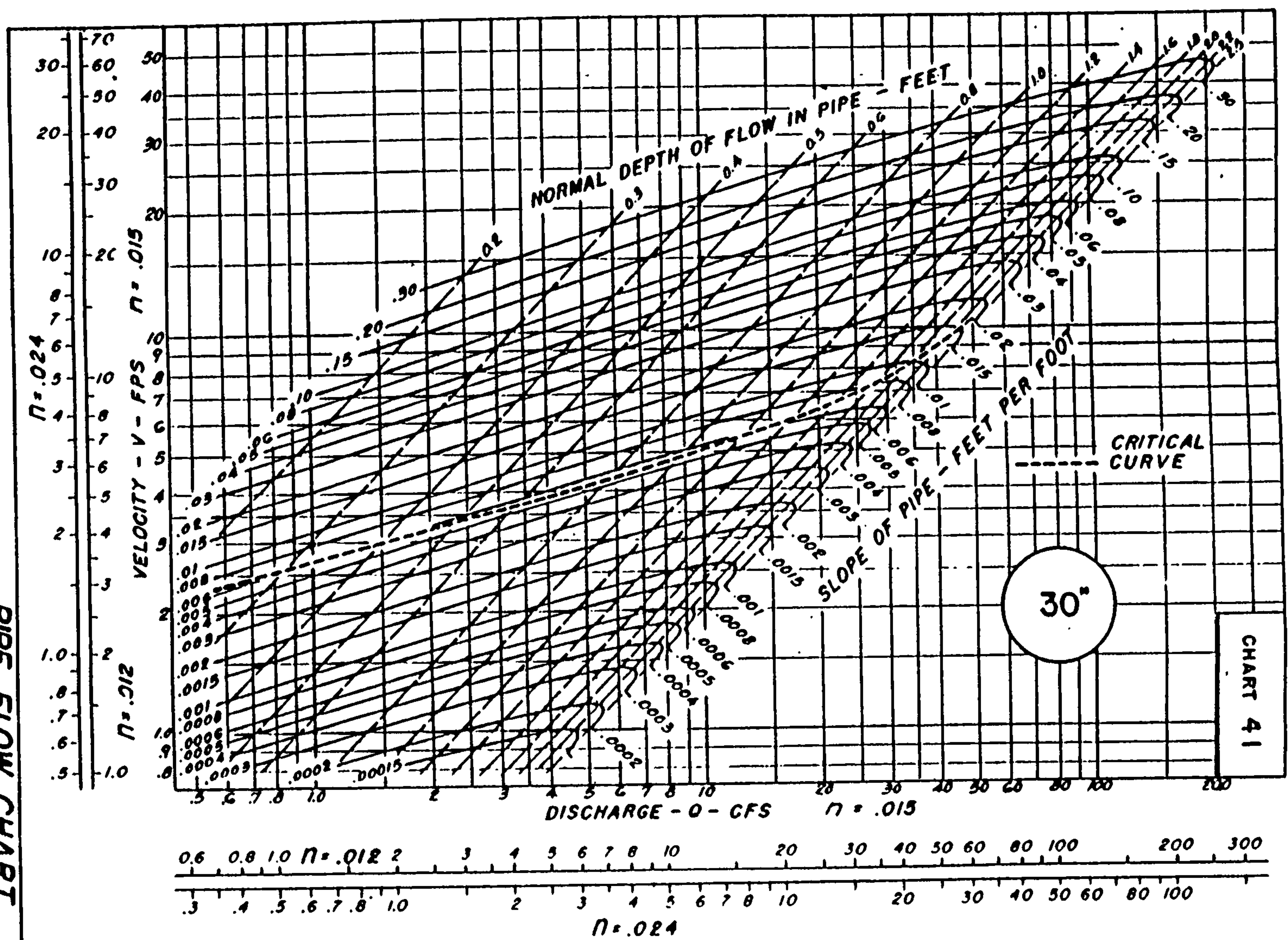
PIPE FLOW CHART
18-INCH DIAMETER



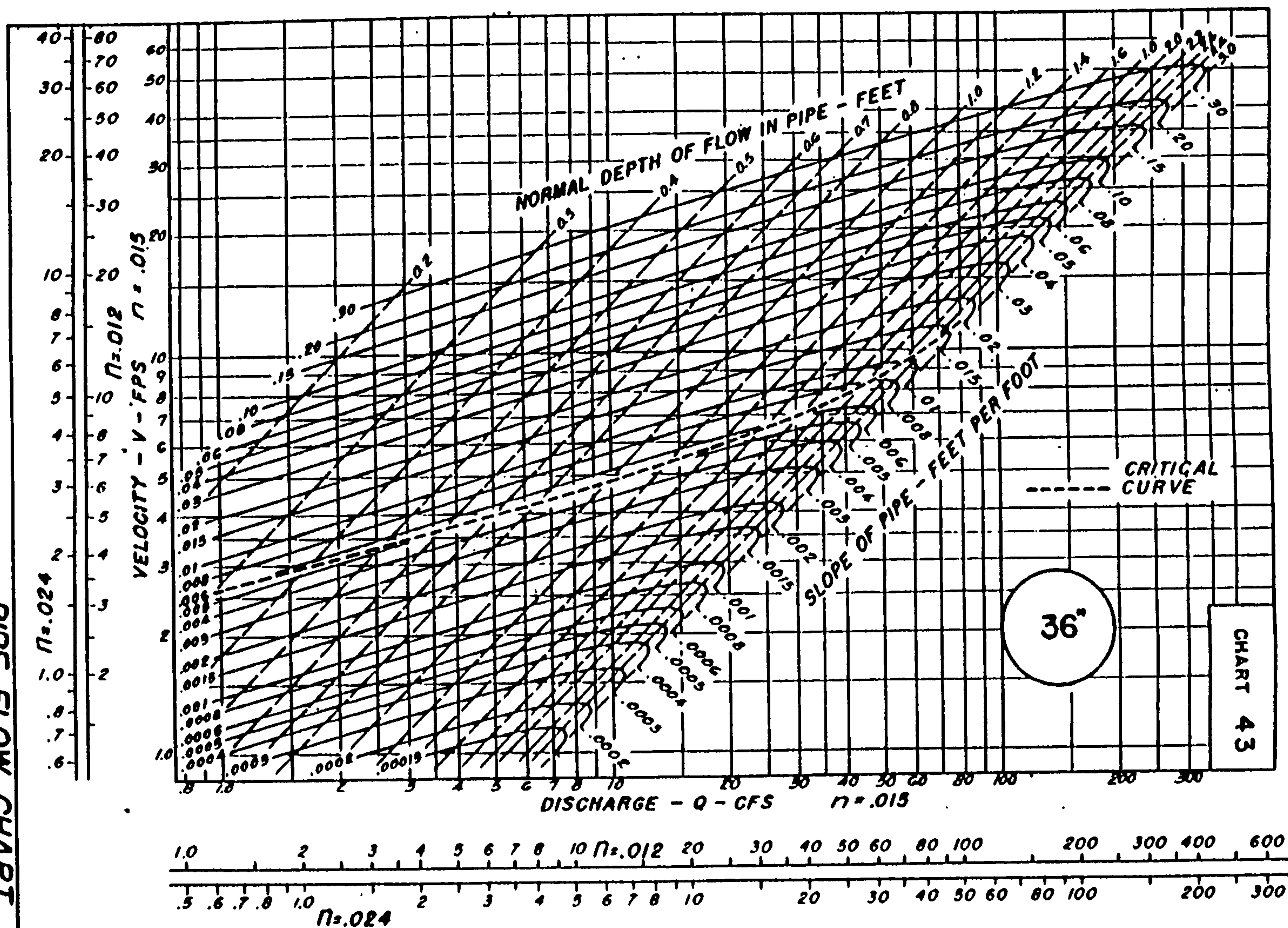
PIPE FLOW CHART
24-INCH DIAMETER



PIPE FLOW CHART
30-INCH DIAMETER



PIPE FLOW CHART
36-INCH DIAMETER



APPENDIX C
HYDRAULICS

1*****

* WATER SURFACE PROFILES

*

* U.S. ARMY CORPS OF ENGINEERS

*
* VERSION OF SEPTEMBER 1988
* THE HYDROLOGIC ENGINEERING CENTER *
* ERROR: 01,02
* 609 SECOND STREET, SUITE D *
* UPDATED: 4 APRIL 1989
* DAVIS, CALIFORNIA 95616-4687 *
* RUN DATE 9/11/97 TIME 20:52:46
* (916) 756-1104, (916) 551-1748 *

	X	X	XXXXXXXX	XXXXX	XXXXX
	X	X	X	X	X
X					
	X	X	X	X	
X					
	XXXXXXXX	XXXX	X	XXXXX	XXXXX
	X	X	X	X	X
	X	X	X	X	X
	X	X	XXXXXXXX	XXXXX	

XXXXXXXX

END OF BANNER

1

9/11/97 20:52:46

PAGE 1

Los Volcanes Ditch

THIS RUN EXECUTED 9/11/97 20:52:46

HEC2 RELEASE DATED SEP 88 UPDATED APR 1989

ERROR CORR - 01,02

MODIFICATION -

T1 CLIFFORD WEST BUSINESS PARK
T2 V-DITCH ON LOS VOLCANES ROAD
T3 100-YEAR / 6-HOUR DESIGN STORM

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q
WSEL	FQ							
	0	2	0	0	.01	0	0	0
	0							

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

43	1	2	26	4	68	3
----	---	---	----	---	----	---

NC	.025	.025	.025	.1	.3
----	------	------	------	----	----

QT	1	21.53
----	---	-------

X1 1 4 0 10.0 0 0 0
 0 0 0
 GR 1.0 0 0 3.0 0 7.0 1.0
 10.0
 1

9/11/97 20:52:46
 PAGE 2

SECNO	DEPTH	CWSEL	CRIWS	WSELK	EG	HV	HL	OLOSS	BANK
ELEV									
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	
LEFT/RIGHT									
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	
SSTA									
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	
ENDST									

*PROF 1

CCHV= .100 CEHV= .300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

1.00	.81	.81	.00	.00	1.08	.26	.00	.00
1.00	22.	0.	22.	0.	0.	5.	0.	0.
1.00	.00	.00	4.11	.00	.000	.025	.000	.00
.56	.010039	0.	0.	0.	0	0	6	.00
9.44								8.88

0

1

9/11/97 20:52:46
 PAGE 3

THIS RUN EXECUTED 9/11/97 20:52:46

HEC2 RELEASE DATED SEP 88 UPDATED APR 1989

ERROR CORR - 01,02

MODIFICATION -

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

100-YEAR / 6-HOUR DE

SUMMARY PRINTOUT

Q	CWSEL	CRIWS	VCH	TOPWID	FRCH	EG
21.530	.81	.00	4.11	8.88	.94	1.08

1

9/11/97 20:52:46
 PAGE 4

1*****
* WATER SURFACE PROFILES *
* VERSION OF SEPTEMBER 1988 *
* ERROR: 01,02 *
* UPDATED: 4 APRIL 1989 *
* RUN DATE 3/ 9/98 TIME 17:13:18 *

* U.S. ARMY CORPS OF ENGINEERS *
* THE HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104, (916) 551-1748 *

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      X      X XXXXXXXX XXXXX      XXXXX
      X      X X      X      X      X      X
      X      X X      X      X      X
      XXXXXXXX XXXX      X      XXXXX XXXXX
      X      X X      X      X      X
      X      X X      X      X      X
      X      X XXXXXXXX XXXXX      XXXXXXXX

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3/ 9/98 17:13:18

PAGE

STREET CAPACITY CALCULATIONS

THIS RUN EXECUTED 3/ 9/98 17:13:18

HEC2 RELEASE DATED SEP 88 UPDATED APR 1989

ERROR CORR - 01,02
MODIFICATION -

T1 OLIVER ROSS ROAD CAPACITY CALCULATIONS
T2 40' FF W/ 8" STD CURB SUB-CRITICAL FLOW
T3 FILE:40FFCLIF.DAT (100-YR 6-HR STORM)

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	0	2	0	1	.0154	0	0	0	0	0

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

	43	1	2	26	4	68	3			
NC	.017	.017	.017	.1	.3					
QT	5	7.88	4.24	12.81	5.21	5.69				
X1	1	9	0	60	0	0	0	0	0	0
GR	1.0	0	.67	9.9	0	10	.125	12	.40	30
GR	.125	48	0	50	.67	50.1	1.0	60		

3/ 9/98 17:13:18

PAGE 2

SECNO	DEPTH	CWSEL	CRIWS	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 1

CCHV= .100 CEHV= .300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

3265 DIVIDED FLOW

1.00	.31	.31	.33	.00	.40	.10	.00	.00	1.00
8.	0.	8.	0.	0.	3.	0.	0.	0.	1.00
.00	.00	2.50	.00	.000	.017	.000	.000	.00	9.95
.015296	0.	0.	0.	0	23	7	.00	27.90	50.05

0

1

3/ 9/98 17:13:18

PAGE 3

T1 SAUL BELL ROAD

T2 100YR 6HR

T3 40FF STD

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	0	3	0	0	.006					
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	2	0	-1	0	0	0	0	0	0	0

1

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PAGE 4

SECNO	DEPTH	CWSEL	CRIWS	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 2

CCHV= .100 CEHV= .300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

3265 DIVIDED FLOW

1.00	.29	.29	.00	.00	.33	.03	.00	.00	1.00
4.	0.	4.	0.	0.	3.	0.	0.	0.	1.00
.00	.00	1.50	.00	.000	.017	.000	.000	.00	9.96
.005931	0.	0.	0.	0	0	7	.00	26.29	50.04

0
1

3/ 9/98 17:13:18

PAGE 5

T1 BLUEWATER
T2 100YR 6HR
T3 40FF STD

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	0	4	0	1	.020					
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	3	0	-1	0	0	0	0	0	0	

1

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PAGE 6

SECNO	DEPTH	CWSEL	CRIWS	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 3

CCHV= .100 CEHV= .300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

3265 DIVIDED FLOW

1.00	.34	.34	.39	.00	.49	.15	.00	.00	1.00
13.	0.	13.	0.	0.	4.	0.	0.	0.	1.00
.00	.00	3.10	.00	.000	.017	.000	.000	.00	9.95
.019969	0.	0.	0.	0	16	7	.00	32.13	50.05

0
1

3/ 9/98 17:13:18

PAGE 7

T1 BLUEWATER
T2 100YR 6HR
T3 40FF STD

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	0	5	0	0	.005					
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	4	0	-1	0	0	0	0	0	0	0

1
3/ 9/98 17:13:18

PAGE 8

SECNO	DEPTH	CWSEL	CRISW	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 4

CCHV= .100 CEHV= .300
*SECNO 1.000
2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

3265 DIVIDED FLOW

1.00	.32	.32	.00	.00	.35	.03	.00	.00	1.00
5.	0.	5.	0.	0.	4.	0.	0.	0.	1.00
.00	.00	1.48	.00	.000	.017	.000	.000	.00	9.95
.004981	0.	0.	0.	0	0	7	.00	29.60	50.05

0
1
3/ 9/98 17:13:18

PAGE 9

T1 BLUEWATER
T2 100YR 6HR
T3 40FF STD

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	0	6	0	1	.010					
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	5	0	-1	0	0	0	0	0	0	0

1

3/ 9/98 17:13:18

PAGE 10

SECNO	DEPTH	CWSEL	CRIWS	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 5

CCHV= .100 CEHV= .300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

3265 DIVIDED FLOW

1.00	.30	.30	.30	.00	.36	.06	.00	.00	1.00
6.	0.	6.	0.	0.	3.	0.	0.	0.	1.00
.00	.00	1.96	.00	.000	.017	.000	.000	.00	9.96
.009899	0.	0.	0.	0	14	7	.00	26.70	50.04

0

1

3/ 9/98 17:13:18

PAGE 11

THIS RUN EXECUTED 3/ 9/98 17:13:18

 HEC2 RELEASE DATED SEP 88 UPDATED APR 1989

ERROR CORR - 01,02

MODIFICATION -

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

FILE:40FFCLIF.DAT (1

SUMMARY PRINTOUT

Q	CWSEL	CRIWS	VCH	TOPWID	FRCH	EG
7.880	.31	.33	2.50	27.90	1.57	.40
4.240	.29	.00	1.50	26.29	1.00	.33
12.810	.34	.39	3.10	32.13	1.71	.49

5.210	.32	.00	1.48	29.60	.88	.35
5.690	.30	.30	1.96	26.70	1.28	.36

1

3/ 9/98 17:13:18

PAGE 12

SUMMARY OF ERRORS AND SPECIAL NOTES

1*****

* WATER SURFACE PROFILES *
U.S. ARMY CORPS OF ENGINEERS *
* VERSION OF SEPTEMBER 1988 *
THE HYDROLOGIC ENGINEERING CENTER *
* ERROR: 01,02 *
609 SECOND STREET, SUITE D *
* UPDATED: 4 APRIL 1989 *
DAVIS, CALIFORNIA 95616-4687 *
* RUN DATE 9/12/97 TIME 11:48:41 *
(916) 756-1104, (916) 551-1748 *

X X XXXXXXX XXXXX XXXXX
X X X X X X X
X X X X X X
XXXXXXXX XXXX X XXXXX XXXXX
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXXXXXX

END OF BANNER
1
9/12/97 11:48:41
PAGE 1

TEMPORARY SWALE
THIS RUN
LOS VOLCANES RD.

EXECUTED 9/12/97 11:48:41

HEC2 RELEASE DATED SEP 88 UPDATED APR 1989

ERROR CORR - 01,02
MODIFICATION -

T1	CLIFFORD WEST BUSINESS PARK									
T2	V-DITCH ON LOS VOLCANES ROAD									
T3	100-YEAR / 6-HOUR DESIGN STORM									
J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0	0	2	0	0	.008	0	0	0	0	
J3	VARIABLE CODES FOR SUMMARY PRINTOUT									
	43	1	2	26	4	68	3			
NC	.025	.025	.025	.1	.3					
QT	1	21.53								
X1	1	4	0	12.0	0	0	0	0	0	
0	0	0								
GR	1.0	0	0	3.0	0	9.0	1.0	12.0		

1
9/12/97 11:48:41
PAGE 2

SECNO	DEPTH	CWSEL	CRIWS	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 1

CCHV= .100 CEHV= .300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

1.00	.73	.73	.00	.00	.93	.20	.00	.00	1.00
22.	0.	22.	0.	0.	6.	0.	0.	0.	1.00
.00	.00	3.62	.00	.000	.025	.000	.000	.00	.82
.008012	0.	0.	0.	0	0	6	.00	10.36	11.18

0

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9/12/97 11:48:41
PAGE 3

THIS RUN

EXECUTED 9/12/97 11:48:41

HEC2 RELEASE DATED SEP 88 UPDATED APR 1989

ERROR CORR - 01,02

MODIFICATION -

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

100-YEAR / 6-HOUR DE

SUMMARY PRINTOUT

Q	CWSEL	CRIWS	VCH	TOPWID	FRCH	EG
21.530	.73	.00	3.62	10.36	.84	.93

1

9/12/97 11:48:41
PAGE 4

SUMMARY OF ERRORS AND SPECIAL NOTES



D. Mark Goodwin & Associates, P.A.
Consulting Engineers and Surveyors

PROJECT Cl. Ford West B. Park
SUBJECT Hydrology
BY DLH DATE 9-12-97
CHECKED _____ DATE _____
SHEET _____ OF _____

Allowable Discharge Calculations

$$Q_{\text{allowable}} = 56.6 \text{ cfs}$$

$$\text{Total Area Unit 1, 2, 3} = 52.1054 \text{ acres}$$

$$\frac{56.6 \text{ cfs}}{52.1054} = 1.08625 \text{ cfs/acre}$$

$$\text{Unit 1 + 2} \quad 33.1363 \text{ acres} (1.08625 \text{ cfs/ac}) = 36.00 \text{ cfs}$$

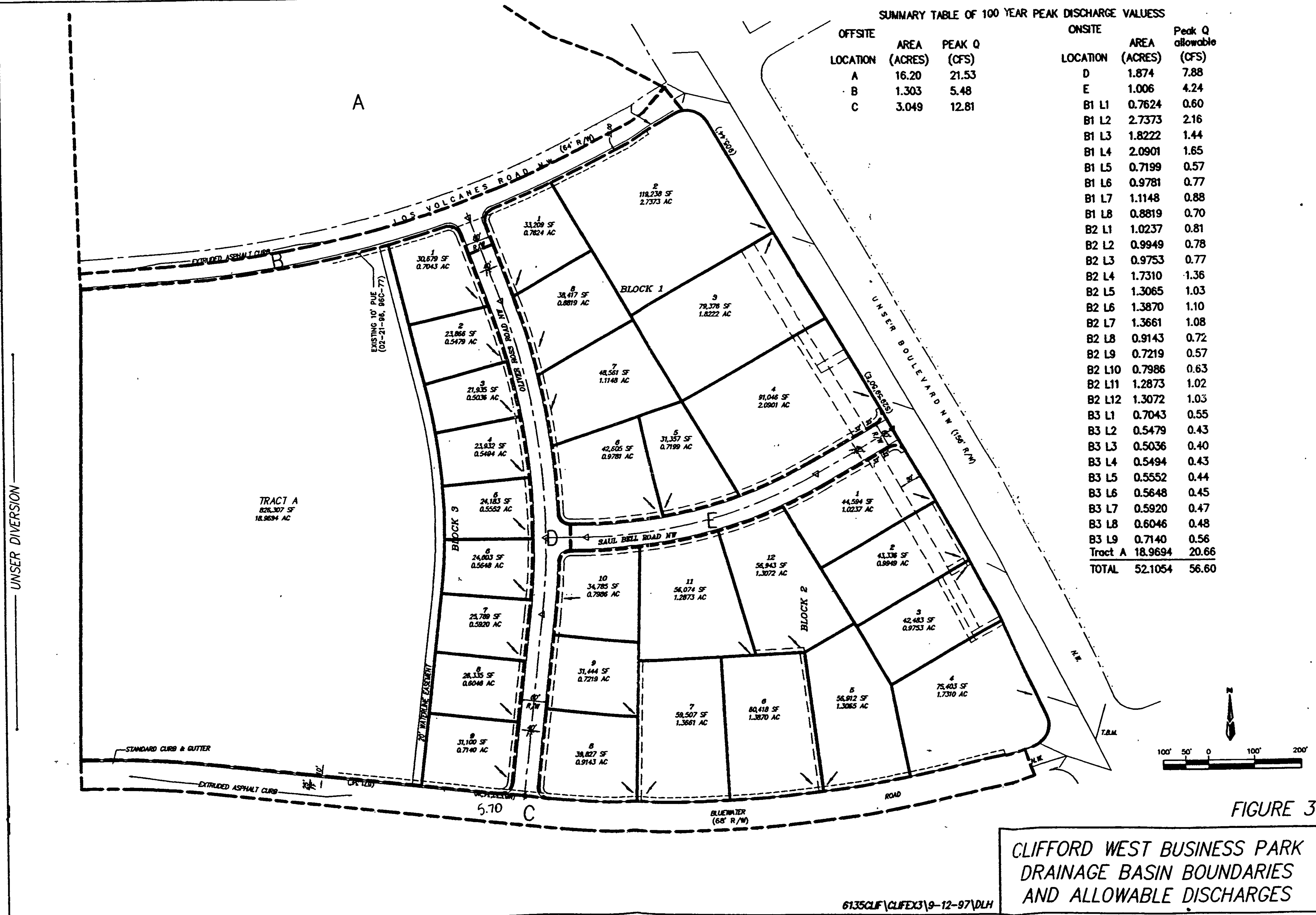
$$\text{Tract A} \quad 18.9694 \text{ acres} (1.08625 \text{ cfs/ac}) = 20.60 \text{ cfs}$$

Summation of Discharge Allowed From All lots
in Unit 1 + 2 =

$$\begin{array}{r} 36.00 \text{ cfs} \\ - 7.88 \text{ cfs Oliver Ross Rd} \\ - 4.24 \text{ cfs Saul Bell Rd.} \\ \hline \end{array}$$

$\Sigma Q_{\text{allowable all Lots Unit 1+2}} \rightarrow 23.88 \text{ cfs}$
 $\Sigma \text{Lot Areas} = 30.2563 \text{ ac.}$

$$Q_{\text{allowable (lots)}} = \frac{23.88 \text{ cfs}}{30.2563 \text{ ac}} = \boxed{0.789257 \text{ cfs/ac}}$$



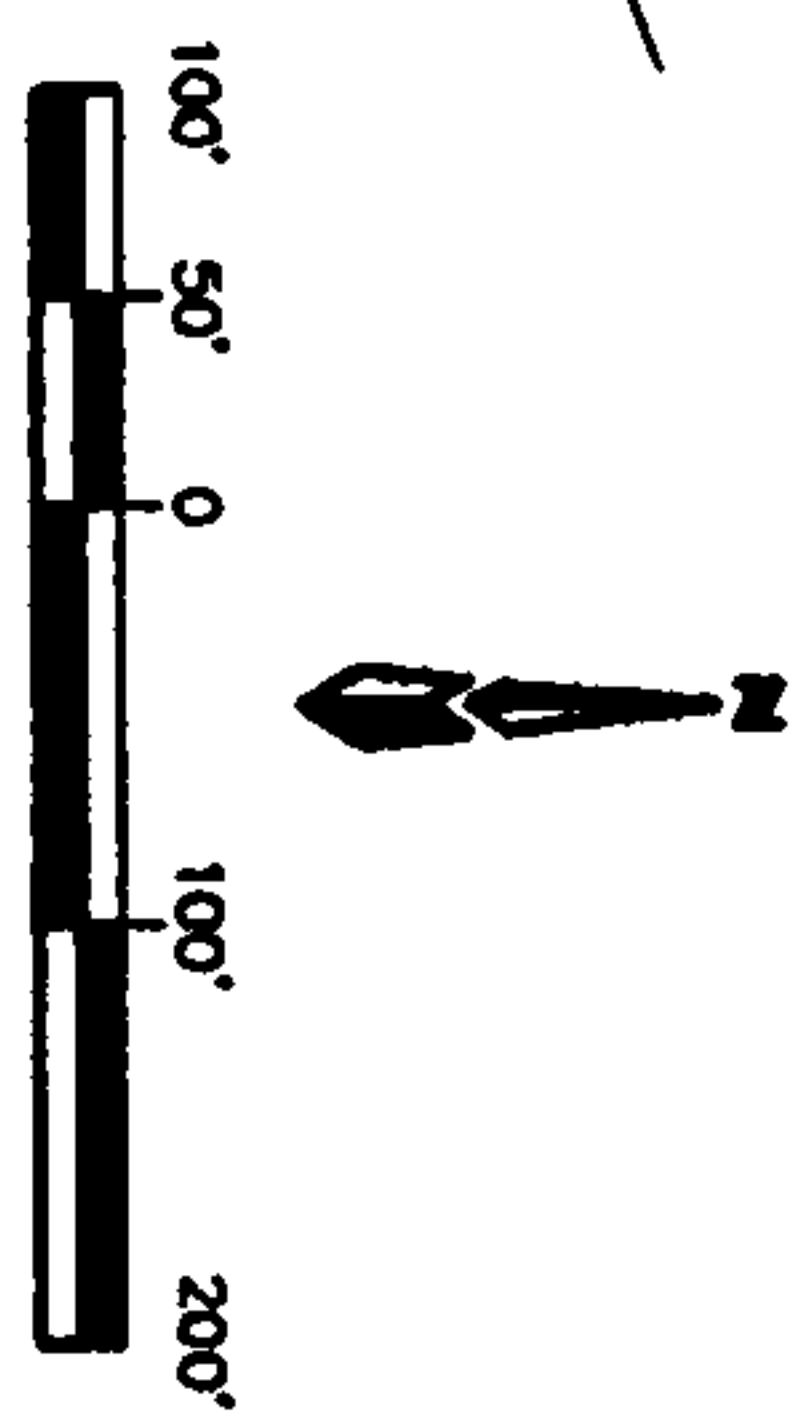
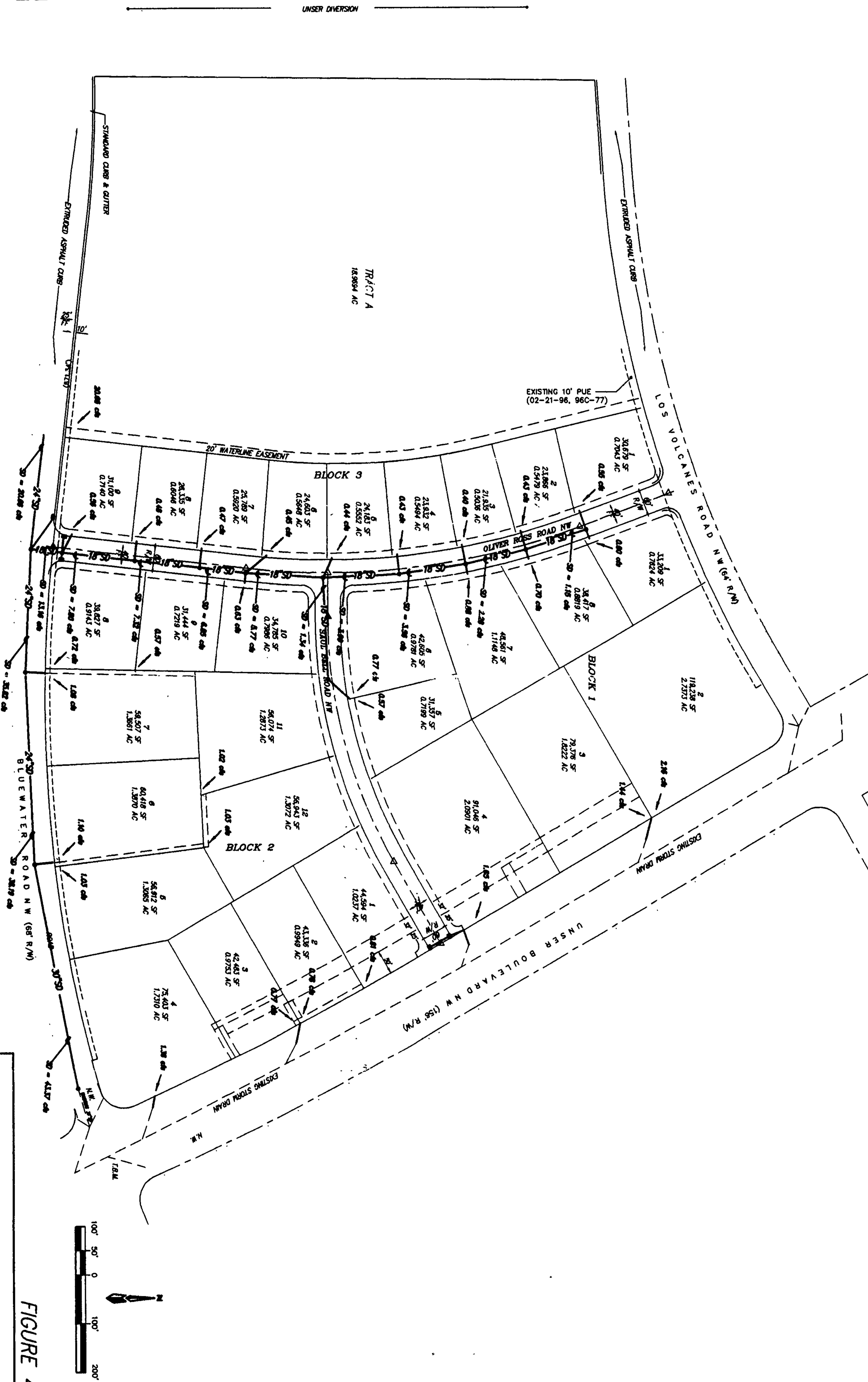


FIGURE 4

CLIFFORD WEST BUSINESS PARK
STORM DRAIN SCHEMATIC

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