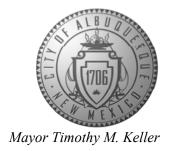
# CITY OF ALBUQUERQUE

Planning Department Brennon Williams, Director



May 18, 2021

Ronald Bohannan, P.E. Tierra West, LLC 5571 Midway Park Place NE Albuquerque, NM 87109

RE: **Southern Tire Mart** 

> **Grading and Drainage Plan** Engineer's Stamp Date: 03/29/21

Hydrology File: K09D047

Dear Mr. Bohannan:

PO Box 1293

Albuquerque

NM 87103

www.cabq.gov

Based upon the information provided in your submittal received 05/04/2021, the Grading & Drainage Plan is approved for Building Permit, Work Order, and for action by the DRB on Site Plan for Building Permit.

Please attach a copy of this approved plan in the construction sets for Building Permit processing along with a copy of this letter. Prior to approval in support of Permanent Release of Occupancy

by Hydrology, Engineer Certification per the DPM checklist will be required.

As a reminder, if the project total area of disturbance (including the staging area and any work within the adjacent Right-of-Way) is 1 acre or more, then an Erosion and Sediment Control

(ESC) Plan and Owner's certified Notice of Intent (NOI) is required to be submitted to the Stormwater Quality Engineer (Doug Hughes, PE, jhughes@cabq.gov, 924-3420) 14 days prior to

any earth disturbance.

If you have any questions, please contact me at 924-3995 or rbrissette@cabq.gov.

Sincerely,

Renée C. Brissette, P.E. CFM Senior Engineer, Hydrology

Renée C. Brissette

Planning Department



# City of Albuquerque

#### Planning Department

#### Development & Building Services Division

#### DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 6/2018)

Project Title: Southern Tire Mart	Building	Permit #:	Hydrology File #:
DRB#:	EPC#:		Work Order#:
Legal Description: Tract 2B Avalon Subdivision			
City Address: Daytona Rd NW Albuquerque N		•	
in Traditions — The Tradition of the Tra			
Applicant: Tierra West, LLC			Contact: Vince Carrica
Address: 5571 Midway Park Place NE Albuquerg	que NM 87	109	
Phone#: 505-858-3100	Fax#:	505-858-1118	E-mail: vcarrica@tierrawestllc.com
Other Contact:			Contact:
Address:			
Phone#:			
TYPE OF DEVELOPMENT: PLAT (	# of lots)	RESIDENCE	X DRB SITE ADMIN SITE
IS THIS A RESUBMITTAL? Yes	X]	No	
DED A DEL MENTE. ED A NODODE A EKON	V 1		A CIE
<b>DEPARTMENT</b> TRANSPORTATION	<u> </u>	HYDROLOGY/DRAIN.	AGE
Check all that Apply:		TYPE OF API	PROVAL/ACCEPTANCE SOUGHT:
THE OF CHIPAMETAL		X BUILDIN	IG PERMIT APPROVAL
TYPE OF SUBMITTAL:	т	CERTIFIC	CATE OF OCCUPANCY
ENGINEER/ARCHITECT CERTIFICATION	N		
PAD CERTIFICATION		PRELIMI	NARY PLAT APPROVAL
CONCEPTUAL G & D PLAN		SITE PLA	AN FOR SUB'D APPROVAL
X GRADING PLAN		X SITE PLA	AN FOR BLDG. PERMIT APPROVAL
X DRAINAGE REPORT		FINAL P	LAT APPROVAL
DRAINAGE MASTER PLAN			
FLOODPLAIN DEVELOPMENT PERMIT A	APPLIC	SIA/ REL	LEASE OF FINANCIAL GUARANTEE
ELEVATION CERTIFICATE		FOUNDA	ATION PERMIT APPROVAL
CLOMR/LOMR		GRADIN	G PERMIT APPROVAL
TRAFFIC CIRCULATION LAYOUT (TCL)	)	SO-19 AI	PPROVAL
TRAFFIC IMPACT STUDY (TIS)		PAVING	PERMIT APPROVAL
STREET LIGHT LAYOUT		GRADIN	G/ PAD CERTIFICATION
OTHER (SPECIFY)	_	WORK O	RDER APPROVAL
PRE-DESIGN MEETING?		CLOMR/	LOMR
		FLOODP	LAIN DEVELOPMENT PERMIT
		OTHER (	(SPECIFY)
DATE SUBMITTED: 3/30/2021	By: _	Vince Carrica	
COA STAFF:	ELECTRO	ONIC SUBMITTAL RECEIVE	ED:

FEE PAID:\_\_\_\_

#### DRAINAGE REPORT

For

# TRACT 2B AVALON SUBDIVISION UNIT 5 ALBUQUERQUE, NEW MEXICO

Prepared by

Tierra West, LLC 5571 Midway Park Place NE Albuquerque, New Mexico 87109

Prepared for

Southern Tire Mart Albuquerque, NM

March 29, 2021

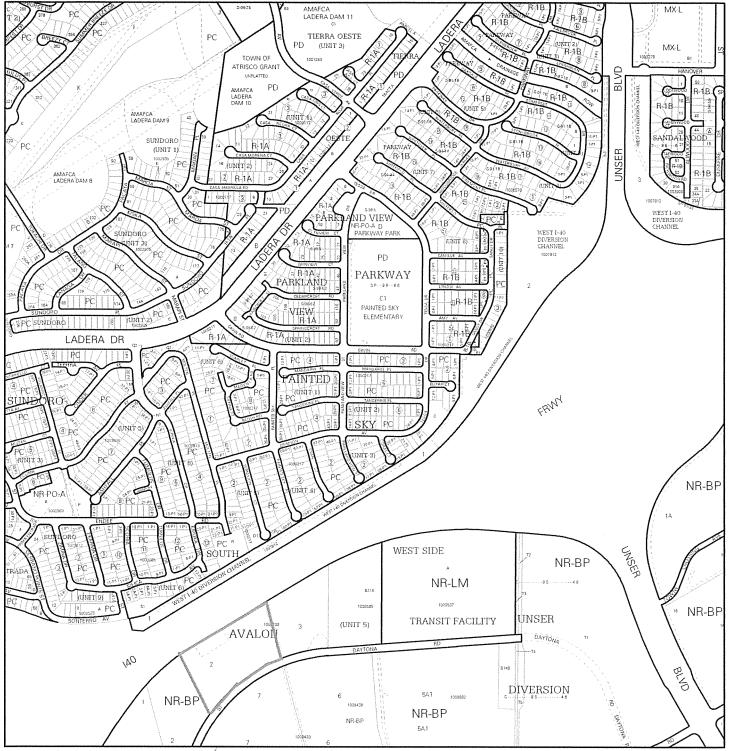




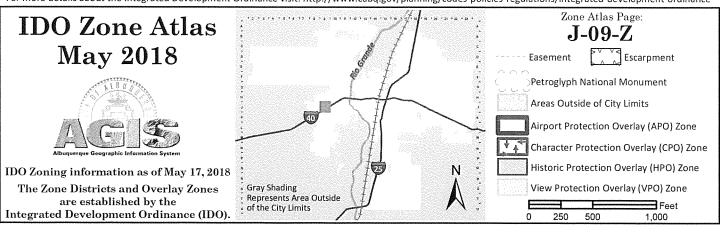
RONALD R BOHANNAN, PE #7868

#### TABLE OF CONTENTS

Zone Atlas Map J-09	1
Location	2
Drainage Basin Designation	2
Existing Drainage Conditions	2
FIRM Map	2
Design Criteria	3
Developed Drainage Conditions	3
Basin Map Proposed Conditions	4
Summary	3
Weighted E Table	5
GRADING AND DRAINAGE PLAN MAP PO	CKET



For more details about the Integrated Development Ordinance visit: http://www.cabq.gov/planning/codes-policies-regulations/integrated-development-ordinance



#### LOCATION

The proposed commercial development is located off Daytona Rd south of Interstate 40 and west of Unser Blvd in southwest Albuquerque. It is comprised of approximately 5.8255 acres zoned NRBP. This report represents a drainage management and grading plan for approval by the City of Albuquerque, for grading and Building Permit submittal.

#### **DRAINAGE BASIN DESIGNATION**

The drainage basins for proposed conditions are as indicated on the BASIN MAP included in this report. The site is broken into ten onsite drainage basins.

#### **EXISTING DRAINGE CONDITIONS**

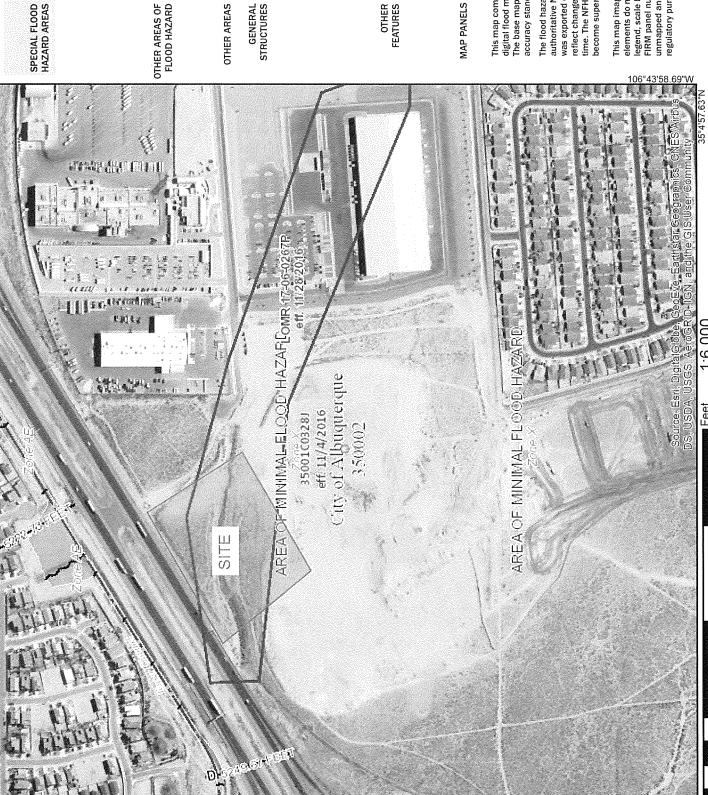
The site is currently vacant with the exception of a roadway turnaround. It is a part of Master Drainage Report for Westpoint 40 (Avalon Subdivision Unit 5) by BHI dated July 2019. It drains predominantly northwest to southeast and is elevated approximately twenty feet above the developed property to the east. An existing drainage way and desilting pond exists in the northeast corner of the site that channels runoff from the Interstate to an existing storm drain in the adjacent property. Runoff from north of the upland is captured in the AMAFCA North I-40 Diversion system. That diversion system removes the bulk of the contributing area to the two arroyos that run diagonally through the site from northwest to south east. Runoff from the existing site is conveyed to the Unser Diversion Pond system via street flow and an existing storm drain in Daytona Rd.

#### FIRM MAP

AMAFCA completed a LOMR to adjust the FEMA mapping for this area (LOMR 17-06-0267P Effective 11/28/2016). The site is no longer located in a designated Flood Hazard Zone Map No. 35001C0328J dated 11/4/2016.

# National Flood Hazard Layer FIRMette





# Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

Regulatory Floodway Zone AE, AO, AH, VE, AF Without Base Flood Elevation (BFE) SPECIAL FLOOD HAZARD AREAS 0.2% Annual Chance Flood Hazard, Area depth less than one foot or with drainag of 1% annual chance flood with average areas of less than one square mile Zone. Future Conditions 1% Annual Chance Flood Hazard Zone X

Area with Flood Risk due to Levee Zone D Area with Reduced Flood Risk due to Levee. See Notes, Zone x

NO SCREEN

Area of Minimal Flood Hazard Zone **Effective LOMRs** 

Area of Undetermined Flood Hazard Zon

Channel, Culvert, or Storm Sewer GENERAL ---- Channel, Culvert, or Storm STRUCTURES INNINININ Levee, Dike, or Floodwall Cross Sections with 1% Annual Chance Water Surface Elevation

Base Flood Elevation Line (BFE)

Jurisdiction Boundary

Coastal Transect Baseline OTHER FEATURES

Hydrographic Feature Profile Baseline

Digital Data Available

No Digital Data Available Unmapped This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The base map shown complies with FEMA's base map

reflect changes or amendments subsequent to this date and The flood hazard information is derived directly from the become superseded by new data over time. This map image is void if the one or more of the following map elements do not appear: base map imagery, flood zone labels,

1,500

1,000

500

#### **DESIGN-CRITERIA**

The drainage plan presented in this report was prepared in accordance with the City of Albuquerque Drainage Ordinances and Chapter 22 of the Development Process Manual DPM. The hydrological analysis is based on the 100-year frequency, 6-hour duration storm, as Represented in Section 22, Part A, Hydrology, of the Development Process Manual. The plan will also include retention of the first flush in on-site landscaped areas. See attached Weighted E Table for excess precipitation values calculated for this site.

#### **DEVELOPED-DRAINAGE CONDITIONS**

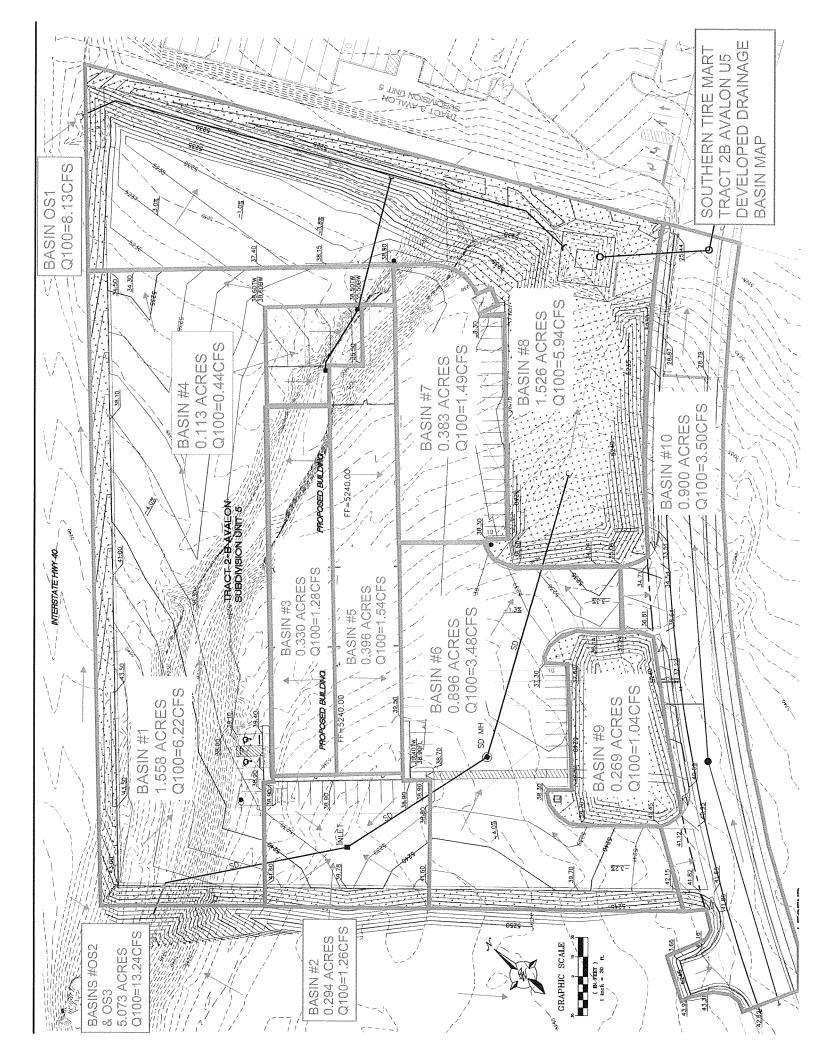
The site is proposed to be developed with a single user, Southern Tire Mart. In coordination with the landowner to the west, a drainage culvert will be constructed to intercept undeveloped upland flows to the west prior to them entering the site. Also, no offsite drainage will enter the site from the north, east and south with the exception of the runoff from a portion of the adjacent Interstate 40 right of way, which will be conveyed in a storm drain culvert from the northeast corner of the site to the proposed water quality pond on site. The onsite water quality pond will free discharge to Daytona roadway and existing storm drain and will be conveyed to the Unser Diversion Pond system located east of the site. Flows will be conveyed through the site via surface flows and a small onsite storm drains. Runoff will then flow to a shallow first flush retention pond before existing the site.

Refer to enclosed Weighted E computation spreadsheet for existing and developed. Storm drain capacities are listed in a table in the appendix.

#### **SUMMARY**

The proposed grading and drainage plan for the proposed development of the existing undeveloped property includes surface flows and an onsite storm drain to convey runoff to a water quality pond. The flows will be routed through first flush pond located in landscaped areas prior to the flows exiting the site to the Daytona right of way. Once in the right of way, flows will be routed to the Unser Diversion Pond system via street flow and an existing storm drain

channel located in Daytona Rd. The storm drain capacity downstream of the site is sufficient to carry the ultimate developed runoff of 52.6 cfs outlined in the I-40 South and Unser Diversion Mini DMP (see attached Plate 2 from the plan).



# Weighted E Method

Zone #1 Developed Basins

	Flow	cfs	6.33	1.19	1.44	0.50	1.73	3.77	1.68	3.28	0.55	3.50	8.13	10.58	2.66		45.32	
100-Year	Volume	(ac-ft)	0.234	0.044	0.054	0.019	0.065	0.140	0.063	0.091	0.015	0.124	0.249	0.347	0.088		1.532	
	Weighted E	(ac-ft)	1.801	1.788	1.970	1.970	1.970	1.879	1.970	0.715	0.670	1.656	0.891	1.112	0.792			
	Treatment D	(acres)	1.355	0.253	0.330	0.113	0.396	0.833	0.383	0.000	0.000	0.612	0.570	1.273	0.306	· · · · · · · · · · · · · · · · · · ·	6.423	
	Treatr	%	87%	%98	100%	100%	100%	93%	100%	%0	%0	%89	17%	34%	23%	**************************************		
	Treatment C	(acres)	0	0	0	0	0	0	0	0.213625	0	0.287912	0	0	0			
	Treatr	%	%0	%0	%0	%0	%0	%0	%0	14%	%0	32%	%0	%0	%0			
	Treatment B	(acres)	0.203	0.041	0.000	0.000	0.000	0.063	0.000	1.312	0.269	0.000	2.781	2.471	0.000			
	Treatr	%	13%	14%	%0	%0	%0	7%	%0	%98	100%	%0	83%	%99	%0			
	reatment A	(acres)	0	0	0	0	0	0	0	0	0	0	0	0	1.023326			
	Treatr	%	%0	%0	%0	%0	%0	%0	%0	%0	%0	%0	%0	%0	%22			
	Area	(sd miles)	0.00243	0.00046	0.00051	0.00018	0.00062	0.00140	09000.0	0.00238	0.00042	0.00141	0.00523	0.00585	0.00208		0.02357	
	Area	(acres)	1.558	0.294	0.330	0.113	968.0	0.896	0.383	1.526	0.269	0.900	3.350	3.744	1.329		15.087	
	Area	(sf)	67855.00	12799.00	14356.00	4938.00	17256.00	39017.00	16702.00	66468.00	11698.00	39192.00	145926.00	163088.00	57891.00		657186.00	
	Basin		1	2	3	4	2	9		ω	6	10	0S-1	OS-2	OS-3		Total	

# Equations:

FIRST FLUSH VOLUME = 9,793 CU.FT.

Volume = Weighted D \* Total Area

Weighted E = Ea\*Aa + Eb\*Ab + Ec\*Ac + Ed\*Ad / (Total Area)

Flow = Qa \* Aa + Qb \* Ab + Qc \* Ac + Qd \* Ad

#### **VOLUME CALCULATIONS**

# SOUTHERN TIRE MART DETENTION POND W/ 1ST FLUSH RETENTION

Ab - Bottom Of The Pond Surface Area

At - Top Of The Pond Surface Area

D - Water Depth

Dt - Total Pond Depth

C - Change In Surface Area / Water Depth

			·
ACTUAL	DEPTH	VOLUME	Q
ELEV.	(FT)	(AC-FT)	(CFS)
5222.00	0	0	0.000
5223.00	1.00	0.0960	0.000
5224.00	2.00	0.2272	0.000
5225.00	3.00	0.4030	0.000
5226.00	4.00	0.6406	0.000
5227.00	5.00	0.9682	5.090
5228.00	6.00	1.4080	6.017
5229.00	7.00	1.4080	10.421

#### Orifice Equation

Q(CFS)=

$$Q = CA SQRT(2gH)$$

Flow

\*

RAINFALL

TYPE=2 RAIN QUARTER=0.0 IN
RAIN ONE=1.87 IN RAIN SIX=2.20 IN
RAIN DAY=2.66 IN DT=0.05 HR

24-HOUR RAINFALL DIST. - BASED ON NOAA ATLAS 14 FOR CONVECTIVE AREAS (NM & AZ) - D1

DT = 0.050000 HOURS END TIME = 24.000002 HOURS 0.0000 0.0022 0.0045 0.0069 0.0096 0.0123 0.0154 0.0197 0.0264 0.0336 0.0412 0.0494 0.0578 0.0664 0.0753 0.0844 0.0946 0.1052 0.1168 0.1387 0.1657 0.2020 0.2430 0.2937 0.3614 0.4375 0.5689 0.7733 1.1234 1.3695 1.5635 1.6610 1.7465 1.8079 1.8568 1.8994 1.9306 1.9592 1.9828 1.9979 2.0087 2.0183 2.0273 2.0352 2.0426 2.0499 2.0568 2.0625 2.0659 2.0692 2.0724 2.0754 2.0784 2.0813 2.0842 2.0870 2.0896 2.0923 2.0949 2.0974 2.0999 2.1023 2.1046 2.1069 2.1092 2.1115 2.1136 2.1158 2.1179 2.1199 2.1220 2.1240 2.1260 2.1280 2.1299 2.1318 2.1337 2.1356 2.1374 2.1392 2.1411 2.1428 2.1446 2.1463 2.1481 2.1498 2.1514 2.1531 2.1548 2.1564 2.1580 2.1596 2.1612 2.1628 2.1643 2.1658 2.1674 2.1689 2.1704 2.1718 2.1733 2.1747 2.1762 2.1776 2.1790 2.1804 2.1818 2.1832 2.1845 2.1859 2.1872 2.1885 2.1899 2.1912 2.1924 2.1937 2.1950 2.1963 2.1975 2.1988 2.2000 2.2013 2.2026 2.2038 2.2051 2.2064 2.2089 2.2102 2.2115 2.2077 2.2128 2.2141 2.2153 2.2166 2.2179 2.2192 2.2204 2.2217 2.2230 2.2243 2.2256 2.2268 2.2281 2.2294 2.2307 2.2319 2.2332 2.2345 2.2358 2.2371 2.2383 2.2396 2.2409 2.2422 2.2434 2.2447 2.2460 2.2473 2.2486 2.2511 2.2498 2.2524 2.2537 2.2549 2.2562 2.2575 2.2588 2.2601 2.2613 2.2626 2.2639 2.2652 2.2664 2.2677 2.2690 2.2703 2.2716 2.2728 2.2741 2.2754 2.2767 2.2779 2.2792 2.2805 2.2818 2.2831 2.2843 2.2856 2.2869

```
2.2882
        2.2894
                 2.2907
                         2.2920
                                  2.2933
                                           2.2946
                                                   2.2958
        2.2984
                 2.2997
                         2.3009
                                  2.3022
                                           2.3035
                                                   2.3048
2.2971
2.3061
        2.3073
                 2.3086
                         2.3099
                                  2.3112
                                           2.3124
                                                   2.3137
                                           2.3214
2.3150
        2.3163
                 2.3176
                         2.3188
                                  2.3201
                                                   2.3227
2.3239
        2.3252
                 2.3265
                         2.3278
                                  2.3291
                                           2.3303
                                                   2.3316
2.3329
        2.3342
                 2.3354
                         2.3367
                                  2.3380
                                           2.3393
                                                   2.3406
        2.3431
2.3418
                 2.3444
                                  2.3469
                                           2.3482
                                                   2.3495
                         2.3457
2.3508
        2.3521
                 2.3533
                         2.3546
                                  2.3559
                                           2.3572
                                                   2.3584
        2.3610
                         2.3636
                                  2.3648
                                           2.3661
2.3597
                 2.3623
                                                   2.3674
        2.3699
                 2.3712
                         2.3725
                                  2.3738
                                           2.3750
                                                   2.3763
2.3687
2.3776
        2.3789
                 2.3802
                         2.3814
                                  2.3827
                                           2.3840
                                                   2.3853
        2.3878
                 2.3891
                         2.3904
                                  2.3917
                                           2.3929
2.3865
                                                   2.3942
2.3955
        2.3968
                 2.3980
                         2.3993
                                  2.4006
                                           2.4019
                                                   2.4032
                                           2.4108
2.4044
        2.4057
                 2.4070
                         2.4083
                                  2.4095
                                                   2.4121
2.4134
        2.4147
                 2.4159
                         2.4172
                                  2.4185
                                           2.4198
                                                   2.4210
                                                   2.4300
                 2.4249
                                           2.4287
2.4223
        2.4236
                         2.4262
                                  2.4274
2.4313
        2.4325
                 2.4338
                         2.4351
                                  2.4364
                                           2.4377
                                                   2.4389
2.4402
        2.4415
                 2.4428
                         2.4440
                                  2.4453
                                           2.4466
                                                   2.4479
2.4492
                                           2.4555
        2.4504
                 2.4517
                         2.4530
                                  2.4543
                                                   2.4568
2.4581
        2.4594
                 2.4607
                         2.4619
                                  2.4632
                                           2.4645
                                                   2.4658
2.4670
        2.4683
                 2.4696
                         2.4709
                                  2.4722
                                           2.4734
                                                   2.4747
2.4760
        2.4773
                 2.4785
                          2.4798
                                  2.4811
                                           2.4824
                                                   2.4837
2.4849
        2.4862
                 2.4875
                          2.4888
                                  2.4900
                                           2.4913
                                                   2.4926
2.4939
        2.4952
                 2.4964
                         2.4977
                                  2.4990
                                           2.5003
                                                   2.5015
                         2.5067
                                  2.5079
                                           2.5092
2.5028
        2.5041
                 2.5054
                                                   2.5105
2.5118
        2.5130
                 2.5143
                          2.5156
                                  2.5169
                                           2.5182
                                                   2.5194
2.5207
        2.5220
                 2.5233
                          2.5245
                                  2.5258
                                           2.5271
                                                   2.5284
2.5297
        2.5309
                 2.5322
                          2.5335
                                  2.5348
                                           2.5360
                                                   2.5373
                 2.5412
2.5386
        2.5399
                          2.5424
                                  2.5437
                                           2.5450
                                                   2.5463
2.5475
        2.5488
                 2.5501
                          2.5514
                                  2.5527
                                           2.5539
                                                    2.5552
                 2.5590
                          2.5603
                                  2.5616
2.5565
        2.5578
                                           2.5629
                                                    2.5642
2.5654
        2.5667
                 2.5680
                          2.5693
                                  2.5705
                                           2.5718
                                                   2.5731
2.5744
        2.5757
                 2.5769
                          2.5782
                                  2.5795
                                           2.5808
                                                   2.5820
2.5833
        2.5846
                 2.5859
                          2.5872
                                  2.5884
                                           2.5897
                                                    2.5910
2.5923
        2.5935
                 2.5948
                          2.5961
                                  2.5974
                                           2.5987
                                                    2.5999
                                  2.6063
2.6012
        2.6025
                 2.6038
                          2.6050
                                           2.6076
                                                    2.6089
2.6102
                 2.6127
                                  2.6153
        2.6114
                          2.6140
                                           2.6165
                                                    2.6178
2.6191
        2.6204
                 2.6217
                          2.6229
                                  2.6242
                                           2.6255
                                                    2.6268
                                  2.6332
                                           2.6344
2.6280
        2.6293
                 2.6306
                          2.6319
                                                    2.6357
2.6370
                 2.6395
                          2.6408
                                  2.6421
                                           2.6434
        2.6383
                                                    2.6447
2.6459
        2.6472
                 2.6485
                          2.6498
                                  2.6510
                                           2.6523
                                                   2.6536
        2.6562
                 2.6574
                          2.6587
2.6549
                                  2.6600
```

\*

\*BASIN 1

\*

COMPUTE NM HYD

ID=1 HYD NO=100.1 AREA=0.00243 SQ MI PER A=0.00 PER B=13.00 PER C=0.00 PER D=87.00 TP=-0.1333 HR MASS RAINFALL=-1 K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428

UNIT PEAK = 8.3466 CFS UNIT VOLUME = 0.9978 B = 526.28 P60 = 1.8700

AREA = 0.002114 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.130992HR TP = 0.133300HR K/TP RATIO = 0.982685 SHAPE CONSTANT, N = 3.593298

UNIT PEAK = 0.77513 CFS UNIT VOLUME = 0.9848 B = 327.08 P60 = 1.8700

AREA = 0.000316 SQ MI IA = 0.50000 INCHES INF = 1.25000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=1 CODE=1

#### PARTIAL HYDROGRAPH 100.10

RUNOFF VOLUME = 2.21066 INCHES = 0.2865 ACRE-FEET
PEAK DISCHARGE RATE = 6.56 CFS AT 1.500 HOURS BASIN AREA = 0.0024 SO. MI.

~

\*

\*BASIN 2

\*

COMPUTE NM HYD ID=2 HYD NO=100.2 AREA=0.00046 SQ MI
PER A=0.00 PER B=14.00 PER C=0.00 PER D=86.00
TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428

UNIT PEAK = 1.5618 CFS UNIT VOLUME = 0.9928 B = 526.28 P60 = 1.8700

AREA = 0.000396 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.130992HR TP = 0.133300HR K/TP RATIO = 0.982685 SHAPE

CONSTANT, N = 3.593298

UNIT PEAK = 0.15802 CFS UNIT VOLUME = 0.9156 B = 327.08

P60 = 1.8700

AREA = 0.000064 SQ MI IA = 0.50000 INCHES INF = 1.25000

INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=2 CODE=1

#### PARTIAL HYDROGRAPH 100.20

RUNOFF VOLUME = 2.19489 INCHES = 0.0538 ACRE-FEET
PEAK DISCHARGE RATE = 1.25 CFS AT 1.500 HOURS BASIN AREA = 0.0005 SQ. MI.

\*

\*

\*BASIN 3

\*

COMPUTE NM HYD ID=3 HYD NO=100.3 AREA=0.00051 SQ MI

PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00

TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE

CONSTANT, N = 7.106428

UNIT PEAK = 2.0135 CFS UNIT VOLUME = 0.9941 B = 526.28

P60 = 1.8700

AREA = 0.000510 SQ MI IA = 0.10000 INCHES INF = 0.04000

INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=3 CODE=1

#### PARTIAL HYDROGRAPH 100.30

RUNOFF VOLUME = 2.41566 INCHES = 0.0657 ACRE-FEET
PEAK DISCHARGE RATE = 1.47 CFS AT 1.500 HOURS BASIN AREA = 0.0005 SQ. MI.

\*

ж

\*BASIN 4

COMPUTE NM HYD ID=4 HYD NO=100.4 AREA=0.00018 SQ MI PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428

UNIT PEAK = 0.71065 CFS UNIT VOLUME = 0.9832 B = 526.28 P60 = 1.8700

AREA = 0.000180 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=4 CODE=1

PARTIAL HYDROGRAPH 100.40

RUNOFF VOLUME = 2.41566 INCHES = 0.0232 ACRE-FEET PEAK DISCHARGE RATE = 0.52 CFS AT 1.500 HOURS BASIN AREA = 0.0002 SQ. MI.

\*BASIN 5

COMPUTE NM HYD ID=5 HYD NO=100.5 AREA=0.00062 SO MI PER A=0.00 PER B=0.00 PER C=0.0 PER D=100.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428

UNIT PEAK = 2.4478 CFS UNIT VOLUME = 0.9951 B = 526.28 P60 = 1.8700

AREA = 0.000620 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=5 CODE=1

PARTIAL HYDROGRAPH 100.50

RUNOFF VOLUME = 2.41566 INCHES = 0.0799 ACRE-FEET PEAK DISCHARGE RATE = 1.78 CFS AT 1.500 HOURS BASIN AREA = 0.0006 SQ. MI.

\*

\*

\*BASIN 6

\*

COMPUTE NM HYD

ID=6 HYD NO=100.6 AREA=0.00140 SQ MI PER A=0.00 PER B=7.00 PER C=0.00 PER D=93.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649 HR TP = 0.133300 HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428

UNIT PEAK = 5.1404 CFS UNIT VOLUME = 0.9971 B = 526.28

P60 = 1.8700

AREA = 0.001302 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.130992HR TP = 0.133300HR K/TP RATIO = 0.982685 SHAPE CONSTANT, N = 3.593298

UNIT PEAK = 0.24047 CFS UNIT VOLUME = 0.9497 B = 327.08 P60 = 1.8700

AREA = 0.000098 SQ MI IA = 0.50000 INCHES INF = 1.25000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=6 CODE=1

PARTIAL HYDROGRAPH 100.60

RUNOFF VOLUME = 2.30527 INCHES = 0.1721 ACRE-FEET
PEAK DISCHARGE RATE = 3.89 CFS AT 1.500 HOURS BASIN AREA = 0.0014 SQ. MI.

\*

\*

\*BASIN 7

\*

COMPUTE NM HYD ID=7 HYD NO=100.7 AREA=0.00060 SQ MI
PER A=0.00 PER B=0.00 PER C=0.00 PER D=100.00
TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE

CONSTANT, N = 7.106428

UNIT PEAK = 2.3688 CFS UNIT VOLUME = 0.9951 B = 526.28

P60 = 1.8700

AREA = 0.000600 SQ MI IA = 0.10000 INCHES INF = 0.04000

INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=7 CODE=1

PARTIAL HYDROGRAPH 100.70

RUNOFF VOLUME = 2.41566 INCHES = 0.0773 ACRE-FEET PEAK DISCHARGE RATE = 1.72 CFS AT 1.500 HOURS BASIN AREA = 0.0006 SQ. MI.

\*BASIN 8

COMPUTE NM HYD

ID=8 HYD NO=100.8 AREA=0.00238 SO MI PER A=0.00 PER B=86.00 PER C=14.0 PER D=0.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.127474HR TP = 0.133300HR K/TP RATIO = 0.956297 SHAPE CONSTANT, N = 3.695096

UNIT PEAK = 5.9689 CFS UNIT VOLUME = 0.9992 B = 334.31

P60 = 1.8700

AREA = 0.002380 SQ MI IA = 0.47900 INCHES INF = 1.19120 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=8 CODE=1

PARTIAL HYDROGRAPH 100.80

RUNOFF VOLUME = 0.87123 INCHES = 0.1106 ACRE-FEET PEAK DISCHARGE RATE = 3.84 CFS AT 1.500 HOURS BASIN AREA = 0.0024 SO. MI.

\*BASIN 9

COMPUTE NM HYD ID=9 HYD NO=100.9 AREA=0.00042 SQ MI PER A=0.00 PER B=100.00 PER C=0.0 PER D=0.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.130992HR TP = 0.133300HR K/TP RATIO = 0.982685 SHAPE CONSTANT, N = 3.593298

UNIT PEAK = 1.0306 CFS UNIT VOLUME = 0.9885 B = 327.08 P60 = 1.8700

AREA = 0.000420 SQ MI IA = 0.50000 INCHES INF = 1.25000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=9 CODE=1

PARTIAL HYDROGRAPH 100.90

RUNOFF VOLUME = 0.83873 INCHES = 0.0188 ACRE-FEET PEAK DISCHARGE RATE = 0.66 CFS AT 1.500 HOURS BASIN AREA = 0.0004 SQ. MI.

\*BASIN 10

COMPUTE NM HYD ID=10 HYD NO=100.10 AREA=0.00141 SQ MI PER A=0.00 PER B=0.00 PER C=32.0 PER D=68.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428

UNIT PEAK = 3.7854 CFS UNIT VOLUME = 0.9966 B = 526.28

P60 = 1.8700

AREA = 0.000959 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.105867HR TP = 0.133300HR K/TP RATIO = 0.794199 SHAPE CONSTANT, N = 4.514592

UNIT PEAK = 1.3138 CFS UNIT VOLUME = 0.9928 B = 388.14

P60 = 1.8700

AREA = 0.000451 SQ MI IA = 0.35000 INCHES INF = 0.83000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =

PRINT HYD ID=9 CODE=1

#### PARTIAL HYDROGRAPH 100.90

RUNOFF VOLUME = 0.83873 INCHES = 0.0188 ACRE-FEET PEAK DISCHARGE RATE = 0.66 CFS AT 1.500 HOURS BASIN AREA = 0.0004 SQ. MI.

\*BASIN OS-1

COMPUTE NM HYD ID=11 HYD NO=100.11 AREA=0.00523 SQ MI PER A=0.00 PER B=83.00 PER C=0.0 PER D=17.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428

UNIT PEAK = 3.5102 CFS UNIT VOLUME = 0.9959 B = 526.28 P60 = 1.8700

AREA = 0.000889 SO MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.130992HR TP = 0.133300HR K/TP RATIO = 0.982685 SHAPE CONSTANT, N = 3.593298

UNIT PEAK = 10.651 CFS UNIT VOLUME = 0.9999 B = 327.08 P60 = 1.8700

AREA = 0.004341 SQ MI IA = 0.50000 INCHES INF = 1.25000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=11 CODE=1

#### PARTIAL HYDROGRAPH 100.11

RUNOFF VOLUME = 1.10681 INCHES = 0.3087 ACRE-FEET PEAK DISCHARGE RATE = 9.28 CFS AT 1.500 HOURS BASIN AREA = 0.0052 SQ. MI.

\*BASIN OS-2

COMPUTE NM HYD ID=12 HYD NO=100.12 AREA=0.00585 SQ MI PER A=0.00 PER B=66.00 PER C=0.0 PER D=34.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428

UNIT PEAK = 7.8527 CFS UNIT VOLUME = 0.9978 B = 526.28

P60 = 1.8700

AREA = 0.001989 SQ MI IA = 0.10000 INCHES INF = 0.04000

INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

 $\dot{K}$  = 0.130992HR TP = 0.133300HR K/TP RATIO = 0.982685 SHAPE CONSTANT, N = 3.593298

UNIT PEAK = 9.4739 CFS UNIT VOLUME = 0.9997 B = 327.08

P60 = 1.8700

AREA = 0.003861 SQ MI IA = 0.50000 INCHES INF = 1.25000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=12 CODE=1

PARTIAL HYDROGRAPH 100.12

RUNOFF VOLUME = 1.37488 INCHES = 0.4290 ACRE-FEET PEAK DISCHARGE RATE = 11.69 CFS AT 1.500 HOURS BASIN AREA = 0.0059 SQ. MI.

\*BASIN OS-3

COMPUTE NM HYD ID=13 HYD NO=100.13 AREA=0.00208 SQ MI

PER A=77.00 PER B=0.00 PER C=0.0 PER D=23.00

TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428

UNIT PEAK = 1.8887 CFS UNIT VOLUME = 0.9941 B = 526.28

P60 = 1.8700

AREA = 0.000478 SQ MI IA = 0.10000 INCHES INF = 0.04000

INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.163684HR TP = 0.133300HR K/TP RATIO = 1.227936 SHAPE CONSTANT, N = 2.899626

UNIT PEAK = 3.2866 CFS UNIT VOLUME = 0.9943 B = 273.54

P60 = 1.8700

AREA = 0.001602 SQ MI IA = 0.65000 INCHES INF = 1.67000

INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=13 CODE=1

#### PARTIAL HYDROGRAPH 100.13

ID=20 HYD NO=100.20 ID=20 ID=13

RUNOFF VOLUME = 1.03965 INCHES = 0.1153 ACRE-FEET PEAK DISCHARGE RATE = 3.13 CFS AT 1.500 HOURS BASIN AREA = 0.0021 SQ. MI.

ADD HYD

*						
ADD	HYD	ID=20	HYD	NO=100.20	ID=1	ID=2
ADD	HYD	ID=20	HYD	NO=100.20	ID=20	ID=3
ADD	HYD	ID=20	HYD	NO=100.20	ID=20	ID=4
ADD	HYD	ID=20	HYD	NO=100.20	ID=20	ID=5
ADD	HYD	ID=20	HYD	NO=100.20	ID=20	ID=6
ADD	HYD	ID=20	HYD	NO=100.20	ID=20	ID=7
ADD	HYD	ID=20	HYD	NO=100.20	ID=20	ID=8
ADD	HYD	ID=20	HYD	NO=100.20	ID=20	ID=9
ADD	HYD	ID=20	HYD	NO=100.20	ID=20	ID=11
ADD	HYD	ID=20	HYD	NO=100.20	ID=20	ID=12

\*

\*ROUTE BASIN 1 THRU 9 & OS-1,OS-2 & OS3 THROUGH WATER QUALITY POND

\*

DO	ITE	DECE	RVOTR
r		D.E.D.E	- ハソひょん

### ID=55 HYD NO=200.1 INFLOW ID=20 CODE=24 OUTFLOW (CFS) STORAGE(AC-FT) ELEVATION(FT

OUTFLOW	(CFS) STO	RAGE(AC-FT) ELEVAT	ELEVATION(FT)	
	0.000	0.0000	22.00	
	0.010	0.0960	23.00	
	0.020	0.2272	24.00	
	0.030	0.4030	25.00	
	0.040	0.6406	26.00	
	5.090	0.9682	27.00	
	6.017	1.4080	28.00	
	10.421	1.4080	29.00	

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
0.00 1.20	0.00 4.10	22.00 22.49	0.000 0.047	0.00 0.00
2.40	1.51	27.29	1.098	5.36
3.60	0.07	26.36	0.757	1.84
4.80 6.00	0.08 0.14	26.08 26.03	0.667 0.650	0.45 0.19
7.20	0.15	26.02	0.648	0.16
8.40	0.15	26.02	0.648	0.15
9.60	0.15	26.02	0.648	0.15
10.80 12.00	0.15 0.15	26.02 26.02	0.648 0.648	0.15 0.15
13.20	0.15	26.02	0.648	0.15
14.40	0.15	26.02	0.648	0.15
15.60	0.15	26.02	0.648	0.15
16.80	0.15	26.02	0.648	0.15
18.00 19.20	0.15 0.15	26.02 26.02	0.648 0.648	0.15 0.15
20.40	0.15	26.02	0.648	0.15
21.60	0.15	26.02	0.648	0.15
22.80	0.15	26.02	0.648	0.15

24.00	0.15	26.02	0.648	0.15
25.20	0.00	26.00	0.641	0.04
26.40	0.00	25.98	0.637	0.04
27.60	0.00	25.97	0.633	0.04
28.80	0.00	25.95	0.629	0.04
30.00	0.00	25.93	0.625	0.04
31.20	0.00	25.92	0.621	0.04
32.40	0.00	25.90	0.617	0.04
33.60	0.00	25.88	0.613	0.04
34.80	0.00	25.87	0.609	0.04
36.00	0.00	25.85	0.606	0.04
37.20	0.00	25.84	0.602	0.04
38.40	0.00	25.82	0.598	0.04
39.60	0.00	25.80	0.594	0.04
40.80	0.00	25.79	0.590	0.04
42.00	0.00	25.77	0.587	0.04
43.20	0.00	25.76	0.583	0.04
44.40	0.00	25.74	0.579	0.04
45.60	0.00	25.73	0.576	0.04
46.80	0.00	25.71	0.572	0.04
48.00	0.00	25.70	0.568	0.04
49.20	0.00	25.68	0.565	0.04
50.40	0.00	25.66	0.561	0.04
51.60	0.00	25.65	0.557	0.04
52.80	0.00	25.63	0.554	0.04
54.00	0.00	25.62	0.550	0.04
55.20	0.00	25.60	0.546	0.04
56.40	0.00	25.59	0.543	0.04
57.60	0.00	25.57	0.539	0.04
58.80	0.00	25.56	0.536	0.04
60.00	0.00	25.54	0.532	0.04
61.20	0.00	25.53	0.529	0.04
62.40	0.00	25.51	0.525	0.04
63.60	0.00	25.50	0.522	0.04
64.80	0.00	25.49	0.518	0.03
66.00	0.00	25.47	0.515	0.03
TIME	INFLOW	ELEV	VOLUME	OUTFLOW
(HRS)	(CFS)	(FEET)	(AC-FT)	(CFS)
67.20	0.00	25.46	0.511	0.03
68.40	0.00	25.44	0.508	0.03
69.60	0.00	25.43	0.505	0.03
70.80	0.00	25.41	0.501	0.03
72.00	0.00	25.40	0.498	0.03
73.20	0.00	25.39	0.494	0.03
74.40	0.00	25.37	0.491	0.03
75.60	0.00	25.36	0.488	0.03
76.80	0.00	25.34	0.484	0.03
78.00	0.00	25.33	0.481	0.03

79.20	0.00	25.32	0.478	0.03	
80.40	0.00	25.30	0.475	0.03	
81.60	0.00	25.29	0.471	0.03	
82.80	0.00	25.27	0.468	0.03	
84.00	0.00	25.26	0.465	0.03	
85.20	0.00	25.25	0.462	0.03	
86.40	0.00	25.23	0.458	0.03	
87.60	0.00	25.22	0.455	0.03	
88.80	0.00	25.21	0.452	0.03	
90.00	0.00	25.19	0.449	0.03	
91.20	0.00	25.18	0.446	0.03	
92.40	0.00	25.17	0.443	0.03	
93.60	0.00	25.15	0.439	0.03	
94.80	0.00	25.14	0.436	0.03	
96.00	0.00	25.13	0.433	0.03	
97.20	0.00	25.11	0.430	0.03	
98.40	0.00	25.10	0.427	0.03	
99.60	0.00	25.09	0.424	0.03	
100.80			0.421	0.03	
	0.00	25.08	0.421	0.03	
102.00	0.00	25.06 25.05	0.415	0.03	
103.20	0.00			0.03	
104.40	0.00	25.04	0.412	0.03	
105.60	0.00	25.02	0.409		
106.80	0.00	25.01	0.406	0.03	
108.00	0.00	25.00	0.403	0.03	
109.20	0.00	24.98	0.400	0.03	
110.40	0.00	24.97	0.397	0.03	
111.60	0.00	24.95	0.394	0.03	
112.80	0.00	24.93	0.391	0.03	
114.00	0.00	24.92	0.388	0.03	
115.20	0.00	24.90	0.385	0.03	
116.40	0.00	24.88	0.382	0.03	
117.60	0.00	24.87	0.380	0.03	
118.80	0.00	24.85	0.377	0.03	
120.00	0.00	24.83	0.374	0.03	
121.20	0.00	24.82	0.371	0.03	
122.40	0.00	24.80	0.368	0.03	
123.60	0.00	24.79	0.366	0.03	
124.80	0.00	24.77	0.363	0.03	
126.00	0.00	24.76	0.360	0.03	
127.20	0.00	24.74	0.357	0.03	
128.40	0.00	24.72	0.355	0.03	
129.60	0.00	24.71	0.352	0.03	
130.80	0.00	24.69	0.349	0.03	
132.00	0.00	24.68	0.347	0.03	
133.20	0.00	24.66	0.344	0.03	
TIME	INFLOW	ELEV	VOLUME	OUTFLOW	
(HRS)	(CFS)	(FEET)	(AC-FT)	(CFS)	
` ,	` '	, ,	,	` '	

134.40	0.00	24.65	0.341	0.03
135.60	0.00	24.63	0.339	0.03
136.80	0.00	24.62	0.336	0.03
138.00	0.00	24.60	0.333	0.03
139.20	0.00	24.59	0.331	0.03
140.40	0.00	24.58	0.328	0.03
141.60	0.00	24.56	0.326	0.03
142.80	0.00	24.55	0.323	0.03
144.00	0.00	24.53	0.321	0.03
145.20	0.00	24.52	0.318	0.03
146.40	0.00	24.50	0.316	0.03
147.60	0.00	24.49	0.313	0.02
148.80	0.00	24.48	0.311	0.02
150.00	0.00	24.46	0.308	0.02
151.20	0.00	24.45	0.306	0.02
152.40	0.00	24.43	0.303	0.02
153.60	0.00	24.42	0.301	0.02
154.80	0.00	24.41	0.299	0.02
156.00	0.00	24.39	0.296	0.02
157.20	0.00	24.38	0.294	0.02
158.40	0.00	24.37	0.292	0.02
159.60	0.00	24.35	0.289	0.02
160.80	0.00	24.34	0.287	0.02
162.00	0.00	24.33	0.285	0.02
163.20	0.00	24.31	0.282	0.02
164.40	0.00	24.30	0.280	0.02
165.60	0.00	24.29	0.278	0.02
166.80	0.00	24.27	0.275	0.02
168.00	0.00	24.26	0.273	0.02
169.20	0.00	24.25	0.271	0.02
170.40	0.00	24.24	0.269	0.02
171.60	0.00	24.22	0.267	0.02
172.80	0.00	24.21	0.264	0.02
174.00	0.00	24.20	0.262	0.02
175.20	0.00	24.19	0.260	0.02
176.40	0.00	24.17	0.258	0.02
177.60	0.00	24.16	0.256	0.02
178.80	0.00	24.15	0.254	0.02
180.00	0.00	24.14	0.251	0.02
181.20	0.00	24.13	0.249	0.02
182.40	0.00	24.11	0.247	0.02
183.60	0.00	24.10	0.245	0.02
184.80	0.00	24.09	0.243	0.02
186.00	0.00	24.08	0.241	0.02
187.20	0.00	24.07	0.239	0.02
188.40	0.00	24.05	0.237	0.02
189.60	0.00	24.03	0.235	0.02
190.80	0.00	24.04	0.233	0.02
192.00	0.00	24.03	0.231	
193.20	0.00	24.02		0.02
193.20	0.00	74. AT	0.229	0.02

194.40	0.00	24.00	0.227	0.02		
195.60	0.00	23.98	0.225	0.02		
196.80	0.00	23.97	0.223	0.02		
198.00	0.00	23.95	0.221	0.02		
199.20	0.00	23.94	0.219	0.02		
PEAK DISCHAR	GE =	5.539 CF	S - PEAK	OCCURS AT HOUF	2.00	
MAXIMUM WATE	R SURFACE	ELEVATION	= 2	7.484		
MAXIMUM STOR	AGE =	1.1810	AC-FT	INCREMENTAL	TIME=	0.050000HRS

PRINT HYD ID=55 CODE=1

PARTIAL HYDROGRAPH 200.10

RUNOFF VOLUME = 1.28866 INCHES = 1.5230 ACRE-FEET PEAK DISCHARGE RATE = 5.54 CFS AT 2.000 HOURS BASIN AREA = 0.0222 SQ. MI.

ADD HYD

ID=60 HYD NO=100.60 ID=10 ID=55

\*TOTAL RUNOFF FROM SITE AND FRONTING ROADWAY PRINT HYD ID=60 CODE=1

PARTIAL HYDROGRAPH 100.60

RUNOFF VOLUME = 1.33061 INCHES = 1.6726 ACRE-FEET PEAK DISCHARGE RATE = 7.19 CFS AT 1.650 HOURS BASIN AREA = 0.0236 SQ. MI.

FINISH

NORMAL PROGRAM FINISH END TIME (HR:MIN:SEC) = 14:29:02

