CITY OF ALBUQUERQUE

Planning Department Alan Varela, Interim Director



Mayor Timothy M. Keller

December 22, 2021

Ronald Bohannan, P.E. Tierra West, LLC 5571 Midway Park Place NE Albuquerque, NM 87109

RE: Titan 150k Spec Conceptual Grading and Drainage Plans Engineer's Stamp Date: 12/06/21 Hydrology File: K09D051

Dear Mr. Bohannan:

Sincerely,

Based upon the information provided in your submittal received 11/04/2021, the Conceptual Grading & Drainage Plans are approved for action by the DRB for Site Plan for Building Permit.

Albuquerque As a reminder, if the project total area of disturbance (including the staging area and any work within the adjacent Right-of-Way) is 1 acre or more, then an Erosion and Sediment Control (ESC) Plan and Owner's certified Notice of Intent (NOI) is required to be submitted to the Stormwater Quality Engineer (Doug Hughes, PE, jhughes@cabq.gov, 924-3420) 14 days prior to any earth disturbance.

NM 87103

If you have any questions, please contact me at 924-3995 or <u>rbrissette@cabq.gov</u>.

www.cabq.gov

Renée C. Brissette

Renée C. Brissette, P.E. CFM Senior Engineer, Hydrology Planning Department

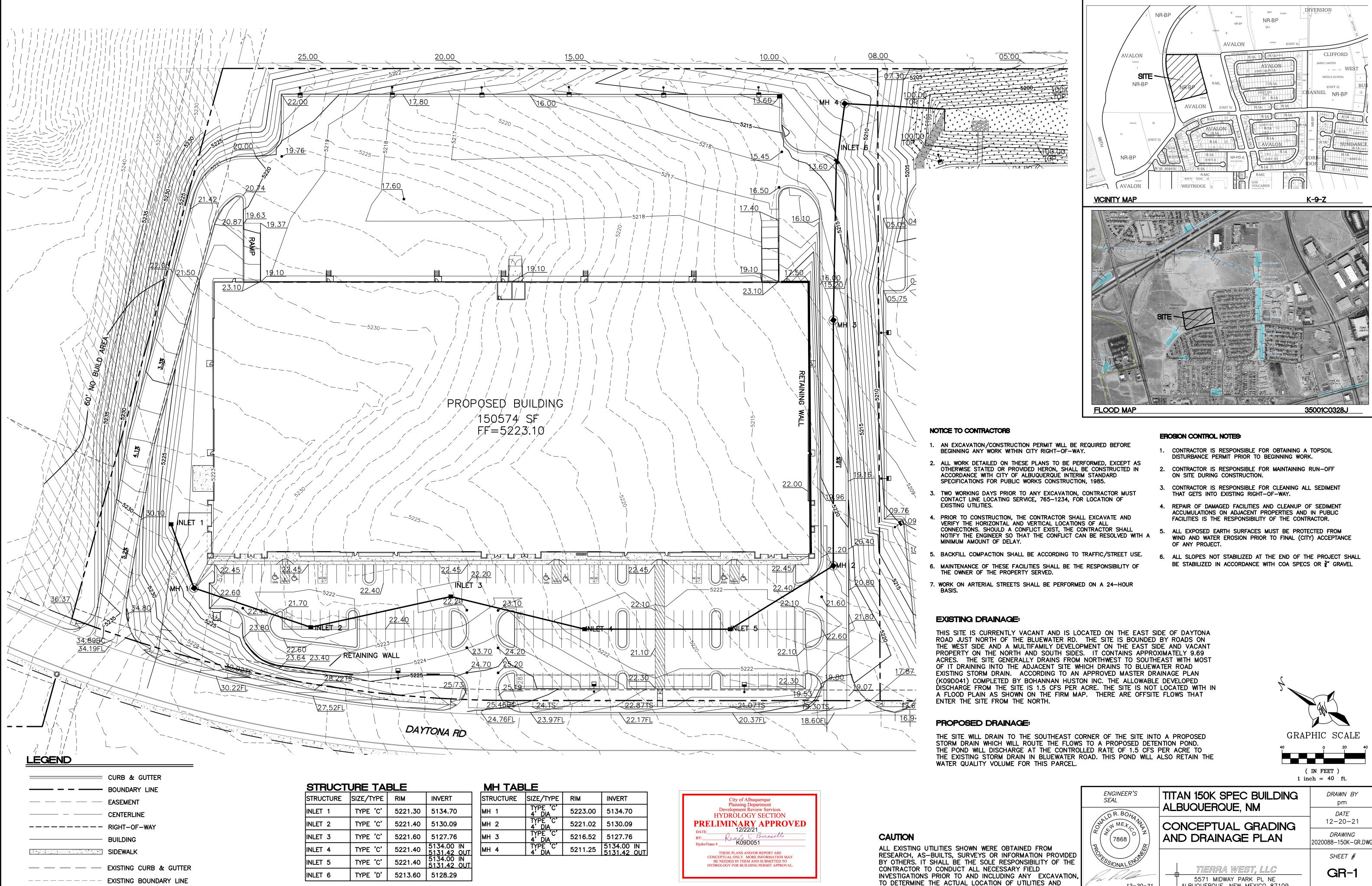


City of Albuquerque

Planning Department Development & Building Services Division DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 6/2018)

| Project Title: Titan 150K Spec | Building Permit #: | Hydrology File #: |
|--|-----------------------------|---|
| DRB#: | EPC#: | Work Order#: |
| Legal Description: TR 9 Plat of TRS 1 Thru 2 | 2 Avalon | |
| City Address: Bluewater Rd NW Albuquerque | | |
| Applicant: Tierra West, LLC | | Contact: |
| Address: 5571 Midway Park Place NE Albuquerq | ue NM 87109 | |
| Phone#: 505-858-3100 | Fax#: 505-858-1118 | E-mail: |
| Other Contact: | | Contact: |
| Address: | | |
| Phone#: | Fax#: | E-mail: |
| TYPE OF DEVELOPMENT: PLAT (# | of lots)RESIDENCE | X DRB SITE ADMIN SITE |
| IS THIS A RESUBMITTAL? Yes | X_No | |
| DEPARTMENT TRANSPORTATION | <u> </u> | NAGE |
| Check all that Apply: | TYPE OF AI | PPROVAL/ACCEPTANCE SOUGHT: |
| TYPE OF SUBMITTAL: | | NG PERMIT APPROVAL |
| ENGINEER/ARCHITECT CERTIFICATION | CERTIF | ICATE OF OCCUPANCY |
| PAD CERTIFICATION | | |
| X CONCEPTUAL G & D PLAN | | IINARY PLAT APPROVAL LAN FOR SUB'D APPROVAL |
| GRADING PLAN | | AN FOR SUB D'APPROVAL AN FOR BLDG. PERMIT APPROVAL |
| DRAINAGE REPORT | | PLAT APPROVAL |
| DRAINAGE MASTER PLAN | FIINAL | ILAI AFFROVAL |
| FLOODPLAIN DEVELOPMENT PERMIT A | PPLIC SIA/ RE | LEASE OF FINANCIAL GUARANTEE |
| ELEVATION CERTIFICATE | | ATION PERMIT APPROVAL |
| CLOMR/LOMR | | NG PERMIT APPROVAL |
| TRAFFIC CIRCULATION LAYOUT (TCL) | Old ID II SO-19 A | |
| TRAFFIC IMPACT STUDY (TIS) | | G PERMIT APPROVAL |
| STREET LIGHT LAYOUT | | NG/ PAD CERTIFICATION |
| OTHER (SPECIFY) | | ORDER APPROVAL |
| PRE-DESIGN MEETING? | CLOMR | 2/LOMR |
| | FLOOD | PLAIN DEVELOPMENT PERMIT |
| | OTHER | (SPECIFY) |
| | | Carrica |
| | | |
| COA STAFF: | ELECTRONIC SUBMITTAL RECEIV | /ED: |
| | | |

FEE PAID:



RETAINING WALL

| | _ |
|--|---|
| ERT | |
| 34.70 | |
| 30.09 | |
| 27.76 | |
| 4.00 IN 1. <u>42 OUT</u> 4.00 IN | |
| 4.00 IN 1.42 OUT | |
| 28.29 | |
| | |

| MH TAB | LE | | |
|-----------|--------------------|---------|---------------------------|
| STRUCTURE | SIZE/TYPE | RIM | INVERT |
| MH 1 | TYPE 'C' 4' DIA | 5223.00 | 5134.70 |
| MH 2 | TYPE 'C' 4' DIA | 5221.02 | 5130.09 |
| MH 3 | TYPE 'C' 4' DIA | 5216.52 | 5127.76 |
| MH 4 | TYPE 'C' 4' DIA | 5211.25 | 5134.00 IN 5131.42 OUT |
| | | | |

12-20-21 ALBUQUERQUE, NEW MEXICO 87109 (505) 858-3100 JOB # RONALD R. BOHANNAN www.tierrawestllc.com P.E. #7868 2020088

OTHER IMPROVEMENTS, PRIOR TO STARTING THE WORK. ANY CHANGES FROM THIS PLAN SHALL BE COORDINATED WITH AND APPROVED BY THE ENGINEER.

MASTER DRAINAGE REPORT

For

TRACT 9A & 9B AVALON SUBDIVISION UNIT 5 ALBUQUERQUE, NEW MEXICO

Prepared by

Tierra West, LLC 5571 Midway Park Place NE Albuquerque, New Mexico 87109

Prepared for

Westpointe 40 Developr Albuquerque, NM

November 19, 2021

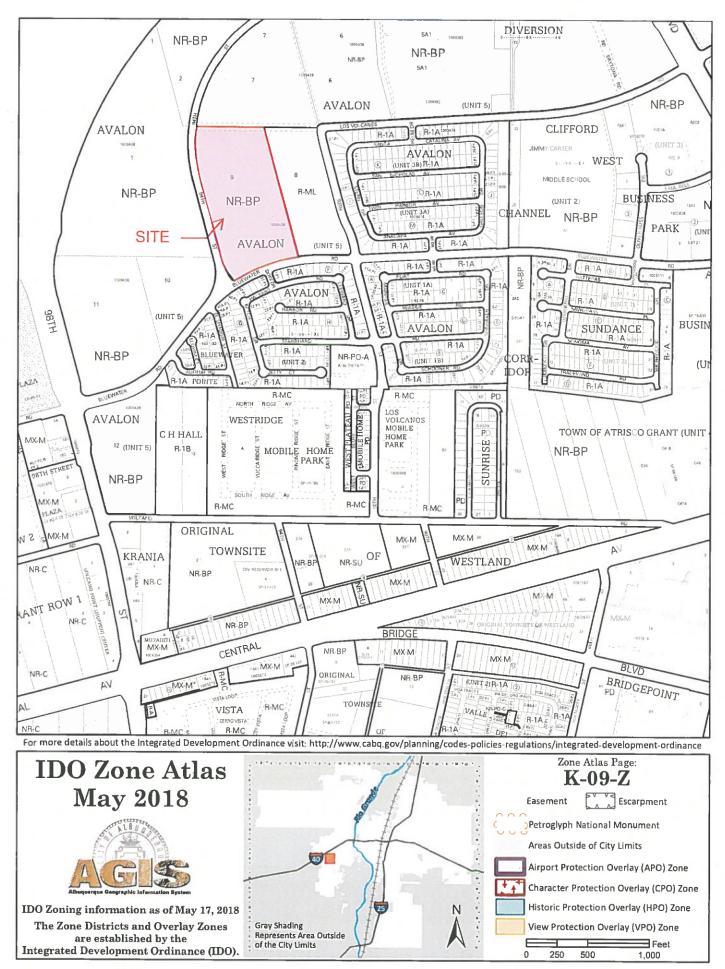
| City of Albuquerque |
|---|
| Planning Department |
| Development Review Services |
| HYDROLOGY SECTION |
| PRELIMINARY APPROVED |
| DATE: 12/22/21 |
| BY: Ranée C. Brissette |
| HydroTrans # K09D050 & K09D051 |
| THESE PLANS AND/OR REPORT ARE |
| CONCEPTUAL ONLY. MORE INFORMATION MAY |
| BE NEEDED IN THEM AND SUBMITTED TO |
| HYDROLOGY FOR BUILDING PERMIT APPROVAL. |
| HYDROLOGY FOR BUILDING PERMIT APPROVAL. |





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LOCATION

The proposed commercial development is located off Daytona Rd south of Interstate 40, east of 98th St., north of Bluewater Rd and west of Unser Blvd in southwest Albuquerque. It is comprised of approximately 16.1021 acres zoned NRBP. This report represents a mini-master drainage management and grading plan for approval by the City of Albuquerque, for grading and Building Permit submittal.

DRAINAGE BASIN DESIGNATION

The drainage basins for proposed conditions are as indicated on the BASIN MAP included in this report. The site is broken into two onsite drainage basins.

EXISTING DRAINGE CONDITIONS

The site is currently vacant with the exception of a temporary drainage pond in the southeast corner of the site. It is a part of Master Drainage Report for Westpointe 40 (Avalon Subdivision Unit 5) by BHI dated July 2019 (K09D041). The site drains predominantly northwest to southeast. Runoff from the existing site is conveyed to the existing temporary drainage pond in the southeast corner of the site via surface flow. The pond overflows to Blue Water Rd. and into an existing storm drain.

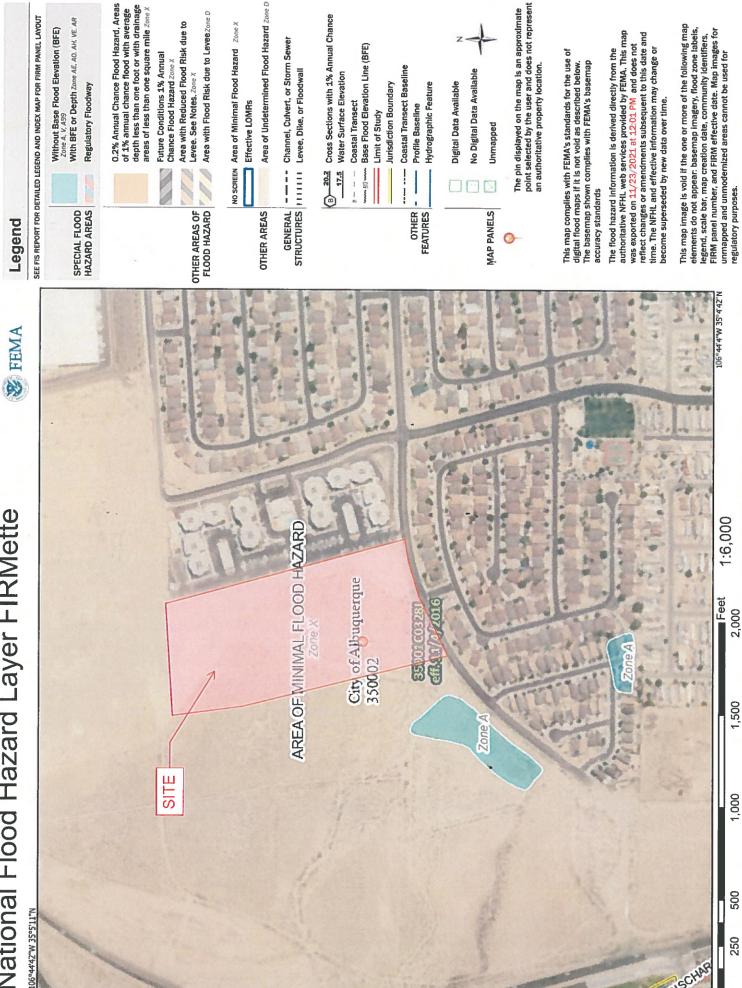
FIRM MAP

The site is not located in a designated flood plain as shown on the attached Flood Hazard Zone Map No. 35001C0328J dated 11/4/2016.

DESIGN-CRITERIA

The drainage plan presented in this report was prepared in accordance with the City of Albuquerque Drainage Ordinances and Chapter 6 of the Development Process Manual DPM. The hydrological analysis is based on the 100-year frequency, 24-hour duration storm, as Represented in Article 6-2(A), Hydrology, of the Development Process Manual. The plan will also include retention of the storm water quality in





2,000 Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

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landscaped areas and a storm water detention pond. See attached Weighted E Table for excess precipitation values calculated for this site.

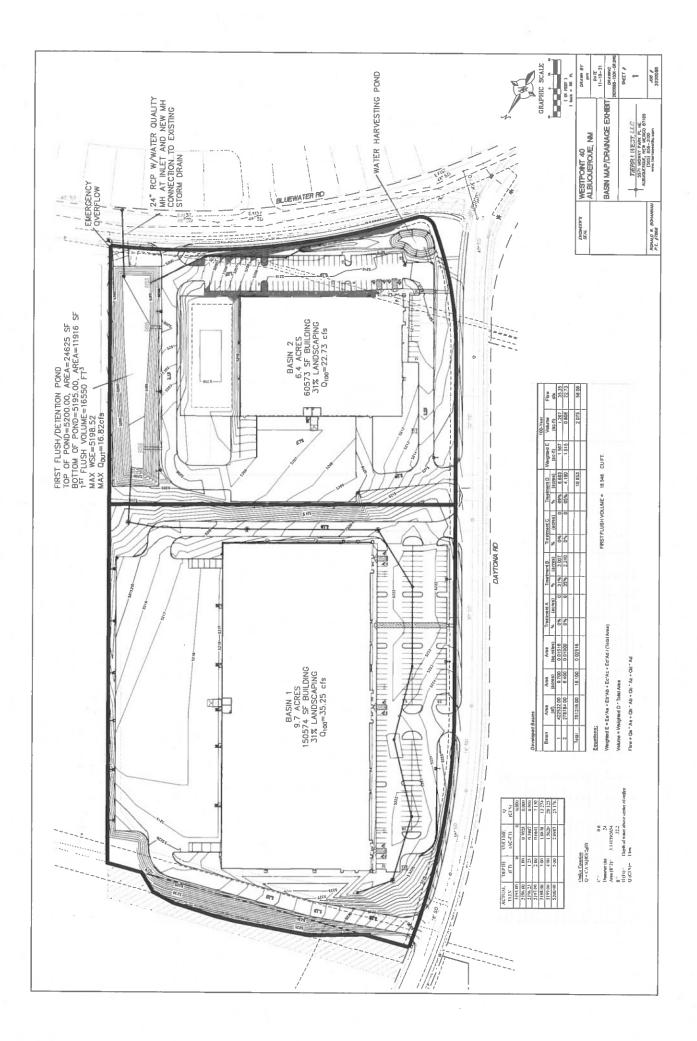
DEVELOPED-DRAINAGE CONDITIONS

The site is proposed to be developed with two users, Blue Sky Development and a 150K spec building. The overall 16.1021 acre Tract 9 parcel will be platted into two parcels. Tract 9A will be a 9.6888 acre parcel and will contain the 150K spec building. Tract 9B will be a 6.4133 acre parcel and will contain the Blue Sky Development. Both tracks will drain to a proposed detention pond in the southeast corner of Tract 9B via surface flows and onsite storm drains. The proposed adjacent Daytona Rd. will be constructed with a storm drain to capture runoff from the roadway and from future development of properties to the west of Daytona.

The proposed outfall for both the onsite storm drain pond and the Daytona Rd. storm drain will be to an existing storm drain in Bluewater Rd. The onsite storm drain pond will retain the required first flush volumes from both Tract 9A & 9B under developed conditions. The outfall from the pond will discharge to the existing Bluewater Rd. storm drain at or below the allowable discharge rate of 1.5 CFS per acre (23.4 CFS) as noted in Table 2-Allowable Discharge Summary, pg. 12 of the Master Drainage Report For Westpointe 40 (Avalon Subdivision Unit 5) prepared by BHI dated July 25, 2019 (K09D041). See attached excerpt. Refer to enclosed Weighted E computation spreadsheet for undeveloped and developed conditions.

SUMMARY

The proposed grading and drainage plan for the proposed development of the existing undeveloped Tracts 9A & 9B properties includes surface flows and an onsite storm drain to convey runoff to a water quality and storm water detention pond. The pond will retain first flush volumes for both tracts and the pond will exit the site to the existing storm drain in the Bluewater Rd. right of way. The storm drain capacity downstream of the site is sufficient to carry the ultimate developed runoff as outlined in the I-40 South and Unser Diversion Mini DMP.



Zone #1

| DdSIIIS |
|----------|
| _ 11 _ |
| SAEIODEC |
| |
| |
| |
| |

| | Flow | cfs | 12.51 | 8.26 | 20.77 | |
|----------|------------|------------|-----------|-----------|-------------|--|
| 100-Year | Volume | (ac-ft) | 0.356 | 0.235 | 0.590 | |
| | Weighted E | (ac-ft) | 0.440 | 0.440 | | |
| | reatment D | (acres) | 0.000 | 0.000 | 0.000 | |
| | Treat | % | %0 | %0 | | |
| | reatment C | (acres) | 0 | 0 | | |
| | Treatn | % | %0 | %0 | | |
| | reatment B | (acres) | 0.000 | 0.000 | | |
| | Treatr | % | %0 | %0 | | |
| | reatment A | (acres) | 9.7 | 6.4 | | |
| | Treati | % | 100% | 100% | | |
| | Area | (sq miles) | 0.01516 | 0.01000 | 0.02516 | |
| | Area | (acres) | 9.700 | 6.400 | 16.100 | |
| | Area | (sf) | 422532.00 | 278784.00 | 701316.00 | |
| | Basin | | - | 2 | Total | |

Developed Basins

| _ | | | <u></u> | _ | T | T | Ţ, |
|----------|-------------|------------|-----------|-----------|-----------|---|----|
| | Flow | cfs | 35.35 | 22.73 | 58.08 | | |
| 100-Year | Volume | (ac-ft) | 1.267 | 0.808 | 2.075 | | |
| | Weighted E | (ac-ft) | 1.567 | 1.515 | | | |
| | reatment D | (acres) | 6.693 | 4.160 | 10.853 | | |
| | Treat | % | %69 | 65% | | | |
| | Treatment C | (acres) | 0 | 0 | | | |
| | Treat | % | %0 | %0 | | | |
| | Freatment B | (acres) | 3.007 | 2.240 | | | |
| | Treat | % | 31% | 35% | | | |
| | Freatment A | (acres) | 0 | 0 | | | |
| | Treat | % | %0 | %0 | | | |
| | Area | (sq miles) | 0.01516 | 0.01000 | 0.02516 | | |
| | Area | (acres) | 9.700 | 6.400 | 16.100 | | |
| i | Area | (sf) | 422532.00 | 278784.00 | 701316.00 | | |
| | Basin | | - E | 2 | Total | | |

Equations:

Weighted E = Ea*Aa + Eb*Ab + Ec*Ac + Ed*Ad / (Total Area)

Volume = Weighted D * Total Area

Flow = Qa * Aa + Qb * Ab + Qc * Ac + Qd * Ad

FIRST FLUSH VOLUME = 16,546 CU.FT.

VOLUME CALCULATIONS

WESTPOINTE 40 TRACTS 9a &9B

- Ab Bottom Of The Pond Surface Area
- At Top Of The Pond Surface Area

D - Water Depth

- Dt Total Pond Depth
- C Change In Surface Area / Water Depth

Volume = Ab * D + 0.5 * C * D² C = (At - Ab) / Dt Ab = 11,916.00 B.O.P.= 5195.00 At = 24,652.00 T.O.P. = 5200.00 Dt = 5.00 C = 2547.20 B Elev. = 5,195.00

| ACTUAL | DEPTH | VOLUME | Q |
|---------|-------|---------|--------|
| ELEV. | (FT) | (AC-FT) | (CFS) |
| 5195.00 | 0 | 0 | 0.000 |
| 5196.00 | 1.00 | 0.3028 | 0.000 |
| 5196.23 | 1.23 | 0.3807 | 0.000 |
| 5197.00 | 2.00 | 0.6641 | 7.130 |
| 5198.00 | 3.00 | 1.0838 | 13.274 |
| 5199.00 | 4.00 | 1.5620 | 20.125 |
| 5200.00 | 5.00 | 2.0987 | 25.176 |
| | | | |

 $\frac{\text{Orifice Equation}}{Q = CA \text{ SQRT}(2gH)}$

| C = | 0.6 |
|---------------|--|
| Diameter (in) | 24 |
| Area (ft^2)= | 3.141592654 |
| g = | 32.2 |
| H (Ft) = | Depth of water above center of orifice |
| Q (CFS)= | Flow |

| Tract | Allowable Unit Discharge ¹ (cfs/ac) | Drainage Area (ac) | Allowable Discharge (cfs) |
|--|---|--------------------------|---------------------------------|
| Tract 1 | 1.5 | 32.7 | 47.6 |
| Tract 2 – (North portion, drains to Daytona Road storm drain) | 2.3 | 9.5 | 22.0 |
| Tract 2 – (South portion, drains to Bluewater Road storm drain) | 1.5 | 4.3 | 6.2 |
| Tract 3 ² | 2.3 | 5.7 | 13.2 |
| Tract 6 | 3.2 | 14.6 | 46.7 |
| Tract 7 | 3.2 | 14.6 | 46.3 |
| Tract 9 | 1.5 | 16.1 | 23.4 |
| Tract 10 | 1.5 | 7.3 | 10.6 |
| Tract 11 | 1.5 | 16.7 | 24.2 |

Table 2 – Allowable Discharge Summary

¹ Refer to Appendix C for Allowable Unit Discharge calculations, based on downstream capacity, free discharge from ROW, and accommodation of offsite flows.

² Tract 3 is not a part of this Master Drainage Report, but a developed condition allowable discharge is provided based on the assumption that all tracts draining to Daytona Road will be held to the same detention requirements.

2. BLUEWATER ROAD DRAINAGE AREAS

The proposed drainage concept for the portion of the project site draining to Bluewater Road consists of a detention pond along the western boundary of Tract 1 to capture and attenuate offsite flows from I-40 ROW. This pond would allow sediment to drop out and be drained by an 18-inch storm drain (with an associated peak outflow of approximately 10 cfs) that passes through Tract 1 within a new drainage easement and connects to the proposed storm drain in 94th Street, which will connect to the existing storm drain in Bluewater Road. Other detention ponds will be provided to accommodate onsite flows only, will discharge to the existing or proposed storm drains in the adjacent public roadways, and ensure downstream capacities are not exceeded. The conceptual size and design parameters for proposed ponds based on the HEC-HMS modeling are provided in Table 3.

Bohannan 🔔 Huston

| ****** | ***** | ****** | ***** | | |
|--|------------------------------------|-------------------|-----------------|--|--|
| | * TRACTS 9A & 9B - WESTPOINTE 40 * | | | | |
| *************************************** | | | | | |
| <pre>* 100-YEAR, 24-HR STORM (UNDER PROPOSED CONDITIONS) W/ routing ************************************</pre> | | | | | |
| START | TIME=0.0 | | | | |
| * | | | | | |
| * | | | | | |
| RAINFALL | TYPE=2 RAIN QL | JARTER=0.0 IN | | | |
| | RAIN ONE=1.87 | IN RAIN SIX=2.20 | IN | | |
| | RAIN DAY=2.66 | IN DT=0.05 HR | | | |
| * | | | | | |
| * | | | | | |
| *BASIN 1 * | | | | | |
| COMPUTE NM HYD | ID=1 HYD NO=10 | 0.1 AREA=0.01516 | SQ MI | | |
| | PER A=0.00 PER | B=31.00 PER C=0 | .00 PER D=69.00 | | |
| | TP=-0.1333 HR | MASS RAINFALL=-1 | | | |
| PRINT HYD | ID=1 CODE=1 | | | | |
| * | | | | | |
| * | | | | | |
| *BASIN 2 | | | | | |
| | | | | | |
| COMPUTE NM HYD | | 0.2 AREA=0.01000 | | | |
| | | B=35.00 PER C=0 | .00 PER D=65.00 | | |
| PRINT HYD | ID=2 CODE=1 | MASS RAINFALL=-1 | | | |
| | ID=2 CODE=1 | | | | |
| * | | | | | |
| ADD HYD | TD=20 HVD NO=1 | .00.20 ID=1 ID=2 | | | |
| * | 10-20 1110 100-1 | 00.20 10-1 10-2 | | | |
| * | | | | | |
| *ROUTE BASIN 1 & 2 * | THROUGH WATER Q | UALITY DETENTION | POND | | |
| * | | | | | |
| ROUTE RESERVOIR | ID=55 HYD NO=2 | 00.1 INFLOW ID=20 | 0 CODE=24 | | |
| | OUTFLOW (CFS) | STORAGE(AC-FT) E | LEVATION(FT) | | |
| | 0.000 | 0.0000 | 95.00 | | |
| | 0.010 | 0.3028 | 96.00 | | |
| | 0.020 | 0.3807 | 96.23 | | |
| | 7.130 | 0.6641 | 97.00 | | |
| | 13.274 | 1.0838 | 98.00 | | |
| | 20.125 | 1.5620 | 99.00 | | |
| | 25.176 | 2.0987 | 100.00 | | |
| * | | | | | |
| PRINT HYD | ID=55 CODE=1 | | | | |
| * | | | | | |
| | | | | | |
| FINISH | | | | | |

INPUT

DUTPUT

AHYMO PROGRAM (AHYMO-S4) - Version: S4.01a - Rel: 01a RUN DATE (MON/DAY/YR) = 11/23/2021

START TIME (HR:MIN:SEC) = 11:26:28

USER NO.=

AHYMO_Temp_User:20122010

INPUT FILE = C:\Users\Vince\Desktop\HYMO Westpoint_40.txt

RAIN ONE=1.87 IN RAIN SIX=2.20 IN RAIN DAY=2.66 IN DT=0.05 HR

24-HOUR RAINFALL DIST. - BASED ON NOAA ATLAS 14 FOR CONVECTIVE AREAS (NM & AZ) - D1

| DT = 0. | 050000 н | OURS | END T | IME = | 24.0000 | 02 HOURS |
|---------|----------|--------|--------|--------|---------|----------|
| 0.0000 | 0.0022 | 0.0045 | 0.0069 | 0.0096 | 0.0123 | 0.0154 |
| 0.0197 | 0.0264 | 0.0336 | 0.0412 | 0.0494 | 0.0578 | 0.0664 |
| 0.0753 | 0.0844 | 0.0946 | 0.1052 | 0.1168 | 0.1387 | 0.1657 |
| 0.2020 | 0.2430 | 0.2937 | 0.3614 | 0.4375 | 0.5689 | 0.7733 |
| 1.1234 | 1.3695 | 1.5635 | 1.6610 | 1.7465 | 1.8079 | 1.8568 |
| 1.8994 | 1.9306 | 1.9592 | 1.9828 | 1.9979 | 2.0087 | 2.0183 |
| 2.0273 | 2.0352 | 2.0426 | 2.0499 | 2.0568 | 2.0625 | 2.0659 |
| 2.0692 | 2.0724 | 2.0754 | 2.0784 | 2.0813 | 2.0842 | 2.0870 |
| 2.0896 | 2.0923 | 2.0949 | 2.0974 | 2.0999 | 2.1023 | 2.1046 |
| 2.1069 | 2.1092 | 2.1115 | 2.1136 | 2.1158 | 2.1179 | 2.1199 |
| 2.1220 | 2.1240 | 2.1260 | 2.1280 | 2.1299 | 2.1318 | 2.1337 |
| 2.1356 | 2.1374 | 2.1392 | 2.1411 | 2.1428 | 2.1446 | 2.1463 |
| 2.1481 | 2.1498 | 2.1514 | 2.1531 | 2.1548 | 2.1564 | 2.1580 |
| 2.1596 | 2.1612 | 2.1628 | 2.1643 | 2.1658 | 2.1674 | 2.1689 |
| 2.1704 | 2.1718 | 2.1733 | 2.1747 | 2.1762 | 2.1776 | 2.1790 |
| 2.1804 | 2.1818 | 2.1832 | 2.1845 | 2.1859 | 2.1872 | 2.1885 |
| 2.1899 | 2.1912 | 2.1924 | 2.1937 | 2.1950 | 2.1963 | 2.1975 |
| 2.1988 | 2.2000 | 2.2013 | 2.2026 | 2.2038 | 2.2051 | 2.2064 |
| 2.2077 | 2.2089 | 2.2102 | 2.2115 | 2.2128 | 2.2141 | 2.2153 |
| 2.2166 | 2.2179 | 2.2192 | 2.2204 | 2.2217 | 2.2230 | 2.2243 |
| 2.2256 | | 2.2281 | 2.2294 | 2.2307 | 2.2319 | 2.2332 |
| 2.2345 | 2.2358 | 2.2371 | 2.2383 | 2.2396 | 2.2409 | 2.2422 |
| 2.2434 | 2.2447 | 2.2460 | 2.2473 | 2.2486 | 2.2498 | 2.2511 |
| 2.2524 | 2.2537 | 2.2549 | 2.2562 | 2.2575 | 2.2588 | 2.2601 |
| 2.2613 | 2.2626 | 2.2639 | 2.2652 | 2.2664 | 2.2677 | 2.2690 |
| 2.2703 | 2.2716 | 2.2728 | 2.2741 | 2.2754 | 2.2767 | 2.2779 |
| 2.2792 | 2.2805 | 2.2818 | 2.2831 | 2.2843 | 2.2856 | 2.2869 |
| | | | | | | |

| 2.2882 | 2.2894 | 2.2907 | 2.2920 | 2.2933 | 2.2946 | 2.2958 |
|--------|--------|--------|--------|--------|--------|--------|
| 2.2971 | 2.2984 | 2.2997 | 2.3009 | 2.3022 | 2.3035 | 2.3048 |
| 2.3061 | 2.3073 | 2.3086 | 2.3099 | 2.3112 | 2.3124 | 2.3137 |
| 2.3150 | 2.3163 | 2.3176 | 2.3188 | 2.3201 | 2.3214 | 2.3227 |
| 2.3239 | 2.3252 | 2.3265 | 2.3278 | 2.3291 | 2.3303 | 2.3316 |
| 2.3329 | 2.3342 | 2.3354 | 2.3367 | 2.3380 | 2.3393 | 2.3406 |
| 2.3418 | 2.3431 | 2.3444 | 2.3457 | 2.3469 | 2.3482 | 2.3495 |
| 2.3508 | 2.3521 | 2.3533 | 2.3546 | 2.3559 | 2.3572 | 2.3584 |
| 2.3597 | 2.3610 | 2.3623 | 2.3636 | 2.3648 | 2.3661 | 2.3674 |
| 2.3687 | 2.3699 | 2.3712 | 2.3725 | 2.3738 | 2.3750 | 2.3763 |
| 2.3776 | 2.3789 | 2.3802 | 2.3814 | 2.3827 | 2.3840 | 2.3853 |
| 2.3865 | 2.3878 | 2.3891 | 2.3904 | 2.3917 | 2.3929 | 2.3942 |
| 2.3955 | 2.3968 | 2.3980 | 2.3993 | 2.4006 | 2.4019 | 2.4032 |
| 2.4044 | 2.4057 | 2.4070 | 2.4083 | 2.4095 | 2.4108 | 2.4121 |
| 2.4134 | 2.4147 | 2.4159 | 2.4172 | 2.4185 | 2.4198 | 2.4210 |
| 2.4223 | 2.4236 | 2.4249 | 2.4262 | 2.4274 | 2.4287 | 2.4300 |
| 2.4313 | 2.4325 | 2.4338 | 2.4351 | 2.4364 | 2.4377 | 2.4389 |
| 2.4402 | 2.4415 | 2.4428 | 2.4440 | 2.4453 | 2.4466 | 2.4479 |
| 2.4492 | 2.4504 | 2.4517 | 2.4530 | 2.4543 | 2.4555 | 2.4568 |
| 2.4581 | 2.4594 | 2.4607 | 2.4619 | 2.4632 | 2.4645 | 2.4658 |
| 2.4670 | 2.4683 | 2.4696 | 2.4709 | 2.4722 | 2.4734 | 2.4747 |
| 2.4760 | 2.4773 | 2.4785 | 2.4798 | 2.4811 | 2.4824 | 2.4837 |
| 2.4849 | 2.4862 | 2.4875 | 2.4888 | | 2.4913 | 2.4926 |
| 2.4939 | 2.4952 | 2.4964 | 2.4977 | 2.4990 | 2.5003 | 2.5015 |
| 2.5028 | 2.5041 | 2.5054 | 2.5067 | 2.5079 | 2.5092 | 2.5105 |
| 2.5118 | 2.5130 | 2.5143 | 2.5156 | 2.5169 | 2.5182 | 2.5194 |
| 2.5207 | 2.5220 | 2.5233 | 2.5245 | 2.5258 | 2.5271 | 2.5284 |
| 2.5297 | 2.5309 | 2.5322 | 2.5335 | 2.5348 | 2.5360 | 2.5373 |
| 2.5386 | 2.5399 | 2.5412 | 2.5424 | | 2.5450 | 2.5463 |
| 2.5475 | 2.5488 | 2.5501 | 2.5514 | | 2.5539 | 2.5552 |
| 2.5565 | 2.5578 | 2.5590 | 2.5603 | 2.5616 | 2.5629 | 2.5642 |
| 2.5654 | 2.5667 | 2.5680 | 2.5693 | 2.5705 | 2.5718 | 2.5731 |
| 2.5744 | 2.5757 | 2.5769 | 2.5782 | 2.5795 | 2.5808 | 2.5820 |
| 2.5833 | 2.5846 | 2.5859 | 2.5872 | 2.5884 | 2.5897 | 2.5910 |
| 2.5923 | 2.5935 | 2.5948 | 2.5961 | 2.5974 | 2.5987 | 2.5999 |
| 2.6012 | 2.6025 | 2.6038 | 2.6050 | 2.6063 | 2.6076 | 2.6089 |
| 2.6102 | 2.6114 | 2.6127 | 2.6140 | 2.6153 | 2.6165 | 2.6178 |
| 2.6191 | 2.6204 | 2.6217 | 2.6229 | 2.6242 | 2.6255 | 2.6268 |
| 2.6280 | 2.6293 | 2.6306 | 2.6319 | 2.6332 | 2.6344 | 2.6357 |
| 2.6370 | 2.6383 | 2.6395 | 2.6408 | 2.6421 | 2.6434 | 2.6447 |
| 2.6459 | 2.6472 | 2.6485 | 2.6498 | 2.6510 | 2.6523 | 2.6536 |
| 2.6549 | 2.6562 | 2.6574 | 2.6587 | 2.6600 | | |
| | | | | | | |

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*BASIN 1

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COMPUTE NM HYD

ID=1 HYD NO=100.1 AREA=0.01516 SQ MI PER A=0.00 PER B=31.00 PER C=0.00 PER D=69.00 TP=-0.1333 HR MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428UNIT PEAK = 41.298 CFS UNIT VOLUME = 0.9989 B = 526.28 P60 = 1.8700AREA = 0.010460 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000 K = 0.130992HR TP = 0.133300HR K/TP RATIO = 0.982685 SHAPE CONSTANT, N = 3.593298UNIT PEAK = 11.532 CFS UNIT VOLUME = 1.000 B = 327.08 P60 = 1.8700AREA = 0.004700 SQ MI IA = 0.50000 INCHES INF = 1.25000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000 PRINT HYD ID=1 CODE=1 PARTIAL HYDROGRAPH 100.10 RUNOFF VOLUME = 1.92681 INCHES = 1.5579 ACRE-FEET PEAK DISCHARGE RATE = 37.23 CFS AT 1.500 HOURS BASIN AREA = 0.0152 SO. MI. * *BASIN 2 COMPUTE NM HYD ID=2 HYD NO=100.2 AREA=0.01000 SQ MI PER A=0.00 PER B=35.00 PER C=0.00 PER D=65.00 TP=-0.1333 HR MASS RAINFALL=-1 K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428UNIT PEAK = 25.662 CFS UNIT VOLUME = 0.9987 B = 526.28 P60 = 1.8700AREA = 0.006500 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.130992HR TP = 0.133300HR K/TP RATIO = 0.982685 SHAPE

CONSTANT, N = 3.593298UNIT PEAK = 8.5881 CFS UNIT VOLUME = 0.9997 B = 327.08 P60 = 1.8700AREA = 0.003500 SQ MI IA = 0.50000 INCHES INF = 1.25000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000 PRINT HYD ID=2 CODE=1 PARTIAL HYDROGRAPH 100.20 RUNOFF VOLUME = 1.86373 INCHES = 0.9940 ACRE-FEET PEAK DISCHARGE RATE = 24.04 CFS AT 1.500 HOURS BASIN AREA = 0.0100 SO. MI. * * ADD HYD ID=20 HYD NO=100.20 ID=1 ID=2 * * *ROUTE BASIN 1 & 2 THROUGH WATER QUALITY DETENTION POND * * ROUTE RESERVOIR ID=55 HYD NO≈200.1 INFLOW ID=20 CODE=24 OUTFLOW (CFS) STORAGE(AC-FT) ELEVATION(FT) 0.000 0.0000 95.00 0.010 0.3028 96.00 0.020 0.3807 96.23 7.130 0.6641 97.00 13.274 1.0838 98.00 20.125 1.5620 99.00 25.176 2.0987 100.00 TIME INFLOW ELEV VOLUME OUTFLOW (HRS) (CFS) (FEET) (AC-FT) (CFS)

| 0.00 | 0.00 | 95.00 | 0.000 | 0.00 |
|-------|------|-------|-------|-------|
| 1.20 | 7.63 | 95.29 | 0.088 | 0.00 |
| 2.40 | 2.08 | 97.68 | 0.949 | 11.31 |
| 3.60 | 0.11 | 96.40 | 0.443 | 1.57 |
| 4.80 | 0.15 | 96.25 | 0.390 | 0.25 |
| 6.00 | 0.26 | 96.25 | 0.389 | 0.23 |
| 7.20 | 0.28 | 96.26 | 0.391 | 0.27 |
| 8.40 | 0.28 | 96.26 | 0.391 | 0.28 |
| 9.60 | 0.28 | 96.26 | 0.391 | 0.28 |
| 10.80 | 0.28 | 96.26 | 0.391 | 0.28 |
| 12.00 | 0.28 | 96.26 | 0.391 | 0.28 |
| 13.20 | 0.28 | 96.26 | 0.391 | 0.28 |
| 14.40 | 0.28 | 96.26 | 0.391 | 0.28 |
| 15.60 | 0.28 | 96.26 | 0.391 | 0.28 |
| 16.80 | 0.28 | 96.26 | 0.391 | 0.28 |
| 18.00 | 0.28 | 96.26 | 0.391 | 0.28 |
| 19.20 | 0.28 | 96.26 | 0.391 | 0.28 |
| 20.40 | 0.28 | 96.26 | 0.391 | 0.28 |
| 21.60 | 0.28 | 96.26 | 0.391 | 0.28 |
| 22.80 | 0.28 | 96.26 | 0.391 | 0.28 |
| 24.00 | 0.28 | 96.26 | 0.391 | 0.28 |
| 25.20 | 0.00 | 96.23 | 0.381 | 0.04 |
| 26.40 | 0.00 | 96.23 | 0.379 | 0.02 |
| 27.60 | 0.00 | 96.22 | 0.377 | 0.02 |
| 28.80 | 0.00 | 96.21 | 0.375 | 0.02 |
| 30.00 | 0.00 | 96.21 | 0.373 | 0.02 |
| 31.20 | 0.00 | 96.20 | 0.372 | 0.02 |
| 32,40 | 0.00 | 96.20 | 0.370 | 0.02 |
| 33.60 | 0.00 | 96.19 | 0.368 | 0.02 |
| 34.80 | 0.00 | 96.19 | 0.366 | 0.02 |
| 36.00 | 0.00 | 96.18 | 0.364 | 0.02 |
| 37.20 | 0.00 | 96.18 | 0.362 | 0.02 |
| 38.40 | 0.00 | 96.17 | 0.361 | 0.02 |
| 39.60 | 0.00 | 96.17 | 0.359 | 0.02 |
| 40.80 | 0.00 | 96.16 | 0.357 | 0.02 |
| 42.00 | 0.00 | 96.16 | 0.356 | 0.02 |
| 43.20 | 0.00 | 96.15 | 0.354 | 0.02 |
| 44.40 | 0.00 | 96.15 | 0.352 | 0.02 |
| 45.60 | 0.00 | 96.14 | 0.351 | 0.02 |
| 46.80 | 0.00 | 96.14 | 0.349 | 0.02 |
| 48.00 | 0.00 | 96.13 | 0.348 | 0.02 |
| 49.20 | 0.00 | 96.13 | 0.346 | 0.02 |
| 50.40 | 0.00 | 96.12 | 0.345 | 0.02 |
| 51.60 | 0.00 | 96.12 | 0.343 | 0.02 |
| 52.80 | 0.00 | 96.11 | 0.342 | 0.01 |
| 54.00 | 0.00 | 96.11 | 0.340 | 0.01 |
| 55.20 | 0.00 | 96.11 | 0.339 | 0.01 |
| 56.40 | 0.00 | 96.10 | 0.337 | 0.01 |
| 57.60 | 0.00 | 96.10 | 0.336 | 0.01 |
| 58.80 | 0.00 | 96.09 | 0.334 | 0.01 |
| | | | | |

| 60.00 | 0.00 | 96.09 | 0.333 | 0.01 |
|---|--|---|---|--|
| 61.20 | 0.00 | 96.08 | 0.332 | 0.01 |
| 62.40 | 0.00 | 96.08 | 0.330 | 0.01 |
| 63.60 | 0.00 | 96.08 | 0.329 | 0.01 |
| 64.80 | 0.00 | 96.07 | 0.328 | 0.01 |
| 66.00 | 0.00 | 96.07 | 0.326 | 0.01 |
| TIME | INFLOW | ELEV | VOLUME | OUTFLOW |
| (HRS) | (CFS) | (FEET) | (AC-FT) | (CFS) |
| 67.20 | 0.00 | 96.07 | 0.325 | 0.01 |
| 68.40 | 0.00 | 96.06 | 0.324 | 0.01 |
| 69.60 | 0.00 | 96.05 | 0.322 | 0.01 |
| 70.80 | 0.00 | 96.05 | 0.321 | 0.01 |
| 72.00 | 0.00 | 96.05 | 0.320 | 0.01 |
| 73.20 | 0.00 | 96.05 | 0.319 | 0.01 |
| 74.40 | 0.00 | 96.05 | 0.318 | 0.01 |
| 75.60 | 0.00 | 96.04 | 0.316 | 0.01 |
| 76.80 | 0.00 | 96.04 | 0.315 | 0.01 |
| 78.00 | 0.00 | 96.03 | 0.314 | 0.01 |
| 79.20 | 0.00 | 96.03 | 0.313 | 0.01 |
| 80.40 | 0.00 | 96.03 | 0.312 | 0.01 |
| 81.60 | 0.00 | 96.02 | 0.311 | 0.01 |
| 82.80 | 0.00 | 96.02 | 0.310 | 0.01 |
| 84.00 | 0.00 | 96.02 | 0.309 | 0.01 |
| 85.20 | 0.00 | 96.01 | 0.308 | 0.01 |
| 86.40 | 0.00 | 96.01 | 0.307 | 0.01 |
| 87.60 | 0.00 | 96.00 | 0.306 | 0.01 |
| 88.80 | 0.00 | 96.00 | 0.304 | 0.01 |
| 90.00 | 0.00 | 96.00 | 0.303 | 0.01 |
| 91.20 | 0.00 | 96.00 | 0.302 | 0.01 |
| 92.40 93.60 94.80 96.00 97.20 98.40 99.60 | 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | 96.00 95.99 95.99 95.99 95.98 95.98 | 0.301 0.301 0.299 0.298 0.297 | 0.01 0.01 0.01 0.01 0.01 0.01 |
| 100.80 102.00 103.20 104.40 105.60 106.80 | 0.00 0.00 0.00 0.00 0.00 0.00 | 95.98 95.97 95.97 95.97 95.96 95.96 95.96 | 0.296 0.295 0.294 0.293 0.292 0.291 0.290 | 0.01 0.01 0.01 0.01 0.01 0.01 0.01 |
| 108.00 | 0.00 | 95.95 | 0.289 | 0.01 |
| 109.20 | 0.00 | 95.95 | 0.288 | 0.01 |
| 110.40 | 0.00 | 95.95 | 0.287 | 0.01 |
| 111.60 | 0.00 | 95.94 | 0.286 | 0.01 |
| 112.80 | 0.00 | 95.94 | 0.285 | 0.01 |
| 114.00 | 0.00 | 95.94 | 0.284 | 0.01 |

| 115.20 | 0.00 | 95.94 | 0.283 | 0.01 |
|--------|--------|--------|---------|---------|
| 116.40 | 0.00 | 95.93 | 0.282 | 0.01 |
| 117.60 | 0.00 | 95.93 | 0.281 | 0.01 |
| 118.80 | 0.00 | 95.93 | 0.281 | 0.01 |
| 120.00 | 0.00 | 95.92 | 0.280 | 0.01 |
| 121.20 | 0.00 | 95.92 | 0.279 | 0.01 |
| 122.40 | 0.00 | 95.92 | 0.278 | 0.01 |
| 123.60 | 0.00 | 95.91 | 0.277 | 0.01 |
| 124.80 | 0.00 | 95.91 | 0.276 | 0.01 |
| 126.00 | 0.00 | 95.91 | 0.275 | 0.01 |
| 127.20 | 0.00 | 95.91 | 0.274 | 0.01 |
| 128.40 | 0.00 | 95.90 | 0.273 | 0.01 |
| 129.60 | 0.00 | 95.90 | 0.272 | 0.01 |
| 130.80 | 0.00 | 95.90 | 0.271 | 0.01 |
| 132.00 | 0.00 | 95.89 | 0.271 | 0.01 |
| 133.20 | 0.00 | 95.89 | 0.270 | 0.01 |
| | | | | |
| TIME | INFLOW | ELEV | VOLUME | OUTFLOW |
| (HRS) | (CFS) | (FEET) | (AC-FT) | (CFS) |
| | | | | |
| 134.40 | 0.00 | 95.89 | 0.269 | 0.01 |
| 135.60 | 0.00 | 95.88 | 0.268 | 0.01 |
| 136.80 | 0.00 | 95.88 | 0.267 | 0.01 |
| 138.00 | 0.00 | 95.88 | 0.266 | 0.01 |
| 139.20 | 0.00 | 95.88 | 0.265 | 0.01 |
| 140.40 | 0.00 | 95.87 | 0.264 | 0.01 |
| 141.60 | 0.00 | 95.87 | 0.264 | 0.01 |
| 142.80 | 0.00 | 95.87 | 0.263 | 0.01 |
| 144.00 | 0.00 | 95.86 | 0.262 | 0.01 |
| 145.20 | 0.00 | 95.86 | 0.261 | 0.01 |
| 146.40 | 0.00 | 95.86 | 0.260 | 0.01 |
| 147.60 | 0.00 | 95.86 | 0.259 | 0.01 |
| 148.80 | 0.00 | 95.85 | 0.258 | 0.01 |
| 150.00 | 0.00 | 95.85 | 0.258 | 0.01 |
| 151.20 | 0.00 | 95.85 | 0.257 | 0.01 |
| 152.40 | 0.00 | 95.85 | 0.256 | 0.01 |
| 153.60 | 0.00 | 95.84 | 0.255 | 0.01 |
| 154.80 | 0.00 | 95.84 | 0.254 | 0.01 |
| 156.00 | 0.00 | 95.84 | 0.253 | 0.01 |
| 157.20 | 0.00 | 95.83 | 0.253 | 0.01 |
| 158.40 | 0.00 | 95.83 | 0.252 | 0.01 |
| 159.60 | 0.00 | 95.83 | 0.251 | 0.01 |
| 160.80 | 0.00 | 95.83 | 0.250 | 0.01 |
| 162.00 | 0.00 | 95.82 | 0.249 | 0.01 |
| 163.20 | 0.00 | 95.82 | 0.249 | 0.01 |
| 164.40 | 0.00 | 95.82 | 0.248 | 0.01 |
| 165.60 | 0.00 | 95.82 | 0.247 | 0.01 |
| 166.80 | 0.00 | 95.81 | 0.246 | 0.01 |
| 168.00 | 0.00 | 95.81 | 0.245 | 0.01 |
| 169.20 | 0.00 | 95.81 | 0.244 | 0.01 |
| | | | | |

| 170 10 | ~ ~~ | | | | | |
|----------------|---------|-----------|------------|---------------|-------|-------------|
| 170.40 | 0.00 | 95.80 | 0.244 | 0.01 | | |
| 171.60 | 0.00 | 95.80 | 0.243 | 0.01 | | |
| 172.80 | 0.00 | 95.80 | 0.242 | 0.01 | | |
| 174.00 | 0.00 | 95.80 | 0.241 | 0.01 | | |
| 175.20 | 0.00 | 95.79 | 0.241 | 0.01 | | |
| 176.40 | 0.00 | 95.79 | 0.240 | 0.01 | | |
| 177.60 | 0.00 | 95.79 | 0.239 | 0.01 | | |
| 178.80 | 0.00 | 95.79 | 0.238 | 0.01 | | |
| 180.00 | 0.00 | 95.78 | 0.237 | 0.01 | | |
| 181.20 | 0.00 | 95.78 | 0.237 | 0.01 | | |
| 182.40 | 0.00 | 95.78 | 0.236 | 0.01 | | |
| 183.60 | 0.00 | 95.78 | 0.235 | 0.01 | | |
| 184.80 | 0.00 | 95.77 | 0.234 | 0.01 | | |
| 186.00 | 0.00 | 95.77 | 0.234 | 0.01 | | |
| 187.20 | 0.00 | 95.77 | 0.233 | 0.01 | | |
| 188.40 | 0.00 | 95.77 | 0.232 | 0.01 | | |
| 189.60 | 0.00 | 95.76 | 0.231 | 0.01 | | |
| 190.80 | 0.00 | 95.76 | 0.230 | 0.01 | | |
| 192.00 | 0.00 | 95.76 | 0.230 | 0.01 | | |
| 193.20 | 0.00 | 95.76 | 0.229 | 0.01 | | |
| 194.40 | 0.00 | 95.75 | 0.228 | 0.01 | | |
| 195.60 | 0.00 | 95.75 | 0.227 | 0.01 | | |
| 196.80 | 0.00 | 95.75 | 0.227 | 0.01 | | |
| 198.00 | 0.00 | 95.75 | 0.226 | 0.01 | | |
| 199.20 | 0.00 | 95.74 | 0.225 | 0.01 | | |
| PEAK DISCHARGE | = | 16.821 CF | S - PEAK O | CCURS AT HOUR | 1.80 | |
| MAXIMUM WATER | SURFACE | | | .518 | | |
| MAXIMUM STORAG | | | AC-FT | INCREMENTAL | TIME= | 0.050000HRS |
| | | | | | | |

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PRINT HYD ID=55 CODE=1

PARTIAL HYDROGRAPH 200.10

RUNOFF VOLUME = 1.73420 INCHES = 2.3271 ACRE-FEET PEAK DISCHARGE RATE = 16.82 CFS AT 1.800 HOURS BASIN AREA = 0.0252 SQ. MI.

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FINISH

NORMAL PROGRAM FINISH END TIME (HR:MIN:SEC) = 11:26:28

