Community Sciences Corporation P. O. Box 1328 CORRALES, NEW MEXICO 87048

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November 24, 1978 (505) 897-0000 Bentwood Ridge TO Mr. Bruno Conegliano, AMAFCA P.O. Box 1293 Albuquerque, New Mexico 87103 NOV 2 9 1978 **GENTLEMEN:** CITY ENGINEERS llowing items: WE ARE SENDING YOU □ Attached □ Under separate cover via. □ Specifications □ Samples ☐ Plans ☐ Shop drawings ☐ Prints XX Copy of Plat □ Change order ☐ Copy of letter DESCRIPTION DATE NO. COPIES THESE ARE TRANSMITTED as checked below: ☐ Resubmit____copies for approval ☐ Approved as submitted ☐ For approval ☐ Submit _____copies for distribution ☐ Approved as noted ☐ For your use ☐ Return _____ corrected prints ☐ Returned for corrections ☐ As requested D __ XX For review and comment ____19____ PRINTS RETURNED AFTER LOAN TO US FOR BIDS DUE_ We will be requiring signatures in approximately 2 weeks.

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BENTWOOD RIDGE SUBDIVISION DRAINAGE MANAGEMENT PLAN

Prepared For:

ECOS Building & Development Company

Prepared By:

Community Sciences Corporation

November 1978



Kent M. Whitman, P.E.

P.O. Box 1328 Consists, New Mexico 87048 (505) 897-0000 SURVEYING ENGINEERING LAND PLANNING BENTWOOD RIDGE SUBDIVISION

DRAINAGE MANAGEMENT PLAN

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NO. SITO MENTON MENTON

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SURVEYING ENGINEERING LAND PLANNING

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A) PURPOSE AND SCOPE

ECOS Building and Development Company is currently planning development of proximately 3.7 acres in Southwest Albuquerque, into 20 R-1 units. The purpose of this report is to present a drainage management plan for the project (hereinafter called Bentwood Ridge) which is acceptable to the City of Albuquerque and to the Albuquerque Metropolitan Arroyo Flood Control Authority.

B) SITE LOCATION AND TOPOGRAPHY

Bentwood Ridge is located in Southwest Albuquerque immediately south of Central Avenue and east of 59th Street (See Plate 1). The land slopes from north to south at an average rate of 4%. Soils consist largely of fine silts and mixed amounts of well graded sands.

C) DESIGN CRITERIA

1) Engineering Parameters

For calculation of runoff rates and required storage volumes composite runoff coefficients were computed or assumed as follows:

- a) Natural areas 0.4
- b) Overall lot area 0.66
- c) Portions of lots draining to street 0.8
- d) Off-site drainage areas 0.65

All volume calculations have been based on a 100 year-6 hour rainfall of 2.2" (0.18') per AMAFCA requirements.

Rate of runoff calculations have been based on the frequency-intensity – duration relationship for a 100 year storm as presented by Gordon Herkenhoff and Associates in their 1963 Master Plan of Drainage for the City of Albuquerque. This relationship is expressed by the following equation: I=189/(Tc+25).

2) Flood Control Regulations

The drainage plan presented in this report has been designed to comply with the 1972 AMAFCA Resolution in regard to rate and volume of runoff leaving the site. That Resolution has been interpreted to say that the rate and volume of runoff allowed to leave the site after development shall be no greater than the rate and volume running off prior to development.

D) COMPUTATIONAL PROCEDURES

Appendix A contains samples of the various types of hydraulic calculations performed. Proposed easement channels were sized based on the Manning Equation for Uniform Flow. Street carrying capacities were calculated by means of the same equation using City of Albuquerque Standard Street Sections.

Hydrological flow rate calculations are based on the rational runoff method. Times of concentration were calculated using the Kirpich Nomagraph for Overland Flow and the Manning Equation for Estimating Street Flow Velocities. For flow convergence points having both developed and undeveloped areas contributing, composite runoff coefficients were calculated. Volume calculations for sizing individual lot ponds were performed by multiplication of the difference between developed and natural C factors times the 100 year - 6 hour rainfall (0.18) times the appropriate area to obtain cubic feet of water.

E) OFF-SITE DRAINAGE

Runoff will approach the site from a small area to the north which is occupied partially by brush and partially by an existing motel. This small drainage area has been divided into two parts for convenience of analysis. (See Plate 2) Runoff from both parts will be directed around or through the site via graded easement swales. Flows from Part A will be directed between Lots 10 and 11 and into 58th Court S.W. Flows from Part B will be directed along the east boundary of the site and into Churchill Road. Due to the brush and grass existing immediately north of the site, these small off-site drainage areas should yield runoff only during very severe storms.

F) ON-SITE DRAINAGE

The AMAFCA regulations will be met through the use of individual lot ponding areas. Plate 3 illustrates the lot grading scheme proposal as well as the overall platting plan. Flows in 58th Court for a 100 year rainfall will peak at less that 8 cfs - an amount easily accommodated by the street section below curb elevation.

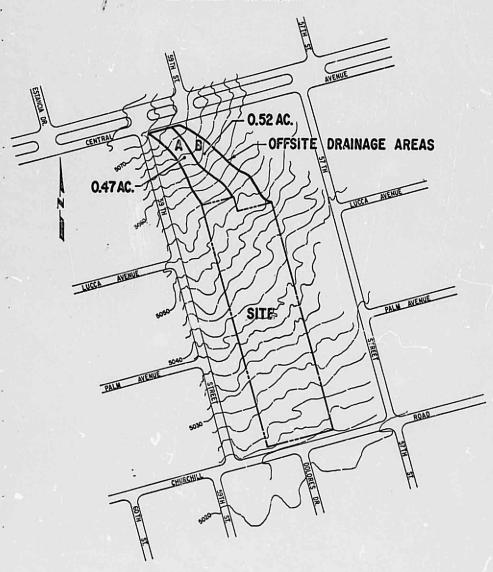
PLATE I LOCATION MAP SCALE: 1" = 800"(APPROX.)



PLATE 2

OFFSITE DRAINAGE MAP

FROM A.M.A.F.C.A. 1" = 200" TOPOGRAPHY



APPENDIX "A" CALCULATIONS

1) Off-site Flow Rates

Assume 50% natural (vegetated) and 50% hardsurfaced.

$$C = (0.5 \times 0.35) + (0.5 \times 0.95) = 0.65$$

 $I_{100} = 5.4 \text{ in/hr}$

- a) Basin A area = 0.47 acres Q_{bo} = 0.65 x 5.4 x 0.47 = 1.65 cfs
- b) Basin B area = 0.52 acres Q₁₀₀ = 0.65 x 5.4 x 0.52 = 1.83 cfs

2) Capacity Section A Swale

Bottom width = 2'

Sideslopes = 3:1

Slope (min) = 2%

Depth = 0.5'

= 0.035 (grass)

$$Q = A \frac{1.49}{n} R \% S \%$$

= 5.1 cfs 77 1.83

Maximum velocity based on maximum slope of 5%, earth bottom at n=0.025, and 1.83 cfs = 3.9 fps - stable

Composite C - Typical Lot

Gross Area = 7,510 S.F.

Roof Area @ C = 0.95 = 1,500 S.F. = 20%

Paved Areas @ C = 0.95 = 1,860 S.F. = 25%

Area in SW Landscaping @ C = 0.7 = 1,000 S.F. = 13%

Area in Lawn @ C = 0.25 = 1,500 S.F. = 20%

Area left natural @ C = 0.4 = 1,650 S.F. = 22%

$$C_{COMP} = (0.45 \times 0.95) + (0.13 \times 0.7) + (0.2 \times 0.25) + (0.4 \times 0.22)$$

= 0.66

4) Required Ponding Volume - Typical Lot

5) Actual Pond Volume

Volume =
$$\frac{5 + (2x6) + (0.6x4)}{2}$$
 x 0.6 x 69
= 402 cf

6) Peak Street Flow Rate