

# CITY OF ALBUQUERQUE

Planning Department  
David Campbell, Director



Mayor Timothy M. Keller

October 12, 2018

David Soule, P.E.  
Rio Grande Engineering  
PO Box 93924  
Albuquerque, NM 87199

RE: **Sunset Gardens Apartments**  
**86<sup>th</sup> and Sunset Gardens SW**  
**Grading Plan Stamp Date: 10/3/18**  
**Drainage Report Stamp Date: undated, 9/18**  
**Hydrology File: L10D032**

Dear Mr. Soule,

PO Box 1293

Based on the submittal received on 10/3/18, the Grading Plan and Drainage Report cannot be approved until the following are corrected and a complete resubmittal is made:

Albuquerque

Prior to Site Plan for Building Permit and Grading Permit:

NM 87103

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1. Provide a full size subbasin map; annotations are illegible on the small size provided and additional detail is required:
  - a. Define (hatch) the areas of impervious vs. pervious land cover.
  - b. Delineate the areas draining to each first flush pond and quantify the required vs. provided volume for each (include supporting calcs in the Report).
  - c. Basin F is ROW and drive entrance and can be exempt from the first flush ponding requirement.
2. Correct the following errors and typos in the Drainage Report:
  - a. Introduction. *Basin U* (not V) is the correct basin to reference from the Valhalla report,  $Q_{100}=24.63\text{cfs}$  is still correct. The Valhalla report is under drainage file *L09D019*.
  - b. Proposed Conditions. Basin A is the south portion (not the SW portion) and Basin B is the southeastern portion (not the SW portion). Basin B will be discharging to 82<sup>nd</sup> St (not 84<sup>th</sup>). Basin C flows are captured by a 24" nyloplast inlet (not a 12").
3. In Appendix B (Hydrology), *Proposed E* should be 12.55cfs, based on the land treatments proposed (see attached spreadsheet). However, the amount of land treatment D is suspect when compared to the grading plan; please correct. Also, *Proposed A* may be overstating the impervious area.
4. Add proposed contour labels and existing minor contour labels.

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5. Should there be a valley gutter or something to convey the flow from the western Basin E pond down to the D-inlet? Also, it seems like underground storage in the vicinity of the D-inlet would be a more effective way to capture all the imperious area runoff, especially if the roof runoff can be directed to the internal drive aisles.
6. Add note on the plan that “No work shall be performed in the public ROW without an approved Work Order or Excavation Permit.”
7. The following drainage infrastructure needs to be listed on the Infrastructure List:
  - a. The single-A inlet on 82<sup>nd</sup> St. This connector pipe will need to be 18” RCP, not 12”; if there’s a 12” stub, it’ll need to be replaced to the manhole with 18”.
  - b. The new single-A inlet and type-E manhole on Sunset Garden.
  - c. The new sidewalk culvert on Sunset Garden.
  - d. Additional drainage infrastructure may be identified, pending final approval of this plan.
8. Provide cross sections, one for each road/property line and at the points of maximum retainage. Include retaining walls and footers, property/ROW lines, existing and proposed grades, horizontal and vertical dimensions, and proposed ROW improvements such as: sidewalk, curb and gutter, and paving.
9. For Hydrology, the cross sections must demonstrate that grading and wall construction near the property line will not endanger adjacent property or constrain its use (DPM Ch.22, section 5 part B). Any such encroachment by the retaining wall (including footer) or stable slope will be subject to the following:
  - a. Any private encroachment into the public ROW will require a revocable permit.
  - b. Any private encroachment into a public easement will require an encroachment agreement.
  - c. Any private encroachment into neighboring private property will require written and signed permission from both property owners.
10. For information. The cross sections should be included in the Site Plan as well.
11. This project requires an ESC Plan, submitted to the Stormwater Quality Engineer (Curtis Cherne PE, ccherne@cabq.gov or 924-3420).
12. If only seeking Site Plan for Building Permit approval at this time, label the grading plan “Conceptual, Not For Construction” or similar and address the SPBP comments. If seeking SPBP and Building Permit simultaneously, forgo the conceptual markings and address all SPBP and Building Permit comments.

## Prior to Building Permit (For Information):

13. Remove any “Conceptual” markings.

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14. Provide sumps around the nyloplast inlets to generate the head required in Appendix C (Hydraulics). The inlet calcs for the basin A inlet and basin E inlet will need to be reassessed once the land treatments are updated.
15. Pipe capacity and profiles for public and private storm drain, calculated along the EGL, will be required prior to building permit or work order, whichever comes first.
16. If not achieving full capture of the first flush runoff, payment of the Fee in Lieu (Amount = BypassVolume x \$8/CF) for the required first flush volume must be made.
17. Additional comments may be provided at Building Permit, based on the outcome of the above remarks and level of detail shown on plans.

Prior to Certificate of Occupancy (For Information):

18. Engineer's Certification, per the DPM Chapter 22.7: *Engineer's Certification Checklist For Non-Subdivision* is required.

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19. A Bernalillo County Recorded [Private Facility Drainage Covenant](#) is required for the stormwater quality pond. The original notarized form, exhibit A (legible on 8.5x11 paper), and recording fee (\$25, payable to Bernalillo County) must be turned into DRC (4th, Plaza del Sol) for routing. Please contact Charlotte LaBadie (clabadie@cabq.gov, 924-3996) or Madeline Carruthers (mtafoya@cabq.gov, 924-3997) regarding the routing and recording process for covenants. The routing and recording process for covenants can take a month or longer; Hydrology recommends beginning this process as soon as possible as to not delay approval for certificate of occupancy.

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20. City acceptance and close-out of the public Work Order will be required, unless financial guarantee has been posted.

If you have any questions, please contact me at 924-3695 or dpeterson@cabq.gov.

Sincerely,

Dana Peterson, P.E.  
Senior Engineer, Planning Dept.  
Development Review Services



# City of Albuquerque

Planning Department  
Development & Building Services Division

## DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 6/2018)

**Project Title:** SUNSET GARDENS APTS **Building Permit #:** \_\_\_\_\_ **Hydrology File #:** \_\_\_\_\_

**DRB#:** \_\_\_\_\_ **EPC#:** \_\_\_\_\_ **Work Order#:** \_\_\_\_\_

**Legal Description:** TRACT 52, UNIT 2 TOWN OF ATRISCO GRANT

**City Address:** SOUTH SIDE OF SUNSETGARDENS BETWEEN 82 AND 86

**Applicant:** \_\_\_\_\_ **Contact:** \_\_\_\_\_

**Address:** \_\_\_\_\_

**Phone#:** \_\_\_\_\_ **Fax#:** \_\_\_\_\_ **E-mail:** \_\_\_\_\_

**Other Contact:** RIO GRANDE ENGINEERING **Contact:** DAVID SOULE

**Address:** PO BOX 93924 ALB NM 87199

**Phone#:** 505.321.9099 **Fax#:** 505.872.0999 **E-mail:** david@riograndeengineering.com

**TYPE OF DEVELOPMENT:** ☐ PLAT ☐ RESIDENCE ☒ DRB SITE ☐ ADMIN SITE

Check all that Apply:

### DEPARTMENT:

☒ HYDROLOGY/ DRAINAGE  
☐ TRAFFIC/ TRANSPORTATION

### TYPE OF SUBMITTAL:

☐ ENGINEER/ARCHITECT CERTIFICATION  
☐ PAD CERTIFICATION  
☐ CONCEPTUAL G & D PLAN  
☒ GRADING PLAN  
☐ DRAINAGE REPORT  
☐ DRAINAGE MASTER PLAN  
☐ FLOODPLAIN DEVELOPMENT PERMIT APPLIC  
☐ ELEVATION CERTIFICATE  
☐ CLOMR/LOMR  
☐ TRAFFIC CIRCULATION LAYOUT (TCL)  
☐ TRAFFIC IMPACT STUDY (TIS)  
☐ STREET LIGHT LAYOUT  
☐ OTHER (SPECIFY) \_\_\_\_\_  
☐ PRE-DESIGN MEETING?

IS THIS A RESUBMITTAL?: ☐ Yes ☒ No

### TYPE OF APPROVAL/ACCEPTANCE SOUGHT:

☒ BUILDING PERMIT APPROVAL  
☐ CERTIFICATE OF OCCUPANCY  
☐ PRELIMINARY PLAT APPROVAL  
☐ SITE PLAN FOR SUB'D APPROVAL  
☒ SITE PLAN FOR BLDG. PERMIT APPROVAL  
☐ FINAL PLAT APPROVAL  
☐ SIA/ RELEASE OF FINANCIAL GUARANTEE  
☐ FOUNDATION PERMIT APPROVAL  
☒ GRADING PERMIT APPROVAL  
☐ SO-19 APPROVAL  
☐ PAVING PERMIT APPROVAL  
☐ GRADING/ PAD CERTIFICATION  
☐ WORK ORDER APPROVAL  
☐ CLOMR/LOMR  
☐ FLOODPLAIN DEVELOPMENT PERMIT  
☐ OTHER (SPECIFY) \_\_\_\_\_

**DATE SUBMITTED:** \_\_\_\_\_ **By:** \_\_\_\_\_

COA STAFF:

ELECTRONIC SUBMITTAL RECEIVED: \_\_\_\_\_

FEE PAID: \_\_\_\_\_

DRAINAGE REPORT

For

**SUNSET GARDENS APARTMENTS**  
**Albuquerque, New Mexico**

Prepared by

Rio Grande Engineering  
PO Box 93924  
Albuquerque, New Mexico 87199

SEPTEMBER 2018



David Soule P.E. No. 14522

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### **Map**

Site Grading and Drainage Plan

## **PURPOSE**

The purpose of this report is to provide the Drainage Management Plan for the development of a 5.8 acre multi family project located on Sunset Gardens Road SW between 86<sup>th</sup> Street and 82<sup>nd</sup> Street SW. This plan was prepared in accordance with the City of Albuquerque design regulations, utilizing the City of Albuquerque's Development Process Manual drainage guidelines, and HYDROCAD. This report will demonstrate that the grading does not adversely affect the surrounding properties, nor the upstream or downstream facilities.

## **INTRODUCTION**

The subject of this report, as shown on the Exhibit A, is a 5.8-acre parcel of land located on the south side of Sunset Gardens Road between 86<sup>th</sup> and 82 streets SW. The legal description of this site is Tract 52, unit 2 Town of Atrisco Grant. As shown on FIRM map35001C0328J, the entire site is located within Flood Zone X. The site has not been developed but is surrounded by fully developed land. The site is in native condition. Due to the upstream construction, the site is not affected by any upland flow other than minor roadway flows adjacent to the site. The site free discharges to the east. The site is located within the Amole Del Norte drainage basin. The site is adjacent to a fully improved storm drain that accounted for the development of this site. The development of the site will require the site to discharge at a rate equal to or less than the fully developed conditions assumed (Basin V-24.63 cfs)for this site in the governing Valhalla drainage report L /9D19,which relevant excerpts can be found in appendix A.

## **EXISTING CONDITIONS**

The site currently does not have structures on it but has been impacted by minor human foot and off road vehicle traffic over the years. The site is not impacted by major upland flows. The surrounding roadway shoulders to drain onto the site. The site currently discharges all of its flow to the East.



VICINITY MAP:

L-09-Z

## National Flood Hazard Layer FIRMette



### Legend

SEE THE REPORT FOR DETAILED LEGEND AND BY MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS		Without Base Flood Elevation (BFE)
		With BFE or Depth
		Regulatory Floodway Zone A, A1, A3, A4, V, V1, V2, V3
OTHER AREAS OF FLOOD HAZARD		0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone 1
		Future Conditions 1% Annual Chance Flood Hazard Zone 1
		Area with Reduced Flood Risk due to Levee See Notes Zone 1
		Area with Flood Risk due to Levee Zone 0
OTHER AREAS		Area of Minimal Flood Hazard Zone 1
		Effective LOMRs
GENERAL STRUCTURES		Area of Undetermined Flood Hazard Zone 0
		Channel, Culvert, or Storm Sewer
OTHER FEATURES		Levee, Dike, or Floodwall
		Channel, Culvert, or Storm Sewer
MAP PANELS		Cross Sections with 1% Annual Chance Water Surface Elevation
		Coastal Tract Base Flood Elevation (BFE) Limit of Study
		Jurisdiction Boundary
		Coastal Tract Baseline Profile Baseline Hydrographic Feature
		Digital Data Available
		No Digital Data Available
		Unmapped
		Unmapped



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The base map shown complies with FEMA's base map accuracy standards.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 5/13/2018 at 10:22:33 AM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: base map imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodified areas cannot be used for regulatory purposes.

FIRM MAP:



## **PROPOSED CONDITIONS**

The proposed improvements consist of a new multi family apartment complex with associated open space and paved parking areas. The lots shall drain from west to east and will be captured by inlets and conveyed to the existing 54" storm drain in Sunset Gardens.

The site consists of 5 onsite basins and one offsite. Basin A contains the south western portion of the site. This basin encompasses 1.02 acres and drains thru several first flush ponds and ultimately discharges 4.24 cfs to a 24" inlet and 18" storm drain that will connect to the existing drain in sunset gardens. Basin B consists of the south western .22 acres of the site. This portion of this site contains the rear portion of some buildings and landscape areas. This basin is below the proposed storm drain connection and will free discharge to 84<sup>th</sup> street. The construction of the western half of the street will include a single A inlet that will capture this flow of 0.7 cfs in addition to the roadway flow. Basin C contains .41 acres consisting of the rear portion of several buildings and the landscape area. The flow is captured by a single 12" inlet connected to the new storm drain that will be connected to the existing Sunset Gardens storm drain. Basin D contains .3 acres consisting of the rear portion of several buildings and the landscaping this basin will discharge 0.31 cfs to Sunset Gardens via a sidewalk culvert. The construction of a single A inlet near the intersection of 84<sup>th</sup> street will capture this flow as well as the flow from the south half of the road that will be constructed. Basin E contains the main portion of the site that encompasses the majority of the buildings and parking lot. This basin generates 10.32 cfs. The flow is captured by a Double A inlet located on the eastern portion of the parking lot. This inlet shall be connected to the existing storm drain in Sunset gardens by a new 24" storm drain.

Basin F contains the southern portion of sunset gardens and the western portion of 86ths that drains to Sunset Gardens. This basin generates 2.70 cfs. This flow is captured by a new single a inlet that drains to the existing storm drain. The site grading contains multiple 1' deep water

quality ponds that capture 6,840 cubic feet, which exceeds the required volume of 3,058 cubic feet.

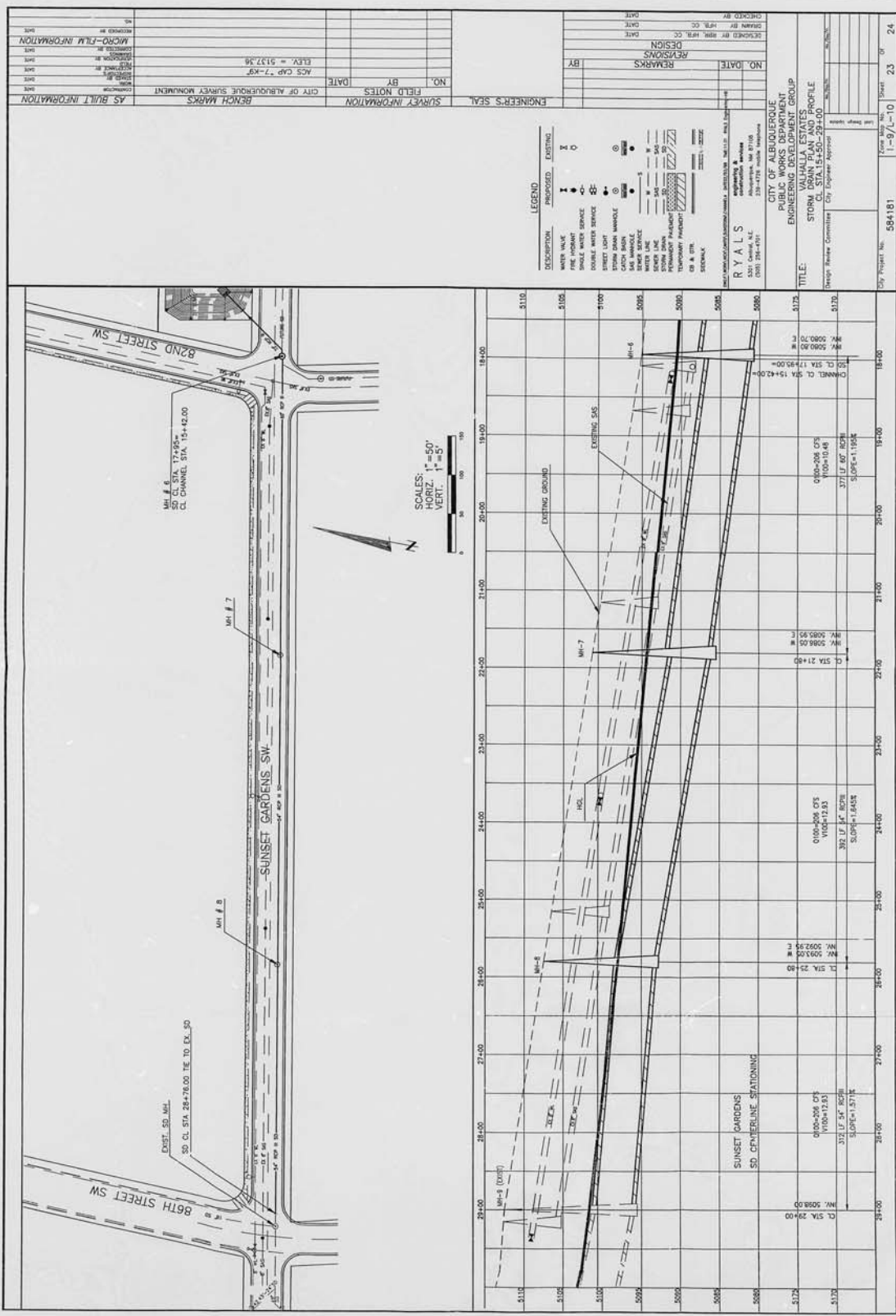
The Basin map and hydraulic calculations is located in appendix A. The pipe and inlet capacities are locate with appendix C. The total flow generated by this development will be 20.18 cfs, which is less than the fully developed assumptions for the storm drain.

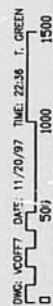
## **SUMMARY AND RECOMMENDATIONS**

This project is a development of multi family on the Southwest Mesa. The site is within the Amole Del Norte drainage basin. The site is adjacent to an existing 54" storm drain. The storm drain was designed to accept 24.63 cfs from this site. This site will discharge 20.18 cfs which is less than allowed. The site will manage its first flush requirement by shallow landscape ponds located around the site. The first flush volume is retained onsite. This drainage plan and report conforms to the governing drainage regulations of the City. Since the effected area site encompasses more than 1 acre, a NPDES permit will be required prior to any construction activity.

## **APPENDIX A**

### **Excerpts from relevant plans**





**"FUTURE" BASINS FOR SUNSET/UNSER STORM SEWER**

ALL BASINS IN FUTURE DEVELOPMENT CONDITION, INCLUDING Y. 50 (SUNSET GARDENS) SC (STORM DRAIN) COMPLETE TO UNSER THEN NORTH TO AMOLE, NO FLOW FROM WEST OF 94th ST. SOUTH OF SC, 94th DRAINS SOUTH PER DESIGN BY ANDREAS, ASBURY, AND ROBERTSON, NORTH OF SC, 94th DRAINS TO CENTRAL BRIDGE (TIERRA BATIA), 50 FEET GRADES POINT IN 94th, 1 LOT N OF EUCARIC ASSIGNED PER SC 222, TOWER/UNSER DAP, FLOW INTO WEST END OF ALLEY AT 90th BE HELD TO EXISTING CONDITIONS OR LESS. INFO PROVIDED BY STORM DRAIN TO BRIDGE BLVD. FLOW FROM BASINS B, C, & D SHOWN FOR PROBABLY: NO FLOW TO SC 50.

SELECTED 100 yr GWR  
PEAK FLOWS SHOWN  
THUS X.Y →

0000 0000 0801

ARHMO SUMMARY TABLE (ARHMO194) - ANAPCA Hydrologic Model - January, 1994  
INPUT FILE = CSGIP00B.DAT

RUN DATE (MON/DAY/YR) = 11/05/1997  
USER NO. = PERSEENG.194

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1	NOTATION
*S FILE CSGIP00A.DAT: Canto / Sunset Gardens, Interim & Future conditions,											
*S (1)00-yr 6-hr storm, version A											
*S											
*S FOR INTERIM CONDITIONS, THE SUNSET GARDENS STORM DRAIN STOPS AT 82nd ST											
*S AND FLOW IS ROUTED IN AN EARTH CHANNEL THROUGH AN UNDEVELOPED BASIN Y											
*S TO THE HEAD OF THE AMOLE CHANNEL. SEE RECALLED HYD 314 AND HYD											
*S FOR FUTURE, THE SUNSET GARDENS STORM DRAIN CONTINUES TO UNSER THEN											
*S NORTH TO THE HEAD OF THE AMOLE CHANNEL. A FULLY DEVELOPED BASIN Y											
*S CONTRIBUTES TO THIS FLOW, AS DO BASINS Y (POINTE WEST), W, & X.											
*S											
*S ALL BASINS --EXCEPT BASIN Y AS NOTED ABOVE-- ARE IN FUTURE FULLY-DEVELOPED											
*S CONDITIONS BASED ON CURRENT ZONING & DEVELOPMENT, CURRENT DEVELOPMENT PLANS,											
*S AND ON ENGINEERING JUDGMENT.											
*S											
RAINFALL TYPE: 1											
COMPUTE NM HYD	I	-	1	.00952	18.54	.617	1.21467	1.500	3.059 PER IMP=	2.220	
COMPUTE NM HYD	H	-	2	.01501	36.62	1.301	1.62555	1.500	3.812 PER IMP=	70.00	
*S E PLUS H PLUS I AT SUNSET GARDENS & 90TH FOLLOWS											
ADD HYD	208.00	16	2	.02453	55.25	1.918	1.46607	1.500	3.519		
*S DIVIDE SO 1ST 3.5 CFS (ID=6) S ON 90TH (ON HOLD): ID=4 E ON SUNSET GARDENS											
DIVIDE HYD	90.S.PAST.SG	3	6	.01052	8.60	.822	1.46607	1.333	1.278		
	SG.E.OF.90	AND	4	.01401	46.65	1.096	1.46607	1.500	5.202		
*S ROUTE MAIN FLOW EAST DOWN SG FROM 90TH, FOLLOW IT TO 86TH ST											
ROUTE MCUNGE	209.00	4	5	.01401	46.50	1.093	1.46262	1.567	5.185 CCODE =	.2	
COMPUTE NM HYD	J	-	1	.00228	5.97	.218	1.79112	1.500	4.093 PER IMP=	65.00	
ADD HYD	210.00	16	5	.01629	51.44	1.311	1.50855	1.567	4.934		
*S CALC CONTRIBUTING PART OF CANTO SITE; THEN ADD TO HYD 210											
COMPUTE NM HYD	SITE.II	-	1	.00839	19.39	.685	1.53130	1.500	3.611 PER IMP=	65.00	
*S PARTIAL WATERBLOCK ==> FLOW > 11.6cfs TO 86TH (ID=7, HOLD FOR LATER)											
DIVIDE HYD	52.TO.53	1	2	.00738	11.60	.602	1.53126	1.433	2.457		
	52.TO.86TH	AND	7	.00101	7.79	.083	1.53126	1.500	12.008		
COMPUTE NM HYD	SITE.III	-	1	.02360	54.51	1.927	1.53130	1.500	3.609 PER IMP=	65.00	
*S TOTAL FLOW LEAVING CANTO NORTH OF SUNSET GARDENS											
ADD HYD	SITE.OUT	16	2	.03038	66.11	2.530	1.53128	1.500	3.335		
*S TOTAL FLOW SUNSET GARDENS WEST OF 86TH											
ADD HYD	SG.W.OF.86	36	5	.04727	115.19	3.841	1.52344	1.533	3.808		
COMPUTE NM HYD	C	-	1	.00127	3.43	.126	1.85607	1.500	4.219 PER IMP=	90.00	
ADD HYD	218.00	16	7	.00228	11.22	.208	1.71179	1.500	7.676		
*S COMBINED FLOW TO 86TH & SUNSET GARDENS FROM NORTH & WEST: HOLD FOR LATER											
ADD HYD	86SG.NAW	36	5	.04955	125.49	4.049	1.53212	1.533	3.957		
*S											
COMPUTE NM HYD	NX	-	1	.01830	32.37	1.099	1.12653	1.500	2.815 PER IMP=	36.40	
*S ADD IN HYD 90.S.PAST.SG, ('HELD' SPILL SOUTH OF SUNSET GDS INTERSECTION)											
ADD HYD	INTO JTDN	16	3	.02882	41.57	1.922	1.25044	1.500	2.254		
*S ROUTE NORTH PART OF OFFSITE THROUGH NORTH STREET IN JTD											
ROUTE MCUNGE	300.00	3	5	.02882	39.88	1.911	1.24326	1.600	2.162 CCODE =	.1	
COMPUTE NM HYD	XS	-	1	.01719	34.17	1.167	1.27301	1.500	3.106 PER IMP=	46.60	
*S ROUTE SOUTH PART OF OFFSITE THROUGH SOUTH STREET IN JTD											
ROUTE MCUNGE	302.00	1	2	.01719	33.65	1.167	1.27335	1.567	3.059 CCODE =	.2	

BTL INTO JTDN 90th = 41.57 + 54.17 = 95.74 Comp to 73.18 7/23/97  
A = 0.3549 NM+NS (90th = 40.0, A = 0.3277)  
%D = 41.34 NO AS AWWWW.

① Dry up 10 yr = 25.41 ± (See CSGIP00B.34M)  
100 yr SPILL OVER THEN → 51.94 - 25.41 = 26.03

25x10

32x10

0000 0000 0802

11-5-74 100 11

FILE = CSG-IFD-B-DAT FROM TO  
HYDROGRAPH ID ID AREA PEAK RUNOFF  
COMAND IDENTIFICATION NO. NO. (SQ MI) (CFS) (AC-FT)

ADD HYD 304.00 26 5 3 .04601 72.69 3.078 1.25449 1.600 2.469  
COMPUTE NM HYD JTD - 17 .02353 54.35 1.922 1.53130 1.500 3.609 PER IMP= 65.00

\*S TOTAL FLOW LEAVING JTD (CANTO III), INCLUDING 86TH ST ROW EAST OF JTD  
ADD HYD JTD.EAT.85 3617 4 .06954 116.71 5.000 1.34815 1.533 2.622

\*S ROUTE TO 86TH & SG INTERSECTION, ASSUME 48" PIPE W/ 1% FRICTION SLOPE  
ROUTE MCUNGE 86.S.07.SG 4 5 .06954 116.55 4.998 1.34764 1.567 2.619 CCODE = .1

\*S AS IF COMBINED FLOWS AT 86TH & SUNSET GARDENS: RETRIEVE 'ON-HOLD' ID=7  
ADD HYD TOT.SG486 56 7 6 .11909 235.70 9.047 1.42440 1.533 3.092

\*S  
JULY 23 91 241.23 35.53

\*S FUTURE/FULL DEVELOPMENT FUTURE/FULL DEVELOPMENT  
\*S ROUTE 86TH TO 82ND IN SUNSET GARDENS: CONC PIPE; SF=.01 APX  
ROUTE 308.00 6 5 .11909 234.12 9.047 1.42440 1.567 3.072  
COMPUTE NM HYD T - 1 .00467 12.22 .446 1.79111 1.500 4.087 PER IMP= 85.00  
ADD HYD 310.00 16 5 3 .12376 244.23 9.493 1.43823 1.567 3.083  
COMPUTE NM HYD U - 1 .01032 24.63 .879 1.59625 1.500 3.729 PER IMP= 70.00  
ADD HYD 312.00 16 3 19 .13408 264.83 10.372 1.45039 1.567 3.086  
COMPUTE NM HYD V - 11 .03200 66.62 2.281 1.33643 1.500 3.253 PER IMP= 50.00  
ADD HYD SG.AT.82ND 11619 3 .16608 323.76 12.653 1.42843 1.533 3.046  
ROUTE 314.00 3 5 .16608 322.21 12.653 1.42844 1.567 3.031  
COMPUTE NM HYD W - 12 .03422 64.02 2.439 1.33643 1.533 2.923 PER IMP= 50.00  
ADD HYD 316.00 126 5 3 .20030 384.09 15.092 1.41271 1.567 2.996  
COMPUTE NM HYD X - 13 .00674 17.11 .620 1.72616 1.500 3.967 PER IMP= 80.00  
ADD HYD SG.AT.UNSER 136 3 4 .20704 398.29 15.712 1.42292 1.567 3.006  
ROUTE 318.00 4 5 .20704 399.01 15.712 1.42292 1.567 3.011  
COMPUTE NM HYD YD - 14 .02964 78.24 2.855 1.80576 1.500 4.125 PER IMP= 85.00

\*S TOTAL UNSER APX 300' S OF AMOLE CHANNEL AT BRIDGE: FUTURE/FULLY DEVELOPED  
ADD HYD FUT.TO.AMOLE 146 5 7 .23668 465.36 18.567 1.47086 1.533 3.072

\*S  
\*S INTERIM INTERIM INTERIM  
\*S INTERIM: RE-USE HYD 312 W/ ID=19, ROUTE IN DIRT CHAN ACROSS BASIN Y EXIST  
ROUTE MCUNGE 502.00 19 5 .13408 260.04 10.374 1.45076 1.600 3.030 CCODE = .2  
COMPUTE NM HYD YE - 15 .02964 26.19 .738 1.46670 1.533 1.380 PER IMP= .00

\*S  
ADD HYD 1ST.2.AMOLE 156 5 8 .16372 281.49 11.112 1.27260 1.600 2.686

\*S  
\*S INTERIM W/ V (POINTE WEST) INTERIM W/ V (POINTE WEST)  
\*S RE-USE HYD 312 W/ ID=19, HYD V W/ ID=11, & HYD YE W/ ID=15  
\*S ROUTE IN DIRT CHAN ACROSS BASIN Y EXIST  
ADD HYD 602.00 19611 3 .16608 323.76 12.653 1.42843 1.533 3.046  
ROUTE MCUNGE 604.00 3 5 .16608 320.37 12.643 1.42737 1.600 3.014 CCODE = .2  
ADD HYD INT.V.2.AMOLE 156 3 98 .19572 349.94 13.390 1.28279 1.533 2.794

\*S  
\*S ALLEY ALLEY ALLEY  
\*S BASINS B, G, & SITE-1 TO ALLEY. BASIN A NOT CONTRIBUTE INTERIM/FUTURE  
\*S FUTURE/INTERIM ALLEY FLOWS FOR INFO ONLY; HOLD TO EXISTING CONDITIONS  
COMPUTE NM HYD B - 1 .01520 38.30 1.376 1.69764 1.500 3.937 PER IMP= 76.00  
COMPUTE NM HYD G - 2 .01501 36.62 1.301 1.62555 1.500 3.812 PER IMP= 70.00  
ADD HYD TO.TOP.ALLEY 16 2 3 .03021 74.82 2.677 1.66180 1.500 3.875  
COMPUTE NM HYD SITE.1 - 1 .00151 3.50 .123 1.53130 1.500 3.624 PER IMP= 65.00  
ADD HYD BOT.ALLEY 16 3 4 .03172 78.42 2.801 1.65558 1.500 3.863  
FINISH

25X

32X



0000 0000 0803

ANYMO SUMMARY TABLE (ANYMO194) - ANAFCA Hydrologic Model - January, 1994  
 INPUT FILE - CSGIPI08.DAT

RUN DATE (MON/DAY/YR) = 11/05/1997  
 USER NO. = PERSENG.194

COMMAND	HYDROGRAPH IDENTIFICATION	FROM TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1	NOTATION
<p>*S FILE CSGIPI08.DAT: Canto / Sunset Gardens, Interim &amp; Future conditions,            *S 10-yr 6-hr storm, version A            *S            *S FOR INTERIM CONDITIONS, THE SUNSET GARDENS STORM DRAIN STOPS AT 82nd ST            *S AND FLOW IS ROUTED IN AN EARTH CHANNEL THROUGH AN UNDEVELOPED BASIN Y            *S TO THE HEAD OF THE AMOLE CHANNEL. SEE RECALLED HYD 314 AND HYD            *S FOR FUTURE, THE SUNSET GARDENS STORM DRAIN CONTINUES TO UNSER THEN            *S NORTH TO THE HEAD OF THE AMOLE CHANNEL. A FULLY DEVELOPED BASIN Y            *S CONTRIBUTES TO THIS FLOW, AS DO BASINS V (POINTE WEST), W, &amp; X.            *S            *S ALL BASINS --EXCEPT BASIN Y AS NOTED ABOVE-- ARE IN FUTURE FULLY-DEVELOPED            *S CONDITIONS BASED ON CURRENT ZONING &amp; DEVELOPMENT, CURRENT DEVELOPMENT PLANS,            *S AND ON ENGINEERING JUDGMENT.            *S            RAINFALL TYPE= 1            COMPUTE NM HYD I - 1 .00952 9.84 .321 .63243 1.500 1.615 PER IMP= 38.00            COMPUTE NM HYD H - 2 .01501 21.94 .766 .95742 1.500 2.284 PER IMP= 70.00            *S E PLUS H PLUS I AT SUNSET GARDENS &amp; 90TH FOLLOWS            ADD HYD 208.00 16 2 3 .02453 31.78 1.088 .83127 1.500 2.024            *S DIVIDE SO 1ST 8.6 CFS (ID=6) S ON 90TH (ON HOLD): ID=4 E ON SUNSET GARDENS            DIVIDE HYD 90.S.PAST.SG 3 6 .01508 8.60 .669 .83127 1.367 .891            SG.E.OF.90 AND 4 .00945 23.18 .419 .83127 1.500 3.835            *S ROUTE MAIN FLOW EAST DOWN SG FROM 90TH, FOLLOW IT TO 86TH ST            ROUTE MCUNGE 209.00 4 5 .00945 22.36 .419 .83156 1.567 3.698 CCODE = .2            COMPUTE NM HYD J - 1 .00228 3.71 .133 1.09340 1.500 2.541 PER IMP= 85.00            ADD HYD 210.00 16 5 3 .01173 25.41 .552 .88241 1.567 3.386            *S CALC CONTRIBUTING PART OF CANTO SITE; THEN ADD TO HYD 210            COMPUTE NM HYD SITE.II - 1 .00839 11.35 .398 .88845 1.500 2.113 PER IMP= 65.00            *S PARTIAL WATERBLOCK ==&gt; FLOW &gt; 11.6cfs TO 86TH (ID=7, HOLD FOR LATER)            DIVIDE HYD 52.YO.53 1 2 .00839 11.35 .398 .88841 1.500 2.113            52.TO.86TH AND 7 .00000 .00 .000 .00000 -.023 .000            COMPUTE NM HYD SITE.III - 1 .02360 31.91 1.118 .88845 1.500 2.112 PER IMP= 65.00            *S TOTAL FLOW LEAVING CANTO NORTH OF SUNSET GARDENS            ADD HYD SITE.OUT 16 2 16 .03199 43.26 1.516 .88843 1.500 2.113            *S TOTAL FLOW SUNSET GARDENS WEST OF 86TH            ADD HYD SG.W.OF.86 3616 5 .04372 66.30 2.068 .88681 1.533 2.370            COMPUTE NM HYD C - 1 .00127 2.15 .078 1.14463 1.500 2.651 PER IMP= 90.00            ADD HYD 218.00 16 7 3 .00127 2.15 .078 1.14442 1.500 2.651            *S COMBINED FLOW TO 86TH &amp; SUNSET GARDENS FROM NORTH &amp; WEST; HOLD FOR LATER            ADD HYD 866SG.NGW 36 5 2 .04499 68.35 2.145 .89409 1.533 2.374            *S            COMPUTE NM HYD NM - 1 .01830 19.79 .655 .67082 1.500 1.690 PER IMP= 42.00            *S ADD IN HYD 90.S.PAST.SG, ('HELD' SPILL SOUTH OF SUNSET GDS INTERSECTION)            ADD HYD INTO.JYON 16 6 3 .03338 28.39 1.323 .74331 1.500 1.329            *S ROUTE NORTH PART OF OFFSITE THROUGH NORTH STREET IN JYD            ROUTE MCUNGE 300.00 3 5 .03338 27.42 1.315 .73832 1.600 1.284 CCODE = .1            COMPUTE NM HYD NS - 1 .01719 29.10 .681 .74294 1.500 1.827 PER IMP= 49.80            *S ROUTE SOUTH PART OF OFFSITE THROUGH SOUTH STREET IN JYD            ROUTE MCUNGE 302.00 1 2 .01719 19.12 .675 .73590 1.600 1.738 CCODE = .1</p>										

10 yr 6-5-97  
 RECALLED 9'S LAND  
 PERMITS @ NN, NS

① APX DRX UP 10-YR \* AND SPILL OVER FROM JYD

25x10

32x10



11-5-97 10:42 PAGE = 2

COMMAND	FROM HYDROGRAPH IDENTIFICATION	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	NOTATION
ADD HYD	304.00	26 5 3	.05057	46.55	1.989	.73740	1.600	1.438	
COMPUTE NM HYD	JYD	- 17	.02353	31.81	1.115	.88845	1.500	2.112 PER IMP=	65.00
*S TOTAL FLOW LEAVING JYD (CARTO III), INCLUDING 86TH ST ROW EAST OF JYD									
ADD HYD	JYD.E.AT.86	3617 4	.07410	69.68	3.104	.78541	1.567	1.469	
*S ROUTE TO 86TH & SG INTERSECTION, ASSUME 48" PIPE W/ 1% FRICTION SLOPE									
ROUTE MCUNGE	86.S.OF.SG	4 5	.07410	69.40	3.104	.78533	1.600	1.463 CCODE =	.2
*S *AS IF* COMBINED FLOWS AT 86TH & SUNSET GARDENS: RETRIEVE 'ON-HOLD' ID=7									
ADD HYD	TOT.SG&86	56 7 6	.11909	135.38	5.249	.82641	1.533	1.776	
*S FUTURE/FULL DEVELOPMENT FUTURE/FULL DEVELOPMENT									
*S ROUTE 86TH TO 82ND IN SUNSET GARDENS: CONC PIPE; SF=.01 APX									
ROUTE	308.00	6 5	.11909	134.17	5.249	.82641	1.567	1.760	
COMPUTE NM HYD	T	- 1	.00467	7.59	.272	1.09340	1.500	2.538 PER IMP=	85.00
ADD HYD	310.00	16 5 3	.12376	140.42	5.521	.83648	1.567	1.773	
COMPUTE NM HYD	U	- 1	.01032	14.66	.517	.93969	1.500	2.219 PER IMP=	70.00
ADD HYD	312.00	16 3 19	.13408	152.60	6.038	.84442	1.567	1.778	
COMPUTE NM HYD	V	- 11	.03200	36.76	1.254	.73474	1.500	1.795 PER IMP=	50.00
ADD HYD	SG.AT.82ND	11619 3	.16608	187.38	7.292	.82329	1.533	1.763	
ROUTE	314.00	3 5	.16608	186.17	7.292	.82329	1.567	1.752	
COMPUTE NM HYD	W	- 12	.03422	35.41	1.341	.73474	1.533	1.617 PER IMP=	50.00
ADD HYD	316.00	126 5 3	.20030	220.23	8.633	.80816	1.567	1.718	
COMPUTE NM HYD	X	- 13	.00674	10.49	.375	1.04216	1.500	2.431 PER IMP=	80.00
ADD HYD	SG.AT.UNSER	136 3 4	.20704	228.90	9.008	.81577	1.567	1.727	
ROUTE	318.00	4 5	.20704	230.04	9.008	.81577	1.567	1.736	
COMPUTE NM HYD	YD	- 14	.02964	48.72	1.742	1.10226	1.500	2.569 PER IMP=	85.00
*S TOTAL UNSER APX 300' S OF AMOLE CHANNEL AT BRIDGE: FUTURE/FULLY DEVELOPED									
ADD HYD	TOT.TO.AMOLE	146 5 7	.23668	270.23	10.750	.85165	1.567	1.784	
*S INTERIM INTERIM INTERIM									
*S INTERIM: RE-USE HYD 312 W/ ID=19, ROUTE IN DIRT CHAN ACROSS BASIN Y EXIST									
ROUTE MCUNGE	502.00	19 5	.13408	150.48	6.033	.84373	1.600	1.754 CCODE =	.2
COMPUTE NM HYD	YE	- 15	.02964	5.10	.142	.08996	1.533	.269 PER IMP=	.00
ADD HYD	INT.2.AMOLE	156 5 8	.16372	154.77	6.176	.70726	1.600	1.477	
*S INTERIM W/ V (POINTE WEST) INTERIM W/ V (POINTE WEST)									
*S RE-USE HYD 312 W/ ID=19, HYD V W/ ID=11, & HYD YE W/ ID=15									
*S ROUTE IN DIRT CHAN ACROSS BASIN Y EXIST									
ADD HYD	602.00	19611 3	.16608	187.38	7.292	.82329	1.533	1.763	
ROUTE MCUNGE	604.00	3 5	.16608	183.87	7.282	.82214	1.600	1.730 CCODE =	.2
ADD HYD	INT.V.2AMOLE	156 3 98	.19572	192.46	7.435	.71223	1.533	1.537	
*S ALLEY ALLEY ALLEY									
*S BASINS B, C, & SITE-1 TO ALLEY. BASIN A NOT CONTRIBUTE INTERIM/FUTURE									
*S FUTURE/INTERIM ALLEY FLOWS FOR INFO ONLY: HOLD TO EXISTING CONDITIONS									
COMPUTE NM HYD	B	- 1	.01520	23.33	.823	1.01536	1.500	2.398 PER IMP=	76.00
COMPUTE NM HYD	C	- 2	.01501	21.94	.766	.95742	1.500	2.284 PER IMP=	70.00
ADD HYD	%O.TOP.ALLEY	16 2 3	.03021	45.27	1.590	.98656	1.500	2.341	
COMPUTE NM HYD	SITE.1	- 1	.00151	2.05	.072	.88845	1.500	2.120 PER IMP=	65.00
ADD HYD	BOT.ALLEY	16 3 4	.03172	47.32	1.661	.98188	1.500	2.331	
FINISH									

ANYMO PROGRAM (ANYMO194) - ANAFCA Hydrologic Model - January, 1994  
 RUN DATE (MON/DAY/YR) = 11/05/1997  
 START TIME (HR:MIN:SEC) = 12:36:46 USER NO. = PERSEENG.194  
 INPUT FILE = CSGIF00B.DAT

```
* file (tg386) csqif00a.dat 10-15-96
* FINISH CODES AT START = 027 038 107 050 083
* 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
* CONTROL CODES AT END = 0 0 0 0 0
* 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
* CONTROL CODES ABOVE FOR HP DESKJET 540 INKJET PRINTER, START IN COL 21
*
* C PRINT CODES: 0=ALL; 1-TOTALS ONLY; 2-EVERY 2ND + TOTALS; 3,5,10,20 SIMILAR
* C RATING CURVE ID NEGATIVE -> COMPUTE BUT NOT PRINT RATING CURVE
* C RATING CURVE # NEGATIVE -> FLOODPLAIN SLOPE, # POSITIVE -> CHANNEL SLOPE
* S FILE CSGIF00A.DAT: Canto / Sunset Gardens, Interim & Future conditions,
* S (1)00-yr 6-hr storm, version A
* S
* S FOR INTERIM CONDITIONS, THE SUNSET GARDENS STORM DRAIN STOPS AT 82nd ST
* S AND FLOW IS ROUTED IN AN EARTH CHANNEL THROUGH AN UNDEVELOPED BASIN Y
* S TO THE HEAD OF THE AMOLE CHANNEL. SEE RECALLED HYD 314 AND HYD ____
* C
* C FOR INTERIM, FLOW AT 82nd & SUNSET GARDENS --PRIOR TO THE ADDITION OF FLOW
* C BASIN V (POINTE WEST SUBDV)-- IS SAVED FOR LATER RECALL AND ROUTING.
* C THE HYDS DIRECTLY FOLLOWING THE UNSAVED HYD 314 DON'T APPLY TO INTERIM
* C
* S FOR FUTURE, THE SUNSET GARDENS STORM DRAIN CONTINUES TO UNSER THEN
* S NORTH TO THE HEAD OF THE AMOLE CHANNEL. A FULLY DEVELOPED BASIN Y
* S CONTRIBUTES TO THIS FLOW, AS DO BASINS V (POINTE WEST), W, & X.
* S
* S ALL BASINS --EXCEPT BASIN Y AS NOTED ABOVE-- ARE IN FUTURE FULLY-DEVELOPED
* S CONDITIONS BASED ON CURRENT ZONING & DEVELOPMENT, CURRENT DEVELOPMENT PLANS,
* S AND ON ENGINEERING JUDGMENT.
* S
* C BASIN & CHANNEL ROUTING PARAMETERS REFLECT THE JUDGMENT OF THE ENGINEER,
* C AND MAY DIFFER FROM OTHER STUDIES IN THE AREA.
* C
* C REVISION NOTES: BASED ON FILES VCF4100 & SGU100.DAT BY TUCKER GREEN P.E.
* C REVISED 10-15-97 TO REFLECT NEW BASIN BOUNDARIES BASED ON
* C DISCUSSION WITH THE CITY, THE ENGINEERS FOR SAD 222, AND
* C DEVELOPERS OF NEARBY PROPERTIES, ESPECIALLY BASINS V & W.
* C IN PARTICULAR: (1) BASIN M (S OF SUNSET GARDENS, BETWEEN
* C 94TH & 98TH) IS REMOVED FROM INTERIM & FUTURE CONDITION CASES
* C BY PROPOSED CONSTRUCTION OF 94TH ST; AND (2) THE HIGH POINT
* C IN 86 ST IS MOVED NORTH TO THE SOUTH PROPERTY LINE OF THE
* C CANTO III SITE (BASIN JTD).
* C
* *****
* S RAINFALLS PER ALBUQUERQUE NM DPM - COMMENT OUT THOSE THAT DON'T APPLY
* S TYPE 1 IS 6-HR STORM PER NOAA ATLAS 2 W PEAK INTENSITY @ 1.4 HRS (EQ C1-C5)
* S FOR 6-HR USE DT = 0.033333 HR = 2 MINUTES
* S TYPE 2 IS 24-HR STORM PER NOAA ATLAS 2 W PEAK INTENSITY @ 1.4 HRS (EQ C1-C6)
* S FOR 24-HR USE DT = 0.0500 HR = 5 MINUTES
* S RAIN QUANTER = 0.0 EXCEPT FOR TYPE 3 (6-HR PHP: SEE ANYMO MANUAL)
* S
* *****
* S RAINFALL AMOUNTS, INCHES
* S HUNDRED TYPE= 2 RAIN QUANTER= 0.0 RAIN ONE= 2.23
* S RAIN SIX= 2.95 RAIN DAY= 3.76 DT= .033333 HR
* S HUNDRED TYPE= 1 0.0 1.90 2.22 2.67 0.033333
* S
* S COMPUTED 6-HOUR RAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2 - PEAK AT 1.40 HR.
* S DT = .033333 HOURS END TIME = 5.999940 HOURS
* S .0000 .0015 .0030 .0046 .0062 .0079 .0096
* S .0113 .0130 .0149 .0167 .0186 .0206 .0226
```

0000 0000 0806

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.0246 .0268 .0290 .0312 .0336 .0360 .0385
.0411 .0438 .0466 .0496 .0526 .0558 .0592
.0627 .0665 .0704 .0757 .0813 .0873 .1002
.1291 .1735 .2373 .3244 .4388 .5847 .7664
.9881 1.1931 1.2789 1.3514 1.4159 1.4745 1.5285
1.5786 1.6255 1.6694 1.7107 1.7497 1.7865 1.8214
1.8544 1.8857 1.9154 1.9436 1.9704 1.9765 1.9822
1.9876 1.9928 1.9977 2.0025 2.0070 2.0114 2.0156
2.0196 2.0235 2.0273 2.0310 2.0346 2.0381 2.0415
2.0448 2.0480 2.0511 2.0542 2.0571 2.0601 2.0629
2.0657 2.0685 2.0712 2.0738 2.0764 2.0789 2.0814
2.0839 2.0863 2.0887 2.0910 2.0933 2.0955 2.0978
2.0999 2.1021 2.1042 2.1063 2.1084 2.1104 2.1124
2.1144 2.1164 2.1183 2.1202 2.1221 2.1240 2.1258
2.1277 2.1295 2.1312 2.1330 2.1347 2.1365 2.1382
2.1399 2.1415 2.1432 2.1448 2.1464 2.1480 2.1496
2.1512 2.1527 2.1543 2.1558 2.1573 2.1588 2.1603
2.1618 2.1633 2.1647 2.1661 2.1676 2.1690 2.1704
2.1718 2.1732 2.1745 2.1759 2.1772 2.1786 2.1799
2.1812 2.1825 2.1838 2.1851 2.1864 2.1876 2.1889
2.1902 2.1914 2.1926 2.1939 2.1951 2.1963 2.1975
2.1987 2.1999 2.2010 2.2022 2.2034 2.2045 2.2057
2.2068 2.2080 2.2091 2.2102 2.2113 2.2124 2.2135
2.2146 2.2157 2.2168 2.2179 2.2189 2.2200

```

\* RAINFALL      YEAR TYPE= 1   0.0   1.23   1.48   1.78   0.033333

```

*****
COMPUTE KM HYD    ID= 1   HYD= 1      DA=0.00952   SQ MI
                  PER A= 12   B= 26      C= 24      D= 38
                  TP= -0.13333 HRS   RAIN= -1

```

```

K = .072665HR   TP = .133330HR   K/TP RATIO = .545000   SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 14.279   CFS   UNIT VOLUME = .9985      B = 526.28      P60 = 1.9000
AREA = .003618 SQ MI   IA = .10000 INCHES   INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

```

```

K = .127510HR   TP = .133330HR   K/TP RATIO = .956348   SHAPE CONSTANT, N = 3.695043
UNIT PEAK = 14.799   CFS   UNIT VOLUME = .9993      B = 334.30      P60 = 1.9000
AREA = .005902 SQ MI   IA = .10000 INCHES   INF = 1.16871 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

```

PRINT STD      ID= 1   CODE= 1

#### HYDROGRAPH FROM AREA 1

```

RUNOFF VOLUME = 1.21467 INCHES      = .6167 ACRE-Feet
PEAK DISCHARGE RATE = 18.64 CFS   AT 1.500 HOURS   BASIN AREA = .0095 SQ. MI.

```

```

*****
COMPUTE KM HYD    ID= 2   HYD= B      DA=0.01501   SQ MI
                  PER A= 0      B= 20      C= 10      D= 70
                  TP= -0.13333 HRS   RAIN= -1

```

```

K = .072665HR   TP = .133330HR   K/TP RATIO = .545000   SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 41.473   CFS   UNIT VOLUME = .9991      B = 526.28      P60 = 1.9000
AREA = .010507 SQ MI   IA = .10000 INCHES   INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

```

25X I □

32X I □

0000 0000 0807

K = .122603HR TP = .133330HR K/TP RATIO = .919546 SHAPE CONSTANT, N = 3.849372  
 UNIT PEAK = 11.652 CFS UNIT VOLUME = .9992 B = 345.00 P60 = 1.9000  
 AREA = .004503 SQ MI IA = .45000 INCHES INF = 1.11000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 2 CODE= 1

# HYDROGRAPH FROM AREA H

RUNOFF VOLUME = 1.62555 INCHES = 1.3013 ACRE-FEET  
 PEAK DISCHARGE RATE = 36.62 CFS AT 1.500 HOURS BASIN AREA = .0150 SQ. MI.

\*  
 \*\*\*\*\*  
 \*S E PLUS H PLUS I AT SUNSET GARDENS & 90TH FOLLOWS  
 ADD HYD ID OUT= 3 HYD= 208 IDIN I= 1 IDIN II= 2  
 PRINT HYD ID= 3 CODE= 1

# PARTIAL HYDROGRAPH 208.00

RUNOFF VOLUME = 1.46607 INCHES = 1.9180 ACRE-FEET  
 PEAK DISCHARGE RATE = 55.25 CFS AT 1.500 HOURS BASIN AREA = .0245 SQ. MI.

\*  
 \*\*\*\*\*  
 \*S DIVIDE SO 1ST 8.6 CFS (ID=6) S ON 90TH (ON HOLD): ID=4 E ON SUNSET GARDENS  
 DIVIDE HYD ID=3 Q=8.6 ID=6 HYD= 90.S.PAST.SG ID=4 HYD= SG.E.OF.90  
 PRINT HYD ID= 4 CODE= 1

# HYDROGRAPH FROM AREA SG.E.OF.90

RUNOFF VOLUME = 1.46607 INCHES = 1.0956 ACRE-FEET  
 PEAK DISCHARGE RATE = 46.65 CFS AT 1.500 HOURS BASIN AREA = .0140 SQ. MI.

PRINT HYD ID= 6 CODE= 1

# HYDROGRAPH FROM AREA 90.S.PAST.SG

RUNOFF VOLUME = 1.46607 INCHES = .8224 ACRE-FEET  
 PEAK DISCHARGE RATE = 8.60 CFS AT 1.333 HOURS BASIN AREA = .0105 SQ. MI.

\*  
 \*\*\*\*\*  
 \*S ROUTE MAIN FLOW EAST DOWN SG FROM 90TH, FOLLOW IT TO 86TH ST  
 \*C APPROX AS 40' F-F STREET, ASSUME APT 2.35% SLOPE  
 \*C ASSUME AS IF BOTH SIDES PAVED, EST n AS .017  
 COMPUTE RATING CURVE CID= -1 VS NO= 1 NO SEGS FOR MANNING n= 1  
 ELMIN= 0 ELMAX= 4 FT CHSLP= .0235 FPSLP= .0235 FT/FT  
 n .017 DIST 40  

DIST	ELEV	DIST	ELEV	DIST	ELEV
0	4	.01	0	20	.40
40	4			39.99	0

 ROUTE NCUNGE ID= 5 HYD= 209 INFLOW HYD ID= 4 DT= 0.0 HR  
 LENGTH= 1055 NSUBRCE= 0 SLOPE= .0235

25X

32X

0000 0000 0808

MAYCODE= 0 RECODE= 0 CCODE= 0  
Inflow ID end= 63 Max Number=600

dt = .0333 hr q0 = 23.33 cfs ck0 = 5.46 fps  
nlen = 4 dlen = 263.75

Depth ft	Area sf	Q cfs	Qbar cfs	ck fps	b ft	C	D	c1	c2	vel fps	fr	tt hr
.00	.0	.0	3.3	2.95	10.5	1.34	.02	.99	.15	2.95	1.40	.099
.21	2.2	6.5	24.6	5.46	30.5	2.48	.02	.99	.43	4.45	1.84	.066
.42	8.8	42.7	86.0	10.29	40.0	4.68	.03	.99	.65	6.59	2.03	.044
.63	17.3	129.3	189.2	14.23	40.0	6.47	.05	.99	.73	8.81	2.12	.033
.84	25.7	249.1	323.0	17.56	40.0	7.99	.07	.98	.78	10.81	2.20	.027
1.05	34.1	396.9	483.2	20.51	40.0	9.33	.10	.98	.81	12.62	2.27	.023
1.26	42.5	569.6	667.1	23.18	40.0	10.54	.12	.98	.83	14.28	2.33	.021
1.47	50.9	764.7	872.5	25.62	40.0	11.66	.14	.98	.84	15.82	2.37	.019
1.68	59.3	980.4	1097.7	27.88	40.0	12.69	.16	.98	.86	17.27	2.41	.017
1.89	67.8	1215.1	1341.3	29.99	40.0	13.64	.18	.98	.87	18.64	2.45	.016
2.11	76.2	1467.6	1602.1	31.97	40.0	14.54	.20	.97	.87	19.93	2.48	.015
2.32	84.6	1736.7	1879.1	33.83	40.0	15.39	.22	.97	.88	21.16	2.50	.014
2.53	93.0	2021.5	2171.3	35.59	40.0	16.19	.25	.97	.89	22.33	2.52	.013
2.74	101.4	2321.1	2478.0	37.25	40.0	16.95	.27	.97	.89	23.45	2.54	.012
2.95	109.9	2634.8	2798.3	38.84	40.0	17.67	.29	.97	.89	24.53	2.56	.012
3.16	118.3	2961.8	3131.6	40.34	40.0	18.36	.31	.97	.90	25.57	2.57	.011
3.37	126.7	3301.5	3477.4	41.78	40.0	19.01	.34	.97	.90	26.56	2.59	.011
3.58	135.1	3653.3	3835.0	43.16	40.0	19.63	.36	.97	.90	27.52	2.60	.011
3.79	143.5	4016.7	4204.0	44.47	40.0	20.23	.38	.96	.91	28.45	2.61	.010
4.00	152.0	4391.2	.0	.00	.0	.00	.00	.00	.00	.00	.00	.000

nlen= 4 Outflow ID end= 0  
Route using Ponce procedure: C1 > 0  
PRINT HYD ID= 5 CODE= 1

PARTIAL HYDROGRAPH 209.00

RUNOFF VOLUME = 1.46262 INCHES = 1.0931 ACRE-Feet  
PEAK DISCHARGE RATE = 46.50 CFS AT 1.567 HOURS BASIN AREA = .0140 SQ. MI.

\*\*\*\*\*  
COMPUTE NH HYD ID= 1 HYD= J DA=0.00228 SQ MI  
PER A= 0 B= 15 C= 0 D= 85  
TP= -0.13333 HRS RAIN= -1

K = .072665HR TP = .133330HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420  
UNIT PEAK = 7.6496 CFS UNIT VOLUME = .9978 B = 526.28 P60 = 1.9000  
AREA = .001938 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR  
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .130790HR TP = .133330HR K/TP RATIO = .980950 SHAPE CONSTANT, N = 3.599935  
UNIT PEAK = .84019 CFS UNIT VOLUME = .9837 B = 327.55 P60 = 1.9000  
AREA = .000342 SQ MI IA = .50000 INCHES INF = 1.25000 INCHES PER HOUR  
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 1 CODE= 1

HYDROGRAPH FROM AREA J

RUNOFF VOLUME = 1.79112 INCHES = .2178 ACRE-Feet  
PEAK DISCHARGE RATE = 5.97 CFS AT 1.500 HOURS BASIN AREA = .0023 SQ. MI.

25x10

32x10



0000 0000 0804

\*\*\*\*\*  
 ADD HYD ID OUT= 3 HYD= 210 IDIN 1= 1 IDIN 11= 5  
 PRINT HYD ID= 3 CODE= 1

## PARTIAL HYDROGRAPH 210.00

RUNOFF VOLUME = 1.50855 INCHES = 1.3108 ACRE-Feet  
 PEAK DISCHARGE RATE = 51.44 CFS AT 1.567 HOURS BASIN AREA = .0163 SQ. MI.

\*\*\*\*\*  
 \*S CALC CONTRIBUTING PART OF CANYO SITE; THEN ADD TO HYD 210  
 COMPUTE NM HYD ID= 1 HYD=SITE.II DA=0.00839 SQ MI  
 PER A= 0 B= 35 C= 0 D= 65  
 TP= -0.13333 HRS RAIN= -1

K = .072665HR TP = .133330HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420  
 UNIT PEAK = 21.526 CFS UNIT VOLUME = .9988 B = 526.28 P60 = 1.9000  
 AREA = .005454 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .130790HR TP = .133330HR K/TP RATIO = .980950 SHAPE CONSTANT, N = 3.599935  
 UNIT PEAK = 7.2141 CFS UNIT VOLUME = .9985 B = 327.55 P60 = 1.9000  
 AREA = .002937 SQ MI IA = .50000 INCHES INF = 1.25000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 1 CODE= 5

## HYDROGRAPH FROM AREA SITE.II

TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS
.000	.0	1.500	19.4	3.000	.2	4.500	.1	6.000	.1
.167	.0	1.667	10.0	3.167	.2	4.667	.1	6.167	.0
.333	.0	1.833	5.9	3.333	.1	4.833	.1	6.333	.0
.500	.0	2.000	4.2	3.500	.1	5.000	.1	6.500	.0
.667	.0	2.167	2.0	3.667	.1	5.167	.1	6.667	.0
.833	.0	2.333	.9	3.833	.1	5.333	.1	6.833	.0
1.000	.0	2.500	.6	4.000	.1	5.500	.1		
1.167	.0	2.667	.4	4.167	.1	5.667	.1		
1.333	.4	2.833	.3	4.333	.1	5.833	.1		

RUNOFF VOLUME = 1.53130 INCHES = .6852 ACRE-Feet  
 PEAK DISCHARGE RATE = 19.39 CFS AT 1.500 HOURS BASIN AREA = .0084 SQ. MI.

\*\*\*\*\*  
 \*S PARTIAL WATERBLOCK ==> FLOW > 11.6cfs TO 86TH (ID=7, WOULD FOR LATER)  
 DIVIDE HYD ID=1 Q=11.6 ID=2 HYD=S2.T0.S3 ID=7 HYD=S2.T0.86TH  
 PRINT HYD ID= 2 CODE= 5

## HYDROGRAPH FROM AREA S2.T0.S3

TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS
.000	.0	1.500	11.6	3.000	.2	4.500	.1	6.000	.1
.167	.0	1.667	10.0	3.167	.2	4.667	.1	6.167	.0
.333	.0	1.833	5.9	3.333	.1	4.833	.1	6.333	.0

25X

32X

.500	.0	2.000	4.2	3.500	.1	5.000	.1	6.500	.0
.667	.0	2.167	2.0	3.667	.1	5.167	.1	6.667	.0
.833	.0	2.333	.9	3.833	.1	5.333	.1	6.833	.0
1.000	.0	2.500	.6	4.000	.1	5.500	.1		
1.167	.0	2.667	.4	4.167	.1	5.667	.1		
1.333	4.8	2.833	.3	4.333	.1	5.833	.1		

RUNOFF VOLUME = 1.53126 INCHES = .6024 ACRE-Feet  
 PEAK DISCHARGE RATE = 11.60 CFS AT 1.433 HOURS BASIN AREA = .0074 SQ. MI.

PRINT HYD ID= 7 CODE= 5

#### HYDROGRAPH FROM AREA S2.T0.86TH

TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS
.000	.0	.333	.0	.667	.0	1.000	.0	1.333	.0
.167	.0	.500	.0	.833	.0	1.167	.0	1.500	7.8

RUNOFF VOLUME = 1.53126 INCHES = .0828 ACRE-Feet  
 PEAK DISCHARGE RATE = 7.79 CFS AT 1.500 HOURS BASIN AREA = .0010 SQ. MI.

\*\*\*\*\*  
 COMPUTE HYD ID= 1 HYD-SITE.III DA=0.02360 SQ MI  
 PER A= 0 B= 35 C= 0 D= 65  
 TP= -0.13333 HRS RAIN= -1

K = .072665HR TP = .133330HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420  
 UNIT PEAK = 60.549 CFS UNIT VOLUME = .9992 B = 526.28 P60 = 1.9000  
 AREA = .015340 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .130790HR TP = .133330HR K/TP RATIO = .980950 SHAPE CONSTANT, N = 3.599933  
 UNIT PEAK = 20.292 CFS UNIT VOLUME = .9997 B = 327.55 P60 = 1.9000  
 AREA = .008260 SQ MI IA = .50000 INCHES INF = 1.25000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 1 CODE= 2

#### HYDROGRAPH FROM AREA SITE.III

TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS
.000	.0	1.467	49.5	2.933	.6	4.400	.2	5.867	.3
.067	.0	1.533	52.4	3.000	.6	4.467	.2	5.933	.3
.133	.0	1.600	38.6	3.067	.5	4.533	.2	6.000	.3
.200	.0	1.667	28.1	3.133	.5	4.600	.2	6.067	.3
.267	.0	1.733	22.1	3.200	.4	4.667	.2	6.133	.2
.333	.0	1.800	18.2	3.267	.4	4.733	.2	6.200	.1
.400	.0	1.867	15.5	3.333	.4	4.800	.2	6.267	.0
.467	.0	1.933	13.4	3.400	.3	4.867	.2	6.333	.0
.533	.0	2.000	11.8	3.467	.3	4.933	.2	6.400	.0
.600	.0	2.067	10.1	3.533	.3	5.000	.2	6.467	.0
.667	.0	2.133	6.9	3.600	.3	5.067	.2	6.533	.0
.733	.0	2.200	4.5	3.667	.3	5.133	.2	6.600	.0
.800	.0	2.267	3.3	3.733	.3	5.200	.3	6.667	.0
.867	.0	2.333	2.7	3.800	.3	5.267	.3	6.733	.0
.933	.0	2.400	2.2	3.867	.3	5.333	.3	6.800	.0
1.000	.0	2.467	1.8	3.933	.2	5.400	.3	6.867	.0
1.067	.0	2.533	1.5	4.000	.2	5.467	.3	6.933	.0

0000 0000 08 11

1.133	.0	2.600	1.3	4.067	.2	5.533	.3	7.000	.0
1.200	.6	2.667	1.1	4.133	.2	5.600	.3	7.067	.0
1.267	5.0	2.733	.9	4.200	.2	5.667	.3		
1.333	13.6	2.800	.8	4.267	.2	5.733	.3		
1.400	28.8	2.867	.7	4.333	.2	5.800	.3		

RUNOFF VOLUME = 1.53130 INCHES = 1.9274 ACRE-Feet  
 PEAK DISCHARGE RATE = 54.51 CPS AT 1.500 HOURS BASIN AREA = .0236 SQ. MI.

\*\*\*\*\*  
 \*S TOTAL FLOW LEAVING CANTO NORTH OF SUNSET GARDENS  
 ADD HYD ID OUT= 16 HYD= SITE.OUT IDIN I= 1 IDIN II= 2  
 PRINT HYD ID= 16 CODE= 1

#### HYDROGRAPH FROM AREA SITE.OUT

RUNOFF VOLUME = 1.53128 INCHES = 2.5298 ACRE-Feet  
 PEAK DISCHARGE RATE = 66.11 CPS AT 1.500 HOURS BASIN AREA = .0310 SQ. MI.

\*\*\*\*\*  
 \*S TOTAL FLOW SUNSET GARDENS WEST OF 86TH  
 ADD HYD ID OUT= 5 HYD= SG.W.OF.86 IDIN I= 3 IDIN II= 16  
 PRINT HYD ID= 5 CODE= 1

#### HYDROGRAPH FROM AREA SG.W.OF.86

RUNOFF VOLUME = 1.52344 INCHES = 3.8406 ACRE-Feet  
 PEAK DISCHARGE RATE = 115.19 CPS AT 1.533 HOURS BASIN AREA = .0473 SQ. MI.

\*\*\*\*\*  
 COMPUTE NH HYD ID= 1 HYD= C DA=0.00127 SQ MI  
 PEN A= 0 B= 10 C= 0 D= 90  
 TP= -0.13333 HRS RAIN= -1

K = .072665HR TP = .133330HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420  
 UNIT PEAK = 4.5116 CPS UNIT VOLUME = .9969 B = 526.28 P60 = 1.9000  
 AREA = .001143 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .130790HR TP = .133330HR K/TP RATIO = .988950 SHAPE CONSTANT, N = 3.599935  
 UNIT PEAK = .31200 CPS UNIT VOLUME = .9579 B = 327.55 P60 = 1.9000  
 AREA = .000127 SQ MI IA = .50000 INCHES INF = 1.25000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 1 CODE= 1

#### HYDROGRAPH FROM AREA C

RUNOFF VOLUME = 1.85607 INCHES = .1257 ACRE-Feet  
 PEAK DISCHARGE RATE = 3.43 CPS AT 1.500 HOURS BASIN AREA = .0013 SQ. MI.

25x1

32x1



\*\*\*\*\*  
 \*C ADD SPILL FROM S2 TO ROAD FLOW IN 86TH N OF SUNSET GARDENS  
 ADD HYD ID OUT= 3 HYD= 218 IDIN I= 1 IDIN II= 7  
 PRINT HYD ID= 3 CODE= 1

PARTIAL HYDROGRAPH 218.00

RUNOFF VOLUME = 1.71179 INCHES = .2085 ACRE-FEET  
 PEAK DISCHARGE RATE = 11.22 CFS AT 1.500 HOURS BASIN AREA = .0023 SQ. MI.

\*\*\*\*\*  
 \*S COMBINED FLOW TO 86TH & SUNSET GARDENS FROM NORTH & WEST; HOLD FOR LATER  
 ADD HYD ID OUT= 7 HYD= 866SG.N&W IDIN I= 3 IDIN II= 5  
 PRINT HYD ID= 7 CODE= 1

HYDROGRAPH FROM AREA 866SG.N&W

RUNOFF VOLUME = 1.53212 INCHES = 4.0491 ACRE-FEET  
 PEAK DISCHARGE RATE = 125.49 CFS AT 1.533 HOURS BASIN AREA = .0496 SQ. MI.

\*\*\*\*\*  
 \*S  
 \*C BASIN NW (N North): CURRENTLY PARTLY DEVELOPED  
 COMPUTE NW HYD ID= 1 HYD= NW DA=0.01830 SQ MI  
 PER A= 28.0 B= 20.2 C= 15.4 D= 36.4  
 TP= -0.13333 HRS RAIN= -1  
 K = .072665HR TP = .133330HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420  
 UNIT PEAK = 26.293 CFS UNIT VOLUME = .9989 B = 526.28 P60 = 1.9000  
 AREA = .006661 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DY = .033333

K = .139008HR TP = .133330HR K/TP RATIO = 1.042583 SHAPE CONSTANT, N = 3.386093  
 UNIT PEAK = 27.229 CFS UNIT VOLUME = .9996 B = 311.92 P60 = 1.9000  
 AREA = .011639 SQ MI IA = .52972 INCHES INF = 1.33321 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DY = .033333

PRINT HYD ID= 1 CODE= 0

HYDROGRAPH FROM AREA NW

TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS
.000	.0	1.400	15.4	2.800	.5	4.200	.1	5.600	.1
.033	.0	1.433	22.7	2.833	.5	4.233	.1	5.633	.1
.067	.0	1.467	29.5	2.867	.4	4.267	.1	5.667	.1
.100	.0	1.500	33.0	2.900	.4	4.300	.1	5.700	.1
.133	.0	1.533	32.2	2.933	.4	4.333	.1	5.733	.1
.167	.0	1.567	28.6	2.967	.3	4.367	.1	5.767	.1
.200	.0	1.600	24.4	3.000	.3	4.400	.1	5.800	.1
.233	.0	1.633	20.7	3.033	.3	4.433	.1	5.833	.1
.267	.0	1.667	17.6	3.067	.3	4.467	.1	5.867	.1
.300	.0	1.700	15.1	3.100	.3	4.500	.1	5.900	.1
.333	.0	1.733	13.1	3.133	.3	4.533	.1	5.933	.1
.367	.0	1.767	11.5	3.167	.2	4.567	.1	5.967	.1
.400	.0	1.800	10.2	3.200	.2	4.600	.1	6.000	.1

0000 0000 08 15

.433	.0	1.833	9.0	3.233	.2	4.633	.1	6.033	.1
.467	.0	1.867	8.2	3.267	.2	4.667	.1	6.067	.1
.500	.0	1.900	7.5	3.300	.2	4.700	.1	6.100	.1
.533	.0	1.933	6.9	3.333	.2	4.733	.1	6.133	.1
.567	.0	1.967	6.4	3.367	.2	4.767	.1	6.167	.1
.600	.0	2.000	6.0	3.400	.2	4.800	.1	6.200	.0
.633	.0	2.033	5.6	3.433	.2	4.833	.1	6.233	.0
.667	.0	2.067	5.1	3.467	.2	4.867	.1	6.267	.0
.700	.0	2.100	4.4	3.500	.2	4.900	.1	6.300	.0
.733	.0	2.133	3.6	3.533	.2	4.933	.1	6.333	.0
.767	.0	2.167	3.0	3.567	.1	4.967	.1	6.367	.0
.800	.0	2.200	2.5	3.600	.1	5.000	.1	6.400	.0
.833	.0	2.233	2.1	3.633	.1	5.033	.1	6.433	.0
.867	.0	2.267	1.9	3.667	.1	5.067	.1	6.467	.0
.900	.0	2.300	1.7	3.700	.1	5.100	.1	6.500	.0
.933	.0	2.333	1.5	3.733	.1	5.133	.1	6.533	.0
.967	.0	2.367	1.4	3.767	.1	5.167	.1	6.567	.0
1.000	.0	2.400	1.3	3.800	.1	5.200	.1	6.600	.0
1.033	.0	2.433	1.2	3.833	.1	5.233	.1	6.633	.0
1.067	.0	2.467	1.1	3.867	.1	5.267	.1	6.667	.0
1.100	.0	2.500	1.0	3.900	.1	5.300	.1	6.700	.0
1.133	.0	2.533	.9	3.933	.1	5.333	.1	6.733	.0
1.167	.0	2.567	.8	3.967	.1	5.367	.1	6.767	.0
1.200	.3	2.600	.8	4.000	.1	5.400	.1	6.800	.0
1.233	1.0	2.633	.7	4.033	.1	5.433	.1	6.833	.0
1.267	2.2	2.667	.7	4.067	.1	5.467	.1	6.867	.0
1.300	3.8	2.700	.6	4.100	.1	5.500	.1	6.900	.0
1.333	6.0	2.733	.6	4.133	.1	5.533	.1		
1.367	9.7	2.767	.5	4.167	.1	5.567	.1		

RUNOFF VOLUME = 1.12653 INCHES = 1.0995 ACRE-Feet  
 PEAK DISCHARGE RATE = 32.97 CFS AT 1.500 HOURS BASIN AREA = .0183 SQ. MI.

\*\*\*\*\*  
 \*S ADD IN HYD 90.S.PAST.SG. ('HELD' SPILL SOUTH OF SUNSET GONS INTERSECTION)  
 ADD HYD ID OUT= 3 HYD= INTO.JYDN IDIN I= 1 IDIN II= 6  
 PRINT HYD ID= 3 CODE= 1

## HYDROGRAPH FROM AREA INTO.JYDN

RUNOFF VOLUME = 1.25044 INCHES = 1.9218 ACRE-Feet  
 PEAK DISCHARGE RATE = 41.57 CFS AT 1.500 HOURS BASIN AREA = .0288 SQ. MI.

\*\*\*\*\*  
 \*S ROUTE NORTH PART OF OFFSITE THROUGH NORTH STREET IN JYD  
 \*C APPROX AS 28' F-F STREET, ASSUME APX 1.8% SLOPE  
 \*C ASSUME PAVED ROAD, EST n AS .017  
 COMPUTE RATING CURVE CID= -1 VS NO= 1 NO SECS FOR MANNING n= 1  
 ELMIN= 0 ELMAX= 4 FT CHSLP= .018 PPSLP= .018 FT/FT  
 n .017 DIST 28  
 DIST ELEV DIST ELEV DIST ELEV DIST ELEV  
 0 4 .01 0 14 .28 27.99 0  
 28 4  
 ROUTE NCURGE ID= 5 HYD= 100 INFLOW HYD ID= 3 DT= 0.0 HR  
 LENGTH= 1338 NSUBRCH= 0 SLOPE= .018  
 MAYCODE= 0 REGCODE= 0 CCODE= 0  
 Inflow ID end=211 Max Number=600

dt = .0333 hr q0 = 20.78 cfs ckd = 5.86 fps

25x10

32x10

0000 0000 08 16

nlen = 4 dlen = 334.50

Depth ft	Area sf	Q cfs	Qbar cfs	ck fps	b ft	C	D	c1	c2	vel fps	fr	tt hr
.00	.0	.0	2.9	2.58	10.5	.93	.02	.98	-.03	2.58	1.40	.144
.21	2.2	5.7	22.3	5.86	24.5	2.10	.03	.98	.36	4.42	1.72	.084
.42	7.9	38.8	68.2	9.97	28.0	3.58	.04	.98	.57	6.31	1.79	.059
.63	13.8	97.6	136.3	13.15	28.0	4.72	.06	.98	.65	8.16	1.86	.046
.84	19.6	175.0	221.8	15.86	28.0	5.69	.08	.98	.70	9.82	1.93	.038
1.05	25.5	268.5	322.2	18.24	28.0	6.54	.10	.97	.74	11.31	1.98	.033
1.26	31.4	376.0	436.0	20.38	28.0	7.31	.13	.97	.76	12.68	2.02	.029
1.47	37.3	496.1	561.9	22.33	28.0	8.01	.15	.97	.78	13.95	2.05	.027
1.68	43.2	627.7	698.7	24.12	28.0	8.65	.17	.97	.80	15.14	2.08	.025
1.89	49.1	769.8	845.8	25.78	28.0	9.25	.19	.96	.81	16.25	2.10	.023
2.11	55.0	921.7	1002.2	27.32	28.0	9.80	.22	.96	.82	17.30	2.12	.021
2.32	60.9	1082.7	1167.4	28.76	28.0	10.32	.24	.96	.83	18.29	2.13	.020
2.53	66.8	1252.2	1340.9	30.10	28.0	10.80	.26	.96	.83	19.23	2.15	.019
2.74	72.7	1429.6	1522.0	31.37	28.0	11.25	.29	.95	.84	20.13	2.16	.018
2.95	78.6	1614.4	1710.4	32.56	28.0	11.68	.31	.95	.85	20.98	2.17	.018
3.16	84.5	1806.3	1905.6	33.69	28.0	12.09	.34	.95	.85	21.80	2.17	.017
3.37	90.4	2004.9	2107.3	34.75	28.0	12.47	.36	.95	.86	22.58	2.18	.016
3.58	96.3	2209.7	2315.1	35.76	28.0	12.83	.38	.95	.86	23.34	2.18	.016
3.79	102.1	2420.5	2528.8	36.73	28.0	13.17	.41	.94	.86	24.06	2.19	.015
4.00	108.0	2637.0	.0	.00	.0	.00	.00	.00	.00	.00	.00	.000

nlen = 4 Outflow ID end=213  
Route using Ponce procedure: C1 > 0  
nlen = 4 Outflow ID end=215  
Route using Maidment procedure: C0, C1 & C2 > 0  
PRINT HYD ID= 5 CODE= 1

## HYDROGRAPH FROM AREA 300.00

RUNOFF VOLUME = 1.24326 INCHES = 1.9108 ACRE-Feet  
PEAK DISCHARGE RATE = 39.88 CPS AT 1.600 HOURS BASIN AREA = .0288 SQ. MI.

\*\*\*\*\*  
\* C BASIN NS (N South): CURRENTLY PARTLY DEVELOPED  
COMPUTE NM HYD ID= 1 HYD= NS DA=0.01719 SQ MI  
PER A= 16.0 B= 28.6 C= 8.8 D= 46.6  
TP= -0.13333 HRS RAIN= -1

K = .072665HR TP = .133330HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420  
UNIT PEAK = 31.619 CPS UNIT VOLUME = .9990 B = 526.28 P60 = 1.9000  
AREA = .008011 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR  
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .136383HR TP = .133330HR K/TP RATIO = 1.022896 SHAPE CONSTANT, N = 3.450895  
UNIT PEAK = 21.806 CPS UNIT VOLUME = .9996 B = 316.73 P60 = 1.9000  
AREA = .009179 SQ MI IA = .52022 INCHES INF = 1.30663 INCHES PER HOUR  
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 1 CODE= 1

## HYDROGRAPH FROM AREA NS

RUNOFF VOLUME = 1.27301 INCHES = 1.1671 ACRE-Feet  
PEAK DISCHARGE RATE = 34.17 CPS AT 1.500 HOURS BASIN AREA = .0172 SQ. MI.

25X

32X

0000 0000 08 17

\*\*\*\*\*  
 \*S ROUTE SOUTH PART OF OFFSITE THROUGH SOUTH STREET IN JVD  
 \*C APPROX AS 28' P-F STREET, ASSUME APX 2.0% SLOPE (STEEPER THAN NORTH)  
 \*C ASSUME PAVED ROAD, EST n AS .017  
 COMPUTE RATING CURVE CID= -1 VS NO= 1 NO SEGS FOR MANNING n= 1  
 ELMIN= 0 ELMAX= 4 FT CHSLP= .020 FPSLP= .020 FT/FT  
 n .017 DIST 28  
 DIST ELEV DIST ELEV DIST ELEV DIST ELEV  
 0 4 .01 0 14 .28 27.99 0  
 28 4  
 ROUTE NCUNGE ID= 2 HYD= 302 INFLOW HYD ID= 1 DT= 0.0 HR  
 LENGTH= 1221 NSUBRC= 0 SLOPE= .020  
 MATCODE= 0 REGCODE= 0 CCODE= 0  
 Inflow ID end=209 Max Number=600  
 dt = .0333 hr q0 = 17.08 cfs ch0 = 6.17 fps  
 nlen = 4 dlen = 305.25

Depth ft	Area sf	Q cfs	Qbar cfs	ch fps	b ft	C	D	c1	c2	vel fps	fr	tt hr
.00	.0	.0	3.0	2.72	10.5	1.07	.02	.98	.04	2.72	1.48	.125
.21	2.2	6.0	23.5	6.17	24.5	2.43	.03	.99	.42	4.65	1.81	.073
.42	7.9	40.9	71.9	10.51	28.0	4.13	.04	.98	.61	6.65	1.88	.051
.63	13.8	102.8	143.7	13.86	28.0	5.45	.06	.98	.69	8.60	1.96	.039
.84	19.6	184.5	233.8	16.72	28.0	6.57	.08	.98	.74	10.35	2.03	.033
1.05	25.5	283.0	339.6	19.23	28.0	7.56	.10	.98	.77	11.92	2.08	.028
1.26	31.4	396.3	459.6	21.49	28.0	8.45	.13	.97	.79	13.37	2.13	.025
1.47	37.3	522.9	592.2	23.54	28.0	9.25	.15	.97	.81	14.71	2.16	.023
1.68	43.2	661.6	736.5	25.43	28.0	10.00	.17	.97	.82	15.96	2.19	.021
1.89	49.1	811.4	891.5	27.17	28.0	10.68	.19	.97	.83	17.13	2.21	.020
2.11	55.0	971.6	1056.4	28.80	28.0	11.32	.21	.97	.84	18.23	2.23	.019
2.32	60.9	1141.3	1230.6	30.31	28.0	11.92	.24	.96	.85	19.28	2.25	.018
2.53	66.8	1319.9	1413.4	31.73	28.0	12.47	.26	.96	.85	20.27	2.26	.017
2.74	72.7	1506.9	1604.3	33.06	28.0	13.00	.28	.96	.86	21.21	2.27	.016
2.95	78.6	1701.8	1802.9	34.32	28.0	13.49	.31	.96	.86	22.12	2.28	.015
3.16	84.5	1904.0	2008.7	35.51	28.0	13.96	.33	.96	.87	22.98	2.29	.015
3.37	90.4	2113.3	2221.3	36.63	28.0	14.40	.35	.95	.87	23.81	2.30	.014
3.58	96.3	2329.3	2440.4	37.70	28.0	14.82	.38	.95	.88	24.60	2.30	.014
3.79	102.1	2551.5	2665.6	38.71	28.0	15.22	.40	.95	.88	25.36	2.31	.013
4.00	108.0	2779.7	.0	.00	.0	.00	.00	.00	.00	.00	.00	.000

nlen= 4 Outflow ID end=206  
 Route using Ponce procedure: C1 > 0  
 PRINT HYD ID= 2 CODE= 1

HYDROGRAPH FROM AREA 302.00

RUNOFF VOLUME = 1.27335 INCHES = 1.1674 ACRE-Feet  
 PEAK DISCHARGE RATE = 33.65 CFS AT 1.567 HOURS BASIN AREA = .0172 SQ. MI.

\*\*\*\*\*  
 \*C ADD NORTH & SOUTH ROUTED OFFSITE, THEN COMPUTE & ADD JVD  
 ADD HYD ID OUT= 3 HYD= 304 IDIN I= 2 IDIN II= 5  
 PRINT HYD ID= 3 CODE= 1

HYDROGRAPH FROM AREA 304.00

RUNOFF VOLUME = 1.25449 INCHES = 3.0782 ACRE-Feet  
 PEAK DISCHARGE RATE = 72.69 CFS AT 1.609 HOURS BASIN AREA = .0460 SQ. MI.

25x10

32x10

\*\*\*\*\*  
 COMPUTE HYD ID= 17 HYD= JYD DA=0.02353 SQ MI  
 PER A= 0 B= 35 C= 0 D= 65  
 TP= -0.13333 HRS RAIN= -1

K = .072665HR TP = .133330HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420  
 UNIT PEAK = 60.370 CFS UNIT VOLUME = .9992 B = 526.28 P60 = 1.9000  
 AREA = .015295 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .130790HR TP = .133330HR K/TP RATIO = .980950 SHAPE CONSTANT, N = 3.599935  
 UNIT PEAK = 20.232 CFS UNIT VOLUME = .9997 B = 327.55 P60 = 1.9000  
 AREA = .008236 SQ MI IA = .50000 INCHES INF = 1.25000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 17 CODE= 2

#### HYDROGRAPH FROM AREA JYD

TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS
.000	.0	1.467	49.3	2.933	.6	4.400	.2	5.867	.3
.067	.0	1.533	52.2	3.000	.6	4.467	.2	5.933	.3
.133	.0	1.600	38.5	3.067	.5	4.533	.2	6.000	.3
.200	.0	1.667	28.0	3.133	.5	4.600	.2	6.067	.3
.267	.0	1.733	22.0	3.200	.4	4.667	.2	6.133	.2
.333	.0	1.800	18.2	3.267	.4	4.733	.2	6.200	.1
.400	.0	1.867	15.4	3.333	.4	4.800	.2	6.267	.0
.467	.0	1.933	13.4	3.400	.3	4.867	.2	6.333	.0
.533	.0	2.000	11.8	3.467	.3	4.933	.2	6.400	.0
.600	.0	2.067	10.1	3.533	.3	5.000	.2	6.467	.0
.667	.0	2.133	6.9	3.600	.3	5.067	.2	6.533	.0
.733	.0	2.200	4.5	3.667	.3	5.133	.2	6.600	.0
.800	.0	2.267	3.3	3.733	.3	5.200	.3	6.667	.0
.867	.0	2.333	2.6	3.800	.3	5.267	.3	6.733	.0
.933	.0	2.400	2.2	3.867	.3	5.333	.3	6.800	.0
1.000	.0	2.467	1.8	3.933	.2	5.400	.3	6.867	.0
1.067	.0	2.533	1.5	4.000	.2	5.467	.3	6.933	.0
1.133	.0	2.600	1.3	4.067	.2	5.533	.3	7.000	.0
1.200	.6	2.667	1.1	4.133	.2	5.600	.3	7.067	.0
1.267	5.0	2.733	.9	4.200	.2	5.667	.3		
1.333	13.6	2.800	.8	4.267	.2	5.733	.3		
1.400	28.8	2.867	.7	4.333	.2	5.800	.3		

RUNOFF VOLUME = 1.53130 INCHES = 1.9217 ACRE-FEET  
 PEAK DISCHARGE RATE = 54.35 CFS AT 1.500 HOURS BASIN AREA = .0235 SQ. MI.

\*\*\*\*\*  
 \*S TOTAL FLOW LEAVING JYD (CANTO III), INCLUDING 86TH ST ROW EAST OF JYD  
 ADD HYD ID OUT= 4 HYD= JYD.E.AT.86 IDIN I= 3 IDIN II= 17  
 PRINT HYD ID= 4 CODE= 1

#### HYDROGRAPH FROM AREA JYD.E.AT.86

RUNOFF VOLUME = 1.34815 INCHES = 4.9998 ACRE-FEET  
 PEAK DISCHARGE RATE = 116.71 CFS AT 1.533 HOURS BASIN AREA = .0695 SQ. MI.



0000 0000 08 19

\*\*\*\*\*  
 \*S ROUTE TO 86TH & SG INTERSECTION, ASSUME 48" PIPE W/ 1% FRICTION SLOPE  
 COMPUTE RATING CURVE CID= -1 VSN= 1 CODE= -1 S= .010 D= 4 FT n= 0.013  
 ROUTE MOUNGE ID= 5 HYD= 86.S.OF.SG INFLOW HYD ID= 4 DT= 0.0 HR  
 LENGTH= 300 NSUBRC= 0 SLOPE= .010  
 HAYCODE= 0 REGCODE= 0 CRODE= 0  
 Inflow ID end=215 Max Number=600

dt = .0333 hr q0 = 58.35 cfs ck0 = 14.67 fps  
 nlen = 1 dlen = 300.00

Depth ft	Area sf	Q cfs	Qbar cfs	ck fps	b ft	C	D	cl	c2	vel fps	fr hr	tt hr
.00	.0	.0	.4	3.02	.9	1.21	.05	.96	.11	3.02	1.42	.028
.21	.2	.8	2.0	5.66	2.1	2.26	.06	.97	.40	4.26	1.59	.020
.42	.7	3.3	5.4	7.74	2.7	3.09	.09	.96	.52	5.58	1.63	.015
.63	1.3	7.6	10.6	9.44	3.1	3.78	.12	.95	.59	6.75	1.66	.012
.83	1.9	13.7	17.5	10.88	3.4	4.35	.16	.94	.64	7.78	1.68	.011
1.04	2.6	21.4	25.9	12.09	3.6	4.84	.20	.93	.67	8.69	1.69	.010
1.25	3.4	30.5	35.6	13.12	3.8	5.25	.24	.93	.69	9.50	1.68	.009
1.46	4.1	40.8	46.5	13.98	3.9	5.59	.28	.92	.71	10.21	1.67	.008
1.67	5.0	52.2	58.3	14.67	4.0	5.87	.33	.91	.72	10.84	1.64	.008
1.88	5.8	64.3	70.7	15.19	4.0	6.08	.39	.90	.73	11.39	1.61	.007
2.08	6.6	77.0	83.4	15.54	4.0	6.22	.45	.88	.74	11.86	1.58	.007
2.29	7.5	89.9	96.3	15.69	4.0	6.28	.51	.87	.74	12.25	1.54	.007
2.50	8.3	102.7	108.9	15.62	4.0	6.25	.58	.85	.74	12.57	1.51	.007
2.71	9.1	115.1	120.9	15.27	4.0	6.11	.66	.83	.74	12.81	1.47	.007
2.92	9.8	126.7	131.9	14.52	4.0	5.81	.76	.80	.74	12.96	1.43	.006
3.13	10.5	137.1	141.5	13.18	4.0	5.27	.89	.75	.72	13.02	1.39	.006
3.34	11.2	145.8	148.9	10.71	4.0	4.29	1.16	.64	.69	12.96	1.35	.006
3.54	11.8	152.0	153.2	5.41	4.0	2.16	2.36	.14	.64	12.76	1.30	.007
3.75	12.2	154.5	154.5	.00	4.0	.00	****	-1.00	1.00	12.46	1.25	.007
4.00	12.6	154.5	.0	.00	.0	.00	.00	.00	.00	.00	.00	.000

nlen= 1 Outflow ID end=215  
 Route using Ponce procedure: C1 > 0  
 nlen= 1 Outflow ID end=216  
 Route using Maidment procedure: C0, C1 & C2 > 0  
 PRINT HYD ID= 5 CODE= 1

## HYDROGRAPH FROM AREA 86.S.OF.SG

RUNOFF VOLUME = 1.34764 INCHES = 4.9979 ACRE-Feet  
 PEAK DISCHARGE RATE = 116.55 CFS AT 1.567 HOURS BASIN AREA = .0695 SQ. MI.

\*\*\*\*\*  
 \*S \*AS IF\* COMBINED FLOWS AT 86TH & SUNSET GARDENS: RETRIEVE 'ON-HOLD' ID=7  
 ADD HYD ID OUT= 6 HYD= TOT.SG686 IDIN I= 5 IDIN II= 7  
 PRINT HYD ID= 6 CODE= 2

## HYDROGRAPH FROM AREA TOT.SG686

TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS
.000	.0	1.467	180.7	2.933	3.5	4.400	1.0	5.867	1.3
.067	.0	1.533	235.7	3.000	3.1	4.467	1.0	5.933	1.3
.133	.0	1.600	211.8	3.067	2.7	4.533	1.0	6.000	1.3
.200	.0	1.667	165.8	3.133	2.4	4.600	1.0	6.067	1.3
.267	.0	1.733	125.4	3.200	2.2	4.667	1.0	6.133	1.1
.333	.0	1.800	98.8	3.267	2.0	4.733	1.0	6.200	.8
.400	.0	1.867	80.9	3.333	1.8	4.800	1.0	6.267	.6
.467	.0	1.933	68.5	3.400	1.7	4.867	1.0	6.333	.3

25x10

32x10

0000 0000 0820

.533	.0	2.000	60.5	3.467	1.6	4.933	1.1	6.400	.2
.600	.0	2.067	51.9	3.533	1.5	5.000	1.1	6.467	.1
.667	.0	2.133	40.9	3.600	1.4	5.067	1.1	6.533	.1
.733	.0	2.200	30.8	3.667	1.3	5.133	1.1	6.600	.1
.800	.0	2.267	22.5	3.733	1.3	5.200	1.1	6.667	.0
.867	.0	2.333	16.4	3.800	1.2	5.267	1.1	6.733	.0
.933	.0	2.400	13.2	3.867	1.2	5.333	1.1	6.800	.0
1.000	.0	2.467	10.9	3.933	1.1	5.400	1.1	6.867	.0
1.067	.0	2.533	9.0	4.000	1.1	5.467	1.2	6.933	.0
1.133	.0	2.600	7.5	4.067	1.1	5.533	1.2	7.000	.0
1.200	1.0	2.667	6.4	4.133	1.1	5.600	1.2	7.067	.0
1.267	10.8	2.733	5.4	4.200	1.1	5.667	1.2	7.133	.0
1.333	32.2	2.800	4.6	4.267	1.0	5.733	1.2		
1.400	77.4	2.867	4.0	4.333	1.0	5.800	1.3		

RUNOFF VOLUME = 1.42440 INCHES = 9.0470 ACRE-FEET  
 PEAK DISCHARGE RATE = 235.70 CFS AT 1.533 HOURS BASIN AREA = .1191 SQ. MI.

\*\*\*\*\*  
 \*S  
 \*S FUTURE/FULL DEVELOPMENT FUTURE/FULL DEVELOPMENT  
 \*S ROUTE 86TH TO 82ND IN SUNSET GARDENS: CONC PIPE; ST=.01 APX  
 \*C IF EST DIAM SHALL -> TRAVEL FASTER -> DNSTR PEAK HIGHER -> CONSERVATIVE  
 \*C VALLEY SEGMENT & REACH NUMBERS ARE USER ID'S NOT USED BY PROG; DUMMIES HERE  
 COMPUTE RATING CURVE CID= -1 VS NO= 11 NO SEGS FOR HANNING n= -1  
 SLOPE= .01 DIAM= 5.0 FT n= .013  
 COMPUTE TRAVEL TIME ID= 5 REACH= 11 NO VS= 1 L= 1100 FT S= .01

# TRAVEL TIME TABLE REACH= 11.0

WATER DEPTH FEET	AVERAGE AREA SQ. FT.	FLOW RATE CFS	TRAVEL TIME HRS
.261	.390	1.37	.0873
.521	1.086	5.93	.0559
.782	1.961	13.79	.0435
1.042	2.966	24.80	.0365
1.303	4.069	38.72	.0321
1.563	5.246	55.24	.0290
1.824	6.479	74.01	.0267
2.084	7.749	94.62	.0250
2.345	9.043	116.65	.0237
2.606	10.345	139.60	.0226
2.866	11.641	162.98	.0218
3.127	12.938	186.22	.0212
3.387	14.159	208.72	.0207
3.648	15.348	229.78	.0204
3.908	16.467	248.64	.0202
4.169	17.492	264.32	.0202
4.429	18.395	275.55	.0204
4.690	19.130	280.16	.0209
5.000	19.635	280.16	.0214

ROUTE ID= 5 HYD= 308 IN ID= 6 DT= 0.0  
 PRINT HYD ID= 5 CODE= 1

HYDROGRAPH FROM AREA 308.00

RUNOFF VOLUME = 1.42440 INCHES = 9.0470 ACRE-FEET  
 PEAK DISCHARGE RATE = 234.12 CFS AT 1.567 HOURS BASIN AREA = .1191 SQ. MI.

25x1

32x1

0000 0000 0821

```

*****
* BASIN T
* COMPUTE NW HYD      ID= 1  HYD= T      DA= .00467 SQ MI
  PER A= 0      B= 15      C= 0      D= 85
  TP= -0.13333 HRS  RAIN= -1

  K = .072665HR  TP = .133330HR  K/TP RATIO = .545000  SHAPE CONSTANT, N = 7.106420
  UNIT PEAK = 15.668 CFS  UNIT VOLUME = .9987  B = 526.28  P60 = 1.9000
  AREA = .003970 SQ MI  IA = .10000 INCHES  INF = .04000 INCHES PER HOUR
  RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

```

```

  K = .130790HR  TP = .133330HR  K/TP RATIO = .980950  SHAPE CONSTANT, N = 3.599935
  UNIT PEAK = 1.7209 CFS  UNIT VOLUME = .9926  B = 327.55  P60 = 1.9000
  AREA = .000701 SQ MI  IA = .50000 INCHES  INF = 1.25000 INCHES PER HOUR
  RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

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PRINT HYD      ID= 1  CODE= 1

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## HYDROGRAPH FROM AREA T

```

RUNOFF VOLUME = 1.79111 INCHES = .4461 ACRE-FEET
PEAK DISCHARGE RATE = 12.22 CFS AT 1.500 HOURS  BASIN AREA = .0047 SQ. MI.

```

```

*****
* ADD HYD      ID OUT= 3  HYD= 310  IDIN I= 1  IDIN II= 5
* PRINT HYD      ID= 3  CODE= 1

```

## HYDROGRAPH FROM AREA 310.00

```

RUNOFF VOLUME = 1.43823 INCHES = 9.4931 ACRE-FEET
PEAK DISCHARGE RATE = 244.23 CFS AT 1.567 HOURS  BASIN AREA = .1238 SQ. MI.

```

```

*****
* BASIN U
* COMPUTE NW HYD      ID= 1  HYD= U      DA= .01032 SQ MI
  PER A= 0      B= 30      C= 0      D= 70
  TP= -0.13333 HRS  RAIN= -1

  K = .072665HR  TP = .133330HR  K/TP RATIO = .545000  SHAPE CONSTANT, N = 7.106420
  UNIT PEAK = 28.514 CFS  UNIT VOLUME = .9990  B = 526.28  P60 = 1.9000
  AREA = .007224 SQ MI  IA = .10000 INCHES  INF = .04000 INCHES PER HOUR
  RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

```

```

  K = .130790HR  TP = .133330HR  K/TP RATIO = .980950  SHAPE CONSTANT, N = 3.599935
  UNIT PEAK = 7.6059 CFS  UNIT VOLUME = .9985  B = 327.55  P60 = 1.9000
  AREA = .003096 SQ MI  IA = .50000 INCHES  INF = 1.25000 INCHES PER HOUR
  RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

```

```

PRINT HYD      ID= 1  CODE= 1

```

## HYDROGRAPH FROM AREA U

```

RUNOFF VOLUME = 1.59625 INCHES = .8786 ACRE-FEET

```

25x10

32x10



0000 0000 0822

PEAK DISCHARGE RATE = 24.63 CFS AT 1.500 HOURS BASIN AREA = .0103 SQ. MI.

\*\*\*\*\*  
 \*C NOTE LARGE ID# - WILL RE-USE THIS HYD LAYER  
 ADD HYD ID OUT= 19 HYD= 312 IDIN I= 1 IDIN II= 3  
 PRINT HYD ID= 19 CODE= 1

HYDROGRAPH FROM AREA 312.00

RUNOFF VOLUME = 1.45039 INCHES = 10.3716 ACRE-FEET  
 PEAK DISCHARGE RATE = 264.83 CFS AT 1.567 HOURS BASIN AREA = .1341 SQ. MI.

\*\*\*\*\*  
 \* BASIN V: 4 IMPERV A LA POINTE WEST DESIGN & DENSITY  
 COMPUTE NM HYD ID= 11 HYD= V DA= .03200 SQ MI  
 PER A= 0 B= 50 C= 0 D= 50  
 TP= -0.13333 BRS RAIN= -1

K = .072665HR TP = .133330HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420  
 UNIT PEAK = 63.155 CFS UNIT VOLUME = .9992 B = 526.28 P60 = 1.9000  
 AREA = .016000 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .130790HR TP = .133330HR K/TP RATIO = .980950 SHAPE CONSTANT, N = 3.599935  
 UNIT PEAK = 39.107 CFS UNIT VOLUME = 1.000 B = 327.55 P60 = 1.9000  
 AREA = .016000 SQ MI IA = .50000 INCHES INF = 1.25000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 11 CODE= 1

HYDROGRAPH FROM AREA V

RUNOFF VOLUME = 1.33643 INCHES = 2.2808 ACRE-FEET  
 PEAK DISCHARGE RATE = 66.62 CFS AT 1.500 HOURS BASIN AREA = .0320 SQ. MI.

\*\*\*\*\*  
 ADD HYD ID OUT= 3 HYD= SG.AT.82ND IDIN I= 11 IDIN II= 19  
 PRINT HYD ID= 3 CODE= 1

HYDROGRAPH FROM AREA SG.AT.82ND

RUNOFF VOLUME = 1.42843 INCHES = 12.6524 ACRE-FEET  
 PEAK DISCHARGE RATE = 323.76 CFS AT 1.533 HOURS BASIN AREA = .1661 SQ. MI.

\*\*\*\*\*  
 \*C ROUTE TO UNSER IN CONC PIPE; SF=.01 APX AVG  
 \*C IF EST DIAM SHALL => TRAVEL FASTER => DNSTR PEAK HIGHER => CONSERVATIVE  
 \*C VALLEY SEGMENT & REACH NUMBERS ARE USER ID'S ONLY; DUMKIES HERE  
 \*C AVAIL SLOPE BTM UNSER/MOLE & SG/82 APX .01 AVG.  
 COMPUTE RATING CURVE CID= -1 VS NO= 11 NO SEGS FOR MARKING n= -1

25X

32X

0000 0000 0823

SLOPE= .01 DIAM= 5.5 FT n= .013  
 COMPUTE TRAVEL TIME ID= 5 REACH= 11 NO VS= 1 L= 1100 FT S= .01

TRAVEL TIME TABLE  
 REACH= 11.0

WATER DEPTH FEET	AVERAGE AREA SQ. FT.	FLOW RATE CFS	TRAVEL TIME HRS
.287	.472	1.76	.0819
.573	1.314	7.65	.0525
.860	2.373	17.78	.0408
1.146	3.589	31.97	.0343
1.433	4.923	49.92	.0301
1.720	6.348	71.23	.0272
2.006	7.839	95.43	.0251
2.293	9.377	122.00	.0235
2.579	10.942	150.40	.0222
2.866	12.518	180.00	.0212
3.153	14.086	210.14	.0205
3.439	15.630	240.11	.0199
3.726	17.132	269.11	.0195
4.013	18.571	296.28	.0192
4.299	19.925	320.59	.0190
4.586	21.166	340.81	.0190
4.872	22.258	355.29	.0191
5.159	23.147	361.23	.0196
5.500	23.758	361.23	.0201

ROUTE ID= 5 HYD= 314 IN ID= 3 DT= 0.0  
 PRINT HYD ID= 5 CODE= 1

HYDROGRAPH FROM AREA 314.00

RUNOFF VOLUME = 1.42844 INCHES = 12.6524 ACRE-Feet  
 PEAK DISCHARGE RATE = 322.21 CFS AT 1.567 HOURS BASIN AREA = .1661 SQ. MI.

\*\*\*\*\*

\*C BASIN W: \$ IMPERV A LA POINTE WEST DESIGN & DENSITY: SAME OWNER & ENGR  
 \*C BASIN W IS ONLY BASIN W Tp (47c) > REGULATORY MINIMUM

COMPUTE NM HYD ID= 12 HYD= W DA= .03422 SQ MI  
 PER A= 0 B= 50 C= 0 D= 50  
 TP= -0.16325 HRS BAIN= -1

K = .088971HR TP = .163250HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420  
 UNIT PEAK = 55.158 CFS UNIT VOLUME = .9997 B = 526.28 P60 = 1.9000  
 AREA = .017110 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .160140HR TP = .163250HR K/TP RATIO = .980950 SHAPE CONSTANT, N = 3.599930  
 UNIT PEAK = 34.330 CFS UNIT VOLUME = .9998 B = 327.55 P60 = 1.9000  
 AREA = .017110 SQ MI IA = .50000 INCHES INF = 1.25000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 12 CODE= 1

HYDROGRAPH FROM AREA W

RUNOFF VOLUME = 1.33643 INCHES = 2.4391 ACRE-Feet  
 PEAK DISCHARGE RATE = 64.02 CFS AT 1.533 HOURS BASIN AREA = .0342 SQ. MI.

25X

32X

0000 0000 0824

\*\*\*\*\*  
 ADD HYD ID OUT= 3 HYD= 316 IDIN I= 12 IDIN II= 5  
 PRINT HYD ID= 3 CODE= 1

HYDROGRAPH FROM AREA 316.00

RUNOFF VOLUME = 1.41271 INCHES = 15.0915 ACRE-FEET  
 PEAK DISCHARGE RATE = 384.09 CFS AT 1.567 HOURS BASIN AREA = .2003 SQ. MI.

\*\*\*\*\*  
 \* BASIN X: R.O.W. FOR SUNSET GARDENS AND (LIMITED ACCESS) UNSER  
 COMPUTE NM HYD ID= 13 HYD= X DA= .00674 SQ MI  
 PER A= 0 B= 20 C= 0 D= 80  
 TP= -0.13333 HRS RAIN= -1

K = .072665HR TP = .133330HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420  
 UNIT PEAK = 21.283 CFS UNIT VOLUME = .9988 B = 526.28 P60 = 1.9000  
 AREA = .005392 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .130790HR TP = .133330HR K/TP RATIO = .980950 SHAPE CONSTANT, N = 3.599935  
 UNIT PEAK = 3.3116 CFS UNIT VOLUME = .9961 B = 327.55 P60 = 1.9000  
 AREA = .001348 SQ MI IA = .50000 INCHES INF = 1.25000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 13 CODE= 1

HYDROGRAPH FROM AREA X

RUNOFF VOLUME = 1.72616 INCHES = .6205 ACRE-FEET  
 PEAK DISCHARGE RATE = 17.11 CFS AT 1.500 HOURS BASIN AREA = .0067 SQ. MI.

\*\*\*\*\*  
 ADD HYD ID OUT= 4 HYD= SG.AT.UNSER IDIN I= 13 IDIN II= 3  
 PRINT HYD ID= 4 CODE= 1

HYDROGRAPH FROM AREA SG.AT.UNSER

RUNOFF VOLUME = 1.42292 INCHES = 15.7120 ACRE-FEET  
 PEAK DISCHARGE RATE = 398.29 CFS AT 1.567 HOURS BASIN AREA = .2070 SQ. MI.

\*\*\*\*\*  
 \*C ROUTE TO UNSER 340 FT X OF SG (APX HALF DIST TO ANOLE CHAN); SF=.01 APX  
 \*C EST DIAM SMALL -> TRAVEL FASTER -> DNSTR PEAK HIGHER -> CONSERVATIVE  
 \*C VALLEY SEGMENT & REACH NUMBERS ARE USER ID'S ONLY; DOWNHILLS HERE  
 COMPUTE RATING CURVE CID= -1 VS NO= 11 NO SEGS FOR HASHING n= -1  
 SLOPE= .01 DIAM= 6.0 FT n= .013  
 COMPUTE TRAVEL TIME ID= 5 REACH= 11 NO VS= 1 L= 340 FT S= .01

TRAVEL TIME TABLE  
 REACH= 11.0

25X

32X

WATER DEPTH FEET	AVERAGE AREA SQ. FT.	FLOW RATE CFS	TRAVEL TIME HRS
.313	.562	2.22	.0239
.625	1.564	9.64	.0153
.938	2.824	22.42	.0119
1.251	4.271	40.32	.0100
1.563	5.859	62.96	.0088
1.876	7.554	89.83	.0079
2.189	9.329	120.35	.0073
2.501	11.159	153.87	.0068
2.814	13.022	189.68	.0065
3.127	14.897	227.01	.0062
3.439	16.764	265.02	.0060
3.752	18.601	302.81	.0058
4.065	20.388	339.39	.0057
4.377	22.101	373.65	.0056
4.690	23.712	404.31	.0055
5.003	25.189	429.82	.0055
5.315	26.489	448.07	.0056
5.628	27.547	455.57	.0057
6.000	28.274	455.57	.0059

ROUTE ID= 5 HYD= 318 IN ID= 4 DT= 0.0  
 PRINT HYD ID= 5 CODE= 1

## HYDROGRAPH FROM AREA 318.00

RUNOFF VOLUME = 1.42292 INCHES = 15.7120 ACRE-Feet  
 PEAK DISCHARGE RATE = 399.01 CFS AT 1.567 HOURS BASIN AREA = .2070 SQ. MI.

\*\*\*\*\*  
 \* BASIN Y DEVELOPED: EST ENTIRE SITE; ZONING = O-1; USE 1/4 INPVT AS FOR C-2  
 \* WHEN BUILT, W APX 200' POSS DRAIN TO BRIDGE PER GREINER FOR BRIDGE BLVD SD  
 COMPUTE KM HYD ID= 14 HYD= YD DA= .02964 SQ MI  
 PER A= 0 B= 10 C= 5 D= 85  
 TP= -0.13333 HRS RAIN= -1

K = .072665HR TP = .133330HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420  
 UNIT PEAK = 99.445 CFS UNIT VOLUME = .9993 B = 526.28 P60 = 1.9000  
 AREA = .025194 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .122603HR TP = .133330HR K/TP RATIO = .919546 SHAPE CONSTANT, N = 3.849372  
 UNIT PEAK = 11.504 CFS UNIT VOLUME = .9992 B = 345.00 P60 = 1.9000  
 AREA = .004446 SQ MI IA = .45000 INCHES INF = 1.11000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 14 CODE= 1

## HYDROGRAPH FROM AREA YD

RUNOFF VOLUME = 1.80576 INCHES = 2.8545 ACRE-Feet  
 PEAK DISCHARGE RATE = 78.24 CFS AT 1.500 HOURS BASIN AREA = .0296 SQ. MI.

\*\*\*\*\*  
 \*S TOTAL UNSER APX 300' S OF ANOLE CHANNEL AT BRIDGE: FUTURE/FULLY DEVELOPED  
 ADD HYD ID OUT= 7 HYD= FUT.YO.ANOLE IDIN I= 14 IDIN II= 5

0000 0000 0826

PRINT HYD ID: 7 CODE: 1

## HYDROGRAPH FROM AREA FUT.TO.AMOLE

RUNOFF VOLUME = 1.47086 INCHES = 10.5665 ACRE-FEET  
 PEAK DISCHARGE RATE = 465.36 CFS AT 1.533 HOURS BASIN AREA = .2367 SQ. MI.

```

*****
#S
#S
#S INTERIM INTERIM INTERIM
#S INTERIM: RE-USE HYD 312 W/ ID=19, ROUTE IN DIRT CHAN ACROSS BASIN Y EXIST
#C APPROX AS 12' BOTTOM, 38:1W SIDESLOPES, n=.030, L APX 1250, S=.005
COMPUTE RATING CURVE CID= -1 VS NO= 1 NO SEGS FOR MANNING n= 1
ELMIN= 0 ELMAX= 8 FT CHSLP= .005 FPSLP= .005 FT/FT
n .030 DIST 60
DIST ELEV DIST ELEV DIST ELEV DIST ELEV
0 8 24 0 36 0 60 8
ROUTE NCURGE ID= 5 HYD= 502 INFLOW HYD ID= 19 DT= 0.0 HR
LENGTH= 1250 NSUBRCH= 0 SLOPE= .005
MATCODE= 0 RECODE= 0 CCODE= 0
Inflow ID end=224 Max Number=600
dt = .0333 hr q0 = 132.42 cfs ch0 = 6.19 fps
nlen = 3 dlen = 416.67

```

Depth	Area	Q	Qbar	ck	b	C	D	c1	c2	vel	fr	tt
ft	sf	cfs	cfs	fps	ft					fps		hr
.00	.0	.0	5.1	1.84	7.3	.53	.18	.78	-.17	1.84	.52	.189
.42	5.6	10.3	22.1	3.56	15.8	1.03	.19	.83	.10	2.48	.58	.140
.84	12.2	34.0	51.0	4.64	18.3	1.34	.29	.78	.24	3.22	.61	.108
1.26	19.9	69.8	93.8	5.48	20.8	1.58	.39	.73	.33	3.85	.63	.090
1.68	28.7	117.8	148.3	6.19	23.4	1.78	.49	.70	.39	4.41	.65	.079
2.11	38.6	178.8	216.0	6.83	25.9	1.97	.59	.67	.44	4.91	.66	.071
2.53	49.5	253.3	297.7	7.42	28.4	2.14	.68	.64	.48	5.37	.68	.065
2.95	61.4	342.1	394.0	7.97	30.9	2.29	.77	.62	.51	5.80	.69	.060
3.37	74.5	445.9	505.7	8.49	33.5	2.44	.85	.60	.53	6.20	.70	.056
3.79	88.6	565.5	633.6	8.98	36.0	2.59	.94	.58	.56	6.59	.71	.053
4.21	103.7	701.7	778.4	9.46	38.5	2.72	1.03	.57	.58	6.96	.72	.050
4.63	119.9	855.1	940.9	9.92	41.1	2.86	1.11	.55	.60	7.32	.73	.047
5.05	137.2	1026.6	1121.7	10.36	43.6	2.99	1.19	.54	.61	7.66	.74	.045
5.47	155.6	1216.8	1321.6	10.80	46.1	3.11	1.27	.53	.63	8.00	.74	.043
5.89	175.0	1426.4	1541.3	11.22	48.6	3.23	1.36	.51	.64	8.32	.75	.042
6.32	195.5	1656.2	1781.5	11.63	51.2	3.35	1.44	.50	.65	8.64	.76	.040
6.74	217.0	1906.8	2042.9	12.04	53.7	3.47	1.52	.49	.67	8.95	.76	.039
7.16	239.6	2178.9	2326.1	12.44	56.2	3.58	1.60	.48	.68	9.25	.77	.038
7.58	263.3	2473.3	2631.9	12.82	58.7	3.69	1.68	.47	.69	9.55	.78	.036
8.00	288.0	2790.4	.0	.00	.0	.00	.00	.00	.00	.00	.00	.000

nlen= 3 Outflow ID end=228  
 Route using Ponce procedure: C1 > 0  
 PRINT HYD ID= 5 CODE= 1

## OUTFLOW HYDROGRAPH RESERVOIR 502.00

RUNOFF VOLUME = 1.45076 INCHES = 10.3742 ACRE-FEET  
 PEAK DISCHARGE RATE = 260.04 CFS AT 1.600 HOURS BASIN AREA = .1341 SQ. MI.

25X

32X



0000 0000 0827

```
*****
* BASIN YE
COMPUTE NM HYD ID= 15 HYD= YE DA=0.02964 SQ MI
PER A= 97 B= 0 C= 3 D= 0
TP= -0.13333 HRS RAIN= -1
```

```
K = .161262HR TP = .133330HR K/TP RATIO = 1.209496 SHAPE CONSTANT, N = 2.939924
UNIT PEAK = 61.553 CFS UNIT VOLUME = .9995 B = 276.89 P60 = 1.9000
AREA = .029640 SQ MI 1A = .64100 INCHES INF = 1.64480 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333
```

```
PRINT HYD ID= 15 CODE= 1
```

## HYDROGRAPH FROM AREA YE

```
RUNOFF VOLUME = .46670 INCHES = .7378 ACRE-FEET
PEAK DISCHARGE RATE = 26.19 CFS AT 1.533 HOURS BASIN AREA = .0296 SQ. MI.
```

```
*
*****
*S
ADD HYD ID OUT= 8 HYD= INT.2.ANOLE IDIN I= 15 IDIN II= 5
PRINT HYD ID= 8 CODE= 1
```

## HYDROGRAPH FROM AREA INT.2.ANOLE

```
RUNOFF VOLUME = 1.27260 INCHES = 11.1120 ACRE-FEET
PEAK DISCHARGE RATE = 281.49 CFS AT 1.600 HOURS BASIN AREA = .1637 SQ. MI.
```

```
*
*****
*S
*S INTERIM W/ V (POINTE WEST) INTERIM W/ V (POINTE WEST)
*S RE-USE HYD 312 W/ ID=19, HYD V W/ ID=11, & HYD YE W/ ID=15
*S ROUTE IN DIRT CHAN ACROSS BASIN Y EXIST
ADD HYD ID OUT= 3 HYD= 602 IDIN I= 19 IDIN II= 11
PRINT HYD ID= 3 CODE= 1
```

## HYDROGRAPH FROM AREA 602.00

```
RUNOFF VOLUME = 1.42843 INCHES = 12.6524 ACRE-FEET
PEAK DISCHARGE RATE = 323.76 CFS AT 1.533 HOURS BASIN AREA = .1661 SQ. MI.
```

```
*
*****
*C APPROX AS 12' BOTTOM, 3H:1V SIDESLOPES, n=.030, L APX 1250, S=.005
COMPUTE RATING CURVE CID= -1 VS NO= 1 NO SEGS FOR MARKING n= 1
ELMIN= 0 ELMAX= 8 FT CHSLP= .005 FFSLP= .005 FT/FT
n .030 DIST 60
DIST ELEV DIST ELEV DIST ELEV DIST ELEV
0 8 24 0 36 0 60 8
ROUTE NCUNGE ID= 5 HYD= 604 INFLOW HYD ID= 3 DT= 0.0 HR
LENGTH= 1250 NSUBRC= 0 SLOPE= .005
MAYCODE= 0 REGCODE= 0 CCODE= 0
Inflow ID end=222 Max Number=600
```

25x10

32x10

0000 0000 0828

dt = .0333 hr q0 = 161.88 cfs ch0 = 6.19 fps  
 nlen = 3 dlen = 416.67

Depth ft	Area sf	Q cfs	Qbar cfs	ch fps	b ft	C	D	c1	c2	vel fps	fr	tt hr
.00	.0	.0	5.1	1.84	7.3	.53	.18	.78	-.17	1.84	.52	.189
.42	5.6	10.3	22.1	3.56	15.8	1.03	.19	.83	.10	2.48	.58	.140
.84	12.2	34.0	51.9	4.64	18.3	1.34	.29	.78	.24	3.22	.61	.108
1.26	19.9	69.8	93.8	5.48	20.8	1.58	.39	.73	.33	3.85	.63	.090
1.68	28.7	117.8	148.3	6.19	23.4	1.78	.49	.70	.39	4.41	.65	.079
2.11	38.6	178.8	216.0	6.83	25.9	1.97	.59	.67	.44	4.91	.66	.071
2.53	49.5	253.3	297.7	7.42	28.4	2.14	.68	.64	.48	5.37	.68	.065
2.95	61.4	342.1	394.0	7.97	30.9	2.29	.77	.62	.51	5.80	.69	.060
3.37	74.5	445.9	505.7	8.49	33.5	2.44	.85	.60	.53	6.20	.70	.056
3.79	88.6	565.5	633.6	8.98	36.0	2.59	.94	.58	.56	6.59	.71	.053
4.21	103.7	701.7	778.4	9.46	38.5	2.72	1.03	.57	.58	6.96	.72	.050
4.63	119.9	855.1	940.9	9.92	41.1	2.86	1.11	.55	.60	7.32	.73	.047
5.05	137.2	1026.6	1121.7	10.36	43.6	2.99	1.19	.54	.61	7.66	.74	.045
5.47	155.6	1216.8	1321.6	10.80	46.1	3.11	1.27	.53	.63	8.00	.74	.043
5.89	175.0	1426.4	1541.3	11.22	48.6	3.23	1.36	.51	.64	8.32	.75	.042
6.32	195.5	1656.2	1781.5	11.63	51.2	3.35	1.44	.50	.65	8.64	.76	.040
6.74	217.0	1906.8	2042.9	12.04	53.7	3.47	1.52	.49	.67	8.95	.76	.039
7.16	239.6	2178.9	2326.1	12.44	56.2	3.58	1.60	.48	.68	9.25	.77	.038
7.58	263.3	2473.3	2631.9	12.82	58.7	3.69	1.68	.47	.69	9.55	.78	.036
8.00	288.0	2790.4	.0	.00	.0	.00	.00	.00	.00	.00	.00	.000

nlen= 3 Outflow ID end=227

Route using Ponce procedure: C1 > 0

PRINT HYD ID= 5 CODE= 1

HYDROGRAPH FROM AREA 604.00

RUNOFF VOLUME = 1.42737 INCHES = 12.6430 ACRE-Feet  
 PEAK DISCHARGE RATE = 320.37 CFS AT 1.600 HOURS BASIN AREA = .1661 SQ. MI.

\*\*\*\*\*  
 \*C RE-USE HYD YE W/ ID=15, ADD TO ROUTED FLOW  
 ADD HYD ID OUT= 98 HYD= INT.V.2ANOLE IDIN I= 15 IDIN II= 3  
 PRINT HYD ID= 9 CODE= 1

OUTFLOW HYDROGRAPH REACH .00

RUNOFF VOLUME = .00000 INCHES = .0000 ACRE-Feet  
 PEAK DISCHARGE RATE = .00 CFS AT .000 HOURS BASIN AREA = .0000 SQ. MI.

\*\*\*\*\*  
 \*S  
 \*S  
 \*S ALLEY ALLEY ALLEY  
 \*S BASINS B, G, & SIVE-1 TO ALLEY. BASIN A NOT CONTRIBUTE INTERIM/FUTURE  
 \*S FUTURE/INTERIM ALLEY FLOWS FOR INFO ONLY; HOLD TO EXISTING CONDITIONS  
 \*\*\*\*\*

\* BASIN B  
 COMPUTE NM HYD ID= 1 HYD= B DA=0.01520 SQ MI  
 PER A= 0 B= 16 C= 8 D= 76  
 TP= -0.13333 HRS RAIN= -1

K = .072665HR TP = .133330HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420

25x10

32x10

UNIT PEAK = 45.598 CFS UNIT VOLUME = .9991 B = 526.28 P60 = 1.9000  
 AREA = .011552 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .1226038R TP = .1333308R K/TP RATIO = .919546 SHAPE CONSTANT, N = 3.849372  
 UNIT PEAK = 9.4394 CFS UNIT VOLUME = .9990 B = 345.00 P60 = 1.9000  
 AREA = .003648 SQ MI IA = .45000 INCHES INF = 1.11000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 1 CODE= 1

#### HYDROGRAPH FROM AREA B

RUNOFF VOLUME = 1.69764 INCHES = 1.3762 ACRE-FEET  
 PEAK DISCHARGE RATE = 38.30 CFS AT 1.500 HOURS BASIN AREA = .0152 SQ. MI.

\*\*\*\*\*  
 \* BASIN G  
 COMPUTE NM HYD ID= 2 HYD= G DA=0.01501 SQ MI  
 PER A= 0 B= 20 C= 10 D= 70  
 TP= -0.13333 HRS RAIN= -1

K = .0726658R TP = .1333308R K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420  
 UNIT PEAK = 41.473 CFS UNIT VOLUME = .9991 B = 526.28 P60 = 1.9000  
 AREA = .010507 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .1226038R TP = .1333308R K/TP RATIO = .919546 SHAPE CONSTANT, N = 3.849372  
 UNIT PEAK = 11.652 CFS UNIT VOLUME = .9992 B = 345.00 P60 = 1.9000  
 AREA = .004503 SQ MI IA = .45000 INCHES INF = 1.11000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 2 CODE= 1

#### HYDROGRAPH FROM AREA G

RUNOFF VOLUME = 1.62555 INCHES = 1.3013 ACRE-FEET  
 PEAK DISCHARGE RATE = 36.62 CFS AT 1.500 HOURS BASIN AREA = .0150 SQ. MI.

\*\*\*\*\*  
 ADD HYD ID OUT= 3 HYD= TO.TOP.ALLEY IDIN I= 1 IDIN II= 2  
 PRINT HYD ID= 3 CODE= 1

#### HYDROGRAPH FROM AREA TO.TOP.ALLEY

RUNOFF VOLUME = 1.66180 INCHES = 2.6775 ACRE-FEET  
 PEAK DISCHARGE RATE = 74.92 CFS AT 1.500 HOURS BASIN AREA = .0302 SQ. MI.

\*\*\*\*\*  
 \* BASIN SITE.1  
 COMPUTE NM HYD ID= 1 HYD= SITE.1 DA=0.00151 SQ MI  
 PER A= 0 B= 35 C= 0 D= 55



0000 0000 0830

TP = -0.1333 HRS RAIN = -1

K = .07265HR TP = .133330HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420  
 UNIT PEAK = 3.8741 CFS UNIT VOLUME = .9965 B = 526.28 P60 = 1.9000  
 AREA = .000982 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

K = .130790HR TP = .133330HR K/TP RATIO = .980950 SHAPE CONSTANT, N = 3.599935  
 UNIT PEAK = 1.2984 CFS UNIT VOLUME = .9894 B = 327.55 P60 = 1.9000  
 AREA = .000529 SQ MI IA = .50000 INCHES INF = 1.25000 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333

PRINT HYD ID= 1 CODE= 1

HYDROGRAPH FROM AREA SITE 1

RUNOFF VOLUME = 1.53130 INCHES = .1233 ACRE-Feet  
 PEAK DISCHARGE RATE = 3.50 CFS AT 1.500 HOURS BASIN AREA = .0015 SQ. MI.

\*\*\*\*\*  
 ADD HYD ID OUT= 4 HYD= BOT.ALLEY IDIN I= 1 IDIN II= 3  
 PRINT HYD ID= 4 CODE= 1

HYDROGRAPH FROM AREA BOT.ALLEY

RUNOFF VOLUME = 1.65558 INCHES = 2.8008 ACRE-Feet  
 PEAK DISCHARGE RATE = 78.42 CFS AT 1.500 HOURS BASIN AREA = .0317 SQ. MI.

\*\*\*\*\*  
 FINISH

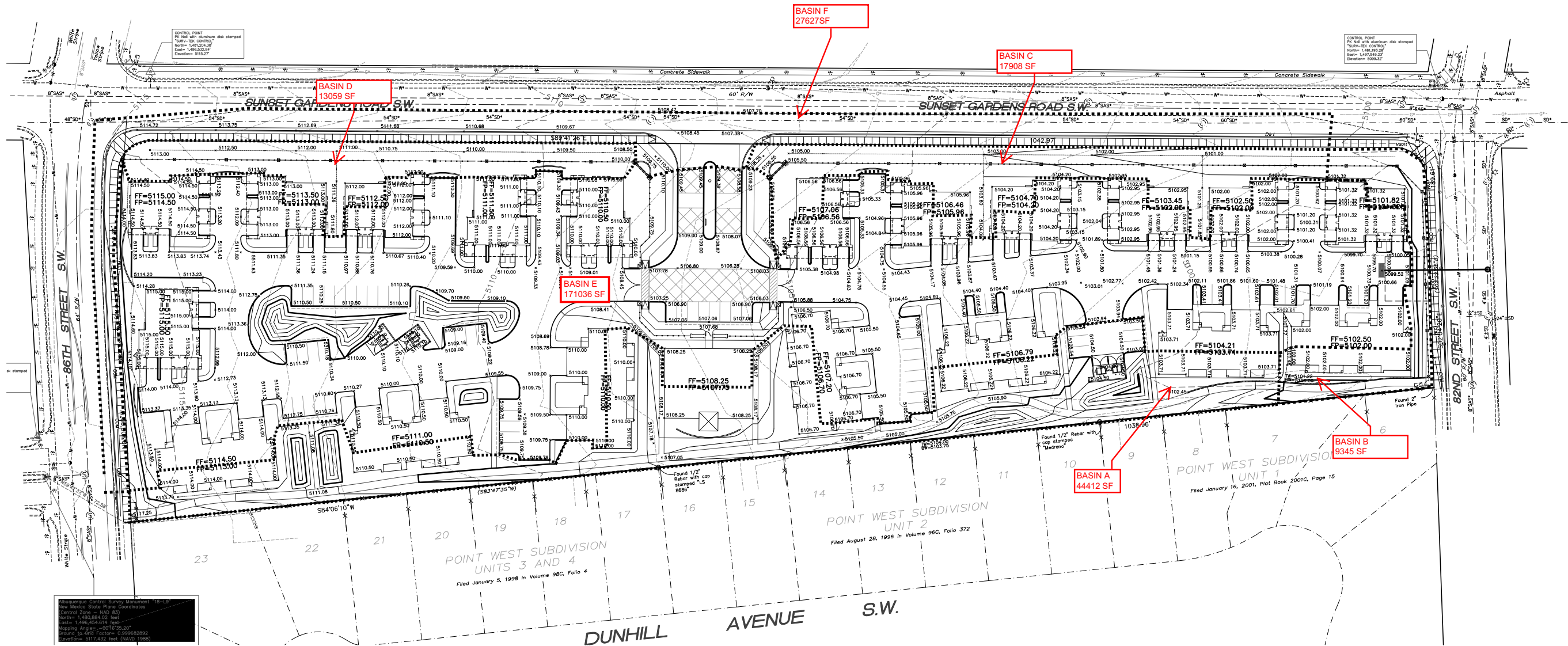
NORMAL PROGRAM FINISH END TIME (HR:MIN:SEC) = 12:37:11

25 X 1

32 X 1

**APPENDIX B**

**SITE HYDROLOGY**



## Weighted E Method

											100-Year, 6-hr.		
Basin	Area (sf)	Area (acres)	Treatment A		Treatment B		Treatment C		Treatment D		Weighted E (ac-ft)	Volume (ac-ft)	Flow cfs
			%	(acres)	%	(acres)	%	(acres)	%	(acres)			
ALLOWED													24.63
PROPOSED A	44412.00	1.020	0%	0	5%	0.051	6%	0.0612	89%	0.907	1.846	0.157	4.24
PROPOSED B	9345.00	0.215	0%	0	20%	0.043	44%	0.0944	36%	0.077	1.279	0.023	0.70
PROPOSED C	17908.00	0.411	0%	0	16%	0.066	60%	0.2467	24%	0.099	1.174	0.040	1.27
PROPOSED D	13059.00	0.300	0%	0	20%	0.060	47%	0.1409	33%	0.099	1.249	0.031	0.96
PROPOSED E	171036.00	3.926	0%	0	20%	0.785	47%	1.8454	33%	1.296	1.124	0.368	10.32
PROPOSED F	27627.00	0.634	0%	0	0%	0.000	8%	0.0507	92%	0.583	0.158	0.008	2.70

TOTAL

2.478

20.18

### Equations:

Weighted E =  $E_a \cdot A_a + E_b \cdot A_b + E_c \cdot A_c + E_d \cdot A_d$  / (Total Area)

Volume = Weighted D \* Total Area

Flow =  $Q_a \cdot A_a + Q_b \cdot A_b + Q_c \cdot A_c + Q_d \cdot A_d$

Where for 100-year, 6-hour storm- zone 1

Ea= 0.44	Qa= 1.29
Eb= 0.67	Qb= 2.03
Ec= 0.99	Qc= 2.87
Ed= 1.97	Qd= 4.37

ONSITE Conditions

FIRST FLUSH WATER QUALITY VOLUME

	REQUIRED	PROVIDED
	(CF)	(CF)
WATER QUALITY	3058	6840

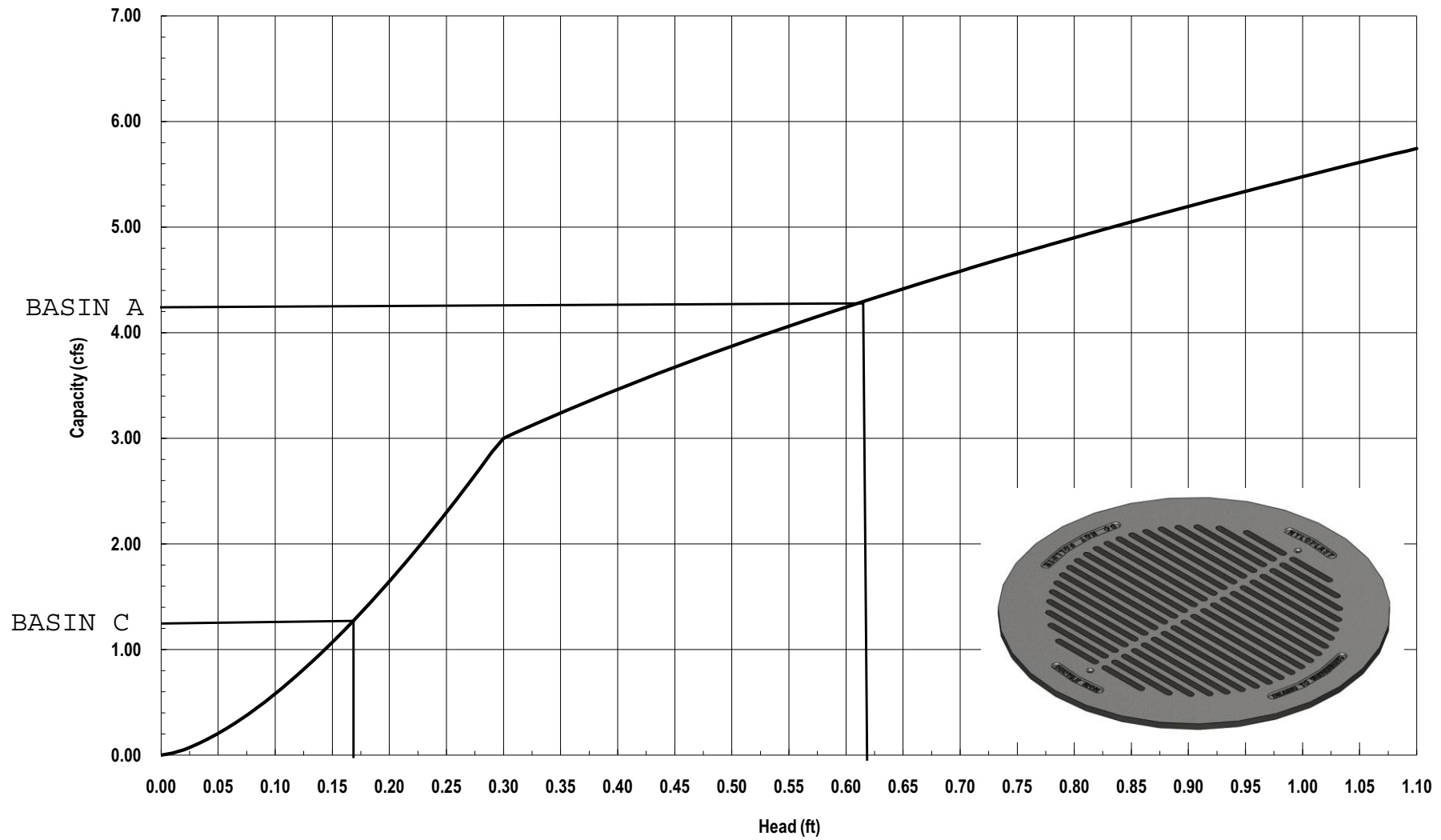
### Narrative

This site is within the boundary of the Amole del norte drainage basin. The site is identified as basin U within the Val Halla drainage report. this site drains to an existing storm drain within sunset gardens. This site is allowed to drain 24.63 cfs. We are draining 20.18 cfs to this storm drain there is no upland flow. This plan provided for onsite ponding of the water quality volume  
This plan is in conformance to the master drainage plan

**APPENDIX C**

**HYDRAULIC CALCULATIONS**

Nyloplast 24" Drop In Grate Inlet Capacity Chart



3130 Verona Avenue • Buford, GA 30518  
 (866) 888-8479 / (770) 932-2443 • Fax: (770) 932-2490  
 © Nyloplast Inlet Capacity Charts June 2012



## ***DROP INLET CALCULATIONS***

INLET	TYPE OF INLET	AREA (SF)	Q (CFS)	H (FT)	H ALLOW (FT)
INLET A	DOUBLE	7.68	20.64	0.3115	1

### ORIFICE EQUATION

$$Q = CA \sqrt{2gH}$$

$$C = 0.6$$

$$g = 32.2$$

\* FLOW DOUBLED DUE TO SUMP CONDITION

## Pipe Capacity

Pipe	D	Slope	Area	R	Q Provided	Q Required	Velocity
	(in)	(%)	(ft^2)		(cfs)	(cfs)	(ft/s)
EXISTISTING	24	3	3.14	0.5	34.05	14.56	4.63

### Manning's Equation:

$$Q = 1.49/n * A * R^{(2/3)} * S^{(1/2)}$$

A = Area

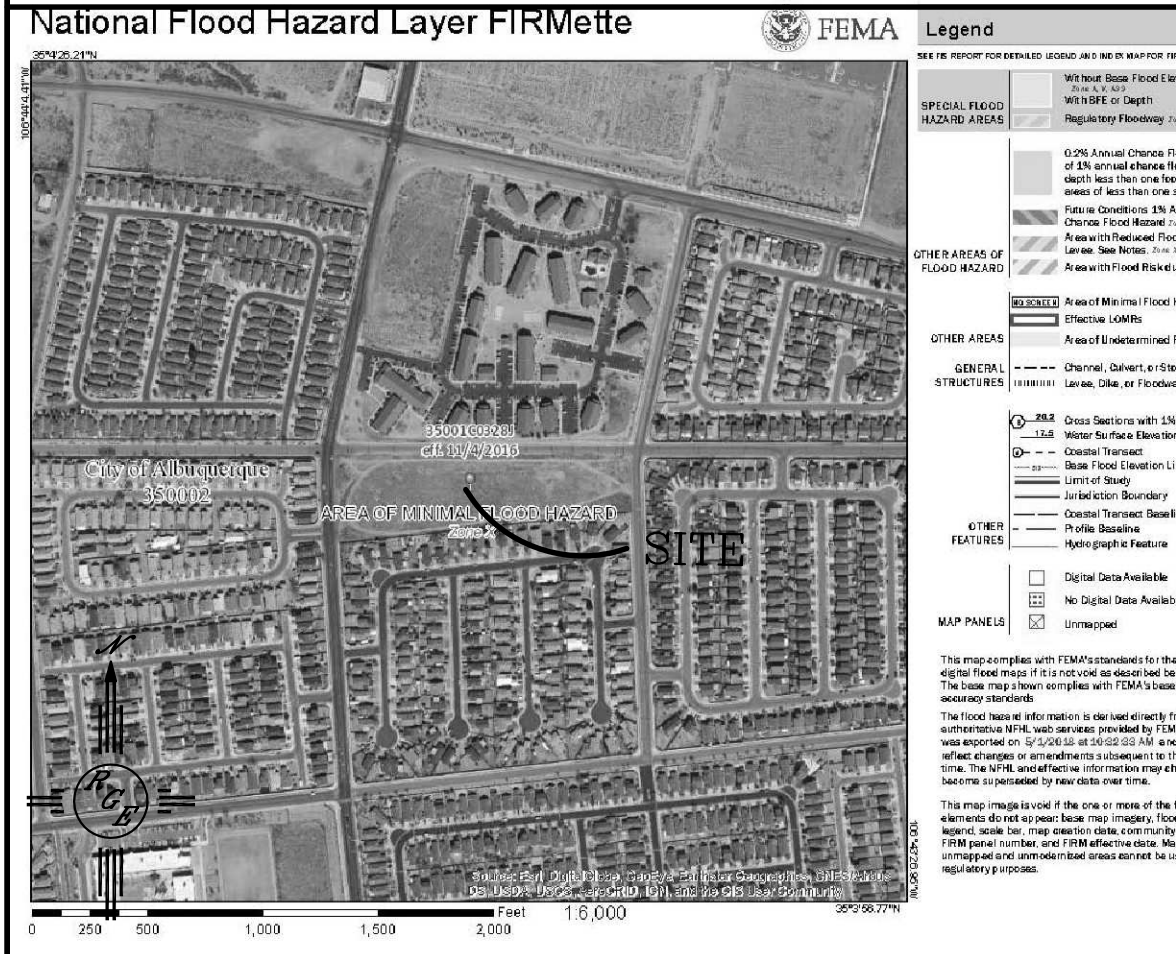
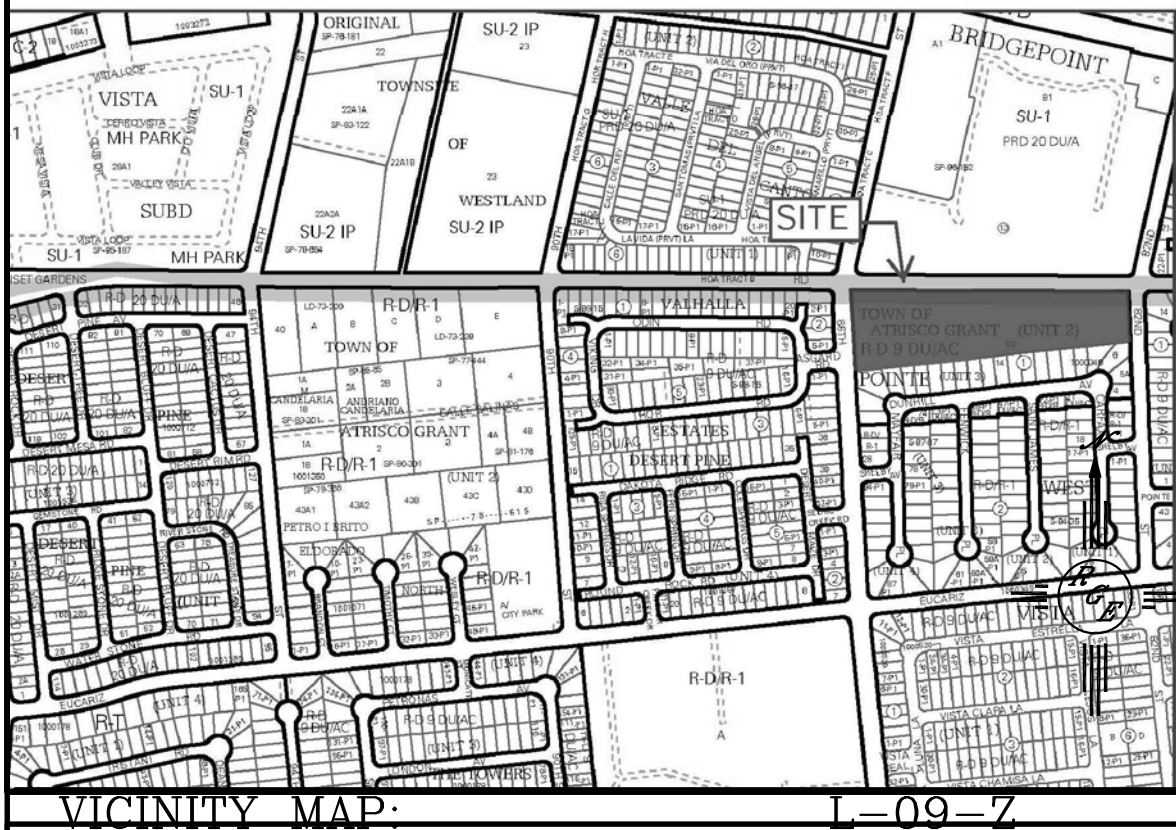
R = D/4

S = Slope

n = 0.015

EROSION CONTROL NOTES:

1. CONTRACTOR IS RESPONSIBLE FOR OBTAINING A TOPSOIL DISTURBANCE PERMIT PRIOR TO BEGINNING WORK.
2. CONTRACTOR IS RESPONSIBLE FOR MAINTAINING RUN-OFF ON SITE DURING CONSTRUCTION.
3. CONTRACTOR IS RESPONSIBLE FOR CLEANING ALL SEDIMENT THAT GETS INTO EXISTING RIGHT-OF-WAY.
4. REPAIR OF DAMAGED FACILITIES AND CLEANUP OF SEDIMENT ACCUMULATIONS ON ADJACENT PROPERTIES AND IN PUBLIC FACILITIES IS THE RESPONSIBILITY OF THE CONTRACTOR.
5. ALL EXPOSED EARTH SURFACES MUST BE PROTECTED FROM WIND AND WATER EROSION PRIOR TO FINAL ACCEPTANCE OF ANY PROJECT.

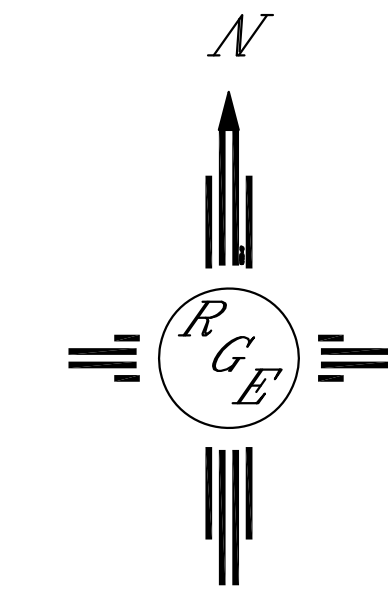


**FIRM MAP:**  
**LEGAL DESCRIPTION:**  
TRACT 52, UNIT 2, TOWN OF ATRISCO GRANT

NOTES:

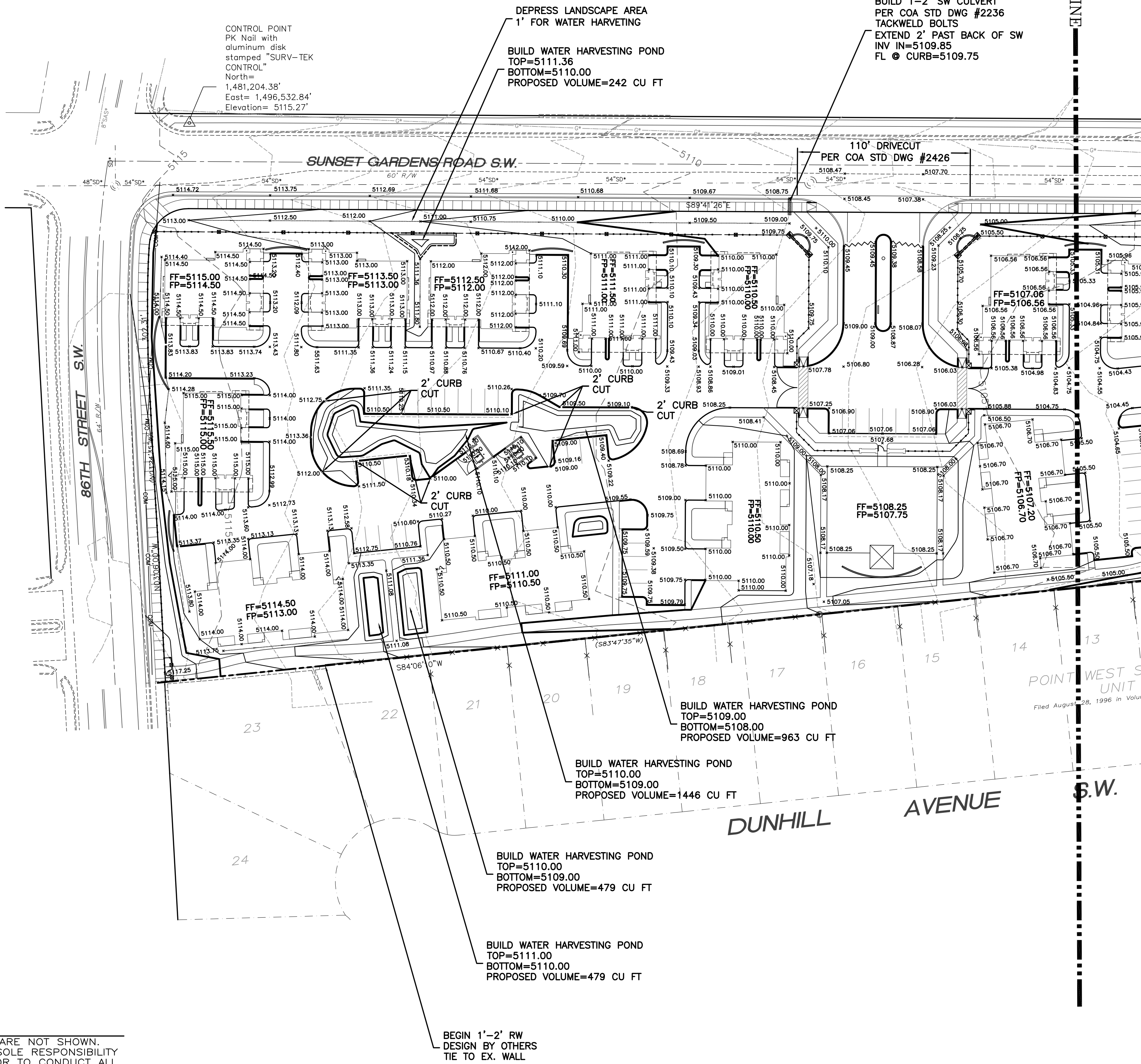
1. ALL SPOT ELEVATIONS REPRESENT FLOWLINE ELEVATION UNLESS OTHERWISE NOTED.
2. ALL CURB AND GUTTER TO 6" HEADER UNLESS OTHERWISE NOTED.
3. ALL RETAINING WALL DESIGN SHALL BE BY OTHERS.
4. ALL NEW PAVING SHALL BE 6" PCC OVER 8" SUBGRADE PREPARATION IN CONFORMANCE TO ACI 330R-08. UNLESS OTHERWISE NOTED.
5. ANY CURBS OR PAVEMENT NEGATIVELY IMPACTED BY CONSTRUCTION ACTIVITY SHALL BE REPLACED TO MATCH EXISTING CONDITIONS.
6. ALL SITE WORK SHALL CONFORM TO CITY OF ALBUQUERQUE STANDARDS FOR PUBLIC WORKS CONSTRUCTION EDITION 9

LEGEND	
---	EXISTING CONTOUR
- - - -	EXISTING INDEX CONTOUR
---	PROPOSED CONTOUR
---	PROPOSED INDEX CONTOUR
---	SLOPE TIE
x 4048.25	EXISTING SPOT ELEVATION
x 4048.25	PROPOSED SPOT ELEVATION
---	BOUNDARY
---	CENTERLINE
---	RIGHT-OF-WAY
---	PROPOSED CURB
---	EXISTING CURB AND GUTTER
---	PROPOSED SIDEWALK
---	EXISTING SIDEWALK
---	PROPOSED SCREEN WALL
---	FLOWLINE



GRAPHIC SCALE  
SCALE: 1"=40'

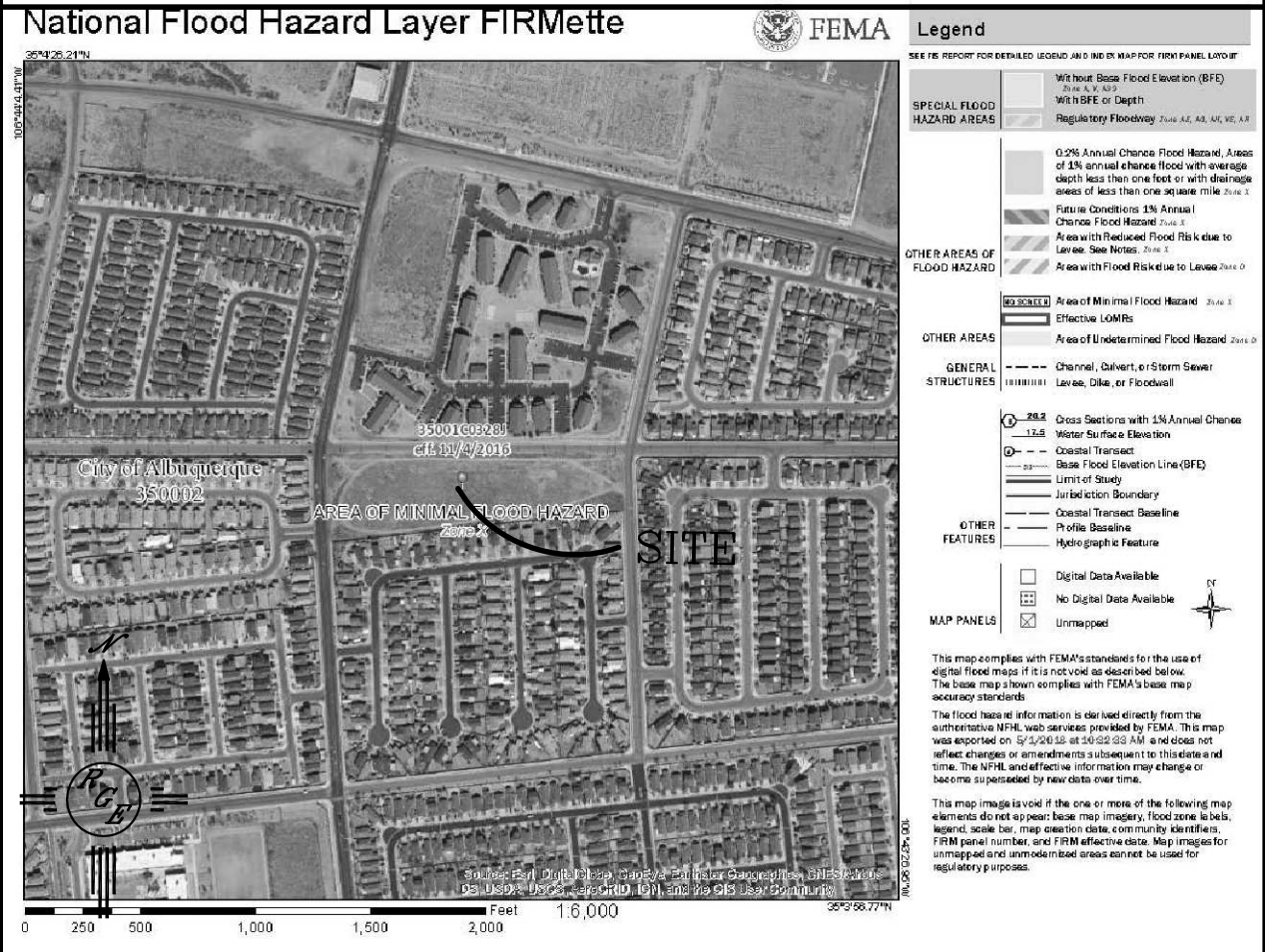
**CAUTION:**  
EXISTING UTILITIES ARE NOT SHOWN.  
IT SHALL BE THE SOLE RESPONSIBILITY  
OF THE CONTRACTOR TO CONDUCT ALL  
NECESSARY FIELD INVESTIGATIONS PRIOR  
TO ANY EXCAVATION TO DETERMINE THE  
ACTUAL LOCATION OF UTILITIES & OTHER  
IMPROVEMENTS.





EROSION CONTROL NOTES:

1. CONTRACTOR IS RESPONSIBLE FOR OBTAINING A TOPSOIL DISTURBANCE PERMIT PRIOR TO BEGINNING WORK.
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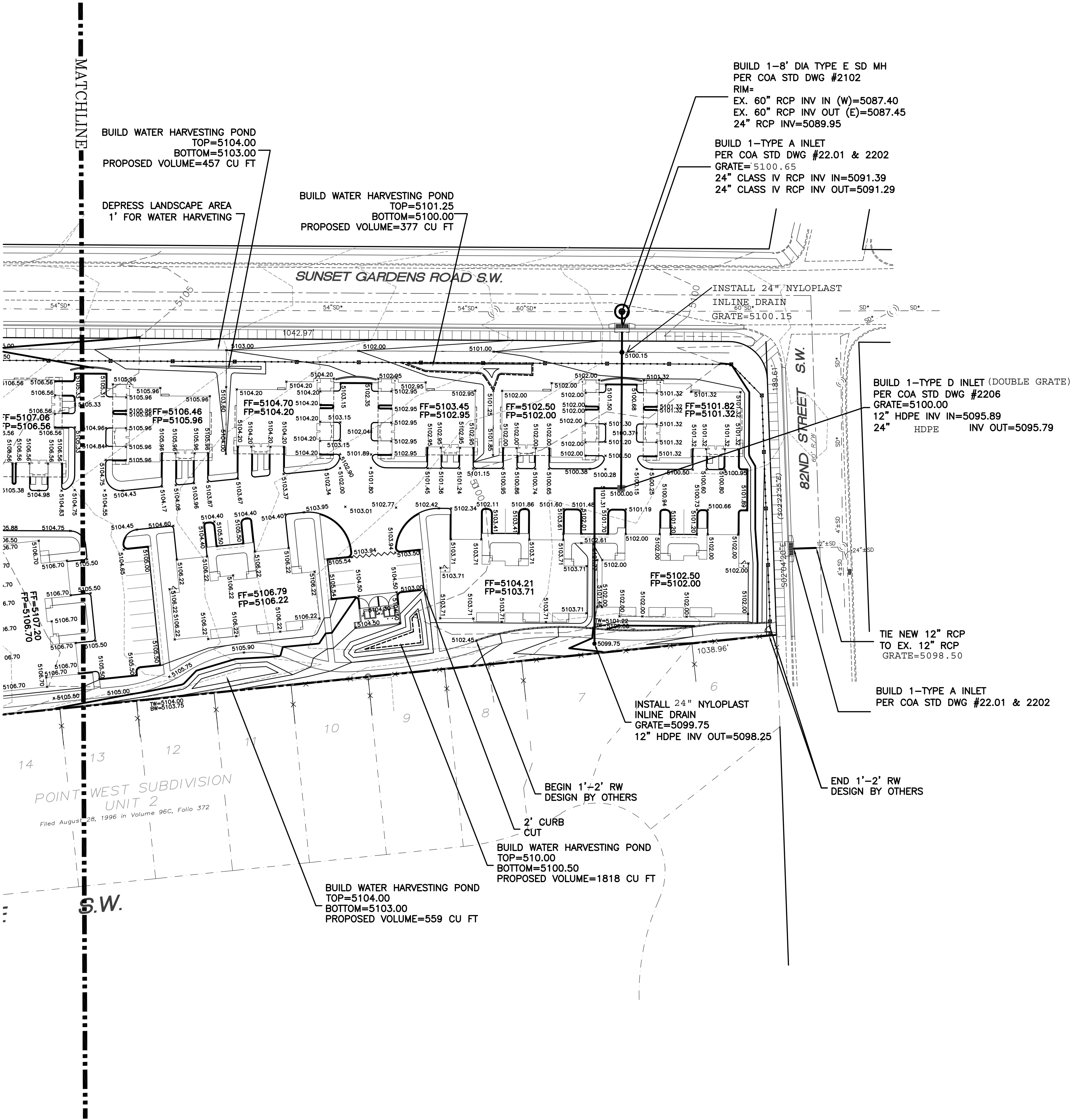


LEGAL DESCRIPTION:  
TRACT 52, UNIT 2, TOWN OF ATRISCO GRANT

- NOTES:
1. ALL SPOT ELEVATIONS REPRESENT FLOWLINE ELEVATION UNLESS OTHERWISE NOTED.
  2. ALL CURB AND GUTTER TO 6" HEADER UNLESS OTHERWISE NOTED.
  3. ALL RETAINING WALL DESIGN SHALL BE BY OTHERS.
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LEGEND	
-----5414-----	EXISTING CONTOUR
-----5415-----	EXISTING INDEX CONTOUR
-----5414-----	PROPOSED CONTOUR
-----5415-----	PROPOSED INDEX CONTOUR
-----5415-----	SLOPE TIE
× 4048.25	EXISTING SPOT ELEVATION
× 4048.25	PROPOSED SPOT ELEVATION
-----	BOUNDARY
-----	CENTERLINE
-----	RIGHT-OF-WAY
-----	PROPOSED CURB
-----	EXISTING CURB AND GUTTER
-----	PROPOSED SIDEWALK
-----	EXISTING SIDEWALK
-----	PROPOSED SCREEN WALL
-----	FLOWLINE

<div>ENGINEER'S SEAL</div> <div>DAVID SOULE NEW MEXICO 14522 REGISTERED PROFESSIONAL ENGINEER</div> <div>10/3/18</div> <div>DAVID SOULE P.E. #14522</div>	86TH AND SUNSET GARDENS GRADING AND DRAINAGE PLAN	DRAWN BY WCWJ
		DATE 7-17-18
		21894-LAYOUT-5-01-18
<div>10/3/18</div> <div>DAVID SOULE P.E. #14522</div>	<div>Rio Grande Engineering</div> <div>1606 CENTRAL AVENUE SE SUITE 201 ALBUQUERQUE, NM 87106 (505) 872-0999</div>	SHEET # 2
		JOB # 21894



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EXISTING UTILITIES ARE NOT SHOWN.  
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