

# CITY OF ALBUQUERQUE

Planning Department  
Brennon Williams, Director



Mayor Timothy M. Keller

November 12, 2020

Howard Cake, P.E.  
TyLin International  
500 4th St NW, Suite 403F  
Albuquerque, NM 87102

**RE: Shari Vista  
Draft Drainage Memo  
Engineer's Stamp Date: No Stamp  
Hydrology File: L12D013**

Dear Mr. Cake:

PO Box 1293

Albuquerque

NM 87103

www.cabq.gov

Based upon the information provided in your submittal received 11/03/2020, the Draft Drainage Memo **is not** approved for Work Order. The following comments need to be addressed for approval of the above referenced project:

1. Per the Department of Municipal Development, the City is not willing to accept maintenance on the underground infiltrators that you have designed for placement in the street, unless the County agrees to maintain them.
2. Since this project centers around this underground system, any further review of the Draft Drainage Memo is pointless at this time.

If you have any questions, please contact me at 924-3995 or [rbrissette@cabq.gov](mailto:rbrissette@cabq.gov).

Sincerely,

A handwritten signature in purple ink that reads "Renée C. Brissette".

Renée C. Brissette, P.E. CFM  
Senior Engineer, Hydrology  
Planning Department



# City of Albuquerque

Planning Department  
Development & Building Services Division

## DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 11/2018)

**Project Title:** \_\_\_\_\_ Building Permit #: \_\_\_\_\_ Hydrology File #: \_\_\_\_\_

DRB#: \_\_\_\_\_ EPC#: \_\_\_\_\_ Work Order#: \_\_\_\_\_

Legal Description: \_\_\_\_\_

City Address: \_\_\_\_\_

**Applicant:** \_\_\_\_\_ Contact: \_\_\_\_\_

Address: \_\_\_\_\_

Phone#: \_\_\_\_\_ Fax#: \_\_\_\_\_ E-mail: \_\_\_\_\_

**Owner:** \_\_\_\_\_ Contact: \_\_\_\_\_

Address: \_\_\_\_\_

Phone#: \_\_\_\_\_ Fax#: \_\_\_\_\_ E-mail: \_\_\_\_\_

**TYPE OF SUBMITTAL:** \_\_\_\_\_ PLAT (\_\_\_\_ # OF LOTS) \_\_\_\_\_ RESIDENCE \_\_\_\_\_ DRB SITE \_\_\_\_\_ ADMIN SITE

IS THIS A RESUBMITTAL?: \_\_\_\_\_ Yes \_\_\_\_\_ No

**DEPARTMENT:** \_\_\_\_\_ TRAFFIC/ TRANSPORTATION \_\_\_\_\_ HYDROLOGY/ DRAINAGE

Check all that Apply:

**TYPE OF SUBMITTAL:**

- ENGINEER/ARCHITECT CERTIFICATION
- PAD CERTIFICATION
- CONCEPTUAL G & D PLAN
- GRADING PLAN
- DRAINAGE MASTER PLAN
- DRAINAGE REPORT
- FLOODPLAIN DEVELOPMENT PERMIT APPLIC
- ELEVATION CERTIFICATE
- CLOMR/LOMR
- TRAFFIC CIRCULATION LAYOUT (TCL)
- TRAFFIC IMPACT STUDY (TIS)
- OTHER (SPECIFY) \_\_\_\_\_
- PRE-DESIGN MEETING?

**TYPE OF APPROVAL/ACCEPTANCE SOUGHT:**

- BUILDING PERMIT APPROVAL
- CERTIFICATE OF OCCUPANCY
- PRELIMINARY PLAT APPROVAL
- SITE PLAN FOR SUB'D APPROVAL
- SITE PLAN FOR BLDG. PERMIT APPROVAL
- FINAL PLAT APPROVAL
- SIA/ RELEASE OF FINANCIAL GUARANTEE
- FOUNDATION PERMIT APPROVAL
- GRADING PERMIT APPROVAL
- SO-19 APPROVAL
- PAVING PERMIT APPROVAL
- GRADING/ PAD CERTIFICATION
- WORK ORDER APPROVAL
- CLOMR/LOMR
- FLOODPLAIN DEVELOPMENT PERMIT
- OTHER (SPECIFY) \_\_\_\_\_

DATE SUBMITTED: \_\_\_\_\_ By: \_\_\_\_\_

COA STAFF:

ELECTRONIC SUBMITTAL RECEIVED: \_\_\_\_\_

FEE PAID: \_\_\_\_\_

**Subject:** Draft Drainage Memo for Shari Vista Road (Pear Road to End of Shari Vista Road), Albuquerque, New Mexico  
**Bernalillo County Engineering Services On-Call**  
**Task Order #3, P.W.C.O. 2020-XXXX**

October 27, 2020

This memo documents the drainage improvements for the Shari Vista Road project (Pear Road to End of Shari Vista Road). Included are the onsite hydrologic and hydraulic calculations for the proposed drainage infrastructure based on the roadway improvements. A hydraulic analysis was performed to determine the extent of drainage improvements required to address ponding issues within the roadway.

### **SITE DESCRIPTION**

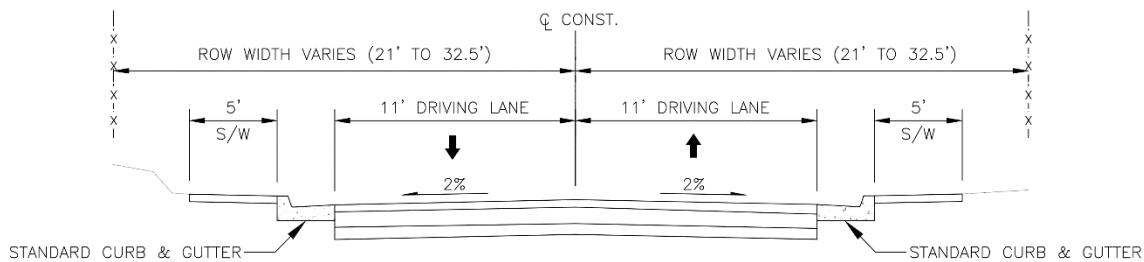
The Shari Vista Road project is located in Albuquerque, New Mexico. Shari Vista Road is an existing 2-lane roadway without curb and gutter or pedestrian facilities. Shari Vista terminates at a cul-de-sac and does not have an outlet. Roadway slopes vary greatly and have a longitudinal slope ranging from zero to 0.5% with an average cross-slope of 0.5%. The roadway is bounded in all directions by single-family residential developments. The area is relatively flat.

Existing onsite stormwater runoff flows from adjacent properties onto Shari Vista Road. There are no existing storm inlets or drainage infrastructure within the project corridor.

**Exhibit 1 in Appendix C** displays the Shari Vista Road existing conditions and hydrologic results.

### **PROPOSED IMPROVEMENTS**

The general design of the proposed roadway is a two-lane facility with curb, gutter and sidewalk on each side. The typical section is at a normal crown with a low point within the cul-de-sac where stormwater runoff will be captured by proposed storm inlets routes flows to a proposed underground storage chamber located within the corridor. **Figure 1** depicts the proposed typical section for the Shari Vista project.



**Figure 1 Proposed Typical Section**

## **OFFSITE HYDROLOGY**

Smaller localized flow generated within the residential development adjacent to the roadway are analyzed as onsite stormwater runoff. Based on our initial review, the proposed roadway improvements along Shari Vista Road will not impact offsite or onsite flow patterns or concentration points.

Re-evaluating the offsite hydrology is beyond the scope of this project. However, future review of the Pear Road improvement project, drainage report and field verification of flow patterns and concentration points will be conducted upon receipt of the Pear Road improvement project documents. Based on current conditions along Pear Road and adjacent residences, existing grading, wall elevations and elevations slope away from Shari Vista Road. There is not expected to be any offsite flow impacts.

## **HYDROLOGIC CALCULATIONS**

A hydrologic evaluation was performed for the Shari Vista Road project using the methodology from Chapter 6 of the City of Albuquerque Development Process Manual (DPM) (2020). The peak discharges for the 2-year, 10-year, and 100-year frequency design storms were calculated for the existing and proposed conditions of the new improvements. As specified in the DPM, the 6-hour storm duration for these events was used. Only the improvement areas were calculated. The existing areas consist of both soil type C (unpaved lots, roads, trails and desert landscaping) and soil type D (impervious areas) as specified in the DPM. **Table 1** summarizes the onsite stormwater discharge.

**Table 1 Onsite Subbasin Discharge**

Basin ID	Contributing Area (sf)	Contributing Area (ac)	Q <sub>P2</sub> Discharge (cfs)	Q <sub>P10</sub> Discharge (cfs)	Q <sub>P100</sub> Discharge (cfs)
BASIN01	61,721	1.42	1.1	2.5	4.6

**Exhibit 2 in Appendix C** displays the Shari Vista proposed improvements. Onsite hydrologic calculations are provided in **Appendix A**.

## **HYDRAULIC CALCULATIONS**

Onsite roadway drainage is intercepted by COA standard detail storm drain inlets located either on-grade or in sumps. The inlets are designed at the low point of the roadway, within the cul-de-sac, based upon criteria established within Chapter 6 of the DPM. Once intercepted, storm water is conveyed via connector pipes which discharge to the proposed underground storage chamber.

Inlet capacities and spread calculations for storm inlets were calculated using Bentley FlowMaster V8i. FlowMaster calculates inlet interception capacity and spread based on roadway variables including cross-slope, pavement grade, etc. Clogging factors used for curb openings and grate calculations were 80% and 50%, respectively.

Spread calculations were performed just upstream of catch basins utilizing the concrete gutter and asphalt Manning's n-values. According to the DPM, flow depths in the event of a 10-year design discharge may not exceed 0.5 feet in any collector or arterial street. For a 100-year design discharge, flow depths may not exceed 0.2 feet above curb height and shall be contained within the street right-of-way. Once the spread calculations were performed and deemed adequate, catch basins were placed and designed to capture a minimum of 80% of the incoming flow. Bypass flows were routed to the appropriate downstream catch basin.

Inlet capacities and spread calculations are provided in **Appendix B**.

**Table 2 Shari Vista Proposed Storm Inlets – 10-year Design Storm**

Inlet ID	Station	Type	Storm Runoff Captured (cfs)	Inlet Efficiency	Calculated Spread (ft)
<b>Inlet-01</b>	3+96 RT	Type A Single, On Grade	1.17	93%	9.6
<b>Inlet-02</b>	4+17 LT	Type A Single, On Grade	1.17	93%	9.6
<b>Inlet-03</b>	4+21 RT	Type A Single, Double Wing, Sag	0.17	100%	-

StormCAD version V8i (Select Series 5, Bentley 2016) was used to calculate and document the storm drain hydraulics. The captured flow from each grate inlet was input into the StormCAD model to calculate the storm drain system hydraulic grade line (HGL) accounting for friction loss, junctions, bends transitions, and manholes. The headloss method used to model the storm drain systems is derived from the Federal Highway Administration Hydraulic Engineering Circular No. 22, Second Edition (HEC-22) Urban Drainage Design Manual (2009). The HEC-22 Headloss method computes an adjusted headloss coefficient using correction factors for the diameter of the pipe, flow depth, relative flow, plunging flow, and benching of the structure. These correction factors are then multiplied to the initial headloss coefficient and then multiplied to the velocity head at the outlet pipe to determine the total junction headloss for the storm inlet and manhole structures.

The proposed storm drain system is modeled for a 100-year design storm event. The hydraulic criteria for the storm drain system is such that the 100-year HGL is maintained below the gutter elevation for this project.

The results for the StormCAD analysis is provided in **Appendix B**.

#### **STORMWATER STORAGE CHAMBER**

The proposed underground stormwater storage chamber will provide storage volume for a 100-year, 6-hour design storm. The total storage volume required for the project is 0.14 ac-ft, approximately 6,285 cubic feet. The excess precipitation and volumetric runoff calculation has been provided in **Appendix A**. The infrastructure stage-storage volume report has been provided in **Appendix B**.

The existing utilities within Shari Vista Road run parallel with multiple service lines crossing the roadway to the adjacent properties. The proposed underground storage chamber and storm drain system cross underground gas, water, cable utilities. The potential utility conflicts will be coordinated with each utility company.

### **SUMMARY**

This memo documents the drainage analysis of the Shari Vista roadway improvements. Three storm inlets are proposed within the cul-de-sac of Shari Vista Road to capture stormwater runoff and conveyed to an underground stormwater storage chamber proposed within the Shari Vista Road corridor. The proposed roadway improvements and storm drain infrastructure adequately address the existing ponding issues.

Sincerely,

Howard Cake , P.E.  
Sr. Project Manager  
T.Y. Lin International

Tate Toledo, P.E.  
Project Engineer  
T.Y. Lin International

## **APPENDIX A**

**Hydrologic Data & Calculations**

## On-Site Subbasin Calculations

**Project:** Shari Vista Road  
**Location:** Albuquerque, NM  
**Date:** October 7, 2020

**References:** City of Albuquerque Development Process Manual (2020),  
Chapter 6 - Drainage, Flood Control, and Erosion Control

Precipitation Zone: 1	Intensity
	2-yr, 6-hr= 1.86
	10-yr, 6-hr= 3.00
	100-yr, 6-hr= 4.77

**Basin ID:** BASIN01

### 1. Land Treatment Areas

A:	0 sq.ft.	0.00 ac.
B:	0 sq.ft.	0.00 ac.
C:	48732 sq.ft.	1.12 ac.
D:	12989 sq.ft.	0.30 ac.
TOTAL:	61721 sq.ft.	1.42 ac.

### 2. Weighted C\*A, Rational Coefficient\*Acre

$C^*A_2 =$	0.6
$C^*A_{10} =$	0.8
$C^*A_{100} =$	1.0

### 3. Peak Discharge, Q

$Q_2 =$	1.1 cfs
$Q_{10} =$	2.5 cfs
$Q_{100} =$	4.6 cfs

**Excess Precipitation & Volumetric Runoff****Project:** Shari Vista Road**Location:** Albuquerque, NM**Date:** October 6, 2020**References:** City of Albuquerque Development Process Manual (2020),  
Chapter 6 - Drainage, Flood Control, and Erosion Control**Precipitation Zone:** 1**Basin ID:** Shari Vista**1. Land Treatment Areas, A**

A:	0 sq.ft.	0.00 ac.
B:	0 sq.ft.	0.00 ac.
C:	48732 sq.ft.	1.12 ac.
D:	12989 sq.ft.	0.30 ac.
Total:	61721 sq.ft.	1.42 ac.

**2. Excess Precipitation, E**

A:	0.55 in.
B:	0.73 in.
C:	0.95 in.
D:	2.24 in.

**2. Weighted E**

E\*A / Total A= 1.22

**3. Runoff Volume (6-hour), V<sub>360</sub>**

Weighted E \* Total A= 0.14 acre-ft  
**6283 cf**

**Required Volume = 6285 cf**



**NOAA Atlas 14, Volume 1, Version 5**  
**Location name: Albuquerque, New Mexico, USA\***  
**Latitude: 35.0641°, Longitude: -106.6862°**  
**Elevation: 4942.65 ft\*\***  
 \* source: ESRI Maps  
 \*\* source: USGS



### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps & aerials](#)

### PF tabular

<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour)<sup>1</sup></b>										
<b>Duration</b>	<b>Average recurrence interval (years)</b>									
	<b>1</b>	<b>2</b>	<b>5</b>	<b>10</b>	<b>25</b>	<b>50</b>	<b>100</b>	<b>200</b>	<b>500</b>	<b>1000</b>
<b>5-min</b>	<b>2.03</b> (1.75-2.36)	<b>2.64</b> (2.27-3.06)	<b>3.53</b> (3.02-4.10)	<b>4.24</b> (3.61-4.91)	<b>5.20</b> (4.40-6.01)	<b>5.94</b> (5.02-6.89)	<b>6.73</b> (5.65-7.80)	<b>7.57</b> (6.31-8.76)	<b>8.71</b> (7.18-10.11)	<b>9.60</b> (7.86-11.1)
<b>10-min</b>	<b>1.55</b> (1.33-1.80)	<b>2.00</b> (1.72-2.33)	<b>2.69</b> (2.30-3.13)	<b>3.22</b> (2.75-3.73)	<b>3.95</b> (3.35-4.58)	<b>4.52</b> (3.82-5.24)	<b>5.13</b> (4.30-5.93)	<b>5.76</b> (4.80-6.67)	<b>6.62</b> (5.46-7.67)	<b>7.31</b> (5.98-8.46)
<b>15-min</b>	<b>1.28</b> (1.10-1.49)	<b>1.66</b> (1.42-1.93)	<b>2.22</b> (1.90-2.58)	<b>2.66</b> (2.27-3.09)	<b>3.27</b> (2.77-3.78)	<b>3.74</b> (3.16-4.33)	<b>4.24</b> (3.55-4.90)	<b>4.76</b> (3.96-5.51)	<b>5.47</b> (4.51-6.34)	<b>6.04</b> (4.94-7.00)
<b>30-min</b>	<b>0.862</b> (0.742-1.00)	<b>1.12</b> (0.958-1.30)	<b>1.49</b> (1.28-1.74)	<b>1.79</b> (1.53-2.08)	<b>2.20</b> (1.87-2.55)	<b>2.52</b> (2.13-2.91)	<b>2.85</b> (2.39-3.30)	<b>3.21</b> (2.67-3.71)	<b>3.69</b> (3.04-4.27)	<b>4.07</b> (3.33-4.71)
<b>60-min</b>	<b>0.533</b> (0.459-0.619)	<b>0.690</b> (0.592-0.803)	<b>0.925</b> (0.792-1.08)	<b>1.11</b> (0.947-1.29)	<b>1.36</b> (1.15-1.58)	<b>1.56</b> (1.32-1.80)	<b>1.77</b> (1.48-2.04)	<b>1.98</b> (1.65-2.30)	<b>2.28</b> (1.88-2.64)	<b>2.52</b> (2.06-2.91)
<b>2-hr</b>	<b>0.302</b> (0.260-0.358)	<b>0.387</b> (0.332-0.459)	<b>0.512</b> (0.438-0.606)	<b>0.614</b> (0.522-0.720)	<b>0.754</b> (0.636-0.884)	<b>0.868</b> (0.727-1.01)	<b>0.988</b> (0.821-1.16)	<b>1.11</b> (0.919-1.30)	<b>1.29</b> (1.05-1.51)	<b>1.44</b> (1.16-1.68)
<b>3-hr</b>	<b>0.216</b> (0.187-0.255)	<b>0.275</b> (0.237-0.324)	<b>0.360</b> (0.311-0.424)	<b>0.429</b> (0.368-0.502)	<b>0.524</b> (0.445-0.611)	<b>0.600</b> (0.508-0.700)	<b>0.682</b> (0.573-0.794)	<b>0.769</b> (0.640-0.895)	<b>0.889</b> (0.732-1.03)	<b>0.987</b> (0.804-1.15)
<b>6-hr</b>	<b>0.126</b> (0.110-0.147)	<b>0.158</b> (0.138-0.185)	<b>0.204</b> (0.178-0.238)	<b>0.241</b> (0.209-0.280)	<b>0.290</b> (0.250-0.337)	<b>0.329</b> (0.282-0.381)	<b>0.370</b> (0.316-0.429)	<b>0.412</b> (0.350-0.478)	<b>0.472</b> (0.396-0.547)	<b>0.521</b> (0.433-0.605)
<b>12-hr</b>	<b>0.070</b> (0.061-0.080)	<b>0.088</b> (0.077-0.100)	<b>0.111</b> (0.098-0.127)	<b>0.130</b> (0.114-0.148)	<b>0.155</b> (0.135-0.176)	<b>0.174</b> (0.151-0.198)	<b>0.194</b> (0.167-0.220)	<b>0.215</b> (0.184-0.244)	<b>0.243</b> (0.206-0.276)	<b>0.266</b> (0.223-0.303)
<b>24-hr</b>	<b>0.039</b> (0.035-0.045)	<b>0.049</b> (0.044-0.056)	<b>0.061</b> (0.054-0.069)	<b>0.071</b> (0.063-0.080)	<b>0.084</b> (0.074-0.095)	<b>0.094</b> (0.083-0.106)	<b>0.105</b> (0.092-0.118)	<b>0.115</b> (0.101-0.130)	<b>0.130</b> (0.112-0.146)	<b>0.141</b> (0.121-0.158)
<b>2-day</b>	<b>0.021</b> (0.018-0.023)	<b>0.026</b> (0.023-0.029)	<b>0.032</b> (0.029-0.036)	<b>0.037</b> (0.033-0.041)	<b>0.044</b> (0.039-0.048)	<b>0.049</b> (0.043-0.054)	<b>0.054</b> (0.047-0.060)	<b>0.059</b> (0.052-0.066)	<b>0.066</b> (0.058-0.074)	<b>0.071</b> (0.062-0.079)
<b>3-day</b>	<b>0.015</b> (0.014-0.017)	<b>0.019</b> (0.017-0.021)	<b>0.023</b> (0.021-0.025)	<b>0.026</b> (0.024-0.029)	<b>0.031</b> (0.028-0.034)	<b>0.034</b> (0.031-0.038)	<b>0.038</b> (0.034-0.042)	<b>0.041</b> (0.037-0.045)	<b>0.046</b> (0.041-0.051)	<b>0.049</b> (0.044-0.054)
<b>4-day</b>	<b>0.012</b> (0.011-0.013)	<b>0.015</b> (0.014-0.016)	<b>0.018</b> (0.017-0.020)	<b>0.021</b> (0.019-0.023)	<b>0.025</b> (0.022-0.027)	<b>0.027</b> (0.025-0.030)	<b>0.030</b> (0.027-0.032)	<b>0.032</b> (0.029-0.035)	<b>0.036</b> (0.032-0.039)	<b>0.038</b> (0.035-0.042)
<b>7-day</b>	<b>0.008</b> (0.007-0.009)	<b>0.010</b> (0.009-0.011)	<b>0.012</b> (0.011-0.013)	<b>0.014</b> (0.012-0.015)	<b>0.016</b> (0.014-0.017)	<b>0.017</b> (0.016-0.018)	<b>0.019</b> (0.017-0.020)	<b>0.020</b> (0.018-0.022)	<b>0.022</b> (0.020-0.024)	<b>0.023</b> (0.021-0.025)
<b>10-day</b>	<b>0.006</b> (0.006-0.007)	<b>0.008</b> (0.007-0.008)	<b>0.009</b> (0.009-0.010)	<b>0.011</b> (0.010-0.011)	<b>0.012</b> (0.011-0.013)	<b>0.013</b> (0.012-0.014)	<b>0.015</b> (0.013-0.016)	<b>0.016</b> (0.015-0.017)	<b>0.017</b> (0.016-0.019)	<b>0.019</b> (0.017-0.020)
<b>20-day</b>	<b>0.004</b> (0.003-0.004)	<b>0.005</b> (0.004-0.005)	<b>0.006</b> (0.005-0.006)	<b>0.006</b> (0.006-0.007)	<b>0.007</b> (0.007-0.008)	<b>0.008</b> (0.007-0.009)	<b>0.009</b> (0.008-0.009)	<b>0.009</b> (0.008-0.010)	<b>0.010</b> (0.009-0.011)	<b>0.010</b> (0.010-0.011)
<b>30-day</b>	<b>0.003</b> (0.003-0.003)	<b>0.004</b> (0.003-0.004)	<b>0.004</b> (0.004-0.005)	<b>0.005</b> (0.005-0.005)	<b>0.006</b> (0.005-0.006)	<b>0.006</b> (0.006-0.007)	<b>0.007</b> (0.006-0.007)	<b>0.007</b> (0.006-0.008)	<b>0.007</b> (0.007-0.008)	<b>0.008</b> (0.007-0.008)
<b>45-day</b>	<b>0.002</b> (0.002-0.003)	<b>0.003</b> (0.003-0.003)	<b>0.004</b> (0.003-0.004)	<b>0.004</b> (0.004-0.004)	<b>0.004</b> (0.004-0.005)	<b>0.005</b> (0.004-0.005)	<b>0.005</b> (0.005-0.005)	<b>0.005</b> (0.005-0.006)	<b>0.006</b> (0.005-0.006)	<b>0.006</b> (0.005-0.006)
<b>60-day</b>	<b>0.002</b> (0.002-0.002)	<b>0.003</b> (0.002-0.003)	<b>0.003</b> (0.003-0.003)	<b>0.003</b> (0.003-0.004)	<b>0.004</b> (0.004-0.004)	<b>0.004</b> (0.004-0.004)	<b>0.004</b> (0.004-0.004)	<b>0.005</b> (0.004-0.005)	<b>0.005</b> (0.005-0.005)	<b>0.005</b> (0.005-0.005)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

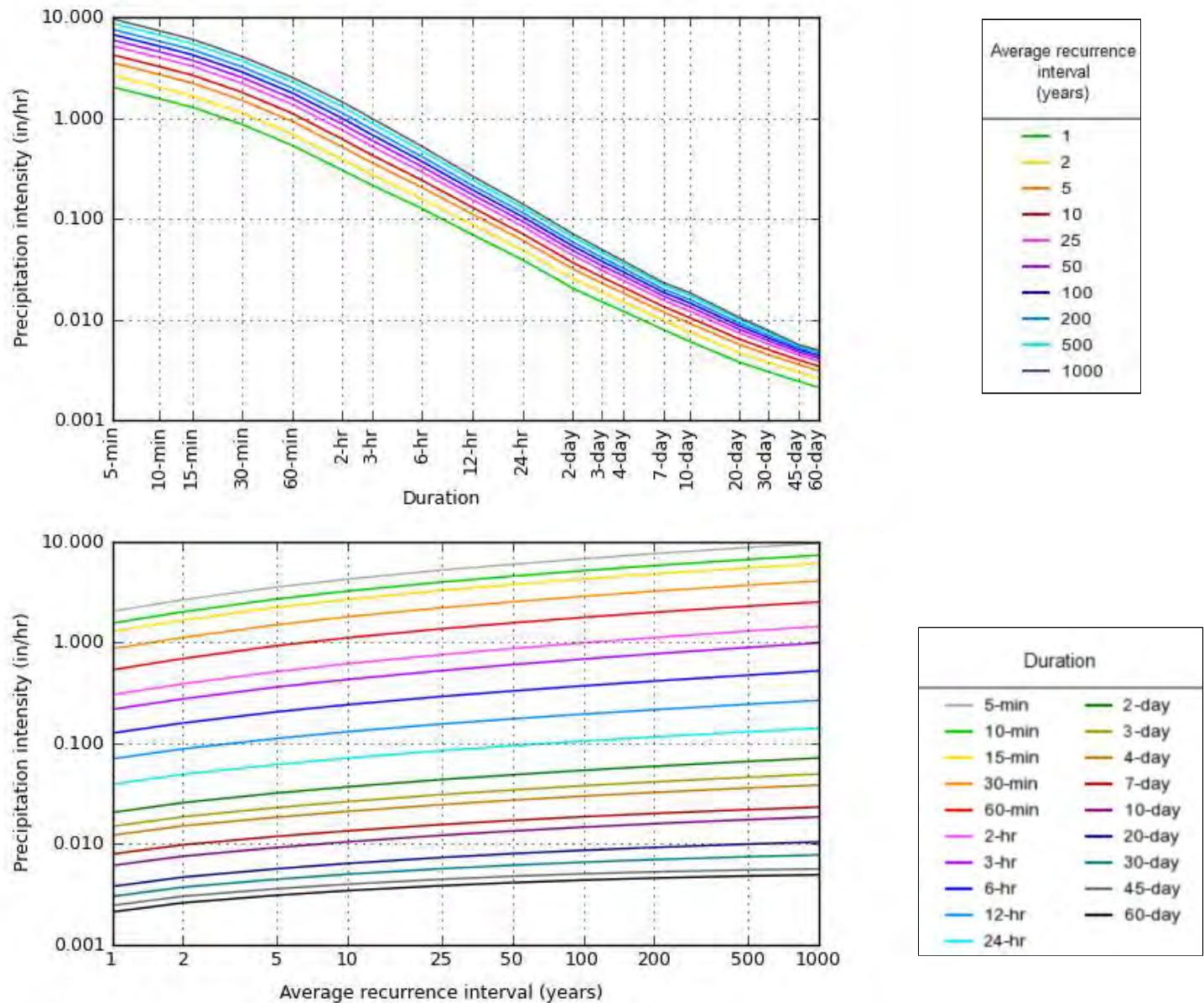
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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### PF graphical

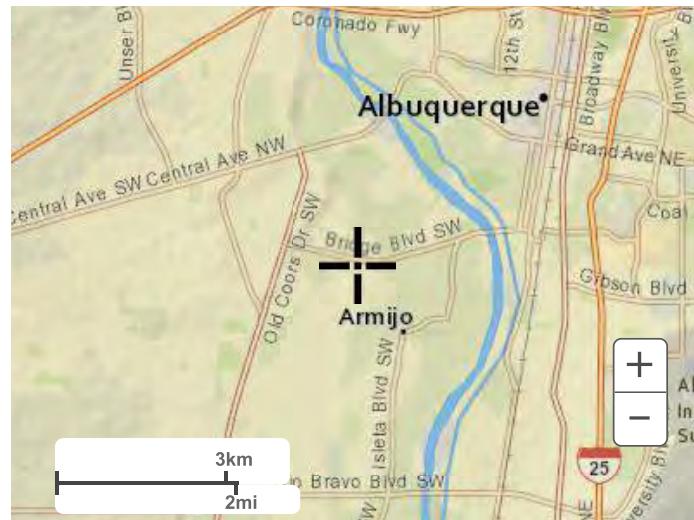
PDS-based intensity-duration-frequency (IDF) curves  
Latitude: 35.0641°, Longitude: -106.6862°



NOAA Atlas 14, Volume 1, Version 5

Created (GMT): Wed Jun 10 20:06:22 2020

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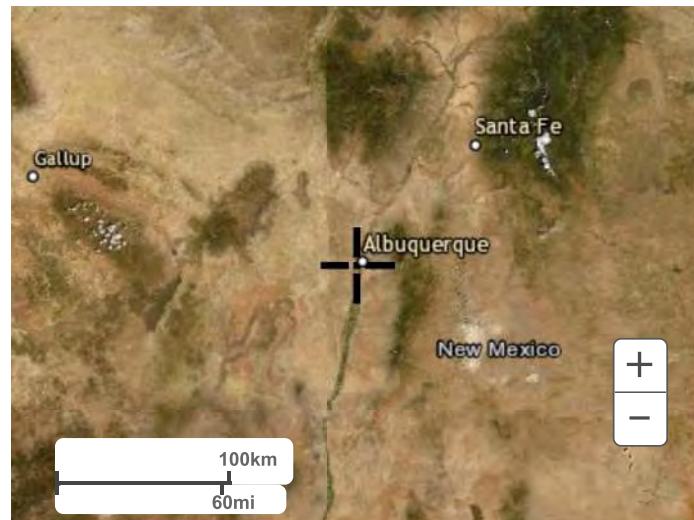
Large scale terrain



Large scale map



Large scale aerial



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**NOAA Atlas 14, Volume 1, Version 5****Location name: Albuquerque, New Mexico, USA\*****Latitude: 35.0641°, Longitude: -106.6862°****Elevation: 4942.65 ft\*\***

\* source: ESRI Maps

\*\* source: USGS

**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps & aerials](#)
**PF tabular**

Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.169 (0.146-0.197)	0.220 (0.189-0.255)	0.294 (0.252-0.342)	0.353 (0.301-0.409)	0.433 (0.367-0.501)	0.495 (0.418-0.574)	0.561 (0.471-0.650)	0.631 (0.526-0.730)	0.726 (0.598-0.840)	0.800 (0.655-0.927)
10-min	0.258 (0.222-0.300)	0.334 (0.287-0.389)	0.448 (0.383-0.521)	0.537 (0.458-0.622)	0.659 (0.559-0.763)	0.754 (0.637-0.873)	0.855 (0.716-0.989)	0.960 (0.800-1.11)	1.10 (0.910-1.28)	1.22 (0.997-1.41)
15-min	0.320 (0.275-0.372)	0.414 (0.356-0.482)	0.555 (0.475-0.646)	0.665 (0.568-0.772)	0.817 (0.693-0.946)	0.934 (0.789-1.08)	1.06 (0.888-1.23)	1.19 (0.991-1.38)	1.37 (1.13-1.59)	1.51 (1.24-1.75)
30-min	0.431 (0.371-0.501)	0.558 (0.479-0.649)	0.747 (0.640-0.870)	0.896 (0.765-1.04)	1.10 (0.933-1.27)	1.26 (1.06-1.46)	1.43 (1.20-1.65)	1.60 (1.34-1.86)	1.84 (1.52-2.13)	2.03 (1.67-2.36)
60-min	0.533 (0.459-0.619)	0.690 (0.592-0.803)	0.925 (0.792-1.08)	1.11 (0.947-1.29)	1.36 (1.15-1.58)	1.56 (1.32-1.80)	1.77 (1.48-2.04)	1.98 (1.65-2.30)	2.28 (1.88-2.64)	2.52 (2.06-2.91)
2-hr	0.605 (0.519-0.716)	0.774 (0.663-0.918)	1.02 (0.876-1.21)	1.23 (1.04-1.44)	1.51 (1.27-1.77)	1.74 (1.45-2.03)	1.98 (1.64-2.31)	2.23 (1.84-2.60)	2.59 (2.11-3.02)	2.87 (2.32-3.36)
3-hr	0.649 (0.562-0.765)	0.825 (0.712-0.973)	1.08 (0.934-1.27)	1.29 (1.11-1.51)	1.57 (1.34-1.84)	1.80 (1.53-2.10)	2.05 (1.72-2.38)	2.31 (1.92-2.69)	2.67 (2.20-3.11)	2.96 (2.42-3.46)
6-hr	0.753 (0.656-0.880)	0.949 (0.828-1.11)	1.22 (1.07-1.43)	1.44 (1.25-1.68)	1.74 (1.50-2.02)	1.97 (1.69-2.28)	2.22 (1.89-2.57)	2.47 (2.09-2.86)	2.83 (2.37-3.28)	3.12 (2.59-3.62)
12-hr	0.840 (0.737-0.959)	1.06 (0.931-1.21)	1.34 (1.18-1.53)	1.57 (1.37-1.78)	1.87 (1.63-2.12)	2.10 (1.82-2.38)	2.34 (2.02-2.66)	2.59 (2.21-2.94)	2.93 (2.48-3.33)	3.20 (2.69-3.65)
24-hr	0.941 (0.834-1.07)	1.18 (1.05-1.33)	1.47 (1.31-1.67)	1.71 (1.51-1.93)	2.02 (1.78-2.28)	2.26 (1.99-2.55)	2.52 (2.20-2.83)	2.77 (2.41-3.11)	3.11 (2.69-3.50)	3.38 (2.91-3.80)
2-day	0.986 (0.879-1.11)	1.23 (1.10-1.38)	1.54 (1.37-1.72)	1.77 (1.58-1.98)	2.09 (1.86-2.33)	2.33 (2.07-2.60)	2.58 (2.28-2.87)	2.83 (2.49-3.16)	3.16 (2.77-3.53)	3.42 (2.98-3.82)
3-day	1.08 (0.976-1.19)	1.34 (1.22-1.48)	1.65 (1.50-1.82)	1.90 (1.72-2.09)	2.23 (2.01-2.45)	2.47 (2.22-2.72)	2.72 (2.44-2.99)	2.98 (2.66-3.27)	3.31 (2.94-3.64)	3.56 (3.15-3.92)
4-day	1.17 (1.07-1.28)	1.45 (1.33-1.58)	1.77 (1.62-1.93)	2.02 (1.85-2.20)	2.36 (2.15-2.56)	2.61 (2.38-2.84)	2.87 (2.61-3.11)	3.12 (2.83-3.39)	3.45 (3.12-3.75)	3.69 (3.33-4.02)
7-day	1.34 (1.23-1.45)	1.65 (1.52-1.79)	2.00 (1.84-2.17)	2.27 (2.09-2.45)	2.62 (2.41-2.83)	2.88 (2.64-3.11)	3.13 (2.87-3.38)	3.38 (3.09-3.64)	3.68 (3.37-3.98)	3.90 (3.57-4.22)
10-day	1.47 (1.35-1.59)	1.82 (1.67-1.97)	2.21 (2.04-2.39)	2.52 (2.33-2.72)	2.93 (2.70-3.15)	3.23 (2.97-3.47)	3.53 (3.24-3.79)	3.82 (3.50-4.11)	4.19 (3.82-4.51)	4.46 (4.06-4.80)
20-day	1.82 (1.67-1.98)	2.25 (2.08-2.45)	2.73 (2.51-2.96)	3.08 (2.84-3.34)	3.53 (3.25-3.82)	3.85 (3.54-4.16)	4.16 (3.82-4.49)	4.44 (4.08-4.79)	4.79 (4.39-5.17)	5.03 (4.61-5.43)
30-day	2.17 (2.00-2.35)	2.69 (2.48-2.90)	3.23 (2.97-3.47)	3.62 (3.33-3.89)	4.10 (3.78-4.40)	4.44 (4.09-4.76)	4.76 (4.38-5.10)	5.05 (4.65-5.41)	5.39 (4.96-5.77)	5.62 (5.17-6.02)
45-day	2.65 (2.45-2.86)	3.28 (3.03-3.53)	3.89 (3.60-4.18)	4.32 (4.00-4.64)	4.83 (4.48-5.18)	5.17 (4.80-5.55)	5.47 (5.09-5.86)	5.72 (5.33-6.12)	5.98 (5.59-6.39)	6.12 (5.74-6.52)
60-day	3.05 (2.82-3.30)	3.76 (3.49-4.06)	4.47 (4.15-4.81)	4.97 (4.62-5.34)	5.56 (5.17-5.98)	5.96 (5.55-6.40)	6.32 (5.88-6.78)	6.62 (6.18-7.11)	6.95 (6.50-7.46)	7.13 (6.70-7.65)

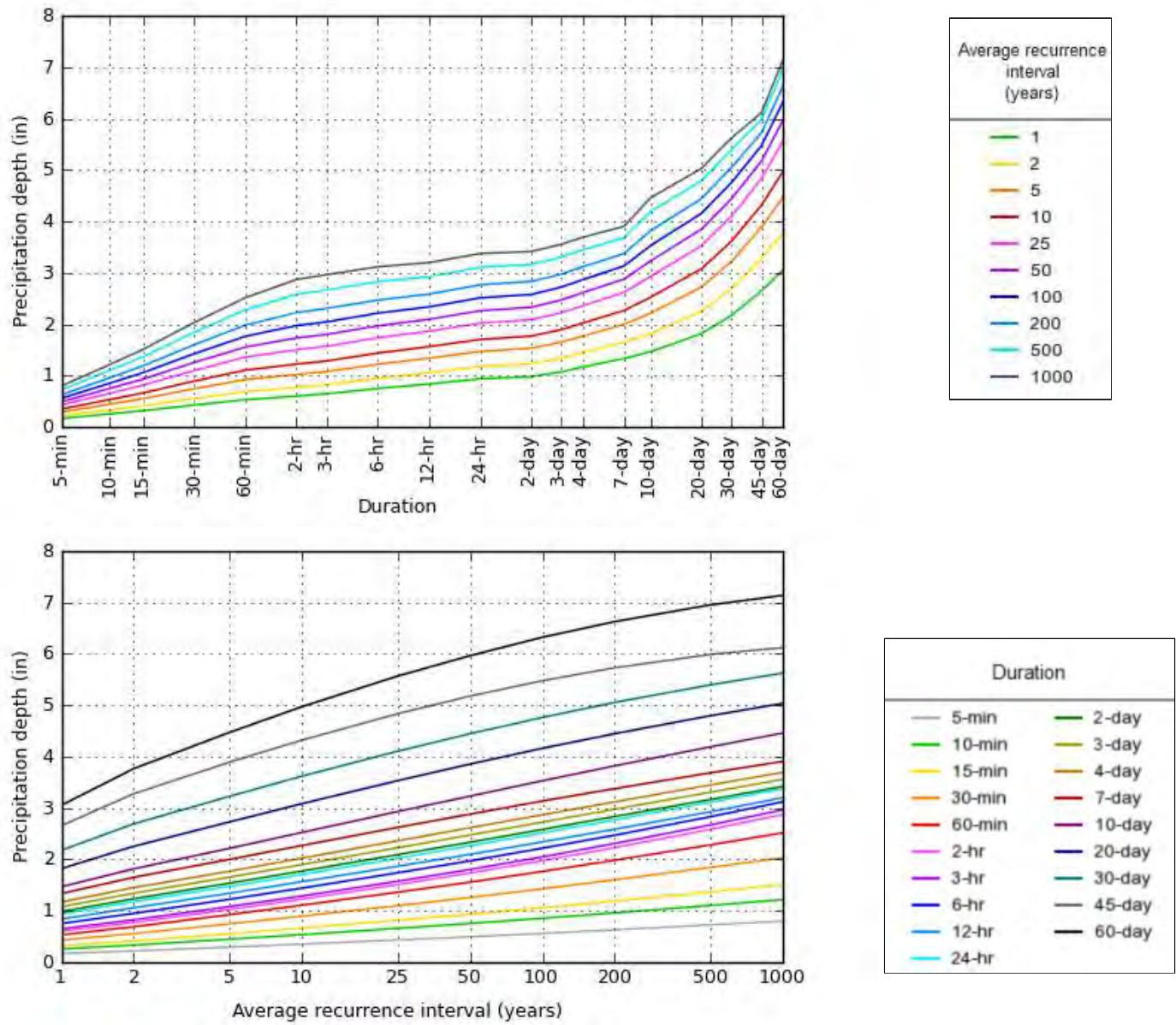
<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PDS-based depth-duration-frequency (DDF) curves  
Latitude: 35.0641°, Longitude: -106.6862°



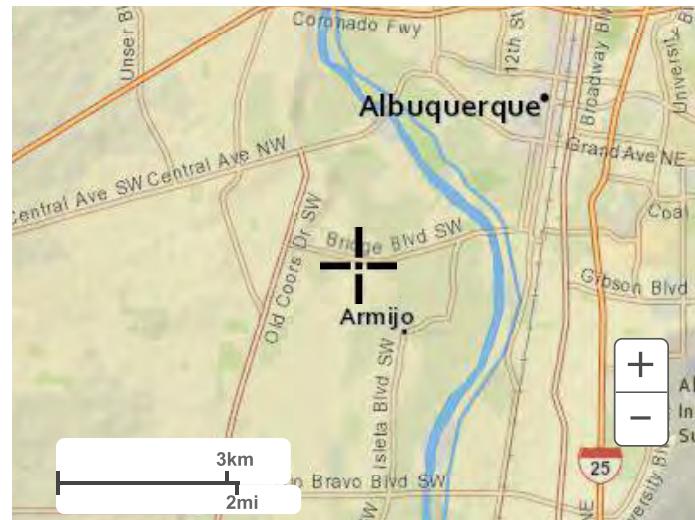
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## Maps & aerials

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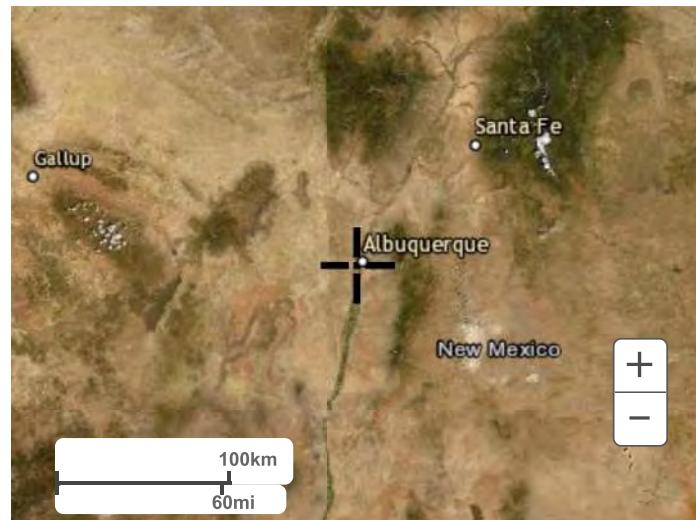
Large scale terrain



Large scale map



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## **APPENDIX B**

### **Hydraulic Calculation**

**Project:** Shari Vista Road  
**Location:** Albuquerque, NM  
**Date:** October 7, 2020  
**Subject:** Inlet Summary Calculations

**Proj. Engineer:** T. Toledo  
**Checker:** A. Herting / H. Cake

10-year Design Storm																	
Inlet (ID)	Road	Station	Offset	Contributing Subbasins	Inlet Type	Wing/Inlet Opening (ft)	Effective Opening (ft)	Slope (ft/ft)	Subbasin Flow (cfs)	Total Flow (Including Bypass) (cfs)	Captured Flow (cfs)	Captured Flow (%)	Bypass Flow (cfs)	Bypass To (Inlet ID)	Max Spread (ft)	Calculated Spread (ft)	Spread Acceptable? (Yes/No)
Inlet-01	Shari Vista Road	3+96	30' Rt	BASIN01	Type 'A', Single	7.5	6.0	0.0050	1.26	1.26	1.17	93%	0.09	Inlet-03	12.5	9.6	Yes
Inlet-02	Shari Vista Road	4+17	20' Lt	BASIN01	Type 'A', Single	7.5	6.0	0.0050	1.26	1.26	1.17	93%	0.09	Inlet-03	12.5	9.6	Yes
Inlet-03	Shari Vista Road	4+21	11' Rt	BASIN01	Type 'A', Single, Double Wing	14.5	11.6	SUMP	-	0.17	0.17	-	0.00	End of Project	-	-	-

100-year Design Storm																	
Inlet (ID)	Road	Station	Offset	Contributing Subbasins	Inlet Type	Wing/Inlet Opening (ft)	Effective Opening (ft)	Slope (ft/ft)	Subbasin Flow (cfs)	Total Flow (Including Bypass) (cfs)	Captured Flow (cfs)	Captured Flow (%)	Bypass Flow (cfs)	Bypass To (Inlet ID)	Calculated Spread (ft)	Calculated Depth (in)	Depth Acceptable? (Yes/No)
Inlet-01	Shari Vista Road	3+96	30' Rt	BASIN01	Type 'A', Single	7.5	6.0	0.0050	2.32	2.32	1.90	82%	0.42	Inlet-03	12.2	3.3	Yes
Inlet-02	Shari Vista Road	4+17	20' Lt	BASIN01	Type 'A', Single	7.5	6.0	0.0050	2.32	2.32	1.90	82%	0.42	Inlet-03	12.2	3.3	Yes
Inlet-03	Shari Vista Road	4+21	11' Rt	BASIN01	Type 'A', Single, Double Wing	14.5	11.6	SUMP	-	0.85	0.85	-	0.00	End of Project	-	-	-

**Notes:**

- 1) Effective opening for curb inlets is 80%. If a grate is included, a 50% clogging factor is applied
- 2) Captured flow calculations were performed using Bentley Flowmaster V8i.
- 3) Spread calculations were performed using Bentley Flowmaster V8i.
- 4) Storm Inlet Types per COA Standard Detail Drawings, Revised May 2020, Update 1C
- 5) Per COA DPM, flow depths in the event of a 10-year design discharge may not exceed 0.5 feet in any collector or arterial street. One lane free of flowing or standing water in each traffic direction must be preserved on arterial street
- 6) Per COA DPM, flow depths in the event of a 100-year design discharge may not exceed 0.2 feet above curb height and shall be contained within the street right-of-way

## Worksheet for 10yr Spread Calculation - S=0.50%

---

### Project Description

---

Friction Method	Manning Formula
Solve For	Normal Depth

---

### Input Data

---

Channel Slope	0.005 ft/ft
Discharge	1.26 cfs

---

### Section Definitions

Station (ft)	Elevation (ft)
0+00	10.00
0+00	10.00
0+01	9.33
0+02	9.40
0+13	9.62

### Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 10.00)	(0+02, 9.40)	0.013
(0+02, 9.40)	(0+13, 9.62)	0.017

---

### Options

---

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

---

### Results

---

Normal Depth	2.7 in
Elevation Range	9.3 to 10.0 ft
Flow Area	0.9 ft <sup>2</sup>
Wetted Perimeter	9.7 ft
Hydraulic Radius	1.2 in
Top Width	9.57 ft
Normal Depth	2.7 in
Critical Depth	2.4 in
Critical Slope	0.009 ft/ft
Velocity	1.35 ft/s
Velocity Head	0.03 ft
Specific Energy	0.25 ft
Froude Number	0.759
Flow Type	Subcritical

---

### GVF Input Data

---

## **Worksheet for 10yr Spread Calculation - S=0.50%**

---

### GVF Input Data

---

Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0

---

---

### GVF Output Data

---

Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	0.00 ft/s
Upstream Velocity	0.00 ft/s
Normal Depth	2.7 in
Critical Depth	2.4 in
Channel Slope	0.005 ft/ft
Critical Slope	0.009 ft/ft

---

## Worksheet for 10yr Storm Inlet 1&2 - On Grade

Project Description	
Solve For	Efficiency
Input Data	
Discharge	1.25 cfs
Slope	0.005 ft/ft
Gutter Width	2.50 ft
Gutter Cross Slope	0.042 ft/ft
Road Cross Slope	0.020 ft/ft
Roughness Coefficient	0.013
Local Depression	2.8 in
Local Depression Width	90.0 in
Grate Width	2.08 ft
Grate Length	3.3 ft
Grate Type	P-50 mm (P-1 -7/8")
Clogging	50.0 %
Curb Opening Length	6.0 ft
Options	
Calculation Option	Use Both
Grate Flow Option	Exclude None
Results	
Efficiency	93.39 %
Intercepted Flow	1.17 cfs
Bypass Flow	0.08 cfs
Spread	7.6 ft
Depth	2.5 in
Flow Area	0.6 ft <sup>2</sup>
Gutter Depression	0.7 in
Total Depression	3.4 in
Velocity	1.95 ft/s
Splash Over Velocity	7.39 ft/s
Frontal Flow Factor	1.000
Side Flow Factor	0.115
Grate Flow Ratio	0.641
Equivalent Cross Slope	0.047 ft/ft
Active Grate Length	1.7 ft
Length Factor	0.383
Total Interception Length	11.3 ft

## Worksheet for 10yr Storm Inlet 3 - Sag

Project Description	
Solve For	Spread
Input Data	
Discharge	0.17 cfs
Gutter Width	2.50 ft
Gutter Cross Slope	0.042 ft/ft
Road Cross Slope	0.020 ft/ft
Local Depression	2.8 in
Local Depression Width	174.0 in
Grate Width	2.08 ft
Grate Length	3.3 ft
Grate Type	P-50 mm (P-1 -7/8")
Clogging	50.0 %
Curb Opening Length	11.6 ft
Opening Height	0.5 ft
Curb Throat Type	Horizontal
Throat Incline Angle	90.00 degrees
Options	
Calculation Option	Use Both
Results	
Spread	1.9 ft
Depth	-1.4 in
Gutter Depression	0.7 in
Total Depression	3.4 in
Open Grate Area	3.1 ft <sup>2</sup>
Active Grate Weir Length	5.4 ft

## Worksheet for 100yr Spread Calculation - S=0.50%

---

### Project Description

---

Friction Method	Manning Formula
Solve For	Normal Depth

---

### Input Data

---

Channel Slope	0.005 ft/ft
Discharge	2.32 cfs

---

### Section Definitions

Station (ft)	Elevation (ft)
0+00	10.00
0+00	10.00
0+01	9.33
0+02	9.40
0+13	9.62

### Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 10.00)	(0+02, 9.40)	0.013
(0+02, 9.40)	(0+13, 9.62)	0.017

---

### Options

---

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

---

### Results

---

Normal Depth	3.3 in
Elevation Range	9.3 to 10.0 ft
Flow Area	1.5 ft <sup>2</sup>
Wetted Perimeter	12.4 ft
Hydraulic Radius	1.4 in
Top Width	12.15 ft
Normal Depth	3.3 in
Critical Depth	3.0 in
Critical Slope	0.008 ft/ft
Velocity	1.55 ft/s
Velocity Head	0.04 ft
Specific Energy	0.31 ft
Froude Number	0.781
Flow Type	Subcritical

---

### GVF Input Data

---

## **Worksheet for 100yr Spread Calculation - S=0.50%**

---

### GVF Input Data

---

Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0

---

---

### GVF Output Data

---

Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	0.00 ft/s
Upstream Velocity	0.00 ft/s
Normal Depth	3.3 in
Critical Depth	3.0 in
Channel Slope	0.005 ft/ft
Critical Slope	0.008 ft/ft

---

## Worksheet for 100yr Storm Inlet 1&2 - On Grade

Project Description	
Solve For	Efficiency
Input Data	
Discharge	2.32 cfs
Slope	0.005 ft/ft
Gutter Width	2.50 ft
Gutter Cross Slope	0.042 ft/ft
Road Cross Slope	0.020 ft/ft
Roughness Coefficient	0.013
Local Depression	2.8 in
Local Depression Width	90.0 in
Grate Width	2.08 ft
Grate Length	3.3 ft
Grate Type	P-50 mm (P-1 -7/8")
Clogging	50.0 %
Curb Opening Length	6.0 ft
Options	
Calculation Option	Use Both
Grate Flow Option	Exclude None
Results	
Efficiency	81.89 %
Intercepted Flow	1.90 cfs
Bypass Flow	0.42 cfs
Spread	9.9 ft
Depth	3.0 in
Flow Area	1.0 ft <sup>2</sup>
Gutter Depression	0.7 in
Total Depression	3.4 in
Velocity	2.22 ft/s
Splash Over Velocity	7.39 ft/s
Frontal Flow Factor	1.000
Side Flow Factor	0.093
Grate Flow Ratio	0.523
Equivalent Cross Slope	0.043 ft/ft
Active Grate Length	1.7 ft
Length Factor	0.277
Total Interception Length	15.6 ft

## Worksheet for 100yr Storm Inlet 3 - Sag

Project Description	
Solve For	Spread
Input Data	
Discharge	0.85 cfs
Gutter Width	2.50 ft
Gutter Cross Slope	0.042 ft/ft
Road Cross Slope	0.020 ft/ft
Local Depression	2.8 in
Local Depression Width	174.0 in
Grate Width	2.08 ft
Grate Length	3.3 ft
Grate Type	P-50 mm (P-1 -7/8")
Clogging	50.0 %
Curb Opening Length	11.6 ft
Opening Height	0.5 ft
Curb Throat Type	Horizontal
Throat Incline Angle	90.00 degrees
Options	
Calculation Option	Use Both
Results	
Spread	3.6 ft
Depth	-0.3 in
Gutter Depression	0.7 in
Total Depression	3.4 in
Open Grate Area	3.1 ft <sup>2</sup>
Active Grate Weir Length	5.4 ft

**Project:** Shari Vista Road

**Location:** Albuquerque, NM

**Date:** 10/19/2020

**Scenario:** Proposed 100 year Design Storm - StormCAD Results

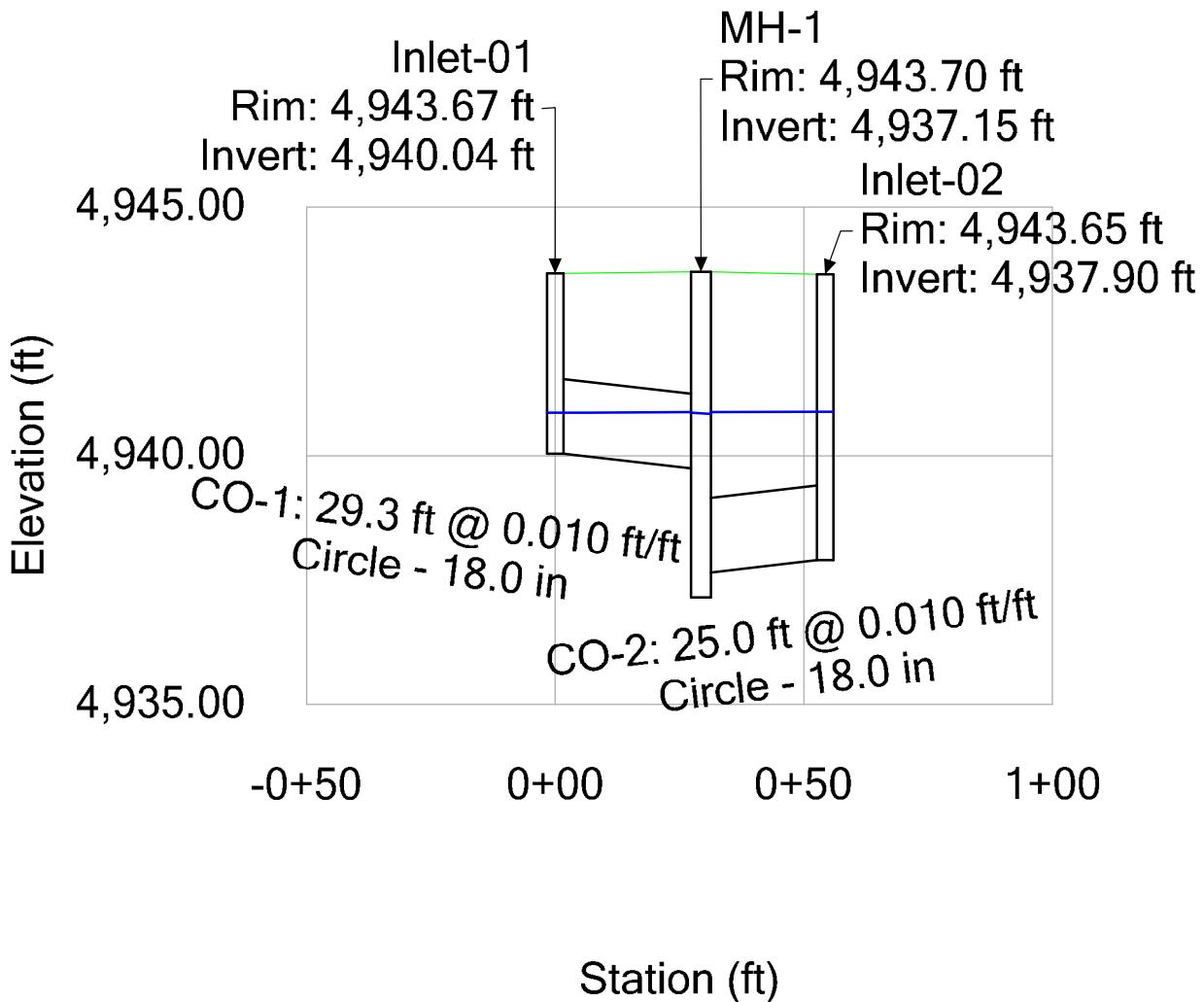
Label	Start Node	Stop Node	Invert (Start) (ft)	Invert (Stop) (ft)	Length (ft)	Slope (ft/ft)	Diameter (Inches)	# of Barrels	Manning's n	Velocity (ft/sec)	Flow (cfs)	Full Flow Capacity (cfs)	Full Flow Capacity (%)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)
CO-1	Inlet-01	MH-1	4940.04	4939.75	29.3	0.010	18	1	0.013	4.49	1.90	10.45	18.2	4943.67	4943.70	4940.87	4940.88	4940.92	4940.90
CO-2	Inlet-02	MH-1	4937.90	4937.65	25.0	0.010	18	1	0.013	1.08	1.90	10.50	18.1	4943.65	4943.70	4940.89	4940.88	4940.91	4940.90
CO-3	Inlet-03	MH-1	4939.89	4939.75	13.7	0.010	18	1	0.013	3.60	0.85	10.62	8.0	4943.63	4943.70	4940.87	4940.87	4940.87	4940.87
CO-4	MH-1	O-1	4937.15	4937.09	5.8	0.010	24	1	0.013	1.48	4.65	23.01	20.2	4943.70	4944.00	4940.84	4940.84	4940.88	4940.87

Label	Downstream Conduit	Ground Elevation (ft)	Invert Elevation (ft)	Inlet Location	Headloss Method	HEC-22 Benching Method	Headloss (ft)	Captured Flow (cfs)	Capture Efficiency (%)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)
Inlet-01	CO-1	4943.67	4940.04	On Grade	HEC-22 Energy (Second Edition)	Depressed	0	1.90	100	4,940.87	4,940.87	4,940.92	4,940.92
Inlet-02	CO-2	4943.65	4937.90	On Grade	HEC-22 Energy (Second Edition)	Depressed	0	1.90	100	4,940.89	4,940.89	4,940.91	4,940.91
Inlet-03	CO-3	4943.63	4939.89	In Sag	HEC-22 Energy (Second Edition)	Depressed	0	0.85	100	4,940.87	4,940.87	4,940.87	4,940.87

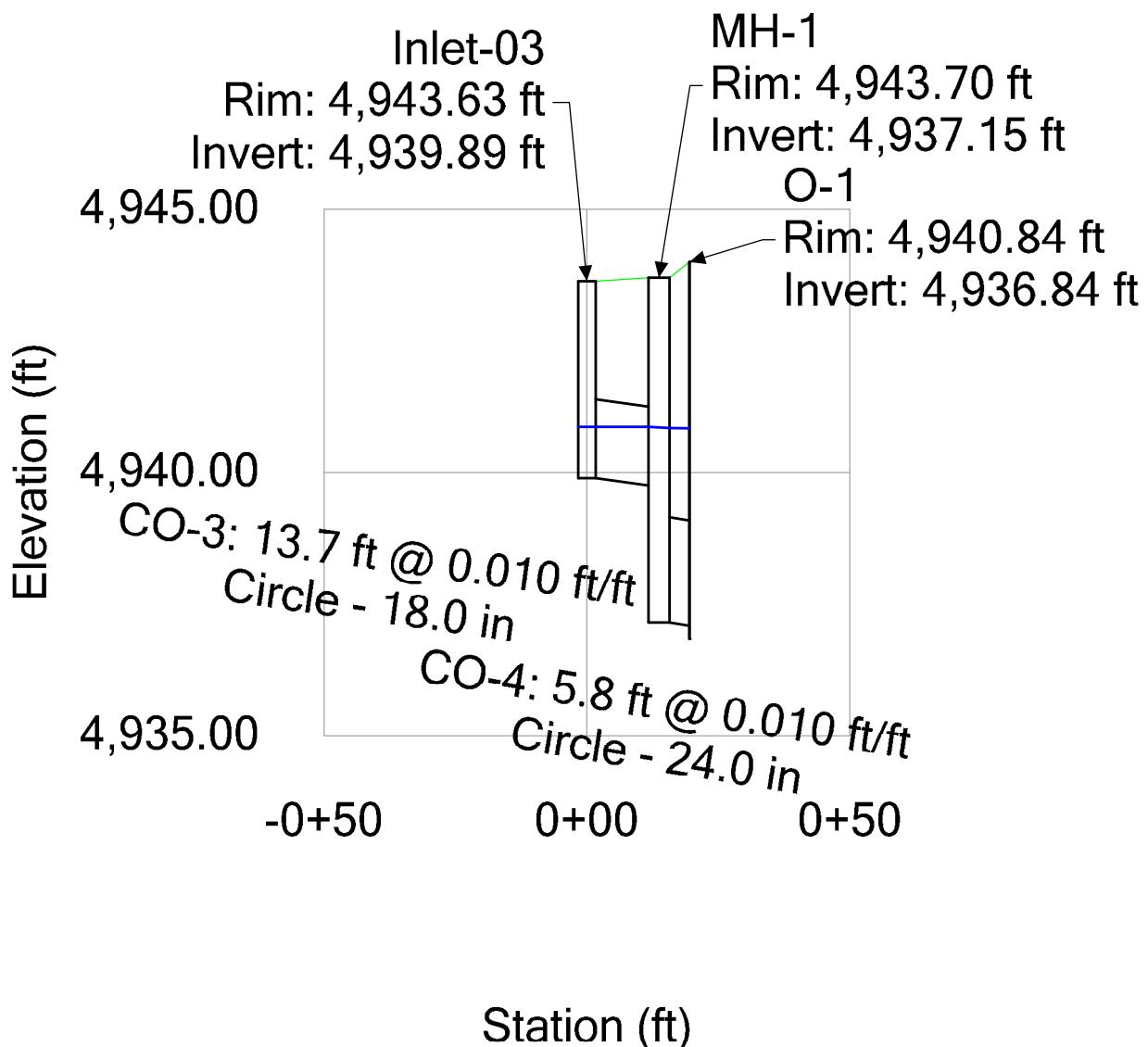
Label	Downstream Conduit	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Depth (In) (ft)	Depth (Out) (ft)	Flow (Total Out) (cfs)	Headloss Method	HEC-22 Benching Method	Headloss (ft)	Velocity (ft/sec)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Energy Grade Line (In) (ft)	Energy Grade Line (Out) (ft)
MH-1	CO-4	4943.70	4937.15	0.76	0.76	4.65	HEC-22 Energy (Second Edition)	Depressed	0.02	1.48	4940.87	4940.84	4940.87	4940.88

Label	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	User Defined Tailwater (ft)	Hydraulic Grade (ft)	Total Flow (cfs)	Notes
O-1	4944.00	4936.84	User Defined Tailwater	4940.84	4940.84	4.65	Underground Storage Chamber

**Profile Report**  
**Engineering Profile - Inlet 1 and Inlet 2 Lateral (ShariVista\_100yr.stsw)**



**Profile Report**  
**Engineering Profile - Inlet 3 to Chamber (ShariVista\_100yr.stsw)**





# CULTEC Stormwater Design Calculator

Date:	October 06, 2020
Project Information:	
SHARI VISTA ROAD	
ALBUQUERQUE, NM	

Project Number:	P.W.C.O XXX
Calculations Performed By:	
TATE TOLEDO, P.E.	
TY LIN INTERNATIONAL	
CHECKED BY: HOWARD CAKE, P.E.	

## RECHARGER 902HD

Recharger 902HD Chamber Specifications		
Height	48.0	inches
Width	78.0	inches
Length	4.10	feet
Installed Length	3.67	feet
Bare Chamber Volume	63.47	cu. feet
Installed Chamber Volume	99.22	cu. feet



Breakdown of Storage Provided by Recharger 902HD Stormwater System	
Within Chambers	3,623.31 cu. feet
Within Feed Connectors	- cu. feet
Within Stone	2,695.32 cu. feet
<b>Total Storage Provided</b>	<b>6,318.6 cu. feet</b>
Total Storage Required	6285.00 cu. feet

## Materials List

Recharger 902HD		
<b>Total Number of Chambers Required</b>	57	pieces
Separator Row Chambers	57	pieces
Chamber Units	57	pieces
End Caps	2	pieces
HVLV FC-48 Feed Connectors	0	pieces
CULTEC No. 410 Non-Woven Geotextile	853	sq. yards
CULTEC No. 4800 Woven Geotextile	238	feet
Stone	250	cu. yards

Separator Row Qty Included in Total

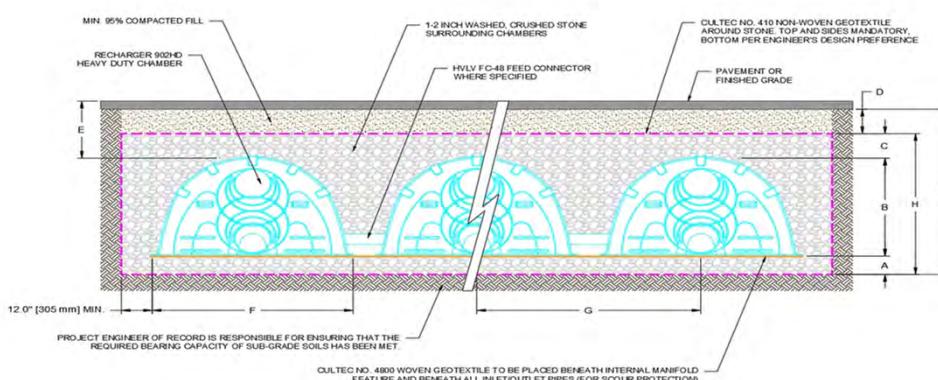
Based on 2 Internal Manifolds

## Bed Detail



Bed Layout Information		
Number of Rows Wide	1	pieces
Number of Chambers Long	57	pieces
Chamber Row Width	6.50	feet
Chamber Row Length	210.00	feet
Bed Width	8.50	feet
Bed Length	212.00	feet
Bed Area Required	1802.02	sq. feet
Length of Separator Row	210.00	feet

Bed detail for reference only. Not project specific. Not to scale.



Conceptual graphic only. Not job specific.

Cross Section Table Reference			
<b>A</b>	Depth of Stone Base	9.0	inches
<b>B</b>	Chamber Height	48.0	inches
<b>C</b>	Depth of Stone Above Units	12.0	inches
<b>D</b>	Depth of 95% Compacted Fill	12.0	inches
<b>E</b>	Max. Depth Allowed Above the Chamber	8.33	feet
<b>F</b>	Chamber Width	78.0	inches
<b>G</b>	Center to Center Spacing	7.25	feet
<b>H</b>	Effective Depth	5.75	feet
<b>I</b>	Bed Depth	6.75	feet



## CULTEC Stage-Storage Calculations

Date:	October 6, 2020
<b>Project Information:</b>	
SHARI VISTA ROAD	
ALBUQUERQUE, NM	

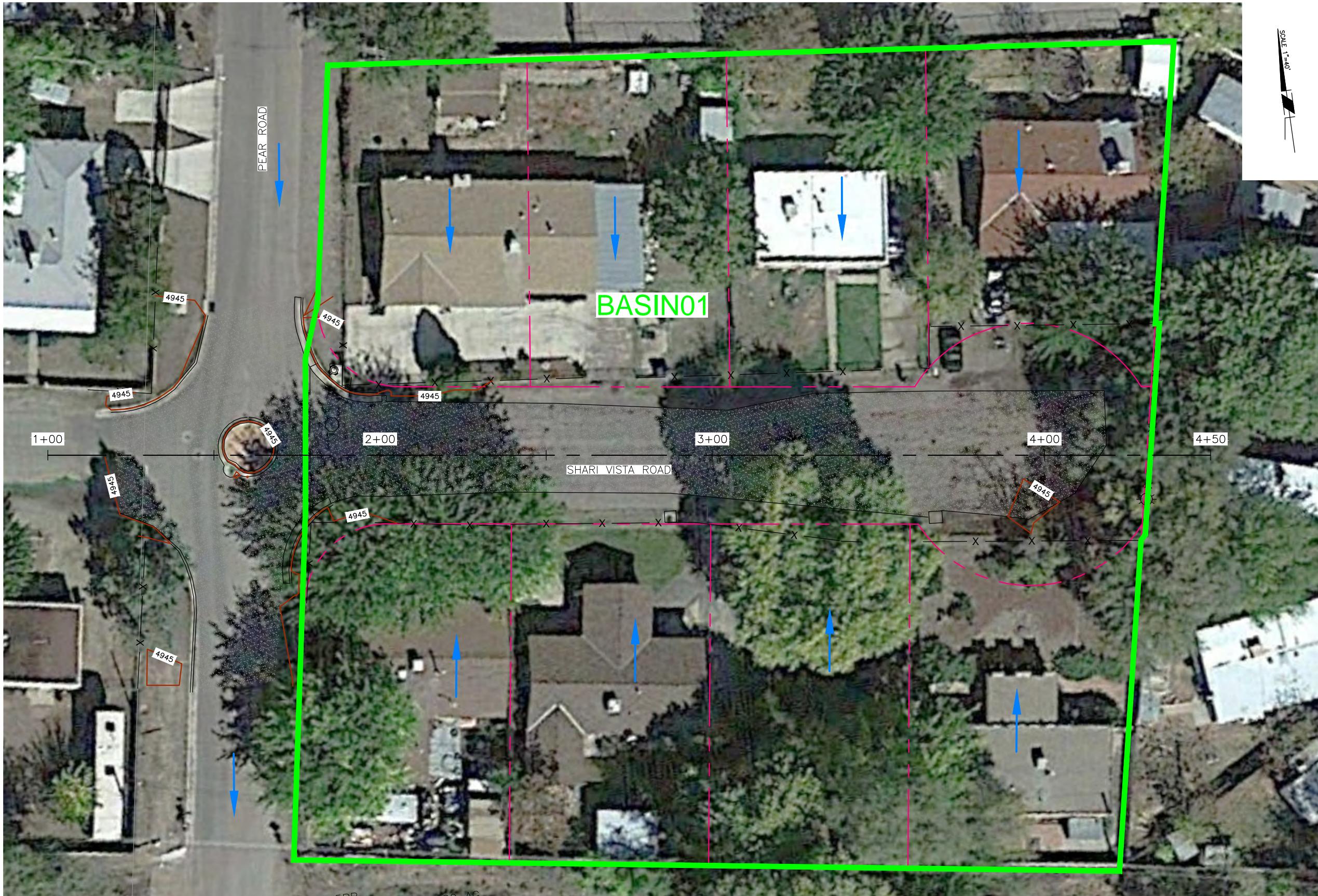
Project Number:
P.W.C.O XXX

Chamber Model - **Recharger 902HD**  
Number of Rows- 1 units  
Total Number of Chambers - 57 units  
HVLV FC-48 Feed Connectors- 0 units  
Stone Void - 40 %  
Stone Base - 9 inches  
Stone Above Units - 12 inches  
Area - 1802.02 ft2  
Base of Stone Elevation - 4936.09

Recharger 902HD Incremental Storage Volumes													
Height of System		Chamber Volume		HVLV Feed Connector Volume		Stone Volume		Cumulative Storage Volume		Total Cumulative Storage Volume		Elevation	
in	mm	ft³	m³	ft³	m³	ft³	m³	ft³	m³	ft³	m³	ft	m
69.0	1753	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	6318.52	178.92	4941.84	4937.84
68.0	1727	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	6258.46	177.22	4941.76	4937.82
67.0	1702	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	6198.39	175.52	4941.67	4937.79
66.0	1676	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	6138.32	173.82	4941.59	4937.77
65.0	1651	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	6078.25	172.12	4941.51	4937.74
64.0	1626	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	6018.19	170.42	4941.42	4937.72
63.0	1600	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	5958.12	168.71	4941.34	4937.69
62.0	1575	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	5898.05	167.01	4941.26	4937.66
61.0	1549	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	5837.98	165.31	4941.17	4937.64
60.0	1524	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	5777.92	163.61	4941.09	4937.61
59.0	1499	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	5717.85	161.91	4941.01	4937.59
58.0	1473	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	5657.78	160.21	4940.92	4937.56
57.0	1448	4.2	0.1	0.0	0.0	58.4	1.7	62.598	1.8	5597.72	158.51	4940.84	4937.54
56.0	1422	10.5	0.3	0.0	0.0	55.9	1.6	66.372	1.9	5535.12	156.74	4940.76	4937.51
55.0	1397	14.7	0.4	0.0	0.0	54.2	1.5	68.880	2.0	5468.75	154.86	4940.67	4937.49
54.0	1372	25.2	0.7	0.0	0.0	50.0	1.4	75.162	2.1	5399.87	152.91	4940.59	4937.46
53.0	1346	33.5	0.9	0.0	0.0	46.7	1.3	80.189	2.3	5324.70	150.78	4940.51	4937.44
52.0	1321	41.9	1.2	0.0	0.0	43.3	1.2	85.194	2.4	5244.51	148.51	4940.42	4937.41
51.0	1295	46.1	1.3	0.0	0.0	41.6	1.2	87.713	2.5	5159.32	146.10	4940.34	4937.39
50.0	1270	50.3	1.4	0.0	0.0	40.0	1.1	90.221	2.6	5071.61	143.61	4940.26	4937.36
49.0	1245	56.5	1.6	0.0	0.0	37.5	1.1	93.983	2.7	4981.39	141.06	4940.17	4937.33
48.0	1219	56.5	1.6	0.0	0.0	37.5	1.1	93.983	2.7	4887.40	138.40	4940.09	4937.31
47.0	1194	60.7	1.7	0.0	0.0	35.8	1.0	96.491	2.7	4793.42	135.73	4940.01	4937.28
46.0	1168	62.8	1.8	0.0	0.0	34.9	1.0	97.757	2.8	4696.93	133.00	4939.92	4937.26
45.0	1143	64.9	1.8	0.0	0.0	34.1	1.0	98.999	2.8	4599.17	130.23	4939.84	4937.23
44.0	1118	69.1	2.0	0.0	0.0	32.4	0.9	101.507	2.9	4500.17	127.43	4939.76	4937.21
43.0	1092	71.2	2.0	0.0	0.0	31.6	0.9	102.773	2.9	4398.66	124.56	4939.67	4937.18
42.0	1067	73.2	2.1	0.0	0.0	30.8	0.9	104.015	2.9	4295.89	121.65	4939.59	4937.16
41.0	1041	73.2	2.1	0.0	0.0	30.8	0.9	104.015	2.9	4191.88	118.70	4939.51	4937.13
40.0	1016	75.4	2.1	0.0	0.0	29.9	0.8	105.281	3.0	4087.86	115.76	4939.42	4937.11
39.0	991	77.4	2.2	0.0	0.0	29.1	0.8	106.523	3.0	3982.58	112.77	4939.34	4937.08
38.0	965	79.6	2.3	0.0	0.0	28.2	0.8	107.801	3.1	3876.06	109.76	4939.26	4937.06
37.0	940	81.6	2.3	0.0	0.0	27.4	0.8	109.031	3.1	3768.25	106.70	4939.17	4937.03
36.0	914	81.6	2.3	0.0	0.0	27.4	0.8	109.043	3.1	3659.22	103.62	4939.09	4937.00
35.0	889	83.7	2.4	0.0	0.0	26.6	0.8	110.297	3.1	3550.18	100.53	4939.01	4936.98
34.0	864	83.7	2.4	0.0	0.0	26.6	0.8	110.285	3.1	3439.88	97.41	4938.92	4936.95
33.0	838	85.8	2.4	0.0	0.0	25.7	0.7	111.551	3.2	3329.60	94.28	4938.84	4936.93
32.0	813	85.8	2.4	0.0	0.0	25.7	0.7	111.551	3.2	3218.05	91.12	4938.76	4936.90
31.0	787	85.8	2.4	0.0	0.0	25.7	0.7	111.563	3.2	3106.50	87.97	4938.67	4936.88
30.0	762	87.9	2.5	0.0	0.0	24.9	0.7	112.805	3.2	2994.93	84.81	4938.59	4936.85
29.0	737	87.9	2.5	0.0	0.0	24.9	0.7	112.805	3.2	2882.13	81.61	4938.51	4936.83
28.0	711	87.9	2.5	0.0	0.0	24.9	0.7	112.805	3.2	2769.32	78.42	4938.42	4936.80
27.0	686	90.0	2.5	0.0	0.0	24.1	0.7	114.059	3.2	2656.52	75.22	4938.34	4936.78
26.0	660	90.0	2.5	0.0	0.0	24.1	0.7	114.059	3.2	2542.46	71.99	4938.26	4936.75
25.0	635	92.1	2.6	0.0	0.0	23.2	0.7	115.325	3.3	2428.40	68.76	4938.17	4936.73
24.0	610	92.1	2.6	0.0	0.0	23.2	0.7	115.313	3.3	2313.08	65.50	4938.09	4936.70
23.0	584	94.2	2.7	0.0	0.0	22.4	0.6	116.567	3.3	2197.76	62.23	4938.01	4936.67
22.0	559	94.2	2.7	0.0	0.0	22.4	0.6	116.567	3.3	2081.20	58.93	4937.92	4936.65
21.0	533	94.2	2.7	0.0	0.0	22.4	0.6	116.579	3.3	1964.63	55.63	4937.84	4936.62
20.0	508	94.2	2.7	0.0	0.0	22.4	0.6	116.567	3.3	1848.05	52.33	4937.76	4936.60
19.0	483	96.3	2.7	0.0	0.0	21.6	0.6	117.833	3.3	1731.48	49.03	4937.67	4936.57
18.0	457	96.3	2.7	0.0	0.0	21.6	0.6	117.833	3.3	1613.65	45.69	4937.59	4936.55
17.0	432	96.3	2.7	0.0	0.0	21.6	0.6	117.833	3.3	1495.82	42.36	4937.51	4936.52
16.0	406	96.3	2.7	0.0	0.0	21.6	0.6	117.833	3.3	1377.99	39.02	4937.42	4936.50
15.0	381	98.3	2.8	0.0	0.0	20.7	0.6	119.075	3.4	1260.15	35.68	4937.34	4936.47
14.0	356	98.4	2.8	0.0	0.0	20.7	0.6	119.087	3.4	1141.08	32.31	4937.26	4936.45
13.0	330	100.5	2.8	0.0	0.0	19.9	0.6	120.341	3.4	1021.99	28.94	4937.17	4936.42
12.0	305	100.5	2.8	0.0	0.0	19.9	0.6	120.352	3.4	901.65	25.53	4937.09	4936.39
11.0	279	100.5	2.8	0.0	0.0	19.9	0.6	120.341	3.4	781.30	22.12	4937.01	4936.37
10.0	254	100.5	2.8	0.0	0.0	19.9	0.6	120.352	3.4	660.96	18.72	4936.92	4936.34
9.0	229	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	540.61	15.31	4936.84	4936.32
8.0	203	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	480.54	13.61	4936.76	4936.29
7.0	178	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	420.47	11.91	4936.67	4936.27
6.0	152	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	360.40	10.21	4936.59	4936.24
5.0	127	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	300.34	8.50	4936.51	4936.22
4.0	102	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	240.27	6.80	4936.42	4936.19
3.0	76	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	180.20	5.10	4936.34	4936.17
2.0	51	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	120.13	3.40	4936.26	4936.14
1.0	25	0.0	0.0	0.0	0.0	60.1	1.7	60.067	1.7	60.07	1.70	4936.17	4936.12
0.0	0	0.0	0.0	0.0	0.0	0.0	0.0	0.000	0.0	0.00	0.00	4936.09	4936.09

## **APPENDIX C**

**Drainage Exhibits**



#### LEGEND

- SUBBASIN
- BASIN01
- FLOW ARROW
- EXISTING CONTOURS
- EXISTING STORM DRAIN

Basin ID	BASIN01	
Contributing Area	61,720.8 sf	0.30 ac
Q <sub>P2</sub> Discharge	1.1 cfs	
Q <sub>P10</sub> Discharge	2.5 cfs	
Q <sub>P100</sub> Discharge	4.6 cfs	



**SHARI VISTA ROAD**  
PEAR RD. TO END OF SHARI VISTA RD.  
P.W.C.O. 2020-XXXX

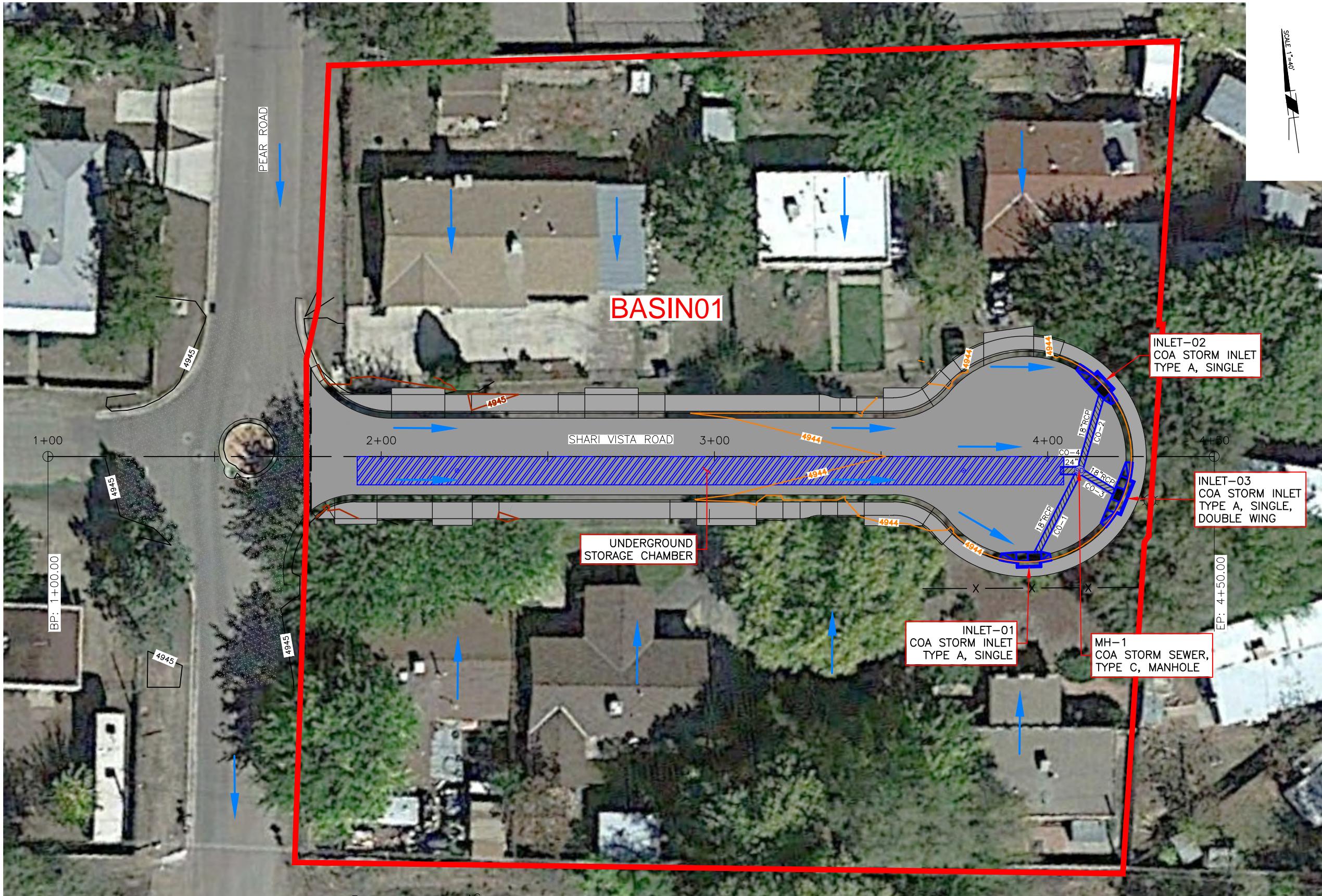
#### EXHIBIT 1

#### ONSITE DRAINAGE MAP

#### EXISTING CONDITIONS

0 15' 30' 60'  
SCALE: 1" = 30'

**TY-LIN INTERNATIONAL**  
engineers | planners | scientists



#### LEGEND

- SUBBASIN
- BASIN01 SUBBASIN ID
- FLOW ARROW
- EXISTING CONTOURS
- PROPOSED CONTOURS
- PROPOSED STORM DRAIN INFRASTRUCTURE

Basin ID	BASIN01	
Contributing Area	61,720.8 sf	0.30 ac
Q <sub>P2</sub> Discharge	1.1 cfs	
Q <sub>P10</sub> Discharge	2.5 cfs	
Q <sub>P100</sub> Discharge	4.6 cfs	



SHARI VISTA ROAD  
PEAR RD. TO END OF SHARI VISTA RD.  
P.W.C.O. 2020-XXXX

#### EXHIBIT 2

#### ONSITE DRAINAGE MAP

#### PROPOSED CONDITIONS

0 15' 30' 60'  
SCALE: 1" = 30'

**TY-LIN INTERNATIONAL**  
engineers | planners | scientists