

I certify that I have personally inspected the Tract 93 site and the surrounding terrain. The representation of the land and the contours are as presented on these drawings and the accompanying text as of October 1997.

Marvin R Kortum OCT 20 1997
Marvin R Kortum Date

Topographic survey by Southwest Survey Company, Inc. Boundary data shown is from recorded warrantee deed, filed in Bernalillo County, New Mexico, D92A PG 547. Apparent property corners are for orientation only.

NOTES

- All berms and earthwork supporting structures must be compacted to 95% of maximum dry density (Modified Proctor Test).
- Elevations of building pads are based on slab on grade.
- Quantitative earthwork estimates should be based on more detailed topographic cross sections of the work area.
- Add to the height of the existing berm along the west property line.
- Construct swale through the east gate to permit outflow from the interior courtyard to the pond area.
- Construct earthen pond to dimensions noted. Sides of the pond are to be planted with vegetation to reduce erosion.
- Install roof gutter to collect and direct roof runoff to the east pond. Gutter shall be 6 inches or larger, and shall be set at a 0.5% slope (1/8 inch per foot) or larger. The gutter shall direct the flow to a rundown into the pond, or empty directly into the center of the pond.



LEGAL DESCRIPTION: Tract 93, M. R. G. C. D. Map # 41, Section 30 T 10 N, R 3 E, Bernalillo County, New Mexico.

L-13

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HYDROLOGY SECTION

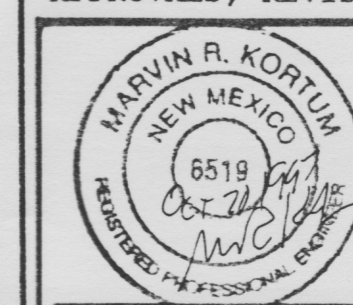
TRACT 94B1, MRGCD MAP #41
(1-013-056-254-288-20404)
(S 53°30'00" E)
(76.00')

FND #4 REBAR

LEGEND

- ⊙ = POWER POLE
- ⊙ = SEWER MANHOLE
- ⊙ = WATER METER
- CL = CENTERLINE
- TP = TOP OF PAVEMENT (EDGE)
- ⊙ = PROPOSED SURFACE ELEVATION
- 4-4- = PROPOSED CONTOUR

Preliminary APPROVALS, REVISIONS Marvin R Kortum October 20, 1997
BY DATE



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GRADING AND DRAINAGE
TRACT 93, MRGCD MAP NO. 41

PROJECT NO. MAP NO. SHEET OF

L-13 1 3

EXISTING fp Limit

BASIS OF ELEVATIONS FOR THIS SURVEY IS ACS CONTROL STATION 10-L13 THE PUBLISHED ELEVATION IS 4944.553, AND IS LOCATED IN THE MEDIAN AT THE INTERSECTION OF BRIDGE BOULEVARD SW AND ISLETA BOULEVARD SW.

SET TEMPORARY BENCH MARK
40d NAIL IN POWER POLE F17C
ELEVATION = 4945.175

TRACT 92A1, MRGCD MAP #41
(1-013-056-248-255-31013)

BLVD. SW.

ISLETA

TRACT 94B2, MRGCD MAP #41
(1-013-056-233-285-20401)
(S 78°28'00" E)

STORAGE BUILDING
FF = 4944.25

RESIDENCE/OFFICE
FF = 4944.86

STORAGE BUILDING
FF = 4944.28

FND 1" IRON PIPE

OCTOBER 20, 1997
RUNOFF FOR TRACT 93, M. R. G. C. D MAP 41
TOTAL AREA IS 0.6606 ACRES.

TABLE I A
Runoff Estimate: For on-site Basin A of 0.6606 acres, for the complete site, with gravel surface between the buildings

Runoff Factors Zone 1		CURRENT USE				PROPOSED USE			
		Area	Percent	Peak	Total	Area	Percent	Peak	Total
Land use	Peak	Total		Runoff	Runoff			Runoff	Runoff
	CFS/acre	inches	SF	CFS	CF	SF		CFS	CF
1 A	1.29	0.44	28775.00	1.000	0.9	1055.1	0.00	0.000	0.0
2 B	2.03	0.67	0.00	0.000	0.0	0.0	0.00	0.000	0.0
3 C	2.87	0.99	0.00	0.000	0.0	0.0	21375.00	0.743	1.4
4 D	4.37	1.97	0.00	0.000	0.0	0.0	7400.00	0.257	0.7
5	1.47								
TOTALS			28775.00	1.000	0.9	1055.1	28775.00	1.000	2.2
			0.6606 acre				0.6606 acre		3884.8

TABLE I A-1
Runoff Estimate: For on-site Basin A-1 of 0.5952 acres with gravel surface between the buildings
Basin A-1 consists of buildings, interior courtyard and east yard.

Runoff Factors Zone 1		CURRENT USE				PROPOSED USE			
		Area	Percent	Peak	Total	Area	Percent	Peak	Total
Land use	Peak	Total		Runoff	Runoff			Runoff	Runoff
	CFS/acre	inches	SF	CFS	CF	SF		CFS	CF
1 A	1.29	0.44	25925.00	1.000	0.8	950.6	0.00	0.000	0.0
2 B	2.03	0.67	0.00	0.000	0.0	0.0	0.00	0.000	0.0
3 C	2.87	0.99	0.00	0.000	0.0	0.0	18525.00	0.715	1.2
4 D	4.37	1.97	0.00	0.000	0.0	0.0	7400.00	0.285	0.7
5	1.47								
TOTALS			25925.00	1.000	0.8	950.6	25925.00	1.000	2.0
			0.5952 acre				0.5952 acre		3649.6

TABLE I A-2
Runoff Estimate: For on-site Basin A of 0.0654 acres with gravel surface between the buildings
Basin A-2 is the strip of land north of the north building

Runoff Factors Zone 1		CURRENT USE				PROPOSED USE			
		Area	Percent	Peak	Total	Area	Percent	Peak	Total
Land use	Peak	Total		Runoff	Runoff			Runoff	Runoff
	CFS/acre	inches	SF	CFS	CF	SF		CFS	CF
1 A	1.29	0.44	2850.00	1.000	0.1	104.5	0.00	0.000	0.0
2 B	2.03	0.67	0.00	0.000	0.0	0.0	0.00	0.000	0.0
3 C	2.87	0.99	0.00	0.000	0.0	0.0	2850.00	1.000	0.2
4 D	4.37	1.97	0.00	0.000	0.0	0.0	0.00	0.000	0.0
5	1.47								
TOTALS			2850.00	1.000	0.1	104.5	2850.00	1.000	0.2
			0.0654 acre				0.0654 acre		235.1

TABLE B
Runoff Estimate: For off-site Basin B of 0.0976 acres, (1/2 off Isleta Blvd. along west of Tract 93)

Runoff Factors Zone 1		CURRENT USE				PROPOSED USE			
		Area	Percent	Peak	Total	Area	Percent	Peak	Total
Land use	Peak	Total		Runoff	Runoff			Runoff	Runoff
	CFS/acre	inches	SF	CFS	CF	SF		CFS	CF
1 A	1.29	0.44	4250.00	1.000	0.1	155.8	0.00	0.000	0.0
2 B	2.03	0.67	0.00	0.000	0.0	0.0	0.00	0.000	0.0
3 C	2.87	0.99	0.00	0.000	0.0	0.0	850.00	0.200	0.1
4 D	4.37	1.97	0.00	0.000	0.0	0.0	3400.00	0.800	0.3
5	1.47								
TOTALS			4250.00	1.000	0.1	155.8	4250.00	1.000	0.4
			0.0976 acre				0.0976 acre		1044.8

TABLE C
Runoff Estimate: For roof runoff.

Runoff Factors Zone 1		NORTH BUILDING				SOUTH BUILDING			
		Area	Percent	Peak	Total	Area	Percent	Peak	Total
Land use	Peak	Total		Runoff	Runoff			Runoff	Runoff
	CFS/acre	inches	SF	CFS	CF	SF		CFS	CF
1 A	1.29	0.44	0.00	0.000	0.0	0.0	0.00	0.000	0.0
2 B	2.03	0.67	0.00	0.000	0.0	0.0	0.00	0.000	0.0
3 C	2.87	0.99	0.00	0.000	0.0	0.0	0.00	0.000	0.0
4 D	4.37	1.97	2826.00	1.000	0.3	463.9	2685.60	1.000	0.3
5	1.47								
TOTALS			2826.00	1.000	0.3	810.1	2685.60	1.000	0.3
			0.0649 acre				0.0617 acre		769.9

NOTES:

- Runoff factors from Section 22.2, DPM, January, 1993
- Land use descriptions: A. Uncompacted soil
B. Landscaped
C. Compacted soil
D. Impervious areas
- Peak runoff = Area (acres) x factor (CFS/acre) = CFS
- Total runoff = Area (SF) x factor (inches) / 12 (inches / foot) = CF
- Peak and total runoff is based on 6 hour, 100 year frequency storm
- Line 5 estimates additional contribution for 10 day storm, equation a=9, Section 22.2, DPM
[V10 day=V360+ADx(P10 day-P360)/12]; P10 day=3.67'', P360=2.20'' so P10-P360=1.47

The numbers shown on the tables are recorded to the significant number shown primarily to aid in tracking computations. Results are reasonably valid only to the first number, ie. 5643.7 represents a result between about 5000 and 6000.

OCTOBER 20, 1997
TABLE D
POND CONFIGURATION, TRACT 93

FOR RECTANGULAR SHAPED PONDS
Volume of ponds: V=volume of pyramid for end sections plus volume of prism for mid section.
(d/3)(Area of top surface + Area of bottom + square root of At x Ab)+cross section area of prism x length
Side slope: feet horizontal to feet vertical

depth		side slope		Top dimensions		Bottom dimensions		Capacity	Area
				length	width	length	width		
d (ft)		(ft/ft)		lt (ft)	wt (ft)	lb (ft)	wb (ft)	V (CF)	SF
1	3	54	8	48	2	258.0	432		
1.5	3	100	10	91	1	798.0	1000		

PONDS FOR TRACT 93, BASIN A-2, DIRECT PRECIPITATION ONLY

PONDS FOR TRACT 93, BASIN A-2, INCLUDING SOME ROOF RUNOFF FROM THE NORTH BUILDING

FOR DIRECT PRECIPITATION ONLY
REQUIRED 100 YEAR, 6 HOUR STORM 235.1 CF
REQUIRED 100 YEAR, 10 DAY STORM 235.1 CF
WITH 10% SILTING FACTOR
REQUIRED 100 YEAR, 6 HOUR STORM 258.6 CF
REQUIRED 100 YEAR, 10 DAY STORM 258.6 CF

FOR TRIANGULAR SHAPED PONDS
Volume of ponds: V=volume of pyramid
(d/3)(Area of top surface + Area of bottom + square root of At x Ab)+cross section area of prism x length
Side slope: feet horizontal to feet vertical

depth		side slope		Top dimensions		area	Bottom dimensions		Capacity	Area
				length	width		length	width		
d (ft)		(ft/ft)		lt (ft)	wt (ft)	SF	lb (ft)	wb (ft)	V (CF)	SF
1	3	83	38	1577	68	31	1054	950.7	1577	
2.5	60	48	1440	5	4	10	3051.8	1440		
TOTAL									4002.5	
REQUIRED 100 YEAR, 6 HOUR STORM						2743.1 CF				
REQUIRED 100 YEAR, 10 DAY STORM						3649.6 CF				
WITH 8% SILTING FACTOR						2962.5 CF				
REQUIRED 100 YEAR, 6 HOUR STORM						3941.6 CF				
REQUIRED 100 YEAR, 10 DAY STORM							4002.5 capacity is more than need			3941.6

TABLE E
ROOF GUTTER CAPACITIES
TRACT 93
OCTOBER 20, 1997

Ditch capacities of portland cement concrete channel.
Q=Area x Velocity; Velocity=1.486/n x (Rh)^{2/3} x (s)^{1/3}

Mannings	n	Ditch Slope (A)	Side slope (B)	Bottom width (C)	Depth (D)	Top width (E)	Area (F)	Wetted Perimeter (G)	Hydraulic Radius (H)	Velocity (I) FPS	Capacity (J) CFS	Froude # (K)	Sequent depth (L) Ft	Sloped (M) Ft	Trapezoid (N) Ft
1	0.011	5.000	0	0.330	0.20	0.3	0.1	0.730	0.090	1.924	0.127	0.76	0.14	0.16	0.12
2	0.011	10.000	0	0.330	0.20	0.3	0.1	0.730	0.090	2.721	0.180	1.07	0.22	0.26	0.19
3	0.011	5.000	0	0.500	0.20	0.5	0.1	0.900	0.111	2.208	0.221	0.87	0.17	0.20	0.14
4	0.011	10.000	0	0.500	0.20	0.5	0.1	0.900	0.111	3.122	0.312	1.23	0.26	0.31	0.22
5	0.011	5.000	0	0.500	0.33	0.5	0.2	1.160	0.142	2.603	0.429	0.80	0.24	0.29	0.21
6	0.011	10.000	0	0.500	0.33	0.5	0.2	1.160	0.142	3.681	0.607	1.13	0.39	0.46	0.33

REQUIRED Q100 = 0.3 CFS

- (A) Ft(vertical)/1000 Ft(horizontal)
(B) Ft(horizontal)/1 Ft(vertical)
(C) Froude No. (Fn)=velocity/(g x area/top width)^{0.5}
(D) Sequent depth for rectangular level channel, y2=(y1/2)x(((1+8 x Fn²)^{0.5}) -1)
(E) Sequent depth for sloping rectangular channel
y2=((y1/2)/cos slope angle) x (((1+8(((10⁰ x slope angle)²) x Fn²)^{0.5})-1)
(F) Correction factor for trapezoidal channel, figure 3.4
(G) Reference: Richard B French, Open Channel Hydraulics, 1985

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GRADING AND DRAINAGE PLAN
TRACT 93, MRGCD MAP NO. 41
ESTIMATES