CITY OF ALBUQUERQUE

Planning Department Alan Varela, Director



Mayor Timothy M. Keller

December 8, 2023

Christopher Archuleta, P.E. Respec 7770 Jefferson NE, Suite 200 Albuquerque, NM 87109

RE: John Street Pond Feasibility Design Analysis Report Engineer's Stamp Date: 11/09/23 Hydrology File: L14D067

Dear Mr. Archuleta:

Based upon the information provided in your submittal received 11/09/2023, the Analysis Report is preliminary approved.

1. Once a 90% Construction Drawings Set is complete, please submit the final design

(.pdf) is emailed to PLNDRS@cabq.gov along with the Drainage Transportation

Grading Plans and Drainage Report to Hydrology for review and approval. This digital

PO Box 1293 PRIOR TO WORK ORDER APPROVAL:

Information Sheet.

Albuquerque

NM 87103

If you have any questions, please contact me at 924-3995 or <u>rbrissette@cabq.gov</u>.

www.cabq.gov

Renée C. Brissette

Renée C. Brissette, P.E. CFM Senior Engineer, Hydrology Planning Department

Sincerely,



City of Albuquerque

Planning Department Development & Building Services Division

DRAINAGE AND TRANSPORTATION INFORMATION SHEET (DTIS)

Project Title:	Hydrology File #
City Address, UPC, OR Parcel:	
Applicant/Agent:	Contact:
	Phone:
Email:	
Applicant/Owner:	Contact:
	Phone:
Email:	
(Please note that a DFT SITE is one that need	ds Site Plan Approval & ADMIN SITE is one that does not need it.)
TYPE OF DEVELOPMENT: PLAT	(#of lots) RESIDENCE
DFT	SITE ADMIN SITE
RE-SUBMITTAL: YES NO	
DEPARTMENT: TRANSPORTA	TION HYDROLOGY/DRAINAGE
Check all that apply under Both the Type	of Submittal and the Type of Approval Sought:
TYPE OF SUBMITTAL:	TYPE OF APPROVAL SOUGHT:
ENGINEER/ARCHITECT CERTIFICA	TION BUILDING PERMIT APPROVAL
PAD CERTIFICATION	CERTIFICATE OF OCCUPANCY
CONCEPTUAL G&D PLAN	CONCEPTUAL TCL DFT APPROVAL
GRADING & DRAINAGE PLAN	PRELIMINARY PLAT APPROVAL
DRAINAGE REPORT	FINAL PLAT APPROVAL
DRAINAGE MASTER PLAN	SITE PLAN FOR BLDG PERMIT DFT
CLOMR/LOMR	APPROVAL
TRAFFIC CIRCULATION LAYOUT (7	SIA/RELEASE OF FINANCIAL GUARANTEE
ADMINISTRATIVE	FOUNDATION PERMIT APPROVAL
TRAFFIC CIRCULATION LAYOUT F APPROVAL	OR DFT GRADING PERMIT APPROVAL
TRAFFIC IMPACT STUDY (TIS)	SO-19 APPROVAL
STREET LIGHT LAYOUT	PAVING PERMIT APPROVAL
OTHER (SPECIFY)	GRADING PAD CERTIFICATION
omer(billen i)	WORK ORDER APPROVAL
	CLOMR/LOMR
	OTHER (SPECIFY)

DATE SUBMITTED: ____



COMMENT RESPONSE LETTER

- To: City of Albuquerque Hydrology Section (Planning Department)
- From: RESPEC
- Date: November 9, 2023
- RE: John Street Pond Feasibility Design Analysis Report Engineer's Stamp Date: No date Hydrology File: L14D067

COA HYDROLOGY COMMENT RESPONSES

RESPEC's responses are in Blue.

1. Once the Report is ready for approval, please provide an engineer's stamp with a signature and date. Report is stamped, signed, and dated.

2. Please note that the Hydrology Section has yet to review and approve the updated South Broadway Drainage Management Plan (March, 2023. Please note that these DMPs are used by the Hydrology Section to ensure that new developments within the watershed follows any site restrictions to the allowable discharge as outlined in these MDPs. Something else to note is that the City of Albuquerque has a limit of 430 cfs in the San Jose Drain at the City Limit which makes this at capacity currently all the way to the Rio Grande River. South Broadway DMP (2023) has been submitted to hydrology.

3. In 2.1 Existing Conditions, the section just refers to the updated SBDMP without a map. A map showing the existing subbasins similar to Figure 3 (Proposed Subbasin Map) would be helpful. A figure showing existing conditions subbasins in the vicinity to John Street Pond was added to the report.

4. In 2.2 Proposed Conditions, why are all the Curve Number (CN) the same? Hydrology section has found if you are using a soil map within Albuquerque, then the resulting flows are off. As in the DPM, Hydrology Section recommends using the following CNs depending on the land treatment and using a weighted CN.

a. The use of just four Curve Number (CN) values, one for each of the land treatments already described in the DPM: A=76, B=80, C=85 and D=98. This way the hydrologic soil groups don't need to be determined to select the CN and the soil maps do not need to be consulted.

b. For example, John Street Pond Basin 1 has 85% impervious but uses a CN 86. If you use a weighted CN, then you get 0.85*98 + 0.15*85 which gives a CN 96.

7770 JEFFERSON STREET NE SUITE 200 Albuquerque, NM 87109 505.243.2287





c. For example, John Street Pond Basin 2 has 20% impervious but uses a CN 86. If you use a weighted CN, then you get 0.20*98 + 0.80*85 which gives a CN 87.6.

As you can see using the weighted CN gets a more accurate representation of the existing conditions or proposed conditions. RESPEC maintained the same hydrology procedures discussed in the Alameda SWMM Drainage Study (October 2022) report, which is also referenced in the South Broadway DMP (March 2023). The Alameda SWMM Drainage Study discusses in depth the hydrology practices and curve number (CN) selection. Below is a screenshot of verbiage from the Alameda SWMM Drainage Study report for context. The subarea routing method used, from the SWMM hydrology manual, was the "impervious method" which routes the directly connected area (roofs to driveways into the street into the storm systems) over pervious area (grass, compacted parking lots, etc.). Since the area around John Street Pond has similar lot sizes, the CN selected was applied to the pervious area of the subbasin. Since the Hydrologic soils report showed a mixture of groups A-D for the watershed, RESPEC conservatively used CNs in HSG C since the drainage area is developed with compacted pervious soils. Therefore, for these lots around the John Street area, RESPEC used an average CN of lot sizes 1/8, 1/3 and 1/4. RESPEC will provide the Alameda SWMM Drainage Study report.

parameters are orugianin determining runon and volume estimates in the model.

2.2.1 OVERVIEW OF SWMM HYDROLOGY

The hydrologic methods available in PCSWMM provides an effective tool for the analysis of subbasins that occur in valley conditions that are typically depressed and unable to drain out. This is because PCSWMM treats each subbasin or sub-catchment as a polygon for which a volume analysis is performed to generate a runoff hydrograph. The sub-catchment polygon is divided into an impervious portion, representing the directly connected impervious areas and a pervious portion which represents all pervious areas. The two types of areas are then internally routed using a subarea routing method. There are three principal methods for subarea routing which are discussed in detail the general definition of terms below. Initial abstractions for areas that are depressed can then be manipulated to capture effect of depression storage and excess ponding that will occur. There are several key parameters that are required to generate hydrographs.

A general definition of terms is provided below:

- » Sub-catchment: The equivalent term for a subbasin.
- » Area: Subbasin area based measured from ArcGIS Pro.
- Hydrologic Area Width: The estimated width for sheet flow. This is a difficult parameter to estimate as the width for sheet flow in any subbasin is subjective. Alternatively, PCSWMM recommends computing the longest flow path, as this is a parameter easily measured based on topographic data. The overland flow width can then be estimated by taking the ratio of the basin area to the longest flow path. PCSWMM recommends that this parameter is one that should be calibrated as the width and area for the sub-catchment greatly affects the peak. For this analysis, RESPEC measured the longest flow path for each sub-catchment. PCSWMM has a built-in function that lets the user determine if the flow path or the width will be used as the direct input. The Alameda Drain model was set to select the longest flow path as the direct input which allowed the model to compute the width. Flow path lengths were adjusted for some sub-catchments to calibrate the runoff results.
- Subarea Routing Method: Determines how the computed runoff for a sub-catchment polygon gets routed internally. There are three primary routing methods: pervious, impervious or outlet.
 - The Pervious method assumes that some percentage of the runoff from the impervious
 area is directed through the pervious area in the sub-catchment. This method requires
 a composite curve number to be defined for the entire sub-catchment.
 - The Impervious method implies that some portion of the pervious area is routed over the directly connected impervious area. This method requires the directly connected impervious area be defined as a percentage whereas a curve number is assigned to pervious area.
 - The outlet method does not do internal routings. In this method, runoff from both the impervious area and pervious area are routed directly to the outlet of the subcatchment.

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5. Figure 4, Overview of Storm Drain Improvements. It would be very helpful if you include the Q100 at the storm pipe for both the existing and the proposed on the map. (See below) This should be help explain how the whole proposed system will help with the capacity in the existing storm drain by the proposed detention & pump station. These were added to the figure.

6. In 3.2.1 John Street Gravity Pond. For Option 1 & Option 2, the emergency spillway Q100 is shown in the tables but which design is being proposed for the COA Ported Riser Principle Spillway is being used in each option and the Q100 at the discharge is not mentioned either. Option 1 has a 30-inch RCP and Option 2 has a 24-inch RCP but that is all the information is given. These were discussed and revised in the report.

JOHN STREET POND FEASIBILITY Design Analysis Report

REPORT RSI-3390



PREPARED BY Christopher Archuleta Shamas Din Hugh Floyd

RESPEC 7770 Jefferson Street NE, Suite 200 Albuquerque, New Mexico 87109

PREPARED FOR One Albuquerque 1 Civic Plaza, #7057 Albuquerque, New Mexico 87109

NOVEMBER 2023

Project Number W0505.23002

City of Albuquerque Planning Department Development Review Services HYDROLOGY SECTION
PRELIMINARY APPROVED DATE: 12/08/23 BY: Renee Brussette HydroTrans # L14D067
THESE PLANS AND/OR REPORT ARE CONCEPTUAL ONLY. MORE INFORMATION MAY BE NEEDED IN THEM AND SUBMITTED TO HYDROLOGY FOR BUILDING PERMIT APPROVAL.





CERTIFICATION

I, Christopher S. Archuleta, do hereby certify that this report was duly prepared by me or under my direction and that I am a duly registered Professional Engineer under the laws of the state of New Mexico.

Christopher S. Archuleta, P.E. NMPE No. 29025

November 9, 2023



Date

i.



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LIST OF ACRONYMS

cfs	cubic feet per second
COA	City of Albuquerque
EOPC	Engineer's Opinion of Probable Cost
GPM	gallons per minute
hp	horsepower
PCSWMM	Personal Computer Storm Water Management Model
SBDMP	South Broadway Drainage Master Plan
SUE	subsurface utility engineering
ТС	time of concentration
TDH	total dynamic head

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1.0 INTRODUCTION

1.1 PURPOSE

RESPEC Company, LLC (RESPEC) was tasked with conducting a feasibility report for the city-owned property, outlined in red in Figure 1. This task came from the conceptual options proposed in the South Broadway Drainage Master Plan (SBDMP) [RESPEC, 2023]¹ to help reduce historical flooding in the South Broadway study area. RESPEC suggested completing a feasibility report on the John Street Pond facility before preparing a full design. In the SBDMP update, RESPEC recommended the city move forward with Option 4, which includes two ponds, a detention pond, a pump station, and storm drain improvements. Furthermore, RESPEC recommended getting more detailed data including topographic and subsurface utility engineering (SUE) because the basis of the SBDMP update was built using asbuilt information from the 1930s. This detailed information has helped RESPEC refine the proposed options plus give a better idea of what options are feasible.



Figure 1. Vicinity Map.

RESPEC, 2023. *South Broadway Drainage Master Plan*, prepared by RESPEC, Albuquerque, NM, for the City of Albuquerque, Albuquerque, NM.



1.2 SITE CHARACTERISTICS AND FIELDWORK

The property is owned by the City of Albuquerque (COA) and is located at the intersections west of John Street, south of Thaxton Avenue, east of Williams Street, and north of Englewood Drive. The existing site conditions are undisturbed, with slopes ranging from 0.5 percent to 1 percent sloping toward the west. The site has poor land cover comprised of native desert landscapes throughout the property. The surrounding urban area is fully developed and consists of residential lots of varying size and commercial properties.

RESPEC conducted fieldwork at the project site and surrounding areas concerning the John Street feasibility limit in April 2023, including the Barelas Ditch easement, Thaxton Avenue, John Street, and Williams Street. Figure 2 illustrates the areas where key storm drain infrastructure is proposed. The purpose of field observation was to confirm existing site conditions. Additional photographs and an annotated map are included in Appendix A.

1.3 REPORT GOALS

The following project steps are detailed in this report:

- / Acquire SUE and a topographic survey for the project area
- / Integrate SUE data into the model and design
- Acquire geotechnical analysis of the site for soil conditions, erosion control measures, and slope stability and verify the groundwater level
- / Analyze the pump flowrates and horsepower, electrical requirements, and coordinate with pump manufacturers for the pump station, wet well, and force main design
- / Explore prefabricated wet well options for the pump station
- / Prepare the John Street Pond Facility's construction phasing plan and conceptual level site design
- / Provide an Engineer's Opinion of Probable Cost (EOPC)

After the design analysis report is approved, the project's next phase is developing construction plans. The construction plans will encompass the John Street Pond facility with the associated storm drain improvements; however, these improvements will be strategically phased to stay within the COA's budget.

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2.0 HYDROLOGIC ANALYSIS

2.1 EXISTING CONDITIONS

All existing hydrology methodologies and input parameters were extracted from the SBDMP [RESPEC, 2023]. Personal Computer Storm Water Management Model (PCSWMM) hydrology and input parameters, such as the initial abstraction, depression storage, and the curve numbers, were used to discuss the subbasin delineation. Appendix A contains the SBDMP. Figure 3 illustrates the existing conditions basin boundaries around the John Street Pond from the SBDMP.

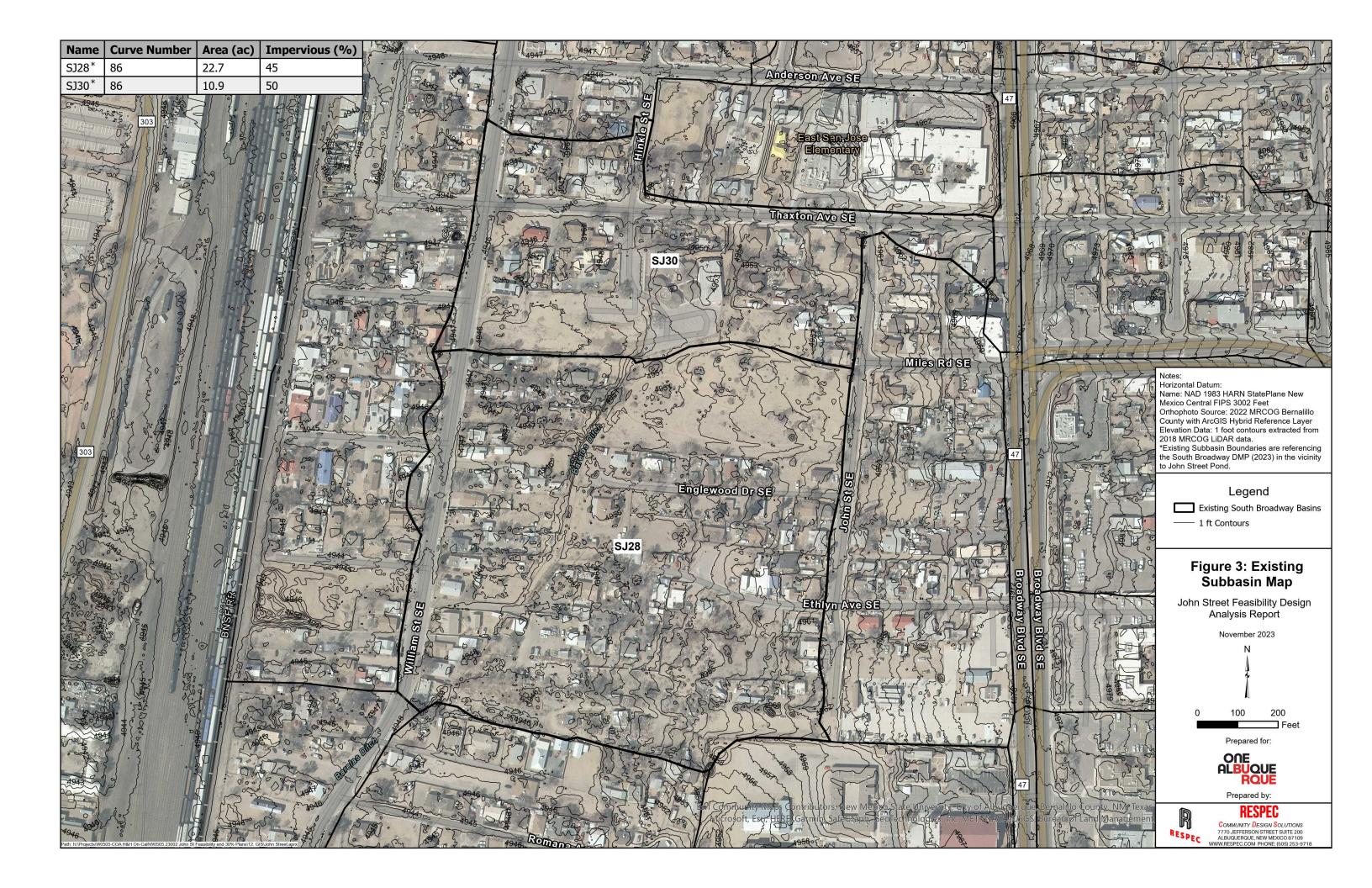
2.2 PROPOSED CONDITIONS

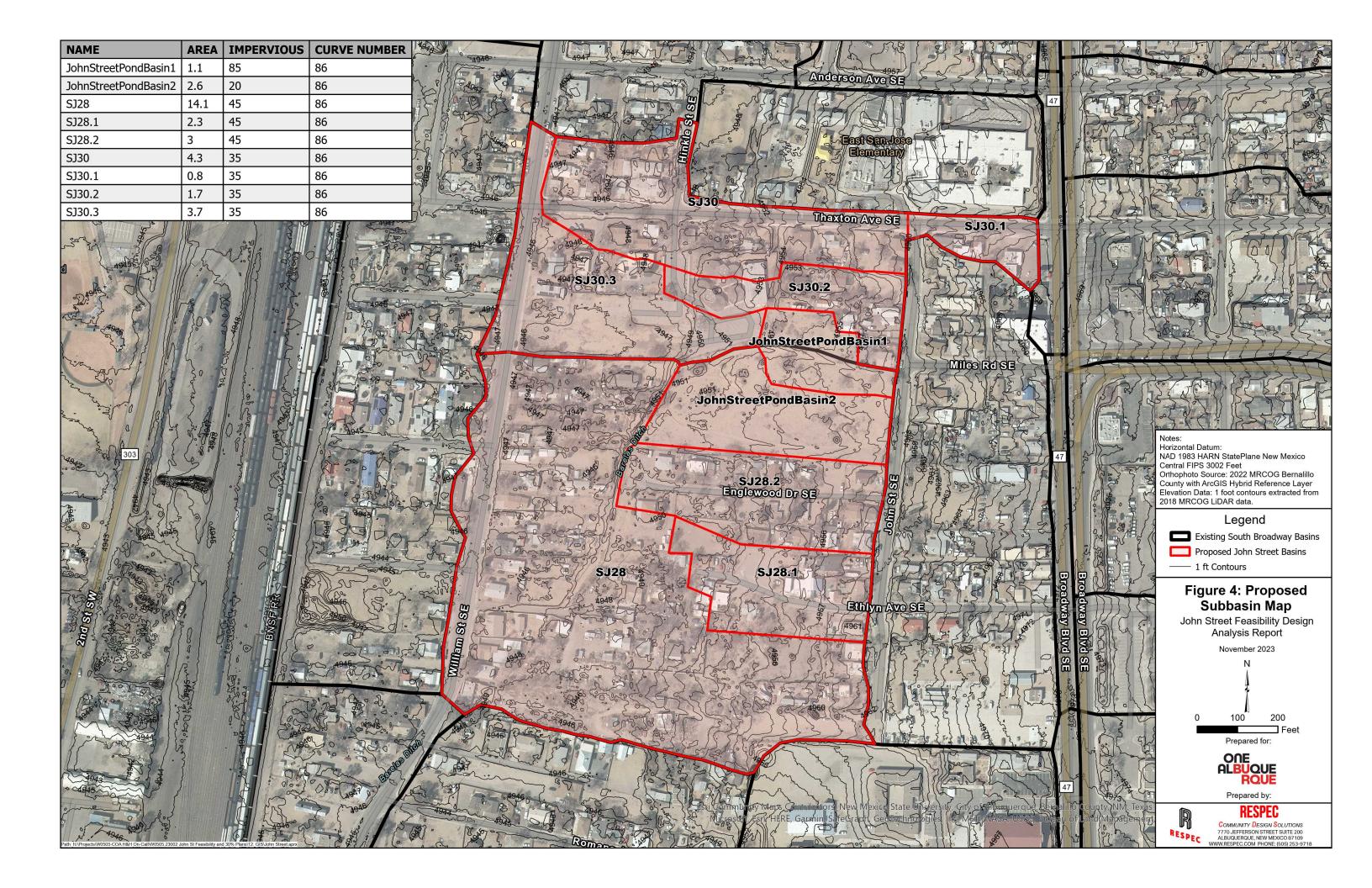
Some basin boundaries were strategically split to analyze runoff volumes and peak discharges going to the proposed John Street Pond. The proposed John Street Pond Basin 1 and John Street Pond Basin 2's impervious parameter was updated from the existing conditions to reflect the proposed improvements. Table 1 compares the existing and proposed basin impervious parameters. Figure 4 illustrates the proposed conditions basin boundaries around the John Street Pond.

1			
Existing Basin Name	Impervious (%)	Proposed Basin Name	Impervious (%)
SJ28	45	John Street Basin 2	20
SJ30	35	John Street Basin 1	85

 Table 1. Summary of Personal Computer Storm Water Management

 Model Input Parameters







This design analysis report reassesses the John Street Pond and provides a more detailed facility analysis. The existing hydraulic system for South Broadway indicates significant deficiencies throughout the South Broadway Watershed. Options to help mitigate flooding throughout the system in the SBDMP were developed. The SBDMP provided the COA with a list of proposed improvements and recommended priorities that were listed in the order that each proposed project should be designed and constructed. The priority from the SBDMP was to analyze and develop construction plans for the John Street Pond. RESPEC used the COA's *Design Process Manual* [COA, 2020]² for the improvement's design criteria.

3.1 EXISTING CONDITIONS

RESPEC updated the existing conditions PCSWMM model from the SBDMP [RESPEC, 2023] using SUE information provided by High Mesa Consulting Group [Cala, 2023]³ for the area between Thaxton Avenue and Englewood Drive and Broadway Boulevard and Williams Street. This information included storm drainpipe sizes, inverts, and manhole rim elevations. The SBDMP is included in Appendix A and provides further insight into the hydraulic modeling parameters. The updated model version was also updated to version 5.2.4.

3.2 PROPOSED CONDITIONS

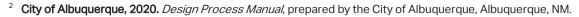
RESPEC is proposing future improvements to include a gravity and pump station pond, where an electric building will house a wet well and all required accessories for pumps. The southern pond, John Street Gravity Pond, will divert flows from Broadway Boulevard through a 66-inch storm drain that eventually discharges into the Barelas Ditch storm drain toward the property's southwest corner. The John Street Gravity Pond will divert flows by one of the following two storm drain alternatives:

- I Diverting water from Broadway Boulevard heading west on Thaxton Avenue, south on John Street, and into the pond
- / Diverting water west on Gibson Boulevard, south onto John Street, and into the pond

The northern pond, John Street Pump Station Pond, will divert flows from Williams Street through a 66-inch storm drain pumped into either Williams Street or Broadway Boulevard. For the John Street Pump Station Pond, RESPEC's initial analysis was to continue the storm drain east on Thaxton Avenue, south through the existing Barelas Ditch easement into the pond; however, the storm drain corridor would be too constricted and may cause stability issues through the easement. The John Street Pump Station Pond is discussed further in Section 3.2.2. Figure 5 provides an overview of the storm drain improvements. Detailed plan and profiles of the storm drain alternatives are included in Appendix B.

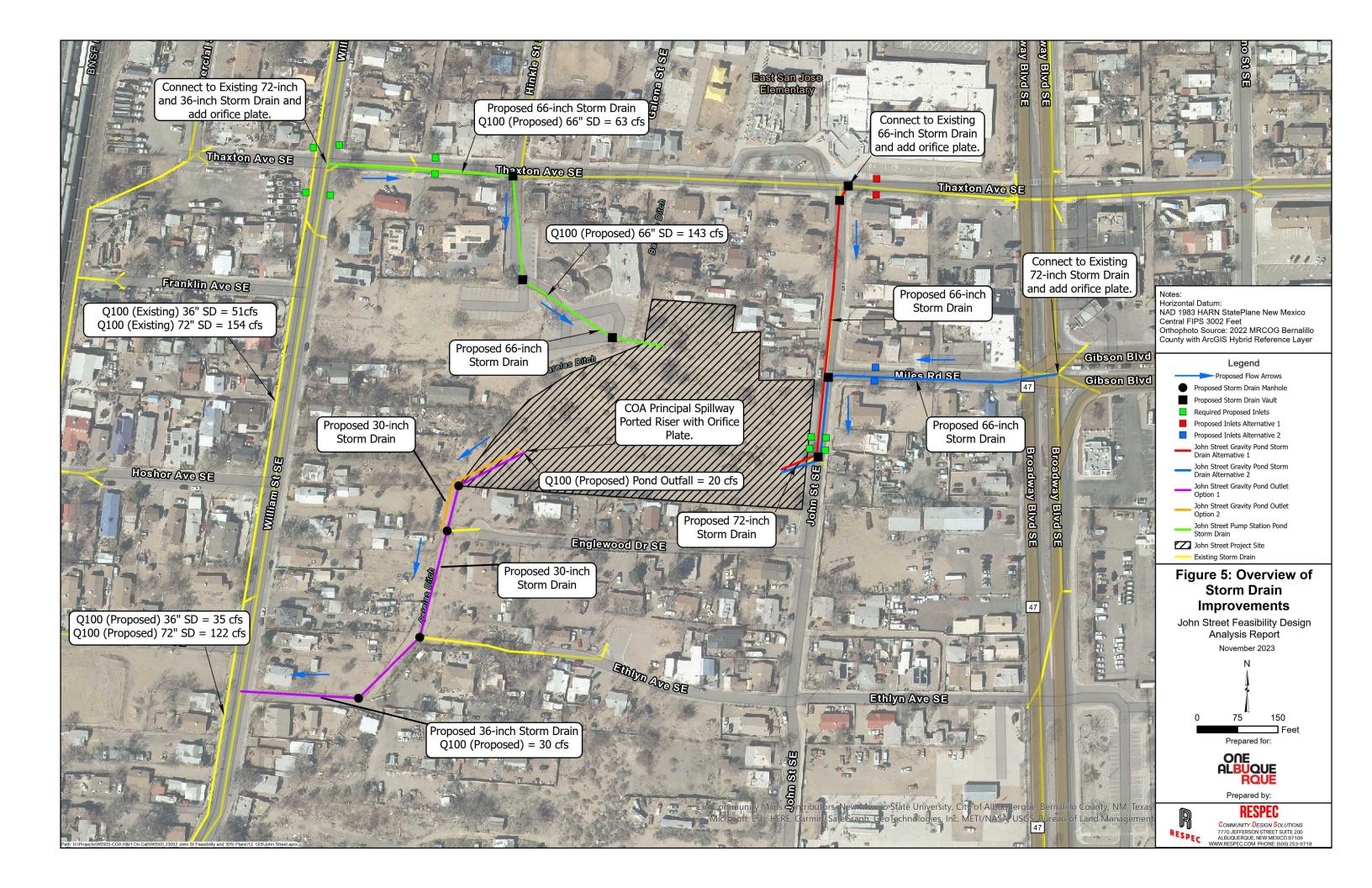
3.2.1 JOHN STREET GRAVITY POND

Option 1 has a 6-foot embankment with a standard COA principal spillway ported riser that will discharge to the Barelas Ditch storm drain. The Barelas Ditch storm drain will be replaced with a new



³ Cala, C. G., 2023. Proposed John Street Pond, Albuquerque, NM, prepared by High Mesa Consulting Group, Albuquerque, NM.

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storm drain connecting to Williams Street's existing storm drain. The emergency spillway is designed to convey the 100-year inflow discharge and will be lined with shotcrete for erosion protection. The storm drain inlet will have a riprap apron to help dissipate the 166 cubic feet per second (cfs) of flow that enters the pond. The summary of improvements for Option 1 is listed in Table 2. This apron basin was designed following the *Drainage Process Manual* [COA, 2020]. Detailed calculations for the design process are provided in Appendix B. Figure 6 illustrates the detailed grading plan for Option 1. The cost for Alternative 1 is \$7,177,000, and for Alternative 2 is \$7,266,000. An EOPC for each alternative is included in Appendix C.

Structure Type	Description	
Pond	Pond Invert = 4,941 feet (ft)Top of Pond = 4,957 ftDesign Volume = 10.5 acre-ft to the emergency spillwayCOA Ported Riser Principal Spillway Design # 19, Type 4 (30-inch outfall). 100-yearflow = xxx cfs	
Emergency Spillway	Shotcrete lined spillway 1 ft deep by 65 ft long to convey 100-year flow = 166 cfs	
Inlet Apron	27 ft wide by 32 ft long by 3 ft deep; riprap thickness is 2 ft using D_{50} of 12 inches	

Table 2. Option 1 Summary of Improvements	S
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Option 2 has a 6-foot (ft) embankment with a standard COA principal spillway ported riser that will discharge to the Barelas Ditch storm drain. The Barelas Ditch storm drain will be replaced with a new storm drain that will connect to the existing storm drain in Williams Street. The emergency spillway is designed to convey the 100-year inflow discharge and will be lined with shotcrete for erosion protection. The storm drain inlet will have a riprap apron to help dissipate the 195 cfs of flow that enters the pond. The summary of improvements for Option 2 is listed in Table 3. This apron basin was designed following the *Drainage Process Manual* [COA, 2020]. Detailed calculations for the design process are provided in Appendix B. Figure 7 illustrates the detailed grading plan for Option 2. The cost for Alternative 1 is \$6,600,000 and \$6,779,000 for Alternative 2. An EOPC is included in Appendix C.

Table 3. Option	n 2 Summary of	Improvements
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Structure Type	Description	
	Pond invert = 4,947.4 ft Top of Pond = 4,957 ft	
Pond	Design Volume = 8.2 acre-ft to the emergency spillway	
FUIU	COA Ported Riser Principal Spillway Design # 1, Type 1 (30-inch outfall). 100-year flow = xxx cfs	
Emergency Spillway	shotcrete lined spillway 1 ft deep by 80 ft long to convey 100-year flow = 195 cfs	
Inlet Apron	27 ft wide by 32 ft long by 3 ft deep; riprap thickness is 2.5 ft using $D_{\rm 50}$ of 15 inches	

3.2.2 JOHN STREET PUMP STATION POND AND SITE DESIGN

The John Street Pump Station Pond will have 1V:1.5H shotcrete lined slopes and a 1V:6H shotcrete lined access road. Figures 6 and 7 illustrate the grading plan for the John Street Pump Station Pond. The John Street Pump Station Pond will flow into the concrete wet well and include a duplex or triplex pump station, depending on the chosen pump configuration, that will be housed in a 30-ft by 50-ft building along with the wet well and electrical components. This building will be located on the

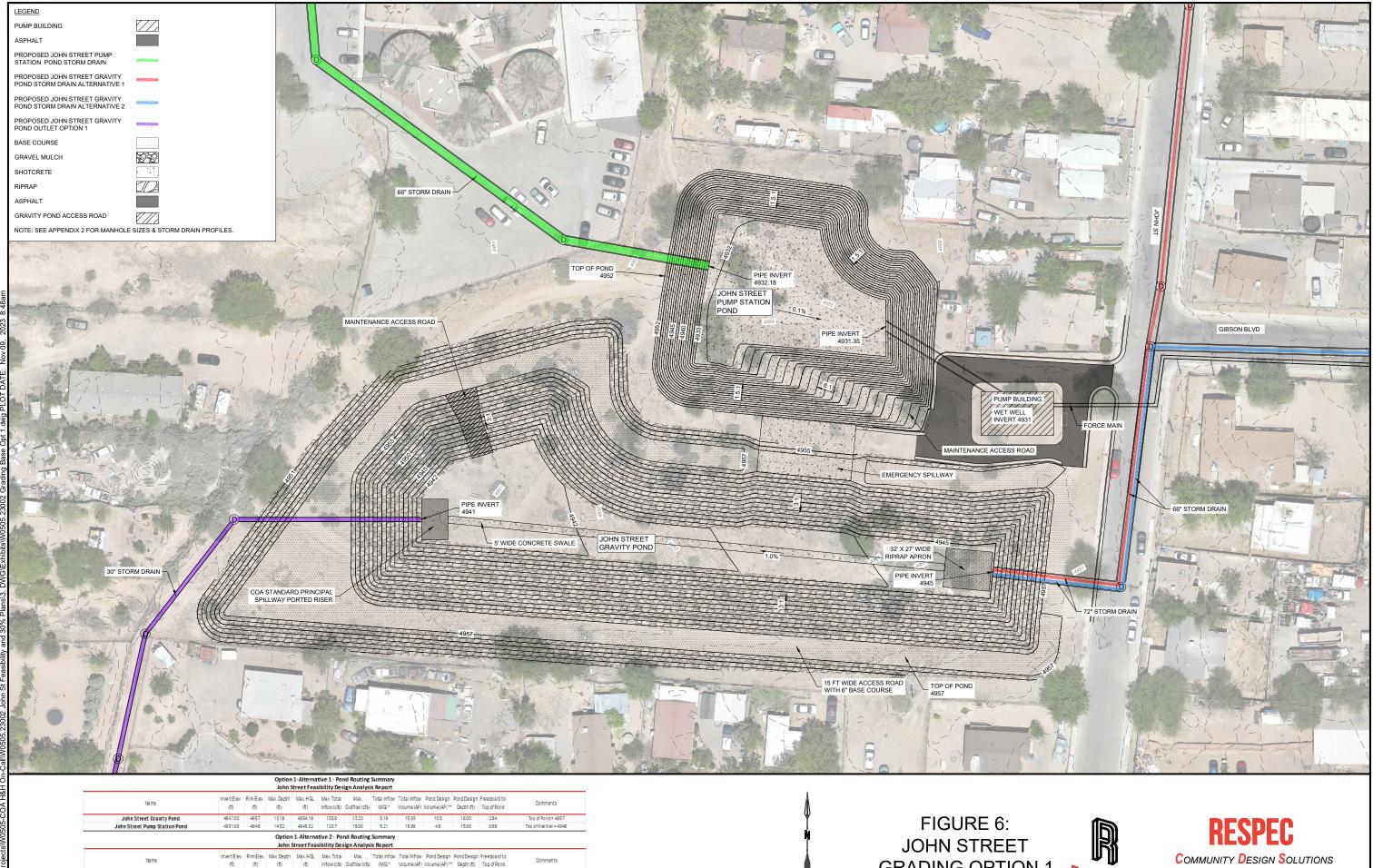


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property's east side and accessible from John Street. There are three pump station configurations described in the following text. An overview of the pump station building and entrance to the site is illustrated in Figure 8.





12.27 13.7

4941.00 4957

4931.00 4946

John Street Gravity Pond

John Street Pump Station Pond

*Pond volume converting from million gallons (MG) to acre-ft (AF) is multiplying by 3.07
**Design volume measured to the emergency spillway

4953.27 165.6 12.74 4.72 4944.70 111.6 18.00 4.58

14.49 14.06

10.5 4.8

16.00 15.00

3.73 1.30

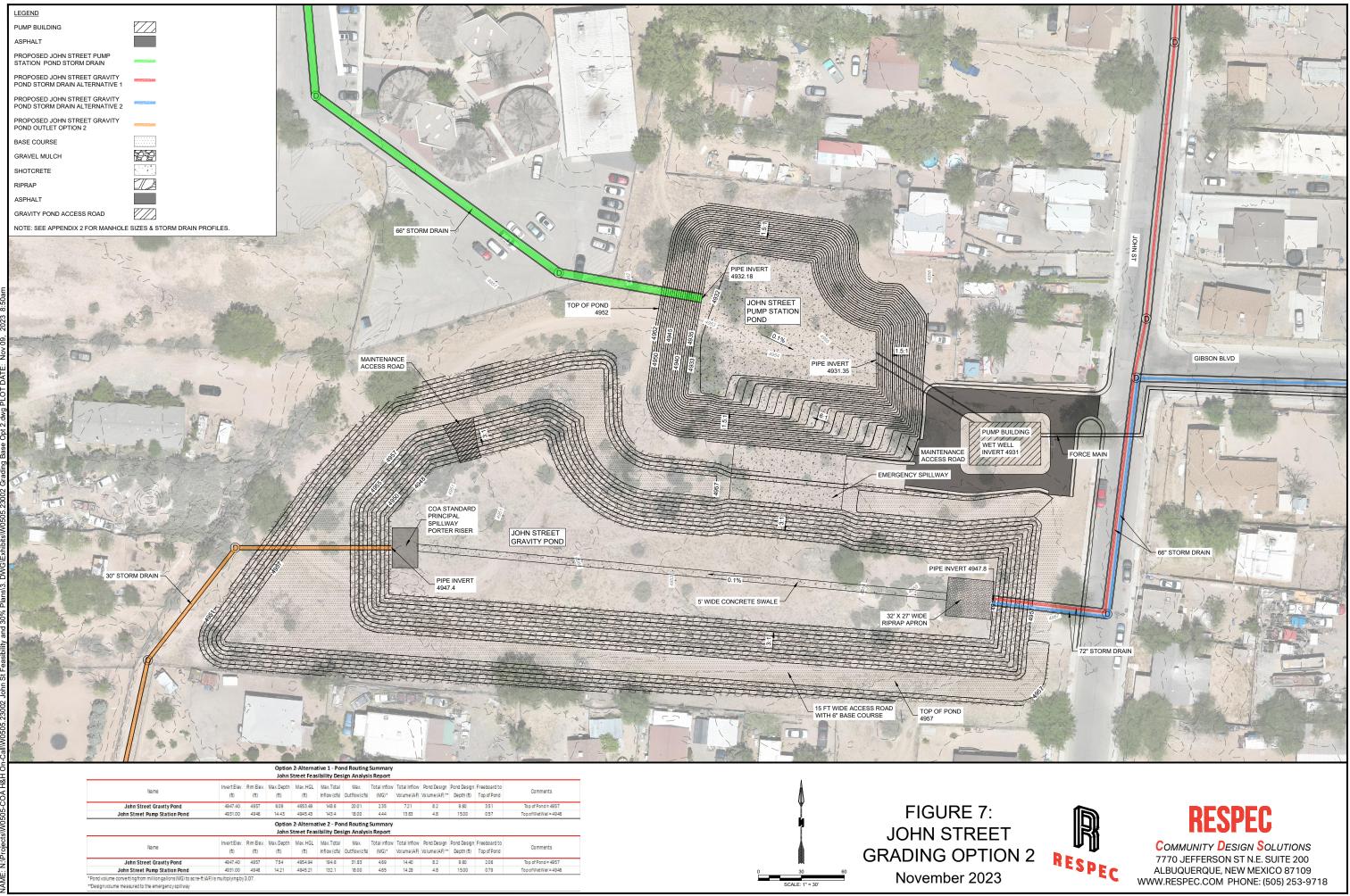
Top of Pond = 4957

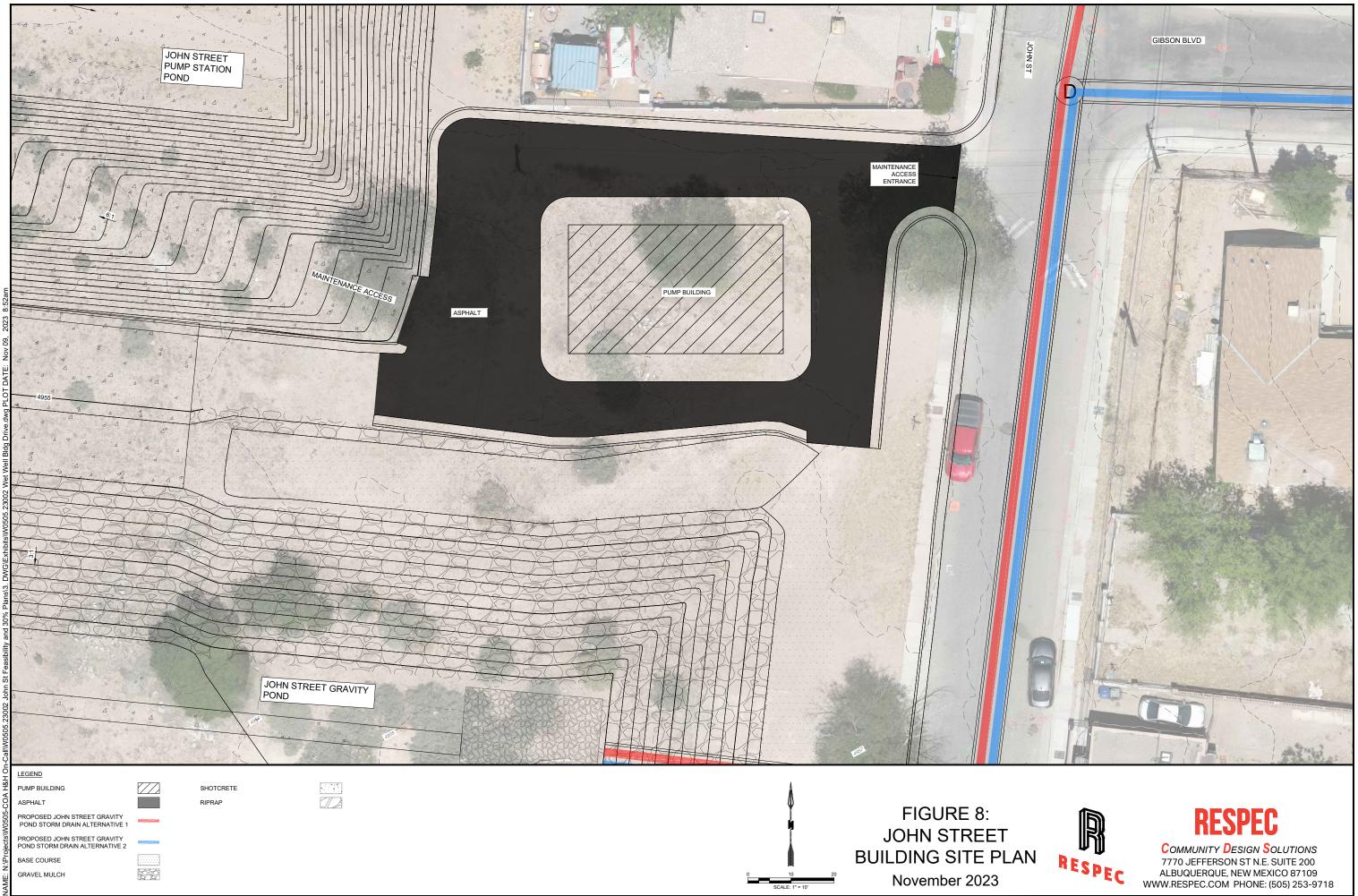
Top of Wet Weil = 4946

SCALE: 1" = 30'

November 2023









Pump Station Design Specifications:

- / Wet well depth = 15 ft
- / Broadway (total dynamic head [TDH]) = 25 ft
- / Williams (TDH) = 20 ft
- / Pond design volume = 4.7 acre-ft at 1.5H:1V slope
- Pump discharge (target flowrate) = 18 cfs or 8,100 gallons per minute
- / Force main diameter discharge line = 24 inches with approximately 3 ft per second velocities

3.2.3 CONFIGURATION 1: DUPLEX SYSTEM (2 X FLYGT NP3531, 90HP)

This system contains two pumps: one sump pump for low flows with a total flowrate of approximately 1 cfs and one main pump that pumps 18 cfs, the total designed flowrate for the pump station. With this configuration, a third pump could be installed if the other pump fails or as a backup. The backup pump would have the same specifications as the main pump and provide room for upgrades. In this configuration, the pumps will be running in parallel. The sump pump is a 5-horsepower (hp) pump with a 6-inch discharge line with 67 percent operating efficiency. The main pump is a 90-hp pump with a 20-inch discharge line with 81 percent operating efficiency. The wet well would not be prefabricated, and the minimum dimensions would need to be 12 ft by 20 ft or 12 ft in diameter.

3.2.4 CONFIGURATION 2: TRIPLEX SYSTEM (3 X FLYGT NP3202, 35HP)

This system will contain three pumps: one sump pump for low flows with a total flowrate of approximately 1 cfs and two main pumps that pump 18 cfs combined (approximately 9 cfs per pump), the total designed flowrate for the pump station. With this configuration, a fourth pump could be installed if the other pump fails or as a backup. The backup pump would have the same specifications as the main pumps and provide room for upgrades. In this configuration, the pumps will be running in parallel. The sump pump is a 5-hp pump with a 6-inch discharge line and 67 percent operating efficiency. The main pump is a 34-hp pump with a 12-inch discharge line and 78 percent operating efficiency. The wet well would not be prefabricated, and the minimum dimensions would need to be 12 ft by 13 ft or 15 ft in diameter.

3.2.5 CONFIGURATION 3: DUPLEX SYSTEM (4 X FLYGT NP3153, 20HP)

This system will have two separate wet wells to house two main pumps in each wet well, four pumps in total. There will be a third wet well with one sump pump for low flows and a total flowrate of approximately 1 cfs. In each wet well, two main pumps will pump 9 cfs combined (approximately 4.5 cfs per pump) in each wet well. In this configuration, the pumps will be running in parallel. The sump pump is a 5-hp pump with a 6-inch discharge line and 67 percent operating efficiency. The main pump is a 20-hp pump with an 8-inch discharge line and 78 percent operating efficiency. The wet well would be prefabricated with a 6-ft diameter.

RESPEC coordinated with manufacturers to prepare a prefabricated pump system to lower construction costs and reduce lead time. RESPEC will continue to work with pump manufacturers to ensure the best available options are provided during the project's next phases. The cost estimates

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included the backup pumps in each configuration; however, to simplify calculations, backup pumps were not included in this design report.

The pump specifications, minimum wet well sizes, curves, and other related information from the manufacturer are provided in Appendix B as well as the preliminary calculations, pump curves, and pump schematics for the pump station. Appendix B also includes the electrical requirements and calculations as a supplemental report. The estimated costs for each pump configuration are listed in Table 4, and the detailed cost breakdowns are included in Appendix C.

Configuration No.	Configuration Type	Total Cost (\$)
1	Duplex System	1,230,000
2	Triplex System	894,300
3	Duplex Stations	574,000

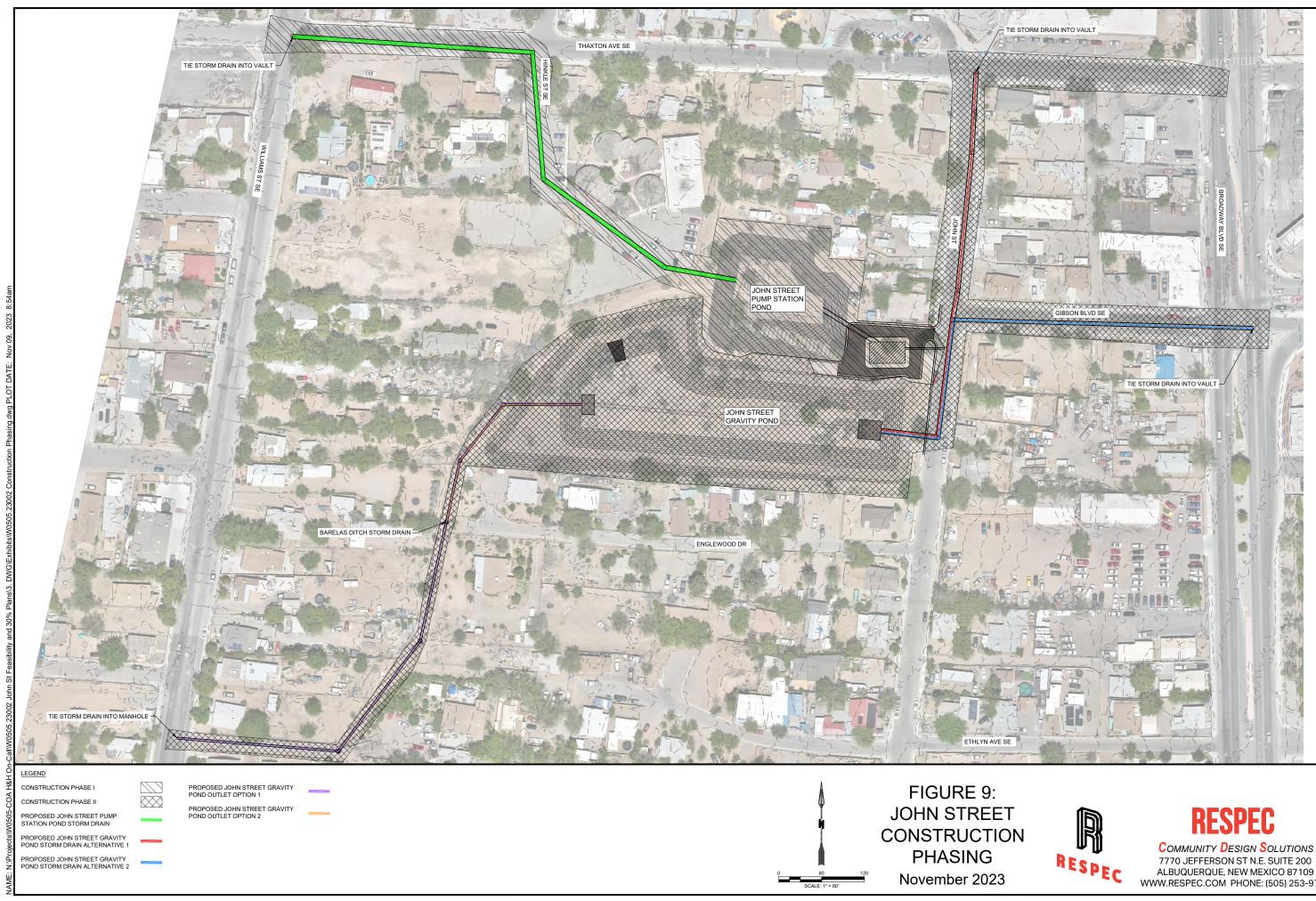




4.0 CONCLUSION AND RECOMMENDATION

In this feasibility report, RESPEC focused on two pond options with two storm drain alternatives for the John Street facility. The gravity pond options focus on balancing earthwork quantities, creating enough storage volume for this project phase while accommodating additional runoff volume that could be conveyed from future improvements. The pump station pond was similar between options since the focus was refining the pump station system, wet well size, and exploring prefabricated options, but created additional design volume in the pond for future improvements. RESPEC recommends Option 2, Alternative 1 with Pump Configuration 3, to be the most effective. This option creates sufficient capacity in the system for this project phase and plans for future improvements to the system as additional funding becomes available. The project will be split into two phases: (1) constructing the John Street Pump Station Pond and (2) diverting the storm drain on Williams Street. The second phase is constructing the John Street Gravity Pond, diverting the storm drain on Broadway Boulevard, and improving the Barelas Ditch storm drain. This phasing plan is depicted in Figure 9.





7770 JEFFERSON ST N.E. SUITE 200 ALBUQUERQUE, NEW MEXICO 87109 WWW.RESPEC.COM PHONE: (505) 253-9718



APPENDIX A BACKGROUND INFORMATION





A-1

RSI-3390



APPENDIX A: BACKGROUND INFORMATION

The following items are included in Appendix A:

- / Albuquerque Bernalillo County Water Utility Authority As-Builts
- / City of Albuquerque Standard Documents
 - » Principal Spillway Ported Riser Drawings
 - » Principal Spillway Ported Riser Report
- / RESPEC Site Visit
 - » Photographs
 - » Annotated Photograph Map
- *I* South Broadway Drainage Master Plan by RESPEC
- / John Street Storm Drain Engineering Report by GEO-TEST





APPENDIX B Hydraulic Analysis







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APPENDIX B: HYDRAULIC ANALYSIS

The following items are included in Appendix B:

- / Existing Conditions South Broadway Model (PCSWMM 5.2.4)
- / Proposed Conditions Model Option 1 (Alt1 & Alt 2) and Option 2 (Alt 1 & Alt 2) PCSWMM 5.2.4
- / Table 2.1 Elevation Storage Discharge John Street Gravity Pond Option 1
- / Table 2.2 Elevation Storage Discharge John Street Pump Station Pond Option 1
- / Table 2.3 Elevation Storage Discharge John Street Gravity Pond Option 2
- / Table 2.4 Elevation Storage Discharge John Street Pump Station Pond Option 2
- / Table 2.5 Option 1-Alternative 1 Pond Routing Summary
- / Table 2.6 Option 1-Alternative 2 Pond Routing Summary
- / Table 2.7 Option 2-Alternative 1 Pond Routing Summary
- / Table 2.8 Option 2-Alternative 2 Pond Routing Summary
- / Table 2.9 Riprap Apron Sizing Option 1
- / Table 2.10 Riprap Apron Sizing Option 2
- / Table 2.11 John Street Sump Inlet Calculations
- / Table 2.12 Williams Street Sump Inlet Calculations
- / John Street Proposed Storm Drain Conceptual Plan and Profiles
- / CTA Electrical Feasibility Report for John Street Pond
- / Proposed Storm Drain Hydraulic Grade Line Profiles (SWMM)
 - » Option 1 Alternative 1 Gravity Plan & Profile (with PCSWMM HGL)
 - » Option 1 Alternative 1 Pump Plan & Profile (with PCSWMM HGL)
 - » Option 1 Alternative 2 Gravity Plan & Profile (with PCSWMM HGL)
 - » Option 1 Alternative 2 Pump Plan & Profile (with PCSWMM HGL)
 - » Option 2 Alternative 1 Gravity Plan & Profile (with PCSWMM HGL)
 - » Option 2 Alternative 1 Pump Plan & Profile (with PCSWMM HGL)
 - » Option 2 Alternative 2 Gravity Plan & Profile (with PCSWMM HGL)
 - » Option 2 Alternative 2 Pump Plan & Profile (with PCSWMM HGL)
- / Supporting Documents and References
 - » Pump Manufacturer Curves
 - » Pump Manufacturer Wet Well Details
 - » Urban Storm Drainage Criteria Manual (USDCM) Volume 2
 - » Mile High Flood District (MHFD) Riprap Type Specification
 - » Hydraulic Design of WW Lift Stations
 - » COA Type "A" Double Wing SD 2201A
 - » COA DPM Type Double A 2% Slope on Grade Nominal Grate Capacity





APPENDIX C ENGINEER'S OPINION OF PROBABLE COST





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APPENDIX C: ENGINEER'S OPINION OF PROBABLE COST

The following items are included in Appendix C:

- / Table 3.1 Engineers Opinion of Probable Cost Option 1 Alternative 1
- / Table 3.2 Engineers Opinion of Probable Cost Option 1 Alternative 2
- / Table 3.3 Engineers Opinion of Probable Cost Option 2 Alternative 1
- / Table 3.4 Engineers Opinion of Probable Cost Option 2 Alternative 2
- / Table 3.5 Pump Station Configuration Cost Estimates

