# CITY OF ALBUQUERQUE

Planning Department Alan Varela, Director



Mayor Timothy M. Keller

August 24, 2023

Åsa Nilsson-Weber, P.E. Isaacson & Arfman, P.A. 128 Monroe St. N.E Albuquerque, NM 87108

# RE: Phil Chacon Park - Renovation Grading Plans & Drainage Report Engineer's Stamp Date: 08/02/23 Hydrology File: L19D077

Dear Ms. Nilsson-Weber:

PO Box 1293 Based upon the information provided in your submittal received 08/02/2023, the Grading Plans & Drainage Report are approved for Building Permit and Grading Permit. Please attach a copy of this approved plan in the construction sets for Building Permit processing along with a copy of this letter.

# Albuquerque **PRIOR TO CERTIFICATE OF OCCUPANCY:**

1. Engineer's Certification, per the DPM Part 6-14 (F): Engineer's Certification Checklist For<br/>Non-Subdivision is required.

www.cabq.gov

As a reminder, if the project total area of disturbance (including the staging area and any work within the adjacent Right-of-Way) is 1 acre or more, then an Erosion and Sediment Control (ESC) Plan and Owner's certified Notice of Intent (NOI) is required to be submitted to the Stormwater Quality Engineer (Dough Hughes, PE, jhughes@cabq.gov, 924-3420) 14 days prior to any earth disturbance.

If you have any questions, please contact me at 924-3995 or <u>rbrissette@cabq.gov</u>.

Sincerely,

Renée C. Brissette

Renée C. Brissette, P.E. CFM Senior Engineer, Hydrology Planning Department



# **City of Albuquerque**

Planning Department

Development & Building Services Division

# DRAINAGE AND TRANSPORTATION INFORMATION SHEET NO FEE. CITY PROJECT

NOTEL,		1	
Project Title: Phil C	hacon Park	Building Permit #	Hydrology File # <u>L-19</u>
DRB#Ren	ovation	EPC#	
Legal Description: <u>A</u> within the S	n Unplatted Tract of 5/2 SE/4 NW/4 of Se	Land City Add ction 30, T.10.N., R.4	dress OR Parcel <u>7600 Southern Ave.</u> S E., N.M.P.M.
Applicant/Agent: Isa	aacson & Arfman, In	C. Contact:	: Bryan J. Bobrick
Address: 128 Monro	be Street NE	Phone	e: (505) 268-8828
Email: bryanb@iaci	ivil.com		
Applicant/Owner: C	ity of Albuquerque	Contact	t: Jesse Scott
Address: Parks	& Recreation Depar	tment Phone	e: <u>(505) 768-5364</u>
Email: jessesco	ott@cabq.gov	· · · · · · · · · · · · · · · · · · ·	
TYPE OF DEVELOP: RE-SUBMITTAL:	MENT:PLAT (#orYESXNO	f lots)RESIDENCE _	_DRB SITEADMIN SITE: _X
<b>DEPARTMENT:</b> Check all that apply:	TRANSPORTAT	TON X HYDROLO	DGY/DRAINAGE
TYPE OF SUBMIT	ſAL:	TYPE OF APPR	OVAL/ACCEPTANCE SOUGHT:
ENGINEER/ARCH	ITECT CERTIFICATIO	DN <u>X</u> BUILD	DING PERMIT APPROVAL
PAD CERTIFICAT	ION	CERTI	FICATE OF OCCUPANCY
CONCEPTUAL G&	D PLAN	CONCI	EPTUAL TCL DRB APPROVAL
X GRADING PLAN	DT	PRELI	MINARY PLAT APPROVAL
DRAINAGE KEPU	KI YED DI AN		LAN FOR SUB'D APPROVAL
	EK PLAIN ZELODMENT DEDMIT	SILE P.	DI AT ADDOVAL
FLOOD I LAN DEV		AIT	TEAT AT ROVAL
	INCALL		DATION PERMIT APPROVAL
TRAFFIC CIRCUL	ATION LAYOUT (TCI	X  GRAD	ING PERMIT APPROVAL
ADMINISTRATIVI	E	SO-19	APPROVAL
TRAFFIC CIRCUL	ATION LAYOUT FOR	DRB PAVIN	G PERMIT APPROVAL
APPROVAL		GRADI	ING PAD CERTIFICATION
TRAFFIC IMPACT	STUDY (TIS)	WORK	ORDER APPROVAL
STREET LIGHT LA	AYOUT	CLOM	R/LOMR
OTHER (SPECIFY)	)	FLOOD	D PLAN DEVELOPMENT PERMIT
PRE-DESIGN MEE	TING?	OTHER	R (SPECIFY)

DATE SUBMITTED: August 2, 2023

AUGUST 2, 2023

# SUPPLEMENTAL CALCULATIONS

FOR

# PHIL CHACON PARK RENOVATIONS

# ALBUQUERQUE, NEW MEXICO

City of Albuquerque Planning Department Development Review Services HYDROLOGY SECTION
APPROVED DATE: 08/24/23 BY: Ronee Consulta HydroTrans # L19D077
THE APPROVAL OF THESE PLANS/REPORT SHALL NOT BE CONSTRUED TO PERMIT VIOLATIONS OF ANY CITY ORDINANCE OR STATE LAW, AND SHALL NOT PREVENT THE CITY OF ALBUQUER OUR EROM REQUIRING SPECIFICATIONS, OR BERGOR OF DIMENSIONS IN FLANS SPECIFICATIONS, OR GED, MODIFIED OR ALTERED WITHOUT AUTHORIZATION.

PREPARED BY





128 Monroe Street NE Albuquerque, NM 87108 505-268-8828 | www.iacivil.com

I&A Project No. 2573

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# **PROJECT SUMMARY**

Phil Chacon Park shall be redeveloped with playgrounds, recreation fields and walks. The existing parking lot at the north end of the project shall be resurfaced.

The proposed grading of the site shall follow the existing drainage patterns with the northerly portion of the site draining to Southern Ave. and the remainder of the site draining to the southwest area of the park.

The developed discharge to Southern Ave. will be the same as the historical rate. Since basins 2 and 3 (playground areas with 12-inch thick bark) will retain the storm water, the developed discharge from the remainder of the site discharging to the southwest corner of the park will be reduced—38.4 cfs developed; 40.1 cfs historical.

A rock-lined rundown will be installed south of the basketball field to convey 14.1 cfs to the west

The storm drain is designed to carry the 10-year flows. In larger storms, the additional flows will overtop the depressed areas at the inlets and surface drain to the historical discharge locations at the southwest area of the park.

Storm Water Quality (SWQ):

Two SWQ ponds will be installed east and north of the basketball courts at the southwest corner of the park to retain the volume of 0.26 inches falling on the impervious areas.

SWQ volume required = 2,523 cf SWQ volume provided = 2,488 cf

See Appendices for hydrology, SWQ pond volume, storm drain and rundown calculations.

# **APPENDIX** A

Hydrology Calculations for 100-yr, 6-hr Storm Hydrology Calculations for 10-yr, 6-hr Storm SWQ Pond Volume Calculations

Job Name:	Phil Chacon	Park
Client:	PLAND	
Date Prepared:	2/23/2023	
Date Modified:	4/11/2023	
Precipitation Zone:	3	

			CALC	ULATIONS: Phil (	Chacon	Park : 43565		
		Based on Cit	y of Albuq	uerque DMP, Article	6-2 Hyd	drology dated Ju	ine 26, 2020	)
			10	0-YEAR, 6-HOUR C	CALCU	LATIONS		
AREA OF SITE:	:			711460	SF	=	16.33	ACRE
				100-year, 6-hour				
HISTORIC FLO	<b>DWS</b> :			DEVELOPED FL(	<b>OWS:</b>			EXCESS PRECIP:
		Treatment SF	%	-		Treatment SF	%	Precip. Zone 3
Area A	=	0	0%	Area A	=	0	0%	$E_{A} = 0.67$
Area B	=	615199	86.47%	Area B	=	594738	83.59%	$E_{\rm B} = 0.86$
Area C	=	0	0%	Area C	=	0	0%	$E_{\rm C} = 1.09$
Area D	=	96261	13.53%	Area D	=	116722	16.41%	$E_{\rm D} = 2.58$
Total Area	=	711460	100%	Total Area	=	711460	100%	-
On-Site Weighter	d Exces	s Precipitation ( Weighted E =	100-Year,	6-Hour Storm) $\frac{E_AA_A + E_BA_B + E_CA}{A_A + A_B + A_C}$	$\frac{A_{C} + E_{D}}{A_{D}}$	AD		
Historic E		1.09	in.	Developed E	=	1.14	4 in.	]
On-Site Volume Historic V <sub>360</sub>	of Run	off: V360 = 64785	CF	E*A / 12 Developed V <sub>360</sub>		67718	8 CF	]
On-Site Peak Discharge Rate: $Qp = Q_{pA}A_A + Q_{pB}A_B + Q_{pC}A_C + Q_{pD}A_D / 43,560$ For Precipitation Zone 3								
Q <sub>pA</sub>	=	1.84		$Q_{pC}$	=	3.17		
$Q_{pB}$	=	2.49		Q <sub>pD</sub>	=	4.49		
Historic Q <sub>p</sub>	=	45.1	CFS	Developed Q <sub>p</sub>	=	46.0	) CFS	]
· ·				• •				+

100-yr, 6-hr

BASIN NO. 1			DESCRI	PTION		To Southern	n Ave.
Area of basin flows =	61484	SF			=	1.41 Ac.	
	01101					LAND TR	EATMENT
	Sub-basin Weigh	ted Exc	ess Precin	itation		A =	0%
	Weighted E	=		1 75 i	n	B=	48%
	Sub-basin Volum	e of Ru	noff:	11,01		C =	0%
	V <sub>260</sub>	=		8989	CF	D =	52%
	Sub-basin Peak D	ischarg	e Rate:			Stormwate	er Ouality Volume
	Qp	=	,	5.0	cfs		693 CF
BASIN NO. 2	a		DESCRI	PTION		Self Pond	ling
Area of basin flows =	12954	SF			=	0.3 Ac.	
						LAND TR	EATMENT
	Sub-basin Weigh	ted Exc	ess Precip	itation:		A =	0%
	Weighted E	=	•	1.08 i	n.	B =	87%
	Sub-basin Volum	e of Ru	noff:			C =	0%
	V <sub>360</sub>	=		1170	CF	D =	13%
	Sub-basin Peak D	ischarg	e Rate:			Stormwate	er Quality Volume
	Q <sub>P</sub>	=		0.8	cfs	<u> </u>	36 CF
BASIN NO. 3			DESCRI	PTION		Self Pond	ling
Area of basin flows =	28717	SF			=	0.7 Ac.	
						LAND TR	EATMENT
	Sub-basin Weight	ted Exc	ess Precip	itation:		A =	0%
	Weighted E	=		1.08 i	n.	$\mathbf{B} =$	87%
	Sub-basin Volum	e of Ru	noff:			C =	0%
	V <sub>360</sub>	=		2593	CF	D =	13%
	Sub-basin Peak D	oischarg	e Rate:			Stormwate	er Quality Volume
	Q <sub>P</sub>	=		1.8	cfs		81 CF
BASIN NO. 4			DESCRI	PTION			
Area of basin flows =	157805	SF			=	3.6 Ac.	
						LAND TR	EATMENT
	Sub-basin Weight	ted Exc	ess Precip	itation:		A =	0%
	Weighted E	=		1.08 i	n.	$\mathbf{B} =$	87%
	Sub-basin Volum	e of Ru	noff:			C =	0%
	V <sub>360</sub>	=		14250	CF	D =	13%
	Sub-basin Peak D	ischarg	ge Rate:			Stormwate	er Quality Volume
	Q <sub>P</sub>	=		10.0	cfs		444 CF
BASIN NO. 5			DESCRI	PTION			
Area of basin flows =	24304	SF			=	0.6 Ac.	
						LAND TR	EATMENT
	Sub-basin Weight	ted Exc	ess Precip	itation:		A =	0%
	Weighted E	=		1.08 i	n.	$\mathbf{B} =$	87%
	Sub-basin Volum	e of Ru	noff:			C =	0%
	V <sub>360</sub>	=		2195	CF	D =	13%
	Sub-basin Peak D	ischarg	e Rate:			Stormwate	er Quality Volume
	Q <sub>P</sub>	=		1.5	cfs		68 CF

BASIN NO. 6			DESCRI	PTION			
Area of basin flows =	38718	SF			=	0.9 Ac.	
						LAND TRE	EATMENT
	Sub-basin Weight	ed Exc	ess Precip	oitation:		A =	0%
	Weighted E	=		1.08 i	n.	$\mathbf{B} =$	87%
	Sub-basin Volum	e of Ru	inoff:			C =	0%
	V <sub>360</sub>	=		3496	CF	D =	13%
	Sub-basin Peak D	ischarg	ge Rate:			Stormwater	Quality Volume
	Q <sub>P</sub>	=		2.5	cfs		109 CF
BASIN NO. 7			DESCRI	PTION			
Area of basin flows =	84544	SF			=	1.9 Ac.	
						LAND TRE	EATMENT
	Sub-basin Weight	ed Exc	ess Precip	oitation:		A =	0%
	Weighted E	=		1.08 i	n.	B =	87%
	Sub-basin Volum	e of Ru	inoff:			C =	0%
	V <sub>360</sub>	=		7634	CF	D =	13%
	Sub-basin Peak D	ischarg	ge Rate:			Stormwater	Quality Volume
	Q <sub>P</sub>	=		5.3	cfs		238 CF
BASIN NO. 8			DESCRI	PTION			
Area of basin flows =	22515	SF			=	0.5 Ac.	
						LAND TRE	EATMENT
	Sub-basin Weight	ed Exc	ess Precip	oitation:		A =	0%
	Weighted E	=		1.08 i	n.	B =	87%
	Sub-basin Volum	e of Ru	inoff:			C =	0%
	V <sub>360</sub>	=		2033	CF	D =	13%
	Sub-basin Peak D	ischarg	ge Rate:			Stormwater	Quality Volume
	Q <sub>P</sub>	=		1.4	cfs		63 CF
BASIN NO. 9			DESCRI	PTION			
Area of basin flows =	153154	SF			=	3.5 Ac.	
						LAND TRI	EATMENT
	Sub-basin Weight	ed Exc	ess Precip	oitation:		A =	0%
	Weighted E	=	00	1.08 i	n.	B =	87%
	Sub-basin Volum	e of Ru	inoff:	10000	~ 7	C =	0%
	V <sub>360</sub>	=	<b>D</b> .	13830	CF	D =	13%
	Sub-basin Peak D	ischarg	ge Rate:	~ <b>-</b>	0	Stormwater	Quality Volume
	Q <sub>P</sub>	=		9.7	cts		431 CF
BASIN NO. 10			DESCRI	PTION			
Area of basin flows =	127173	SF			=	2.9 Ac.	
	011 1 107 11	1 5	р <sup>.</sup>	•, ,•		LAND TRE	EATMENT
	Sub-basin Weight	ed Exc	ess Precip	oitation:		A =	0%
	Weighted E	=		1.08 1	n.	B =	8 / %0
	Sub-basin Volum	e of Ku	inoII:	11494	CE	C =	U%0 120/
	V <sub>360</sub>	=	Date:	11484	UF	D =	13%
	Sub-basin Peak D	ischarg	ge Kate:	0.0	C	Stormwater	Quality Volume
	$Q_P$	=		8.0	cis		358 CF

10-yr, 6-hr

BASIN NO. 1		DESCRI	<b>PTION</b>		To Southern	Ave.
Area of basin flows =	61484	SF		=	1.41 Ac.	
					LAND TR	EATMENT
	Sub-basin Weight	ted Excess Precip	pitation:		A =	0%
	Weighted E	=	1.02 i	n.	$\mathbf{B} =$	48%
	Sub-basin Volum	e of Runoff:			C =	0%
	V <sub>360</sub>	=	5206	CF	D =	52%
	Sub-basin Peak D	ischarge Rate:				
	Q <sub>P</sub>	=	2.8	cfs		
BASIN NO. 2		DESCRI	IPTION		Self Pond	ing
Area of basin flows =	12954	SF		=	0.3 Ac.	
					LAND TR	EATMENT
	Sub-basin Weight	ted Excess Precip	pitation:		A =	0%
	Weighted E	=	0.51 i	n.	$\mathbf{B} =$	87%
	Sub-basin Volum	e of Runoff:			C =	0%
	V <sub>360</sub>	=	549	CF	D =	13%
	Sub-basin Peak D	ischarge Rate:				
	Q <sub>P</sub>	=	0.4	cfs		
BASIN NO. 3		DESCRI	IPTION		Self Pond	ing
Area of basin flows =	28717	SF		=	0.7 Ac.	
					LAND TR	EATMENT
	Sub-basin Weight	ted Excess Precip	pitation:		A =	0%
	Weighted E	=	0.51 i	n.	$\mathbf{B} =$	87%
	Sub-basin Volum	e of Runoff:			C =	0%
	V <sub>360</sub>	=	1218	CF	D =	13%
	Sub-basin Peak D	ischarge Rate:				
	Q <sub>P</sub>	=	0.9	cfs		
BASIN NO. 4		DESCRI	<b>IPTION</b>			
Area of basin flows =	157805	SF		=	3.6 Ac.	
					LAND TR	EATMENT
	Sub-basin Weight	ted Excess Precip	pitation:		A =	0%
	Weighted E	=	0.51 i	n.	$\mathbf{B} =$	87%
	Sub-basin Volum	e of Runoff:			C =	0%
	V <sub>360</sub>	=	6694	CF	D =	13%
	Sub-basin Peak D	ischarge Rate:				
	Q <sub>P</sub>	=	4.7	cfs		
BASIN NO. 5		DESCRI	IPTION			
Area of basin flows =	24304	SF		=	0.6 Ac.	
					LAND TR	EATMENT
	Sub-basin Weight	ted Excess Precip	pitation:		A =	0%
	Weighted E	=	0.51 i	n.	$\mathbf{B} =$	87%
	Sub-basin Volum	e of Runoff:			C =	0%
	V <sub>360</sub>	=	1031	CF	D =	13%
	Sub-basin Peak D	ischarge Rate:			-	
	Q <sub>P</sub>	=	0.7	cfs		

BASIN NO. 6		DESCR	IPTION			
Area of basin flows =	38718	SF		=	0.9 Ac.	
					LAND TR	REATMENT
	Sub-basin Weight	ed Excess Prec	ipitation:		A =	0%
	Weighted E	=	0.51	in.	B =	87%
	Sub-basin Volum	e of Runoff:			C =	0%
	V <sub>360</sub>	=	1642	CF	D =	13%
	Sub-basin Peak D	ischarge Rate:				
	Qp	=	1.2	cfs		
BASIN NO. 7	·	DESCR	IPTION			
Area of basin flows =	84544	SF		=	1.9 Ac.	
					LAND TR	REATMENT
	Sub-basin Weight	ed Excess Prec	ipitation:		A =	0%
	Weighted E	=	0.51	in.	$\mathbf{B} =$	87%
	Sub-basin Volum	e of Runoff:			C =	0%
	V <sub>360</sub>	=	3586	CF	D =	13%
	Sub-basin Peak D	ischarge Rate:				
	Q <sub>P</sub>	=	2.5	cfs		
BASIN NO. 8		DESCR	IPTION			
Area of basin flows =	22515	SF		=	0.5 Ac.	
					LAND TR	EATMENT
	Sub-basin Weight	ed Excess Prec	ipitation:		A =	0%
	Weighted E	=	0.51	in.	$\mathbf{B} =$	87%
	Sub-basin Volum	e of Runoff:			C =	0%
	V <sub>360</sub>	=	955	CF	D =	13%
	Sub-basin Peak D	ischarge Rate:			Stormwate	er Quality Volume
	Q <sub>P</sub>	=	0.7	cfs	. <u></u>	0 CF
BASIN NO. 9		DESCR	IPTION			
Area of basin flows =	153154	SF		=	3.5 Ac.	
					LAND TR	REATMENT
	Sub-basin Weight	ed Excess Prec	ipitation:		A =	0%
	Weighted E	=	0.51	in.	$\mathbf{B} =$	87%
	Sub-basin Volum	e of Runoff:			C =	0%
	V <sub>360</sub>	=	6496	CF	D =	13%
	Sub-basin Peak D	ischarge Rate:				
	Q <sub>P</sub>	=	4.6	cfs		
BASIN NO. 10		DESCR	IPTION			
Area of basin flows =	127173	SF		=	2.9 Ac.	
					LAND TR	EATMENT
	Sub-basin Weight	ed Excess Prec	ipitation:		A =	0%
	Weighted E	=	0.51	in.	$\mathbf{B} =$	87%
	Sub-basin Volum	e of Runoff:			C =	0%
	V <sub>360</sub>	=	5394	CF	D =	13%
	Sub-basin Peak D	ischarge Rate:				
	Q <sub>P</sub>	=	3.8	cfs		

BASIN SUMMARY						
Basin No.	Description	Q 100 (CFS)	Q10 (CFS)	SWQV (CF)		
1	To Southern Ave.	5.0	2.8	693		
2	Self Ponding	0.8	0.4	36		
3	Self Ponding	1.8	0.9	81		
4	To SW Offsite Pond	10.0	4.7	444		
5	To SW Offsite Pond	1.5	0.7	68		
6	To Rundown	2.5	1.2	109		
7	To Storm Drain	5.3	2.5	238		
8	To Storm Drain	1.4	0.7	63		
9	To Storm Drain	9.7	4.6	431		
10	To Storm Drain	8.0	3.8	358		
TOTAL		46.0	22.3	2,523		

24.4

Total to Storm Drain

11.6 cfs (12.8 cfs bypass)

Total Q to Rundown

**14.1** cfs (=11.6+2.5)

SWQ POND EAST OF BASKETBALL COURT				
Contour	Area	Volume		
50.5	842			
52.0	1400	1682 CF		
POND VO	LUME =	1682 CF		

SWQ POND NORTH OF BASKETBALI COURT				
Contour	Area	Volume		
50.0	558			
50.6	2130	806 CF		
POND VO	LUME =	<b>806</b> CF		

# **APPENDIX B**

Rundown Calculations Storm Drain Calculations Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

# **RUNDOWN SOUTH OF BASKETBALL COURT**

Trapezoidal		Highlighted	
Bottom Width (ft)	= 4.00	Depth (ft)	= 0.78
Side Slopes (z:1)	= 3.00, 3.00	Q (cfs)	= 14.10
Total Depth (ft)	= 1.00	Area (sqft)	= 4.95
Invert Elev (ft)	= 100.00	Velocity (ft/s)	= 2.85
Slope (%)	= 1.00	Wetted Perim (ft)	= 8.93
N-Value	= 0.035	Crit Depth, Yc (ft)	= 0.62
		Top Width (ft)	= 8.68
Calculations		EGL (ft)	= 0.91
Compute by:	Known Q		
Known Q (cfs)	= 14.10		



Reach (ft)



Project Name: Enter Project Name..2573 SD-10YR.

04-12-2023



Project Name: Enter Project Name..2573 SD-10YR.





Project Name: Enter Project Name..2573 SD-10YR.

Profile View





Project File: 2573 SD-10 YEAR.sws

**Profile View** 









Project Name: Enter Project Name..2573 SD-10YR.





Project Name: Enter Project Name..2573 SD-10YR.

04-12-2023



Project Name: Enter Project Name..2573 SD-10YR.

04-12-2023



**Profile View** 

Project Name: Enter Project Name..2573 SD-10YR.

04-12-2023



**Profile View** 

Project Name: Enter Project Name..2573 SD-10YR.

04-12-2023



# Energy Grade Line Calculations

Project Name: Enter Project Name..2573 SD-10YR.

04-12-2023

67     51.83     0.012     0.659     51.45     5       30     53.52     0.012     0.659     51.45     5       30     53.52     0.012     1.282     53.28     5       30     53.52     0.012     0.557     53.38     5     5       39     58.15     0.012     0.012     0.267     53.83     5		HGL Vel Ve Elev (ft) (ft/s) ((	epth Area HGL Vei Ve (ft) (sqft) (ft) (ft)s) (	Invert Depth Area HGL Vel H Elev (ft) (ft) (sqft) (ft) (ft) ((11/s) (	Lengt Lengt Elev Depth Area HGL Vel Vel H Hft (ft) (sqft) (ft) (ft) (ft) (tt/s) (	EGL L Hivert Depth Area HGL Vel H (ft) (ft) (ft) (sqft) (ft) (ft) (ft) (ft) (ft) (ft) (ft) (	Vel EGL en   Vel EGL L   Invert Depth Area   Head Elev Depth   (ff) (ff) (ff)   (ff) (ff) (ff)	Vel Vel EGL L Invert Depth Area Elev Vel H. (ft) (ft) (sqft) (ft) (ft) (ft) (sqft) (ft) (ft) (ft) (sqft) (ft) (ft) (ft) (ft) (ft) (ft) (ft) (	HGL Vel Vel EGL Len Elev Depth Area HGL Vel H Elev (ft) (ft) (ft) (ft) (ft) (ft) (ft) (ft)	Area HGL Vel Vel EGL L Invert Depth Area HGL Vel	Depth Area HGL Vel EGL L   Invert Depth Area HGL Vel Vel   Invert Elev Depth Area HGL Vel   Invert Elev Depth Area HGL Vel   Invert Invert Depth Area HGL Vel   Invert Invert Depth Area HGL Vel	Invert Depth Area HGL Vel Vel EGL L Invert Depth Area HGL Vel Vel HGL (ft) (ft) (sqft) (ft) (ft) (ft) (ft) (ft) (ft) (ft) (	Q Big Big   Invert Depth Area HGL Vel EGL Edl Invert Depth Area HGL Vel Vel Edl Vel <t< th=""></t<>
0.30     53.52     0.012     1.282     53.28       0.06     53.70     0.012     0.086     53.64     5       0.026     53.94     0.012     0.267     53.83     5       0.20     53.94     0.012     0.267     53.83     5       0.20     58.15     0.012     0.267     53.83     5       0.07     58.28     0.012     0.111     58.23     5       0.07     58.33     0.012     0.111     58.23     5       0.07     58.33     0.012     0.111     58.23     5     5       0.07     60.46     0.012     0.123     5     5     5     5       0.07     60.46     0.012     0.169     60.43     6	6.56 0	51.16	1.50 1.77 51.16	49.40 1.50 1.77 51.16	63.36     49.40     1.50     1.77     51.16	51.17 63.36 49.40 1.50 1.77 51.16	0.67 51.17 63.36 49.40 1.50 1.77 51.16	6.57     0.67     51.17     63.36     49.40     1.50     1.77     51.16	50.50     6.57     0.67     51.17     63.36     49.40     1.50     1.77     51.16	1.77     50.50     6.57     0.67     51.17     63.36     49.40     1.50     1.77     51.16	1.50 <sup>3</sup> 1.77     50.50     6.57     0.67     51.17     63.36     49.40     1.50     1.77     51.16	49.00     1.50 <sup>3</sup> 1.77     50.50     6.57     0.67     51.17     63.36     49.40     1.50     1.77     51.16	11.60     49.00     1.50 <sup>3</sup> 1.77     50.50     6.57     0.67     51.17     63.36     49.40     1.50     1.77     51.16
0.06   53.70   0.012   0.086   53.64     0.26   53.94   0.012   0.257   53.83     0.38   58.15   0.012   3.960   57.76     0.05   58.28   0.012   0.012   53.83     0.06   58.28   0.012   0.012   58.28     0.05   58.33   0.012   0.013   58.33     0.06   58.33   0.012   0.013   58.31     0.07   60.37   0.012   0.013   58.31     0.01   60.01   0.012   1.523   59.76     0.11   60.20   0.012   0.199   60.31     0.01   60.46   0.013   0.025   60.43     0.00   60.69   0.012   0.213   60.65     0.00   59.91   0.012   0.213   60.65     0.00   59.31   60.65   60.61     0.00   59.91   0.012   0.213   60.65     0.00   59.14   60.66   60.65   6     0.00   59.14   58.31   5	2 4.41 0	53.22	1.50 1.77 53.22	51.20 1.50 1.77 53.22	272.58 51.20 1.50 1.77 53.22	52.24 272.58 51.20 1.50 1.77 53.22	0.30 52.24 272.58 51.20 1.50 1.77 53.22	4.41     0.30     52.24     272.58     51.20     1.50     1.77     53.22	51.93     4.41     0.30     52.24     272.58     51.20     1.50     1.77     53.22	1.77     51.93     4.41     0.30     52.24     272.58     51.20     1.50     1.77     53.22	1.50     1.77     51.93     4.41     0.30     52.24     272.58     51.20     1.50     1.77     53.22	49.40     1.50     1.77     51.93     4.41     0.30     52.24     272.58     51.20     1.50     1.77     53.22	7.80     49.40     1.50     1.77     51.93     4.41     0.30     52.24     272.58     51.20     1.50     1.77     53.25
0.26   53.94   0.012   0.257   53.83   5     0.39   58.15   0.012   3.960   57.76   5     0.07   58.28   0.012   3.960   57.76   5     0.05   58.33   0.012   0.013   58.33   5     0.06   58.33   0.012   0.013   58.31   5     0.05   58.33   0.012   1.523   58.31   5     0.11   60.37   0.012   1.523   58.31   5     0.11   60.37   0.012   1.523   58.31   5     0.01   60.46   0.012   0.287   60.43   6     0.01   60.46   0.012   0.169   60.65   6     0.00   60.46   0.012   0.213   60.65   6     0.00   59.91   0.012   0.213   60.65   6     0.00   59.91   0.012   0.780   60.65   6     0.00   59.14   0.012   0.780   60.65   6     0.00   59.14   59.14	2.04 0	53.63	1.00 0.79 53.63	51.70 1.00 0.79 53.63	49.98 51.70 1.00 0.79 53.63	53.61     49.98     51.70     1.00     0.79     53.63	0.06 53.61 49.98 51.70 1.00 0.79 53.63	2.04     0.06     53.61     49.98     51.70     1.00     0.79     53.63	53.54     2.04     0.06     53.61     49.98     51.70     1.00     0.79     53.63	0.79     53.54     2.04     0.06     53.61     49.98     51.70     1.00     0.79     53.63	1.00     0.79     53.54     2.04     0.06     53.61     49.98     51.70     1.00     0.79     53.63	51.20     1.00     0.79     53.54     2.04     0.06     53.61     49.98     51.70     1.00     0.79     53.63	1.60     51.20     1.00     0.79     53.54     2.04     0.06     53.61     49.98     51.70     1.00     0.79     53.63
0.39   58.15   0.012   3.960   57.76   5     0.007   58.28   0.012   0.111   58.23   5     0.005   58.33   0.012   0.111   58.23   5     0.015   58.33   0.012   0.111   58.33   5     0.016   59.90   0.012   1.523   58.31   5     0.11   60.20   0.012   1.523   59.76   5     0.11   60.20   0.012   0.169   60.09   6     0.017   60.46   0.012   0.169   60.43   6     0.016   60.46   0.012   0.169   60.43   6     0.015   60.69   0.012   0.199   60.65   6     0.016   60.69   0.012   0.213   60.65   6     0.010   59.91   0.012   0.780   60.65   6     0.020   59.14   0.012   0.201   59.30   6     0.030   59.76   59.14   5   5   5     0.030   59.76   59.14	4.07 0	53.69	1.00 0.79 53.69	51.80 1.00 0.79 53.69	37.37 51.80 1.00 0.79 53.69	53.69 37.37 51.80 1.00 0.79 53.69	0.26 53.69 37.37 51.80 1.00 0.79 53.69	4.08     0.26     53.69     37.37     51.80     1.00     0.79     53.69	53.43     4.08     0.26     53.69     37.37     51.80     1.00     0.79     53.69	0.79     53.43     4.08     0.26     53.69     37.37     51.80     1.00     0.79     53.69	1.00     0.79     53.43     4.08     0.26     53.69     37.37     51.80     1.00     0.79     53.69	51.20     1.00     0.79     53.43     4.08     0.26     53.69     37.37     51.80     1.00     0.79     53.69	3.20     51.20     1.00     0.79     53.43     4.08     0.26     53.69     37.37     51.80     1.00     0.79     53.69
0.07   58.28   0.012   0.111   58.23     0.06   58.33   0.012   0.013   58.31   5     0.05   58.33   0.012   1.523   59.76   5     0.15   59.90   0.012   1.523   59.76   5     0.11   60.20   0.012   1.523   59.76   5     0.11   60.20   0.012   0.169   60.37   60.09   5     0.01   60.46   0.013   0.287   60.09   6   6     0.00   60.69   0.012   0.199   60.65   6   6     0.01   59.91   0.012   0.213   60.65   6   6     0.01   59.91   0.012   0.213   60.65   6   6     0.02   59.91   0.012   0.213   60.65   6   6     0.01   59.91   0.012   0.203   59.14   6   6     0.036   59.76   0.012   0.203   59.14   6   6     0.036   53.06   0.012   0.203 <td>5.01 0</td> <td>57.76</td> <td>0.762 0.64 57.76</td> <td>57.00 0.76<sup>2</sup> 0.64 57.76</td> <td>310.82 57.00 0.76<sup>2</sup> 0.64 57.76</td> <td>54.19     310.82     57.00     0.76<sup>2</sup>     0.64     57.76</td> <td>0.26 54.19 310.82 57.00 0.76<sup>2</sup> 0.64 57.76</td> <td>4.08     0.26     54.19     310.82     57.00     0.76<sup>2</sup>     0.64     57.76</td> <td>53.93     4.08     0.26     54.19     310.82     57.00     0.76<sup>2</sup>     0.64     57.76</td> <td>0.79     53.93     4.08     0.26     54.19     310.82     57.00     0.76<sup>2</sup>     0.64     57.76</td> <td>1.00     0.79     53.93     4.08     0.26     54.19     310.82     57.00     0.76<sup>2</sup>     0.64     57.76</td> <td>51.80     1.00     0.79     53.93     4.08     0.26     54.19     310.82     57.00     0.76<sup>2</sup>     0.64     57.76</td> <td>3.20     51.80     1.00     0.79     53.93     4.08     0.26     54.19     310.82     57.00     0.76<sup>2</sup>     0.64     57.76</td>	5.01 0	57.76	0.762 0.64 57.76	57.00 0.76 <sup>2</sup> 0.64 57.76	310.82 57.00 0.76 <sup>2</sup> 0.64 57.76	54.19     310.82     57.00     0.76 <sup>2</sup> 0.64     57.76	0.26 54.19 310.82 57.00 0.76 <sup>2</sup> 0.64 57.76	4.08     0.26     54.19     310.82     57.00     0.76 <sup>2</sup> 0.64     57.76	53.93     4.08     0.26     54.19     310.82     57.00     0.76 <sup>2</sup> 0.64     57.76	0.79     53.93     4.08     0.26     54.19     310.82     57.00     0.76 <sup>2</sup> 0.64     57.76	1.00     0.79     53.93     4.08     0.26     54.19     310.82     57.00     0.76 <sup>2</sup> 0.64     57.76	51.80     1.00     0.79     53.93     4.08     0.26     54.19     310.82     57.00     0.76 <sup>2</sup> 0.64     57.76	3.20     51.80     1.00     0.79     53.93     4.08     0.26     54.19     310.82     57.00     0.76 <sup>2</sup> 0.64     57.76
0.05   58.33   0.012   0.013   58.31     0.15   59.90   0.012   1.523   59.76     0.11   60.20   0.012   1.523   59.76     0.11   60.37   0.012   0.287   60.09     0.11   60.37   0.012   0.287   60.09     0.07   60.46   0.013   0.085   60.43     0.06   60.69   0.012   0.199   60.63     0.00   60.69   0.012   0.273   60.43     0.01   59.91   0.012   0.213   60.65     0.00   60.69   0.012   0.213   60.65     0.00   59.91   0.012   0.213   60.65     0.00   58.30   0.012   0.780   60.65     0.00   59.76   0.012   0.780   60.65     0.36   59.76   0.012   0.780   59.30     0.36   59.74   59.30   59.14   59.14	2.07 0	58.22	0.62 0.34 58.22	57.60 0.62 0.34 58.22	41.62 57.60 0.62 0.34 58.22	58.17     41.62     57.60     0.62     0.34     58.22	0.06 58.17 41.62 57.60 0.62 0.34 58.22	2.01     0.06     58.17     41.62     57.60     0.62     0.34     58.22	58.11     2.01     0.06     58.17     41.62     57.60     0.62     0.34     58.22	0.35     58.11     2.01     0.06     58.17     41.62     57.60     0.62     0.34     58.22	0.67 0.35 58.11 2.01 0.06 58.17 41.62 57.60 0.62 0.34 58.22	57.00     0.67     0.35     58.11     2.01     0.06     58.17     41.62     57.60     0.62     0.34     58.22	0.70 57.00 0.67 0.35 58.11 2.01 0.06 58.17 41.62 57.60 0.62 0.34 58.22
0.15   59.90   0.012   1.523   59.76   5     0.11   60.20   0.012   0.287   60.09   6     0.07   60.37   0.012   0.287   60.09   6     0.07   60.46   0.012   0.287   60.09   6     0.07   60.46   0.012   0.279   60.43   6     0.05   60.69   0.012   0.273   60.65   6     0.00   60.69   0.012   0.213   60.65   6     0.00   60.69   0.012   0.213   60.65   6     0.01   59.91   0.012   0.213   60.65   6     0.00   58.30   0.012   0.780   60.65   6     0.00   58.30   0.012   0.780   59.90   5     0.01   59.91   0.012   0.780   59.90   5     0.36   59.76   0.012   0.780   59.14   5     0.36   53.06   0.012   0.800   59.14   5	1.87 0	58.28	0.32 58.28	57.70 0.58 0.32 58.28	6.71     57.70     0.58     0.32     58.28	58.32 6.71 57.70 0.58 0.32 58.28	0.05 58.32 6.71 57.70 0.58 0.32 58.28	1.72     0.05     58.32     6.71     57.70     0.58     0.32     58.28	58.27     1.72     0.05     58.32     6.71     57.70     0.58     0.32     58.28	0.35 58.27 1.72 0.05 58.32 6.71 57.70 0.58 0.32 58.28	0.67 0.35 58.27 1.72 0.05 58.32 6.71 57.70 0.58 0.32 58.28	57.60     0.67     0.35     58.27     1.72     0.05     58.32     6.71     57.70     0.58     0.32     58.28	0.60     57.60     0.67     0.35     58.27     1.72     0.05     58.32     6.71     57.70     0.58     0.32     58.28
0.11   60.20   0.012   0.287   60.09   6     0.07   60.37   0.012   0.169   60.30   6     0.07   60.46   0.013   0.085   60.43   6     0.07   60.46   0.012   0.169   60.43   6     0.07   60.48   0.012   0.199   60.65   6     0.06   60.69   0.012   0.233   60.65   6     0.005   60.69   0.012   0.213   60.65   6     0.01   59.91   0.012   0.213   60.65   6     0.01   59.91   0.012   0.213   60.65   6     0.02   60.69   0.012   0.780   60.65   6     0.03   59.76   0.012   0.780   59.14   5     0.36   53.06   0.012   0.800   59.14   5     0.36   53.06   0.012   0.800   59.14   5	3 3.07 0	59.7(	).37 <sup>2</sup> 0.20 59.70	59.39 0.37 <sup>2</sup> 0.20 59.7	47.58 59.39 0.37 <sup>2</sup> 0.20 59.7	58.38     47.58     59.39     0.37 <sup>2</sup> 0.20     59.70	0.05 58.38 47.58 59.39 0.37 <sup>2</sup> 0.20 59.7	1.76     0.05     58.38     47.58     59.39     0.37 <sup>2</sup> 0.20     59.71	58.33     1.76     0.05     58.38     47.58     59.39     0.37 <sup>2</sup> 0.20     59.7	0.34     58.33     1.76     0.05     58.38     47.58     59.39     0.37 <sup>2</sup> 0.20     59.70	0.63 0.34 58.33 1.76 0.05 58.38 47.58 59.39 0.37 <sup>2</sup> 0.20 59.7	57.70     0.63     0.34     58.33     1.76     0.05     58.38     47.58     59.39     0.37 <sup>2</sup> 0.20     59.71	0.60     57.70     0.63     0.34     58.33     1.76     0.05     58.38     47.58     59.39     0.37 <sup>2</sup> 0.20     59.71
0.07   60.37   0.012   0.169   60.30     0.07   60.46   0.013   0.085   60.43   6     0.06   60.69   0.012   0.199   60.65   6     0.07   60.48   0.012   0.199   60.65   6     0.07   60.69   0.012   0.279   60.65   6     0.06   60.69   0.012   0.213   60.65   6     0.05   60.69   0.012   0.213   60.65   6     0.06   60.69   0.012   0.213   60.65   6     0.005   60.69   0.012   0.202   59.90   6   6     0.005   58.30   0.012   0.780   60.65   6   6     0.000   58.30   0.012   0.203   59.14   5   6   6     0.36   53.06   0.012   0.800   52.72   5   6   6	09 2.65 C	30.	0.30 <sup>2</sup> 0.15 60.	59.79 0.30 <sup>2</sup> 0.15 60.	40.33 59.79 0.30 <sup>2</sup> 0.15 60.	59.91     40.33     59.79     0.30 <sup>2</sup> 0.15     60.	0.03 59.91 40.33 59.79 0.30 <sup>2</sup> 0.15 60.	1.46     0.03     59.91     40.33     59.79     0.30 <sup>2</sup> 0.15     60.	59.88     1.46     0.03     59.91     40.33     59.79     0.30 <sup>2</sup> 0.15     60.	0.27     59.88     1.46     0.03     59.91     40.33     59.79     0.30 <sup>2</sup> 0.15     60.	0.49     0.27     59.88     1.46     0.03     59.91     40.33     59.79     0.30 <sup>2</sup> 0.15     60.	59.39     0.49     0.27     59.88     1.46     0.03     59.91     40.33     59.79     0.30 <sup>2</sup> 0.15     60.	0.40     59.39     0.49     0.27     59.88     1.46     0.03     59.91     40.33     59.79     0.30 <sup>2</sup> 0.15     60.
0.07   60.46   0.013   0.085   60.43   60.43     0.05   60.69   0.012   0.199   60.65   6     0.07   60.48   0.012   0.279   60.65   6     0.06   60.69   0.012   0.213   60.65   6     0.01   59.91   0.012   0.213   60.65   6     0.01   59.91   0.012   0.213   60.65   6     0.01   59.91   0.012   0.780   60.65   6     0.00   58.30   0.012   0.780   60.65   6     0.00   58.30   0.012   1.290   58.30   6     0.80   59.76   0.012   1.290   59.14   6     0.36   53.06   0.012   0.800   59.14   6	0.30 2.11 0	0	0.212 0.09 6	60.09 0.21 <sup>2</sup> 0.09 6	29.67 60.09 0.21 <sup>2</sup> 0.09 6	60.20     29.67     60.09     0.21 <sup>2</sup> 0.09     6	0.01 60.20 29.67 60.09 0.21 <sup>2</sup> 0.09 6	0.92 0.01 60.20 29.67 60.09 0.21 <sup>2</sup> 0.09 6	60.19     0.92     0.01     60.20     29.67     60.09     0.21 <sup>2</sup> 0.09     6	0.22 60.19 0.92 0.01 60.20 29.67 60.09 0.21 <sup>2</sup> 0.09 6	0.40 0.22 60.19 0.92 0.01 60.20 29.67 60.09 0.21 <sup>2</sup> 0.09 6	59.79     0.40     0.22     60.19     0.92     0.01     60.20     29.67     60.09     0.21 <sup>2</sup> 0.09     6	0.20 59.79 0.40 0.22 60.19 0.92 0.01 60.20 29.67 60.09 0.21 <sup>2</sup> 0.09 6
0.05   60.69   0.012   0.139   60.65     0.07   60.48   0.012   0.279   60.41   6     0.05   60.69   0.012   0.213   60.65   6     0.05   60.69   0.012   0.213   60.65   6     0.01   59.91   0.012   0.213   60.65   6     0.01   59.91   0.012   0.780   60.65   6     0.00   58.30   0.012   0.780   60.65   6     0.00   58.30   0.012   0.780   59.14   6     0.80   59.76   0.012   1.290   59.14   6     0.36   53.06   0.012   0.800   59.14   6     0.36   53.06   0.012   0.800   52.72   5	i0.39 2.09 0	(()	0.21 0.10 6	60.18 0.21 0.10 6	8.75 60.18 0.21 0.10 6	60.38     8.75     60.18     0.21     0.10     6	0.09 60.38 8.75 60.18 0.21 0.10 6	2.37     0.09     60.38     8.75     60.18     0.21     0.10     6	60.28     2.37     0.09     60.38     8.75     60.18     0.21     0.10     6	0.08     60.28     2.37     0.09     60.38     8.75     60.18     0.21     0.10     6	0.19‡     0.08     60.28     2.37     0.09     60.38     8.75     60.18     0.21     0.10     6	60.09     0.19‡     0.08     60.28     2.37     0.09     60.38     8.75     60.18     0.21     0.10     6	0.20     60.09     0.19‡     0.08     60.28     2.37     0.09     60.38     8.75     60.18     0.21     0.10     6
0.07   60.48   0.012   0.279   60.41   6     0.05   60.69   0.012   0.213   60.65   6     0.01   59.91   0.012   0.213   60.65   6     0.01   59.91   0.012   0.02   59.90   5     0.00   58.30   0.012   0.02   59.90   5     0.00   58.30   0.012   1.290   58.30   5     0.80   59.76   0.012   1.290   58.30   5     0.36   59.76   0.012   1.290   59.14   5     0.36   53.06   0.012   0.800   59.14   5	65 1.72 0	30.	0.15 <sup>2</sup> 0.06 60.	60.50 0.15 <sup>2</sup> 0.06 60.	40.00 60.50 0.15 <sup>2</sup> 0.06 60.	60.50     40.00     60.50     0.15 <sup>2</sup> 0.06     60	0.06 60.50 40.00 60.50 0.15 <sup>2</sup> 0.06 60	2.00     0.06     60.50     40.00     60.50     0.15 <sup>2</sup> 0.06     60	60.31     2.00     0.06     60.50     40.00     60.50     0.15 <sup>2</sup> 0.06     60	0.05 60.31 2.00 0.06 60.50 40.00 60.50 0.15 <sup>2</sup> 0.06 60.	0.13 0.05 60.31 2.00 0.06 60.50 40.00 60.50 0.15 0.06 60.	60.18     0.13‡     0.05     60.31     2.00     0.06     60.50     40.00     60.50     0.15²     0.06     60	0.10 60.18 0.13‡ 0.05 60.31 2.00 0.06 60.50 40.00 60.50 0.15 <sup>2</sup> 0.06 60
0.05   60.69   0.012   0.213   60.65   6     0.01   59.91   0.012   0.02   59.90   5     0.01   59.91   0.012   0.02   59.90   5     0.05   60.69   0.012   0.780   60.65   6     0.00   58.30   0.012   0.780   60.65   6     0.00   58.30   0.012   1.290   58.30   5     0.80   59.76   0.012   1.290   59.14   5     0.36   53.06   0.012   1.290   59.14   5	41 2.11 0	30.	0.212 0.09 60.	60.20 0.21 <sup>2</sup> 0.09 60.	16.82     60.20     0.21 <sup>2</sup> 0.09     60.	60.20     16.82     60.20     0.21 <sup>2</sup> 0.09     60.	0.01 60.20 16.82 60.20 0.21 <sup>2</sup> 0.09 60.	0.92 0.01 60.20 16.82 60.20 0.21 <sup>2</sup> 0.09 60.	60.19     0.92     0.01     60.20     16.82     60.20     0.21 <sup>2</sup> 0.09     60	0.22 60.19 0.92 0.01 60.20 16.82 60.20 0.21 <sup>2</sup> 0.09 60	0.40 0.22 60.19 0.92 0.01 60.20 16.82 60.20 0.21 <sup>2</sup> 0.09 60	59.79     0.40     0.22     60.19     0.92     0.01     60.20     16.82     60.21 <sup>2</sup> 0.09     60	0.20     59.79     0.40     0.22     60.19     0.92     0.01     60.20     16.82     60.20     0.21 <sup>2</sup> 0.09     60
0.01   59.91   0.012   0.002   59.90   59.90     0.05   60.69   0.012   0.780   60.65   6     0.000   58.30   0.012   0.780   60.65   6     0.000   58.30   0.012   1.290   58.30   6   6     0.010   59.76   0.012   1.290   59.14   6	0.65 1.72 0	8	0.15 <sup>2</sup> 0.06 60	60.50 0.15 <sup>2</sup> 0.06 60	12.70 60.50 0.15 <sup>2</sup> 0.06 60	60.48     12.70     60.50     0.15 <sup>2</sup> 0.06     60	0.01 60.48 12.70 60.50 0.15 <sup>2</sup> 0.06 60	0.71 0.01 60.48 12.70 60.50 0.15 <sup>2</sup> 0.06 60	60.47     0.71     0.01     60.48     12.70     60.50     0.15 <sup>2</sup> 0.06     60	0.14 60.47 0.71 0.01 60.48 12.70 60.50 0.15 <sup>2</sup> 0.06 60	0.28 0.14 60.47 0.71 0.01 60.48 12.70 60.50 0.15 <sup>2</sup> 0.06 60	60.19     0.28     0.14     60.47     0.71     0.01     60.48     12.70     60.50     0.15 <sup>2</sup> 0.06     60	0.10     60.19     0.28     0.14     60.47     0.71     0.01     60.48     12.70     60.50     0.15 <sup>2</sup> 0.06     60
0.05   60.69   0.012   0.780   60.65     0.00   58.30   0.012   0.001   58.30     0.036   59.76   0.012   1.290   59.14     0.36   53.06   0.012   0.800   59.14	9.89 0.97 0	LO I	0.38 0.21 5	59.51 0.38 0.21 5	3.55 59.51 0.38 0.21 5	59.90 3.55 59.51 0.38 0.21 5	0.01 59.90 3.55 59.51 0.38 0.21 5	0.70 0.01 59.90 3.55 59.51 0.38 0.21 5	59:90     0.70     0.01     59:90     3.55     59:51     0.38     0.21     5	0.28 59.90 0.70 0.01 59.90 3.55 59.51 0.38 0.21 5	0.51 0.28 59.90 0.70 0.01 59.90 3.55 59.51 0.38 0.21 5	59.39     0.51     0.28     59.90     0.70     0.01     59.90     3.55     59.51     0.38     0.21     5	0.20 59.39 0.51 0.28 59.90 0.70 0.01 59.90 3.55 59.51 0.38 0.21 5
0.00   58.30   0.012   0.001   58.30     0.80   59.76   0.012   1.290   59.14   5     0.36   53.06   0.012   0.800   52.72   5	60.65 1.72 0		0.15 <sup>2</sup> 0.06	60.50 0.15 <sup>2</sup> 0.06	26.47 60.50 0.15 <sup>2</sup> 0.06	59.92     26.47     60.50     0.15 <sup>2</sup> 0.06     1	0.00 59.92 26.47 60.50 0.15 <sup>2</sup> 0.06	0.45 0.00 59.92 26.47 60.50 0.15 <sup>2</sup> 0.06	59.91     0.45     0.00     59.92     26.47     60.50     0.15 <sup>2</sup> 0.06	0.22 59.91 0.45 0.00 59.92 26.47 60.50 0.15 <sup>2</sup> 0.06	0.40 0.22 59.91 0.45 0.00 59.92 26.47 60.50 0.15 <sup>2</sup> 0.06	59.51     0.40     0.22     59.91     0.45     0.00     59.92     26.47     60.50     0.15 <sup>2</sup> 0.06	0.10     59.51     0.40     0.22     59.91     0.45     0.00     59.92     26.47     60.50     0.15 <sup>2</sup> 0.06
0.80   59.76   0.012   1.290   59.14   5     0.36   53.06   0.012   0.800   52.72   5	58.30 0.36 0		0.50 0.28	57.80 0.50 0.28	14.77 57.80 0.50 0.28	58.30     14.77     57.80     0.50     0.28	0.00 58.30 14.77 57.80 0.50 0.28	0.29 0.00 58.30 14.77 57.80 0.50 0.28	58.30     0.29     0.00     58.30     14.77     57.80     0.50     0.28	0.35     58.30     0.29     0.00     58.30     14.77     57.80     0.50     0.28	0.67     0.35     58.30     0.00     58.30     14.77     57.80     0.50     0.28	57.60     0.67     0.35     58.30     0.29     0.00     58.30     14.77     57.80     0.50     0.28	0.10     57.60     0.67     0.35     58.30     0.29     0.00     58.30     14.77     57.80     0.50     0.28
0.36 53.06 0.012 0.800 52.72 5	8.96 7.16 0	LO LO	0.67 0.35 5	57.50 0.67 0.35 5	35.33 57.50 0.67 0.35 5	58.47     35.33     57.50     0.67     0.35     5	0.80 58.47 35.33 57.50 0.67 0.35 5	7.16     0.80     58.47     35.33     57.50     0.67     0.35     5	57.67     7.16     0.80     58.47     35.33     57.50     0.67     0.35     5	0.35     57.67     7.16     0.80     58.47     35.33     57.50     0.67     0.35     5	0.67 <sup>3</sup> 0.35     57.67     7.16     0.80     58.47     35.33     57.50     0.67     0.35     5	57.00     0.67 <sup>3</sup> 0.35     57.67     7.16     0.80     58.47     35.33     57.50     0.67     0.35     5	2.50     57.00     0.67 <sup>3</sup> 0.35     57.67     7.16     0.80     58.47     35.33     57.50     0.67     0.35     5
	2.70 4.84 0	io .	1.00 0.79 5.	50.00 1.00 0.79 5	82.41 50.00 1.00 0.79 5	52.26 82.41 50.00 1.00 0.79 5	0.36 52.26 82.41 50.00 1.00 0.79 5	4.84     0.36     52.26     82.41     50.00     1.00     0.79     51	51.90     4.84     0.36     52.26     82.41     50.00     1.00     0.79     5	0.79     51.90     4.84     0.36     52.26     82.41     50.00     1.00     0.79     53	1.00 <sup>3</sup> 0.79     51.90     4.84     0.36     52.26     82.41     50.00     1.00     0.79     51	49.40     1.00 <sup>3</sup> 0.79     51.90     4.84     0.36     52.26     82.41     50.00     1.00     0.79     51	3.80     49.40     1.00 <sup>3</sup> 0.79     51.90     4.84     0.36     52.26     82.41     50.00     1.00     0.79     51

# **APPENDIX C**

Drainage Basin Exhibit



IECTS\2500-2599\2573\DWG\2573 C-701 BASIN EXH.dwg Asa 8/2/2023 2:50 PM

DRAINAGE NOTES:

PHIL CHACON PARK SHALL BE REDEVELOPED WITH PLAYGROUNDS, RECREATION FIELDS AND WALKS. THE EXISTING PARKING LOT AT THE NORTH END OF THE PROJECT SHALL BE RESURFACED.

THE PROPOSED GRADING OF THE SITE SHALL FOLLOW THE EXISTING DRAINAGE PATTERNS WITH A PORTION OF THE SITE DRAINING TO SOUTHERN AVE. AND THE REMAINDER OF THE SITE DRAINING TO THE SOUTHWEST CORNER OF THE PARK.

THE DEVELOPED DISCHARGE TO SOUTHERN AVE. WILL BE THE SAME AS THE HISTORICAL. SINCE BASINS 2 AND 3 (PLAYGROUND AREAS) WILL FULLY RETAIN THE STORM WATER, THE DEVELOPED DISCHARGE AT THE SOUTHWEST CORNER OF THE PARK WILL BE REDUCED (38.4 CFS DEVELOPED; 40.1 CFS HISTORICAL).

THE STORM DRAIN IS DESIGNED TO CARRY THE 10-YEAR FLOWS; THE REMAINDER WILL BE BYPASSED.

STORM WATER QUALITY (SWQ):

TWO STORM WATER QUALITY (SWQ) PONDS WILL BE INSTALLED EAST AND NORTH OF THE BASKETBALL COURTS AT THE SOUTHWEST CORNER OF THE PARK TO RETAIN THE VOLUME OF 0.26" FALLING ON THE IMPERVIOUS AREAS.

SWQ VOLUME REQUIRED = 2,523 CF SWQ VOLUME PROVIDED = 2,488 CF

	BAS	IN SUMMA	RY	
Basin No.	Description	Q 100 (CFS)	Q10 (CFS)	SWQV (CF)
1	To Southern Ave.	5.0	2.8	693
2	Self Ponding	0.8	0.4	36
3	Self Ponding	1.8	0.9	81
4	To SW Offsite Pond	10.0	4.7	444
5	To SW Offsite Pond	1.5	0.7	68
6	To Rundown	2.5	1.2	109
7	To Storm Drain	5.3	2.5	238
8	To Storm Drain	1.4	0.7	63
9	To Storm Drain	9.7	4.6	431
10	To Storm Drain	8.0	3.8	358
TOTAL		46.0	22.3	2,523
	Total to Storm Drain	24.4	11.6	cfs (12.8 cfs bypas:

Total Q to Rundown

<b>11.6</b> cfs (12.8 cfs bypas	s
<b>14.1</b> cfs (=11.6+2.5)	

SWQ PO	ND EAST (	OF BASKETBALL
	00	RI
Contour	Area	Volume
50.5	842	
52.0	1400	1682 CF
POND VO	LUME =	1682 CF

SWQ PON	ID NORTH	OF BASKETBALL					
	COU	IRT					
Contour	Area	Volume					
50.0	558						
50.6	2130	806 CF					
POND VO	LUME =	806 CF					

Job Name:	Phil Chacon	Park
Client:	PLAND	
Date Prepared:	2/23/2023	
Date Modified:	4/11/2023	
Precipitation Zone:	3	

			CALC	ULATIONS: Phil C	Chacon	Park : 43565		
		Based on Cit	y of Albuq	uerque DMP, Article	6-2 Hyd	drology dated Jur	ne 26, 2020	)
			10	0-YEAR, 6-HOUR C	CALCU	LATIONS		
AREA OF SITE:				711460	SF	=	16.33	ACRE
				100-year, 6-hour				
HISTORIC FLO	OWS:			<b>DEVELOPED FLO</b>	<b>DWS</b> :			EXCESS PRECIP:
		Treatment SF	%			Treatment SF	%	Precip. Zone 3
Area A	=	0	0%	Area A	=	0	0%	$E_{A} = 0.67$
Area B	=	615199	86.47%	Area B	=	594738	83.59%	$E_{\rm B} = 0.86$
Area C	=	0	0%	Area C	=	0	0%	$E_{\rm C} = 1.09$
Area D	=	96261	13.53%	Area D	=	116722	16.41%	$E_{\rm D} = 2.58$
Total Area	=	711460	100%	Total Area	=	711460	100%	
On-Site Weighte	d Exces	s Precipitation (	100-Year,	6-Hour Storm)				
_		Weighted E =		$\underline{E}_{A}A_{A} + \underline{E}_{B}A_{B} + \underline{E}_{C}A$	$A_{C} + E_{D}$	A <sub>D</sub>		
				$A_A + A_B + A_C$	$+ A_D$			
Historic E	=	1.09	in.	Developed E	=	1.14	in.	
				• – –				
On-Site Volume	of Runo	off: $V360 =$		E*A / 12				
Historic V <sub>360</sub>	=	64785	CF	Developed V <sub>360</sub>	=	67718	CF	
				•				
On-Site Peak Dis	charge	Rate: $Qp = Q_{pA}$	A <sub>A</sub> +Q <sub>pB</sub> A	$_{\rm B}+Q_{\rm pC}A_{\rm C}+Q_{\rm pD}A_{\rm D}/43$	3,560			
For Precipitation	Zone	3	-	-				
$Q_{pA}$	=	1.84		$Q_{pC}$	=	3.17		
Q <sub>pB</sub>	=	2.49		Q <sub>pD</sub>	=	4.49		
Historic Q <sub>p</sub>	=	45.1	CFS	Developed Q <sub>p</sub>	=	46.0	CFS	

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Enginee	er							
PHIL CHACON PARK	BFNOVATION		CITY OF ALBUOUEROUE					
DESIGN ISSUE: DEVELOPMENT	PROJECT NUMBER: IA 2573	FILE: -	DRAWN BY: ÂNW-BJB	CHECKED BY: ÂNW	DATE: 2023-08-02			
No Date Description	Т Т	E						
DR E E SHEET C		NA SII IB <sup>MBE</sup>	N N IT ≣R	E				

![](_page_27_Figure_0.jpeg)

![](_page_27_Figure_42.jpeg)

![](_page_28_Figure_0.jpeg)

![](_page_29_Figure_0.jpeg)

![](_page_29_Figure_1.jpeg)

DATE:

HydroTrans #\_\_\_\_

KEY MAP

![](_page_29_Figure_3.jpeg)

![](_page_30_Figure_0.jpeg)

![](_page_31_Figure_0.jpeg)

![](_page_32_Figure_0.jpeg)

![](_page_32_Figure_1.jpeg)

![](_page_32_Figure_2.jpeg)

KEY MAP

![](_page_32_Figure_4.jpeg)

![](_page_33_Figure_0.jpeg)

![](_page_33_Picture_1.jpeg)

![](_page_33_Figure_2.jpeg)

KEY MAP

![](_page_33_Figure_4.jpeg)

![](_page_34_Figure_0.jpeg)

![](_page_35_Figure_0.jpeg)