

The site is located at the N.W. corner of the intersection of Southern Avenue and Conchas Street. Conchas Street is paved with standard curb and gutter. Southern Avenue is paved but without curb and gutter. Southern Avenue is in the corridor for Gibson Boulevard extension. Property north and west of the site is developed. The propterty to the north is developed as warehousing and property to the west is mini warehouse units with asphalt parking. The property slopes from east to west a an average slope of approximately 1.5 percent.

PROPOSED CONDITIONS:

It is proposed to construct warehouses and asphalt parking on the site as shown. Due to the future construction of Gibson Boulevard, construction of curb and gutter on Southern Boulevard is not recommended at this time by Traffic Engineering. Due to downstream storm drainage improvements, and due to the fact that the site is an infill site, unrestricted discharge would otherwise be acceptable except for Southern Avenue being without curb and gutter. A detention pond is proposed to reduce developed discharge to the existing rate.

DRAINAGE CRITERIA:

The calculations shown on this plan were prepared in accordance with Section 22.2, Hydrology, of the Development Process Manual, Volume 2, Design Criteria, for the City of Albuquerque, in cooperation with Bernalillo County, New Mexico and the Albuquerque Metropolitan Arroyo Flood Control Authority, January, 1993.

The site is west of the Eubank Boulevard and is, therefore, in Precipitation Zone 3.

LAND					Existing Site Areas % Sq.Ft. Acres					
IREAIMENI	100-yr.	1U-yr.	100-yr.	10-yr.	/•	<u> </u>	ACTES	/,	<u> </u>	ACTES
A	1.87	0.58	0.66	0.19	0.0	0	0.0	0.0	. 0	0.0000
В	2.60	1.19	0.92	0.36	00.0	0	0.0000	8.0	4,458	0.1023
С	3.45	2.00	1.29	0.62	100.0	56,123	1.2884	20.0	11,241	0.2581
D	5.02	3.39	2.36	1.50	00.0	. 0	0.0000	72. 0	40,424	0.9280
Totals	* *				100.0	58,123	1.2884	100.0	56,123	1.2884

PEAK DISCHARGE:

EXISTING CONDITIONS:

 $= 1.2884 \times 3.45 = 4.45 \text{ cfs}$ = 1.2884 * 2.00 = 2.58 cfsQ10

DEVELOPED CONDITIONS:

 $Q100 = 0.1023 \times 2.60 + 0.2581 \times 3.45 + 0.9280 \times 5.02 = 5.81 \text{ cfs}$ $= 0.1023 \times 1.19 + 0.2581 \times 2.00 + 0.9280 \times 3.39 = 3.78 \text{ cfs}$

VOLUME 100-YEAR, 6-HOUR:

EXISTING CONDITIONS:

 $V100 = (56,123 \times 1.29)/12 = 6,033 \text{ CF}$ V10 = (56,123 * 0.62)/12 = 2,900 CF

DEVELOPED CONDITIONS (THE PROPERTY OF THE PROP

V100 = $(4,458 \times 0.92 + 11,241 \times 1.29 + 40,424 \times 2.36)/12 = 9,500 \text{ CF}$ $V10 = (4,458 \times 0.36 + 11,241 \times 0.62 + 40,424 \times 1.50)/12 = 5,768 \text{ CF}$

V100 V10 SUMMARY OF VOLUMES AND PEAK DISCHARGE RATES

2,900 5,768 2,868 6,033 9,500 5.81 1.36 3.78 DEVELOPED 1.20 INCREASE

OFF-SITE FLOW:

There is no off-site flow associated with this site. The property to the north is graded to drain to Trumbull Avenue, SE,

DOWNSTREAM CAPACITY:

THE SITE WILL DRAIN INTO SOUTHERN AVENUE WHICH IS PAVED BUT DOES NOT HAVE CURB AND GUTTER. THE SITE DISCHARGE WILL ENTER SOUTHERN AVENUE AND BE CONVEYED BY THE ROADSIDE DITCHES TO MOON AVENUE WHICH DOES HAVE CURB AND GUTTER AND A STORM DRAINAGE SYSTEM. THERE IS A FLOOD ZONE IN MOON STREET BEGINNING NORTH OF TRUMBULL AVENUE. A 54" RCP STORM DRAIN LINE HAS BEEN INSTALLED IN MOON STREET PARALLEL TO THE EXISTING 36" RCP STORM DRAIN LINE AND THE THE TWO LINES ARE INTERCONNECTED AT MANHOLES. THE NEW LINE IS A "WASH" LINE FOR THE CITY RESERVOIRS AT GARCIA AND TRUMBULL. IT IS IMPORTANT THAT THE DISCHARGE FROM THE DEVELOPED SITE NOT BE INCREASED SIGNIFICANTLY OVER THE EXISTING PEAK DISCHARGE. THE EXISTING PEAK DISCHARGE IS 4.45 CFS. DEVELOPED RUNDFF IS 5.81 CFS AND THE INCREASE IS 1.36 CFS. IN ORDER TO LIMIT SITE DISCHARGE TO THE EXISTING 4.45 CFS, IT IS PROPOSED TO HAVE A DETENTION POND WEST OF BUILDING NO. 1 WITH SPILLWAY AND POSITIVE DISCHARGE PIPES. THE AREA AVAILABLE IS LIMITED BUT IT WILL BE POSSIBLE TO LIMIT THE FLOW TO THE EXISTING 100-YEAR PEAK DISCHARGE IT WILL ALSO BE NECESSARY TO LINE THE POND BOTTOM WITH AN IMPERVIOUS POND LINER SINCE THE POND WILL BE CLOSER THAN 15 FEET FROM THE BUILDING AND THE PROPERTY LINE.

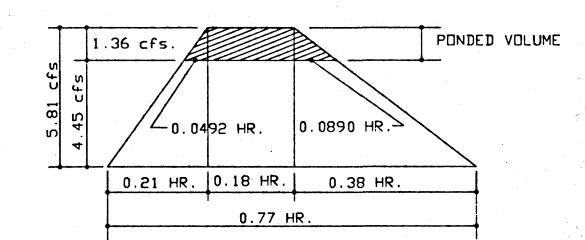
DRAINAGE CALCULATIONS:

POND CALCULATIONS

 $t_R = (2.107 * E * A_T / Q_P) - (0.25 A_D / A_T)$ $E = 0.08 \times 0.92 + 0.20 \times 1.29 + 0.72 \times 2.36 = 2.03 in.$ $A_T = 1.2884 \text{ AC}$ $A_D = 0.9280 \text{ AC}$ $Q_D = 5.81 \text{ CFS}$ $t_{\rm R} = (2.107 \pm 2.03 \pm 1.2884 / 5.81) - (0.25 \pm 0.9280 / 1.2884) = 0.77 \, \rm HR.$ $t_p = (0.7 * t_c) + ((1/6 - (A_T / A_T))/12)$ $t_p = (0.7 \times 0.2) + ((1.6 - (0.9280 / 1.2884)) / 12) = 0.21 HR.$

Continue the Peak $0.25 (A_D / A_T) = 0.25 (0.9280/1.2884) = 0.18 HR.$

HYDROGRAPH FOR SMALL WATERSHEDS:



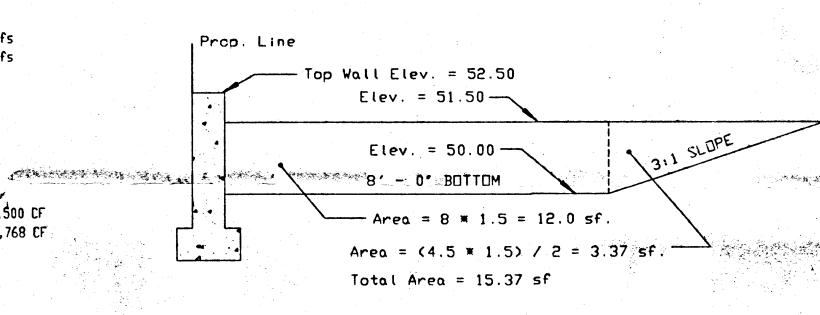
PDND VDLUME: $V = [(0.0492 \times 1.36)1/2 + (0.18 \times 1.36) + (0.0890 \times 1.36)1/2] \times 3600$ V = 1,220 CF

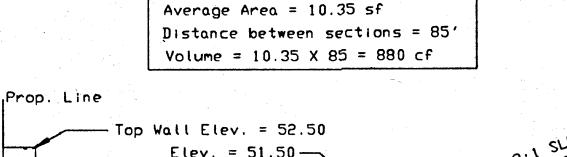
ACTUAL POND VOLUME :

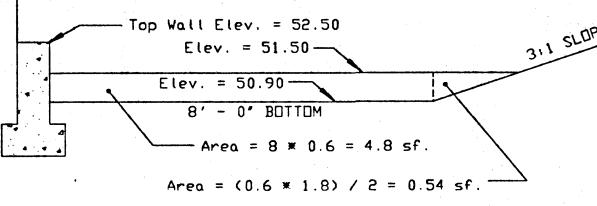
Ponding will take place along the west and north sides of Building No. 1 and in the silting basin.

North side of Building No. 1: Use Pyramid Equation, V = BH/3 B = Surface Area = 216 sf. H = Depth at west end = 51.4 - 50.8 = 0.6 ft. $V = (216 \times 0.6)/3 = 43 \text{ cf}$

West side of Building No. 1: Use Average End Area Method.







Total Area = 5.34 sf

Sedimentation Basin.

Area = $15 \times 15 \times 1.5 = 337$ cf.

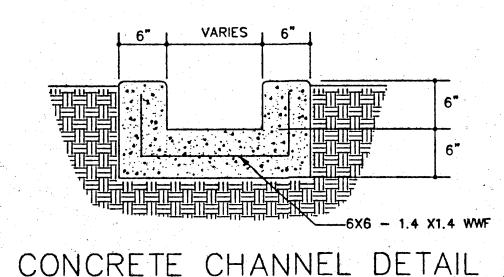
TOTAL ACTUAL POND VOLUME: V = 43 + 880 + 337 = 1260 CF > 1220 CF.

EROSION CONTROL REQUIREMENTS:

The Contractor shall be responsible for compliance with the following:

originating from the site.

- 1. No sediment-bearing water shall be allowed to discharge from the site during construction. During grading operations and until the project has been completed, all adjacent property rights-of-way, and easements shall be protected from flooding by runoff from the site.
- Should the contractor fail to prevent sediment-bearing water from entering public right-of-way, he shall promptly remove from the public right-of-way any and all sedimentation
- Control of sediment-bearing waters will be accomplished by use of a compacted earth berm of adequate height. The berm shall be located along the downstream perimeter of the



1" = 1'-0"

PUND PUSITIVE DISCHARGE:

Design Q = 4.45 cfs. It is desireable to use a number of small diameter pipes rather than one large one. Use Orifice Equation, $Q = CA(2GH)^{1/2}$ C = 0.6 A = 0.0855 sf for 4' dia. PVC. H = 1.17' (Vert. dist. between spillway and center of pipe).

 $Q = 0.6 \times 0.0855 (2 \times 32.16 \times 1.17)^{1/2} = 0.445 \text{ cfs.}$ "Use 10 each 4" PVC pipes through concrete cutoff wall.

POND OVERFLOW SPILLWAY:

Use Weir Equation, $Q = CLH^{3/2}$ C = 3.0 L = 10.0' H = 0.34' or approx. 4' $Q = 3.0 \times 10.0 \times 0.34^{3/2} = 5.95 \text{ cfs} > 5.81 \text{ cfs}.$

FLOW AT ANALYSIS POINTS:

East side of Building No. 3 and East Parking Lot. (ANALYSIS POINT 1) Treat. B = 0.0197 ac. Treat C = 0.0302 ac. Treat. D = 0.1469 ac. $Q = (0.0197 \times 2.60 + 0.0302 \times 3.45 + 0.1469 \times 5.02) = 0.84 \text{ cfs}$

Area South of Building No 3: (ANALYSIS PDINT 2) Treat. B = 0.0241 ac. Treat D = 0.0478 ac.

 $Q = (0.0241 \times 2.60 + 0.0478 \times 5.02 = 0.30 \text{ cfs} (Accum. Sum = 1.14 \text{ cfs.})$

Area Between Ridges of Building No. 2 and Building No 3: (ANALYSIS PDINT 3) Treat C = 0.0909 ac. Treat. D = 0.2020 ac. Q = (0.0909 * 3.45 + 0.2020 * 5.02 = 1.33 cfs If the landscaped area S. of the sidewalk is included, Q = 1.43 cfs. (ANALYSIS PDINT 3A) (Accum. Sum = 2.57 cfs)

Area in front of Building No. 2: (ANALYSIS PDINT 4)

Treat. B = 0.0069 ac. Treat D = 0.0647 ac.

Q = (0.0069 * 2.60 + 0.0647 * 5.02 = 0.34 cfs (Accum. Sum = 2.91 cfs)

Area between Buildings No 1 and No. 2 and W half of Building No. 2: (ANALYSIS PDINT 5) Treat C = 0.0559 ac. Treat. D = 0.2515 ac

 $Q = (0.0559 \times 3.45 + 0.2515 \times 5.02 = 1.46 \text{ cfs} (Accum, Sum = 4.37 \text{ cfs})$

Area north of Building No 1: (ANALYSIS PDINT 6) Treat C = 0.0379 ac. Treat. D = 0.1010 ac.

Q = (0.0379 * 3.45 + 0.1010 * 5.02 = 0.64 cfs (Accum. Sum = 5.01 cfs)

Area west of Building No 1: (ANALYSIS POINT IS POND) Treat C = 0.0725 ac. $Q = 0.0725 \times 3.45 = 0.25$ cfs

Area South of Building No 1: (ANALYSIS POINT IS POND) Treat. C = 0.0126 ac. Treat D = 0.1010 ac.

 $Q = (0.0126 \times 3.45 + 0.1010 \times 5.02 = 0.55 \text{ cfs} \text{ (Accum. Sum = 5.81 cfs)}$ CHANNEL FLOW:

CHANNEL NO. 1 Channel at SE corner of Building No. 3

Q = 0.84 (Design Flow) $Q = CLH^{3/2}$ $L = Q/(CH^{3/2})$ C = 3.0H = 0.4' L = 0.84 / (3.0 × 0.4^{3/2}) = 1.10 Use 1.5' Check Capacity by Manning's Equation: $Q = A(1.486/N)R^{2/3} S^{1/2}$ N = 0.013 S = 0.0020 ft/ft A = 0.4 * 1.5 = 0.6 sf. P = 2.3'R = A/P = 0.26 $Q = 0.6(1.486/0.013)(0.26)^{2/3}(0.002)^{1/2} = 1.25 cfs.$

CHANNEL ND. 2:

Channel between Building No. 2 and Building No. 3, east end. Q = 1.23 cfs Based on calcs for Channel No. 1, 1.5' is adequate.

CHANNEL NO. 3:

Channel between Building No. 2 and Building No. 3, w/ SW culvert. Q = 1.33 cfs Based on calcs for Channel No. 1, 2.0' is adequate.

CHANNEL NO. 4:

Channel between Building No. 2 and Building No. 3, West of Junction. Q = 2.57 cfs Use Manning's Equation. Try 2.0' Channel, Flow Depth = 0.45 A = 0.9 sf P = 2.9' R = 0.31 $Q = 0.9 (1.486 / 0.013)(0.31)^{2/3} (0.005)^{1/2} = 3.33 cfs (Adequate).$

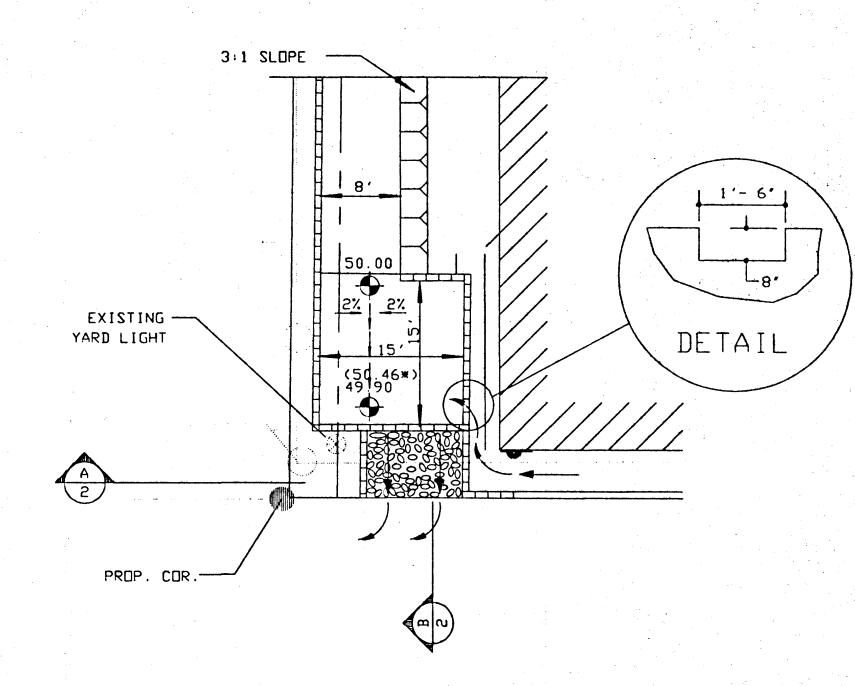
CHANNEL NO. 5:

Channel near SW corner of Building No. 2. Q = 2.91 cfs. Based on Calcs, for Channel No. 4, 2.0' Channel is Adequate.

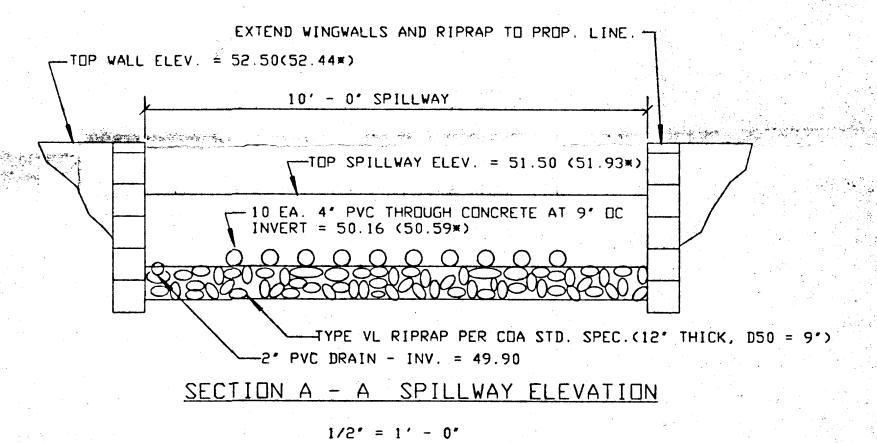
CHANNEL NO. 6:

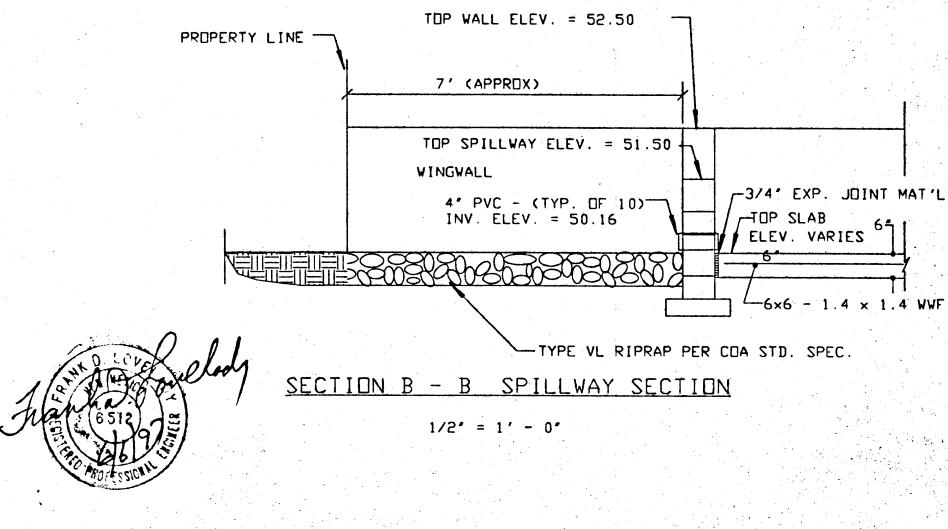
North side of Building No. 1. Q = 5.01 cfs. D = 0.9'Use Manning's Equation. V-shaped Channel with 3:1 side slopes. A = 2.43 P = 5.69' R = 0.43 N = 0.023 (Gravel).

 $\sqrt[3]{Q} = 2.43 (1.486 / 0.023) (0.43)^{2/3} (0.0050)^{1/2} = 6.32 \text{ cfs} > 5.01 \text{ cfs}.$

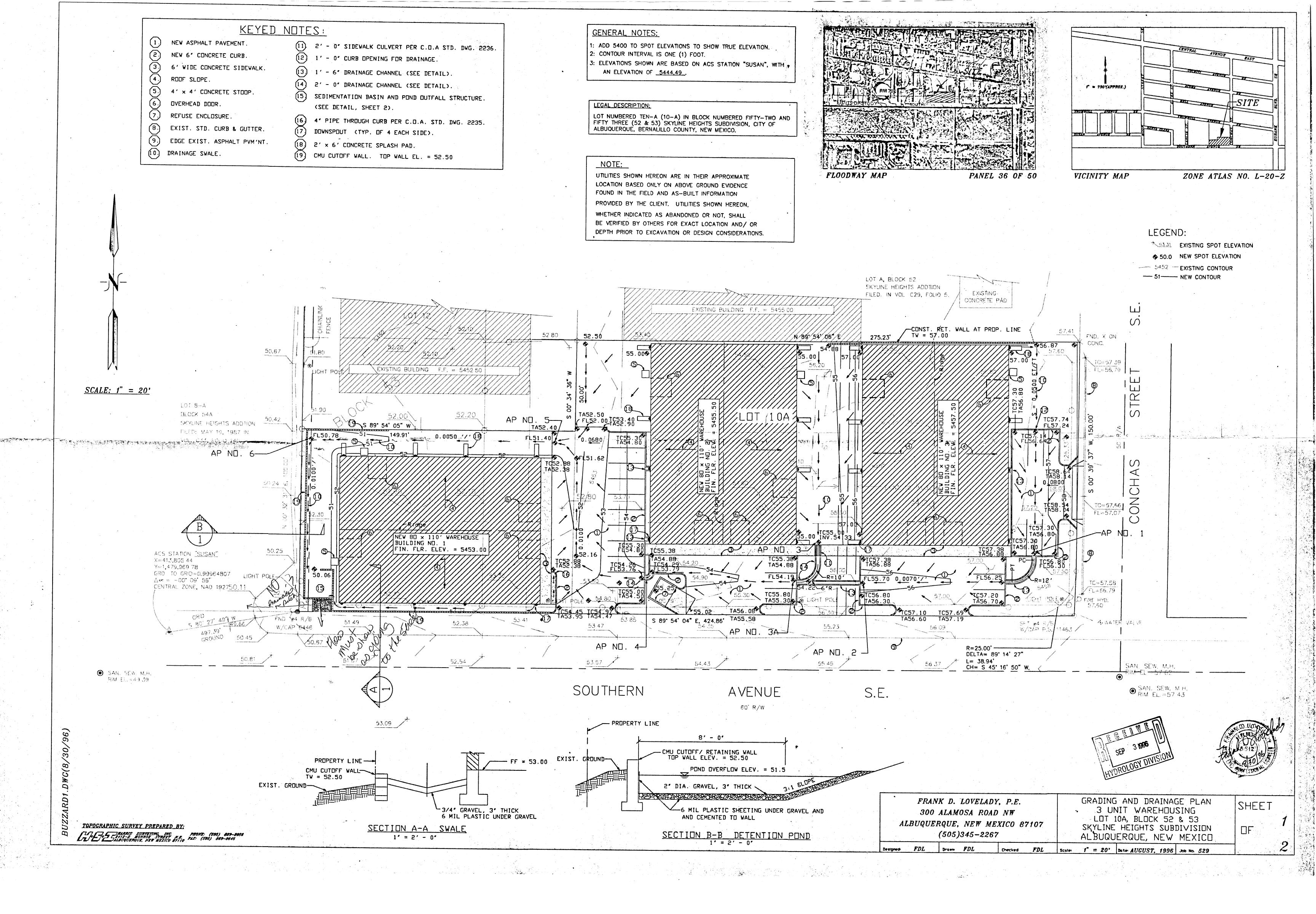


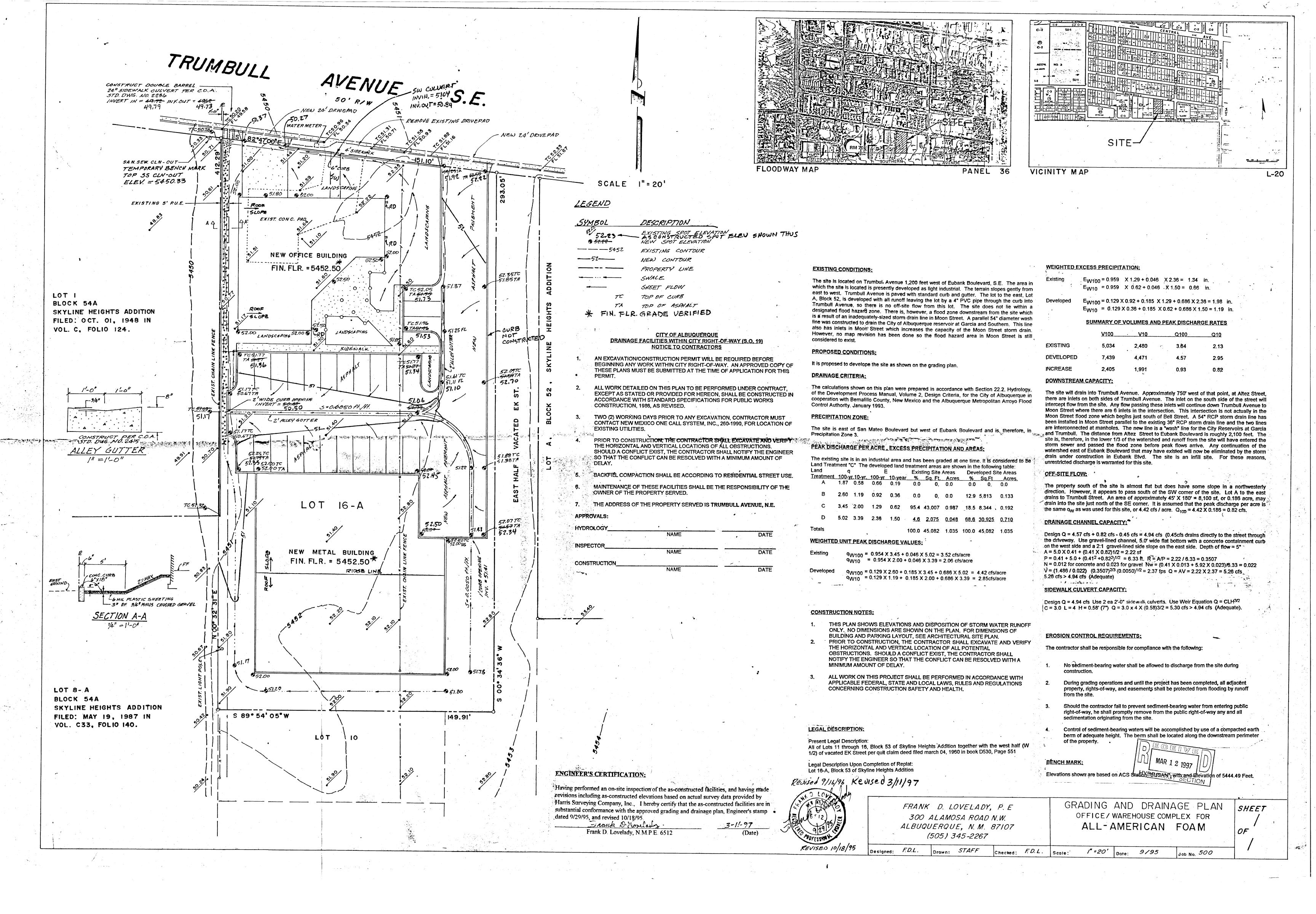
SEDIMENTATION BASIN AND POND DISCHARGE STRUCTURE DETAIL 1" = 10'





DRAINAGE CALCULATIONS FRANK D. LOVELADY, P.E. SHEET 3 UNIT WAREHOUSING 300 ALAMOSA ROAD NW LOT 10A, BLOCK 52 & 53 ALBUQUERQUE, NEW MEXICO 87107 SKYLINE HEIGHTS SUBDIVISION (505)345-2267 ALBUQUERQUE, NEW MEXICO 1" = 20' Date: JUNE, 1997 Job No. 529 Designed FDL Drawn FDL





PROPOSED CONDITIONS:

It is proposed to construct warehouses and asphalt parking on the site as shown. Due to the future construction of Gibson Boulevard, construction of curb and gutter on Southern Boulevard is not recommended at this time by Traffic Engineering. Due to downstream storm drainage improvements, and due to the fact that the site is an infill site, unrestricted discharge would otherwise be acceptable except for Southern Avenue being without curb and gutter. A detention pond is proposed to reduce developed discharge to the existing rate.

DRAINAGE CRITERIA:

The calculations shown on this plan were prepared in accordance with Section 22.2, Hydrology, of the Development Process Manual, Volume 2, Design Criteria, for the City of Albuquerque, in cooperation with Bernalillo County, New Mexico and the Albuquerque Metropolitan Arroyo Flood Control Authority, January, 1993.

The site is west of the Eubank Boulevard and is, therefore, in Precipitation Zone 3.

PRECIPITATION ZONE:

LAND TREATM								Areas Acres			
				•				0.0			
				•				0.0000			
C		3.45	2.00	1.29	0.62	100.0	56,123	1.2884	20.0	11,241	0.2581
· D		5.02	3.39	2.36	1.50	00.0	0	0.0000	72.0	40,424	0.9280
Total	5		• • •			100.0	58,123	1.2884	100.0	56,123	1.2884

PEAK DISCHARGE:

EXISTING CONDITIONS:

Q100 = 1.2884 = 3.45 = 4.45 cfs Q10 = 1.2884 = 2.00 = 2.58 cfs DEVELOPED CONDITIONS:

> Q100 = $0.1023 \times 2.60 + 0.2581 \times 3.45 + 0.9280 \times 5.02 = 5.81 \text{ cfs}$ Q10 = $0.1023 \times 1.19 + 0.2581 \times 2.00 + 0.9280 \times 3.39 = 3.78 \text{ cfs}$

VOLUME 100-YEAR, 6-HOUR:

EXISTING CONDITIONS:

V100 = $(56,123 \times 1.29)/12 = 6,033$ CF V10 = $(56,123 \times 0.62)/12 = 2,900$ CF

DEVELOPED CONDITIONS:

V100 = (4,458 * 0.92 + 11,241 * 1.29 + 40,424 * 2.36)/12 = 9,500 CF V10 = (4,458 * 0.36 + 11,241 * 0.62 + 40,424 * 1.50)/12 = 5,768 CF

SUMMARY OF VOLUMES AND PEAK DISCHARGE RATES:

				*.
EXISTING	6,033	2,900	4.45	2.58
DEVELOPED	9,500	5,768	5.81	3.78
INCREASE	3,467	2,868	1.36	1.20

There is no off-site flow associated with this site. The property to the north is graded to drain to Trumbull Avenue, SE.

DOWNSTREAM CAPACITY:

THE SITE VILL DRAIN INTO SOUTHERN AVENUE WHICH IS PAVED BUT DOES NOT HAVE CURB AND GUTTER. THE SITE DISCHARGE VILL ENTER SOUTHERN AVENUE AND BE CONVEYED BY THE ROADSIDE DITCHES TO MOON AVENUE WHICH DOES HAVE CURB AND GUTTER AND A STORM DRAINAGE SYSTEM. THERE IS A FLOOD ZONE IN MOON STREET BEGINNING NORTH OF TRUMBULL AVENUE. A 54° RCP STORM DRAIN LINE HAS BEEN INSTALLED IN MOON STREET PARALLEL TO THE EXISTING 36° RCP STORM DRAIN LINE AND THE THE TWO LINES ARE INTERCONNECTED AT MANHOLES. THE NEW LINE IS A "WASH" LINE FOR THE CITY RESERVOIRS AT GARCIA AND TRUMBULL. IT IS IMPORTANT THAT THE DISCHARGE FROM THE DEVELOPED SITE NOT BE INCREASED SIGNIFICANTLY OVER THE EXISTING PEAK DISCHARGE. THE EXISTING PEAK DISCHARGE IS 4.45 CFS. DEVELOPED RUNDEF IS 5.81 CFS AND THE INCREASE IS 1.36 CFS. IN ORDER TO LIMIT SITE DISCHARGE TO THE EXISTING 4.45 CFS, IT IS PROPOSED TO HAVE A DETENTION POND VEST OF BUILDING NO. 1 VITH SPILLVAY AND POSITIVE DISCHARGE PIPES. THE AREA AVAILABLE IS LIMITED BUT IT VILL BE POSSIBLE TO LIMIT THE FLOW TO THE EXISTING 100-YEAR PEAK DISCHARGE.

IT VILL ALSO BE NECESSARY TO LIMIT THE FLOW TO THE EXISTING 100-YEAR PEAK DISCHARGE.

IT VILL BE CLOSER THAN 15 FEET FROM THE BUILDING AND THE PROPERTY LINE.

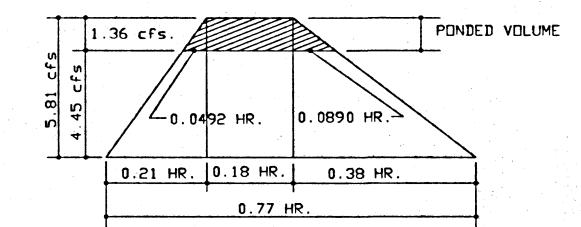
DRAINAGE CALCULATIONS:

PUND CALCULATIONS

 $t_B = (2.107 * E * A_T / Q_P) - (0.25 A_D / A_T)$ E = 0.08 * 0.92 + 0.20 * 1.29 + 0.72 * 2.36 = 2.03 in. $A_T = 1.2884 AC A_D = 0.9280 AC Q_P = 5.81 CFS$

HYDROGRAPH FOR SMALL WATERSHEDS:

 $t_B = (2.107 \pm 2.03 \pm 1.2884 / 5.81) - (0.25 \pm 0.9280 / 1.2884) = 0.77 \, \text{HR.} \\ t_P = (0.7 \pm t_C) + ((1/6 - (A_D / A_T))/12) \\ t_P = (0.7 \pm 0.2) + ((1.6 - (0.9280 / 1.2884)) / 12) = 0.21 \, \text{HR.} \\ \text{Continue the Peak} \quad 0.25 \, (A_D / A_T) = 0.25 \, (0.9280/1.2884) = 0.18 \, \text{HR.} \\$



POND VOLUME: $V = [(0.0492 \times 1.36)1/2 + (0.18 \times 1.36) + (0.0890 \times 1.36)1/2] \times 3600$ V = 1,220 CF

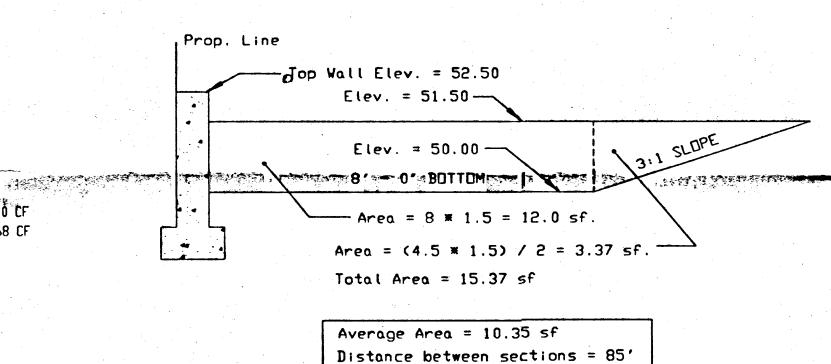
ACTUAL POND VOLUME:

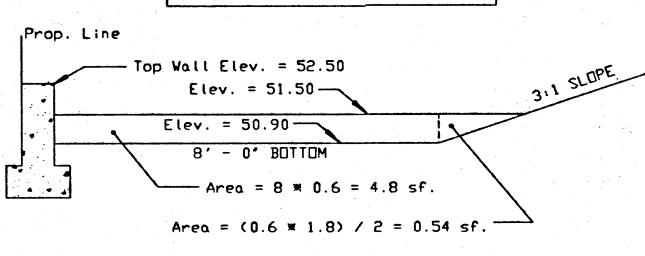
Ponding will take place along the west and north sides of Building No. 1 and in the silting basin.

North side of Building No. 1: Use Pyramid Equation, V = BH/3 B = Surface Area = 216 sf.H = Depth at west end = 51.4 - 50.8 = 0.6 ft.

V = (216 * 0.6)/3 = 43 cf

West side of Building No. 1: Use Average End Area Method.





Volume = $10.35 \times 85 = 880 \text{ cf}$

Total Area = 5.34 sf

Sedimentation Basin.

Area = $15 \times 15 \times 1.5 = 337$ cf.

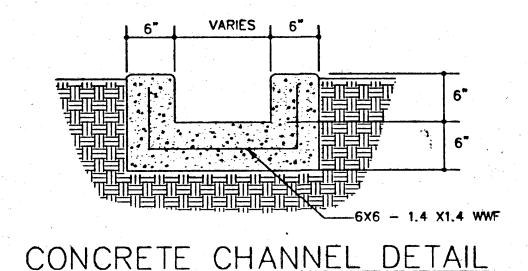
TOTAL ACTUAL POND VOLUME: V = 43 + 880 + 337 = 1260 CF > 1220 CF.

EROSION CONTROL REQUIREMENTS:

The Contractor shall be responsible for compliance with the following:

- 1. No sediment-bearing water shall be allowed to discharge from the site during construction.
- 2. During grading operations and until the project has been completed, all adjacent property rights-of-way, and easements shall be protected from flooding by runoff from the site.

 3. Should the contractor fail to prevent sediment-bearing water from entering public right-
- 3. Should the contractor fail to prevent sediment-bearing water from entering public right-of-way, he shall promptly remove from the public right-of-way any and all sedimentation originating from the site.
- 4. Control of sediment-bearing waters will be accomplished by use of a compacted earth berm of adequate height. The berm shall be located along the downstream perimeter of the property.



1'' = 1' - 0''

POND POSITIVE DISCHARGE:

Design Q = 4.45 cfs. It is desireable to use a number of small diameter pipes rather than one large one. Use Drifice Equation, Q = $CA(2GH)^{1/2}$ C = 0.6 A = 0.0855 sf for 4' dia. PVC. H = 1.17' (Vert. dist. between spillway and center of pipe).

Q = 0.6 = 0.0855 (2 = 32.16 = 1.17) = 0.445 cfs.

Use 10 each 4" PVC pipes through concrete cutoff wall.

POND OVERFLOW SPILLWAY:

Use Veir Equation, $Q = CLH^{3/2}$ C = 3.0 L = 10.0' H = 0.34' or approx. 4' $Q = 3.0 \pm 10.0 \pm 0.34^{3/2} = 5.95$ cfs > 5.81 cfs.

FLOW AT ANALYSIS POINTS:

East side of Building No. 3 and East Parking Lot. (ANALYSIS PDINT 1)

Treat. B = 0.0197 ac. Treat C = 0.0302 ac. Treat. D = 0.1469 ac. $Q = (0.0197 \pm 2.60 + 0.0302 \pm 3.45 + 0.1469 \pm 5.02) = 0.84$ cfs

Area South of Building No 3: (ANALYSIS POINT 2)

Treat. B = 0.0241 ac. Treat D = 0.0478 ac.

Q = (0.0241 x 2.60 + 0.0478 x 5.02 = 0.30 cfs (Accum. Sum = 1.14 cfs.)

Area Between Ridges of Building No. 2 and Building No 3: (ANALYSIS POINT 3)

Treat C = 0.0909 ac. Treat. D = 0.2020 ac.

Treat C = 0.0909 ac. Treat. D = 0.2020 ac. Q = (0.0909 * 3.45 + 0.2020 * 5.02 = 1.33 cfs If the landscaped area C = 0.0909 is included, C = 0.43 cfs. (ANALYSIS PDINT 3A) (Accum. Sum = 2.57 cfs)

Area in front of Building No. 2: (ANALYSIS PDINT 4)

Treat. B = 0.0069 ac. Treat D = 0.0647 ac.

 $Q = (0.0069 \times 2.60 + 0.0647 \times 5.02 = 0.34 \text{ cfs} \text{ (Accum. Sum = 2.91 cfs)}$

Area between Buildings No 1 and No. 2 and W. half of Building No. 2: (ANALYSIS POINT 5) Treat C = 0.0559 ac. Treat. D = 0.2515 ac. Q = (0.0559 * 3.45 + 0.2515 * 5.02 = 1.46 cfs (Accum. Sum = 4.37 cfs)

Area north of Building No 1: (ANALYSIS PDINT 6)

Treat C = 0.0379 ac. Treat. D = 0.1010 ac.

 $Q = (0.0379 \times 3.45 + 0.1010 \times 5.02 = 0.64 \text{ cfs (Accum. Sum} = 5.01 \text{ cfs})$

Area west of Building No 1: (ANALYSIS POINT IS POND)

Treat C = 0.0725 ac. Q = 0.0725 X 3.45 = 0.25 cfs

Area South of Building No 1: (ANALYSIS POINT IS POND)

Treat. C = 0.0126 ac. Treat D = 0.1010 ac.

 $Q = (0.0126 \times 3.45 + 0.1010 \times 5.02 = 0.55 \text{ cfs} \text{ (Accum. Sum = 5.81 cfs)}$

CHANNEL FLOW:

CHANNEL NO. 1 Channel at SE corner of Building No. 3.

Q = 0.84 (Design Flow) Q = CLH $^{3/2}$ L = Q/(CH $^{3/2}$) C = 3.0 H = 0.4' L = 0.84 / (3.0 * 0.4 $^{3/2}$) = 1.10' Use 1.5' Check Capacity by Manning's Equation. Q = A(1.486/N)R $^{2/3}$ S $^{1/2}$ N = 0.013 S = 0.0020 ft/ft A = 0.4 * 1.5 = 0.6 sf. P = 2.3' R = A/P = 0.26 Q = 0.6(1.486/0.013)(0.26) $^{2/3}$ (0.002) $^{1/2}$ = 1.25 cfs.

CHANNEL ND. 2:

Channel between Building No. 2 and Building No. 3, east end.

Q = 1.23 cfs Based on calcs for Channel No. 1, 1.5' is adequate.

CHANNEL NO. 3:

Channel between Building No. 2 and Building No. 3, w/ SW culvert. Q = 1.33 cfs Based on calcs for Channel No. 1, 2.0' is adequate.

CHANNEL NO. 4:

Channel between Building No. 2 and Building No. 3, West of Junction. Q = 2.57 cfs Use Manning's Equation. Try 2.0' Channel, Flow Depth = 0.45 A = 0.9 sf P = 2.9' R = 0.31 $Q = 0.9 (1.486 / 0.013)(0.31)^{2/3} (0.005)^{1/2} = 3.33 \text{ cfs}$ (Adequate).

CHANNEL ND. 5: Channel near SW

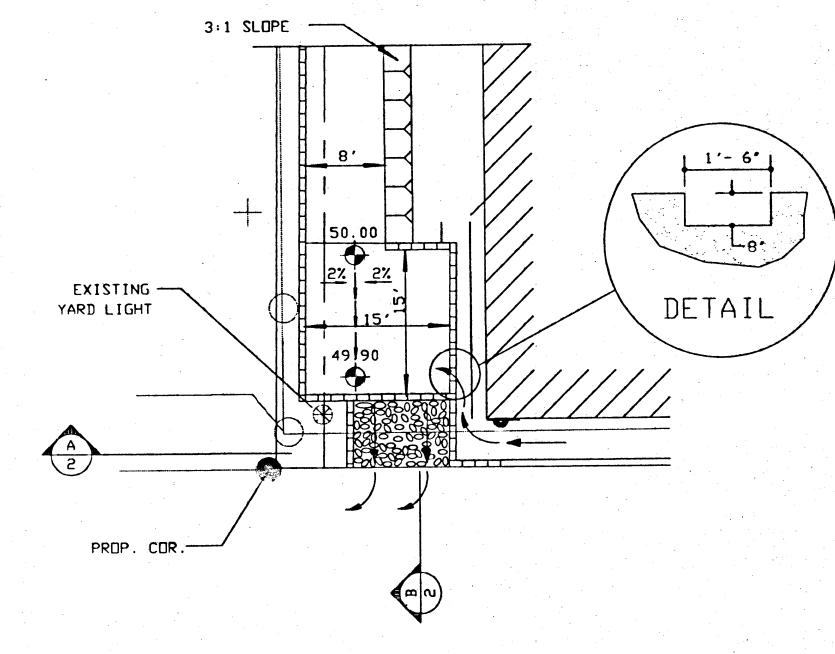
Channel near SW corner of Building No. 2. $Q=2.91\ cfs$. Based on Calcs. for Channel No. 4, 2.0' Channel is Adequate.

CHANNEL NO. 6:

North side of Building No. 1. Q = 5.01 cfs. D = 0.9'Use Manning's Equation. V-shaped Channel with 3:1 side slopes.

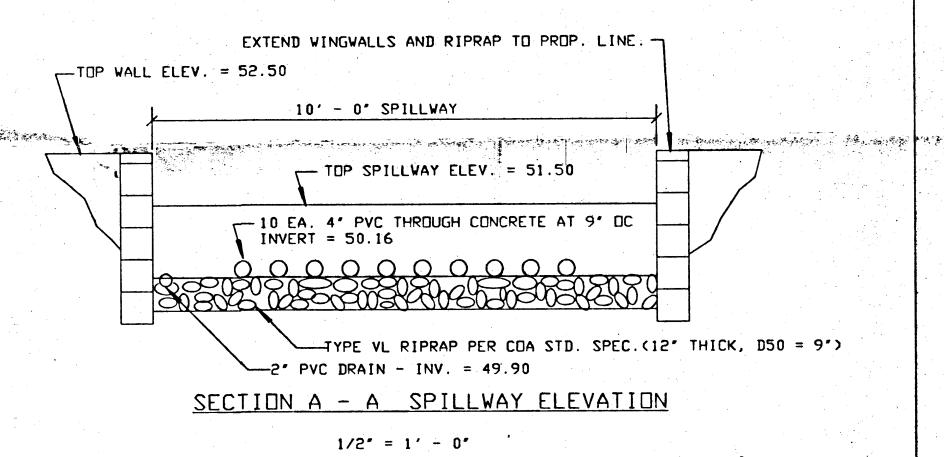
A = 2.43 P = 5.69' R = 0.43 N = 0.023 (Gravel).

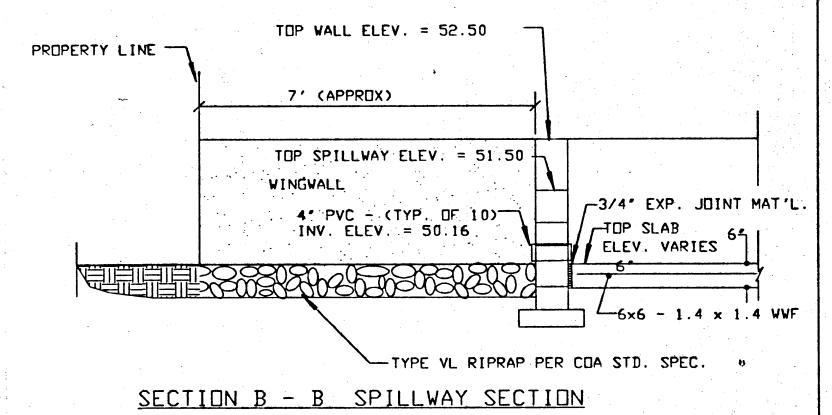
 $Q = 2.43 (1.486 / 0.023) (0.43)^{2/3} (0.0050)^{1/2} = 6.32 cfs > 5.01 cfs.$



SEDIMENTATION BASIN AND POND DISCHARGE STRUCTURE DETAIL

1' = 10'





or elody

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DRAINAGE CALCULATIONS

3 UNIT WAREHOUSING
LOT 10A, BLOCK 52 & 53
SKYLINE HEIGHTS SUBDIVISION
ALBUQUERQUE, NEW MEXICO

1/2" = 1' - 0"

OF

SHEET

Designed FDL Drawn FDL Checked FDL Scales 1" = 20' Date: AUGUST, 1996 Job No. 529

