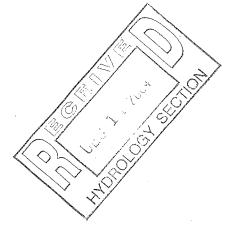
DRAINAGE STUDY FOR SIERRA RANCH SUBDIVISION

DECEMBER 16, 2004

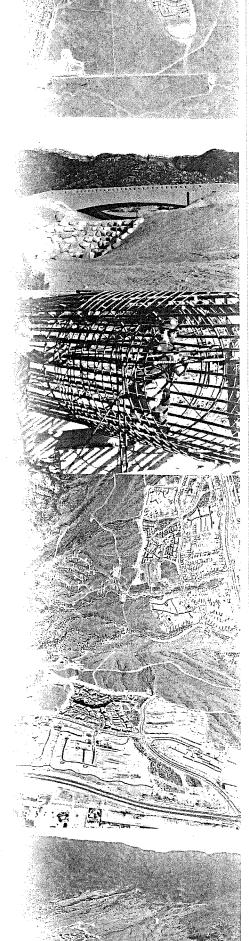


Prepared for:

Curb Inc. 5160 San Francisco NE Albuquerque, NM 87109

Bohannan Huston:

ENGINEERING A
SPATIAL DATA A
ADVANCED TEGNNOLOGIES A





City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

May 24, 2004



N-8

Mr. Bo K. Johnson, P.E. Curb, Inc. 5160 San Francisco DR. NE Albuquerque, NM 87109

RE: Water and Sewer Availability Statement

Tract 1A, 1B, 1C and 1D of the Lands of Rio Bravo Partners

Mr. Johnson:

Project Information: The project site consists of approximately 103 acres of undeveloped property both north and south of Gibson west of Messina in southwest Albuquerque. Current zoning is R-LT as governed by the Rio Bravo Sector Plan. Recent sketch plat submittals have suggested that this site will be subdivided into approximately 590 individual lots which will be developed as single family residences. Please be advised that this configuration will not be allowed due to the fact that some of these proposed lots would be located above serviceable elevations. Based on the existing topography, the dwellings within tracts 1B and 1C will have pad elevations between 5,160 and 5,255 feet and will be serviceable within the 2W pressure zone. Tracts 1A and 1D are located within the 3W pressure zone and are, therefore, not serviceable.

Existing Conditions: As of the date of this correspondence, there are no existing structures present on-site. Nearby construction projects include the El Rancho Grande subdivisions as well as a 20-/18-inch bottom of zone water transmission line which will supply pressure zones 2W and 2WR. Please refer to project number 679581 for specifics regarding this line. The Snow Vista sanitary sewer interceptor, which will be the outfall for the region, is currently in the design phase and will be located east of the site.

Metered Water Service will be contingent on the completion and acceptance of the improvements associated with the adjacent El Rancho Grande developments and the 18-inch bottom of zone transmission line in Mesa Arenosco Drive. Service to tracts 1B and 1C will require the extension of a 20-inch Master Plan top of zone 2W line south from Cartagena to Gibson. At Gibson, the line will reduce to an 18-inch and proceed west across the northern frontage of tract 1B. A 12-inch must also be constructed south of tract 1C from the 18-inch Mesa Arenosco line west to the southwest corner of tract 1C. In addition to the perimeter lines described, looped water lines must be constructed at standard locations within each of the rights-of-way internal to the subdivision. Internal lines for tract 1B will connect to both the 20-inch top of zone line and the proposed 8-inch main in Messina. Internal lines for tract 1C will be connected to both the 18-inch top of zone line and the new 12-inch line to the south. These lines will be a combination of 8-inch and 6-inch mains to which routine service connections may be made.

Sanitary Sewer Service will be contingent on the completion and acceptance of the Snow Vista Interceptor and the improvements associated with the adjacent El Rancho Grande developments. Minimum 8-inch collectors along with manholes at regular intervals must be constructed within each of the rights-of-way internal to the subdivision. The sewer lines within tract 1B will outfall to the southern 8-inch line in Unit 11. Tract 1C will outfall to the 10-inch at the southwest corner

of Unit 15. Upon completion and acceptance of each of these improvements, service for each parcel will be available via routine connection.

Fire Protection: Fire flow rates are determined by the Fire Marshal based on both the size and type of construction. In addition to fire hydrants located at each street intersection, additional hydrants will be required so as not to exceed a maximum distance of 500 feet from any given structure. This distance is measured as the fire equipment travels. The precise number and location of each fire hydrant must be coordinated with the Fire Marshal and approved prior to DRC approval.

Design and Construction of all required improvements will be at the developer / property owner's expense and must be coordinated through the City of Albuquerque via the DRC / City Work Order process. Both water and sewer stubs to each property must be included with the design of the new lines. Designs must be by a New Mexico registered professional engineer. Construction must be by a licensed, bonded public utility contractor.

Easements: City of Albuquerque public water and sewer easements are required for all public lines to be constructed outside of dedicated rights-of-way. Minimum easement widths shall be 20-feet where single service lines are to be constructed and 25-feet where both water and sewer lines are included. Acceptable easements must be documented prior to DRC approval.

Utility Expansion Charges: In addition to installation and construction costs, both sanitary sewer and metered water service to each property will be subject to Utility Expansion Charges (UEC). These charges are payable at the time service is requested and will be based on the ordinances in effect at the time of connection.

Pro Rata Charges: Any and all outstanding pro rata charges assessed towards this property will be due at the time of development. The costs of perimeter and off-site water and sanitary sewer lines may be prorated against adjacent benefiting properties. Such assessments must be requested at the time of development in order to be considered.

Closure: This statement of availability will remain in effect for a period of one (1) year from the date of issue and applies only to the development identified herein. Its validity is, in part, contingent upon the continuing accuracy of the information supplied by the developer. Changes in the proposed development may require reevaluation of availability and should be brought to the attention of the Utility Development Section of the City of Albuquerque as soon as possible. Any outstanding pro rata and standby assessments must be paid at the time service is taken. All charges and rates collected will be based on the ordinances and policies in effect at the time service is actually requested and authorized.

Please feel free to contact the undersigned at (505) 924-3987, or by fax at (505) 924-3864 if you have questions regarding the information presented herein or need additional information.

Sincerely,

Jeremy Hoover, E.I.T. Engineering Associate

Utility Development Services

Public Works Department

Cc: Christian J. Sholtis, P.E. – Bohannan Huston

f/ availability

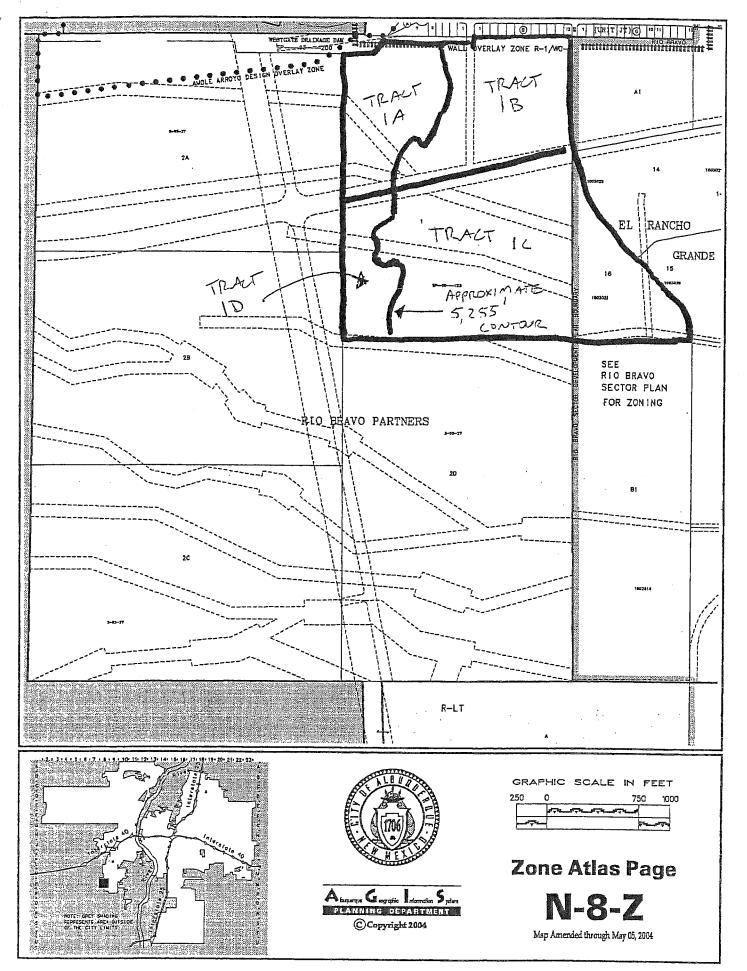
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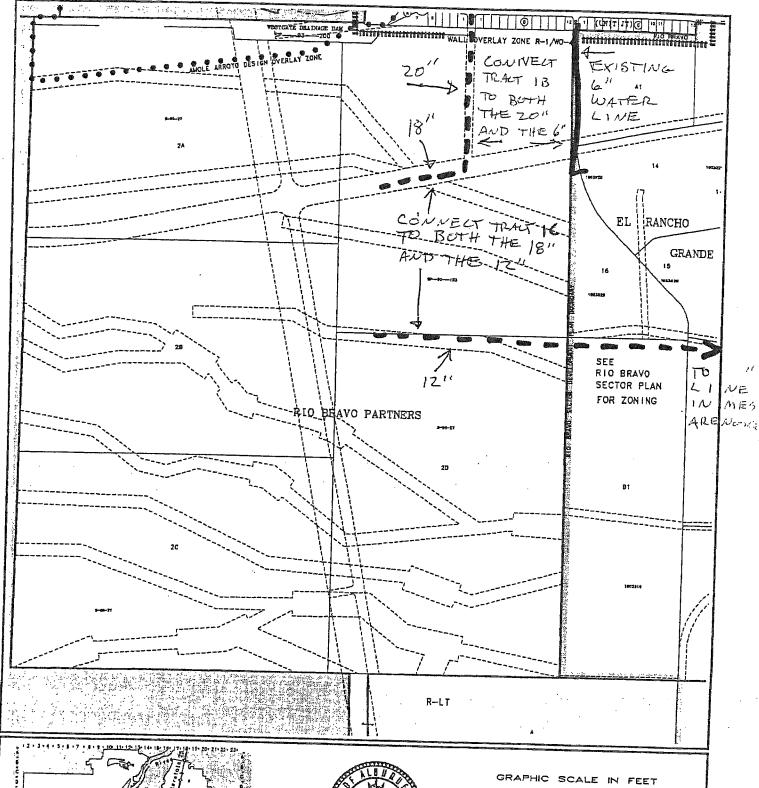
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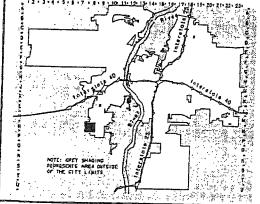
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SITE MAP

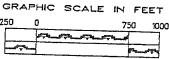






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PLANNING DEPARTMENT

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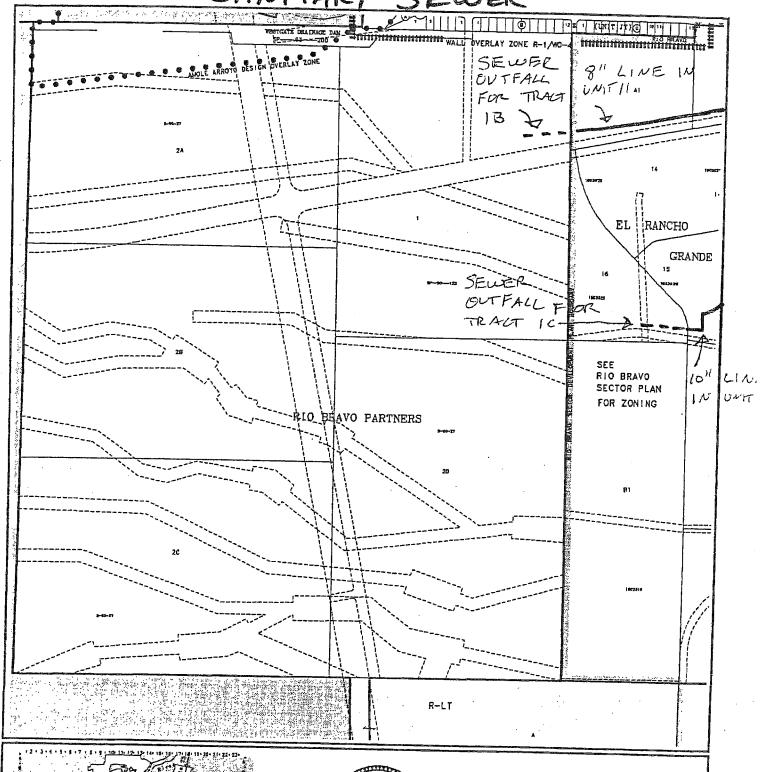


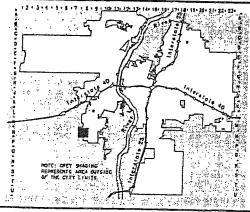
Zone Atlas Page

N-8-Z

Map Amended through May 05, 2004

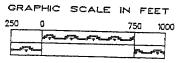
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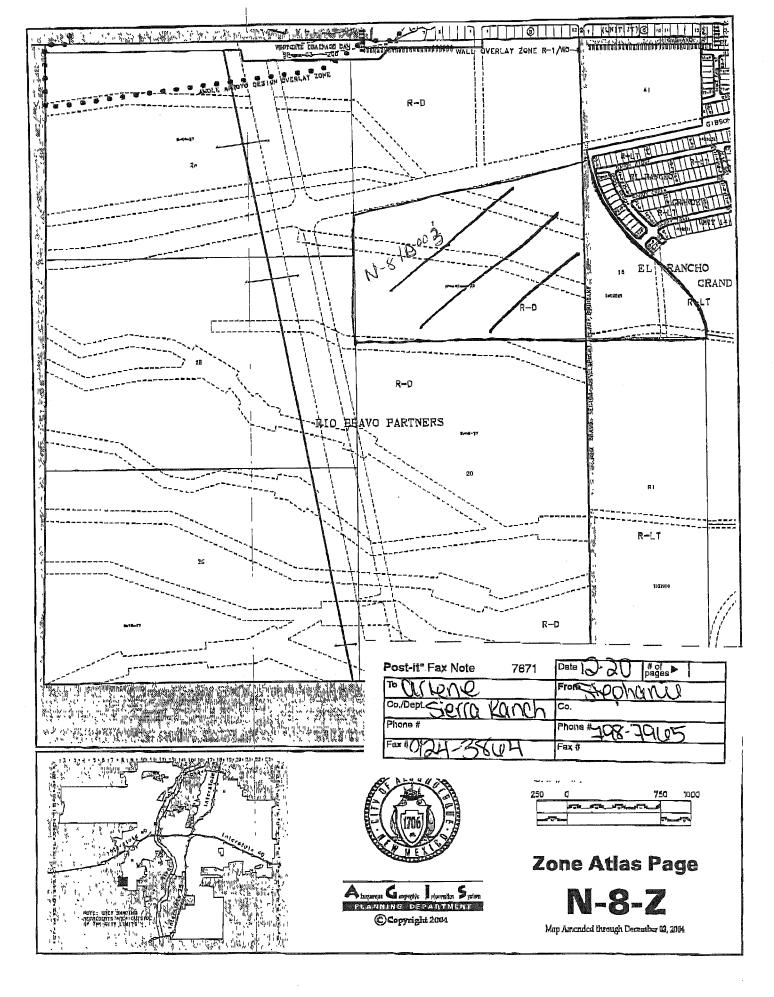
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Zone Atlas Page

N-8-Z

Map Amended through May 05, 2004



DRAINAGE AND TRANSPORTATION INFORMATION SHEET

(REV. 1/28/2003rd)

PROJECT TITLE: SIERRA RANCH SUBDIVISION DRB #EPC#:	ZONE MAP/DRG. FILE #_N-8/D3 WORK ORDER#:
LEGAL DESCRIPTION: El Rancho Grande Tracts 16B and 16C, Tow CITY ADDRESS: South of Gibson Blvd., East of 118 th Street,	n of Atrisco Grant West of Messina Drive, North of Amole Mesa Avenue
ENGINEERING FIRM: Bohannan Huston, Inc. ADDRESS: 7500 Jefferson NE – Courtyard I CITY, STATE: Albuquerque, NM	PHONE: (505) 823-1000
OWNER: Curb Inc. ADDRESS: 5160 San Francisco NE CITY, STATE: Albuquerque, NM	CONTACT: Bo Johnson PHONE: 899-9656 ZIP CODE: 87109
ARCHITECT: ADDRESS: CITY, STATE: SURVEYOR: ADDRESS: CITY, STATE:	PHONE: ZIP CODE: CONTACT: PHONE: ZIP CODE:
CONTRACTOR: ADDRESS: CITY, STATE:	PHONE:
CHECK TYPE OF SUBMITTAL:	S. DEV. PLAN FOR SUB'D. APPROVAL S. DEV. PLAN FOR BLDG. PERMIT APPROVAL SECTOR PLAN APPROVAL FINAL PLAT APPROVAL FOUNDATION PERMIT APPROVAL BUILDING PERMIT APPROVAL CERTIFICATE OF OCCUPANCY (PERM.) CERTIFICATE OF OCCUPANCY (TEMP.) X GRADING PERMIT APPROVAL PAVING PERMIT APPROVAL WORK ORDER APPROVAL OTHER (SPECIFY)
WAS A PRE-DESIGN CONFERENCE ATTENDED: YES NO COPY PROVIDED	E Recd 12-20-04
DATE SUBMITTED: December 16, 2004	_BY:Scott Steffen
Requests for approvals of Site Development Plans and/or Subdi	vision Plats shall be accompanied by a drainage submittal.

Requests for approvals of Site Development Plans and/or Subdivision Plats shall be accompanied by a drainage submittal. The particular nature, location and scope of the proposed development defines the degree of drainage detail. One or more of the following levels of submittal may be required based on the following:

- **1. Conceptual Grading and Drainage Plan:** Required for approval of Site Development Plans greater than five (5) acres and Sector Plans.
- **2. Drainage Plans:** Required for building permits, grading permits, paving permits and site plans less than five (5) acres.
- **3. Drainage Report:** Required for subdivisions containing more than ten (10) lots or constituting five (5) acres or more.

DRAINAGE STUDY FOR SIERRA RANCH SUBDIVISION

DECEMBER 16, 2004

Prepared for:

CURB INC. 5160 SAN FRANCISCO NE ALBUQUERQUE, NM 87109

Prepared by:

BOHANNAN HUSTON, INC. COURTYARD I 7500 JEFFERSON STREET NE ALBUQUERQUE, NM 87109

PREPARED BY:

Scott Steffen, P.E. Date

1-25-05



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EXHIBIT 2 - GRADING PLAN
EXHIBIT 3 - DEVELOPED CONDITIONS BASIN MAP
EXHIBIT 4 - OFFSITE BASIN MAP

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I. INTRODUCTION

This drainage study establishes a drainage management plan for the proposed development of Sierra Ranch. This subdivision is approximately 71 acres of residential (R-LT, R-D) land to be subdivided into 383 single family residential lots. The property is adjacent to the Rio Bravo Sector Plan and is located on Albuquerque's southwest mesa, south of the future Gibson Boulevard and east of 118th Street. Sierra Ranch is in the Amole Arroyo Watershed and encompassed by the Amole-Hubbell Drainage Management Plan.

This study provides hydrologic and hydraulic analysis and provides a drainage management plan as necessary to support the planned 383-unit development. More specifically, this report is submitted in conjunction with the preliminary plat application. Preliminary plat approval and grading plan approval is requested. Prior to final plat and building permit approvals of this project, the City of Albuquerque (COA) must approve final grading plans and work order construction plans.

II. METHODOLOGY

Existing and proposed site hydrological conditions were analyzed for the 100-year, 6-hour storm in accordance with the revised Section 22.2, Hydrology, of the Development Process Manual (DPM) for the City of Albuquerque, dated January 1993. The Arid-lands Hydrologic Model (AHYMO) was utilized to determine peak flow rates for design of the storm drainage improvements within the project. The 100-year, 6-hour storm is used as the design event. The results are included in **Appendix A.** Street capacities were analyzed using Manning's equation, consistent with the revised DPM Section 22.2. The storm sewer system is analyzed using current DPM methods for gravity flow conditions. All data and calculations supporting this study are located in **Appendix B.**

The hydrologic analysis is also based on the approved drainage report: <u>Amole-Hubbell</u>

<u>Drainage Management Plan, Volume I, Final Facilities Plan Report</u> dated July 22, 1999, prepared by Leedshill-Herkenhoff, Inc.

III. EXISTING CONDITIONS

A. Topography

Sierra Ranch is currently undeveloped land with grades ranging from approximately 3% to 6%. The area generally slopes from northwest to southeast. Soils in the area have an SCS soil classification of BCC (Bluepoint loamy fine sand). BCC soils consist of deep, somewhat excessively drained soils formed in sandy alluvial soils, with rapid permeability, slow runoff characteristics, and severe hazard for wind erosion. Vegetation is light consisting mostly of native grasses.

B. Existing Drainage Patterns

Sierra Ranch is located in the Amole Arroyo Drainage Basin. The site generally drains from northwest to southeast. Areas to the east are currently being developed as residential subdivisions. Areas to the north and west of the site are currently undeveloped and discharge undeveloped runoff through the site.

IV. PROPOSED DEVELOPED CONDITIONS

Sierra Ranch subdivision is a proposed single-family residential development with 383 lots on 71 acres. Proposed street configurations are shown on the *Preliminary Plat*, **Exhibit 1.** The Amole-Hubbell DMP allows for full discharge of developed flows from the Amole Arroyo Basin to the Amole and Hubbell Lake storage facilities.

The percent impervious land treatment for the proposed conditions is determined from Table A-5 of the DPM, Section 22.2. The land treatment values used in the AHYMO analysis are the same as the Gibson Boulevard DMP.

A. Offsite Flows

No offsite flows reach the site from the south or east because the natural ground slopes away from Sierra Ranch on these sides. The offsite flow from the north will be intercepted by El Rancho Grande Unit 16 or a temporary pond on that property. If Unit 16 or Gibson Blvd. is built before Sierra Ranch, then the undeveloped runoff from the north

offsite basin (See Offsite Basin Map) will be contained or intercepted by others. If Sierra Ranch is developed before Unit 16, then the undeveloped runoff from the north offsite basin will be contained by a temporary pond within Unit 16. This pond has been sized to contain flows produced from a 100-year 6-hour design storm. If a larger storm occurs, the pond will overflow to the Gibson Blvd. right-of-way.

The property to the west of Sierra Ranch is currently undeveloped. Temporary ponds will be placed to capture the western offsite historic flows until that property develops or 118th Street is built. Since Sierra Ranch will be developed with two phases, each phase must be analyzed separately for offsite flows.

When Phase 1 is developed, the offsite undeveloped flows from Phase 2 and offsite basins 3 and 4 will be contained with a temporary pond on Phase 2. If the Phase 1 development occurs before 118th Street is built, then the temporary pond on Phase 2 will be increased to accommodate additional undeveloped runoff from offsite basins 1 and 2. This pond (See Offsite Basin Map) has been sized to contain flows produced from a 100-year 6-hour design storm. If a larger storm occurs, the pond will overflow to the right-ofway of Walnut Canyon Road.

When Phase 2 is developed, the historic runoff from offsite basins 3 and 4 will be contained with temporary ponds on the property to the west of Phase 2 or the ponds will be located in Phase 2 on encumbered lots. If the Phase 2 development occurs before 118th Street is built, additional temporary ponds will be built on the adjacent parcel within the existing 150' drainage easement to accommodate runoff from offsite basins 1 and 2. These ponds are sized to contain twice the 100-year, 6-hour storm.

The Sierra Ranch subdivision is required to accept developed flows from the western offsite parcel. A storm drain stub will be provided through an easement at the western side of the subdivision. This storm drain will be sized to accept fully developed residential flows from the offsite parcel, based on current zoning.

B. Onsite Flows

Developed runoff from Sierra Ranch will be conveyed by the internal street system to Bison Springs Street, where it will be collected by a public storm drain system. See **Appendix B** for street capacity and inlet capacity calculations. This drainage plan proposes discharging 250 cfs to the storm drain in Messina Drive. Portions of Gibson Blvd., Messina Drive, and Amole Mesa will also discharge into the master storm drain system. (See Basin Map A for contributing basins.) The storm drain is part of the master planned system and has been designed to accept all of the developed runoff from Sierra Ranch.

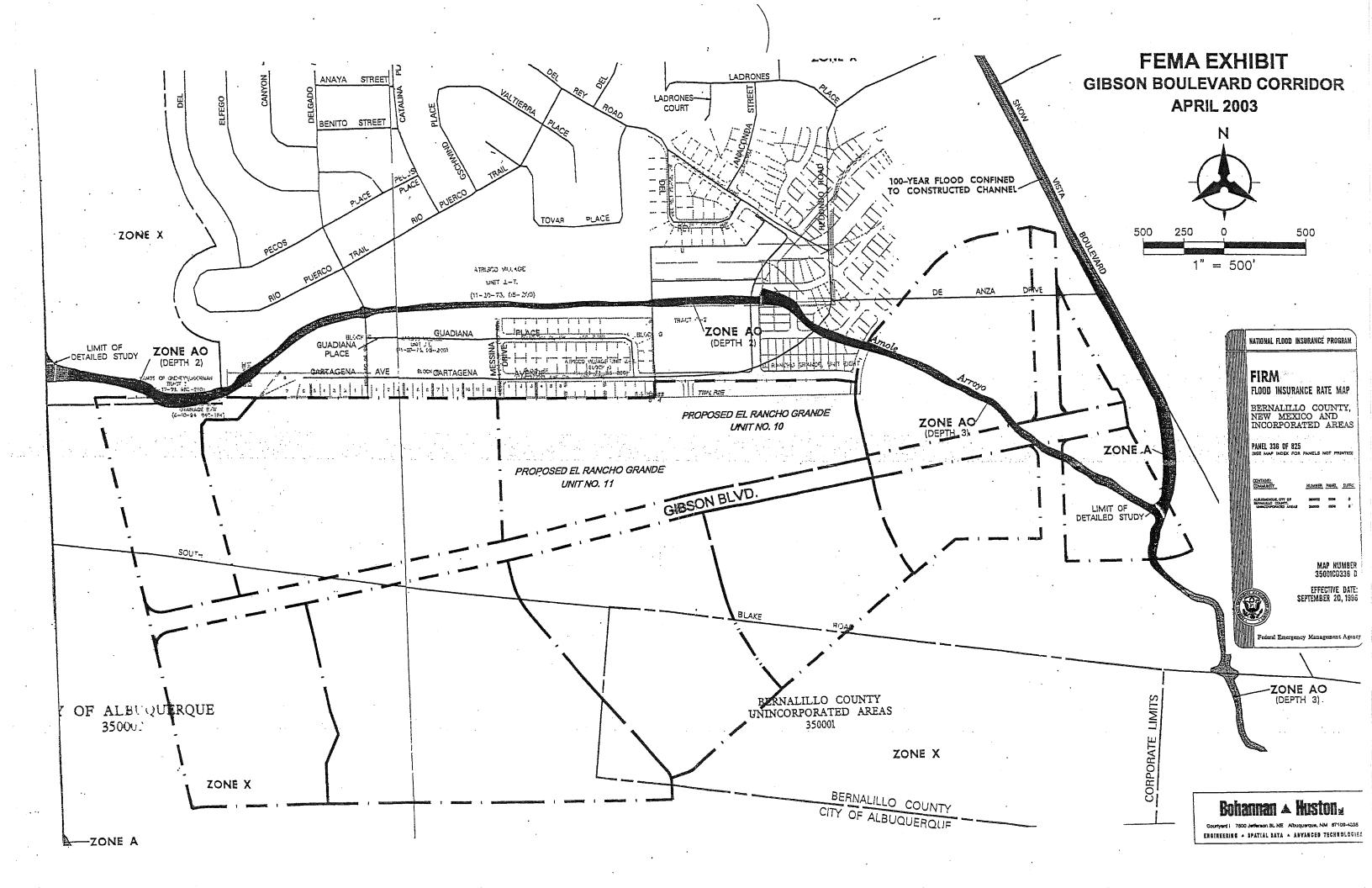
A surge pond located in the park at the southeast corner of the subdivision is connected to the outfall storm drain system in Messina Drive. No developed flows from Sierra Ranch will directly discharge into the pond. The 100-year, 6-hour storm peak flow in the Messina Drive storm drain upstream of the surge pond is 514 cfs. The storm drain system downstream of the surge pond is designed to pass 226 cfs before the hydraulic grade line of the system rises to a level that water will surge into the pond. The peak flow of the 2-year storm is 171 cfs. The peak flow of the 5-year storm is 250 cfs. The storage volume required for the surge pond is 4.2 acre-feet. See **Exhibit 2**, *Grading Plan*, for the location of the pond.

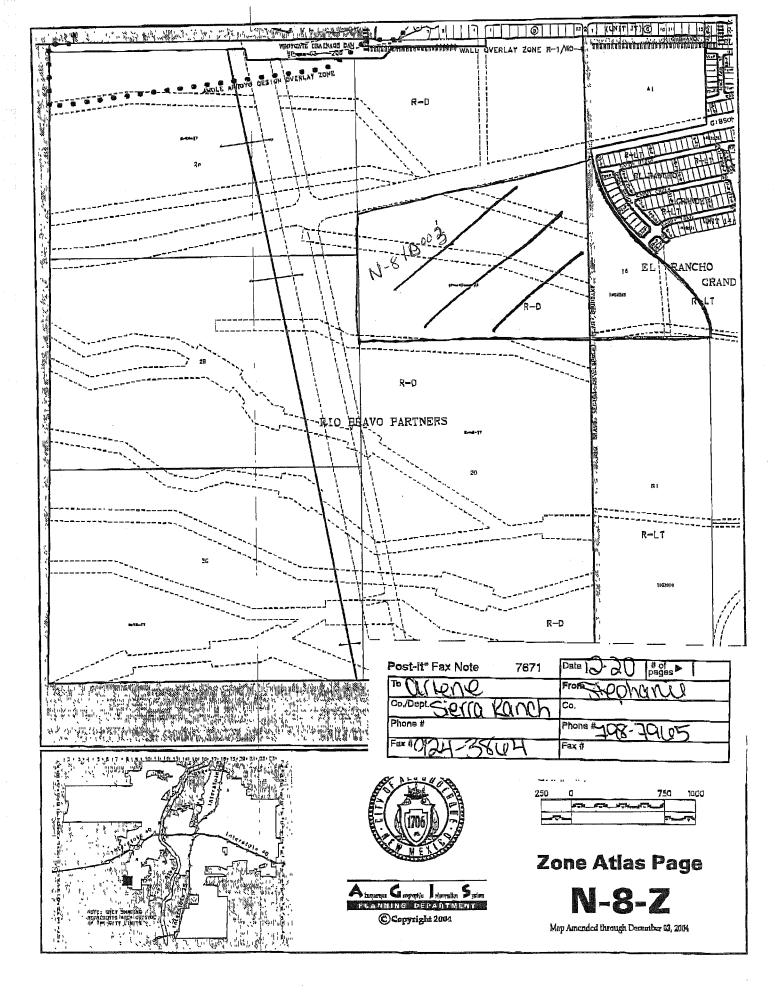
C. FEMA Floodplain

As designated on Panel 336 of 825 (Map number 35001C0336D) of the National Flood Insurance Program, Flood Insurance Rate Maps published by FEMA for Bernalillo County, New Mexico, effective date September 20, 1996, there is no existing flood hazard zone (zone AO) within the proposed development. See the FEMA Floodplain exhibit provided at the end of the report text.

V. CONCLUSION

This report provides a detailed study of the developed runoff and street capacities for the proposed Sierra Ranch Subdivision. Included is the preliminary plat, proposed conditions basin map, grading plan, infrastructure list, and all necessary hydrologic and hydraulic analyses. This drainage plan maintains the overall drainage pattern of the area and allows for the safe management of storm runoff in permanent as well as interim conditions.





DRAINAGE AND TRANSPORTATION INFORMATION SHEET

(REV. 1/28/2003rd)

PROJECT TITLE: SIEDRB#_	RRA RANCH SUBDIVISION	ZON	E MAP/DRG. FILE # <u>N-8/</u> RK ORDER#:	<u></u>
	El Rancho Grande Tracts 16B and 16C, Tov	n of Atrisco	Grant	
CITY ADDRESS:	South of Gibson Blvd., East of 118 th Street,	West of Mes	sina Drive, North of Amole Me	sa Avenue
ENGINEERING FIRM: ADDRESS: CITY, STATE:	Bohannan Huston, Inc. 7500 Jefferson NE – Courtyard I Albuquerque, NM		CONTACT: Scott Steffer PHONE: (505) 823-7 ZIP CODE: 87109	1000
OWNER: ADDRESS: CITY, STATE:	Curb Inc. 5160 San Francisco NE Albuquerque, NM		CONTACT: Bo Johnson PHONE: 899-9656 ZIP CODE: 87109	1
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WAS A PRE-DESIGN CO YES NO COPY PROVIDE	<u>ONFERENCE ATTENDED</u> :		E Recd	12-20-04
DATE SUBMITTED:	December 16, 2004	_BY:	Scott Steffen	· · · · · · · · · · · · · · · · · · ·
Requests for approvals	s of Site Development Plans and/or Subdi	vision Plats	shall be accompanied by a	drainage submittal

Requests for approvals of Site Development Plans and/or Subdivision Plats shall be accompanied by a drainage submittal The particular nature, location and scope of the proposed development defines the degree of drainage detail. One or more of the following levels of submittal may be required based on the following:

- 1. Conceptual Grading and Drainage Plan: Required for approval of Site Development Plans greater than five (5) acres and Sector Plans.
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APPENDICES

APPENDIX A - AHYMO INPUT AND SUMMARY FILES FOR

DEVELOPED CONDITIONS

APPENDIX B - STREET CAPACITY AND STORM DRAIN INLET ANALYSIS

APPENDIX C - INFRASTRUCTURE LIST

APPENDIX A

AHYMO INPUT AND SUMMARY FILES
FOR DEVELOPED CONDITIONS

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	PEAK DISCHARGE (CFS)	RANCH SUBDIVISION (ERG 14 RA.HYM ERRA.OUT 8			*S************************************	*S************************************	48.70	.01830 42.24	*S************************************	.00242 6.30 .234	*S************************************	*S****** 5.98 .223	.00193 5.02 5.02	21.06736	.00990 15.66 .439	
	AREA (SQ MI)	PROJECT NAME: SIERRA RANCH SUBI DATE: DECEMBER 9, 2004 INPUT FILE NAME: SIERRA.HYM OUTUPUT FILE NAME: SIERRA.OUT PROJECT NUMBER: 050188 COMMENTS:100 YEAR-6 HOUR S'		*S************************************	.01950	.02090	*S************************************	01830	. 00267	.00242	68000° 68000°	.00230	.00193	.00912	******	
- (26-	TO ID NO.	PROJECT NAME: SIERRA R DATE: DECEMBER 9, 2004 INPUT FILE NAME: SIERR OUTUPUT FILE NAME: SIE PROJECT NUMBER: 050188 COMMENTS: 100 YEAR-		* - + + + + + + + + + + + + + + + + + +	* C *	4 4	10 +	* * * * * * * * * * * * * * * * * * *	****	*	12	£ + + + + + + + + + + + + + + + + + + +	14	15	16	
(АНҮМС	FROM ID NO.	I NAME DECEM FILE N I FILE I NUMB		*	• + + + + + + + + + + + + + + + + + + +	: + : + : + : +	:) :	: * : ! * : ! *	* * * * *	K + + + + + + + + + + + + + + + + + + +	: * : * : ! * : *	:) : 1) : 1 	;) ; ; ; ;	; -	* * * * * * * *	
PROGRAM SUMMARY TABLE (AHYMO_97) FILE = SIERRA.HYM	HYDROGRAPH IDENTIFICATION	PROJECT NAME: DATE: DECEMBII INPUT FILE NAM OUTUPUT FILE PROJECT NUMBER COMMENTS:	*S ////////////////////////////////////	**************************************	BASIN.B	BASIN.C	BASIN.D	*S************************************	GIBSON.1	*S************************************	AMOLE. 1	AMOLE.2	COMPUTE NM HYD COMPUTE NM HYD	OFF. PRCL	*S************************************	
PROGRAM SUMWARY TZ FILE = SIERRA.HYM	IDE		////////TYPE= 1	*******	M HYD	M HYD	M HYD	******* 4 HYD ******	******* M HYD	******* M HYD	M HYD	M HYD	M HYD	K K K K K K K K K K K K K K K K K K K	******* M HYD *******	
AHYMO PROG INPUT FILE	COMMAND	* * * * * * * * * * * * * * * * * * *	*S ////////////////////////////////////	*S************************************	COMPUTE NM HYD	COMPUTE NM HYD	COMPUTE NM HYD	*S************************************	*S************************************	*S****** COMPUTE NI	COMPUTE NM HYD	COMPUTE NM HYD	*S************************************	COMPUTE NM HYD	*S************************************	FINISH

```
*S*
               PROJECT NAME: SIERRA RANCH SUBDIVISION (ERG 16SOUTH)
*S*
               DATE: NOVEMBER 9, 2004
*S*
               INPUT FILE NAME: OFFSITE.HYM
               OUTUPUT FILE NAME: OFFSITE.OUT
*S*
*S*
               PROJECT NUMBER: 050188
                         100 YEAR-6 HOUR STORM
*S*
               COMMENTS:
TIME=0.0 HR PUNCH CODE=0
                     RAIN QUARTER=0.0
RAINFALL
               TYPE=1
               RAIN ONE=1.90 IN RAIN SIX=2.20 IN
               RAIN DAY=2.60 IN DT=0.05 HRS
*S****IF SIERRA RANCH IS BUILT BEFORE GIBSON BLVD., A POND WILL BE BUILT ON THE
*S****NORTHERN TRACT TO ACCOMMODATE THIS OFFSITE BASIN.************************
               ID=1 HYD NO=NORTH DA=0.1458 SQ MI
COMPUTE NM HYD
               PER A=100 PER B=0 PER C=0 PER D=0
               TP=-0.1333 HR
                           MASSRAIN=-1
               ID=1 CODE=1
PRINT HYD
*5*********************************
               ID=2 HYD NO=BASIN.1
COMPUTE NM HYD
                                 DA=0.0351 SQ MI
               PER A=100 PER B=0 PER C=0 PER D=0
               TP=-0.1333 HR
                          MASSRAIN=-1
PRINT HYD
               ID=2
                    CODE=1
ID=4 HYD NO=BASIN.2 DA=0.0197 SQ MI
COMPUTE NM HYD
               PER A=100 PER B=0 PER C=0
                                    PER D=0
               TP=-0.1333 HR MASSRAIN=-1
               ID=4 CODE=1
PRINT HYD
*5**********************************
*S****IF 118TH IS BUILT BEFORE SIERRA RANCH SUB., THEN PONDS WILL BE BUILT TO
COMPUTE NM HYD ID=5 HYD NO=BASIN.3 DA=0.00433 SQ MI
PER A=100 PER B=0 PER C=0 PER D=0
          TP=-0.1333 HR
                          MASSRAIN=-1
PRINT HYD
              ID=5
                    CODE=1
ID=6 HYD NO=BASIN.4 DA=0.00433 SO MI
COMPUTE NM HYD
               PER A=100 PER B=0 PER C=0 PER D=0
               TP=-0.1333 HR
                          MASSRAIN=-1
PRINT HYD
               ID=6 CODE=1
 *S****IF SIERRA RANCH IS BUILT BEFORE 118TH, THEN PONDS WILL BE BUILT TO
 *S****ACCOMMODATE FLOWS FROM BASINS 1&3 AND BASINS 2&4.*************************
               ID=7 HYD NO=BASIN.1.3 ID I=2
ADD HYD
                                          ID II=5
PRINT HYD
               ID=7
                     CODE=1
 ID=8 HYD NO=BASIN.2.4 ID I=4
                                          ID II=6
ADD HYD
               ID=8
                     CODE=1
PRINT HYD
 *5**********************************
 *S*****PHASE 1 OF THE SIERRA RANCH SUBDIVISION WILL BE BUILT BEFORE PHASE 2.
 *S****THEREFORE, PONDS WILL BE BUILT ON PHASE 2 TO ACCOMMODATE OFFSITE FLOWS****
               ID=9 HYD NO=PHASE.2 DA=0.0448 SQ MI
 COMPUTE NM HYD
               PER A=100 PER B=0 PER C=0
                                      PER D=0
               TP=-0.1333 HR
                           MASSRAIN=-1
                    CODE=1
 PRINT HYD
               TD=9
 *5*********************************
               ID=10
                      HYD NO=BASIN.1234
                                    ID I=7 ID II=8
 ADD HYD
               ID=10
                     CODE=1
 PRINT HYD
 *5**********************************
 *S*****IF PHASE 1 IS BUILT BEFORE 118TH, a POND WILL BE BUILT ON PHASE 2 TO
 *S****ACCOMMODATE ALL THE FLOW FROM THE OFFSITE WESTERN BASINS
 ADD HYD
              ID=11 HYD NO=WEST.TOTAL ID I=9 ID II=10
               ID=11
 PRINT HYD
                      CODE=1
 *5****************************
 FINISH
```

(AHYMO_97)	
MO PROGRAM SUMMARY TABLE	FILE = OFFSITE.HYM
AHYMO	INPUT

0	PEAK PER (HOURS) ACRE NOTATION		TIME= .00 RAIN6= 2.200	1.500 1.373 PER IMP= .00	1.500 1.314 PER IMP= .00	1.500 1.314 PER IMP= .00	1.500 1.316 PER IMP= .00	1.500 1.316 PER IMP= .00	1.500 1.314	1.500 1.314 PER IMP= .00	1.500 1.314	1.500 1.314
	RUNOFF (INCHES)			.44903	.44903	.44903	.44903	.44903	.44903	.44903	.44903	.44903
RUNOFF	VOLUME (AC-FT)	16SOUTH)	11111111111	BUILT ON THE ************************************	.841	.472	E BUILT TO ********* .104	.104	LT TO ******** .944 ********* .575 ************************	SITE FLOWS*** 1.073	1.520 ************************************	2.593
PEAK	DISCHARGE (CFS)	(ERG	CT NUMBER: 050188 COMMENTS:100 YEAR-6 HOUR STORM ////////////////////////////////////	POND WILL BE N.******** 128.08	29.51	16.57	SUB., THEN PONDS WILL BE BUILT TO **********************************	3 · 6 · 5 · 5 · 5 · 5 · 5 · 5 · 5 · 5 · 5	THEN PONDS WILL BE BUILT TO ASSESSED TO THE	2 TO ACCOMMODATE OFFSITE FLOWS*** 04480 37.66 1.073	**************************************	ERN BASINS 91.03 *******
	AREA (SQ MI)	PROJECT NAME: SIERRA RANCH SUBDIVISION DATE: NOVEMBER 9, 2004 INPUT FILE NAME: OFFSITE.HYM OUTUPUT FILE NAME: OFFSITE.OUT	150188 YEAR-6 HOUR ST	BSON BLVD., A OFFSITE BASII	03210	01970	NCH SUB., THEND 4.************************************	.00433	BTH, THEN PONI AND BASINS 26. ************************************		.*************************************	OFFSITE WEST:
O.T.		IE: SIE IMBER 9, NAME: LE NAME:	135K: 0 TS:100 //////	FORE GI	* 2	* * * * * * * * * * * * * * * * * * *	EERRA RA INS 3 AN	* * * *	[BEFORE 11 23 2& 5 7 7 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	SUILT ON	******* 8 10 *******	7ROM THE
OFFSILE: MIN	HYDROGRAPH ID IDENTIFICATION NO.	PROJECT NAME: SIERRA R DATE: NOVEMBER 9, 2004 INPUT FILE NAME: OFFSI OUTUPUT FILE NAME: OFF	PROJE	RAINFALL TYPE= 1 *S****IF SIERRA RANCH IS BUILT BEFORE GIBSON BLVD., A POND WILL BE BUILT ON THE *S****NORTHERN TRACT TO ACCOMMODATE THIS OFFSITE BASIN.************************************	*S************************************	*S************************************	*S*****IF 118TH IS BUILT BEFORE SIERRA RANCH *S****ACCOMMODATE FLOWS FROM BASINS 3 AND 4 COMPUTE NM HYD BASIN.3 - 5	*S************************************	*S************************************	*S*****PHASE I OF THE SIEKKA KANCH SUBLIVISION *S*****THEREFORE, PONDS WILL BE BUILT ON PHASE COMPUTE NM HYD PHASE.2 - 9	*S************************************	*S*****IF PHASE I IS BOILD BEFORE IIOIN, C. TON WESTERN BASINS *S*****ACCOMMODATE ALL THE FLOW FROM THE OFFSITE WESTERN BASINS WEST.TOTAL 9&10 11 **S*********************************
INPUT FILE = OFFSILE.MIN	COMMAND	* * * * ;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;	*S* *S* *S ////////	RAINFALL TYPE= 1 *S****IF SIERRA R *S****NORTHERN TR COMPUTE NM HYD	*S************************************	*S************************************	*S************************************	*S**********	*S************************************	*S****PHASE I *S****THEREFOI COMPUTE NM HYD	*S************************************	*S****1F PHP *S****ACCOMIV ADD HYD

APPENDIX B

STREET CAPACITY AND STORM DRAIN INLET ANALYSIS

SIERRA RANCH SUBDIVISION Internal Street and Storm Drain Inlet Capacity Calculations December 2004

1. Four Mile Road Basin A Q = 37 cfs

The total amount of developed runoff produced from Basin A and a small amount from Gibson Blvd. exceeds the street capacity of Four Mile Road. Therefore, inlets will be placed at the eastern end of the street to intercept a portion of the flow (See Grading Plan for proposed inlet locations). Excess flow will continue on the surface east towards Bison Springs Street. Roll curb may be installed to Lot 254. See PC stream output and inlet nomograph.

2. Corona Ranch Road

Basin B Q = 45 cfs

The total amount of developed runoff produced from Basin B exceeds the street capacity of Corona Ranch Road. Therefore, inlets will be placed before Salado Creek Street to intercept a portion of the flow (See Grading Plan for proposed inlet locations). Excess surface flow will continue east towards Bison Springs Street. Roll curb may be installed to Lot 276. See PC stream output and inlet nomograph. Developed runoff from the western offsite parcel will also discharge through Basin B, however, all the flow will be contained in the storm drain.

3. Walnut Canyon Road

Basin C

Q = 48 cfs

The total amount of developed runoff produced from Basin C exceeds the street capacity of Walnut Canyon Road. Therefore, inlets will be placed at the unit boundary to intercept a portion of the flow (See Grading Plan for proposed inlet locations). The remaining surface flow will continue east towards Bison Springs Street. Roll curb may be installed to Devils Tower Street. See PC stream output and inlet nomograph.

4. Buck Island Road

Basin D

Q = 49 cfs

The total amount of developed runoff produced from Basin D exceeds the street capacity of Buck Island Road. Therefore, inlets will be placed beginning at Lot 139 to intercept a portion of the flow (See Grading Plan for proposed inlet locations). The remaining surface flow will continue east towards Bison Springs Street. Roll curb may be installed to Mountaintop Drive. See PC stream output and inlet nomograph.

5. Pipestone Road

Basin E Q = 42 cfs

The total amount of developed runoff produced from Basin E and a small amount from Amole Mesa Avenue exceeds the street capacity of Pipestone Road. Therefore, inlets will be placed at Mountaintop Drive and Gila Cliff Drive to intercept a portion of the flow (See Grading Plan for proposed inlet locations). The remaining surface flow will continue east towards Big Springs Road. Roll curb may be installed to Devils Tower Street. See PC stream output and inlet nomograph.

6. Big Springs Road

Basin D

Q = 49 cfs

The total amount of developed surface runoff at the east end of Big Springs Road is 21 cfs. A roadway the size of Big Springs Road with standard curb can carry more than 53 cfs. Therefore, inlets are not required in Big Springs Road. The flow will continue east towards Bison Springs Street. See PC stream output.

7. Bison Springs Street

Basins A, B, C, D, E, and offsite parcel Q = 246 cfs

The total developed runoff from the subdivision and the western offsite parcel flows to Bison Springs Street on the roadway surface or in a storm drain. Any remaining surface flow will be captured by inlets in this street. At the southern stub terminus of Bison Springs Street, the internal storm drain connects to the master storm drain system in Messina Drive. The master storm drain system is planned to accommodate all the developed runoff from this subdivision.

The sump inlet located at the southern stub terminus of Bison Springs Street is designed to capture the remaining surface runoff produced from a 100-year 6-hour storm. If a greater storm event occurs, the stub street will act as an emergency overflow spillway towards the surge pond.

FOUR MILE ROAD

MANNING'S N=	.017	SLOPE=	.037
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DOTNE	D.T.CIII	זיהו דהו	DOTNE	DICT	דאר דייד	חרדאותו ה	TOO T	3T 1737		
POINT 1	DIST 0.00	ELEV 0.83	POINT 5	DIST 11.00	ELEV 0.13	POINT D 9 37.		ELEV .67		
2	8.38	0.67	. 6	23.00	0.41			.67		
3	8.83	0.67		35.00	0.13	11 46.		.83		
4	9.00	0.00	8	37.00	0.00			.00		
□ WSEL	DEPTH	FLOW	FLOW V	WETTED	FLOW	TOPWID	VEL	ENERGY		
	INC	AREA	RATE	PER	VEL		HEAD	HEAD	•	
(FT)	(FT)	SQ.FT.	(CFS)	(FT)	(FPS)	(FT)	(FT)	(FT)		
0.01	0.01	0.00	0.0	0.33	0.48	0.31	0.00	0.01		
0.02	0.02	0.01	0.0	0.66	0.75	0.63	0.01	0.03		
0.03	0.03	0.01	0.0	0.99	0.99	0.94	0.02	0.05		
0.04	0.04	0.03	0.0	1.32	1.20	1.25	0.02	0.06		
0.05	0.05	0.04 0.06	0.1 0.1	1.64 1.97	1.39 1.57	1.56	0.03	0.08		
0.06 0.07	0.06 0.07	0.08	0.1	2.30	1.74	1.88 2.19	0.04 0.05	0.10 0.12		2 4
0.07	0.08	0.10		2.63	1.90	2.50	0.05	0.12		
0.00	0.09	0.13	0.3	2.96	2.06	2.81	0.07	0.14		
0.10	0.10	0.16	0.3	3.29	2.21	3.13	0.08	0.18		
0.11	0.11	0.19	0.4	3.62	2.35	3.44	0.09	0.20		
0.12	0.12	0.23	0.6	3.95	2.49	3.75	0.10	0.22		,
0.13	0.13	0.26	0.7	4.28	2.63	4.07	0.11	0.24		
0.14	0.14	0.31	0.8	5.15	2.58	4.93	0.10	0.24		
0.15	0.15	0.36	0.9	6.03	2.58	5.79	0.10	0.25		•
0.16	0.16	0.43	1.1	6.91	2.62	6.65	0.11	0.27		
0.17	0.17	0.50	1.3	7.79	2.68	7.51	0.11	0.28		
	0.18	0.58		8.67	2.76	and the second s			المعاوضية الماد المواجعة المراجعة الماد الماد	
	0.19	0.66			2.84	9.24	•	0.32		
0.20	0.20	0.76	2.2	10.42			0.13	0.33		
0.21	0.21	0.87	2.6		3.03	10.96	0.14	0.35		
0.22	0.22 0.23	0.98 1.10	3.1 3.6	12.18 13.06	3.13 3.24	11.83 12.69	0.15 0.16	0.37 0.39		
0.23	0.23	1.23	4.1	13.00	3.34	13.55	0.10	0.39		
0.25	0.25	1.37	4.7	14.81	3.44	14.41	0.18	0.43		
0.26	0.26	1.52	5.4	15.69	3.55	15.27	0.20	0.46		
0.27	0.27	1.68	6.1	16.57	3.65	16.14	0.21	0.48		-
0.28	0.28	1.84	6.9	17.45	3.76	17.00	0.22	0.50		
0.29	0.29	2.02	7.8	18.32	3.86	17.86	0.23	0.52	-Pau	01102
0.30	0.30	2.20	8.7	19.20	3.97	18.72	0.24	0.54		CURB
0.31	0.31	2.39	9.7	20.08	4.07	19.59	0.26	0.57	LIN	11T
0.32	0.32	2.59	10.8	20.96	4.17	20.45	0.27	0.59		
0.33	0.33	2.80	12.0	21.84	4.28	21.31	0.28	0.61		
0.34						22.17		0.64		
0.35 0.36			14.5 15.9		4.48 4.58	23.03 23.90	0.31 0.33	0.66 0.69		
0.30		3.48 3.72	17.4			24.76	0.33		,	
0.38			19.0	26.23	4.78	25.62	0.35	0.73		
0.39			20.7		4.88	26.48				
0.40			22.4			27.35	0.38	0.78		
0.41			24.3				0.40			
0.42		5.06	26.7		5.27	28.21	0.43			
0.43	0.43	5.35	29.2	28.90	5.46	28.22	0.46	0.89		
☐ WSEL	DEPTH			WETTED	FLOW	TOPWID	VEL	ENERGY		
	INC	AREA		PER	VEL		HEAD			
(FT)			. (CFS)			(FT)				
0.45		5.91	34.5				0.53	0.98		
0.46			37.2			28.23				
0.47			40.1	28.98	6.19	28.24		1.07		
0.48			43.0	29.01	6.37	28.24				
0.49	0.49	7.04	46.0	29.03	6.54	28.25	0.66	1.15		

FOUR MILE ROAD

POINT	DIST	ELEV	POINT	T DIST	ELEV	POINT	DIST	ELEV		
1	0.00	0.83	5	11.00	0.13			0.67		
2.	8.38	0.67	. 6	23.00	0.41			0.67		
3 .	8.83	0.67		35.00	0.13			0.83		*
4	9.00	0.00	8	37.00	0.00			0.00		
□ WSEL	DEPTH	FLOW		WETTED	FLOW	TOPWID	VEL	ENERGY		
	INC	AREA	RATE	PER	VEL		HEAD	HEAD		
(FT)	(FT)	SQ.FT.	(CFS)	(FT)	(FPS)	(FT)		(FT)		
0.01	0.01	0.00	0.0	0.33	0.46	0.31		0.01		
0.02	0.02	0.01	0.0	0.66	0.72	0.63				
0.03	0.03	0.01	0.0	0.99	0.95	0.94	0.01	0.04		
0.04	0.04	0.03	0.0	1.32	1.15	1.25		0.06		
0.05	0.05	0.04	0.1	1.64	1.33	1.56				
0.06	0.06	0.06	0.1	1.97	1.50	1.88				
0.07	0.07	0.08	0.1	2.30	1.67	2.19				
0.08	0.08	0.10	0.2	2.63	1.82	2.50			• .	
0.09	0.09	0.13	0.2	2.96		2.81			•	
0.10	0.10	0.16	0.3	3.29	2.12	3.13				
0.11	0.11	0.19	0.4	3.62	2.25	3.44				
0.12	0.12	0.23	0.5		2.39	3.75				
0.13 0.14	0.13 0.14	0.26 0.31	0.7 0.8	4.28 5.15	2.52	4.07				
0.14	0.14	0.31	0.8		$2.47 \\ 2.47$	4.93 5.79				
0.15	0.15	0.36	1.1	6.03	$2.47 \\ 2.51$	6.65				
0.13	0.17	0.50	1.3	7.79	2.57					0
		0.58					0.10	0.27		
	0.19			9.54		9.24		0.23		
0.20			2.1	10.42			0.12			
0.21			2.5		2.91	10.96				
0.22			2.9	12.18	3.00	11.83				
0.23		1.10	3.4	13.06	3.10	12.69				
0.24			3.9	13.93	3.20	13.55				÷
025			4.5	14.81	3.30	14.41				
0.26	0.26	1.52	5.2	15.69	3.40	15.27				* <u>=</u>
0.27	0.27	1.68	5.9	16.57	3.50	16.14	0.19	0.46		
0.28	0.28	1.84	6.6	17.45	3.60	17.00	0.20	0.48		
0.29			7.5	18.32	3.70	17.86				
0.30			8.4	19.20	3.80	18.72				
0.31			9.3	20.08	3.90	19.59				
0.32			10.4	20.96	4.00	20.45				
0.33			11.5	21.84	4.10	21.31				
0.34			12.7	22.71	4.20	22.17				
0.35			13.9	23.59	4.30	23.03				
0.36 0.37			15.3 16.7	24.47	4.39	23.90			•	
0.38			18.2	25.35 26.23	4.49 4.58	24.76				
0.39			19.8	27.10	4.68	25.62 26.48				
0.40			21.5	27.10	4.77	27.35				
0.41			23.3	28.86	4.86	28.21				
0.42			25.6		5.05	28.21				
0.43			28.0	28.90	5.23	28.22			سرسر برمساند	2.0.
□ WSEL	DEPTH		FLOW		FLOW	TOPWID	VEL	ENERGY	STREET	CAPACIT
	INC	AREA	RATE	PER	VEL	-01.11	HEAD	HEAD	•	
(FT)	(FT)			(FT)	(FPS)	(FT)	(FT)	(FT)		
0.45			33.0		5.59	28.23				
0.46			35.7		5.76	28.23				
0.47			38.4		5.93	28.24				
0.48			41.2		6.10	28.24				
0.49			44.1		6.27	28.25				

CORONA RANCH ROAD

MANNING'S N	= .017	SLOPE=	.037
THE THINK THE		O4014	

POINT DIST ELEV POINT DIST ELEV POINT D	Tom Ditai
	IST ELEV
1 0.00 0.83 5 11.00 0.13 9 37.	
2 8.38 0.67 6 23.00 0.41 10 37.	
3 8.83 0.67 7 35.00 0.13 11 46.	
	0.00
U WSEL DEPTH FLOW FLOW WETTED FLOW TOPWID	VEL ENERGY
INC AREA RATE PER VEL	HEAD HEAD
(FT) (FT) SQ.FT. (CFS) (FT) (FPS) (FT)	(FT) (FT)
	0.00 0.01
0.02 0.02 0.01 0.0 0.66 0.75 0.63	0.01 0.03
0.03 0.03 0.01 0.0 0.99 0.99 0.94	0.02 0.05
0.04 0.04 0.03 0.0 1.32 1.20 1.25	0.02 0.06
0.05 0.05 0.04 0.1 1.64 1.39 1.56	0.03 0.08
0.06 0.06 0.06 0.1 1.97 1.57 1.88	0.04 0.10
0.07 0.07 0.08 0.1 2.30 1.74 2.19	0.05 0.12
0.08 0.08 0.10 0.2 2.63 1.90 2.50	0.06 0.14
	0.07 0.16
0.10 0.10 0.16 0.3 3.29 2.21 3.13	0.08 0.18
0.11 0.11 0.19 0.4 3.62 2.35 3.44	0.09 0.20
0.12 0.12 0.23 0.6 3.95 2.49 3.75	0.10 0.22
0.13 0.13 0.26 0.7 4.28 2.63 4.07	0.11 0.24
0.14 0.14 0.31 0.8 5.15 2.58 4.93	0.100.24
0.15 0.15 0.36 0.9 6.03 2.58 5.79	0.10 0.25
0.16 0.16 0.43 1.1 6.91 2.62 6.65	0.11 0.27
	0.11 0.27
	- T.O. 12 / O. 30 - Francisco de la companya de la
0.19 0.19 0.66 1.9 9.54 2.84 9.24	0.13 0.32
0.20 0.20 0.76 2.2 10.42 2.94 10.10	0.13 0.33
0.21 0.21 0.87 2.6 11.30 3.03 10.96	0.14 0.35
0.22 0.22 0.98 3.1 12.18 3.13 11.83	0.15 0.37
0.23 0.23 1.10 3.6 13.06 3.24 12.69	0.16 0.39
0.24 0.24 1.23 4.1 13.93 3.34 13.55	0.17 0.41
0.25 0.25 1.37 4.7 14.81 3.44 14.41	
0.26 0.26 1.52 5.4 15.69 3.55 15.27	0.20 0.46
0.27 0.27 1.68 6.1 16.57 3.65 16.14	0.21 0.48
0.28 0.28 1.84 6.9 17.45 3.76 17.00	0.22 0.50
0.29 0.29 2.02 7.8 18.32 3.86 17.86	0.23 0.52
0.30 0.30 2.20 8.7 19.20 3.97 18.72	0.24 0.54 7 4
0.31 0.31 2.39 9.7 20.08 4.07 19.59	0.26 0.57 ROLL CURB
0.32 0.32 2.59 10.8 20.96 4.17 20.45	
0.33 0.33 2.80 12.0 21.84 4.28 21.31	0.27 0.59 0.28 0.61 LIMIT
0.34 0.34 3.02 13.2 22.71 4.38 22.17	
0.35 0.35 3.25 14.5 23.59 4.48 23.03	0.31 0.66
0.36 0.36 3.48 15.9 24.47 4.58 23.90	0.33 0.69
0.37 0.37 3.72 17.4 25.35 4.68 24.76	
0.38 0.38 3.98 19.0 26.23 4.78 25.62	0.35 0.73
0.39 0.39 4.24 20.7 27.10 4.88 26.48	0.37 0.76
0.40 0.40 4.50 22.4 27.98 4.98 27.35	0.38 0.78
0.41 0.41 4.78 24.3 28.86 5.07 28.21	0.40 0.81
	0.43 0.85
0.43 0.43 5.35 29.2 28.90 5.46 28.22	0.46 0.89
☐ WSEL DEPTH FLOW FLOW WETTED FLOW TOPWID	VEL ENERGY
INC AREA RATE PER VEL	HEAD HEAD
(FT) (FT) $SQ.FT.$ (CFS) (FT) (FPS) (FT)	(FT) (FT)
0.45 0.45 5.91 34.5 28.94 5.83 28.23	0.53 0.98
0.46 0.46 6.19 37.2 28.96 6.01 28.23	0.56 1.02
0.20 0.20 0.40 0.40 0.01 20.20	3.30 1.02
	0 60 1 07
0.47 0.47 6.48 40.1 28.98 6.19 28.24	0.60 1.07
	0.60 1.07 0.63 1.11 0.66 1.15

MANNING'S N= .017 SLOPE= .0316

1.15.771/1.TIA	D 11	OI, BHOI		_						
POINT	DIST	ELEV	POINT	DIST	ELEV	POINT I	DIST	ELEV		
1	0.00	0.83	5	11.00	0.13	9 37.				
2	8 38	0.67	6	23.00	0.41.	1037.				
	8.83	0.67		35.00	0.13			.83		
4	9.00			37.00	0.00	12 0.		- 00		
		FLOW		WETTED	FLOW		VEL			
	INC	APEA	PATE	OHD	WET.					
(FT)	(FT)	SO FT	(CES)	(FT)	(EDG)	(FT)	(ET)	(Em.)		
0.01	0.01	0.00	0.0	0.33	0.44	0.31	0.00	0.01		
0.02	0.02			0.66		0.63	0.00	0.01		
0.02	0.02	0.01	0.0	0.99		0.03	0.01			
0.03	0.03	0.01	0.0	1.32	0.91	0.94	0.01	0.04		
0.04	0.04	0.03	0.1	1.64	1.11	1.25 1.56	0.02	0.06		
	0.05				1.28	1.56	0.03	0.08	•	
0.06			0.1	1.97	1.45	1.88	0.03	0.09		
0.07	0.07	0.08	0.1	2.30	1.61	2.19	0.04	0.11		
0.08	0.08	0.10	0.2	2.63 2.96	1.76	2.50 2.81	0.05	0.13		-
0.09	0.09	0.13	0.2	2.96	1.90	2.81	0.06			
0.10	0.10	0.16	0.3	3.29	2.04			0.16		
0.11	0.11	0.19	0.4	3.62	2.17	3.44	0.07			
0.12	0.12	0.23	0.5	3.95	2.30	3.75	0.08			
0.13	0.13	0.26	0.6	4.28	2.43	4.07	0.09	0.22		
0.14	0.14	0.31				4.93	0.09	0.23		
	0.15	0.36	0.9	6.03	2.39	5.79	0.09	0.24		
0.16	0.16	0.43	1.0	6.91 7.79	2.42	6.65 7.51	0.09	0.25 0.27		
0.17	0.17	0.50	1.2	7.79	2.48	7.51	0.10	0.27		
0.18	0.18	0.58	1.5	8.67	2.55	8.38	0.10	0.28	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	gerake jawa wa
0.19	0.19	0.66	1.7	9.54	2.63	9.24	0.11	0.30		
0.20	0.20	0.76	2.1	10.42	2.71	10.10	0.11	0.31		
0.21	0.21		2.4	11.30	2.80	10.96	0.12			
0.22	0.22		2.8			11.83	0.13			
0.23	0.23	1.10	3.3							
0.24	0.24	1 22	3 0	13.93	3.09	13.55	0.15	0.39		
0.25	0.25		4.4	14.81	3.09 3.18	14.41	0.16	0.41		
0.26	0.26	1.52	5.0	15.69	3.28					
0.27	0.27		5.7	16.57	3.38	16.14	0.18			
0.28	0.28	1.84	6.4	17.45	3.47	17.00	0.19			
0.29	0.29	2.02	6.4 7.2	17.45 18.32	3.57	17.86	0.20			
0.30	0.30	2.20	8.1	19.20	3.67	18.72	0.21			
0.31			9.0	20.08	3.76	19.59				
0.32			10.0	20.00	3.86	20.45	0.23			
0.33	0.32 0.33	2.80		20.96 21.84	3.95	20.45 21.31	0.24			
0.34	0.34	3.02	12.2	22.71	4.05	22.17	0.25	0.59		
0.35	0.35	3.25	13.4	23.59	4.14	23.03	0.23			
0.36	0.35		14.7	24.47					~	
					4.23	23.90	0.28	0.64	,	
0.37	0.37		16.1	25.35		24.76	0.29			
0.38	0.38		17.6	26.23	4.42	25.62	0.30			
0.39	0.39		19.1		4.51	26.48	0.32			
0.40	0.40		20.7		4.60	27.35	0.33			
0.41	0.41		22.4	28.86	4.69	28.21	0.34			
0.42	0.42	5.06	24.7	28.88	4.87	28.21	0.37			
0.43	0.43		27.0	28.90	5.04	28.22	0.40	0.83 ENERGY	CTORI	<u>س</u> ـــــــــ
□ WSEL	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	VEL	ENERGY	2 IKU	-1
	INC	AREA	RATE	PER	VEL		HEAD	HEAD	<i>A</i>)	PACITY
(FT)	(FT)	SQ.FT.	(CFS)	(FT)	(FPS)	(FT)	(FT)	(FT)	_	
0.45	0.45	5.91	31.9	28.94	5.39		0.45			
0.46			34.4		5.56		0.48			
0.47			37.1		5.72		0.51			
0.48			39.8		5.88	28.24	0.54			
0.49			42.6		6.04		0.57			
		,			- · • •	_0.23	5.57	1.00		•

alyzer Report

Orainage Structure Analyzer

STORM DRAIN FROM

pe Hydraulic Analysis

OFFSITE PARCEL

Date: Thursday, November 18, 2004 13:28:40

Input Data

| ape | Circular | RC C76-A | Roughness | 0.013000 | Cithod | Manning | ow Rate | 21.1 cfs | Lope | 2.000% | Size (W x T): | 24.00 x 2.5000 |

tput Results

Flow Rate 21.1 cfs
.ope 2.000%
'D 0.59
Capacity 32.0 cfs
Velocity 10.88 ft/s
.pth 1.18 ft
.itical Depth 1.64 ft
Size (W x T): 24.00 x 2.5000

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A alyzer Report
```

Drainage Structure Analyzer

I pe Hydraulic Analysis

SALADO CREEK ST.

Date: Thursday, November 18, 2004 13:55:00

Input Data

: ape	Circular
l terial	RC C76-A
Roughness	0.013000
1 thod	Manning
] ow Rate	36.9 cfs
£_ope	2.400%
Size (W x T):	24.00×2.5000

tput Results

t tput Results			
Flow Rate		36.9	cfs
ope		2.400%	
D D		0.88	
Capacity		35.0	cfs
Velocity		12.62	ft/s
pth		1.76	ft
itical Depth		1.93	ft
Size (W x T):	24.00 x	2.5000	

WALNUT CANYON ROAD

MANNING	'S N= .	017 SLOP	E= .03	88						
POINT	DIST	ELEV	POINT	DIST	ELEV			ELEV		
1	0.00	0.83	5	11.00	0.13			.67		
2	8.38	0.67	6 .		0.41			.67		
3	8.83	0.67	7	35.00	0.13		.00 0	.83		
4	9.00	0.00	8	37.00	0.00	12 0	.00 0	.00		
☐ WSEL	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	VEL	ENERGY		
	INC	AREA	RATE	PER	VEL		HEAD	HEAD		
(FT)	(FT)	SQ.FT.	(CFS)	(FT)	(FPS)	(FT)	(FT)	(FT)		
0.01	0.01	0.00	0.0	0.33	0.49		0.00	0.01		
0.02	0.02	0.01	0.0	0.66	0.77		0.01	0.03		
0.03	0.03	0.01	0.0	0.99	1.01	0.94	0.02	0.05		
0.04	0.04	0.03	0.0	1.32	1.01 1.23	1.25	0.02	0.06		
0.05	0.05	0.04	0.1	1.64	1.42	1.56	0.03	0.08		
0.06	0.06	0.06	0.1	1.97	1.61	1.88	0.04	0.10		
0.07	0.07	0.08 0.10	0.1	2.30	1.78	2.19		0.12		
0.08	0.08	0.10	0.2	2.63	1.95 2.11	2.50	0.06	0.14		
0.09	0.09	0.13	0.3	2.96	2.11	2.81	0.07	0.16		
0.10	0.10	0.16	0.4	3.29	2.26	3.13	0.08	0.18		
0.11	0.11	0.19	0.5	3.62	2.41	3.44	0.09	0.20		
0.12	0.12	0.23	0.6	3.95	2.55 2.69	3.75	0.10			
0.13	0.13	0.23 0.26	0.7	4.28	2.69	4.07	0.11	0.24		
0.14	0.14	0.31	0.8	5.15	2.64	4.93	0.11	0.25		
0.15	0.15	0.36 0.43 0.50	1.0	6.03	2.64 2.68 2.75	5.79	0.11	0.26		
0.16	0.16	0.43	1.1	6.91	2.68	6.65	0.11			
0.17	0.17	0.50	1.4	6.91 7.79	2.75	7.51	0.12	0.29	•	
0.18.	0.18	0.58:	1.6	8.67	2.82	:8.38	0.12	0.30		and the second
0.19	0.19	0.66	1.9	9.54	2.91	9.24	0.13	0.32		
0.20		0.76	2.3	10.42	3.01	10.10	0.14			4
0.21	0.21	0.87	2.7	11.30	3.11	10.96	0.15			
0.22	0.22	0.98	3.1	12.18		11.83				
0.23	0.23	1.10	3.7 4.2 4.8 5.5	13.06	3.31	12.69	0.17			
0.24	0.24	1.23	4.2	13.93	3.42	13.55	0.18			
0.25	0.25	1.37	4.8	14.81	3.42 3.53	14.41	0.19			
0.26	0.26	1.52	5.5	15.69	3.63	15.27	0.21	0.47		
0.27	0.27	1.68	6.3	16.57	3.74	16.14	0.22	0.49		
0.28	0.28	1.84	7.1	17.45	3.85	17.00	0.23	0.51		
0.29	0.29	2.02	8.0	18.32	3.96	17.86	0.24	0.53	ROLL	1400
0.30	0.30		8.9	19.20	4.06	18.72	0.26		ROLL	CURB
0.31	0.31	2.39	10.0	20.08	4.17	19.59	0.27	0.58	LI	MIT
0.32	0.32	2.59	11.1	20.96	4.28	20.45	0.28	0.60	<u></u>	, and I
0.33	0.33		12.3	21.84	4.38	21.31	0.30	0.63		
0.34	0.34	3.02	13.5	22.71	4.48	22.17	0.31	0.65		
0.35	0.35		14.9	23.59	4.59	23.03	0.33			
0.36	0.36	3.48	16.3	24.47		23.90	0.34	0.70		
0.37	0.37		17.8	25.35	4.79	24.76	0.36	0.73		
0.38	0.38	3.98	19.5	26.23	4.89	25.62	0.37	0.75		
0.39	0.39	4.24	21.2	27.10	5.00	26.48	0.39	0.78		
0.40	0.40		23.0	27.98	5.10	27.35	0.40	0.80		
0.41	0.41	4.78	24.8	28.86	5.19	28.21	0.42	0.83		
0.42	0.42		27.3	28.88	5.39	28.21	0.45	0.87		
0.43	0.43	5.35	29.9	28.90	5.59	28.22	0.49	0.92		
□ WSEL	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	VEL	ENERGY		
	INC	AREA	RATE	PER	VEL		HEAD	HEAD		
(FT)	(FT)	SQ.FT.	(CFS)	(FT)	(FPS)	(FT)	(FT)	(FT)		
0.45			35.3	28.94	5.97	28.23	0.55	1.00		-
0.46			38.1	28.96	6.16	28.23	0.59	1.05		
0.47			41.1	28.98	6.34	28.24	0.62			
0.48			44.1	29.01	6.52	28.24				
0.49	0.49	7.04	47.2	29.03	6.70	28.25	0.70	1.19		

SEPTEMBER 1994

MANNING'S N=	.017	SLOPE=	.0275
THANKINI D II —	. 0 1 /		. 0 2 / 3

POINT	DIST	ELEV	POINT	DIST	ELEV	POINT D	IST	ELEV		
1	0.00	0.83		11.00	0.13	9 37.	17 0	.67		
2 .	8.38	0.67	6	23.00	0.41	10 37.	63 0	.67		
3	8.83	0.67		35.00	0.13	11 46.	00 0	.83		
4	9.00	0.00		37.00	0.00	12 0.	00 0	.00		
☐ WSEL	DEPTH	FLOW		ETTED	FLOW	TOPWID	VEL	ENERGY		
	INC	AREA	RATE	PER	VEL		HEAD	HEAD		
(FT)	(FT)	SQ.FT.	(CFS)	(FT)	(FPS)	(FT)	(FT)	(FT)		
0.01	0.01	0.00	0.0	0.33	0.41	0.31	0.00	0.01		
0.02	0.02	0.01	0.0	0.66	0.65	0.63	0.01			
0.03	0.03	0.01	0.0	0.99	0.85	0.94	0.01	0.04		
0.04	0.04	0.03	0.0	1.32	1.03	1.25	0.02	0.06		
0.05	0.05	0.04	0.0	1.64	1.20	1.56	0.02	0.07		
0.06	0.06	0.06	0.1	1.97	1.35	1.88	0.03	0.09		
	0.07	0.08		2.30	1.50	2.19	0.03	0.10		
0.08	.0.08	0.10		2.63	1.64	2.50	0.04	0.12	•	
0.09	0.09	0.13 0.16	0.2 0.3	2.96 3.29	1.77	2.81 3.13	0.05	0.14 0.16		
0.10	0.10 0.11	0.19	0.3	3.62	1.90 2.03	3.44	0.06 0.06	0.16		•
0.11 0.12	0.11		0.5		2.03	3.44	0.08		-	
0.12	0.12	0.25	0.6	4.28	2.13	4.07	0.08	0.19		
0.13	0.13	0.20	0.7	5.15	2.27	4.93	0.08	0.21		
0.15	0.14	0.36	0.8	6.03	2.23	5.79	0.08	0.22		
0.16	0.15	0.43	1.0		2.26	6.65	0.08	0.23		
0.17	0.17	0.50	1.1	7.79	2.31		0.08	0.25		
0.18		0.58				8.38				and the second second
0.19	0.19	0.66	1.6	9.54	2.45	9.24	0.09	0.28		
0.20		0.76			2.53			0.30		
0.21	0.21	0.87	2.3	11.30		10.96	0.11	0.32		
0.22	0.22	0.98	2.6	12.18		11.83	0.11	0.33		
0.23	0.23	1.10	3.1	13.06	2.79	12.69	0.12	0.35		-
0.24	0.24	1.23	3.5	13.93	2.88	13.55	0.13	0.37		
0.25	0.25	1.37	4.1	14.81	2.97	14.41	0.14	0.39		
0.26	0.26	1.52	4.7	15.69	3.06	15.27	0.15	0.41		
0.27	0.27	1.68	5.3	16.57	3.15	16.14	0.15	0.42		
0.28	0.28	1.84	6.0	17.45	3.24	17.00	0.16	0.44		
0.29	0.29	2.02	6.7	18.32	3.33	17.86	0.17	0.46		
0.30	0.30	2.20	7.5	19.20	3.42	18.72	0.18	0.48		
0.31	0.31	2.39	8.4	20.08	3.51	19.59	0.19	0.50		
0.32	0.32	2.59	9.3	20.96	3.60		0.20	0.52		
0.33	0.33	2.80	10.3	21.84	3.69	21.31	0.21	0.54		
0.34	0.34	3.02	11.4	22.71	3.78	22.17	0.22			
0.35	0.35	3.25	12.5	23.59	3.86					•
0.36		3.48	13.7	24.47	3.95		0.24			
0.37		3.72	15.0	25.35	4.04	24.76	0.25			
0.38		3.98	16.4	26.23	4.12	25.62	0.26			
0.39		4.24	17.8	27.10	4.21	26.48	0.27			
0.40		4.50	19.3	27.98	4.29	27.35	0.29			
0.41			20.9	28.86	4.37	28.21	0.30			
0.42		5.06	23.0	28.88	4.54	28.21	0.32			
0.43		5.35	25.2	28.90 WETTED	4.71	28.22	0.34			
□ WSEL	DEPTH				FLOW	TOPWID	VEL	ENERGY		
/ mm)	INC	AREA	RATE (CES)	PER (FT)	VEL	(mam)	HEAD	HEAD		
(FT) 0.45	(FT) 0.45	SQ.FT. 5.91	(CFS) 29.7	28.94	(FPS) 5.03	(FT) 28.23	(FT) 0.39	(FT)		
0.45			32.1	28.96	5.18	28.23	0.39	0.84	-STREE	57
0.40			34.6	28.98	5.10	28.24	0.44		_ \\ \V \\	ACITY
0.47			37.1	29.01	5.49	28.24	0.44		UMP	40119
0.49			39.7	29.03	5.64	28.25	0.49			1
U. 1 2	0.49	,.04	٠. ١	د ب . د د	J. U±	20.23	0.47	U. 20		

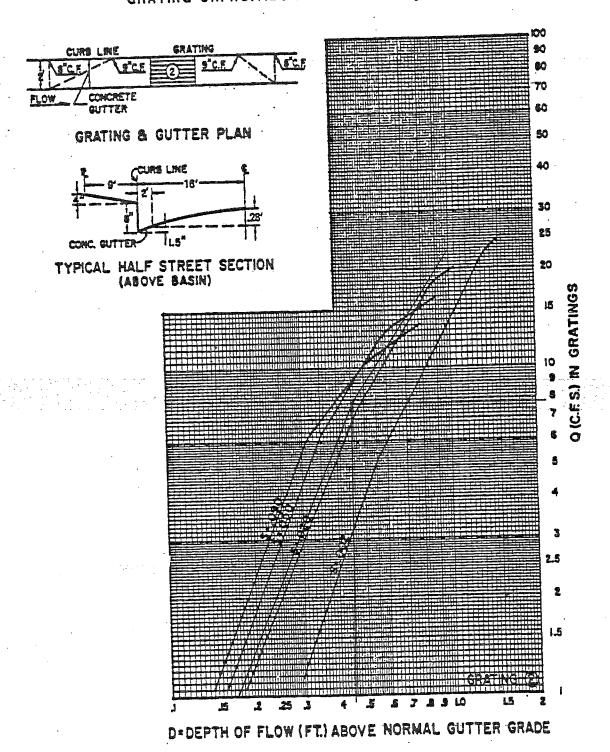
WALNUT CANYON ROAD

MANNING'S	S N= .	017 SLOP	E= .032	2					
POINT I	DIST	ELEV	POINT	DIST	ELEV	POINT D	IST E	LEV	
	0.00	0.83	5	11.00	0.13		17 0.		
	3.38	0.67	. 6	23.00	0.41				
	3.83	0.67	7	35.00	0.13		00 0.		
	9.00	0.00	8	37.00	000		00 0.		
□ WSEL	DEPTH	FLOW		WETTED	FLOW	TOPWID		ENERGY	
L 110111	INC	AREA	RATE	PER	VEL	1011111	HEAD	HEAD	
(FT)	(FT)	SQ.FT.			(FPS)	(TT)	(FT)	(FT)	and a
0.01	0.01	0.00	0.0		0.44	0.31	0.00	0.01	
0.02	0.02	0.01	0.0	0.66	0.70	0.63	0.01	0.03	
- 0.03	0.03		0.0	0.99	0.92	0.94	0.01	0.04	
0.04	0.04	0.03	0.0	1.32	1.11	1.25	0.02	0.06	
0.05	0.05	0.04	0.1	1.64	1.29	1.56	0.03	0.08	
0.06	0.06	0.06	0.1	1.97	1.46	1.88	0.03	0.09	
0.07	0.07	0.08	0.1	2.30	1.62	2.19	0.04	0.11	
	0.08	0.10	0.2	2.63	1.77	2.50	0.05	0.13	*
0.09	0.09	0.13	0.2	2.96	1.91	2.81	0.06		** *
0.10	0.10	0.16	0.3	3.29	2.05	3.13	0.07	0.17	
0.11	0.11	0.19	0.4	3.62	2.19	3.44	0.07	0.18	
0.12	0.12	0.23	0.5	3.95		3.75	0.08	0.20	
0.13	0.13	0.26	0.6	4.28	2.44	4.07	0.09	0.22	
0.14	0.14	0.31	0.7	5.15	2.40	4.93	0.09	0.23	
0.15	0.15	0.36	n a	6 03	2.40	5.79		0.24	•
0.16	0.16	0.43		6.91	2.44		0.09		
0.17	0.17		1.2	7.79		7.51	0.10	0.27	
0.18		0.58		8.67	2.56	8.38	0.10	0.28	en en gran de la proposición de la compansión de la compa
0.19	0.19		1.8	9.54	2.64	9.24	0 11		
0.20		0.76			2.73		0.12	0.32	
0.21	0.21	0.87	2.4	11.30	2.82	10.96	0.12	0.33	•
0.22	0.22		2.9		2.91	11.83			
0.23	0.23	1.10	3.3	13.06	3.01	12.69		0.37	
0.24	0.24	1.23	3.8	13.93	3.11	13.55	0.15	0.39	
0.25	0.25	1.37	4.4	14.81	3.20	14.41	0.16	0.41	
0.26	0.26	1.52	5.0	15.69	3.30	15.27	0.17	0.43	
0.27	0.27	1.68	5.7	16.57	3.40	16.14	0.18	0.45	
0.28	0.28	1.84	6.4	17.45	3.50	17.00	0.19	0.47	
0.29	0.29	2.02	7.3	18.32	3.59	17.86	0.20	0.49	
0.30	0.30	2.20	8.1	19.20	3.69	18.72	0.21	0.51	
0.31	0.31	2.39	9.1	20.08	3.79	19.59		0.53	
0.32	0.32		10.1		3.88	20.45	0.23	0.55	
0.33	0.33	2.80	11.1	21.84	3.98	21.31	0.25	0.58	
0.34	0.34		12.3	22.71	4.07	22.17	0.26	0.60	
0.35	0.35	3.25	13.5	23.59	4.17	23.03	0.27	0.62	•
0.36	0.36		14.8	24.47		23.90	0.28	0.64	
0.37	0.37		16.2	25.35	4.35	24.76	0.29	0.66	
0.38	0.38		17.7		4.45	25.62	0.31	0.69	
0.39	0.39		19.2	27.10	4.54	26.48	0.32	0.71	
0.40	0.40		20.8	27.98	4.63	27.35	0.33	0.73	
0.41	0.41		22.6	28.86	4.72	28.21	0.35	0.76	
0.42	0.42		24.8	28.88	4.90	28.21	0.37	0.79	
0.43	0.43		27.1		5.08	28.22	0.40	0.83	STREET
☐ WSEL	DEPTH		FLOW	WETTED	FLOW	TOPWID	VEL	ENERGY	STREET CAPACITY
,·	INC	AREA	RATE	PER	VEL	/ \	HEAD	HEAD	CAPACITY
(FT)	(FT)	SQ.FT.		(FT)	(FPS)	(FT)	(FT)	- /	1
0.45	0.45		32.1		5.42	28.23	0.46	0.91	•
0.46	0.46		34.6		5.59	28.23	0.49	0.95	
0.47	0.47		37.3		5.76		0.51	0.98	
0.48	0.48		40.0		5.92		0.54	1.02	
0.49	0.49	7.04	42.8	29.03	6.08	28.25	0.57	1.06	

WALNUT CANTON ROAD

Chapter 22 - Drainage, Flood Control and Erosion Control

GRATING CAPACITIES FOR TYPE 'A' , 'C' and'D'



SLOPE=2.82, D=0.45, Q=7.8 cfs D=0.44, Q=7.6 cfs

PLATE 22.3 D-5

May 2001 SLOPE = 2.62, D= 0.4, Q = 5.8 CM

22-144 8-15

1 alyzer Report

Orainage Structure Analyzer

F pe Hydraulic Analysis

WALNUT CANTON RD.

Onte: Thursday, November 18, 2004 13:57:30

£ ape		Circular
Muterial		RC C76-A
Roughness		0.013000
No thod	The second secon	Manning
I ow Rate		52.5 cfs
Siope	englij i Fil	3.200%
Size $(W \times T)$:	4	30.00×2.7500

(tput Results				
Flow Rate			52.5	cfs
: ope			3.200%	
€ D		· ·	0.63	
Capacity	1,144.		73.4	cfs
Velocity	11 · · · · · · · · · · · · · · · · · ·		16.25	ft/s
] pth		****	1.56	ft
(itical Depth	e e e e e e e e e e e e e e e e e e e	-	2.32	ft
Size (W x T):		30.00 2	c 2.7500	

```
1 alyzer Report
Drainage Structure Analyzer
                                  WALNUT CANYON ROAD.
E se Hydraulic Analysis
Pate: Thursday, November 18, 2004 13:58:57
Input Data
27 2,22222
§ ape
                                 Circular
h terial
                                 RC C76-A
                                 0.013000
Roughness
1 thod
                                  Manning
                                     67.7 cfs
1 ow Rate
S.ope
                                   2.600%
Size (W \times T):
                            30.00 \times 2.7500
tput Results
Flow Rate
                                     67.7 cfs
: ope
                                   2.600%
← D
                                     0.84
                                     66.1 cfs
Capacity
```

15.34 ft/s

2.11 ft

2.43 ft

30.00 x 2.7500

Velocity

itical Depth

Size $(W \times T)$:

l pth

```
1 ilyzer Report
```

Prainage Structure Analyzer

WALNUT CANYON RD.

? pe Hydraulic Analysis

SO TO MESSINA DR.

Date: Tuesday, December 14, 2004 08:04:26

Input Data

: tput Results

_____ 124.0 cfs Flow Rate 2.000% { ope 0.72 c D 142.3 cfs Capacity 16.66 ft/s Velocity 2.53 ft I pth 3.27 ft (itical Depth 42.00 x 3.5000 Size $(W \times T)$:

BUCK ISLAND ROAD

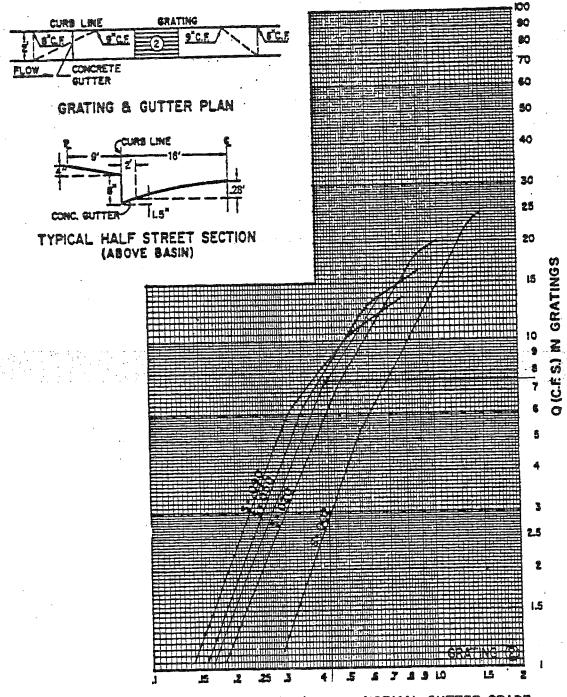
MANNING'S N= .017 SLOPE= .034

POINT	DIST	ELEV	POINT	DIST	ELEV	POINT	DIST I	ELEV	
1	0.00	0.83	5	11.00	0.13			.67	
. 2	8.38		6	23.00	0.41		.63 0		
3	8.83	0.67		35.00	0.13			.83	
4	9.00	0.00	8	37.00	0.00			.00	
□ WSEL	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	VEL	ENERGY	
C MOTE	INC .		RATE	PER	VEL	TOTWID	HEAD	HEAD	
(FT)	(FT)	SQ.FT.	(CFS)	(FT)	(FPS)	(FT)	(FT)	(FT)	
0.01	0.01	0.00	0.0	0.33	0.46	0.31		0.01	
0.02	0.02	0.01	0.0	0.66	0.72	0.63	0.01	0.03	
0.02	0.03	0.01	0.0	0.99	0.95	0.94	0.01	0.03	
0.03	0.04	0.03	0.0	1.32	1.15	1.25		0.04	
0.05	0.05	0.03	0.1	1.64	1.33	1.56	0.03	0.08	
0.06	0.06	0.06	0.1	1.97	1.50	1.88	0.04	0.10	
0.07	0.07	0.08	0.1	2.30	1.67	2.19		0.11	
0.08	0.08	0.10	0.2	2.63	1.82	2.50	0.05	0.13	
0.09	0.09	0.13	0.2	2.96	1.97	2.81	0.06	0.15	
0.10	0.10	0.16	0.3	3.29	2.12	3.13	0.07	0.17	
	0.11	0.19	0.4	3.62	2.25	3.44	0.08	0.19	
0.12	0.12	0.23	0.5	3.95	2.39	3.75	0.09	0.21	
0.13	0.13	0.26	0.7	4.28	2.52	4.07		0.23	
0.14	0.14	0.31	0.8	5.15	2.47	4.93		0.23	
0.15	0.15	0.36	0.9	6.03	2.47	5.79		0.25	
0.16	0.16	0.43		6.91	2.51	6.65		0.26	
0.17	0.17	0.50	1.3	7.79	2.57	7.51		0.27	
0.18	0.18	0.58	1.5	8,67	2.64		0.11	0.29	ورادا عرواه ويعفره والمراوعي والفووجات
	0.19	0.66	1.8	9.54	2.72	9.24	0.12	0.31	
0.20	0.20	0.76	2.1	10.42	2.81	10.10	0.12	0.32	
0.21	0.21	0.87		11.30	2.91	10.96	0.13	0.34	
0.22	0.22	0.98 1.10	2.9	12.18	3.00	11.83		0.36	
0.23	0.23	1.10	3.4	13.06	3.10	12.69	0.15	0.38	
0.24	0.24	1.23		13.93	3.20	13.55		0.40	
0.25	0.25	1.37	4.5	14.81	3.30	14.41		0.42	
0.26	0.26	1.52	5.2	15.69	3.40	15.27		0.44	
0.27	0.27	1.68	5.9	16.57	3.50	16.14		0.46	
0.28	0.28	1.84	6.6	17.45	3.60	17.00		0.48	
0.29	0.29	2.02	7.5	18.32	3.70	17.86		0.50	
0.30	0.30	2.20	8.4	19.20	3.80	18.72		0.52	ROLL CURB LIMIT
0.31		2.39	9.3		3.90	19.59 20.45		0.55	1 1 1 2 1 5
0.32	0.32	2.59 2.80	10.4 11.5		4.00 4.10	20.45		0.57	LIMIT
0.33 0.34			12.7		4.20			0.55	
0.35					4.30	23.03		0.64	
0.35			15.3		4.39			0.66	
0.37			16.7		4.49			0.68	
0.38			18.2		4.58			0.71	
0.39			19.8		4.68				
0.40			21.5		4.77				
0.41			23.3		4.86				
0.42			25.6		5.05			0.82	
0.43			28.0		5.23				200000000000000000000000000000000000000
☐ WSEL	DEPTH			WETTED	FLOW	TOPWID	VEL	ENERGY	-STREET CAPACITY
	INC	AREA	RATE	PER	VEL		HEAD	HEAD	j
(FT)	(FT)	SQ.FT.	(CFS)	(FT)	(FPS)	(FT)	(FT)	(FT)	
0.45			33.0						
0.46			35.7		5.76				
0.47			38.4		5.93	28.24			
0.48	0.48	6.76	41.2		6.10	28.24	0.58	1.06	
0.49	0.49	7.04	44.1	29.03	6.27	28.25	0.61	1.10	

Buck Island Road

Chapter 22 - Drainage, Flood Control and Erosion Control

GRATING CAPACITIES FOR TYPE 'A' , 'C' and'D'



D-DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

Slope = 3.42

$$D = 0.43, 7.5 \text{ cfs}$$

 $D = 0.42, 7.4 \text{ cfs}$

PLATE 22.3 D-5

Drainage Structure Analyzer

? >e Hydraulic Analysis

Buck Island Road

Onte: Friday, November 12, 2004 11:05:43

Input Data

•		
S ape	Circular	
M :erial	RC C76-A	
Roughness	0.013000	
M thod	Manning	
F ow Rate	15.0 c	fs
S_ope	3.400%	
Size (W x T):	18.00×2.0000	

C tput Results

_					

Flow	Rate			15.0	cfs
eqc 3	<u> </u>			3.400%	
ć D			 	0.66	
Capac	city			19.4	cfs
Veloc	city		 	12.11	ft/s
I pth	n _			0.99	ft
C it:	ical Depth			1.40	ft
Size	$(T \times W)$:		18.00	x 2.0000	

PIPESTONE ROAD

MANNING S N= .UI/ SLOPE=	MANNING'S N=	.017	SLOPE=	.0447
--------------------------	--------------	------	--------	-------

				_ ,					
POINT	DIST	ELEV	POINT	DIST	ELEV	POINT	DIST	ELEV	
1	0.00	0.83	5	11.00	0.13			0.67	
2	8.38	0.67	6	23.00			7.63		
3	8.83	0.67		35.00	0.13			0.83	
4	9.00		8	37.00	0.00			0.00	÷ .
□ WSEL	DEPTH	FLOW		WETTED	FLOW	TOPWID	VEL		
	INC	AREA	RATE	PER	VEL	1011111	HEAD	HEAD	
(FT)	(FT)	SQ.FT.		(FT)	(FPS)	(FT)	(FT)		
0.01	0.01	õ.00	0.0	0.33	0.52	0.31			
0.02	0.02	0.01	0.0	0.66	0.83	0.63			
0.03	0.03	0.01	0.0	0.99	1.09				
0.04	0.04	0.03	0.0	1.32	1.32	1.25			
0.05	0.05	0.04	0.1	1.64	1.53	1.56			
0.06	0.06	0.06	0.1	1.97	1.73	1.88			
0.07	0.07	0.08	0.1	2.30	1.91	2.19			
0.08	0.08	0.10	0.2	2.63	2.09	2.50			
0.09	0.09	0.13	0.3	2.96	2.26	2.81			• •
0.10	0.10	0.16	0.4	3.29	2.43	3.13			
0.11	0.11	0.19	0.5	3.62	2.58				
0.12	0.12	0.23	0.6	3.95	2.74	3.75			
0.13	0.13	0.26	0.8	4.28	2.89	4.07			
0.14	0.14	0.31	0.9	5.15	2.83	4.93	0.12		
0.15	0.15	0.36	1.0	6.03	2.84	5.79	0.12	0.27	
0.16	0.16	0.43	1.2	6.91	2.88	6.65	0.13	0.29	
0.17	0.17	0.50	1.5	7.79	2.95	7.51	0.13	0.30	
	0.18	0.58	1.7	8.67		8.38		0.32	a kangan iya iya iya iya i
	0.19	0.66	2.1	9.54	3.12	9.24	0.15	0.34	
0.20	0.20	0.76	2.5			10.10	0.16	0.36	
0.21	0.21	0.87	2.9	11.30	3.33	10.96	0.17	0.38	
0.22	0.22	0.98	3.4	12.18	3.44	11.83			
0.23	0.23	1.10	3.9	13.06		12.69			
0.24	0.24	1.23	4.5	13.93		13.55			·
0.25	0.25		5.2	14.81		14.41			
0.26	0.26	1.52	5.9	15.69	3.90	15.27			
0.27	0.27		6.7	16.57		16.14			
0.28	0.28	1.84	7.6	17.45	4.13	17.00			
0.29	0.29		8.6	18.32	4.25	17.86			
0.30	0.30		9.6	19.20	4.36	18.72			
0.31	0.31		10.7	20.08		19.59			
0.32	0.32		11.9	20.96		20.45			
0.33	0.33		13.2	21.84	4.70	21.3			
0.34	0.34	3.02	14.5	22.71	4.81	22.17			
0.35			16.0			23.03			
0.36			17.5			23.90			
0.37			19.2	25.35		24.76			
0.38	0.38		20.9	26.23		25.62			
0.39			22.7	27.10		26.48			
0.40			24.6	27.98	5.47	27.3			-STREET CAPACITY
0.41			26.7	28.86		28.2			CA 0001111
0.42			29.3	28.88		28.23			CAPACITY
0.43			32.1	28.90		28.22			
☐ WSEL	DEPTH				FLOW	TOPWID	VEL	ENERGY	
/ Torn \	INC	AREA	RATE	PER	VEL	,·	HEAD		
(FT)	(FT)			(FT)	(FPS)	(FT)		(FT)	
0.45			37.9	28.94					
0.46			40.9	28.96					
0.47			44.1						
0.48			47.3	29.01					
0.49	0.49	7.04	50.6	29.03	7.19	28.2	5 0.8	0 1.29	

PIPESTONE ROAD

MANNING'S N= .017 SLOPE= .0255

POINT	DIST			DIST	ELEV	POINT I		ELEV		
1		0.83	5	11.00		9 37.	.17 0	.67		
	8.38	0.67	6	23.00	0.41	10 37.	.63 0	.67		
3 .		0.67 0.00	7	35.00	0.13	11 46 12 0	.00 0	.83		
4		0.00	8	37.00	0.00	12 0	.00 0			
□ WSEI						TOPWID				
·	INC	AREA	RATE	PER	VEL	.	HEAD			
(FT)		SQ.FT.		(FT)	(FPS)	(FT)	(FT)			
0.0			0.0	0.33	0.39	0.31	0.00	0.01		
0.0				0.66	0.63	0.63		0.03		
0.0				0.99	0.82	0.94		0.04		
0.0		0.03	0.0	1.32	0.99	1.25	0.02	0.06		
0.0		0.04 0.06	0.0	1.64 1.97	1.15 1.30	1.56 1.88	0.02 0.03	0.07		
0.0				2.30		2.19		0.09 0.10		
0.0		0.10	0.2	2.63						
0.0		0.13	0.2	2.96		2.50 2.81	0.04 0.05	0.12		
0.1		0.16		3.29	1.83	3.13	0.05	0.15		
0.1				3.62		3.44	0.05	0.13		
0.3			0.5	3.95	2.07	3.75	0.07	0.19		
0.3		0.26	0.6	4.28	2.18	4.07	0.07			
0.3		0.31	0.7	5.15	2.14	4.07 4.93	0.07	0.21		
0.3			0.8	6.03	2.14	5.79	0.07			
0.1				6.91		6.65		0.23		
0.	17 0.17	0.50	1.1	7.79	2.23	7.51	0.08	0.25		
	18 0.18	0.58	1.3	8.67	2.29	8.38	0.08	0.26	en waren in Egiptica	. e.,
0.	19 0.19	0.66	1.6	9.54	2.36	9.24	0.09	0.28		
0.	20 0.20	0.76	1.9	10.42	2.44	10.10	0.09	0.29		
0.	21 0.21	0.87 0.98	2.2	11.30	2.52	10.96	0.10	0.31		
0.		0.98	2.5	12.18	2.60	11.83	0.11	0.33	•	
0.			3.0	13.06		12.69	0.11	0.34		
Ο.		1.23	3.4	13.93	2.77	13.55	0.12			
0.		1.37	3.9 4.5	14.81 15.69	2.86	14.41 15.27	0.13			
0.		1.52	4.5	15.69	2.95	15.27	0.13			
0.			5.1	16.57	3.03	16.14				
0.		1.84	5.8	17.45	3.12	17.00				
	29 0.29	2.02	6.5 7.3	18.32 19.20	3.21	17.86 18.72	0.16			
	30 0.30	2.20	7.3	19.20	3.29	18.72	0.17			
	31 0.31		8.1		3.38	19.59				
	32 0.32		9.0	20.96		20.45			_	•
	33 0.33 34 0.34		9.9 11.0	21.84 22.71	3.55 3.64	21.31		0.53 0.55	-Roll a	1RB
	35 0.35			23.59						
	36 0.36		13.2	24.47		23.03 23.90	0.21 0.22		LIV	117
	37 0.37		14.5	25.35	3.89		0.22			
	38 0.38		15.8	26.23	3.97	25.62	0.23			
	39 0.39		17.2	27.10	4.05	26.48	0.25			
	40 0.40		18.6		4.13	27.35	0.26			
	41 0.41		20.1	28.86	4.21	28.21	0.28			
	42 0.42		22.1	28.88	4.37	28.21	0.30			
	43 0.43		24.2		4.53	28.22	0.32			
☐ WSE				WETTED	FLOW	TOPWID	VEL	ENERGY		
	INC	AREA	RATE	PER	VEL		HEAD	HEAD		
(FT				(FT)	(FPS)	(FT)	(FT)	(FT)		
	45 0.45		28.6	28.94						
	46 0.46		30.9	28.96	4.99		0.39			
	47 0.47		33.3	28.98	5.14		0.41			
	48 0.48		35.7	29.01	5.29		0.43			
0.	49 0.49	7.04	38.2	29.03	5.43	28.25	0.46	0.95		

PIPESTONE ROAD

Chapter 22 - Drainage, Flood Control and Erosion Control

GRATING CAPACITIES FOR TYPE 'A' . "C" and D"

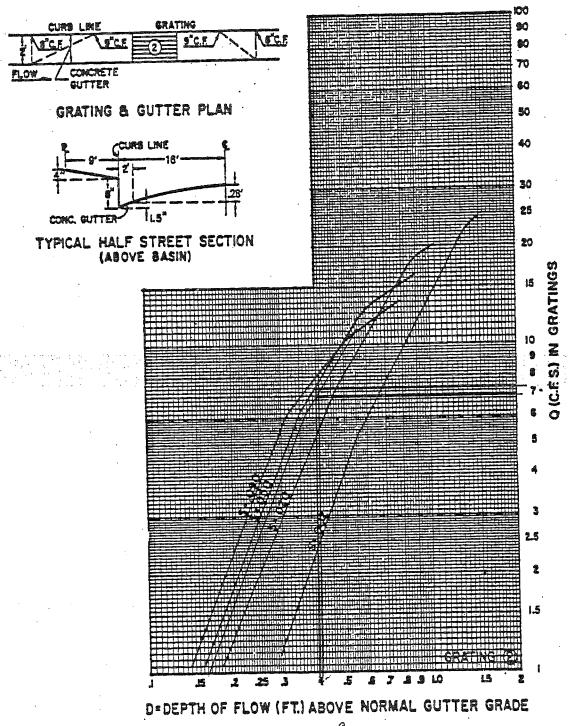


PLATE 22.3 D-5

Slope = 42, D=0.41, Q=7 cfs

```
lyzer Report
```

Drainage Structure Analyzer

e Hydraulic Analysis

Pipe Stone Road

Date: Friday, November 12, 2004 11:07:02

Input Data

 Sipe
 Circular

 Micrial
 RC C76-A

 Roughness
 0.013000

 Michod
 Manning

 Fow Rate
 28.4 cfs

 Sipe
 4.000%

 Size (W x T):
 24.00 x 2.5000

C :put Results

Flow Rate

5 ope
c 0
Capacity
Velocity
I oth
C itical Depth
Size (W x T):

28.4 cfs 4.000% 0.57 45.2 cfs 15.22 ft/s 1.15 ft 1.83 ft 24.00 x 2.5000 Big Springs Road

(FT) (FT) (S) (FT) (FT) (FT) (FT) (FT) (FT) (FT) (FT		MANNING	S N= .	017 SLOP	E= .006	5				
3		POINT	DIST	ELEV	POINT	DIST	ELEV	POINT I	DIST B	LEV
3		1	0.00	0.83	5	11.00	0.13	9 45.	.17 0.	67
A		2	8.38	0.67	6	27.00	0.45	10 45.	.63 0.	67
A		3	8.83	0.67	7	43.00	0.13	11 54.	.00 0.	83
		4	9.00	0.00	8	45.00	0.00	12 0.	.00 0.	.00
(FT) (FT) SQ.FT. (CFS) (FT) (FPS) (FT) (FT) (FT) (FT) (O.01 0.01 0.00 0.00 0.33 0.19 0.31 0.00 0.01 0.00 0.02 0.02 0.02 0.01 0.0 0.66 0.30 0.63 0.00 0.00 0.03 0.03		☐ WSEL	DEPTH	FLTOM	FLOW V		FLOW	TOPWID		ENERGY
0.01 0.01 0.00 0.00 0.03 0.19 0.31 0.00 0.01 0.02 0.03 0.03 0.03 0.01 0.00 0.09 0.40 0.94 0.00 0.03 0.04 0.04 0.04 0.03 0.0 1.32 0.48 1.25 0.00 0.05 0.05 0.05 0.06 0.06 0.0 1.97 0.63 1.88 0.01 0.01 0.07 0.07 0.07 0.08 0.1 2.30 0.70 2.19 0.01 0.08 0.09 0.09 0.09 0.09 0.09 0.09 0.09	•		INC	AREA	RATE	PER	VEL		HEAD	HEAD
0.03			(FT)	SQ.FT.	(CFS)	(FT)	(FPS)	(FT)	(FT)	(FT)
0.03			0.01	0.00	0.0	0.33	0.19	0.31	0.00	0.01
0.06			0.02	0.01	0.0	0.66	0.30	0.63	0.00	0.02
0.06		0.03	0.03	0.01	0.0	0.99	0.40	0.94	0.00	
0.06			0.04	0.03	0.0	1.32	0.48	1.25	0.00	0.04
0.05			0.05	0.04	0.0	1.64	0.56	1.56	0.00	0.05
0.08			0.06	0.06	0.0	1.97	0.63	1.88		
0.12 0.13 0.13 0.26 0.3 4.28 1.06 4.07 0.02 0.15 0.14 0.14 0.31 0.3 5.30 1.02 5.07 0.02 0.15 0.15 0.15 0.15 0.37 0.4 6.32 1.01 6.08 0.02 0.17 0.16 0.16 0.16 0.43 0.4 7.34 1.02 7.08 0.02 0.19 0.19 0.19 0.19 0.69 0.6 9.38 1.07 9.09 0.02 0.20 0.19 0.18 0.18 0.59 0.6 9.38 1.07 9.09 0.02 0.20 0.19 0.19 0.19 0.69 0.6 9.38 1.07 9.09 0.02 0.20 0.20 0.20 0.20 0.80 0.9 11.42 1.15 11.10 0.02 0.22 0.21 0.21 0.91 1.1 12.44 1.19 12.11 0.02 0.23 0.23 0.23 0.23 1.17 1.5 14.49 1.27 14.12 0.02 0.23 0.23 0.23 1.17 1.5 14.49 1.27 14.12 0.02 0.25 0.25 0.26 1.64 2.3 17.55 1.31 15.12 0.03 0.27 0.25 0.25 1.48 2.0 16.53 1.35 16.13 0.03 0.28 0.26 0.26 0.26 1.64 2.3 17.55 1.40 17.13 0.03 0.29 0.27 0.27 1.82 2.6 18.57 1.44 18.14 0.03 0.29 0.29 0.29 0.20 0.30 0.30 19.59 1.48 19.14 0.03 0.30 0.30 0.28 0.29 0.29 0.20 0.30 0.30 19.59 1.48 19.14 0.03 0.31 0.28 0.28 0.28 0.28 1.03 1.35 1.40 17.13 0.03 0.30 0.28 0.29 0.29 0.20 0.30 0.30 19.59 1.48 19.14 0.03 0.31 0.30 0.30 0.30 0.30 0.30 0.30				0.08	0.1	2.30	0.70	2.19	0.01	0.08
0.12 0.13 0.13 0.26 0.3 4.28 1.06 4.07 0.02 0.15 0.14 0.14 0.31 0.3 5.30 1.02 5.07 0.02 0.15 0.15 0.15 0.15 0.37 0.4 6.32 1.01 6.08 0.02 0.17 0.16 0.16 0.16 0.43 0.4 7.34 1.02 7.08 0.02 0.19 0.19 0.19 0.19 0.69 0.6 9.38 1.07 9.09 0.02 0.20 0.19 0.18 0.18 0.59 0.6 9.38 1.07 9.09 0.02 0.20 0.19 0.19 0.19 0.69 0.6 9.38 1.07 9.09 0.02 0.20 0.20 0.20 0.20 0.80 0.9 11.42 1.15 11.10 0.02 0.22 0.21 0.21 0.91 1.1 12.44 1.19 12.11 0.02 0.23 0.23 0.23 0.23 1.17 1.5 14.49 1.27 14.12 0.02 0.23 0.23 0.23 1.17 1.5 14.49 1.27 14.12 0.02 0.25 0.25 0.26 1.64 2.3 17.55 1.31 15.12 0.03 0.27 0.25 0.25 1.48 2.0 16.53 1.35 16.13 0.03 0.28 0.26 0.26 0.26 1.64 2.3 17.55 1.40 17.13 0.03 0.29 0.27 0.27 1.82 2.6 18.57 1.44 18.14 0.03 0.29 0.29 0.29 0.20 0.30 0.30 19.59 1.48 19.14 0.03 0.30 0.30 0.28 0.29 0.29 0.20 0.30 0.30 19.59 1.48 19.14 0.03 0.31 0.28 0.28 0.28 0.28 1.03 1.35 1.40 17.13 0.03 0.30 0.28 0.29 0.29 0.20 0.30 0.30 19.59 1.48 19.14 0.03 0.31 0.30 0.30 0.30 0.30 0.30 0.30					0.1	2.03	0.//	2.50	0.01	0.09
0.12 0.13 0.13 0.26 0.3 4.28 1.06 4.07 0.02 0.15 0.14 0.14 0.31 0.3 5.30 1.02 5.07 0.02 0.15 0.15 0.15 0.15 0.37 0.4 6.32 1.01 6.08 0.02 0.17 0.16 0.16 0.16 0.43 0.4 7.34 1.02 7.08 0.02 0.19 0.19 0.19 0.19 0.69 0.6 9.38 1.07 9.09 0.02 0.20 0.19 0.18 0.18 0.59 0.6 9.38 1.07 9.09 0.02 0.20 0.19 0.19 0.19 0.69 0.6 9.38 1.07 9.09 0.02 0.20 0.20 0.20 0.20 0.80 0.9 11.42 1.15 11.10 0.02 0.22 0.21 0.21 0.91 1.1 12.44 1.19 12.11 0.02 0.23 0.23 0.23 0.23 1.17 1.5 14.49 1.27 14.12 0.02 0.23 0.23 0.23 1.17 1.5 14.49 1.27 14.12 0.02 0.25 0.25 0.26 1.64 2.3 17.55 1.31 15.12 0.03 0.27 0.25 0.25 1.48 2.0 16.53 1.35 16.13 0.03 0.28 0.26 0.26 0.26 1.64 2.3 17.55 1.40 17.13 0.03 0.29 0.27 0.27 1.82 2.6 18.57 1.44 18.14 0.03 0.29 0.29 0.29 0.20 0.30 0.30 19.59 1.48 19.14 0.03 0.30 0.30 0.28 0.29 0.29 0.20 0.30 0.30 19.59 1.48 19.14 0.03 0.31 0.28 0.28 0.28 0.28 1.03 1.35 1.40 17.13 0.03 0.30 0.28 0.29 0.29 0.20 0.30 0.30 19.59 1.48 19.14 0.03 0.31 0.30 0.30 0.30 0.30 0.30 0.30								2.01	0.01	0.10
0.12 0.13 0.13 0.26 0.3 4.28 1.06 4.07 0.02 0.15 0.14 0.14 0.31 0.3 5.30 1.02 5.07 0.02 0.15 0.15 0.15 0.15 0.37 0.4 6.32 1.01 6.08 0.02 0.17 0.16 0.16 0.16 0.43 0.4 7.34 1.02 7.08 0.02 0.19 0.19 0.19 0.19 0.69 0.6 9.38 1.07 9.09 0.02 0.20 0.19 0.18 0.18 0.59 0.6 9.38 1.07 9.09 0.02 0.20 0.19 0.19 0.19 0.69 0.6 9.38 1.07 9.09 0.02 0.20 0.20 0.20 0.20 0.80 0.9 11.42 1.15 11.10 0.02 0.22 0.21 0.21 0.91 1.1 12.44 1.19 12.11 0.02 0.23 0.23 0.23 0.23 1.17 1.5 14.49 1.27 14.12 0.02 0.23 0.23 0.23 1.17 1.5 14.49 1.27 14.12 0.02 0.25 0.25 0.26 1.64 2.3 17.55 1.31 15.12 0.03 0.27 0.25 0.25 1.48 2.0 16.53 1.35 16.13 0.03 0.28 0.26 0.26 0.26 1.64 2.3 17.55 1.40 17.13 0.03 0.29 0.27 0.27 1.82 2.6 18.57 1.44 18.14 0.03 0.29 0.29 0.29 0.20 0.30 0.30 19.59 1.48 19.14 0.03 0.30 0.30 0.28 0.29 0.29 0.20 0.30 0.30 19.59 1.48 19.14 0.03 0.31 0.28 0.28 0.28 0.28 1.03 1.35 1.40 17.13 0.03 0.30 0.28 0.29 0.29 0.20 0.30 0.30 19.59 1.48 19.14 0.03 0.31 0.30 0.30 0.30 0.30 0.30 0.30			0.10		0.1	3.62		3.13	0.01	0.11
0.13					0.2	3 95	1 00		0.01	0.12
0.15					0.3	4.28	1.06	4.07	0.02	0.15
0.15				0.31	0.3	5.30	1.02	5.07	0.02	0.16
0.18				0.37	0.4	6.32	1.01	6.08	0.02	0.17
0.18		0.16	0.16	0.43	0.4	7.34	1.02	7.08	0.02	0.18
0.22 0.22 1.04 1.3 13.46 1.23 13.11 0.02 0.24 0.23 0.23 0.23 1.17 1.5 14.49 1.27 14.12 0.02 0.25 0.24 0.24 1.32 1.7 1.5 11.31 15.12 0.03 0.27 0.25 0.25 0.26 1.68 2.0 16.53 1.35 16.13 0.03 0.28 0.26 0.26 1.64 2.3 17.55 1.40 17.13 0.03 0.28 0.26 0.26 1.64 2.3 17.55 1.40 17.13 0.03 0.28 0.28 0.28 2.00 3.0 19.59 1.48 19.14 0.03 0.31 0.29 0.29 2.20 3.4 20.61 1.52 20.15 0.04 0.33 0.31 0.29 0.29 2.20 3.4 20.61 1.52 20.15 0.04 0.33 0.31 0.30 0.30 2.41 3.8 21.63 1.57 21.15 0.04 0.34 0.31 0.31 0.31 2.62 4.2 22.65 1.61 22.16 0.04 0.35 0.32 0.32 0.32 2.85 4.7 23.67 1.65 23.16 0.04 0.36 0.33 0.33 0.33 3.09 5.2 24.69 1.69 24.17 0.04 0.37 0.33 0.33 0.35 5.8 25.71 1.73 25.17 0.05 0.39 0.35 0.35 3.59 6.4 26.74 1.78 26.18 0.05 0.40 0.36 0.36 0.36 3.86 7.0 27.76 1.82 27.18 0.05 0.41 0.37 0.37 0.37 4.13 7.7 28.78 1.86 28.19 0.05 0.41 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.44 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.44 0.40 0.40 5.03 9.9 31.84 1.98 31.20 0.06 0.44 0.41 0.41 5.34 10.8 32.86 2.02 32.21 0.06 0.44 0.42 0.42 5.67 11.7 3.88 2.06 33.21 0.06 0.45 0.43 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.40 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.40 0.44 0.45 5.67 11.7 3.88 2.06 33.21 0.06 0.45 0.44 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.44 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.49 0.43 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.49 0.49 0.49 8.16 20.2 37.03 2.47 36.23 0.08 0.5 0.5 0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.5 0.5 0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5				0.51	0.5	8.36	1.05	8.09	0.02	0.19
0.22 0.22 1.04 1.3 13.46 1.23 13.11 0.02 0.24 0.23 0.23 0.23 1.17 1.5 14.49 1.27 14.12 0.02 0.25 0.24 0.24 1.32 1.7 1.5 11.31 15.12 0.03 0.27 0.25 0.25 0.26 1.68 2.0 16.53 1.35 16.13 0.03 0.28 0.26 0.26 1.64 2.3 17.55 1.40 17.13 0.03 0.28 0.26 0.26 1.64 2.3 17.55 1.40 17.13 0.03 0.28 0.28 0.28 2.00 3.0 19.59 1.48 19.14 0.03 0.31 0.29 0.29 2.20 3.4 20.61 1.52 20.15 0.04 0.33 0.31 0.29 0.29 2.20 3.4 20.61 1.52 20.15 0.04 0.33 0.31 0.30 0.30 2.41 3.8 21.63 1.57 21.15 0.04 0.34 0.31 0.31 0.31 2.62 4.2 22.65 1.61 22.16 0.04 0.35 0.32 0.32 0.32 2.85 4.7 23.67 1.65 23.16 0.04 0.36 0.33 0.33 0.33 3.09 5.2 24.69 1.69 24.17 0.04 0.37 0.33 0.33 0.35 5.8 25.71 1.73 25.17 0.05 0.39 0.35 0.35 3.59 6.4 26.74 1.78 26.18 0.05 0.40 0.36 0.36 0.36 3.86 7.0 27.76 1.82 27.18 0.05 0.41 0.37 0.37 0.37 4.13 7.7 28.78 1.86 28.19 0.05 0.41 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.44 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.44 0.40 0.40 5.03 9.9 31.84 1.98 31.20 0.06 0.44 0.41 0.41 5.34 10.8 32.86 2.02 32.21 0.06 0.44 0.42 0.42 5.67 11.7 3.88 2.06 33.21 0.06 0.45 0.43 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.40 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.40 0.44 0.45 5.67 11.7 3.88 2.06 33.21 0.06 0.45 0.44 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.44 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.49 0.43 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.49 0.49 0.49 8.16 20.2 37.03 2.47 36.23 0.08 0.5 0.5 0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.5 0.5 0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5			0.18	0.59	0.6	9.38	1.07	9.09	0.02	0.20
0.22 0.22 1.04 1.3 13.46 1.23 13.11 0.02 0.24 0.23 0.23 0.23 1.17 1.5 14.49 1.27 14.12 0.02 0.25 0.24 0.24 1.32 1.7 1.5 11.31 15.12 0.03 0.27 0.25 0.25 0.26 1.68 2.0 16.53 1.35 16.13 0.03 0.28 0.26 0.26 1.64 2.3 17.55 1.40 17.13 0.03 0.28 0.26 0.26 1.64 2.3 17.55 1.40 17.13 0.03 0.28 0.28 0.28 2.00 3.0 19.59 1.48 19.14 0.03 0.31 0.29 0.29 2.20 3.4 20.61 1.52 20.15 0.04 0.33 0.31 0.29 0.29 2.20 3.4 20.61 1.52 20.15 0.04 0.33 0.31 0.30 0.30 2.41 3.8 21.63 1.57 21.15 0.04 0.34 0.31 0.31 0.31 2.62 4.2 22.65 1.61 22.16 0.04 0.35 0.32 0.32 0.32 2.85 4.7 23.67 1.65 23.16 0.04 0.36 0.33 0.33 0.33 3.09 5.2 24.69 1.69 24.17 0.04 0.37 0.33 0.33 0.35 5.8 25.71 1.73 25.17 0.05 0.39 0.35 0.35 3.59 6.4 26.74 1.78 26.18 0.05 0.40 0.36 0.36 0.36 3.86 7.0 27.76 1.82 27.18 0.05 0.41 0.37 0.37 0.37 4.13 7.7 28.78 1.86 28.19 0.05 0.41 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.44 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.44 0.40 0.40 5.03 9.9 31.84 1.98 31.20 0.06 0.44 0.41 0.41 5.34 10.8 32.86 2.02 32.21 0.06 0.44 0.42 0.42 5.67 11.7 3.88 2.06 33.21 0.06 0.45 0.43 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.40 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.40 0.44 0.45 5.67 11.7 3.88 2.06 33.21 0.06 0.45 0.44 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.44 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.49 0.43 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.49 0.49 0.49 8.16 20.2 37.03 2.47 36.23 0.08 0.5 0.5 0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.5 0.5 0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5				0.69	0.8	10.40	1.11	10.10	0.02	0.21
0.22 0.22 1.04 1.3 13.46 1.23 13.11 0.02 0.24 0.23 0.23 0.23 1.17 1.5 14.49 1.27 14.12 0.02 0.25 0.24 0.24 1.32 1.7 1.5 11.31 15.12 0.03 0.27 0.25 0.25 0.26 1.68 2.0 16.53 1.35 16.13 0.03 0.28 0.26 0.26 1.64 2.3 17.55 1.40 17.13 0.03 0.28 0.26 0.26 1.64 2.3 17.55 1.40 17.13 0.03 0.28 0.28 0.28 2.00 3.0 19.59 1.48 19.14 0.03 0.31 0.29 0.29 2.20 3.4 20.61 1.52 20.15 0.04 0.33 0.31 0.29 0.29 2.20 3.4 20.61 1.52 20.15 0.04 0.33 0.31 0.30 0.30 2.41 3.8 21.63 1.57 21.15 0.04 0.34 0.31 0.31 0.31 2.62 4.2 22.65 1.61 22.16 0.04 0.35 0.32 0.32 0.32 2.85 4.7 23.67 1.65 23.16 0.04 0.36 0.33 0.33 0.33 3.09 5.2 24.69 1.69 24.17 0.04 0.37 0.33 0.33 0.35 5.8 25.71 1.73 25.17 0.05 0.39 0.35 0.35 3.59 6.4 26.74 1.78 26.18 0.05 0.40 0.36 0.36 0.36 3.86 7.0 27.76 1.82 27.18 0.05 0.41 0.37 0.37 0.37 4.13 7.7 28.78 1.86 28.19 0.05 0.41 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.44 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.44 0.40 0.40 5.03 9.9 31.84 1.98 31.20 0.06 0.44 0.41 0.41 5.34 10.8 32.86 2.02 32.21 0.06 0.44 0.42 0.42 5.67 11.7 3.88 2.06 33.21 0.06 0.45 0.43 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.40 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.40 0.44 0.45 5.67 11.7 3.88 2.06 33.21 0.06 0.45 0.44 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.44 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.49 0.43 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.49 0.49 0.49 8.16 20.2 37.03 2.47 36.23 0.08 0.5 0.5 0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.5 0.5 0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5		0.20	0.20	0.80	0.9	11.42	1.15	11.10	0.02	0.22
0.22 0.22 1.04 1.3 13.46 1.23 13.11 0.02 0.24 0.23 0.23 0.23 1.17 1.5 14.49 1.27 14.12 0.02 0.25 0.24 0.24 1.32 1.7 1.5 11.31 15.12 0.03 0.27 0.25 0.25 0.26 1.68 2.0 16.53 1.35 16.13 0.03 0.28 0.26 0.26 1.64 2.3 17.55 1.40 17.13 0.03 0.28 0.26 0.26 1.64 2.3 17.55 1.40 17.13 0.03 0.28 0.28 0.28 2.00 3.0 19.59 1.48 19.14 0.03 0.31 0.29 0.29 2.20 3.4 20.61 1.52 20.15 0.04 0.33 0.31 0.29 0.29 2.20 3.4 20.61 1.52 20.15 0.04 0.33 0.31 0.30 0.30 2.41 3.8 21.63 1.57 21.15 0.04 0.34 0.31 0.31 0.31 2.62 4.2 22.65 1.61 22.16 0.04 0.35 0.32 0.32 0.32 2.85 4.7 23.67 1.65 23.16 0.04 0.36 0.33 0.33 0.33 3.09 5.2 24.69 1.69 24.17 0.04 0.37 0.33 0.33 0.35 5.8 25.71 1.73 25.17 0.05 0.39 0.35 0.35 3.59 6.4 26.74 1.78 26.18 0.05 0.40 0.36 0.36 0.36 3.86 7.0 27.76 1.82 27.18 0.05 0.41 0.37 0.37 0.37 4.13 7.7 28.78 1.86 28.19 0.05 0.41 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.44 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.44 0.40 0.40 5.03 9.9 31.84 1.98 31.20 0.06 0.44 0.41 0.41 5.34 10.8 32.86 2.02 32.21 0.06 0.44 0.42 0.42 5.67 11.7 3.88 2.06 33.21 0.06 0.45 0.43 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.40 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.40 0.44 0.45 5.67 11.7 3.88 2.06 33.21 0.06 0.45 0.44 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.44 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.49 0.43 0.43 0.43 6.01 1.26 34.90 2.09 34.22 0.07 0.5 0.5 0.49 0.49 0.49 8.16 20.2 37.03 2.47 36.23 0.08 0.5 0.5 0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.5 0.5 0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5		0.21	0.21	0.91	1.1	12.44	1.19	12.11	0.02	0.23
0.30 0.30 2.41 3.8 21.63 1.57 21.15 0.04 0.34 0.31 0.31 0.31 2.62 4.2 22.65 1.61 22.16 0.04 0.35 0.32 0.32 0.32 2.85 4.7 23.67 1.65 23.16 0.04 0.35 0.33 0.33 3.09 5.2 24.69 1.69 24.17 0.04 0.35 0.34 0.34 3.33 5.8 25.71 1.73 25.17 0.05 0.39 0.35 0.35 3.59 6.4 26.74 1.78 26.18 0.05 0.40 0.36 0.36 0.36 3.86 7.0 27.76 1.82 27.18 0.05 0.40 0.36 0.37 0.37 4.13 7.7 28.78 1.86 28.19 0.05 0.42 0.38 0.38 4.42 8.4 29.80 1.90 29.19 0.06 0.44 0.39 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.46 0.41 0.41 5.34 10.8 32.86 2.02 32.21 0.06 0.46 0.42 0.42 0.42 5.67 11.7 33.88 2.06 33.21 0.07 0.45 0.42 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.55 0.50 0.42 0.43 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.55 0.45 0.46 0.46 0.46 7.07 11.7 33.88 2.06 33.21 0.07 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45		0.22	0.22	1.04	1.3	13.46	1.23	13.11	0.02	0.24
0.30 0.30 2.41 3.8 21.63 1.57 21.15 0.04 0.34 0.31 0.31 0.31 2.62 4.2 22.65 1.61 22.16 0.04 0.35 0.32 0.32 0.32 2.85 4.7 23.67 1.65 23.16 0.04 0.35 0.33 0.33 3.09 5.2 24.69 1.69 24.17 0.04 0.35 0.34 0.34 3.33 5.8 25.71 1.73 25.17 0.05 0.39 0.35 0.35 3.59 6.4 26.74 1.78 26.18 0.05 0.40 0.36 0.36 0.36 3.86 7.0 27.76 1.82 27.18 0.05 0.40 0.36 0.37 0.37 4.13 7.7 28.78 1.86 28.19 0.05 0.42 0.38 0.38 4.42 8.4 29.80 1.90 29.19 0.06 0.44 0.39 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.46 0.41 0.41 5.34 10.8 32.86 2.02 32.21 0.06 0.46 0.42 0.42 0.42 5.67 11.7 33.88 2.06 33.21 0.07 0.45 0.42 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.55 0.50 0.42 0.43 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.55 0.45 0.46 0.46 0.46 7.07 11.7 33.88 2.06 33.21 0.07 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45		0.23	0.23	1.17	1.5	14.49	1.27	14.12	0.02	0.25
0.30 0.30 2.41 3.8 21.63 1.57 21.15 0.04 0.34 0.31 0.31 0.31 2.62 4.2 22.65 1.61 22.16 0.04 0.35 0.32 0.32 0.32 2.85 4.7 23.67 1.65 23.16 0.04 0.35 0.33 0.33 3.09 5.2 24.69 1.69 24.17 0.04 0.35 0.34 0.34 3.33 5.8 25.71 1.73 25.17 0.05 0.39 0.35 0.35 3.59 6.4 26.74 1.78 26.18 0.05 0.40 0.36 0.36 0.36 3.86 7.0 27.76 1.82 27.18 0.05 0.40 0.36 0.37 0.37 4.13 7.7 28.78 1.86 28.19 0.05 0.42 0.38 0.38 4.42 8.4 29.80 1.90 29.19 0.06 0.44 0.39 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.46 0.41 0.41 5.34 10.8 32.86 2.02 32.21 0.06 0.46 0.42 0.42 0.42 5.67 11.7 33.88 2.06 33.21 0.07 0.45 0.42 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.55 0.50 0.42 0.43 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.55 0.45 0.46 0.46 0.46 7.07 11.7 33.88 2.06 33.21 0.07 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45		0.24	0.24	1.32	1.7	15.51	1.31	15.12	0.03	0.27
0.30 0.30 2.41 3.8 21.63 1.57 21.15 0.04 0.34 0.31 0.31 0.31 2.62 4.2 22.65 1.61 22.16 0.04 0.35 0.32 0.32 0.32 2.85 4.7 23.67 1.65 23.16 0.04 0.35 0.33 0.33 3.09 5.2 24.69 1.69 24.17 0.04 0.35 0.34 0.34 3.33 5.8 25.71 1.73 25.17 0.05 0.39 0.35 0.35 3.59 6.4 26.74 1.78 26.18 0.05 0.40 0.36 0.36 0.36 3.86 7.0 27.76 1.82 27.18 0.05 0.40 0.36 0.37 0.37 4.13 7.7 28.78 1.86 28.19 0.05 0.42 0.38 0.38 4.42 8.4 29.80 1.90 29.19 0.06 0.44 0.39 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.46 0.41 0.41 5.34 10.8 32.86 2.02 32.21 0.06 0.46 0.42 0.42 0.42 5.67 11.7 33.88 2.06 33.21 0.07 0.45 0.42 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.55 0.50 0.42 0.43 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.55 0.45 0.46 0.46 0.46 7.07 11.7 33.88 2.06 33.21 0.07 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45		0.25	0.25	1.48	2.0	16.53	1.35	16.13	0.03	0.28
0.30 0.30 2.41 3.8 21.63 1.57 21.15 0.04 0.34 0.31 0.31 0.31 2.62 4.2 22.65 1.61 22.16 0.04 0.35 0.32 0.32 0.32 2.85 4.7 23.67 1.65 23.16 0.04 0.35 0.33 0.33 3.09 5.2 24.69 1.69 24.17 0.04 0.35 0.34 0.34 3.33 5.8 25.71 1.73 25.17 0.05 0.39 0.35 0.35 3.59 6.4 26.74 1.78 26.18 0.05 0.40 0.36 0.36 0.36 3.86 7.0 27.76 1.82 27.18 0.05 0.40 0.36 0.37 0.37 4.13 7.7 28.78 1.86 28.19 0.05 0.42 0.38 0.38 4.42 8.4 29.80 1.90 29.19 0.06 0.44 0.39 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.46 0.41 0.41 5.34 10.8 32.86 2.02 32.21 0.06 0.46 0.42 0.42 0.42 5.67 11.7 33.88 2.06 33.21 0.07 0.45 0.42 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.55 0.50 0.42 0.43 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.55 0.45 0.46 0.46 0.46 7.07 11.7 33.88 2.06 33.21 0.07 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45		0.26	0.26	1.64	2.3	17.55	1.40	17.13	0.03	0.29
0.30 0.30 2.41 3.8 21.63 1.57 21.15 0.04 0.34 0.31 0.31 0.31 2.62 4.2 22.65 1.61 22.16 0.04 0.35 0.32 0.32 0.32 2.85 4.7 23.67 1.65 23.16 0.04 0.35 0.33 0.33 3.09 5.2 24.69 1.69 24.17 0.04 0.35 0.34 0.34 3.33 5.8 25.71 1.73 25.17 0.05 0.39 0.35 0.35 3.59 6.4 26.74 1.78 26.18 0.05 0.40 0.36 0.36 0.36 3.86 7.0 27.76 1.82 27.18 0.05 0.40 0.36 0.37 0.37 4.13 7.7 28.78 1.86 28.19 0.05 0.42 0.38 0.38 4.42 8.4 29.80 1.90 29.19 0.06 0.44 0.39 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.46 0.41 0.41 5.34 10.8 32.86 2.02 32.21 0.06 0.46 0.42 0.42 0.42 5.67 11.7 33.88 2.06 33.21 0.07 0.45 0.42 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.55 0.50 0.42 0.43 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.55 0.45 0.46 0.46 0.46 7.07 11.7 33.88 2.06 33.21 0.07 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45	- 1	0.27	0.27	2.00	2.0	10.57	1 44	10.14	0.03	0.30
0.30 0.30 2.41 3.8 21.63 1.57 21.15 0.04 0.34 0.31 0.31 0.31 2.62 4.2 22.65 1.61 22.16 0.04 0.35 0.32 0.32 0.32 2.85 4.7 23.67 1.65 23.16 0.04 0.35 0.33 0.33 3.09 5.2 24.69 1.69 24.17 0.04 0.35 0.34 0.34 3.33 5.8 25.71 1.73 25.17 0.05 0.39 0.35 0.35 3.59 6.4 26.74 1.78 26.18 0.05 0.40 0.36 0.36 0.36 3.86 7.0 27.76 1.82 27.18 0.05 0.40 0.36 0.37 0.37 4.13 7.7 28.78 1.86 28.19 0.05 0.42 0.38 0.38 4.42 8.4 29.80 1.90 29.19 0.06 0.44 0.39 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.46 0.41 0.41 5.34 10.8 32.86 2.02 32.21 0.06 0.46 0.42 0.42 0.42 5.67 11.7 33.88 2.06 33.21 0.07 0.45 0.42 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.55 0.50 0.42 0.43 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.55 0.45 0.46 0.46 0.46 7.07 11.7 33.88 2.06 33.21 0.07 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45		0.20	0.20	2.00	3.4	20 61	1 50	77.14	0.03	0.31
0.32		0.29	0.25	2.20	38	21 63	1 57	20.15	0.04	0.33
0.34		0.31	0.31	2.62	4.2	22.65	1.61	22.16	0.04	0.35
0.34		0.32	0.32	2.85	4.7	23.67	1.65	23.16	0.04	0.36
0.34		0.33	0.33	3.09	5.2	24.69	1.69	24.17	0.04	0.37
0.37 0.37 4.13 7.7 28.78 1.86 28.19 0.05 0.42 0.38 0.38 4.42 8.4 29.80 1.90 29.19 0.06 0.44 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.46 0.40 0.40 5.03 9.9 31.84 1.98 31.20 0.06 0.46 0.41 0.41 5.34 10.8 32.86 2.02 32.21 0.06 0.47 0.42 0.42 5.67 11.7 33.88 2.06 33.21 0.07 0.49 0.43 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.50 0.42 0.45 6.7 11.7 33.88 2.06 33.21 0.07 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45		0.34	0.34	3.33	5.8	25.71	1.73	25.17	0.05	0.39
0.37 0.37 4.13 7.7 28.78 1.86 28.19 0.05 0.42 0.38 0.38 4.42 8.4 29.80 1.90 29.19 0.06 0.44 0.39 0.39 4.72 9.1 30.82 1.94 30.20 0.06 0.46 0.40 0.40 5.03 9.9 31.84 1.98 31.20 0.06 0.46 0.41 0.41 5.34 10.8 32.86 2.02 32.21 0.06 0.47 0.42 0.42 5.67 11.7 33.88 2.06 33.21 0.07 0.49 0.43 0.43 6.01 12.6 34.90 2.09 34.22 0.07 0.50 0.42 0.45 6.7 11.7 33.88 2.06 33.21 0.07 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45		0.35	0.35	3.59	6.4	26.74	1.78	26.18	0.05	0.40
0.39		0.36	0.36				1 82	27 19	0 05	0.41
0.39		0.37	0.37	4.13	7.7	28.78	1.86	28.19	0.05	0.42
0.41				4.42	8.4	29.80	1.90	29.19	0.06	0.44
0.41				4.72	9.1	30.82	1.94	30.20	0.06	0.45
O.43				5.03	9.9	31.84	1.98	31.20	0.06	0.46
O.43				5.34	10.8	32.86	2.02	32.21	0.06	0.47
WSEL DEPTH FLOW RATE PER VEL WET (FT) (F				5.67	11.7	33.88	2.06		0.07	
INC										
(FT) (FT) SQ.FT. (CFS) (FT) (FPS) (FT) (FT) (FT) 0.45 0.45 6.71 14.6 36.94 2.17 36.23 0.07 0.52 0.46 0.46 7.07 15.9 36.96 2.25 36.23 0.08 0.54 0.47 0.47 7.44 17.3 36.98 2.32 36.24 0.08 0.59 0.48 0.48 7.80 18.7 37.01 2.40 36.24 0.09 0.55 0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.56 0.50 0.50 8.52 21.7 37.05 2.54 36.25 0.10 0.60 0.51 0.51 8.89 23.2 37.07 2.61 36.26 0.11 0.62 0.52 0.52 9.25 24.8 37.09 2.68 36.26 0.11 0.62 0.54 0.54 9.97 </td <td></td> <td>n warr</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>TOPWID</td> <td></td> <td></td>		n warr						TOPWID		
0.45 0.45 6.71 14.6 36.94 2.17 36.23 0.07 0.52 0.46 0.46 7.07 15.9 36.96 2.25 36.23 0.08 0.54 0.47 0.47 7.44 17.3 36.98 2.32 36.24 0.08 0.55 0.48 0.48 7.80 18.7 37.01 2.40 36.24 0.09 0.57 0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.55 0.50 0.50 8.52 21.7 37.05 2.54 36.25 0.10 0.60 0.51 0.51 8.89 23.2 37.07 2.61 36.26 0.11 0.62 0.52 0.52 9.25 24.8 37.09 2.68 36.26 0.11 0.63 0.53 0.53 9.61 26.4 37.11 2.75 36.27 0.12 0.61 0.54 0.54 9.97 28.1 37.13 2.82 36.27 0.12 0.62 0.55<		(PC)						(FT)		
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0.47 0.47 7.44 17.3 36.98 2.32 36.24 0.08 0.55 0.48 0.48 7.80 18.7 37.01 2.40 36.24 0.09 0.57 0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.58 0.50 0.50 8.52 21.7 37.05 2.54 36.25 0.10 0.60 0.51 0.51 8.89 23.2 37.07 2.61 36.26 0.11 0.62 0.52 0.52 9.25 24.8 37.09 2.68 36.26 0.11 0.63 0.53 0.53 9.61 26.4 37.11 2.75 36.27 0.12 0.69 0.54 0.54 9.97 28.1 37.13 2.82 36.27 0.12 0.69 0.55 0.55 10.34 29.8 37.15 2.89 36.28 0.13 0.61 0.56 0.56 10.70 31.6 37.17 2.95 36.28 0.14 0.70 0.5										0.54
0.48 0.48 7.80 18.7 37.01 2.40 36.24 0.09 0.57 0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.58 0.50 0.50 8.52 21.7 37.05 2.54 36.25 0.10 0.60 0.51 0.51 8.89 23.2 37.07 2.61 36.26 0.11 0.62 0.52 0.52 9.25 24.8 37.09 2.68 36.26 0.11 0.63 0.53 0.53 9.61 26.4 37.11 2.75 36.27 0.12 0.69 0.54 0.54 9.97 28.1 37.13 2.82 36.27 0.12 0.69 0.55 0.55 10.34 29.8 37.15 2.89 36.28 0.13 0.61 0.56 0.56 10.70 31.6 37.17 2.95 36.28 0.14 0.70 0.57 0.57 11.06 33.4 37.19 3.02 36.29 0.14 0.70 0.									0.08	0.55
0.49 0.49 8.16 20.2 37.03 2.47 36.25 0.09 0.58 0.50 0.50 8.52 21.7 37.05 2.54 36.25 0.10 0.66 0.51 0.51 8.89 23.2 37.07 2.61 36.26 0.11 0.62 0.52 0.52 9.25 24.8 37.09 2.68 36.26 0.11 0.61 0.53 0.53 9.61 26.4 37.11 2.75 36.27 0.12 0.61 0.54 0.54 9.97 28.1 37.13 2.82 36.27 0.12 0.61 0.55 0.55 10.34 29.8 37.15 2.89 36.28 0.13 0.62 0.56 0.56 10.70 31.6 37.17 2.95 36.28 0.14 0.71 0.57 0.57 11.06 33.4 37.19 3.02 36.29 0.14 0.71 0.59 0.59 11.79 37.1 37.23 3.15 36.30 0.15 0.72 0										
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0.52 0.52 9.25 24.8 37.09 2.68 36.26 0.11 0.63 0.53 0.53 9.61 26.4 37.11 2.75 36.27 0.12 0.69 0.54 0.54 9.97 28.1 37.13 2.82 36.27 0.12 0.66 0.55 0.55 10.34 29.8 37.15 2.89 36.28 0.13 0.61 0.56 0.56 10.70 31.6 37.17 2.95 36.28 0.14 0.70 0.57 0.57 11.06 33.4 37.19 3.02 36.29 0.14 0.71 0.58 0.58 11.43 35.2 37.21 3.08 36.29 0.15 0.72 0.59 0.59 11.79 37.1 37.23 3.15 36.30 0.15 0.72 0.60 0.60 12.15 39.0 37.25 3.21 36.30 0.16 0.73 0.61 0.61 12		0.50	0.50	8.52	21.7	37.05	2.54	36.25	0.10	0.60
0.53 0.53 9.61 26.4 37.11 2.75 36.27 0.12 0.69 0.54 0.54 9.97 28.1 37.13 2.82 36.27 0.12 0.66 0.55 0.55 10.34 29.8 37.15 2.89 36.28 0.13 0.61 0.56 0.56 10.70 31.6 37.17 2.95 36.28 0.14 0.70 0.57 0.57 11.06 33.4 37.19 3.02 36.29 0.14 0.71 0.58 0.58 11.43 35.2 37.21 3.08 36.29 0.15 0.71 0.59 0.59 11.79 37.1 37.23 3.15 36.30 0.15 0.72 0.60 0.60 12.15 39.0 37.25 3.21 36.30 0.16 0.73 0.61 0.61 12.51 40.9 37.27 3.27 36.31 0.17 0.73 0.62 0.62 12.88 42.9 37.31 3.33 36.31 0.17 0.73 <										0.62
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0.55 0.55 10.34 29.8 37.15 2.89 36.28 0.13 0.68 0.56 0.56 10.70 31.6 37.17 2.95 36.28 0.14 0.70 0.57 0.57 11.06 33.4 37.19 3.02 36.29 0.14 0.70 0.58 0.58 11.43 35.2 37.21 3.08 36.29 0.15 0.70 0.59 0.59 11.79 37.1 37.23 3.15 36.30 0.15 0.70 0.60 0.60 12.15 39.0 37.25 3.21 36.30 0.16 0.70 0.61 0.61 12.51 40.9 37.27 3.27 36.31 0.17 0.70 0.62 0.62 12.88 42.9 37.29 3.33 36.31 0.17 0.70 0.63 0.63 13.24 44.9 37.31 3.39 36.32 0.18 0.80 0.64 0.64 13.60 47.0 37.34 3.45 36.32 0.19 0.80										0.65
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0.58 0.58 11.43 35.2 37.21 3.08 36.29 0.15 0.73 0.59 0.59 11.79 37.1 37.23 3.15 36.30 0.15 0.74 0.60 0.60 12.15 39.0 37.25 3.21 36.30 0.16 0.74 0.61 0.61 12.51 40.9 37.27 3.27 36.31 0.17 0.76 0.62 0.62 12.88 42.9 37.29 3.33 36.31 0.17 0.76 0.63 0.63 13.24 44.9 37.31 3.39 36.32 0.18 0.88 0.64 0.64 13.60 47.0 37.34 3.45 36.32 0.19 0.88 0.65 0.65 13.97 49.1 37.36 3.51 36.33 0.19 0.8 0.66 0.66 14.33 51.2 37.38 3.57 36.33 0.20 0.8 0.67 0.67 14.69 53.4 37.40 3.63 36.34 0.20 0.8 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.70</td>										0.70
0.59 0.59 11.79 37.1 37.23 3.15 36.30 0.15 0.70 0.60 0.60 12.15 39.0 37.25 3.21 36.30 0.16 0.70 0.61 0.61 12.51 40.9 37.27 3.27 36.31 0.17 0.71 0.62 0.62 12.88 42.9 37.29 3.33 36.31 0.17 0.72 0.63 0.63 13.24 44.9 37.31 3.39 36.32 0.18 0.88 0.64 0.64 13.60 47.0 37.34 3.45 36.32 0.19 0.88 0.65 0.65 13.97 49.1 37.36 3.51 36.33 0.19 0.8 0.66 0.66 14.33 51.2 37.38 3.57 36.33 0.20 0.8 0.67 0.67 14.69 53.4 37.40 3.63 36.34 0.20 0.8										0.71
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0.64 0.64 13.60 47.0 37.34 3.45 36.32 0.19 0.81 0.65 0.65 13.97 49.1 37.36 3.51 36.33 0.19 0.81 0.66 0.66 14.33 51.2 37.38 3.57 36.33 0.20 0.81 0.67 0.67 14.69 53.4 37.40 3.63 36.34 0.20 0.81										
0.65 0.65 13.97 49.1 37.36 3.51 36.33 0.19 0.8 0.66 0.66 14.33 51.2 37.38 3.57 36.33 0.20 0.8 0.67 0.67 14.69 53.4 37.40 3.63 36.34 0.20 0.8										
0.66 0.66 14.33 51.2 37.38 3.57 36.33 0.20 0.8 0.67 0.67 14.69 53.4 37.40 3.63 36.34 0.20 0.8										0.84
0.67 0.67 14.69 53.4 37.40 3.63 36.34 0.20 0.8										0.86
										0.87
										0.88

BISON SPRINGS ST.

PC PROGRAM STREAM

MANNING	'S N= .0	17 SLOPE=	031				•		
POINT	DIST	ELEV I	POINT	DIST	ELEV I	POINT DI	ST EL	EV	• :
1		0.83		1.00	0.13	9 37.1		7	
2		0.67		3.00	0.41	10 37.6		7	**
3		0.67		5.00	0.13	11 46.0		3	
3 4	9.00	0.00		37.00	0.00	12 0.0			
□ WSEL	DEPTH			ETTED				NERGY	
□ M2FT	INC		RATE	PER	VEL			HEAD	
/ mm\	(FT)		(CFS)	(FT)	(FPS)	(FT)	(FT)	(FT)	
(FT)	0.01	0.00	0.0	0.33	0.44	0.31	0.00	0.01	
0.01		0.00	0.0	0.55	0.44	0.63	0.01	0.03	
0.02	0.02		0.0	0.99	0.05	0.03	0.01	0.04	÷
0.03	0.03	0.01	0.0	1.32	1.10	1.25	0.02	0.06	•
0.04	0.04	0.03	0.0	1.64	1.27	1.56	0.03	0.08	
0.05	0.05	0.04	0.1	1.97	1.44	1.88	0.03	0.09	
0.06	0.06	0.06		2.30	1.59	2.19	0.04	0.11	:
0.07	0.07	0.08	0.1			2.50	0.05	0.13	
0.08	0.08	0.10	0.2	2.63	1.74	2.81	0.05	0.15	
0.09	0.09	0.13	0.2	2.96	1.88		0.06	0.15	
0.10		0.16	0.3	3.29	2.02	3.13		0.18	
0.11		0.19	0.4	3.62	2.15	3.44	0.07		
0.12		0.23	0.5	3.95	2.28	3.75	0.08	0.20	•
0.13		0.26	0.6	4.28	2.41	4.07	0.09	0.22	•
0.14		0.31	0.7	5.15	2.36	4.93	0.09	0.23	
0.15		0.36	0.9	6.03	2.36	5.79	0.09	0.24	. :
0.16		0.43	1.0	6.91	2.40	6.65	0.09	0.25	
0.17	0.17	0.50	1.2	7.79	2.45	7.51	0.09	0.26	
0.18		0.58	1.5	8.67	2.52	8.38	0.10	0.28	
0.19	0.19	0.66	1.7	9.54	2.60	9.24	0.11	0.30	
0.20	0.20	0.76	2.0	10.42	2.69	10.10	0.11	0.31	
0.21	0.21	0.87	2.4	11.30	2.78	10.96	0.12	0.33	•
0.22		0.98	2.8	12.18	2.87	11.83	0.13	0.35	
0.23		1.10	3.3	13.06	2.96	12.69	0.14	0.37	:
0.24		1.23	3.8	13.93	3.06	13.55	0.15	0.39	:
0.25		1.37	4.3	14.81	3.15	14.41	0.15	0.40	
0.26		1.52	4.9	15.69	3.25	15.27	0.16	0.42	·
0.27		1.68	5.6	16.57	3.34	16.14	0.17	0.44	
0.28			6.3	17.45	3.44	17.00	0.18	0.46	
0.29			7.1	18.32	3.54	17.86	0.19	0.48	
0.30			8.0	19.20	3.63	18.72	0.20	0.50	
0.3			8.9	20.08	3.73	19.59	0.22	0.53	
0.3			9.9	20.96	3.82	20.45	0.23	0.55	•
0.3			11.0		3.92	21.31	0.24	0.57	
0.3			12.1	22.71	4.01	22.17	0.25	0.59	
0.3			13.3	23.59	4.10	23.03	0.26	0.61	
0.3			14.6	24.47	4.19	23.90	0.27	0.63	•
0.3			16.0	25.35	4.28	24.76	0.29	0.66	
0.3			17.4	26.23	4.38	25.62	0.30	0.68	
0.3			18.9	27.10	4.47		0.31	0.70	
0.3			20.5	27.98	4.55		0.32	0.72	•
			22.2	28.86	• •		0.33	0.74	
0.4			24.4	28.88	4.82		0.36	0.78	
0.4			26.7	28.90	5.00		0.39	0.82	
0.4				WETTED	FLOW	TOPWID	VEL	ENERGY	4
☐ WSEL			FLOW			TOPWID		HEAD	
	INC	AREA	RATE	PER	VEL (TEC)	/ mm\	HEAD		
(FT)			(CFS)	(FT)	(FPS)		(FT)	(FT)	
0.4			31.6	28.94				0.89	-STREET CAPACITY
0.4			34.1				0.47	0.93	000000
0.4			36.7					0.97	CAPACILY
0.4			39.4					1.01	
0.4	19 0.4	9 7.04	42.1	29.03	5.99	28.25	0.56	1.05	
	•				4.29 - 7.5				•

MANNING'S N= .017 SLOPE= .025

PC PROGRAM STREAM

POINT	DIST	ELEV	POINT	DIST	ELEV	POINT D	IST EL	EV
1	0.00	0.83	5	11.00	0.13	9 37.	17 0.6	7
2	8.38	0.67	6 7	23.00	0.41	10 37.	63 0.6	7
3	8.83	0.67	7	35.00	0.13	11 46.	00 0.8	3
4	9.00	0.00	8	37.00	0.00		0.0	0
□ WSEL	9.00 5.00	FLOW		WETTED	FLOW	TOPWID		NERGY
□ M2FT	TNC	עשטע	DATE		VEL			HEAD
/ mm \	TIAC	AREA SQ.FT.	(CEG)	(FT)	(FPS)	(FT)	(FT)	
(FT)		0.00	0.0	0.33	0.39	0.31	0.00	
0.01	0.01		0.0	0.66	0.52	0.53		
0.02	0.02	0.01	0.0	0.99	0.02	0.63 0.94	0.01 0.01	0.04
0.03	0.03	0.01	0.0	1.32	0.01	1.25	0.02	0.06
0.04	0.04		0.0	1.52	1.14	1.56	0.02	0.07
0.05	0.05	0.04	0.1	1 07		1.88	0.03	0.09
0.06	0.06	0.06	0.1		1.43	2.19	0.03	0.10
0.07	0.07	0.08	0.1	2.30	1.56	2.50	0.04	0.12
0.08	0.08	0.10	0.2	4.63	1.69	2.81	0.04	0.13
0.09		0.13	0.2	2.90	1 03		0.05	0.15
0.10	0.10	0.16	0.3	3.29	1.81	3.44	0.06	0.17
0.11		0.19	0.4	3.62	1.93 2.05	3.44	0.00	0.17
0.12		0.23	0.5					0.19
0.13		0.26	0.6				0.07	0.20
0.14		0.31	0.7		2.12			0.21
0.15		0.36	0.8		2.12			0.22
0.16		0.43	0.9	6.91	2.15		0.07	0.25
0.17			1.1		2.20	7.51	0.08	
0.18		0.00	1.3		2.27	8.38		0.26
0.19		0.66	1.6		2.34			0.27
0.20	0.20		1.8	10.42	2.41	10.10		0.29
0.21	0.21			11.30	2.49	10.96		0.31
0.22	0.22				2.58			0.32
0.23	0.23		2.9		2.66			0.34
0.24			3.4	13.93	2.74	13.55		0.36
0.25	0.25	1.37	3.9	14.81	2.83	14.41		0.37
0.26	0.26		4.4		2.92			0.39
0.27	7 0.27		5.0		3.00			0.41
0.28	0.28		5.7		3.09	17.00	0.15	0.43
0.29	9 0.29	2.02	6.4		3.18		0.16	
0.30	0.30		7.2		3.26			
0.3	1 0.31	2.39		0 20.08	3.35	19.59 20.45	0.17	0.48
0.33	2 0.32	2.59	8.9	9 20.96	3.43	20.45	0.18	0.50
0.33				9 21.84	3.52	21.31	0.19	
0.3	4 0.34	3.02	10.	9 22.71	3.60	22.1/		
0.3	5 0.35	3.25			3.68			0.56
0.3	6 0.36	3.48	13.		3.77			0.58
0.3	7 0.37	7 3.72	14.	3 25.35	3.85			0.60
0.3	8 0.38	3.98	15.	6 26.23	3.93			0.62
0.3	9 0.39	9 4.24	17.		4.0			0.64
0.4		0 4.50	18.	4 27.98	4.0			0.66
0.4	1 0.4	1 4.78	19.	9 28.86	4.1	7 28.21		0.68
0.4	2 0.4	2 5.06	21.	9 28.88	4.3			0.71
0.4	3 0.4	3 5.35	24.	0 28.90	4.4	9 28.22		0.74
☐ WSEL	DEPT:	H FLOW	FLOW	WETTED	FLOW	TOPWID	VEL	ENERGY
	INC	AREA	RATE	E PER	VEL		HEAD	HEAD
(FT)) SQ.FT	. (CFS	s) (FT)	(FPS			(FT)
0.4				.3 28.94	4.7	9 28.2	3 0.36	0.81
0.4				.6 28.96	4.9	4 28.2		0.84
0.4				.0 28.98	5.0	9 28.2		
0.4			35.	.4 29.01	. 5.2	3 28.2		
0.4			37	.8 29.03	5.3	8 28.2	5 0.45	0.94

MANNING'S N=	.017	SLOPE=	.035

PC PROGRAM STREAM

THEMILING		02.							
POINT	DIST	ELEV	POINT	DIST	ELEV	POINT D	IST E	ELEV	
1	0.00	0.83	5	11.00	0.13			.67	•
2	8.38	0.67	6	23.00	0.41			.67	
	8.83			35.00		11 46.		.83	
4	0.05	0.07	, 8	37.00		12 0.		.00	
4 □ WSEL	7.00 2.00	0.00 FLOW	FLOW W			TOPWID		ENERGY	
п мэгр	DECIL	AREA	RATE	PER	VET.	TOLWID	HEAD		
(mm)	/ TMC	SQ.FT.				(FT)			
		0.00	0.0	0.33	0.46	U 31	0.00	0.01	
	0.01		0.0	0.55	0.40	0.31 0.63	0.00	0.01	
0.02	0.02	0.01	0.0		0.73	0.83	0.01	0.03	
0.03	0.03	0.01			1 17	1,25	0.01	0.04	
0.04	0.04						0.02	0.08	
0.05	0.05		0.1		1.35 1.53	1.56 1.88	0.03	0.10	
0.06	0.06		0.1	1.97	1.69	2.19	0.04	0.10	
0.07	0.07	0.08	0.1	2.30		2.13		0.11	
0.08	0.08	0.10		2.63	1.85	2.50	0.05		
0.09	0.09		0.3	2.96	2.00	2.81	0.06	0.15	
0.10	0.10	0.16	0.3	3.29	2.15	3.13 3.44	0.07	0.17	
0.11	0.11		0.4	3.62	2.29	3.44	0.08	0.19	
0.12	0.12		0.5			3.75	0.09	0.21	
0.13	0.13			4.28	2.56	4.07	0.10	0.23	
0.14	0.14		0.8	5.15 6.03	2.51 2.51	4.93	0.10	0.24	
0.15	0.15	0.36	0.9	6.03	2.51	5.79		0.25	
0.16	0.16		1.1	6.91	2.55			0.26	
0.17			1.3	7.79	2.61	7.51	0.11	0.28	
0.18			1.5	7.79 8.67 9.54	2.68	8.38 9.24	0.11	0.29	
0.19		0.66	1.8	9.54	2.76	9.24	0.12	0.31	
0.20	0.20	0.76	2.2	10.42	2.85			0.33	
0.21	0.21				2.95	10.96		0.35	
0.22	0.22	0.98	3.0	12.18	3.05	11.83		0.36	
0.23	0.23	1.10	3.5	13.06	3.15	12.69	0.15		
0.24	0.24		4.0	13.93	3.25	13.55	0.16	0.40	
0.25	0.25	1.37	4.6	14.81					
0.26	0.26	1.52	5.3	15.69	3.45	15.27			
0.27	0.27	1.68	6.0	16.57	3.55		0.20		
0.28	0.28	1.84	6.7	17.45	3.66				
0.29	0.29	2.02	7.6	18.32	3.76		0.22	0.51	
0.30	0.30	2.20	8.5	19.20	3.86 3.96	18.72	0.23	0.53	
0.31	0.31	2.39			3.96	19.59	0.24	0.55	
0.32	0.32	2.59	10.5	20.96	4.06	20.45	0.26	0.58	
0.33		2.80	11.7	21.84	4.16	21.31	0.27		
0.34		3.02	12.9	22.71	4.26	22.17	0.28	0.62	
0.35	0.35	3.25	14.1	23.59	4.36	23.03	0.29	0.64	
0.36	0.36	3.48	15.5	24.47	4.46	23.90	0.31	0.67	
0.37			17.0	25.35	4.55	24.76	0.32	0.69	
0.38			18.5	26.23	4.65	25.62	0.34	0.72	
0.39			20.1	27.10	4.74		0.35	0.74	
0.40		0 4.50	21.8	27.98	4.84	27.35	0.36	0.76	
0.43			23.6		4.93			0.79	
0.42			25.9		5.12				
0.43			28.4		5.31				< 10
□ WSEL				WETTED	FLOW		VEL		-STREET CAPA
	INC			PER	VEL		HEAD	HEAD	CADE
(FT)	(FT				(FPS)	(FT)	(FT)	(FT)	J 117
0.4									
0.4									
0.4									
0.4									
0.4									
0.4	J 0. ±	,.04	11.0	27.03	0.50	. 20.23	0.0.	- 4-14	

BISON SPRINGS ST.

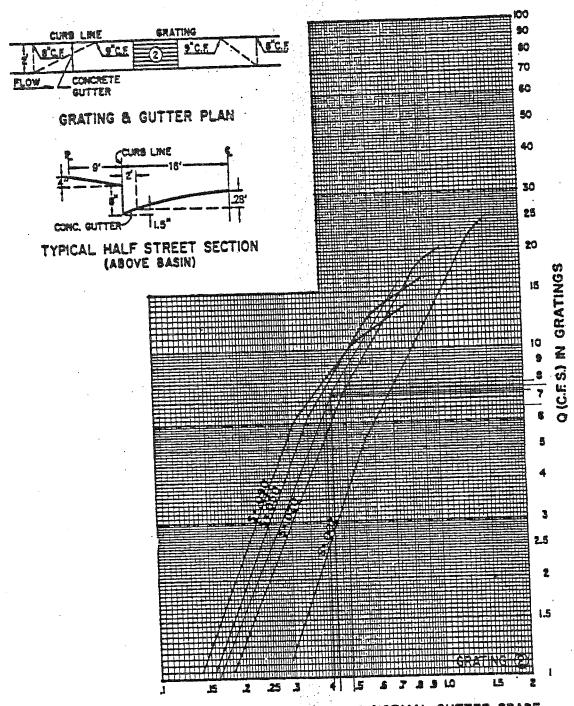
MANNING'S N= .017 SLOPE= .018

		•			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				
POINT	DIST	ELEV	POINT	DIST	ELEV POINT D	IST EL	EA		*
1		0.83			0.13 9 37.				
2		0.67			0.41 10 37.				
		0.67			0.13 11 46.				
3				37.00		00 0.0			
4		0.00					NERGY		
□ WSEL	DEPTH	FLOW			FLOW TOPWID		and the second s		
	INC	AREA	RATE	PER	VEL		HEAD		
(FT)	(FT)	SQ.FT.	(CFS)	(FT)	(FPS) (FT)	(FT)	(FT)		
0.01	0.01	0.00	0.0	0.33	0.33 0.31	0.00	0.01		
0.02	0.02	0.01	0.0	0.66	0.53 0.63	0.00	0.02		•
0.03	0.03	0.01	0.0	0.99	0.69 0.94	0.01	0.04		
	0.04	0.03	0.0	1.32	0.84 1.25	0.01	0.05		
0.04			0.0	1.64	0.97 1.56	0.01	0.06		
0.05	0.05	0.04							
0.06	0.06	0.06	0.1	1.97	1.09 1.88	0.02	0.08		
0.07	0.07	0.08	0.1	2.30	1.21 2.19	0.02	0.09		.*
0.08	0.08	0.10	0.1	2.63	1.33 2.50	0.03	0.11		•
0.09	0.09	0.13	0.2	2.96	1.43 2.81	0.03	0.12		
0.10	0.10	0.16	0.2	3.29	1.54 3.13	0.04	0.14		
0.11	0.11	0.19	0.3	3.62	1.64 3.44	0.04	0.15 '		
0.12	0.12	0.23	0.4	3.95	1.74 3.75	0.05	0.17		•
	0.12	0.26	0.5	4.28	1.83 4.07	0.05	0.18		
0.13					1.80 4.93	0.05	0.19		
0.14	0.14	0.31	0.6	5.15					
0.15	0.15	0.36	0.7	6.03	1.80 5.79	0.05	0.20		
0.16	0.16	0.43	0.8	6.91	1.83 6.65	0.05	0.21		
0.17	0.17	0.50	0.9	7.79	1.87 7.51	0.05	0.22		
0.18	0.18	0.58	1.1	8.67	1.92 8.38	0.06	0.24		•
0.19	0.19	0.66	1.3	9.54	1.98 9.24	0.06	0.25		
0.20	0.20	0.76	1.6	10.42	2.05 10.10	0.07	0.27		
0.21	0.21	0.87	1.8	11.30	2.11 10.96	0.07	0.28		
		0.98	2.1	12.18	2.18 11.83	0.07	0.29		1.
0.22			2.5	13.06	2.26 12.69	0.08	0.31		. '
0.23		1.10					0.32		
0.24		1.23	2.9	13.93	2.33 13.55	0.08			
0.25		1.37	3.3	14.81	2.40 14.41	0.09	0.34		
0.26	0.26	1.52	3.8	15.69	2.48 15.27	0.10	0.36		
0.27	0.27	1.68	4.3	16.57	2.55 16.14	0.10	0.37		
0.28		1.84	4.8	17.45	2.62 17.00	0.11	0.39		
0.29		2.02	5.4	18.32	2.69 17.86	0.11	0.40		•
0.30		2.20	6.1	19.20	2.77 18.72	0.12	0.42		
0.31		2.39	6.8	20.08	2.84 19.59	0.13	0.44		•
0.31	0.32	2.59	7.6	20.96	2.91 20.45	0.13	0.45		
			8.4	21.84	2.98 21.31	0.14	0.47		•
0.33		2.80					0.48		
0.34		3.02	9.2	22.71	3.05 22.17	0.14			
0.35		3.25	10.1	23.59	3.13 23.03	0.15	0.50		
0.36		3.48	11.1	24.47	3.20 23.90	0.16	0.52		
0.37	7. 0.37	3.72	12.2	25.35	3.26 24.76	0.17	0.54		
0.38	0.38	3.98	13.3	26.23	3.33 25.62	0.17	0.55		
0.39	0.39	4.24	14.4	27.10	3.40 26.48		0.57		•
0.40	0.40	4.50	15.6	27.98	3.47 27.35	0.19	0.59		
0.41	0.41	4.78	16.9	28.86	3.54 28.21	0.19	0.60		
0.42		5.06	18.6	28.88	3.67 28.21	0.21	0.63		•
0.43			20.4	28.90	3.81 428.22		0.66		
□ WSEL				WETTED	FLOW TOPWID	VEL	ENERGY		
□ M2FT	DEPTH								
	INC		RATE	PER	VEL	HEAD	HEAD		
(FT)	(FT)			(FT)	(FPS) (FT)	(FT)	(FT)		
0.49			24.0	28.94	4.07 3 28.23		0.71		
0.46	6 0.46	6.19	26.0	28.96	4.19 28.23		0.73		*
0.4	7 0.47	6.48	28.0	28.98	4.32 28.24		0.76		
0.4		6.76	30.0	29.01	4.44 28.24		0.79		•
0.4			32.1	29.03	4.56 28.25		0.81		
0.5			34.3	29.05	4.68 28.29		0.84		
0.5				29.07	4.80 28.26		0.87		0.1000 -1
				29.09			0.89	STREET	CAPACITY
0.5								- 11	• 1
0.5				29.11	5.03 28.2		0.92		
0.5				29.13	5.14 28.2		0.95		
0.5				29.15	5.25 28.2		0.98		
0.5	6 0.56	9.02	48.4	29.17	5.36 28.2	0.45	1.01		

BISON SPRINGS ST.

Chapter 22 - Drainage, Flood Control and Erosion Control

GRATING CAPACITIES FOR TYPE 'A' . 'C' and'D'



D-DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

PLATE 22.3 D-5

SLOPE=3.52, D=0.43, Q=7.3 of SLOPE=1.82, D=0.48, D=75 ds

22-144

rainage Structure Analyzer

pe Hydraulic Analysis

Bison Springs St.

te: Friday, November 12, 2004 11:01:15

Input Data

Circular
RC C76-A
0.013000
Manning
43.4 cfs
2.500%
30.00 x 2.7500

itput Results

Flow Rate	43.4 cfs
lope	2.500%
/D	0.60
Capacity	64.9 cfs
Velocity	14.16 ft,
epth	1.50 ft
ritical Depth	2.19 ft
Size (W x T):	30.00 x 2.7500

Drainage Structure Analyzer

pe Hydraulic Analysis

BISON SPRINGS ST. SO

WALNUT CANYON TO BUCK ISLAND

Date: Tuesday, December 14, 2004 08:05:00

itput Results

14.6 cfs Flow Rate 3.500% lope 0.64 /D 19.7 cfs capacity 12.19 ft/s Velocity 0.96 ft epth ritical Depth 1.39 ft. 18.00 x 2.0000: size (W x T):

Orainage Structure Analyzer

pe Hydraulic Analysis

BISON SPRINGS ST. SD BUCK ISLAND TO BIG SPRINGS

Date: Tuesday, December 14, 2004 08:06:07

Input Data	
lape	Circular
iterial	Circular RC C76-A
Roughness	0.013000
thod	Manning
low Rate	44.4 cfs
Liope	1.800%
Size (W x T):	30.00 x 2.7500
	i de la companya de
itput Results	11.

~~~~~~~~	
Flow Rate	44.4 cfs
lope	1.800%
/D	0.68
capacity	55.0 cfs
Velocity	12.47 ft/s
epth	1.70 ft
ritical Depth	2.21 ft
Size (W x T):	30.00 x 2.7500

Drainage Structure Analyzer

BISON SPRINGS ST. SD BIG SPRINGS TO SUMP

pe Hydraulic Analysis

Date: Tuesday, December 14, 2004 08:07:09

Input Data

 lape
 Circular

 .terial
 RC C76-A

 Roughness
 0.013000

 Manning
 Manning

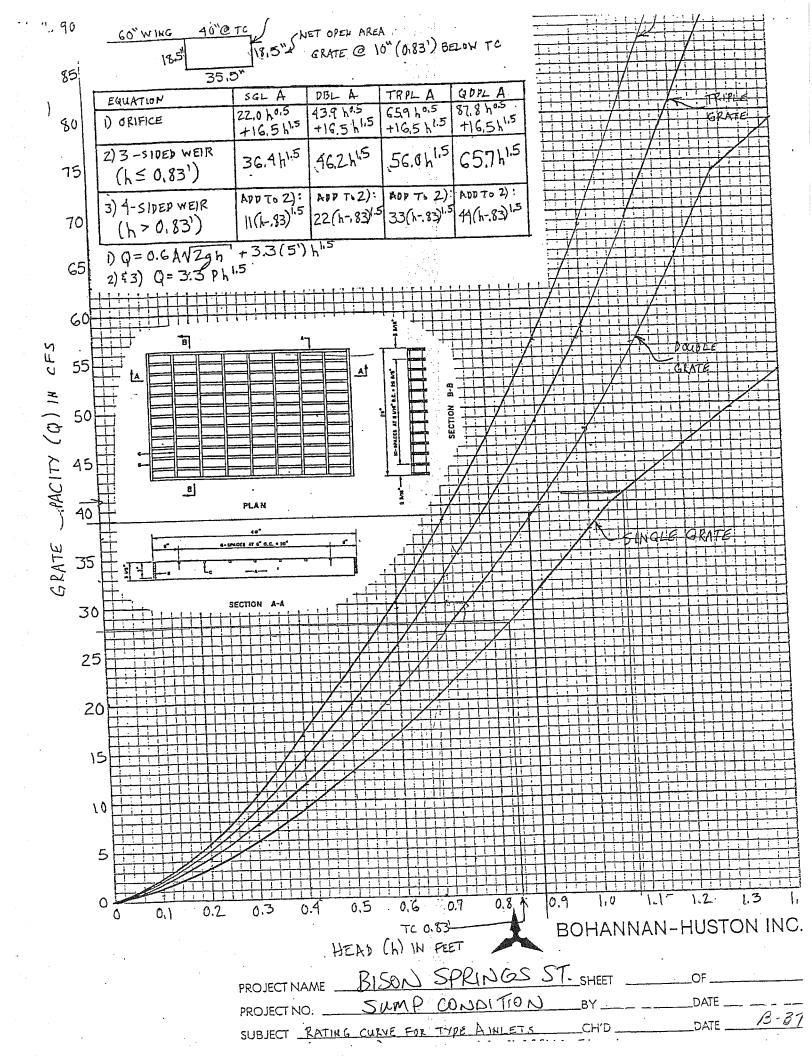
 low Rate
 87.8 cfs

 lope
 1.800%

 Size (W x T):
 36.00 x 3.0000

itput Results

87.8 cfs Flow Rate 1.800% -lope 0.80 -/D 89.5 cfs Lapacity 14.43 ft/s Velocity 2.41 ft epth 2.83 ft ritical Depth 36.00 x 3.0000 size (W x T):



Drainage Structure Analyzer

pe Hydraulic Analysis

SUMP INLET TO Tuesday, December 14, 2004 08:08:35

Tuesday, December 14, 2004 08:08:35

Tuesday, December 14, 2004 08:08:35

Date: Tuesday, December 14, 2004 08:08:35

Input Data

Circular iape RC C76-A terial 0.013000 Roughness Manning thod 126.5 cfs low Rate 1.800% .ope 42.00 x 3.5000 Size (W x T):

itput Results

126.5 cfs Flow Rate 1.800% lope 0.77 /D 135.0 cfs capacity 15.95 ft/s Velocity 2.69 ft apth 3.29 ft ritical Depth  $42.00 \times 3.5000$ size (W x T):

# APPENDIX C

INFRASTRUCTURE LIST

Current DRC Project No.

Figure 12

r 16, _

Date Preliminary Plat Approved: Date Preliminary Plat Expires:

Date Site Plan Approved:

Date Summed:

INFRASTRUCTURE LIST

EXHIBIT "A" TO SUBDIVISION IMPROVEMENTS AGREEMENT DEVELOPMENT REVIEW BOARD (D.R.B.) REQUIRED INFRASTRUCTURE LIST

APPLICATION NO.

DRB Project No.

SIERRA RANCH SUBDIVISION PRELIMINARY PLAT

City Cnst Engineer Following is a summary of PUBLIC/PRIVATE Infrastructure required to be constructed or financially guaranteed for the above development. This Listing is not necessarily a complete listing. During the SIA process and/or unforeseen items have not been included in the Infrastructure listing, the DRC Chair may include those items in the listing and related financial guarantees. All such revisions require guaranteens, if the DRC Chair determines that appurtenant or non-essential items can be deleted from the listing, those items may be deleted as well as the related portions of the financial guarantees. All such revisions require approval by the DRC Chair, the User Department and agentivowner. If such approvals are obtained, these revisions to the listing will be incorporated administratively. In addition, any unforeseen items which arise during construction which are necessary to complete the project and which normally are the Subdivider's responsibility will be required as a condition of project acceptance and close out by the City. Private Inspector မှ

From

Location

Type of Improvement

Size

COA DRC Project#

Sequence #

		R MESSINA DRIVE	RD AMOLE MESA AVENUE	MESSINA DRIVE	BISON SPRINGS STREET	BISON SPRINGS STREET EAST STUB TERMINUS.	BISON SPRINGS STREET	BISON SPRINGS STREET	BISON SPRINGS STREET MESSINA DRIVE	BISON SPRINGS STREET
		CHACO CANYON DR	GIBSON BOULEVARD	WEST BOUNDARY	WEST BOUNDARY	BISON SPRINGS ST	WEST BOUNDARY	WEST BOUNDARY	BISON SPRINGS ST	WEST BOUNDARY
		GIBSON BOULEVARD	MESSINA DRIVE	AMOLE MESA AVE	FOUR MILE ROAD	FOUR MILE ROAD	CORONA RANCH RD	WALNUT CANYON RD	WALNUT CANYON RD	BUCK ISLAND ROAD
	ONSITE PUBLIC ROADWAY IMPROVEMENTS	ARTERIAL PAVING W/ PCC CURB & GUTTER AND PCC 6' WIDE SIDEWALK ON SOUTH SIDE ONLY	RESIDENTIAL PAVING W/ PCC	SIDEWALK ON WEST SIDE ONLY RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4" WIDE SIDEWALK ON NORTH SIDE ONLY	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON NORTH SIDE ONLY*	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*
	ONSITE PUBLIC	30' EOA-F	24' EOA-F	24' EOA-F	28' F-F	24' F-F	28' F-F	28' F-F	52' F.F	28' F-F
SIERRA RANCH SUBDIVISION - UNIT I	5									

Pane 1 of 9

City Cnst Engineer											
City Inspector	~										
Private Inspector											
ę.		BIG SPRINGS ROAD	BISON SPRINGS STREET	FOUR MILE ROAD	WALNUT CANYON ROAD	BUCK ISLAND ROAD	SOUTH STUB TERMINUS	S PIPESTONE ROAD	AMOLE MESA AVENUE	GILA CLIFF DRIVE	
From	WEST BOUNDARY BI		AMOLE MESA AVE	GIBSON BOULEVARD	FOUR MILE ROAD	WALNUT CANYON RD	FOUR MILE ROAD	NORTH STUB TERMINUS PIPESTONE ROAD	PIPESTONE ROAD 07	STUB AND WEST SIDE OF	
Location		PIPESTONE ROAD	BIG SPRINGS ROAD	CHACO CANYON DR	SALADO CREEK ST	CARIZZO PLAIN DR	BISON SPRINGS ST	GILA CLIFF DRIVE	PEDESTRIAN ACCESS BETWEEN LOTS 206/207	DEFERRAL EXHIBIT 'B'. SIDE OF FOUR MILE ROAL	
Type of Improvement	ONSITE PUBLIC ROADWAY IMPROVEMENTS (CONT.)	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4" WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE	SIDEWALK ON BOTH SIDES? RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4 WIDE SIDEWALK ON EAST SIDE ONLY*	6' AC TRAIL	<ul> <li>SIDEWALKS TO BE DEFERRED PER DEFERRAL EXHIBIT'B'</li> <li>WAIVER OF SIDEWALK ON SOUTH SIDE OF FOUR MILE ROAD STUB AND WEST SIDE OF GILA CLIFF DRIVE</li> </ul>	STREET ! IGHTS AS PER COA DPM
Size	ONSITE PUBLIC	28' F-F	36' F-F	48' F-F	28' 돈-두	28' F-F	28' F-F	28' F-F	25' WIDE		===
COA DRC Project#											
SIA Sequence #											

STREET LIGHTS AS PER COA DPM

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City Chst Engineer												,				
City Inspector		_		_												
Private Inspector								_				1				
To			AMOLE MESA AVENUE	BISON SPRINGS STREET	SALADO CREEK STREET	WALNUT CANYON ROAD	BISON SPRINGS STREET	BISON SPRINGS STREET	BIG SPRINGS ROAD	BISON SPRINGS STREET	SOUTH STUB TERMINUS MESSINA DRIVE	MESSINA DRIVE				UIRED
From			GIBSON BLVD	LOT 29	WEST BOUNDARY	CORONA RANCH RD.	WEST BOUNDARY	LOT 138	WEST BOUNDARY	PIPESTONE ROAD	FOUR MILE ROAD BISON SPRINGS ST	BISON SPRINGS ST	:			D GRADING PLAN IS REQ
Location			MESSINA DRIVE	FOUR MILE ROAD	CORONA RANCH RD	SALADO CREEK ST.	WALNUT CANYON RD	BUCK ISLAND ROAD	PIPESTONE ROAD	BIG SPRINGS ROAD	BISON SPRINGS ST PUBLIC EASEMENT	WALNUT CANYON RD.	PARK TRACT	EL RANCHO GRANDE TRACT 16 NORTH	SIERRA RANCH UNIT 2	CATION OF THE APPROVE
Type of improvement		ONSITE PUBLIC STORM DRAIN IMPROVEMENTS	RCP W/ NEC. MH'S, LATERALS & INLETS	RCP W/ NEC. MH'S, LATERÀLS & INLETS	RCP W/ NEC. MH'S, LATERALS & INLETS	RCP W/ NEC. MH'S, LATERALS & INLETS RCP W/ NEC. MH'S, LATERALS	& INLETS RCP W/ NEC. MH'S, LATERALS & INLETS	4.2 ACRE-FEET SURGE POND WITH PUBLIC EASEMENT AND COVENANT AND AGREEMENT	3.5 ACRE-FEET TEMPORARY RETENTION POND WITH PUBLIC EASEMENT AND COVENANT AND AGREEMENT	2.6 ACRE-FEET TEMPORARY RETENTION POND WITH PUBLIC EASEMENT AND COVENANT AND AGREEMENT	A CRADING AND DRAINAGE CERTIFICATION OF THE APPROVED GRADING PLAN IS REQUIRED					
Size		ONSITE PUBLIC	18"-72" DIA	18" DIA	18"-24" DIA	24" DIA	18" - 30" DIA	18" DIA	18" - 24" DIA	24" DIA	18" - 36" DIA 42"					i C
COA DRC Project#	SIERRA RANCH SUBDIVISION - UNIT I	o,														
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NOTE: A GRADING AND DRAINAGE CERTIFICATION OF THE APPROVED GRADING PLAN IS REQUIRED PRIOR TO THE RELEASE OF FINANCIAL GUARANTEES.

THERE WILL BE NO RELEASE OF FINANCIAL GUARANTEE OR SIA UNTIL AGREEMENT IS PROCESSED AND APPROVED WITH AMAFCA FOR CONSTRUCTION OF THE AMOLE ARROYO IMPROVEMENTS.

City Cnst Engineer												
City Inspector									_	_		
Private Inspector									/			
٥.			FOUR MILE ROAD	EAST STUB TERMINUS	BISON SPRINGS ST	BISON SPRINGS ST	BISON SPRINGS ST	BIG SPRINGS RD	BISON SPRINGS ST	SOUTH STUB TERMINUS	NORTH STUB TERMINUS PIPESTONE ROAD WEST BOUNDARY MESSINA DRIVE	MESA ARENOSA
From			GIBSON BLVD	WEST BOUNDARY	AMOLE MESA AVE	FOUR MILE ROAD	NORTH STUB TERMIN WEST BOUNDARY	MESSINA DRIVE				
Location			CHACO CANYON DR	FOUR MILE ROAD	CORONA RANCH RD	WALNUT CANYON RD	BUCK ISLAND ROAD	PIPESTONE ROAD	BIG SPRINGS ROAD	BISON SPRINGS ST	GILA CLIFF DRIVE	AMOLE MESA AVE
Type of Improvement		ONSITE PUBLIC WATERLINE IMPROVEMENTS	WATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S	WATERLINE W/ NEC. VALVES FH'S. MJ'S & RJ'S	WATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S	WATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S WATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S						
Size		ONSITE PUBI	18" DIA	4-8" DIA	6" DIA	6" DIA	6" DIA	6" DIA	6-8" DIA	4-6" DIA	4" DIA	12" DIA 12" DIA
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	City Cnst Engineer			_					-											
	City Inspector		-	-		-														
	Private Inspector		_	•																:
	70		EAST STUB TERMINUS		BISON SPRINGS ST	BISON SPRINGS ST	BISON SPRINGS ST	BIG SPRINGS RD	BISON SPRINGS ST	S PIPESTONE ROAD	SOUTH STUB TERMINUS	MESSINA DRIVE		PUBLIC EASEMENT IN EL RANCHO GRANDE UNIT 15	FUTURE OPEN RANGE AVE. EXISTING STUB					
	From		WEST BOUNDARY		WEST BOUNDARY	WEST BOUNDARY	WEST BOUNDARY	WEST BOUNDARY	PIPESTONE ROAD	NORTH STUB TERMINUS PIPESTONE ROAD	FOUR MILE ROAD	BISON SPRINGS ST	PUBLIC EASEMENT	MESSINA DRIVE	AMOLE MESA AVENUE					
	Location		0 0 0 0 0		CORONA RANCH RD	WALNUT CANYON RD	BUCK ISLAND ROAD	PIPESTONE ROAD	BIG SPRINGS ROAD	GILA CLIFF DRIVE	BISON SPRINGS ST	PUBLIC EASEMENT	MESSINA DRIVE	AMOLE MESA AVE.	PUBLIC EASEMENT IN AMOL EL RANCHO GRANDE UNIT 15					
	Type of Improvement	STNEMBOOGENEED IMPROVEMENTS	SANITANI SENERI IN INC.	SANITARY SEWER W/ NEC. MH'S & SERVICES	SANITARY SEWER WI NEC. MH'S & SERVICES	SANITARY SEWER W/ NEC.	SANITARY SEWER W/ NEC. MH'S. & SERVICES	SANITARY SEWER W/ NEC. MH'S & SERVICES	SANITARY SEWER W/ NEC. MH'S & SERVICES											
	Size		ONSITE PUBLIC	8" DIA	10" DIA	10" DIA	10" DIA	8-10" DIA				. •	:							
	COA DRC Project#	SIERRA RANCH SUBDIVISION - UNIT I																		
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Engineer		_						-									
Inspector															-		
Private Inspector		,						_				,	_				
<b>T</b> o	ED FOR UNIT 2.		CHACO CANTON DA	EAST BOUNDARY	EAST BOUNDARY	EAST BOUNDARY	EAST BOUNDARY	ALAMO CANYON DRIVE	EAST BOUNDARY	EAST BOUNDARY	PIPESTONE ROAD	PIPESTONE ROAD	AMOLE MESA AVENUE	PIPESTONE ROAD	WALNUT CANYON ROAD	PIPESTONE ROAD	
From	NOTE: ALL UNIT 1 PUBLIC IMPROVEMENTS REQUIRED FOR UNIT 2.		WEST BOUNDARY	WEST BOUNDARY	PIPESPRING STREET	PIPESPRING STREET	PIPESPRING STREET	WEST STUB TERMINUS	ALAMO CANYON DR	PIPESPRING STREET	FOUR MILE ROAD	WALNUT CANYON RD	PIPESTONE ROAD	BUCK ISLAND ROAD	FOUR MILE ROAD	BUCK ISLAND ROAD	AD STUB
Location	IOTE: ALL UNIT 1 PUBLIC		GIBSON BOULEVARD	AMOLE MESA AVE	FOUR MILE ROAD	CORONA RANCH RD	WALNUT CANYON RD	BUCK ISLAND ROAD	BUCK ISLAND ROAD	PIPESTONE ROAD	PIPESPRING STREET	DEVILS TOWER ST	ALAMO CANYON DR	ALAMO CANYON DR	FOSTER RANCH ST	MOUNTAINTOP DR	DEFERRAL EXHIBIT 'B'. IDE OF BUCK ISLAND RO/
Type of Improvement		ONSITE PUBLIC ROADWAY IMPROVEMENTS	ARTERIAL PAVING W/PCC CURB & GUTTER AND PCC 6' WIDE SIDEWALK ON SOUTH SIDE ONLY	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON NORTH SIDE ONLY	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON NORTH SIDE ONLY"	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	SIDEWALK OF THE PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES"	RESIDENTIAL PAVING WI PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	RESIDENTIAL PAVING W/PCC CURB & GUTTER AND PCC 4' WIDE SIDEWALK ON BOTH SIDES*	SIDEWALKS TO BE DEFERRED PER DEFERRAL EXHIBIT 'B'. WAIVER OF SIDEWALK ON SOUTH SIDE OF BUCK ISLAND ROAD STUB STREET LIGHTS AS PER COA DPM
Size		ONSITE PUBLIC	30' EOA-F	24' EOA-F	28' F-F	28° F-F	28' F-F	24' F-F	28' F-F	28' F-F	28' F-F	28' F-F	48' F-F	28' F-F	28' F-F	28' F-F	
COA DRC	C TIM	Z IINO - NOISIAIGAO															
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City Cnst Engineer							
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City Inspector					-		
Private Inspector	-						
Ť,		PIPESPRING STREET	CORONA RANCH ROAD	PHASE BOUNDARY			IFICATION OF THE APPROVED GRADING PLAN IS REQUIRED NCIAL GUARANTEES. FINANCIAL GUARANTEE OR SIA UNTIL AGREEMENT IS PROCESSED AND APPROVED ON OF THE AMOLE ARROYO IMPROVEMENTS.
From		WEST BOUNDARY	PUBLIC EASEMENT	PIPESPRING STREET	E EASEMENT	E EASEMENT	ED GRADING PLAN IS REQ SIA UNTIL AGREEMENT IS IMPROVEMENTS.
Location		PUBLIC EASEMENT	PIPESPRING STREET	CORONA RANCH RD	150' AMAFCA DRAINAGE EASEMENT	150' AMAFCA DRAINAGE EASEMENT	IFICATION OF THE APPROVED GRADING PLAN IS REQUIRED NCIAL GUARANTEES. FINANCIAL GUARANTEE OR SIA UNTIL AGREEMENT IS PROCION OF THE AMOLE ARROYO IMPROVEMENTS.
Type of improvement	ONSITE PUBLIC STORM DRAIN IMPROVEMENTS	RCP W/ NEC. MH'S, LATERALS & INLETS	RCP W/ NEC. MH'S, LATERALS & INLETS	RCP W/ NEC. MH'S, LATERALS & INLETS	1.6 ACRE-FEET TEMPORARY RETENTION POND WITH PUBLIC EASEMENT AND COVENANT AND AGREEMENT	1.0 ACRE-FEET TEMPORARY RETENTION POND WITH PUBLIC EASEMENT AND COVENANT AND AGREEMENT	NOTE: A GRADING AND DRAINAGE CERTIFICATION OF THE APPROVED GRADING PLAN PRIOR TO THE RELEASE OF FINANCIAL GUARANTEES. THERE WILL BE NO RELEASE OF FINANCIAL GUARANTEE OR SIA UNTIL AGREEP WITH AMAFCA FOR CONSTRUCTION OF THE AMOLE ARROYO IMPROVEMENTS.
Size	ONSITE PUBLIC	18"-24" DIA	18"-24" DIA	18"-24" DIA			NOTE
COA DRC Project #	SIERRA RANCH SUBDIVISION - UNIT 2						
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City Inspector		,																
Private Inspector		1		1			,											
<b>2</b>			EAST BOUNDARY	PIPESTONE ROAD	PIPESTONE ROAD	PIPESTONE ROAD	GIBSON BLVD. AT CHACO CANYON DRIVE	EAST BOUNDARY	WALNUT CANYON ROAD	FOSTER RANCH ST.	PIPESTONE ROAD	ALAMO CANYON DRIVE	AMOLE MESA AVENUE	EAST BOUNDARY				
From			PIPESPRING STREET	PIPESPRING STREET	PIPESPRING STREET	WEST STUB TERMINUS	PIPESPRING STREET	FOUR MILE ROAD	WALNUT CANYON RD	BUCK ISLAND ROAD	DELGADO NIT 16	FOSTER RANCH ST.	FOUR MILE ROAD	DEVILS TOWER ST.	WALNUT CANYON RD.	DEVILS TOWER ST.	PIPESTONE ROAD	WEST BOUNDARY
Location			FOUR MILE ROAD	CORONA RANCH RD	WALNUT CANYON RD	BUCK ISLAND ROAD	PIPESTONE ROAD	PIPESPRING STREET	DEVILS TOWER ST	MOUNTAINTOP DR	PUBLIC EASEMENT IN DELC EL RANCHO GRANDE UNIT 16	FOUR MILE ROAD	FOSTER RANCH ST.	WALNUT CANYON RD.	DEVILS TOWER ST.	PIPESTONE ROAD	ALAMO CANYON DR.	AMOLE MESA AVE
Type of Improvement		ONSITE PUBLIC WATERLINE IMPROVEMENTS	WATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S	WATERLINE W/ NEC. VALVES FH'S. MJ'S & RJ'S	WATERLINE W/ NEC. VALVES FH'S. MJ'S & RJ'S	WATERLINE W/ NEC. VALVES FH's, MJ'S & RJ'S	WATERLINE W/ NEC. VALVES FH'S M.I'S & RJ'S	MATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S										
Size		ONSITE PUBLIC	8" DIA	6" DIA	6" DIA	4-6" DIA	6-8" DIA	8" DIA	6" DIA	6" DIA	20" DIA	18" DIA	18" DIA	18" DIA	18" DIA	18" DIA	18" DIA	12-18" DIA
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