CITY OF ALBUQUERQUE

PLANNING DEPARTMENT - Development Review Services

August 3, 2016

Doug Hughes, P.E.

Mark Goodwin & Associates, P.A.
P.O. Box 90606

Albuquerque, NM 87199



Richard J. Berry, Mayor

RE: Desert Sands Subdivision

Drainage Report, and Grading and Drainage Plan Engineer's Stamp Date 4-27-2016 (File: N09D014)

Dear Mr. Hughes:

Based upon the information provided in your submittal received 6-6-16, the above referenced submittals cannot be approved for Preliminary Plat action by the DRB until the following comments are addressed.

- 1. Retention pond was designed for the 100 yr-10 day storm; however, show the 100-yr 10-day storm volume on Sheet 5 (Volume shown is for the 6-hr storm). Similarly on Sheet 2, Section D-D, volume shown is for the 6-hr storm. What storm is used for the elevation shown the 10day or 6 hr? Label as Max WSEL and indicate the storm. See DPM for freeboard requirements.
- 2. The Offsite First Flush/Water Quality Pond presents some erosion concerns, especially due to the velocity of the flow.
 - a. Provide Rip-Rap into the pond
 - b. An impervious weir at the discharge point appears to be needed.
 - c. Address downstream erosion of the arroyo (per the City Engineer), specific to erosion caused by the water having less sediment content. Are drop structures necessary?
- 3. Retaining wall heights along northern boundary appear to be taller than the 8ft maximum allowed per the zoning code, once the guard height is included. Coordinate with Zoning to determine if wall heights shown are acceptable.
- 4. Pipe size for SD Pipe P-5 is shown as 30" on Construction Drawings, but calculations and tables show 36" dia. pipe. Correction required on Work Order Construction drawings, and not required for approvals.
- 5. Are losses of transition structure/ junction box accurately accounted for in CivilDesign analysis? Will the program account for the 54" SD is coming into the transition structure at 90 deg., and increase the losses? Provide the program input/output to show that the shape was incorporated into the analysis.
- 6. Remove Grading Note 11 (first flush) since it no longer applies.
- 7. Lots 1 & 2 of Block 1 require a retaining wall since drop is greater than 2ft.
- 8. Account for the upstream flows in Colobel. Flow can be found in Drainage Report for Anderson Heights.
- 9. Section Cuts on Sheet 2 show slopes can be up to 2:1. Slope protection is required. DPM Committee has determined new slope protection requirements for updated DPM and can be provided to you if you are interested in using them.

PO Box 1293

Albuquerque

New Mexico 87103

www.cabq.gov

PLANNING DEPARTMENT - Development Review Services

- 10. A approved ESC plan is required prior to approval for grading (or ESC permit)
- 11. Typ. Lot Detail w/ Sideyard wall: plan view shows street slope w/ 4% max, but section states 7.2% max. Typo? Also, provide the relative spot elev. at the front right corner of the lot.
- 12. Section H-H, Sht. 2, shows that SW culverts have reverse flow. Indicate so with a note. On construction drawings a note should state that the lip shown on the standard drawing is to be omitted (due to the reversal of flow). Show Flowline Elev. on both ends of the culverts. Also, multiple culverts in a series have been discouraged due to failures. Can the number of culverts be reduced?
- 13. Lot 1-Block 8, Sht. 1: It is still not clear how the lot will discharge. Response did not seem to address my comment. Low point elev. 36.50 is at NW corner of lot at end of the retaining wall. If you provide a screen wall around the corner and no wall openings, ponding will occur within the lot. If you install wall openings, or if there is no screen wall, it will discharge thru the curb ramp, which is not acceptable.
- 14. Addressing response to comment e. of previous letter: Hydrology will accept flows running along a sidewall, but it is discouraged. The wall could be raised another 0.5' and still not be considered a retaining wall. This would allow a swale without increasing the slope away from the house, and a positive slope in the swale would not cause ponding. This is a recommendation only, based on performance of the wall.
- 15. Addressing your response to comment j. and l. of previous letter: The Revision to Std Drwg 2405A and 2405B, Landscape Buffer Swale detail, shows that erosion protection is to be used. If the slope is high, then larger size cobble should be called out. This Revision is to be used on all major streets, as well as on streets within the subdivision. Since it is part of the Std. Dwg., it is not optional, and must be shown as a detail on the Grading plans.
- 16. Addressing your response to comment k. of previous letter: My comment was intended to state that the runoff from the tract will flow into the Landscape Buffer, which is not optional, (rather than the curb and gutter) and then will need to be directed into the Retention Pond somehow. I was suggesting that it be collected at the SW Culverts where they cross the Landscape Buffer. This may also reduce the number of culverts. If this is not possible, then the flows in the landscape buffer will overflow into the street and into the SW culverts.
- 17. Addressing your response to comment p. of previous letter: It is understood that project is phased, but will be completely graded at once. Show the boundary between Phase 1 and Phase 2. It is the heavy dashed line? If so, define in legend. Also state in the Grading Notes that Phase 2 is to be temporarily stabilized with a spray on stabilizer.
- 18. Sheet 4: Provide Contours At SW corner of subdivision. Provide T.O.Wall and B.O.Wall elevations along the retaining wall up to the end of Farinosa Ave. Verify that the retaining wall extends far enough south.

If you have any questions, you can contact me at 924-3695.

Sincerely,
Letter 1. H

Rita Harmon, P.E.

Senior Engineer, Hydrology

Planning Department

CC: Addressee via Email



City of Albuquerque

Planning Department

Development & Building Services Division

DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 09/2015)

Project Title:	Building Permit #: City Drainage #:
DRB#: EPC#:	
Legal Description:	
City Address:	
Engineering Firm:	Contact:
Address:	
Phone#: Fax#:	E-mail:
Owner:	Contact:
Address:	
Phone#: Fax#:	
Architect:	Contact:
Address:	
Phone#: Fax#:	E-mail:
Other Contact:	Contact:
Address:	
Phone#: Fax#:	E-mail:
DEPARTMENT: HYDROLOGY/ DRAINAGE TRAFFIC/ TRANSPORTATION MS4/ EROSION & SEDIMENT CONTROL	CHECK TYPE OF APPROVAL/ACCEPTANCE SOUGHT: BUILDING PERMIT APPROVAL CERTIFICATE OF OCCUPANCY
	32.11.16.112 61 6666111161
TYPE OF SUBMITTAL: ENGINEER/ ARCHITECT CERTIFICATION	PRELIMINARY PLAT APPROVAL
ENGINEER/ ARCHITECT CERTIFICATION	SITE PLAN FOR SUB'D APPROVAL
CONCEPTUAL G & D PLAN	SITE PLAN FOR BLDG. PERMIT APPROVAL
GRADING PLAN	FINAL PLAT APPROVAL SIA/ RELEASE OF FINANCIAL GUARANTEE
DRAINAGE MASTER PLAN	FOUNDATION PERMIT APPROVAL
DRAINAGE REPORT	GRADING PERMIT APPROVAL
CLOMR/LOMR	SO-19 APPROVAL
	PAVING PERMIT APPROVAL
TRAFFIC CIRCULATION LAYOUT (TCL)	GRADING/ PAD CERTIFICATION
TRAFFIC IMPACT STUDY (TIS)	WORK ORDER APPROVAL
EROSION & SEDIMENT CONTROL PLAN (ESC)	CLOMR/LOMR
OTHER (SPECIFY)	PRE-DESIGN MEETING
	OTHER (SPECIFY)
IS THIS A RESUBMITTAL?: Yes No	
DATE SUBMITTED:By:	
•	

COA STAFF: ELECTRONIC SUBMITTAL RECEIVED: ____

~ 2012 ACEC/NM Award Winner for Engineering Excellence ~ ~ 2008 ACEC/NM Award Winner for Engineering Excellence ~

July 5, 2016

Ms. Rita Harmon
Hydrology Department
City of Albuquerque
600 2nd Street
Albuquerque, NM

Re: Desert Sands Response to Drainage Report Comments

File Number N09D014

Dear Ms. Harmon,

We have revised the Drainage report and Grading Plan to address the comments made in your letter dated June 15, 2016. Please see a description of how each comment has been addressed in red below.

- 1. Per DPM 22-5.1, retention ponds must be designed for the 100 yr-10 day storm, as opposed to 2x 100 yr -6 hr storm (pg 11 of report). Provide calculations quantifying the required volume. Page 11 has been revised to include the 100 year 10 day volume for Basin 120.
- 2. Quantify the first flush volumes and show that the correct volume has been provided. Storm Water Quality, SWQ, volume calculations have been added to page 16 of the Drainage Analysis Report.
- 3. As discussed and offsite ponding area is intended. Provide the pond grading on the G&D Plan set, which is to be certified as part of the Engineer's Certification. The SWQ pond grading has been added to Sheet 3 of the G&D plan, and volume calculations are on page 16 of the drainage report.
- 4. Provide Street Slopes on the Grading Plan. Street slopes have been added to the G&D plan.
- 5. Provide a full size sheet of the Basin Map, showing legible street slopes. Basin map has been added as sheet 5 of the G&D Plan and street slope lettering height has been increased so that it is also legible on the half size plan in the report (p18).
- 6. NMDOT inlets cannot be used unless approved by DMD and City Engineer- use Single A with Dbl. wings in sump. Provide calculations. For single grate, use area of 3.84SF for orifice equation, and length of 10.8 ft for weir. For weir calculations, can use both wings. The NMDOT inlets have been replaced by COA Type Double C inlets since there is a Type A inlet less than 150' upstream of each sump. The FHA HEC-22 method of determining sump inlet flow depth has been added to the report in the table on page 12, and the hydraulic analysis report has been added to Appendix 2. Note that HEC- 22 was not used for inlets on grade because it does not calculate the street flow depth correctly. The nomographs in

appendix 2 have been made more legible in the revised report and the nomographs were used for inlets on grade.

- 7. 98 Street Improvements DR, based on Lands of Salazar report, estimated 137 cfs. Its close enough to the discharge you calculate, but the references should be changed especially since the 2-36" culverts across Street were based on this number. References to the 98th St Improvements Drainage Report, Lands of Salazar Drainage Management Plan, and Longford at Arrowwood Drainage Management Plan were added to the report on pages 11, 12, and 13. All of the reports agree that this site is allowed free discharge and statements to that effect have been added to pages 5, 13, and 17. This Desert Sands Drainage Report does not rely on any of these other reports to demonstrate capacity in the existing 36" culvert, but instead provides HGL calculations to demonstrate adequate capacity. Since this development will be connecting a storm drain to the existing culverts (previously analyzed using culvert procedures) the culverts will be converted to a storm drain system (now analyzed using HGL calculations).
- 8. Raise the pad elevation of Lot 11-P1 to be 8.7 ft. The pad elevation of Lot 11 Block 4 has been raised to 09.2 on sheet 3 of the G&D plan. The grade of Sacate Blanco Ave was raised about half of a foot at the low spot to get it above the HGL there. The Sump inlet table on page 15 has been revised accordingly.
- 9. Move inlets 1 and 2 further upstream so that EGL is lowered. Two inlets (17 and 18) were added upstream of inlets #1 and 2 on the G&D Plan sheets 3, 4, & 5. The Hydrology and Surface Drainage Table on page 14 was updated to reflect the addition of the two new inlets and the Storm Drain Pipe Summary was updated with the new flows intercepted by each inlet.
- 10. On the Civildesign output, handwrite in the sidebar the inlet # and grate el next to the corresponding station. Do the same for MHs and Rim El. (the construction plans are too small to compare the HGL). Also, label the output so that it corresponds to the construction drawing, ie. Sacate Blanco. Inlets and MHs have been hand labled on the WSPGW output along with the elevations. Full size copies of the construction plans are being provided along with the Drainage Report and Grading Plan and better quality half size copies have been provided in the report.
- 11. Provide a conceptual detail of the Transition structure in the report that is from the 54" SD to the 2 36" pipe culverts. How were losses accounted for in Civildesign? A detail of the structure has been added to sheet 3 of the G&D Plan. WSPGW (AKA Civildesign) software uses the equations in the DPM to calculate this transition and all of the other losses. WSPGW is the only software that I know of that actually uses the momentum equation to calculate junction losses in closed conduits per DPM Section 22.3.B.2.d (3). It is one of the few programs accepted by FEMA for Hydraulic calculations in closed conduits (see https://www.fema.gov/hydraulic-numerical-models-meeting-minimum-requirement-national-flood-insurance-program). The City of Albuquerque should insist that all HGL calculations be done with the equations in the DPM and then WSPGW would be the only software that any engineer ever uses.

- 12. Revise the infrastructure list so that each trunk line size is a separate line item. Since more detailed information is available on the G&D Plan, an official DRB document, the infrastructure list remains as it was when originally submitted. Footnote 5 on the Infrastructure List states that final pipe sizes will be determined with DRC review of construction plans.
- 13. Add to the infrastructure list the First flush pond, along with an Agreement and Covenant. Both the first flush pond and the retention pond were added.
- 14. The SD trunk lines need to be moved so that the Curb and Gutter is outside of the trench prism. Laterals should be used to connect the inlets to a MH along the main trunk line. The trunk line has been shifted out from under the curb and gutter on Tierra Dorado Dr., and extra manholes have been added on Sacate Blanco and Francisco Ave.
- 15. An approved ESC plan is required prior to approval for grading (or ESC permit). An E&S plan will be submitted separately.
- 16. Additional Grading Plan comments: (see attached electronic mark up)
- a. Show road slopes The Basin Map has been added to the G&D Plan as sheet 5 and now shows the slopes clearly both on the full sized plan and on the half sized plan bound into the report. The Slopes have also been added to the other 4 G&D sheets.
- b. Retaining wall along southern boundary is shown right up against the existing screen walls and there may be constructability issues. Provide a section cut along the southern boundary. Section K-K has been added to sheet 3 of the G&D and note 12 has been added to sheet 1 to protect the wall on the south and the sidewalks on the west and east.
- c. Spot el= 39.46 between 60-P 1 and 59-P 1 is low. The grades have been lowered along the west edge of the project to make sure that none of the lots are within the 2WR water service zone that has a top of zone elevation of 5140.0.
- d. Provide FL EL. along Pauza Dr Elevations added to sheet 4 along Pauza Dr.
- e. Section B-B implies runoff flows along sidewall, as opposed to a parallel swale. Yes, in order maintain proper drainage away from the pad and to get drainage from the rear yard around the house and to the street the side yard slopes are necessarily too steep to grade a swale between the house and the garden wall. There is a minimum of 0.3' fall away from the house at the highest point on the swale and the swale falls another 1.1' between the high spot in the rear yard and the street, making the swale elevation 1.4' below the pad at the front corner, so the side yard slope is nearly 3:1. The geotechnical report identified collapse prone soils and prescribes foundation design for the houses based on positive drainage away from the house.

- f. Lot 1-P1: how will lot discharge? Low point seems to beat end of retaining wall. Will there be a screen wall around the corner? Runoff should not discharge should curb ramp. On lot 1 block 8 the pad is 2' higher than the grade at the top of the wall, and the wall is not intended to block or channel drainage.
- g. Provide elevations between Lots 1-P1 and 2-P1. Elevations have been added between lots 1 and 2 Block 8 on sheet 1.
- h. North of Lot I6-P1, elev along Ret. Wall is 43.09. Typo? Elevation north of lot 16 block 1 corrected to 47.77 on sheet 1.
- i. Provide Elevations north of Lot 17-P1 Elevation added to street north of lot 17 Block 1 on sheet 1.
- j. South side of Colobel, North of Lots 1 thru 16: How does the area between the Sidewalk and retaining wall drain? Provide proposed contours. It seems that the swale within the landscape buffer should be used to collect these flows. A dirt swale will be erosive at this slope, so the area is planned to sheet drain at 2% towards the street.
- k. On south side of Colobel, east of Pauza, the swale in the landscape buffer should be used. The swale should be able to discharge to the SW culvert downstream with a cut in the channel. The right of way outside of the paved roadway is planned to sheet drain into the curb and gutter at 2%. Drainage in the south side paved roadway is planned to discharge south through the sidewalk culverts into the HOA Tract south of Colobel where the 100 year ten day volume will be retained in the portion of that tract west of 98Th St so that this development will not discharge any drainage into the sump in 98th St. which seems to have been designed as a surge pond with an unknown depth of ponding in 98th St.
- I. Show the landscape buffer swale in the section cuts. If this development actually provides landscaping in the buffer, then the swale will be part of that landscape plan. Otherwise the dirt buffer will sheet drain at 2% into the roadway.
- m. Provide a section of Colobel (showing existing and proposed construction) and existing FL EL along the North side of Colobel to show that it is super-elevated, and that a Water- block is not needed at the Pauza Drive and Colobel intersection. Also, more FL. Elevations on Pauza Dr, south of Cobble should be shown. Pauza drive does not have a water block south of Colobel; instead it is designed to receive drainage from the south half of Colobel in an effort to reduce drainage to the sump in 98th St just south of the intersection of Colobel. This development is not planned to connect any new storm drains or to contribute any new drainage to the existing storm drain in 98th St at the intersection of Colobel. HGL analysis of that existing storm drain system was not included in the WHPacific Drainage Report even though that construction project added inlets at the 98th St sump that are lower than the HGL shown in the original design of the 60" RCP by Wilson & Co. Pauza drive is graded to reduce the flow in Colobel to 98th St.

o. Each lot should have a unique lot number. Many have the same number. Please note that the numbering of lots starts over in each block. The block numbers were on the previous G&D Plan and the symbol has now been added to the legend. The P1 suffix indicates narrower roadways using the DPM infrequent parking design that prescribes the minimum number of off street parking spaces required on each lot dependent on the number of bedrooms in each house.

p. Is this a phased project? if so, an interim grading plan is required for each phase, showing how the drainage for the undeveloped areas are to discharge. Yes this is a phased project with two phases, but it all going to be graded at the same time because the cut from the west half of the site will be used to fill the east half of the site. The east half, especially the north east half of the site has to be filled to a high enough elevation to make it drain to the high spot on 98th St. where the existing double 36" culverts are located at a very shallow depth under 98th St. The west side of the site has to be cut down to a low enough elevation to be served by the 2WR water zone. A verbal description of the "Phasing Plan" will be added to the preliminary Plan in accordance with the 2015 amended subdivision ordinance that allows phased subdivisions to be approved as one project rather than separate projects. The first phase will be the lower half of the development and it will receive drainage from the upstream developed basins as shown on the basin map only with significantly less drainage until Phase 2 infrastructure is constructed. The rough graded phase 2 is to be temporarily stabilized using a spray on stabilizer.

q. What is intended for Tract B? Show proposed contours. Proposed contours have been added to Tract B which is intended as a Private Park. See sheet 1.

Please feel free to contact me with any further questions.

Sincerely,

MARK GOODWIN & ASSOCIATES, PA

James D. Hughes, PE

Senior Engineer

Desert Sands Subdivision Drainage Analysis Report

Prepared For:

LGI Homes - New Mexico, LLC 9150 E. Del Camino Suite 118 Scottsdale, AZ 85258 (415) 595-4293

Prepared By:

Mark Goodwin & Associates, PA PO BOX 90606 Albuquerque, NM 87199 (505) 828-2200

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Introduction

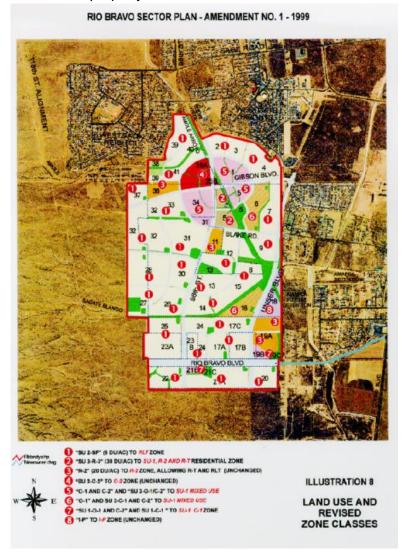
LGI Homes –New Mexico, LLC has a purchase agreement with the Lands of Salazar Trust for the purchase of Tracts A1A and A1B Lands of Salazar Family Trust containing 41.83 acres. LGI Homes wishes to develop a residential subdivision on the property, so they hired Mark Goodwin and Associates to prepare the Preliminary Plat, Grading and Drainage Plan, Drainage Report, Construction Plans, and a request for CLOMR/LOMR.

Project Scope

The Desert Sands Subdivision is a 41.83 acre residential subdivision with 216 single family detached residential lots and 31 duplex lots for a total of 247 lots. The property lies within the Rio Bravo Sector Plan

(Corporation, 1999) and is currently zoned R-LT. This development is consistent with both the current zoning and the sector plan so the next step in the development approval process is the preliminary Plat approval by the City of Albuquerque Development Review Board.

The infrastructure associated with this development consists primarily of onsite public streets with public utilities. The project includes dedication of 3 acres where the frontage streets, 98th St. and Colobel Ave., have already been granted as easements. 98th St. has already been completely constructed as a 4 lane divided arterial roadway with sidewalks and bike lanes on both sides and Colobel has already been constructed to 24' width with sidewalk on the north side. So the only remaining frontage improvement is the completion of Colobel Ave "Major Local" paving section with sidewalk on the south side.



This is a phased project with two phases, but it must be all to be graded at the same time because the cut from the west half of the site will be used to fill the east half of the site. The east half, especially the north east half of the site has to be filled to a high enough elevation to make it drain to the high spot on 98th St. where the existing double 36" culverts are located at a very shallow depth under 98th St. The west side of

the site has to be cut down to a low enough elevation to be served by the 2WR water zone. The first phase will be the lower half of the development and it will receive drainage from the upstream developed basins as shown on the basin map but with significantly less drainage until Phase 2 infrastructure is constructed. The rough graded phase 2 is to be temporarily stabilized using a spray on stabilizer.

An existing upper Zone 2WR 12" water line that crosses diagonally thru the west side of the site will have to be relocated to within the newly proposed onsite streets and an additional 12" water line will need to connect to the existing water lines in 98Th street, offsite, about 100' north and south of the site all with Phase 1. The sanitary sewer outfall is also in 98th St. about 100' south of this site.

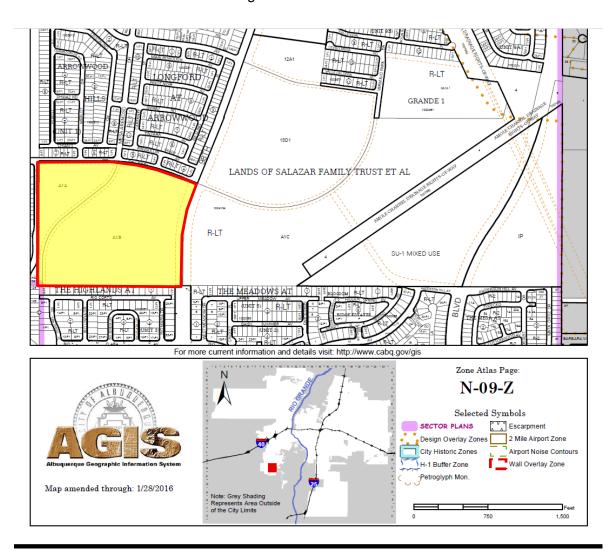
Generally speaking this site will be allowed to discharge 100 year peak flow rates in accordance with the planning history for this site. Nearly all of the onsite storm drainage will free discharge to the existing double 36" RCP culverts under 98th St. Basin 119 will flow south in 98th St and Basin 120 will be retained onsite in a pond. This development is not planned to connect any new storm drains or to contribute any new drainage to the existing storm drain in 98th St at the intersection of Colobel. Pauza drive does not have a water block south of Colobel; instead it is designed to receive drainage from the south half of Colobel in an effort to reduce drainage to the sump in 98th St just south of the intersection of Colobel. An offsite Storm Water Quality pond will be located east of 98Th Street to treat the first flush from the portion of the site that drains to the existing double 36" RCP culverts.

Purpose

The purpose of this Drainage Analysis Report is to fulfill the City of Albuquerque Development Process Manual (Albuquerque, 2008), DPM, requirements as administered by the Hydrology Section Development and Building Services Division the Planning Department of the City of Albuquerque, and as a prerequisite to DRB approval of the Preliminary Plat and Grading Plan.

Location

The Desert Sands Subdivision is located in Southwest Albuquerque New Mexico north of Senator Dennis Chavez Blvd. and west of 98Th St. on Zone Atlas Page N-9.

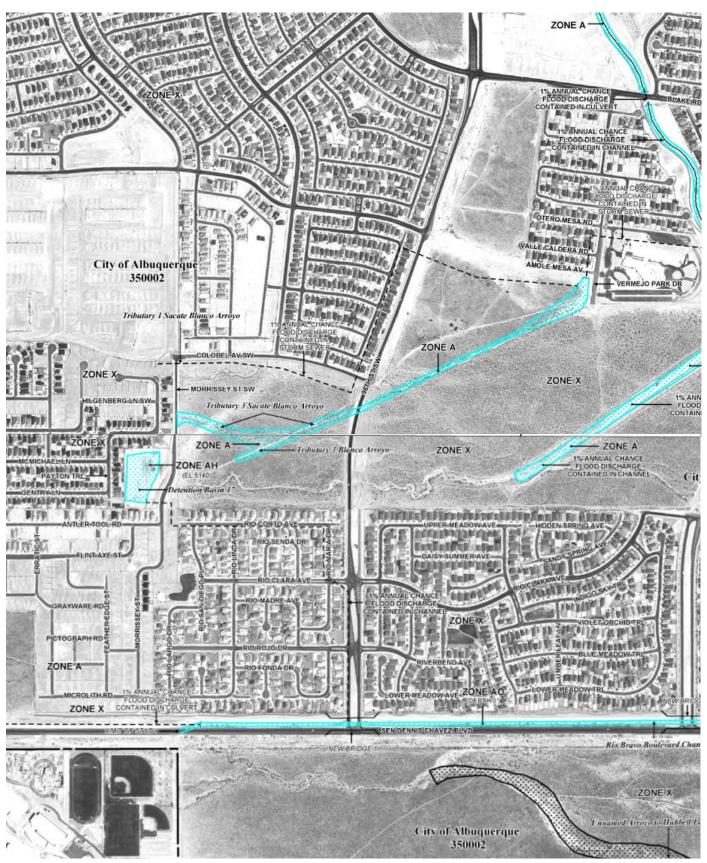


Legal Description

The legal description is Two tracts of land situated within Projected Section 4, Township 9 North Range 2 East, New Mexico Principal Meridian, Town of Atrisco Grant, City of Albuquerque, Bernalillo County New Mexico being all of Tracts A-1-A and A-1-B, Lands of Salazar Family Trust ET AL, as the same is shown and designated on said plat filed for record in the Office of the county Clerk of Bernalillo County, New Mexico on August 1, 2006 in Book 2006C, Page 237 and contains 41.8263 acres more or less.

Flood Hazard Zones

According to FEMA's Flood Insurance Rate Map, see below, Number 35001C0336H and 35001C0338H, Effective August 16, 2012, Tributary 3 of the Sacate Blanco Arroyo bisects this site from west to east.

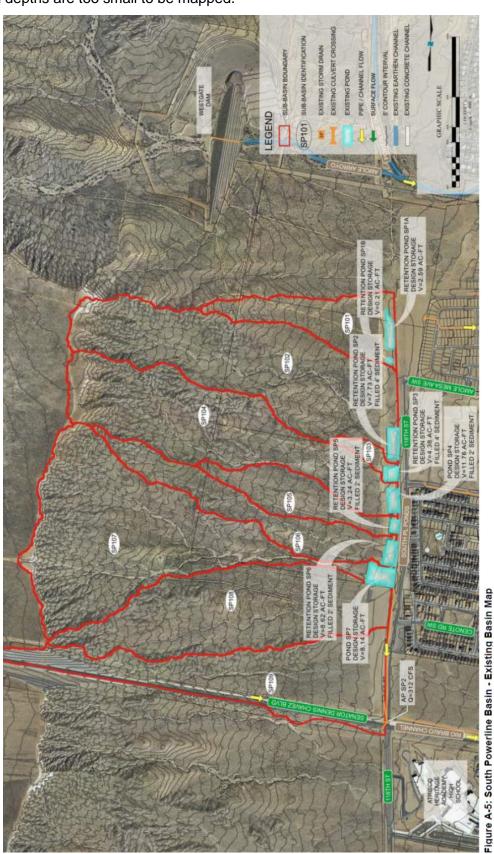


 $F: \\ 1-Projects \\ \\ 2015 \\ A15063 - Desert Sands \\ Drainage \\ \\ 2016-06-20 \ Drainage \ report. \\ docx \\ Drainage \\ A15063 - Desert Sands \\ Drainage \\ D$

However, the upstream offsite drainage basin has been diverted south to the Rio Bravo Channel see Rio Bravo Existing Basin map on page 10). So there should not be any flood plain mapped on this site since the remaining flow rates and depths are too small to be mapped.

Amole Hubble Drainage Master Plan 2013

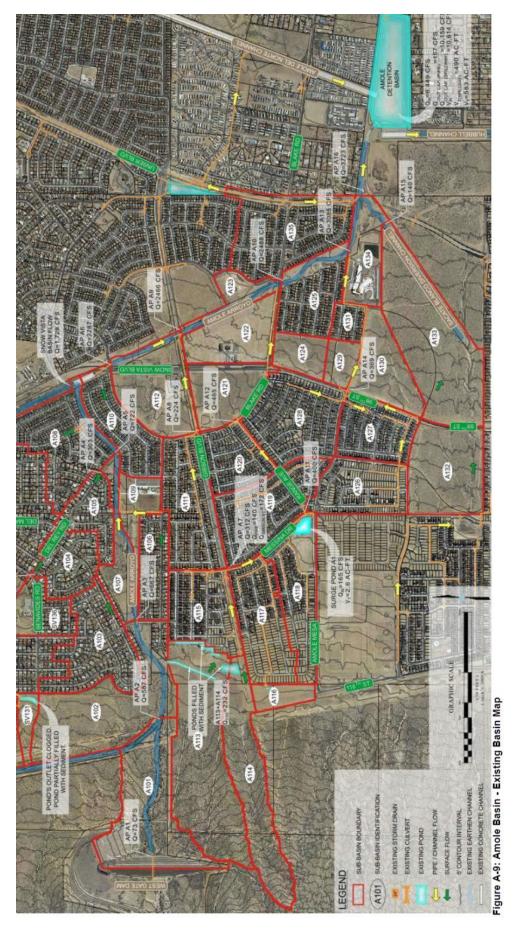
Wilson & Company Engineering prepared the Amole-Hubble Drainage Master Plan Update May 2013 Final Report (Company, 2013) for AMAFCA for the purposes of identifying and prioritizing public drainage projects within the Amole-Hubble watershed. The South Powerline Existing Basin Map (to the right) shows large offsite basins drained through this site until the South Powerline Project, as identified in the Amole Hubble Drainage master Plan diverted the drainage from these basins south to the



Rio Bravo Channel in 2005. See Rio Bravo Existing Basins Map to the right. The Anderson Heights Subdivision was developed in 2006 and diverted the rest of the upstream offsite area to the Rio Bravo Channel.

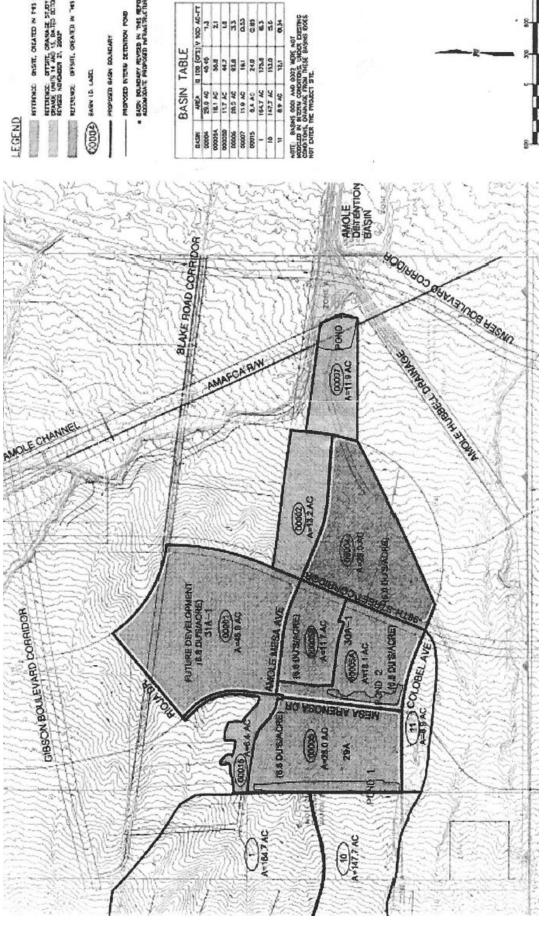


This site is shown on the Amole Existing Basin Map (to the right) as Basin A132. This site is allowed free discharge in the Master Plan hydrology calculations.



Longford at Arrowwood Drainage Management Plan 2005

The Longford at Arrowwood Drainage Management Plan (Wilson & Company, 2005) designed the 60" storm drain in 98th St. north of Colobel Ave. in 98th St. Note that Wilson's design included undeveloped flows from basins 1, 10, and 11(see basin map to the right), and note further that those offsite basins do not contribute drainage to the 60" storm drain in 98th Street any more. However the 2013 98th St Improvements designed by WHPacific added new drainage to the 60" storm drain in 98th St. that had not been planned to drain there in any of the previous reports.



Lands of Salazar Drainage Management Plan 2006

The Lands of Salazar Drainage Management Plan (Community Sciences Corporation, 2006) shows most of the Desert Sands development draining to the Sacate Blanco Arroyo. The 100 year peak flow rate of 132.28 cfs is shown at analysis point #1. AP-1 is located just downstream of 98th St. and includes drainage from basins 2 and 3 but does not include 12.69 from onsite basin 1 which is shown to contribute

to the 18.29 cfs total at AP-A at the intersection of Colobel Ave. and 98th St. This plan establishes the intent to free discharge the peak 100 year storm water runoff from developed condions from basins 2 through 7 through an onsite storm drain into the Amole Channel at Unser Blvd. (AP-4) and to replace the open channel Sacate Blanco with that storm drain. Basins 8, and 9 are also shown to drain to the Amole Channel (AP-5) but Unser Boulevard does not appear to slope in that dirrection. The lands of Salazar Family Trust owns all of this land including the **Desert Sands** Subdivision and is cooperating with LGI Homes - New Mexico, LLC, the developer of **Desert Sands** Subdivision.

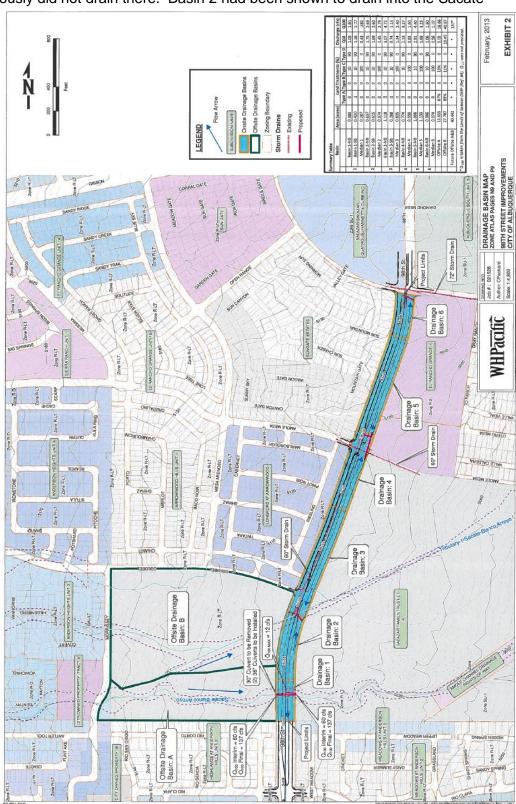


98th Street Improvements Drainage Report 2013

The 98th Street Improvements Drainage Report (WHPacific, 2013) designed 98th St from Gibson Boulevard to Dennis Chavez Boulevard does not include analysis of the 60" storm drain HGL in 98th St north of Colobel Ave even though the 98th St. Improvements project added storm inlets in the 98th Street sump with grate elevations lower than the HGL elevation that had been shown on the 60" storm drain construction plans by Wilson. The 98th St, Improvements project also added 12.8 cfs from basin 2 and the east half of basin 3 that previously did not drain there. Basin 2 had been shown to drain into the Sacate

Blanco Arroyo in the Lands of Salazar Drainage Management Plan, and the east half of basin 3 had been shown to drain east in the Longford @ Arrowwood Drainage Management Plan. WHPacific designed these basins to drain north in the 60" RCP constructed by the Longford @ Arrowwood development through inlets with grate elevations set lower than the previously calculated HGL without including revised HGL calculations in the Drainage Report for that project.

Desert Sands does not contribute any drainage to that 60" RCP that flows north in 98th St. Instead, nearly all of the onsite drainage will free discharge through the existing double 36" RCPs under 98th St in accordance with all of these referenced plans. The capacity of the double 36" RCP culvers will be changed by the construction of the upstream storm drain planned with the Desert Sands Subdivision so the capacity is documented in the Desert Sands Drainage Report rather than using the old capacity calculations in the 98th St. Improvements Drainage Report.



Hydrology

The "PROCEDURE FOR 40 ACRE AND SMALLER BASINS" is implemented in the following table per DPM Section 22.2 Part A to calculate the 100 year peak flow rates for each basin. The basins are shown on the Drainage Plan on sheet 13 of this report.

						Ну	drology	and Surfac	e Drai	nage	Sumr	nary				
			Ну	dro	olo	gy				In	let Calcs	;				
BASIN ID AREA Ground Cover (%) Peak 100-YR Flow Q ₁₀₀ (cfs)							Slope	Depth	Velocity	Energy	Inlet ID	Intercepted	By-pass			
BASIN ID	(Ac)	Α	В	С	D	Incremental	Surface	Location	Curb Type	(%)	(ft)	(fps)	(ft)	#	(cfs)	(cfs)
	, ,	T								. /	,	(, ,	. ,		, , ,	` ′
101	4.10	-	19	19	62	14.93	14.93	Sacate Blanco Ave.	Roll (4")	3.1	0.28	4.0	0.53	-	0.00	14.93
102	3.03	-	19	19	62	11.03	25.96	Sacate Blanco Ave.	Std. (8")	2.9	0.43	4.0	0.68	13 & 14	13.20	12.76
							12.76	Sacate Blanco Ave.	Std. (8")	Sump				15 & 16	12.76	
103	3.32	-	19	19		12.09	12.09	Farinosa Ave.	Roll (4")	3.6	0.26	4.0	0.51		0.00	12.09
104	1.70	-	19	19	62	6.19	18.27	Farinosa Ave.	Std. (8")	4.1	0.36	4.7	0.70	17 & 18	11.80	6.47
105	4.14	-	19	19	62	15.07	15.07	Andrews Ave.	Roll (4")	3.3	0.28	4.0	0.53	-	0.00	15.07
106	3.08	-	19	19		11.21	26.28	Pauza Drive	Std. (8")	0.5	0.54	2.8	0.66		0.00	26.28
107	1.22	-	19	19	62	4.44	37.20	Farinosa Ave.	Std. (8")	2.7	0.47	5.1	0.87	1 & 2	15.00	22.20
							22.20	Farinosa Ave.	Std. (8")	2.7	0.40	4.1	0.66	3 & 4	12.00	10.20
108	3.56	-	19	19		12.96	26.70	Bosque de Oro Dr.	Std. (8")	0.6	0.54	2.9	0.67	-	0.00	26.70
109	1.06	-	19	19	62	3.86	40.76	Farinosa Ave.	Std. (8")	0.5	0.62	3.4	0.80	5 & 6	15.00	25.76
							25.76	Farinosa Ave.	Std. (8")	Sump				7 & 8	25.76	
111	3.79	-	19	19		13.80	13.80	Artemsia Ave.	Roll (4")	3.5	0.28	4.0	0.53	•	0.00	13.80
112	1.45	-	19	19		5.28	19.08	Artemsia Ave.	Std. (8")	3.5	0.37	4.6	0.70	-	0.00	19.08
113	2.31	ŀ	19	19		8.41	27.49	Artemsia Ave.	Std. (8")	0.8	0.52	3.2	0.68	-	0.00	27.49
116	1.53	-	19	19		5.57	19.31	Artemsia Ave.	Std. (8")	0.7	0.48	2.7	0.59	-	0.00	19.31
117	2.81	-	19	19		10.23	29.54		Std. (8")	0.5	0.57	2.9	0.70	9 & 10	12.20	17.34
118	0.85	-	19	19		3.09	20.44		Std. (8")	Sump				11 & 12	20.44	0.00
119	0.81	-	19	19		2.95	15.70	Sacate Blanco Ave.	Std. (8")	1.8	0.44	4.2	0.71		2.95	12.76
120	1.23	-	0	66	34	4.16		98th St/Colobel								
						130.33									141.10	
Flow from The 100 Ye	Basin 113 ear 6 Hou	devi Ir and	ides a I 10 E	and i Day F	s spl Preci	it evenly between itation depths	en Basins 108 are 2.9" and 5	of DPM Section 22.2 and 116 .95" respectively		29, B=2.03,				120 /	0.24	ac-ft)

		Sto	rm Dra	ain Pip	e Sun	nmary				
Inlet						Pi	pe			
	INLET ID	Q ₁₀₀	Q ₁₀₀	PIPE ID	SLOPE	Diam.	Capacity	Velocity	K	Area
Location	#	cfs	cfs	#	%	in	cfs	fps		sf
Sacate Blanco Ave.	13	6.60	13.20	18	0.50	24	15.99	4.20	226.2	3.142
Sacate Blanco Ave.	14	6.60	6.60	19	0.50	18	7.42	3.74	105.00	1.767
Sacate Blanco Ave.	15	6.38	6.38	20	0.50	18	7.42	3.61	105.00	1.767
Sacate Blanco Ave.	16	6.38	25.96	21	0.50	36	47.16	3.67	666.9	7.069
Farinosa Ave.	1	7.50	7.50	1	1.00	18	10.50	4.24	105	1.767
Farinosa Ave	2	7.50	7.50	2	2.70	18	17.25	4.24	105.00	1.767
Farinosa Ave.	3	6.00	6.00	3	1.00	18	10.50	3.40	105	1.767
Farinosa Ave.	4	6.00	6.00	4	1.00	18	10.50	3.40	105	1.767
Farinosa Ave.		0.00	38.80	5	0.50	36	47.16	5.49	666.9	7.069
Farinosa Ave.	5	7.50	7.50	6	1.00	18	10.50	4.24	105	1.767
Farinosa Ave.	6	7.50	7.50	7	1.00	18	10.50	4.24	105	1.767
Farinosa Ave.			53.80	8	0.60	42	77.92	5.59	1006	9.621
Farinosa Ave.	7	12.88	12.88	9	1.00	24	22.62	4.10	226.2	3.142
Farinosa Ave.	8	12.88	12.88	10	1.00	24	22.62	4.10	226.2	3.142
Farinosa Ave.			79.56	11	0.70	42	84.17	8.27	1006	9.621
Tierra Dorando Dr.	9	6.10	6.10	12	1.00	18	10.50	3.45	105	1.767
Tierra Dorando Dr.	10	6.10	12.20	13	0.50	24	15.99	3.88	226.2	3.142
Tierra Dorando Dr.	11	10.22	10.22	14	1.20	18	11.50	5.78	105	1.767
Tierra Dorando Dr.	12	10.22	32.64	15	0.50	36	47.16	4.62	666.9	7.069
Tierra Dorando Dr.			112.20	16	0.70	54	164.57	7.05	1967	15.904
Lot 29 Esm't			138.15	17	1.00	54	196.70	8.69	1967	15.904
Ex Double 36" RCP @ 98th St.			138.15	18	2.00	36	188.63	9.77	666.9	7.069
Farinosa Ave.	17	5.90	5.90	22	1.00	18	10.50	3.34	105.00	1.767
Farinosa Ave.	18	5.90	5.90	23	1.00	18	10.50	3.34	105.00	1.767
Farinosa Ave.			11.80	24	4.10	24	45.80	3.76	226.2	3.142
Farinosa Ave.			26.80	25	2.70	24	37.17	8.53	226.2	3.142

Hydraulics

Street flow depths and velocities are summarized in the Hydrology and Surface Drainage Summary table on page 13. The depths and velocities are determined from Plate 22.3 D-1 of the DPM (see appendix). The 100 year flow depths should not exceed the top of curb and the energy grade elevation should not exceed the elevation at the street right of way which is typically 0.20' higher than the top of curb. Roll (4") curb is used in the upper portion of the watershed where flow depths are shallow, and Standard (8") curb is used in the lower portion of the watershed.

Storm drain inlets on grade are located where the street drainage capacity is exceeded and the interception rate is determined using Plate 22.3 D-5 as summarized in the table to the right. Inlet capacity at three sump locations is determined using the greatest depth as calculated from the weir and orifice equations as summarized in the following table on page 15. Each of the three sumps is designed to overflow in the event the sump inlet clogs. The overflow will pass over the crest in the street adjacent to the sump. The emergency elevation of the water is determined based on the critical depth as determined from Plate 22.3 D-1. The emergency water surface elevation is lower than the lowest adjacent pad elevation.

Storm pipes are summarized in the table on page 14. The capacities shown in that table are based on the pipe slope and Manning's normal depth for pipe flowing full. Hydraulic Grade Line elevations are determined using WSPGW software. Printouts are in the appendix and the HGL is shown on the pipe profiles also in the appendix.

This development is not planned to connect any new storm drains or to contribute any new drainage to the existing storm drain in 98th St at the intersection of Colobel.

					Sun	ıp Inlet	Summ	Sump Inlet Summary Table	e				
Inlet #	Alignment	Type	Area (SF)	Effective Perimiter (FT)	Q100 (CFS)	Orifice depth ⁽¹⁾ (FT)	wen Depth ⁽²⁾ (FT)	Top of Curb Elevation	100-YR Water Surface Elev.	Overflow Crest Elevation	Emergency Overflow Depth	Emergency Overflow Elevation	Lowest Adjacent Pad Elevation
7	Ε	Db1 'C'	17.39	10.50	12.88	0.02	0.55	5107.51	5107.52	5107.78	0.67	5108.45	5108.70
8	Э	Db1 'C'	17.39	10.50	12.88	0.02	0.55	5107.51	5107.52	5107.78	29.0	5108.45	5108.70
11	F	Db1 'C'	16.09	10.50	10.22	0.02	0.47	5107.59	5107.52	5107.78	29.0	5108.45	5108.70
12	F	Db1 'C'	16.09	10.50	10.22	0.02	0.47	5107.59	5107.52	5107.78	29.0	5108.45	5108.70
15	D	Db1 'C'	16.09	10.50	6.38	0.01	0.34	5107.74	5107.54	5107.57	0.40	5107.97	5108.70
16	D	Db1 'C'	16.09	10.50	6.38	0.01	0.34	5107.74	5107.54	5107.57	0.40	5107.97	5108.70
1)	Orifice Equa	Orifice Equa $Q = 0.6 \text{ A } (2gh)^{0.5}$	h) ^{0,2}	so I	h=(Q/.6/A) ² /2/g	<u>7/8</u>							
2)	Weir Equati $Q = 3 L h^{3/2}$	$Q = 3 L h^{3/2}$		so h	$h=(Q/3/L)^{2/3}$								
3)	The orifice e	The orifice equation is used in accordance with	d in accord	ance with FH.	A HEC-22, 8	and the heigh	nt is added to	o the center of	FHA HEC-22, and the height is added to the center of the grate elevation which is 0.72' below the top of curb elevation.	ation which is	0.72' below th	e top of curb	elevation.
4)	The weir equ	nation is used	in accordan	ce with FHA	HEC-22, and	the height i	is added to t	he lip of gutte	The weir equation is used in accordance with FHA HEC-22, and the height is added to the lip of gutter elevation which is 0.54' below the top of curb elevation.	ich is 0.54' bel	ow the top of o	turb elevation.	
2)	The Area an	d Effective Pe	rimiter are c	alculated by	"Hydraulic"	fool Box 4.2"	in accordan	ce with Federa	The Area and Effective Perimiter are calculated by "Hydraulic Tool Box 4.2" in accordance with Federal Highway Administration HEC-22 3rd eddition, Rev Aug., 2013	dministration	HEC-22 3rd ec	ddition, Rev A	ug., 2013
(9	Emergency (Emergency Overflow from inlets #7, 8, 11, & 12	n inlets #7, 8,	, 11, & 12 goes	s south in al	ignment F to	alignment I	 The total flo 	goes south in alignment F to alignment D. The total flow is 52.58 cfs and has a normal depth of 0.67 at 0.5% slope.	and has a norr	nal depth of 0.	67' at 0.5% slop	be.
7)	Emergency (Emergency Overflow from inlets #15 & 16 goes	n inlets #15 ƙ	k 16 goes east	in alignmer	nt D to 98th 9	St. The total i	flow is 12.28 c	east in alignment D to 98th St. The total flow is 12.28 cfs and has a critical depth of 0.40° at the high spot.	itical depth of	0.40' at the hig	h spot.	

Storm Water Quality Pond

The SWQ volume required by the City of Albuquerque is calculated as 0.34" depth over the area of impervious surfaces. The onsite area that drains to the culvers under 98th St. is 38.76 acres with 62% impervious cover, so the impervious area is:

 $0.62 \times 38.76 = 24.03$ acres.

The required SWQ volume is:

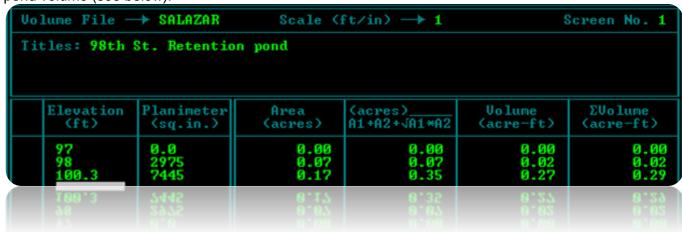
0.34"/12(in/ft) x 24.03 ac = 0.68 ac-ft (or 29,657 cf)

The SWQ pond is to be located east of 98th St. just downstream of the existing double 36" culverts. The pond will be excavated below the elevation of the bed of the arroyo so that overflow will continue down the arroyo at the existing arroyo grade. The downstream arroyo will act as the spillway and there will not be a dam (dam height = 0.0'). The effective volume has a 90' x 90' square top, is 7.5' deep 3:1 sides, leaving a 40' x 40' square bottom.

Vo	lume File —	→ DESERT2	Scale (ft/in> → 1	9	Screen No. 1
Ti	tles: Deser	t Sands Subd	ivision tempo	orary offsite	pon east of S	98th St.
	Elevation (ft)	Planimeter (sq.in.)	Area (acres)	(acres) A1+A2+\A1*A2	Volume (acre-ft)	ΣVolume (acre-ft)
	5080 5087.5	1600 8100	0.04 0.19	0.00 0.31	0.00 0.76	0.00 0.76
	5087.5	8100	0.19	0.31	9.76	0.76

Basin 120 Retention Pond Volume

The retention pond in the northeast corner of the project will be located on the HOA Tract G and will receive drainage from the south half of the public right of way of Colobel Ave between 98th St. and Pauza Dr. So a maintenance agreement and covenant will need to be provided to the City of Albuquerque to insure that the HOA will maintain the retention pond. The volume provided in the pond is greater than the 100 year 10 day runoff volume of 0.24 acre feet. The conic section method is used to calculate the actual pond volume (see below).



Summary

This site will free discharge developed 100 year peak flow rates through the existing double 36" RCP culvert under 98th St. in accordance with all of the history of drainage design and analysis for this basin. Onsite runoff will be conveyed in public streets and storm drains to the discharge point in accordance with the City of Albuquerque design standards as established in the DPM. A Storm Water Quality pond will be located east of 98th St. to serve this development. See the Grading and Drainage Plan for details. Basin 119 will flow south in 98th St and Basin 120 will be retained onsite in a pond.

Drainage Plan

Insert map instead of this page.

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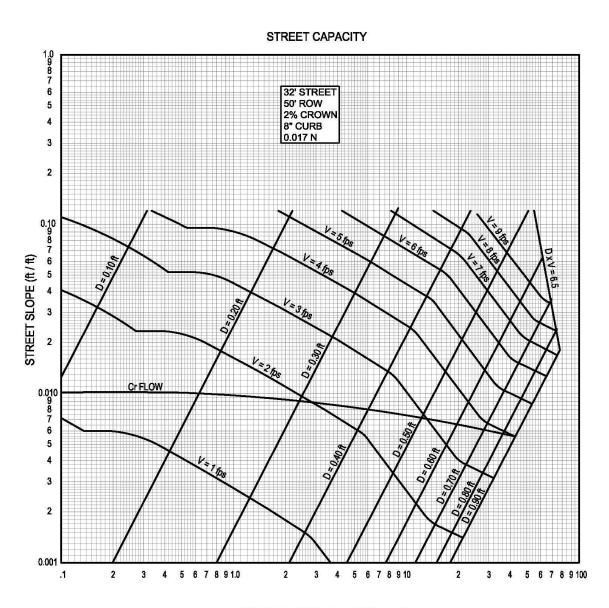
Appendix 1 – Amole-Hubble AHYMO

COMMAND I	RYDROGRAPH DENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAE DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	
DIVIDE HYD	SV136DIV1 SV136DIV2		3	0.02482	48.04	1.884	1.42357	1.567 1.567	3.025		
ROUTE MCUNGE ADD HYD	SV236SUM1RT SV237SUMA	3	1	0.02482	47.96 210.99	1,884	1,42375	1.600		CCODE =	0,2
COMPUTE NM HYD	SV237 SV237SUMB	-	2	0.03272	77,17 284,73	2 007	1.65779	1,533	3.685	PER IMP=	45,85
*S ADSV12						100				CCODE =	0.1
ROUTE MCUNGE COMPUTE NM HYD ADD HYD	5V240 SV240SDM	26.1	1	0.04727	201 88	11.237 4.036 15.273	1.60089	1.533	3.619	PER IMP=	42.00
*S APSV13 ROUTE MCUNGE	5VZ40sumRT			0.17836	385.67	15-278 3-552 18-830	1.60614	1.567		CCODE =	0.2
COMPUTE NM HYD	5V241 SV241SUM	-	1	0.04160	96.36 475.43	3.552	1.60089	1.533		PER IMP-	
*S APSV14 ROUTE MCUNGE	SV241SUMRT	1	2	0.21996 1.40835		18 829			3.376	CCODE =	0.2
ADD HYD VS APSV15	SV243SUMA	106 2	10	1.40835	475.19 1295.82		1,66432	1.667	1.438		
*S APSV16				0.08119	180.79	8.674		1.567		PER IMP=	
COMPUTE NM HYD		-	1	0.08119 0.02884	180.38 80.26	8.668 3.430 12.098	2.00188	1,500	3.471 4.348	CCODE = PER IMP=	0.2
ADD HYD *S APSV17				0.11003							
ROUTE MCUNGE ADD HYD	SV243SUMC	106 2	2	0.11003	246.02 1514.48 63.15 1558.48	12.091 137.101 2.603	2.06042 1.69302	1,600	1.558	CCODE =	0.2
COMPUTE NM HYD ADD HYD +S APSVI8	5VZ44	18 2	2	0.02736	63,15 1558,48	2.603	1.78376	1,533	3.607 1.575	PER IMP=	54.35
DOUTE MCUNGE	SVRASTN	1	47	1.54574	1558:48	139.704	1.69463	1.633	1.575	CCODE =	0.0
*2****** EMI	OF SNOW VIST	A RASTE									
*5**********	*********	******	******		************						
*S****** AMC	LE BASIN			*******		*********					
*S RECALL HYD E	elow From ORI	GINAL D	MP AHY	(O Files unde	r						
*S Folder EX Am *S Offsite flow	ole Hubbell B	asins B	Tile WGI	EXIST.PUN							
*S RECALL HYD	WGDAM		70	18.68360	73.15	167,311	0.16791	11,250	0.006		
*S *S END of RECAL	L HYD										
*S ROUTE MCUNGE	PLBASINRT	46	2	1,23801	287.41	76.085	1.15232	3.100	0.363	CCODE =	0,0
DIVIDE HYD	ADIVSUMA ADIVSUMB	70 and	1	18.67907	73.00 0.15	0.041	0.16791	9.150 11.250	0.006		
ROUTE MCUNGE	ADIVSUMART		3	18.67907	73.00	167-271	0.16791	9.150		CCODE =	0.0
ADD HYD	A2015UNA	34 2	1	19.91708	352.16	243.188	0.22894	3.100	0.028		
	HYDROGRAPH	FROM ID		AREA	PEAK DISCHARGE	RUNOFF	RUNOFF	TIME TO PEAK	CFS PER	PAGE =	12
	DENTIFICATION	ID NO.	NO.	(SQ MI)	DISCHARGE (CFS)	VOLUME (AC-FT)	(INCHES)	PEAK (HOURS)	PER ACRE	PAGE -	
COMPUTE NM HYD ADD HYD	DENTIFICATION	ID NO.	NO.	(SQ MI)	DISCHARGE (CFS)	VOLUME	(INCHES)	PEAK (HOURS)	PER ACRE	NOTATI	004
COMPUTE NM HYD ADD HYD *S APA2 ROUTE MCUNGE	DENTIFICATION A201 A201SUMB A201SUMBRE	ID NO. - 16 2	ID NO. 2 1	(SQ MI) 0.07236 19.98944 19.98944	DISCHARGE (CFS) 122.09 353.26	VOLUME (AC-FT) 4.373 247.561	(INCHES) 1,13307 0,23221 0,23221	PEAK (HOURS) 1.533 3.100	PER ACRE 2.636 0.028	NOTATI PER IMP=	ON 21-72 0.0
COMPUTE NM HYD ADD HYD *S APA2 ROUTE MCUNGE COMPUTE NM HYD COMPUTE NM HYD	A201 A201SUMB A201SUMBRL SV229 SV230	10 NO.	ID NO. 2 1	(SQ MI) 0.07236 19.98944 19.98944 0.02916 0.01824	DISCHARGE (CFS) 122.09 353.26 353.26 69.85 45.29	VOLUME (AC-FT) 4.373 247.561 247.561 2.652 1.774	(INCHES) 1,13307 0,23221 0,23221 1,70546 1,82355	PEAK (HOURS) 1.533 3.100 3.100 1.533 1.533	PER ACRE 2.636 0.028 0.028 3.743 3.880	NOTATI PER IMP= CCODE = PER IMP= PER IMP=	ON 21-72 0.0
COMPUTE NM HYD ADD HYD *S APAZ ROUTE MCUNGE COMPUTE NM HYD COMPUTE NM HYD ADD HYD ROUTE RESERVOIR	A201 A201SUMB A201SUMBRL SV229 SV230 SV230SUM PondSV10	10 NO.	ID NO. 2 1	(SQ MI) 0.07236 19.98944 19.98944 0.02916 0.01824	DISCHARGE (CFS) 122.09 353.26 353.26 69.85 45.29	VOLUME (AC-FT) 4.373 247.561 247.561 2.652 1.774	(INCHES) 1.13307 0.23221 0.23221 1.70546 1.82355 1.75089 1.75089	PEAK (HOURS) 1.533 3.100 3.100 1.533 1.533 1.533	PER ACRE 2.636 0.028 0.028 3.743 3.880 3.795 1.815	NOTATI PER IMP= CCODE = PER IMP= PER IMP= AC-FT=	0.0 49.00 57.00
COMPUTE NM HYD ADD HYD *S APA2 ROUTE MCUNGE COMPUTE NM HYD COMPUTE NM HYD ADD HYD	A201 A201 A201 A201 A201 BUMBRE SV229 SV230 SV23	10 NO. - 18 2 1 - 1 30	1D NO. 2 1 10 1 2 1 30	(SQ MI) 0.07236 19.98944 19.98944 0.02916 0.01824 0.04740 0.04740	DISCHARGE (CFS) 122.09 353.26 353.26 69.85 45.29 115.14 55.05	VOLUME (AC-FT) 4.373 247.561 247.561 2.652 1.774 4.426 4.419	(INCHES) 1,13307 0,23221 0,23221 1,70546 1,82355 1,75089 1,75089 1,74802	PEAK (HOURS) 1.533 3.100 3.100 1.533 1.533 1.533 1.700 1.766	PER ACRE 2.636 0.028 0.028 3.743 3.880 3.795 1.815	NOTATI PER IMP= CCODE = PER IMP= PER IMP= AC-PT=	0.0 49.00 57.00
COMPUTE NM HYD ADD HYD +5 APA2 ROUTE MCUNGE COMPUTE NM HYD ADD HYD BOUTE RESERVOIR ROUTE MCUNGE COMPUTE NM HYD ADD HYD BOUTE MCUNGE COMPUTE NM HYD ADD HYD	A201 SUMBRE SV229 SV230 SUM PondSV10 SV220 SV230 SUM PONDSV10 SV220 SUMP SV20 SUMP SV2	10 NO 16 2 1 - 14 2 1 30 - 26 1	1D NO. 2 1 10 12 1 30 1 2	(SQ MI) 0.07236 19.98944 19.98944 0.02916 0.01824 0.04740 0.04740 0.04740 0.05920	DISCHARGE (CFS) 122.09 353.26 353.26 69.85 45.29 115.14 55.05 54.85 60.67	VOLUME (AC-FT) 4.373 247.561 247.561 2.652 1.774 4.426 4.426 4.419 3.969	(INCHES) 1,13307 0,23221 0,23221 1,70546 1,82355 1,75089 1,75089 1,74802 1,25702	PEAK (HOURS) 1.533 3.100 3.100 1.533 1.533 1.533 1.700 1.766 1.733	PER ACRE 2.636 0.028 0.028 3.743 3.880 3.795 1.815 1.808 1.601	NOTATI PER IMP= CCODE = PER IMP= PER IMP= AC-PT= CCODE = PER IMP=	0.0 49.00 57.00 1.734 0.2 28.49
COMPUTE NM HYD ADD HYD 'S APAZ ROUTE MCUNGE COMPOTE NM HYD ADD HYD ROUTE PESSRWOIR ROUTE MCUNGE COMPUTE NM HYD ADD HYD ROUTE COMPUTE NM HYD ADD HYD ROUTE MCUNGE ADD HYD ROUTE MCUNGE ADD HYD	A201 A201 SUMBR SV229 SV230 SV230 SV230 SV230 SUM Ponds VIO SV230 SUMRT A202.1 SUMA A202.1 SUMA A202.1 SUMA A202.1 SUMA A202.2 SUMB A202.2	10 NO. 16 2 1 - 16 2 1 30 - 26 1 1	1D NO. 2 1 10 12 1 30 1 2	(SQ MI) 0.07236 19.98944 19.98944 0.02916 0.01824 0.04740 0.04740 0.04740 0.05920	DISCHARGE (CFS) 122.09 353.26 353.26 69.85 45.29 115.14 55.05 54.85 60.67	VOLUME (AC-FT) 4.373 247.561 247.561 2.652 1.774 4.426 4.426 4.419 3.969	(INCHES) 1,13307 0,23221 0,23221 1,70546 1,82355 1,75089 1,75089 1,74802 1,25702	PEAK (HOURS) 1.533 3.100 3.100 1.533 1.533 1.533 1.700 1.766 1.733	PER ACRE 2.636 0.028 0.028 3.743 3.880 3.795 1.815 1.808 1.601	NOTATI PER IMP= CCODE = PER IMP= PER IMP= AC-PT= CCODE = PER IMP=	0.0 49.00 57.00 1.734 0.2 28.49
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COMPUTE NM HYD ADD HYD *S APA2 ROUTE MCUNGE COMPUTE NM HYD ADD HYD ADD HYD ADD HYD ADD HYD ADD HYD ROUTE ESSENVOIR ROUTE MCUNGE ADD HYD ADD HYD ROUTE MCUNGE ADD HYD ROUTE MCUNGE ADD HYD ROUTE MCUNGE ADD HYD ROUTE MCUNGE *S APA3 ROUTE MCUNGE *S APA3 ROUTE MCUNGE *S APA4 COMPUTE NM HYD ROUTE MCUNGE *S APA4 ADD HYD COMPUTE NM HYD ROUTE MCUNGE *S APA5 ROUTE MCUNGE *S APA5 ROUTE MCUNGE COMPUTE NM HYD ADD HYD *S APA5 ROUTE MCUNGE COMPUTE NM HYD ADD HYD *S APA5 ROUTE MCUNGE COMPUTE NM HYD ADD HYD *S APA5 ROUTE MCUNGE COMPUTE NM HYD ADD HYD *S APA5 ROUTE MCUNGE COMPUTE NM HYD ADD HYD *S APA5 ROUTE MCUNGE COMPUTE NM HYD ADD HYD HYD *S APA7 ROUTE MCUNGE *SOMPUTE NM HYD ADD HYD ADD HYD *S APA7 ROUTE MCUNGE	A201 SUMB A201 SUMB A201 SUMB A201 SUMB A201 SUMB A202 SUMB A204 SUMB A205 SUMB A210 S	10 NO. 16 2 1 1 100 2 2 1 1 100 2 2 1 1 1 1 1 1 1	10 10 12 1 30 1 2 1 3 1 1 2 1 3 1 1 1 2 1 3 1 1 1 2 1 3 1 1 1 2 1 3 1 1 1 2 1 3 1 1 1 1	(SQ MI) 0,07236 19,98944 0,02916 0,01824 0,04740 0,04740 0,04740 0,05920 0,10660 0,10660 0,10660 0,10660 0,10660 0,10660 0,10660 0,0266 0,03109 0,13376 0,03420 0,03420 0,12118 0,1218	DISCHARGE (CFS) 122,09 353,26 69,85 45,29 115,14 55,05 54,85 60,67 114,85 402,82 53,58 455,77 455,75 74,47 73,94 517,33 47,91 143,75 142,23 149,27 78,99 252,56 251,47 61,77 305,30 305,28 80,961 60,01 668,78 867,19 164,52 1696,67 867,19 164,52 1696,67 87,37 887,19 164,52 1696,67 887,19 164,52 1696,67 887,19 164,52 1696,67 887,19 164,52 1696,67 887,19 164,52 1696,67 17,37 111,71 112,03 2601,00	VOLUME: (AC-FT) 4.373 247.561 247.561 247.561 247.561 247.561 2.552 1.774 4.426 4.419 1.969 8.388 8.388 255.949 1.938 257.887 257.882 2.824 260.707 1.883 5.299 5.290 1.0081 10.080 2.425 12.515 12.516 275.168 275.168 275.168 275.168 4.419 5.057 4.375 1.945 275.168 4.419 5.057 4.6.294 426.171	11NCHES) 113307 0.23221 0.23221 1.70546 1.82355 1.75089 1.75089 1.75089 1.75089 1.75089 1.75089 1.75089 1.75089 1.75089 1.75089 1.75089 1.75089 1.75089 1.75089 1.75089 1.75089 1.75089 1.75089 1.70384 0.24255 1.42270 1.60089 1.59827 1.59849 1.559827 1.60089 1.559827 1.60089 1.559849 1.55974 1.60089 1.55974 1.60089 1.70334 0.24255 1.154210 0.25382 1.55784 1.60089 1.55974 0.25382 1.55974 0.25382 0.25382 0.25382 0.25382 0.25382 0.25382 0.25382 0.25386 0.25386 0.25386 0.25386 0.25386 0.25386 0.25386 0.25386 0.25386 0.25386 0.25386 0.25386 0.25386 0.25386 0.25386 0.25387 0.35572 0.35572 0.35572 0.356300 0.356300	PAK (HOURS) 1.533 3.100 3.100 1.533 1.533 1.700 1.766 1.733 1.733 1.733 1.533 1.533 1.633 1.533 1.600 1.633 1.533 1.600 1.633 1.533 1.600 1.633 1.533 1.600 1.633 1.533 1.600	PER ACRE 2 - 636 0 - 028 3 - 743 3 - 980 3 - 743 3 - 716 0 - 035 3 - 743 3 - 716 0 - 035 3 - 743 3 - 716 0 - 040 3 - 035 3 - 743 3 - 746 0 - 040 3 - 035 3 - 743 3 - 243 3 - 244 0 - 046 3 - 220 3 - 243 3 - 244 0 - 181 0 - 180 0 - 220 3 - 216 3 - 290 0 - 185 0 - 183 3 - 978 3 - 952 3 - 9	NOTATI PER IMP= CCODE = PER IMP= AC-FT= CCODE = PER IMP= CCODE =	0N 21.72 0.0 49.00 57.00 1.734 0.2 28.49 0.0 32.70 0.1 41.50 0.2 42.00 0.1 41.50 0.2 73.00 0.1 64.24

COMMAND I	HYDROGRAPH DENTIFICATION	I ID		AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE :	
ADD HYD ADD HYD	AZ1ZSUMA AZ1ZSUME			0.12735 22.14038	328.91 2806.84	14.280 440.451	2.10246		4.036		
*S APA9 ROUTE MCUNGE COMPUTE NM HYD ROUTE MCUNGE COMPUTE NM HYD ADD HYD	A212SUMBRT A214 A214RT A215 A215SUM	1	10 1 2 1	22.14038 0.02567 0.02567 0.07926 0.10493	2796.09 61.49 61.05 191.61 233.66	440.460 2.335 2.333 7.261 9.594	0,37301 1,70546 1,70423 1,71772 1,71441	1,667 1,533 1,633 1,533 1,533	3,743	CCODE = PER IMP= CCODE = PER IMP=	0.1
+S APA10 ROUTE MCUNGE COMPUTE NM HYD ROUTE MCUNGE COMPUTE NM HYD ADD HYD ADD HYD	A215SUMRt A216 A216Rt A217 A117SUMA	1 1 34 1	2 1 3 1	0.10493 0.00913 0.00913 0.05761 0.06674 0.17167 0.17167	220.08 21.87 21.60 133.19 144.72	5.443	1.69570 1.70410 1.69876 1.50215 1.52903	1.533 1.633 1.533	3.743 3.696 3.613 3.388	CCODE = PER IMP= CCODE = PER IMP=	0.1
ADD HYD ROUTE MOUNGE COMPUTE NM HYD ADD HYD *S ****DIVIDE DIVIDE HYD	A217SUMBRt A218 A218SUMA 235 CFS throu	24 1 1 24 1 1gh 54"	pipe a	and remaining	to Surge Pond	14.600 4.429 19.029	1.63091 1.59467 1.48500 1.56772	1.633 1.533 1.600		CCODE = PER IMP=	0.2 29.70
ROUTE RESERVOIR ADD HYD *S APAI1	A218SUMC PondA1 A218SUMD	2 1630	30	0.04580 0.04580 0.22759		3.830 2.218 17.417	1,56772 0,90789 1,43493	1,600 1,800 1,766	6,607 0.010 1.615	AC-FT=	3.825
ROUTE MCUNGE COMPUTE NM HYD ADD HYD ROUTE MCUNGE COMPUTE NM HYD ADD HYD	A219 A219SUM A219SUMRt A220SUM	26 1	1 2 1	0.06433 0.29192 0.29192 0.03619 0.32811			1.82356 1.50163 1.48130 1.82035 1.51869	1.533 1.533 1.633 1.533	3.879 2.050 1.887	PER IMP= CCODE = PER IMP=	57.00
*S APA12 ROUTE MCUNGE COMPUTE NM HYD ADD HYD ROUTE MCUNGE	A220SUMRt A221 A221SUM A221SUMRt	1 26 1	2	0.32811 0.04187 0.36998 0.36998 0.04520	396.63	26.125 5.098 31.223 30.570	1,49292 2,28291 1,58232 1,54926	1.667 1.500 1.633 1.733	1,889 4,413 1,980 1,884	CCODE = PER IMP= CCODE =	0.2
COMPUTE NM HYD ADD HYD ADD HYD COMPUTE NM HYD ADD HYD *S APA13	A222 A2225UM A2235UMA A223 A2235UMB	26 1 106 1	1 2	0.04520 0.41518 22.55556 0.02061 22.57617		5.539 36.109 476.569 2,479 479.048	2.29752 1.63072 0.39616 2.25499 0.39786	1.667	1,901	PER IMP=	
ROUTE MCUNGE COMPUTE NM HYD ROUTE MCUNGE COMPUTE NM HYD ADD HYD ROUTE MCUNGE ADD HYD	A223SUMBRT A224 A224RI A225 A225SUMBRT A225SUMBRT A225SUMBRT	1 26 I	1 2 1 1 2	22.57617 0.02007 0.02007 0.04681 0.06688 0.06688 22.64305	48.08 47.67 119.33 153.28 153.16	1.826 1.824 4.782 6.606	0.39772 1.70546 1.70410 1.91545 1.85202 1.85193 0.40202	1.533 1.567 1.567	3,743 3,711 3,983 3,581	CCODE =	0.1
*S APA15 COMPUTE NM HYD ROUTE MCUNGE COMPUTE NM HYD	A226 A226Rt A227	-1	1 2 1	0.04817 0.04817 0.04342	122.90 119.56 104.57	4.929 4.909 4.474	1,91841 1,91085 1,93209		3.987 3.878	PER IMP= CCODE = PER IMP=	0.1
						4.4.7.4					
COMMAND ID	HYDROGRAPH ENTIFICATION		ID	APEA (SQ MI)	PEAK DISCHARGE	RUNOFF		TIME TO PEAK	CPS PER ACRE	PAGE =	200
COMMAND ID ADD HYD COMPUTE NM HYD ADD HYD		ID NO. 26 1	ID	(SQ MI)	PEAK DISCHARGE	RUNOFF	RUNOFF	TIME TO PEAK	CFS PER ACRE 3.771		ON.
ADD HYD COMPUTE NM HYD ADD HYD *S APA14 ROUTE MCUNGE COMPUTE NM HYD	A227sum A228 A228sum A228sumrt A228sumrt A229	ID NO. 26 1 - 16 2	ID NO. 1 2 1	(SQ MI) 0.09159 0.06983 0.16142 0.16142 0.01395	PEAK DISCHARGE (CFS) 221.03 167.59 376.88 281.42 33.43	RUNOFF	RUNOFF (INCHES) 1.92091 1.71271	TIME TO FEAR (HOURS) 1.567 1.563 1.567 1.667	CFS PER ACRE 3.771 3.750 3.648 2.724 3.744 2.678	NOTATION PER IMP=	0N 49.50 0.2
ADD HYD COMPUTE NM HYD ADD HYD *S APA14 ROUTE MCUNGE COMPUTE NM HYD	A227sum A228 A228sum A228sumrt A228sumrt A229	ID NO. 26 1 - 16 2	ID NO. 1 2 1	(SQ MI) 0.09159 0.06983 0.16142 0.16142 0.01395	PEAK DISCHARGE (CFS) 221.03 167.59 376.88 281.42 33.43	RUNOFF VOLUME (AC-FT) 9.383 6.379 15.762 14.819 1.269 16.088 4.625 20.714 1.209	RUNOFF (INCHES) 1.92091 1.71271 1.83084 1.72129 1.70546 1.72003	TIME TO FEAR (HOURS) 1.567 1.533 1.567 1.667 1.533 1.667 1.633 1.633 1.633 1.600 1.700	CPS PER ACRE 3.771 3.750 3.648 2.724 3.744 2.678 2.678 2.679 3.976 2.686	NOTATIO	0.2 49.50 49.00 0.2 49.00
ADD HYD COMPUTE NM HYD ADD HYD *S APA14 ROUTE MCUNGE COMPUTE NM HYD	A227sum A228 A228sum A228sumrt A228sumrt A229	TD NO. 26 1 - 16 2 1 - 16 2 1 106 2 1 1 106 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ID NO. 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1	(SQ MI) 0.09159 0.06983 0.16142 0.16142 0.01395	PEAK DISCHARGE (CFS) 221.03 167.59 376.88 281.42 33.43 300.52 300.11 112.97 374.61 396.03 361.65 3769.13 3365.62 171.36 166.32 245.20	RUNOFF VOLUME (AC-FT) 9.383 6.379 15.762 14.819 1.269 16.088 16.089 4.625 20.714 1.209 21.923 21.278 506.647 7.021 6.985 12.206	RUNOFF (INCHES) 1.92091 1.71271 1.83084 1.72129 1.70546 1.72003 1.72019 2.01129 1.77764 1.90795 1.78435	TIME TO PEAK (HOURS) 1.567 1.567 1.567 1.667 1.667 1.667 1.633 1.633 1.533 1.733 1.733 1.733 1.733 1.733 1.733 1.733	CPS. PER ACRE 3.771 3.750 3.648 2.724 3.744 2.677 4.094 2.679 2.686 2.453 0.257 0.230 4.096 3.976 3.976 3.976	NOTATION PER IMP= CCODE = PER IMP= CCODE = PER IMP= PER IMP=	0.2 49.50 0.2 49.00 0.2 69.80 62.80 0.2
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		PROM	TO		PEAK	RUNOFF		TIME TO	CFS	PAGE -	- 15
COMMAND I	HYDROGRAPH DENTIFICATION		ID	AREA (SQ MI)	DISCHARGE (CFS)	VOLUME (AC-FT)	RUNOFF (INCHES)	PEAK (HOURS)	PER	NOTAT	
COMPUTE NM HYD ADD HYD ROUTE MCUNGE	SA206 SA206SUM SA206SUMRT		1 1	0.04163 0.20817 0.20817	101-98 393.55 390.58	3.950 18.587 18.587	1.77927 1.67416 1.67413	1.533 1.567 1.567	2,954	PER IMP- CCODE -	54.00
*S Increased P COMPUTE NM HYD		HOW E	tended			1.962	1.92566	1.533		PER IMP=	
ROUTE MCUNGE	SA207RT	1	2	0.01910	48.62	1.961	1.92477	1.533	3.977	CCODE =	0.1
COMPUTE NM HYD ADD HYD *S APSA3	SA208 SA208SUM	28 1	1	0.03950 0.05860	106.90 155.52	4.608 6.569	2,18735	1.533	4.229	PER IMP=	81,72
ROUTE MCUNGE ADD HYD	SA208SUMRT SA213SUMA	104.2	10	0.05860	140.28 530.87	6.463 25.050	2.06785 1.76061	1.567	3.741	CCODE =	0.2
COMPUTE NM HYD ROUTE MCUNGE	SA209 SA209RT	1	1 2	0.03817 0.03817	98.39 97.29	4.701	2.30949	1.567	4.027	PER IMP= CCODE =	90,00
COMPUTE NM HYD	SA210	-	1	0.05112	131.15	5.863	2.15027	1.533	4.009	PER IMP=	91.18
ADD HYD *S APSA4	SA210SUM		1	0.08929	223.96	10.561		1.567	3.919		
ROUTE MCUNGE COMPUTE NM HYD	5A210SUMRT SA211	-	2	0.08929	222.93 49.88	10.559	2,21722 1.56858	1,567	3.492	CCODE = PER IMP=	
COMPUTE NM HYD ADD HYD	SA212 SA212SUMA	16 3	3	0.06692	145.65 192.83	6.184 8.051	1.73266	1.567	3.401	PER IMP=	50.85
ADD HYD *S APSA5	SA2125UMB	26 1	1	0.17053	415.11	18,610	1,95449	1.567	3.633		
ROUTE MCUNGE ADD HYD	SA212SUMBRT SA213SUMB	106.2	2	0.17853	410.49 938.85	18.597	1.95319	1.600	3.593	CCODE =	0.2
COMPUTE NM HYD ADD HYD	SA213 SA213SUMC	-	2	0.06061	136.03 1068.40	5.280 48.926	1.63324	1.533		PER IMP=	46.75
ROUTE RESERVOIR	PONDSA2	1	30	0.50591	412.78	48.926	1,81331	1.833		AC-FT=	19.074
*S PondSA2 is *S Runoff will	overflow on I	Arenal	Adde	d Elev. 5031'		bined					
*S Increasing		posed l	nas all	owed entire f.		ried to chann					
*S Increased t ROUTE MCUNGE	PONDSA2RT	30	10	0.50591	412.60	48,900	1.81232	1.866		CCODE =	0.1
ROUTE MCUNGE COMPUTE NM HYD	TSBASINRT SA201		1 2	4.97175 0.16721	1656-83 309-58	475.230 16.338	1.83203	1.766	0.521	CCODE = PER IMP=	0.2 58.76
ADD HYD ADD HYD	5A201SUM SA214SUMA		1	5,13896	1908.91 2305.74	491,568 540,468	1.79353	1,733	0.580		
*5 APSA6 ROUTE MCUNGE	SA214SUMART	1	2	5.64487	2305.74	540.468	1.79522	1.733		CCODE =	0.0
COMPUTE NM HYD ADD HYD	SA214 SA214SUMB	26 1	1	0.06684 5.71171	123.59	6.676 547.143	1.87267	1.633		PER IMP=	
ROUTE MCUNGE	SA214SUMBRT	1	2	5.71171	2412.65	547.143	1.79612	1.733	0.660	CCODE =	0.0
ADD HYD	SA215 SA215SUM		1	0.05396 5.76567	112.89 2490.38	5.292 552.435	1.83876	1.567	0.675	PER IMP=	
ROUTE MCUNGE COMPUTE NM HYD	SA215SUMRT SA216	1	2	5.76567 0.13141	2490.78 263.18	552.433 12.990	1.79652	1.733		CCODE = PER IMP=	0.2 59,54
ADD HYD *S APSA7	SA216SUM	26 1	1	5.89708	2701-48	565,423	1.79778	1.700	0.716		
ROUTE MCUNGE COMPUTE NM HYD	SA216SUMRT SA218	1	20	5.89708	2697-01 78-87	565.419 3.008	1.79777	1.700		CCODE = PER IMP=	50.00
COMPUTE NM HYD	SA219 SA219SUM	-	2	0.01224	29.09	1.098	1.68139	1.533		PER IMP-	
		FROM	TO		PRAK	RUNOFF		TIME TO	CFS	PAGE :	= 16
COMMAND T	HYDROGRAPH DENTIFICATION	FROM ID	ID	AREA (SO MI)	PEAK DISCHARGE	RUNOFF VOLUME	RUNOFF	TIME TO PEAK (BOURS)	CFS PER ACRY	PAGE :	
	DENTIFICATION	NO.	ID NO.	(SQ MI)	DISCHARGE (CFS)	VOLUME (AC-FT)	(INCHES)	PEAR (HOURS)	PER ACRE	NOTAT	CON
ROUTE MCUNGE *S Extended St	DENTIFICATION SA219SUMST orm System to	ID NO. 1 Avoid	ID NO. 2 Excess	(SQ MI) 0.04505 Street Flow	DISCHARGE (CFS) 107.41	VOLUME (AC-FT) 4.104	(INCHES) 1.70806	PEAR (HOURS) 1.533	PER ACRE 3,725	NOTAT:	ION 0.2
ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD	SA219SUMRT OF System to SA220 SA220SUM	NO. Avoid - 26 1	ID NO. 2 Excess 1 1	(SQ MI) 0.04505 Street Flow 0.06240 0.10745	DISCHARGE (CFS) 107,41 159.66 266.80	VOLUME (AC-FT) 4-104 7.686 11.790	(INCHES) 1.70806 2.30948 2.05732	PEAR (HOURS) 1.533 1.567 1.567	PER ACRE 3,725 3,998 3,880	NOTAT: CCODE = PER IMP=	0.2 90.00
ROUTE MCUNGE "S Extended St COMPUTE NM HYD ADD HYD ROUTE MCUNGE "S Extended St	DENTIFICATION SAZ19SUMRT OTH System to SAZ20 SAZ20SUMRT OTH SYSTEM to	ID NO. 1 Avoid - 26 1 1 Avoid	ID NG. 2 Excess 1 1 2 Excess	(SQ MI) 0.04505 Street Flow 0.06240 0.10745 0.10745 Street Flow	DISCHARGE (CFS) 107.41 159.66 266.80 232.43	VOLUME (AC-FT) 4.104 7.686 11.790 11.478	(INCHES) 1.70806 2.30948 2.05732 2.00284	PEAN (HOURS) 1.533 1.567 1.567 1.600	PER ACRE 3,725 3,998 3,880 3,380	NOTAT: CCODE = PER IMP= CCODE =	0.2 90.00 0.2
ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD	SAZ19SUMRT OFM System to SAZ20 SAZ20SUM SAZ20SUMRT	ID NO. 1 Avoid - 26 1 1 Avoid	ID NO. 2 Excess 1 1 2	(SQ MI) 0.04505 Street Flow 0.06240 0.10745 0.10745	DISCHARGE (CFS) 107,41 159.66 266.80	VOLUME (AC-FT) 4-104 7.686 11.790	(INCHES) 1.70806 2.30948 2.05732	PEAR (HOURS) 1.533 1.567 1.567	PER ACRE 3,725 3,998 3,880 3,380	NOTAT: CCODE = PER IMP=	0.2 90.00 0.2
ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD BOUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD *S APSA8 ROUTE MCUNGE	SA219SUMRT OFF System to SA220 SA220SUM SA220SUMRT OFF System to OFF System to SA221SUM SA221SUMRT	ID NO. 1 Avoid 26 1 Avoid 26 1	ID NG. 2 Excess 1 1 2 Excess 1 1	(SQ MI) 0.04505 Street Flow 0.06240 0.10745 0.10745 Street Flow 0.00802 0.11547	107.41 159.66 266.80 232.43 21.53	VOLUME (AC-FT) 4-104 7-686 11.790 11.478 0.919	(INCHES) 1.70806 2.30948 2.05732 2.00284 2.14876	PEAK (HOURS) 1.533 1.567 1.567 1.600	PER ACRE 3.725 3.998 3.880 3.380 4.195 3.380	NOTAT: CCODE = PER IMP= CCODE =	0.2 90.00 0.2
ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD *S APSA#	DENTIFICATION SA219SUMRT OFF System to SA220SUMRT OFF System to SA220SUMRT OFF System to SA221SUM SA221SUMRT OFF System to	ID NO. 1 Avoid 26 1 Avoid 26 1 Avoid	ID NO. 2 Excess 1 1 2 Encess 1 1	(SQ MI) 0.04505 Street flow 0.06240 0.10745 0.10745 Street Flow 0.00602 0.11547 0.11547 Street flow	DISCHARGE (CFS) 107.41 159.66 266.80 232.43 21.53 249.80 249.12	VOLUME (AC-FT) 4.104 7.686 11.790 11.478 0.919 12.397	(INCHES) 1.70806 2.30948 2.05732 2.00284 2.14876 2.01297 2.01230	PEAR (HOURS) 1.533 1.567 1.567 1.600 1.533 1.600	PER ACRE 3.725 3.998 3.880 3.380 4.195 3.380 3.371	NOTAT: CCODE = PER IMP= CCODE = PER IMP= CCODE =	0.2 90.00 0.2 81.10
ROUTE MCUNGE "S Extended St COMPUTE NM HYD ADD HYD ROUTE MCUNGE "S Extended St COMPUTE NM HYD ADD HYD "S APSA8 ROUTE MCUNGE "S Extended St COMPUTE NM HYD ADD HYD A	DENTIFICATION SA219SUMBT OFF System to SA220SUMBT OFF System to SA221SUMBT OFF SA221SUMBT OFF System to SA221SUMBT OFF System to	ID NO. 1 Avoid 26 1 Avoid 26 1 Avoid	ID NO. 2 Excess 1 1 2 Encess 1 1	(SQ MI) 0.04505 Street Flow 0.06240 0.10745 0.10745 Street Flow 0.0862 0.11547 0.11547 Street Flow	DISCHARGE (CFS) 107.41 159.66 266.80 232.43 21.53 249.80 249.12	VOLUME (AC-FT) 4.104 7.686 11.790 11.478 0.919 12.397	(INCHES) 1.70806 2.30948 2.05732 2.00284 2.14876 2.01297 2.01230	PEAR (HOURS) 1.533 1.567 1.567 1.600 1.533 1.600	PER ACRE 3.725 3.998 3.880 3.380 4.195 3.380 3.371	NOTAT: CCODE = PER IMP= CCODE = PER IMP= CCODE =	0.2 90.00 0.2 81.10
ROUTE MCUNGE "S Extended St COMPUTE NM HYD ADD HYD ROUTE MCUNGE "S Extended St COMPUTE NM HYD ADD HYD "S APSA6 ROUTE MCUNGE "S Extended St COMPUTE MM HYD ADD HYD "S Extended St COMPUTE NM HYD ADD HYD "S APSA9	DENTIFICATION SA219SUMBT OFF System to SA220SUM SA220SUMBT OFF System SA221 SA221SUMBT OFF SA221SUM SA221SUMBT OFF SA221SUMBT OFF SA222SUMBT	ID NO. 1 Avoid 26 1 1 Avoid 26 1 1 Avoid 26 1	ID NG. 2 Excess 1 1 2 Excess 1 1 2 2 Excess 1 1 1 2 2 Excess 1 1 1 2 2 Excess 1 10	(SQ MI) 0.04505 Street Flow 0.06240 0.10745 0.10745 Street Flow 0.00802 0.11547 Street Flow 0.05066 0.16613	DISCHARGE (CFS) 107,41 159,66 266,80 232,43 21,53 249,80 249,12 121,15 350,46	VOLUME (AC-FT) 4-104 7-686 11.790 11.478 0.919 12.397 12.393 4.876 17.269	(INCHES) 1.70806 2.30948 2.05732 2.00284 2.14876 2.01297 2.01230 1.80470 1.94899	PEAR (HOURS) 1.533 1.567 1.567 1.600 1.533 1.600 1.633	EER ACRE 3,725 3,998 3,880 3,380 4,195 3,380 3,371 3,737 3,296	NOTAT: CCODE = PER IMP= CCODE = PER IMP= CCODE = PER IMP=	0.2 90.00 0.2 81.10 0.2 56.20
ROUTE MCUNGE "S Extended St COMPUTE NM HYD ADD HYD ROUTE MCUNGE "S Extended St COMPUTE NM HYD ADD HYD "S APSA6 ROUTE MCUNGE "S Extended St COMPUTE MM HYD ADD HYD "S Extended St COMPUTE NM HYD ADD HYD "S APSA9	DENTIFICATION SA219SUMBT OFF System to SA220SUM SA220SUMBT OFF System SA221 SA221SUMBT OFF SA221SUM SA221SUMBT OFF SA221SUMBT OFF SA222SUMBT	ID NO. 1 Avoid 26 1 1 Avoid 26 1 1 Avoid 26 1	ID NG. 2 Excess 1 1 2 Excess 1 1 2 2 Excess 1 1 1 2 2 Excess 1 1 1 2 2 Excess 1 10	(SQ MI) 0.04505 Street Flow 0.06240 0.10745 0.10745 Street Flow 0.00802 0.11547 Street Flow 0.05066 0.16613	DISCHARGE (CFS) 107,41 159,66 266,80 232,43 21,53 249,80 249,12 121,15 350,46	VOLUME (AC-FT) 4-104 7-686 11.790 11.478 0.919 12.397 12.393 4.876 17.269	(INCHES) 1.70806 2.30948 2.05732 2.00284 2.14876 2.01297 2.01230 1.80470 1.94899	PEAR (HOURS) 1.533 1.567 1.567 1.600 1.533 1.600 1.633	EER ACRE 3,725 3,998 3,880 3,380 4,195 3,380 3,371 3,737 3,296	NOTAT: CCODE = PER IMP= CCODE = PER IMP= CCODE = PER IMP=	0.2 90.00 0.2 81.10 0.2 56.20
ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD *S APSAB ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD *S APSAB COMPUTE NM HYD COMPUTE NM HYD ROUTE MCUNGE COMPUTE NM HYD	DENTIFICATION \$A219SUMRT OTH System to \$A220SUMRT SA220SUMRT OTH System to \$A221SUMS \$A221SUMST OTH System to \$A221SUMST OTH System to \$A221SUMST OTH System to \$A222SUM \$A223SUM \$A223SUM \$A224SUM \$A224SUM \$A224SUM \$A224SUM \$A224SUM \$A224SUM	ID No. 26 1 26 1 Avoid 26 1 Avoid 26 1	ID NG. 2 Excess 1 1 2 Excess 1	(SQ MI) 0.04505 Street Flow 0.06240 0.10745 Street Flow 0.0802 0.11547 0.11547 0.11547 0.16613 0.07060 0.07060 0.07060 0.01720 0.09790 0.02910	DISCHARGE (CFS) 107,41 159,66 266,80 232,43 21,53 249,80 249,12 121,15 350,46 171,74 170,54 48,30 218,79	VOLUME (AC-FT) 4-104 7-686 11.790 11.478 0.919 12.397 12.393 4.876 17.289 6.866 6.863 2.074 8.937 3.052	(INCHES) 1.70806 2.30948 2.05732 2.00284 2.14876 2.01297 2.01230 1.80470 1.94899 1.82356 1.82278 2.26109 1.906638	PEAR (HOURS) 1.533 1.567 1.567 1.600 1.533 1.600 1.633 1.533 1.500 1.533 1.500 1.533 1.500	PER ACRE 3.725 3.998 3.880 3.380 4.195 3.380 3.371 3.737 3.296 3.801 3.774 4.388 3.894 4.044	NOTATION OF THE PER IMPERIAL PE	90.00 0.2 81.10 0.2 56.20 57.00 0.2 86.71 66.70
ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD *S APSAB ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD *S APSAB COMPUTE NM HYD COMPUTE NM HYD ROUTE MCUNGE COMPUTE NM HYD	DENTIFICATION \$A219SUMRT OTH System to \$A220SUMRT SA220SUMRT OTH System to \$A221SUMS \$A221SUMST OTH System to \$A221SUMST OTH System to \$A221SUMST OTH System to \$A222SUM \$A223SUM \$A223SUM \$A224SUM \$A224SUM \$A224SUM \$A224SUM \$A224SUM \$A224SUM	ID No. 26 1 26 1 Avoid 26 1 Avoid 26 1	ID NG. 2 Excess 1 1 2 Excess 1	(SQ MI) 0.04505 Street Flow 0.06240 0.10745 Street Flow 0.0802 0.11547 0.11547 0.11547 0.16613 0.07060 0.07060 0.07060 0.01720 0.09790 0.02910	DISCHARGE (CFS) 107,41 159,66 266,80 232,43 21,53 249,80 249,12 121,15 350,46 171,74 170,54 48,30 218,79	VOLUME (AC-FT) 4-104 7-686 11.790 11.478 0.919 12.397 12.393 4.876 17.289 6.866 6.863 2.074 8.937 3.052	(INCHES) 1.70806 2.30948 2.05732 2.00284 2.14876 2.01297 2.01230 1.80470 1.94899 1.82356 1.82278 2.26109 1.906638	PEAR (HOURS) 1.533 1.567 1.567 1.600 1.533 1.600 1.633 1.533 1.500 1.533 1.500 1.533 1.500	PER ACRE 3.725 3.998 3.880 3.380 4.195 3.380 3.371 3.737 3.296 3.801 3.774 4.388 3.894 4.044	NOTATION OF THE PER IMPERIAL PE	90.00 0.2 81.10 0.2 56.20 57.00 0.2 86.71 66.70
ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD *S APSAB ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD *S APSAB COMPUTE NM HYD COMPUTE NM HYD ROUTE MCUNGE COMPUTE NM HYD	DENTIFICATION \$A219SUMRT OTH System to \$A220SUMRT SA220SUMRT OTH System to \$A221SUMS \$A221SUMST OTH System to \$A221SUMST OTH System to \$A221SUMST OTH System to \$A222SUM \$A223SUM \$A223SUM \$A224SUM \$A224SUM \$A224SUM \$A224SUM \$A224SUM \$A224SUM	ID No. 26 1 26 1 Avoid 26 1 Avoid 26 1	ID NG. 2 Excess 1 1 2 Excess 1	(SQ MI) 0.04505 Street Flow 0.06240 0.10745 Street Flow 0.0802 0.11547 0.11547 0.11547 0.16613 0.07060 0.07060 0.07060 0.01720 0.09790 0.02910	DISCHARGE (CFS) 107,41 159,66 266,80 232,43 21,53 249,80 249,12 121,15 350,46 171,74 170,54 48,30 218,79	VOLUME (AC-FT) 4-104 7-686 11.790 11.478 0.919 12.397 12.393 4.876 17.289 6.866 6.863 2.074 8.937 3.052	(INCHES) 1.70806 2.30948 2.05732 2.00284 2.14876 2.01297 2.01230 1.80470 1.94899 1.82356 1.82278 2.26109 1.906638	PEAR (HOURS) 1.533 1.567 1.567 1.600 1.533 1.600 1.633 1.533 1.500 1.533 1.500 1.533 1.500	PER ACRE 3.725 3.998 3.880 3.380 4.195 3.380 3.371 3.737 3.296 3.801 3.774 4.388 3.894 4.044	NOTATION OF THE PER IMPERIAL PE	90.00 0.2 81.10 0.2 56.20 57.00 0.2 86.71 66.70
ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD *S APSA8 ROUTE MCUNGE *S Extended St COMPUTE NM HYD ADD HYD *S APSA9 COMPUTE NM HYD ROUTE MCUNGE COMPUTE NM HYD ADD HYD ADD HYD *S APSA11 *S APSA11	DENTIFICATION SA219SUMRT OTH System to SA220SUMRT OTH System to SA221SUMRT OTH System to SA221SUMRT OTH System to SA221SUMRT OTH System to SA222SA22SUM SA223SUM SA223SUM SA224SUM SA224SUM SA224SUM SA225SUMS SA225SUMRT SA226SUMA	ID No. 1 Avoid 26 1 Avoid 26 1 Avoid 26 1 1 16 2	ID NG. Excess 1 1 2 Excess 1 1 1 2 Excess 1 1 1 2 Excess 1 1 10 1 2 1 1 2 1	(SQ MI) 0.04505 Street Flow 0.06240 0.10745 Street Flow 0.0802 0.11547 0.11547 Street Flow 0.05066 0.16613 0.07060 0.07060 0.07060 0.07060 0.07060 0.01720 0.08790 0.02910 0.11690 0.11690	DISCHARGE (CFS) 107,41 159,66 266,80 232,43 21,53 249,80 249,12 121,15 350,46 171,74 170,54 48,30 218,79 75,31 294,10 294,10 628,13	VOLUME (AC-FT) 4.104 7.686 11.790 11.478 0.919 12.397 12.393 4.876 17.269 6.863 2.074 8.937 3.052 11.969 11.969 29.258	(INCHES) 1.70806 2.30948 2.05752 2.00284 2.14876 2.01280 1.80470 1.94899 1.82256 1.82278 2.26109 1.90863 1.96638 1.92300 1.93825	PEAR (HOURS) 1.533 1.567 1.600 1.533 1.600 1.633 1.533 1.500 1.533 1.533 1.533 1.533 1.533	EXR ACRE 3.725 3.998 3.880 3.380 4.195 3.380 3.371 3.737 7.296 3.801 3.774 4.388 3.894 4.094 3.931 3.931 3.931 3.468	NOTATI CCODE = PER IMP= CCODE = PER IMP= CCODE = PER IMP= CCODE = PER IMP= PER IMP= CCODE = CCODE =	0.2 90.00 0.2 81.10 0.2 56.20 57.00 0.2 86.71 66.70
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Appendix 2 – Street Capacity and Grate Capacities



ONE HALF STREET FLOWS (cfs)

GRATING CAPACITIES FOR TYPE "A", "C" AND "D"

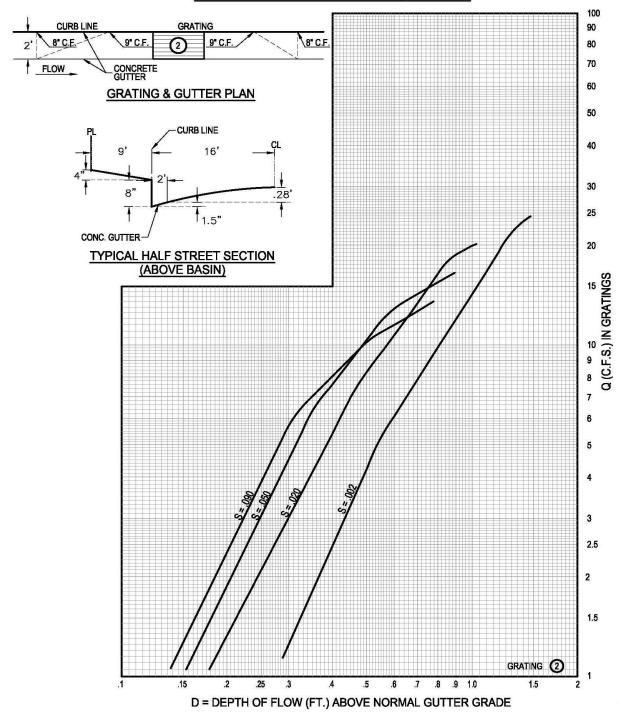


PLATE 22.3 D-5

Appendix 3 – WSPGW – HGL Calculations & Storm Profiles	

Hydraulic Analysis Report

Project Data

Project Title: Desert Sands Subdivision

Designer:

Project Date: Friday, June 17, 2016 Project Units: U.S. Customary Units

Notes:

Curb and Gutter Analysis: Inlets 7 & 8

Notes:

Gutter Input Parameters

Longitudinal Slope of Road: 0.0050 ft/ft Cross-Slope of Pavement: 0.0200 ft/ft

Depressed Gutter Geometry

Cross-Slope of Gutter: 0.0630 ft/ft

Manning's n: 0.0170 Gutter Width: 2.0000 ft Design Flow: 12.8800 cfs

Gutter Result Parameters

Width of Spread: 21.5603 ft Gutter Depression: 1.0320 in

Area of Flow: 4.7345 ft^2

Eo (Gutter Flow to Total Flow): 0.2601 Gutter Depth at Curb: 6.2065 in

Inlet Input Parameters

Inlet Location: Inlet in Sag
Percent Clogging: 0.0000 %
Inlet Type: Equal-length Combo

Grate Type: P - 1-7/8
Grate Width: 2.0000 ft
Grate Length: 6.5000 ft
Length of Inlet: 6.5000 ft

Curb opening height: 6.2500 in Local Depression: 4.2500 in

Inlet Result Parameters

Perimeter: 10.5000 ft

Effective Perimeter: 10.5000 ft

Area: 17.3875 ft^2

Effective Area: 17.3875 ft^2

Depth at center of grate: 0.5509 ft

Computed Width of Spread at Sag: 26.3948 ft

Flow type: Weir Flow

Efficiency: 1.0000

Curb and Gutter Analysis: Inlets 11 & 12

Notes:

Gutter Input Parameters

Longitudinal Slope of Road: 0.0050 ft/ft Cross-Slope of Pavement: 0.0200 ft/ft

Depressed Gutter Geometry

Cross-Slope of Gutter: 0.0630 ft/ft

Manning's n: 0.0170 Gutter Width: 2.0000 ft Design Flow: 10.2200 cfs

Gutter Result Parameters

Width of Spread: 19.7096 ft Gutter Depression: 1.0320 in

Area of Flow: 3.9707 ft^2

Eo (Gutter Flow to Total Flow): 0.2847

Gutter Depth at Curb: 5.7623 in

Inlet Input Parameters

Inlet Location: Inlet in Sag
Percent Clogging: 0.0000 %
Inlet Type: Equal-length Combo

Grate Type: P - 1-7/8 - 4
Grate Width: 2.0000 ft
Grate Length: 6.5000 ft
Length of Inlet: 6.5000 ft

Curb opening height: 6.2500 in Local Depression: 4.2500 in

Inlet Result Parameters

Perimeter: 10.5000 ft

Effective Perimeter: 10.5000 ft

Area: 16.0875 ft^2

Effective Area: 16.0875 ft^2

Depth at center of grate: 0.4722 ft

Computed Width of Spread at Sag: 22.4582 ft

Flow type: Weir Flow Efficiency: 1.0000

Curb and Gutter Analysis: Inlets 15 & 16

Notes:

Gutter Input Parameters

Longitudinal Slope of Road: 0.0200 ft/ft Cross-Slope of Pavement: 0.0200 ft/ft

Depressed Gutter Geometry

Cross-Slope of Gutter: 0.0630 ft/ft

Manning's n: 0.0170 Gutter Width: 2.0000 ft Design Flow: 6.3800 cfs

Gutter Result Parameters

Width of Spread: 12.3955 ft Gutter Depression: 1.0320 in Area of Flow: 1.6225 ft²

Eo (Gutter Flow to Total Flow): 0.4467

Gutter Depth at Curb: 4.0069 in

Inlet Input Parameters

Inlet Location: Inlet in Sag
Percent Clogging: 0.0000 %
Inlet Type: Equal-length Combo

Grate Type: P - 1-7/8 - 4 Grate Width: 2.0000 ft Grate Length: 3.0000 ft Length of Inlet: 3.0000 ft

Curb opening height: 6.2500 in Local Depression: 4.2500 in

Inlet Result Parameters

Perimeter: 7.0000 ft

Effective Perimeter: 7.0000 ft

Area: 7.4250 ft^2

Effective Area: 7.4250 ft^2

Depth at center of grate: 0.4519 ft

Computed Width of Spread at Sag: 21.4463 ft

Flow type: Weir Flow Efficiency: 1.0000

FILE: Sacate.WSW

W S P G W - CIVILDESIGN Version 14.05 Program Package Serial Number: 1454 WATER SURFACE PROFILE LISTING

Date: 6-29-2016 Time: 1:27:30

Lands of Salazar Sacate Blanco Ave. 2016-03-30

*****	************************************	******	********	******	*******	*****	********	******	*******	*******	******	******	****	*****	***
Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/ DiaFT	Base Wtlor or I.D.	ZL	No Wth Prs/Pip	Wth s/Pip
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		_				Ų.									
1000.000	5093.750	1.803	5095.553	138.16	15.57	3.76	5099.32	00.	2.65	2.94	3,000	000.	00.	2 1	0.
110.040	.0245	_ ·	<u> </u>		i <u> </u>	.0225	2.48	1.80	1.58	1.78	.013	00.	00.	PIPE	
1110.040	5096.45	1.863	1.863 5098.314	138.16	14.97	3.48	5101.80	00.	2.65	2.91	3.000	000.	00.	- 2	0.
54.960	.0245	1	1	1	1	.0202	1.11	1.86	1.48	1.78	.013	00.	00.	PIPE	
1165.000	5097.80		099.74	138.16	14.28	3.17	5102.91	00.	2.65	2.87	3.000	000.	00.	~ ~	0.
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7.625	.0032	I .	-	1	1	.0054	.04	3.46	1.00	4.50	.013	- 00.	00.	PIPE	
1178.625	5098.02	3.629	5101.65	138.16	10.0	1.57	5103.22	00.	3.46	3.56	4.500	000.	.00		0.
33.829	. 0032	1	1	<u> </u>	1	.0049	.16	3.63	- 06.	4.50	.013	- 00.	00.	PIPE	
1212.454	5098.13	3.827	5101.96	138.16	9.58	1.43	5103.39	00.	3.46	3.21	4.500	000.	00.	H	0.
-1-	-1-	ī	1	<u> </u>	1	.0045	.37	3,83	. 80	4.50	.013	00.	00.	PIPE	
1295.000	5098.40	4.058	5102.458	138.16	9.15	1.30	5103.76	4.50	3.46	2.68	4.500	000.	.00		0.
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1301.000	5098.60	7.151	5105.75	25.96	3.6	.21	5105.96	00.	1.65	00.	3.000	000.	00.	_	0
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1383.000	1383.000 5098.930	7.018	5105.948	25.96	3.67	.21	5106.16	00.	1.65	00.	3.000	000.	00.	_ H	0.
94.000	ا۔ 9000.	I	<u>1</u>	I	<u> </u> 	.0015	.14	7.02	00.	1.44	.013	00.	00.	PIPE	

Date: 6-29-2016 Time: 1:27:30

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W S P G W - CIVILDESIGN Version 14.05 Program Package Serial Number: 1454 WATER SURFACE PROFILE LISTING

Lands of Salazar Sacate Blanco Ave. 2016-03-30

* * * *	No Wth Prs/Pip	Type Ch ******	0.	r₊1	0.	r _e n	0.	r _e n	0.	ru ^a	0.
*****	No	- Type ****		- PIPE		I- PIPE	_	I = PIPE		I- PIPE	_ 1
****	ZL	ZR ****	00.	.00	00.	00.	00.	00.	00.	00.	00
*****	Base Wt or I.D.	- X-Fall ******	_ 000.	00:	000.	00.	000.	- 00.	000.	00.	000.
*******	Flow Top Height/ Bas Width DiaFT or	- ************************************	3.000	.013	2.000	.013	2.000	.013	1.500	.013	1.500
*****	Flow Top Width	- - N Norm Dp ** *****	00.	 - -	00.	1.05	00.	<u> </u>	00.	.78	001
******	Critical Depth	SE Dpth Froude N ******	1.65	00.	1.31	00.	1.31	00:	66.	00.	66.
*****	Super Elev	- SE Dpth ******	00.	6.51	00.	6.52	00.	00.	00.	6.49	00 -
**********************************	Energy Grd.El.	SF Ave	5106.30	.01	5106.48	.10	5106.65	.01	5107.00	60.	5107.15
	Vel Head	SF Ave *****	.21	.0025	.27	.0034	.27	.0037	.22	.0039	.22
*	Vel (FPS)		3.67		4.20	<u> </u>	4.20	7.	3.73		3.73
*******	Q (CFS)		25.96		13.20		13.20		6.60		09.9
*********************************	Water Elev		6.510 5106.090		6.524 5106.204		6.381 5106.381	-	6.486 5106.786		6.337 5106.937
	Depth (FT)						6.381		6.486		
*******	Invert Elev	L/Elem Ch Slope	1477.000 5099.580	UNCT STR .0250	5099.680	.0114	1509.000 5100.000		0 1	.0136	5100.600
******	Station	L/Elem ******	11477.000 H1477.000	JUNCT STR	1481.000	28.000	1509.000	JUNCT STR 0750	1513.000	22.000	1535.000 TC=510792

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Date: 6-30-2016 Time: 8: 3:41

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W S P G W - CIVILDESIGN Version 14.05 Program Package Serial Number: 1454 WATER SURFACE PROFILE LISTING

* FILE: farinosa.WSW

Lands of Salazar Farinosa Ave 2016-06-29

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Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)		Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	T	Wtl	ZI	No Wth Prs/Pip	ih ip
L/Elem Ch Slope	L/Elem Ch Slope	1 * * * * *	* * * * *	* * * * * * *	* * * * *	SF Ave	- H - ** **	N *	SE Dpth Froude N Norm	Norm Dp	********	X-Fall ******	- ZR ****	Type Ch ******	Ch * *
1000.000	5093.75	1.80	5095.55	138.16	15.57	3.76	5099.32	- 00.	2.65	2.94	3.000	000.	00.	- 2	0
110.040	.0245	1	<u> </u>		<u> </u> 	.0225	2.48	1.80	1.58	1.78	.013	- 00.	00.	PIPE	
1110.040	5096.45	1.863	5098.314	138.16	14.97	3.48	5101.80	00.	2.65	2.91	3.000	000.	00.	2	0
54.960	.0245	I	<u> </u> -	ī	<u> </u> 	.0202	1.11	1.86	1.48	1.78	.013	- 00.	00.	PIPE	
1165.000	5097.80	1.941	5099.741	138.16	14.2	3.17	5102.91	00:	2.65	2.87	3.000	000	00.	~ ~	0
TRANS STR	- -	l -	<u> </u>	ī -	<u>1.</u> 1	.0123	- 70.	1.94	1.37	1	.013	- 00.	00.	- PIPE	
7	5098.000	3.456	5101.456	138.16	10.54	1.73	5103.18	00:	3.46	3.80	4.500	000.	00.		0
7.625	.0032	1	<u> </u>			.0054	.04	3.46	1.00	4.50	.013	00.	00.	PIPE	
1178.625	5098.024	3.62	5101.65	138.16	10.05	1.57	5103.22	00.	3.46	3.56	4.500	000.	00.		0.
33.829	. 0032	<u> </u> -	<u> </u>		<u> </u>	.0049	.16	3,63	06.	4.50	.013	- 00.	00.	PIPE	
1212.454	5098.133	3.827	5101.960	138.16	9.58	1.43	5103.39	00.	3.46	3.21	4.500	000.	00.	H -	0.
82.546	. 0032	I	! -	<u> </u>	I I	.0045	.37	3,83	- 80	4.50	.013	00.	00.	PIPE	
1295.000	5098.400	4.058	5102.458	138.16	9.15	1.30	5103.76	4.50	3.46	2.68	4.500	000.	00.	_	0.
JUNCT STR	.0334		<u> </u>		<u> </u>	.0038	.02	4.50	. 68		.013	00.	00.	PIPE	
1301.000	5098.600	4.828	5103.428	112.20	7.05	77.	5104.20	00.	3.12	00.	4.500	000.	00.		0.
150.000	.0041	 I	<u> </u>		<u>t</u> L	.0033	.49	4.83	00.	3.30	.013	00.	00.	PIPE	
1451.000	5099.22	4.69	5103.91	112.20	7.0	.77.	5104.69	00.	3.12	00.	4.500	000.	00.		0.
JUNCT STR	-1- -1- -135	1	<u> </u>	Ī	1	.0048	.03	00.	00.	1	.013	00.	00.	PIPE	
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FILE: farinosa.WSW

WATER SURFACE PROFILE LISTING

Lands of Salazar Farinosa Ave 2016-06-29

0. |Prs/Pip PIPE PIPE PIPE PIPE PIPE PIPE PIPE PIPE 00. 00. ************************* 00 00 00. Energy | Super | Critical | Flow Top | Height / | Base Wt | |Dia.-FT|or I.D.| 000 00. 000 00. 000. 00. .000 000. 000 00 00. 00. 00. 000. 000 3.000 3.500 3.500 3.500 3.000 2.000 2.000 2.000 .013 .013 .013 .013 .013 |SE Dpth|Froude N|Norm Dp | | Width 00. 2.60 00. 00. 2.08 00. 00. 00. 1.61 00. 00. Elev | Depth 2.79 2.29 1.80 2.29 00. 2.03 2.03 4.58 5.39 00. 5.30 5.07 3.91 5.16 00. 00. 00. 00. 4.45 00. 00. 00. Grd.El. . 58 .03 .18 .02 . 44 .03 1.06 5104.96 5106.15 5105.54 5105.97 5106.36 5106.80 5107.28 5109.44 5110.39 1.06 .49 .49 . 47 SF Avel 1.13 . 47 1.13 0046 0029 0087 0140 Head 0063 0031 8.27 5.59 5.59 8.53 3.76 8.27 ī 5.49 5.49 8.53 (FPS) 79.56 79.56 53.80 38.80 26.80 53.80 38.80 26.80 Q (CFS) 4.583 5103.903 4.448 5104.478 5.387 5105.488 5.158 5105.668 5.295 5105.895 4.335 5106.335 5.066 5110.167 3.910 5106.151 5108.311 Depth | Water Elev 3.311 (FT) .0601 .**37** 5102.240 5100.510 5100.030 5100.100 5100.600 5099.320 5102.000 5105.000 | Invert L/Elem |Ch Slope 5105.100 .0212 .0108 .0077 .0065 .0199 .0151 .0117 Elev 1549.000 11442-1-JUNCT STR 1754.000 7 1#1 -1-1618.000 M#4 - I-1888.000 M##6-I-Station 1457.000 63.000 92.000 555.000 1624.000 130.000 130.000 12 = 510 126.000 1015 - MI INCI

Date: 6-30-2016 Time: 8: 3:41

FILE: farinosa.WSW

W S P G W - CIVILDESIGN Version 14.05 Program Package Serial Number: 1454

MATER SURFACE PROFILE LISTING

Lands of Salazar Farinosa Ave

ZL |Prs/Pip No Wth PIPE PIPE 00. Vel | Energy | Super |Critical|Flow Top|Height/|Base Wt| Head | Grd.El.| Elev | Depth | Width |Dia.-FT|or I.D.| 000. 000. .00 1.500 -1-6 .00 -1- 3.01 .01 .01 .01 .17 .110.89 .132 .22 5110.79 -|-10. 0029 .01 .17 5111.00 11.80 3.76 Q | Vel (CFS) | (FPS) 5.90 5.90 1.510 5110.830 | Invert | Depth | Water | 2016-06-29 2.965 5110.574 3.011 5110.722 Elev (FT) | El -1-2040.000 5109.320 Inlet # 7- -1-Station | Elev | 2018.000 5107.610 18.000

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FILE: Tierra.WSW

Program Package Serial Number: 1454 W S P G W - CIVILDESIGN Version 14.05

WATER SURFACE PROFILE LISTING

Salazar

Lands of

Tierra Dorado Dr.

1212.454 1178.625 1171.000 Station | 1000.000 1295.000 1451.000 150.000 82.546 33.829 54.960 7.625 |Ch Slope 5093.750 5098.000 5096.451 Invert 5098.133 5099.220 5098.600 5098.024 5097.800 5098.400 Elev .0166 .0334 .0334 .0041 .0032 .0032 .0032 .0245 .0245 1 <u>|</u> <u>|</u> 1 (FT) 4.696 4.058 Depth 4.828 3.827 3.629 3.456 1.941 1.863 1.803 1 5103.916 5101.960 5101.653 5101.456 5098.314 2016-06-30 5103.428 5102.458 5099.741 5095.553 Elev Water <u>|</u> 1 (CES) 138.16 138.16 138.16 138.16 112.20 112.20 138.16 138.16 138.16 <u>|</u> 1 1 (EPS) 10.54 14.97 Vel 10.05 14.28 9.58 9.15 1 1 1 SF Ave Head .0054 .0225 .0033 .0045 .0123 .0202 .0028 1.43 .0049 1.57 1.73 3.48 3.76 .0038 3.17 1.30 5103.22 5102.91 Grd.El. | Elev | Depth | Width Energy | Super |Critical|Flow Top|Height/|Base Wt| ΗF 2.48 .04 .07 |SE Dpth|Froude N|Norm Dp | "N" | X-Fall| 4.50 1.94 1.50 3.83 3.63 1.80 4.83 3.46 1.86 00 00 00 00 1.37 . 68 1.58 .00 . 90 3.30 4.50 4.50 4.50 3.56 2.68 3.21 3.80 2.87 2.91 2.94 .00 . 00 |Dia.-FT|or I.D.| .013 4.500 .013 .013 .013 4.500 4.500 .013 .013 .013 .013 . 000 .000 .000 .000 .000 .00 .000 000 000 000 .00 .00 .00 .00 .00 .00 .00 ZR ZL.00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 00 .00 00 00 00 00 00 |Prs/Pip ***** Type Ch PIPE PIPE PIPE PIPE PIPE PIPE PIPE PIPE PIPE \vdash N \vdash N 2 0 . . 0 .

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Date: 6-30-2016

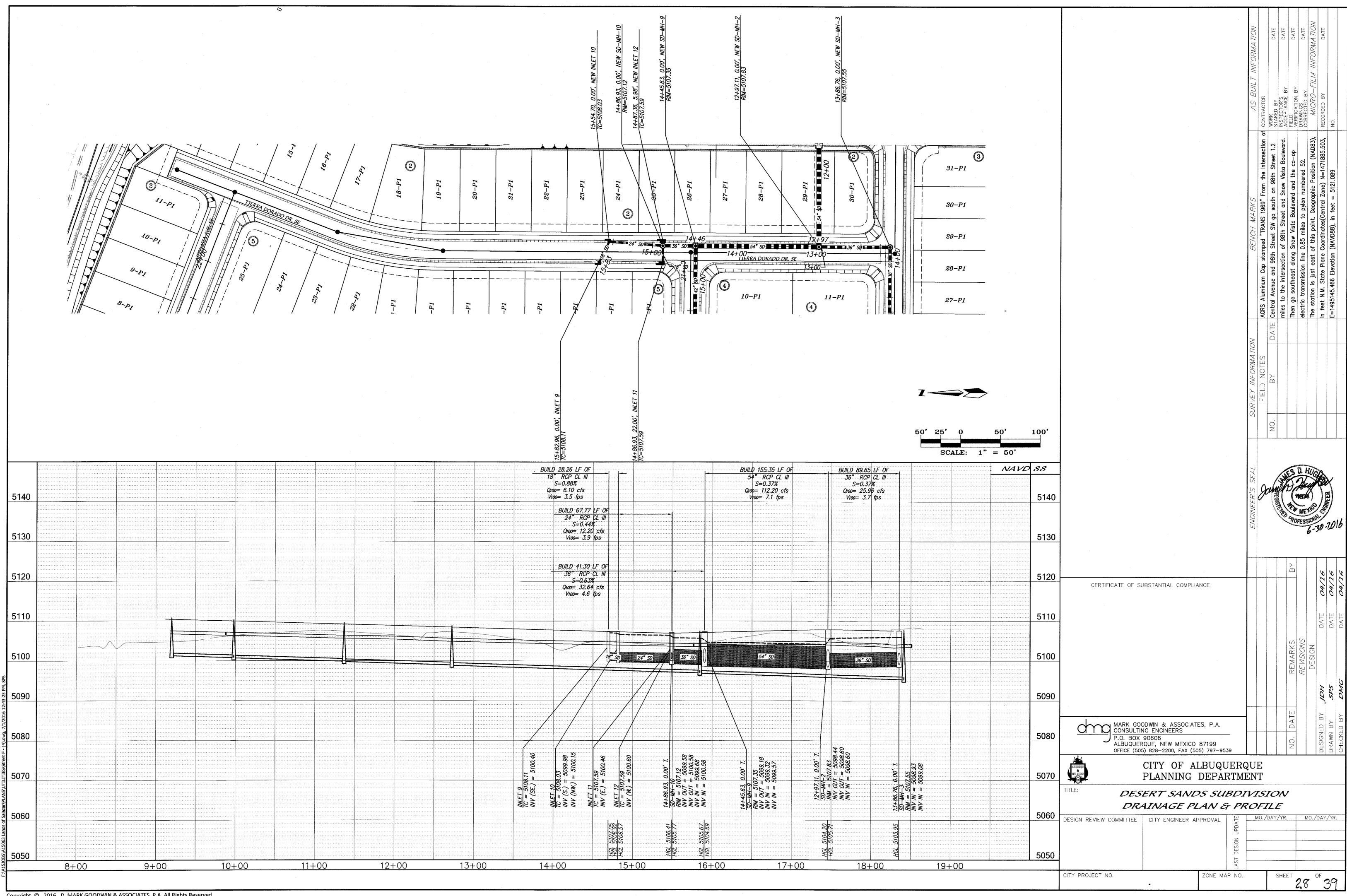
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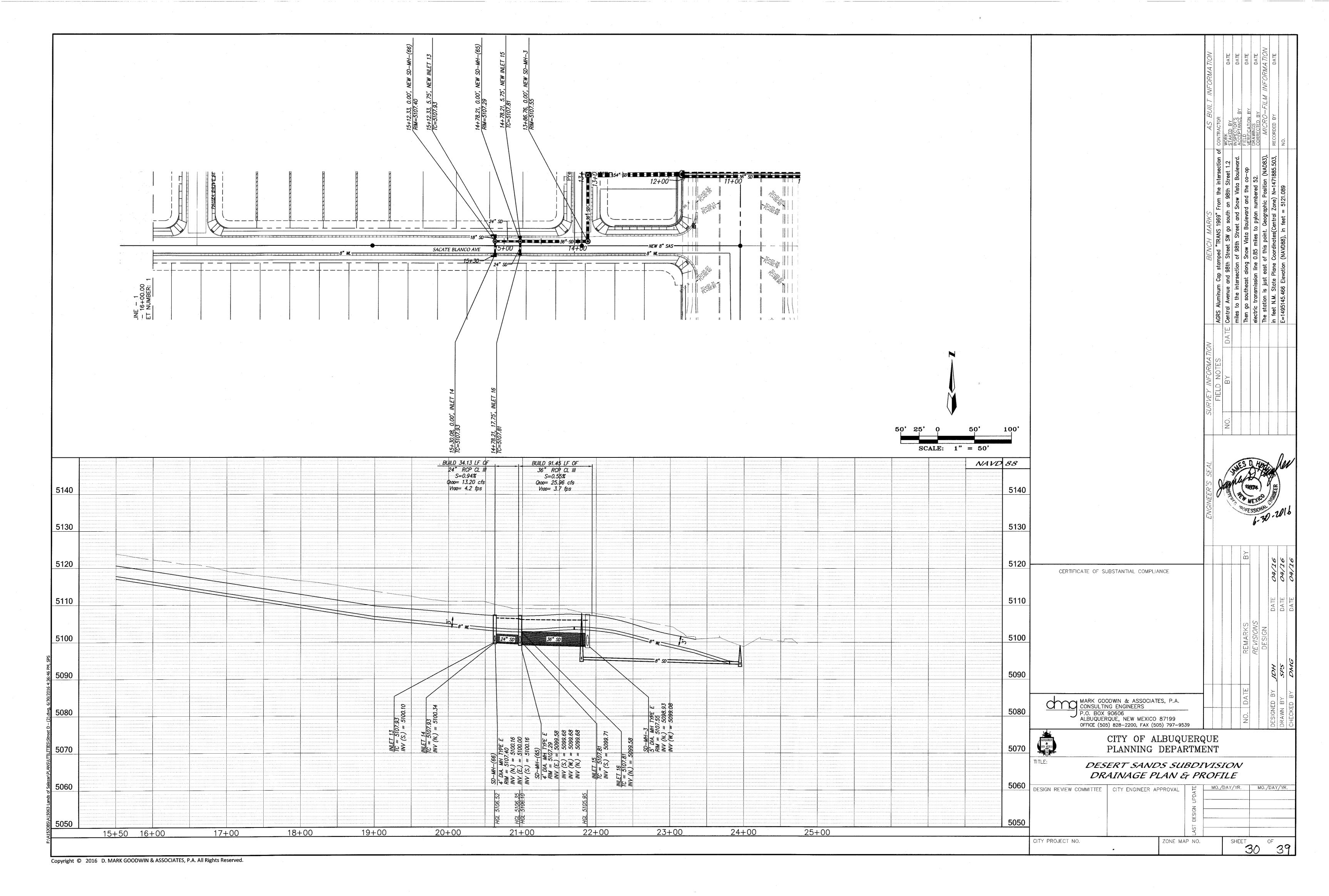
W S P G W - CIVILDESIGN Version 14.05 Program Package Serial Number: 1454 WATER SURFACE PROFILE LISTING

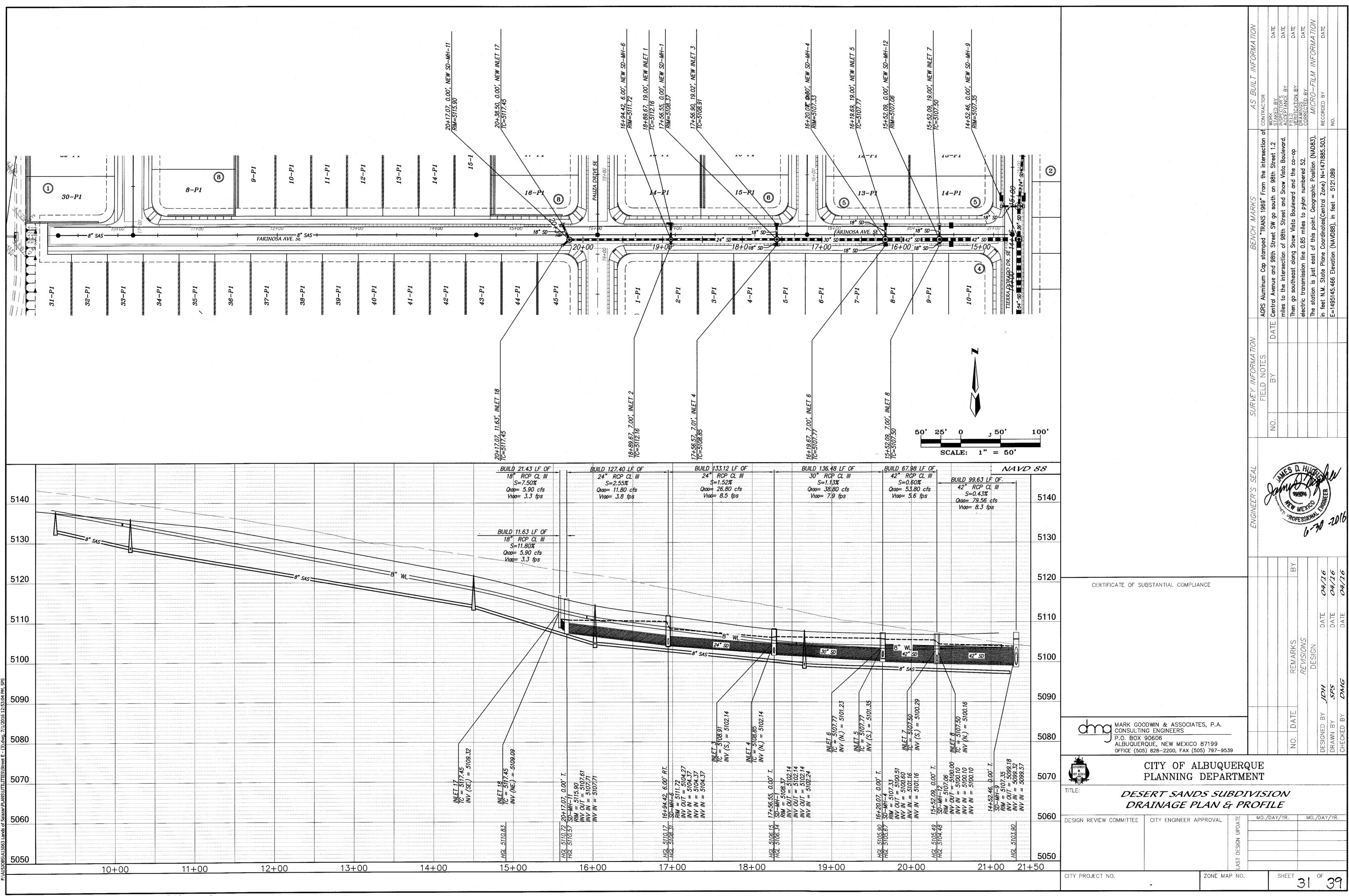
26.000 Thet#9 1583.000 72:5198-	JUNCT STR TC - SIDUL 1557.000	1553,000	63.000	1490.000	JUNCT STI	1484.000	27.000	1457.000	L/Elem ******	Station	***
5100.400	5100.150	5099.980	.0048	5099.680	3.0167	5099.580	0 .0096	5099.320	Ch Slope	Invert Elev	*******
6.647	6.754	6.578	1	6.695		6.150	1 - 1	6.346	*	Depth (FT)	Lands Tie 2
5107.046	5106.904	5106.558		5106.375	_	5105.730	ا <u>ا</u>	5105.666	******	Water Elev	Lands of Salazar Tierra Dorado 2016-06-30
6.10	6.10	12.20	. 1	12.20	ı	32.64	1	32.64	*	Q (CFS)	ar do Dr.
3.45	3.45	3.88	1 1	3.88		4.62		4.62	*	Vel (FPS)	** ** * * * * * * * * * * * * * * * *
.19	.0031	. 23	.0029	. 23	.0027	. 33	.0024	33	SF Ave	Vel Head	* * * * * *
.09	.01	5106.79	.18	5106.61	.02	5106.06	.06	5106.00	****** ******	Energy Grd.El.	TT.
6.75	6.58	.00	6.69	.00	6.15	.00	6.35	.00	SE Dpth F	Super	* * * * * * * * * * * * * * * * * * *
95	.00	1.26	.00	1.26	.00	1.85	.00	1.85	Dpth Froude N Norm Dp	Critical Depth	* * * * * * *
83	.00	.00	1.33	.00		.00	1.50	.00	Norm Dp *****	Flow Top Width	** ** ** ** ** *
1.500	.013	2.000	.013	2.000	.013	3.000	.013	3.000		Critical Flow Top Height/ Base Wt Depth	* * * * * * * * *
.000	.000	.000	.00	.000	.00	.000	.00	.000	********	Base Wt	* * * * * * * * * * * * * * * * * * *
	.00	.00	.00	.00	.00	.00	.00	.00	ZR + **	ZL	* * * *
PIPE	PIPE 1 .0	1 .0	PIPE	1 .0	BIPE	1 .0	HAIA	1 .0	Type Ch *****	No Wth	* * * * * * *

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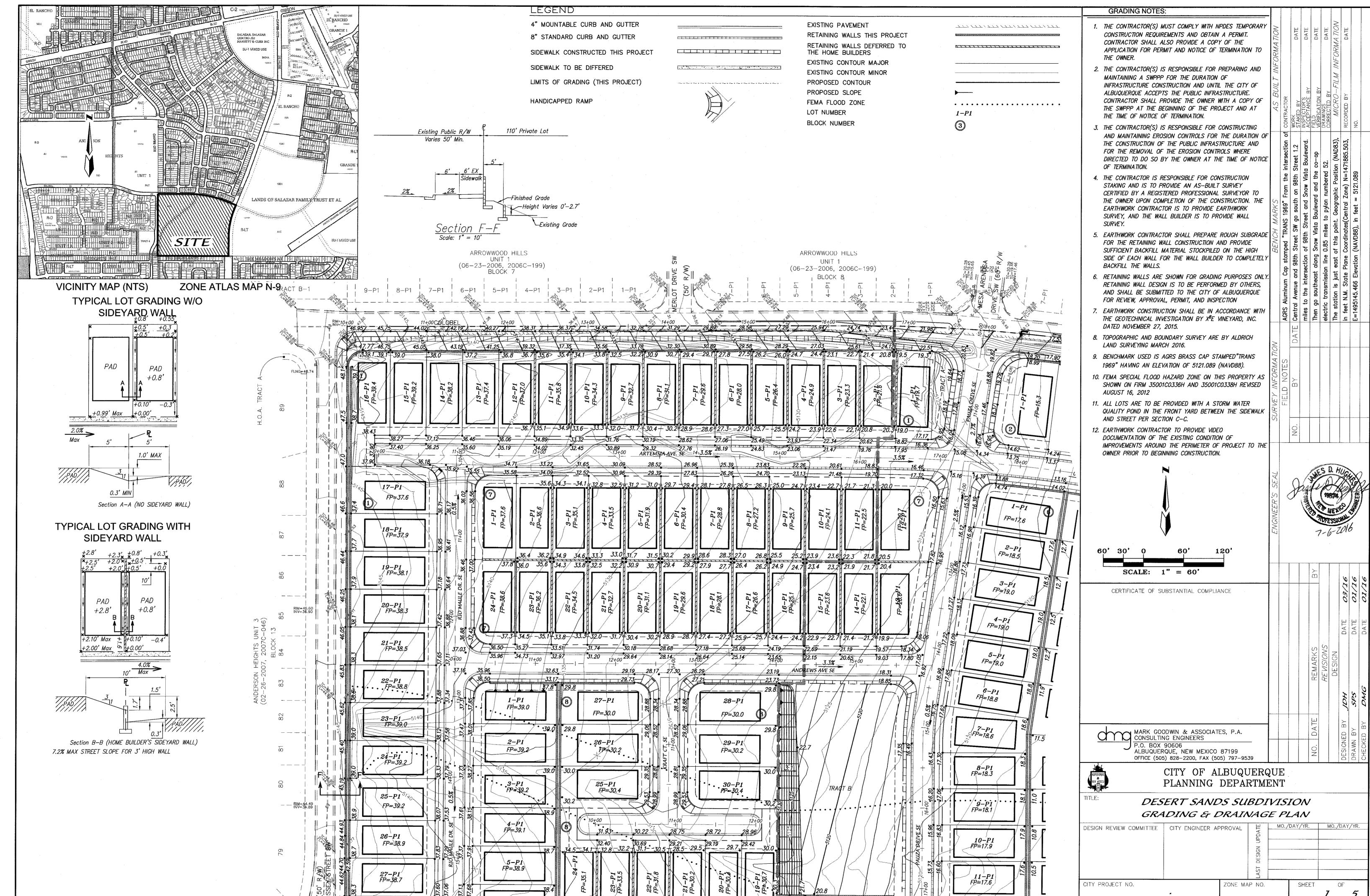


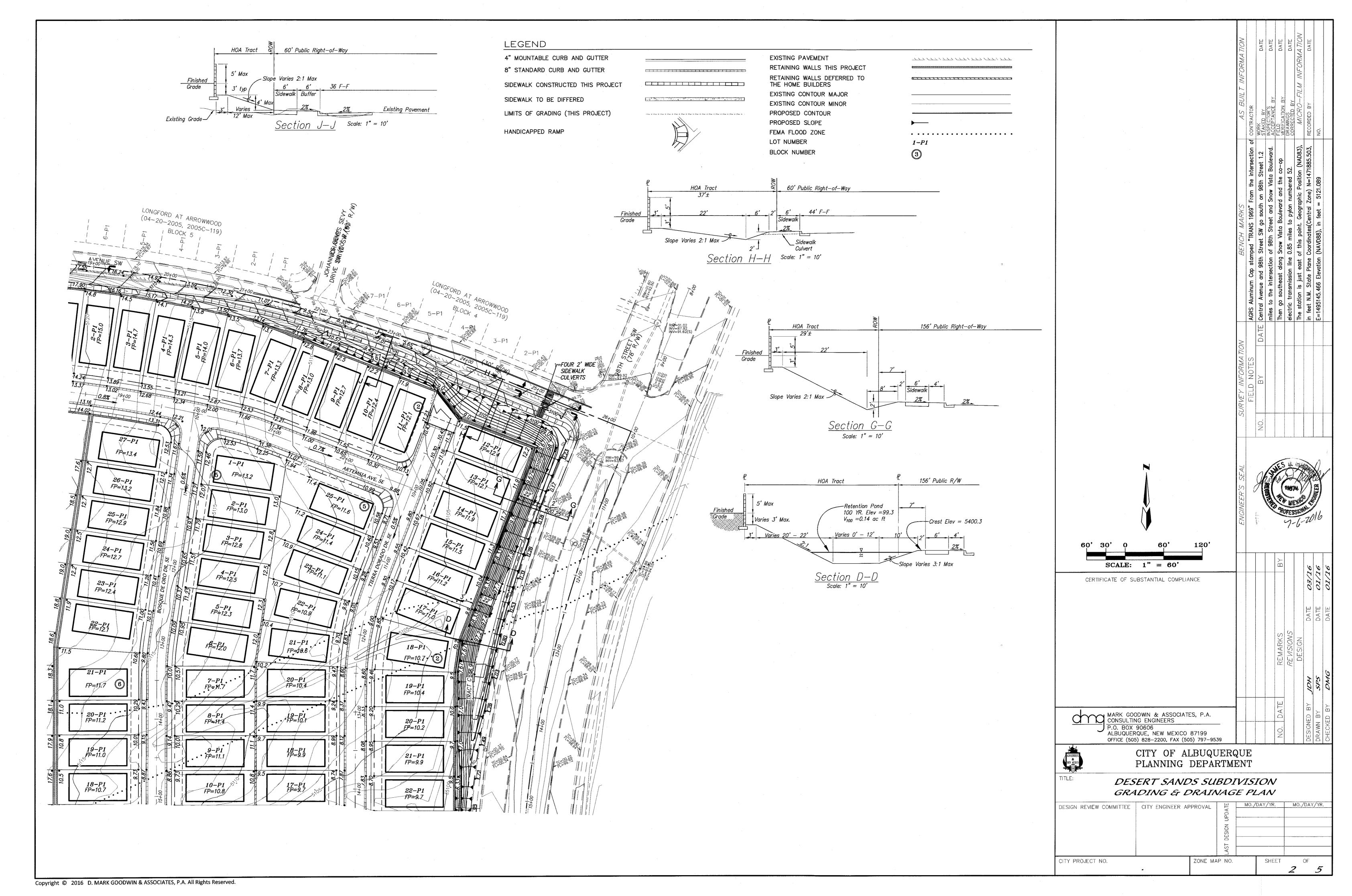




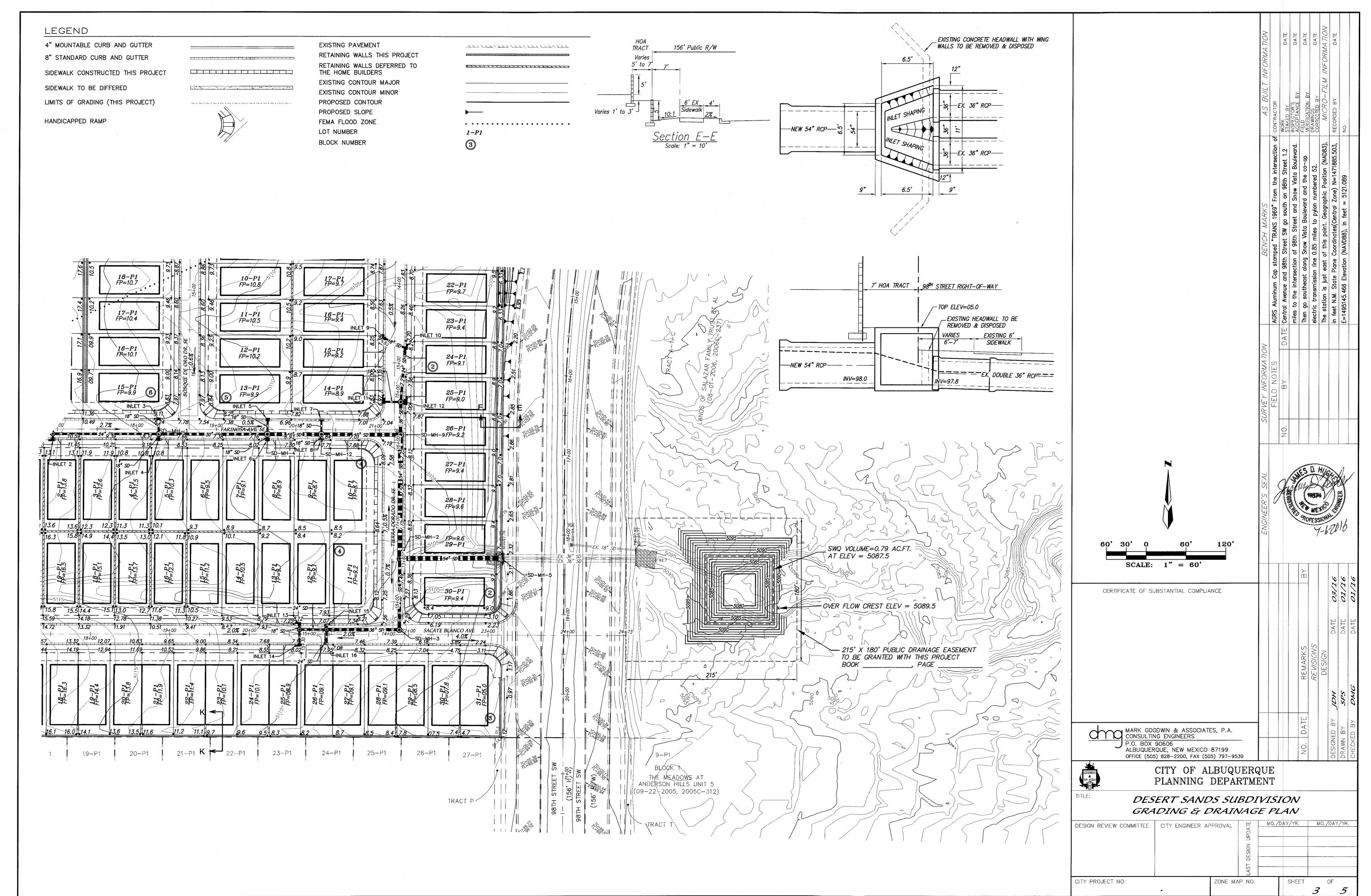
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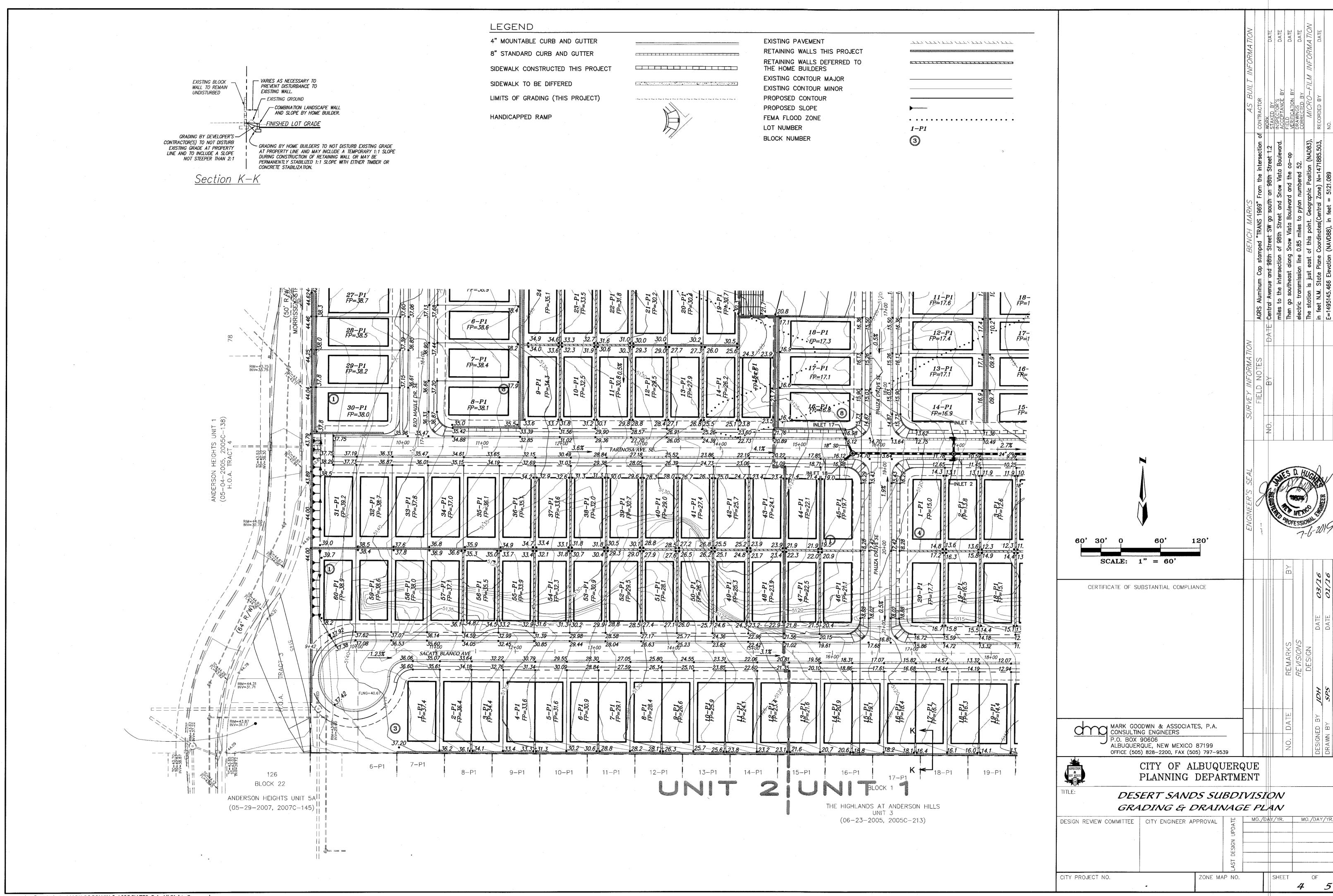
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