

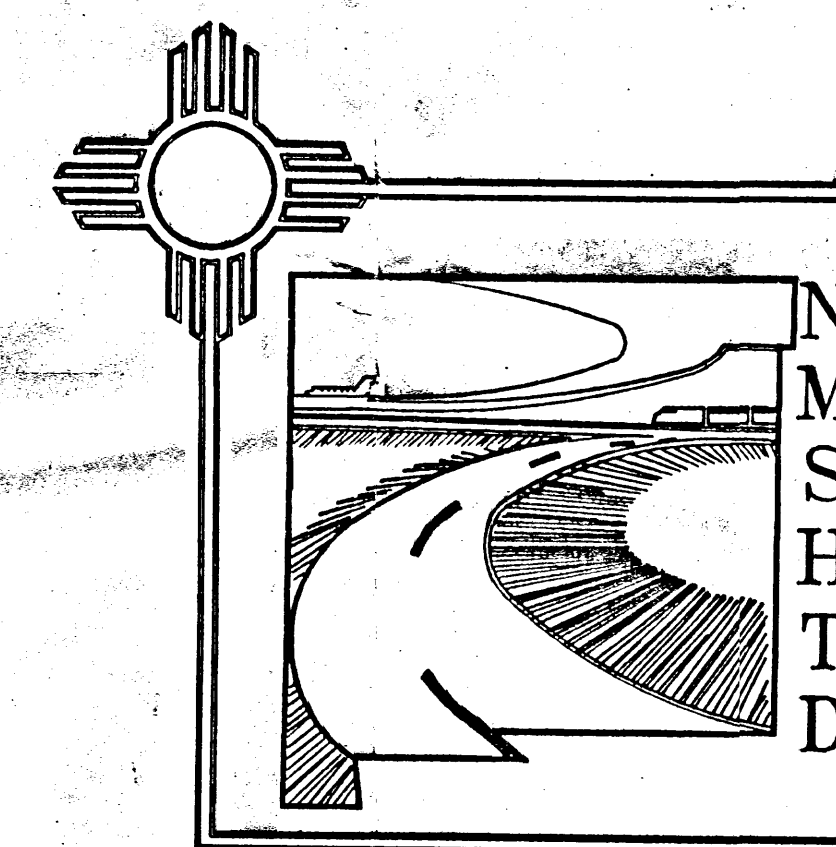
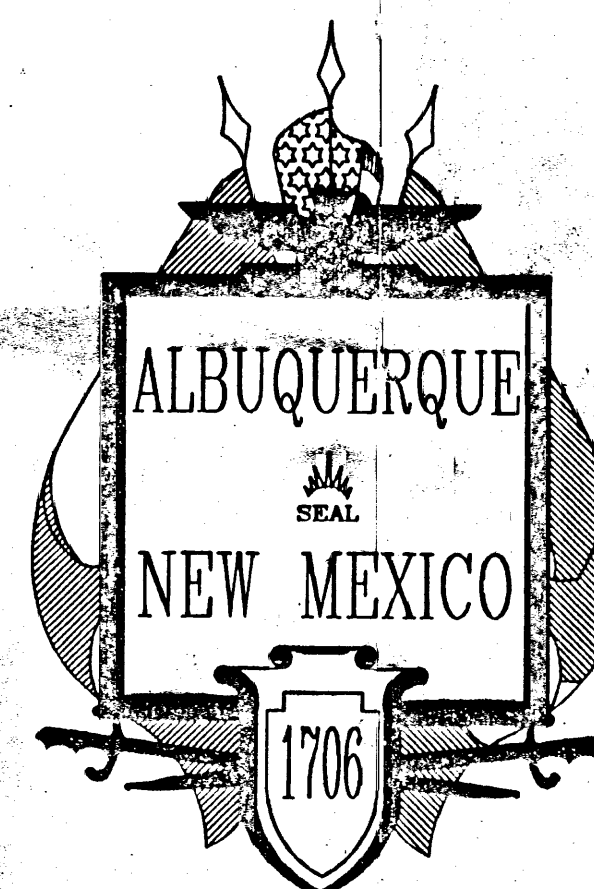
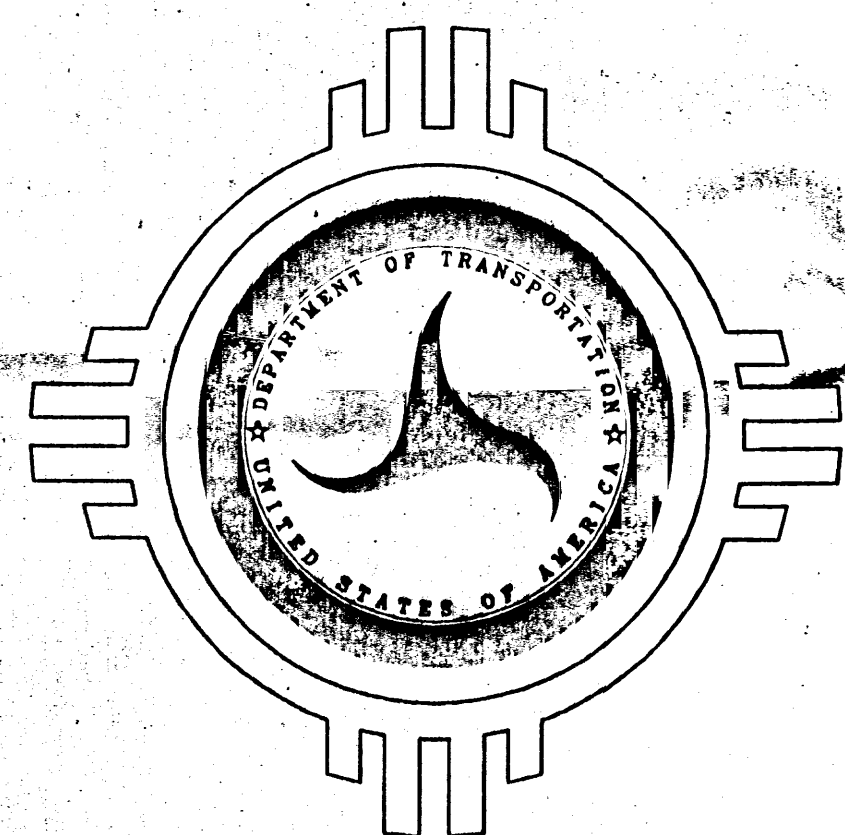
CONSTRUCTION PLANS FOR SUNPORT BOULEVARD — PHASE I

(STA. 65+00 TO STA. 95+00)

TPE-HDP-9253(1)

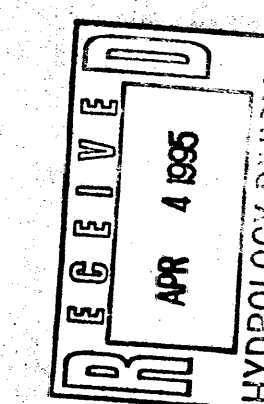
CN-9441

BERNALILLO COUNTY



Approved *Richard B. Rafel* Date 6/15/94
CITY ENGINEER

Approved *Carroll D. Young* Date 7-15-94
SECRETARY
P.E./L.S. NO. 4480



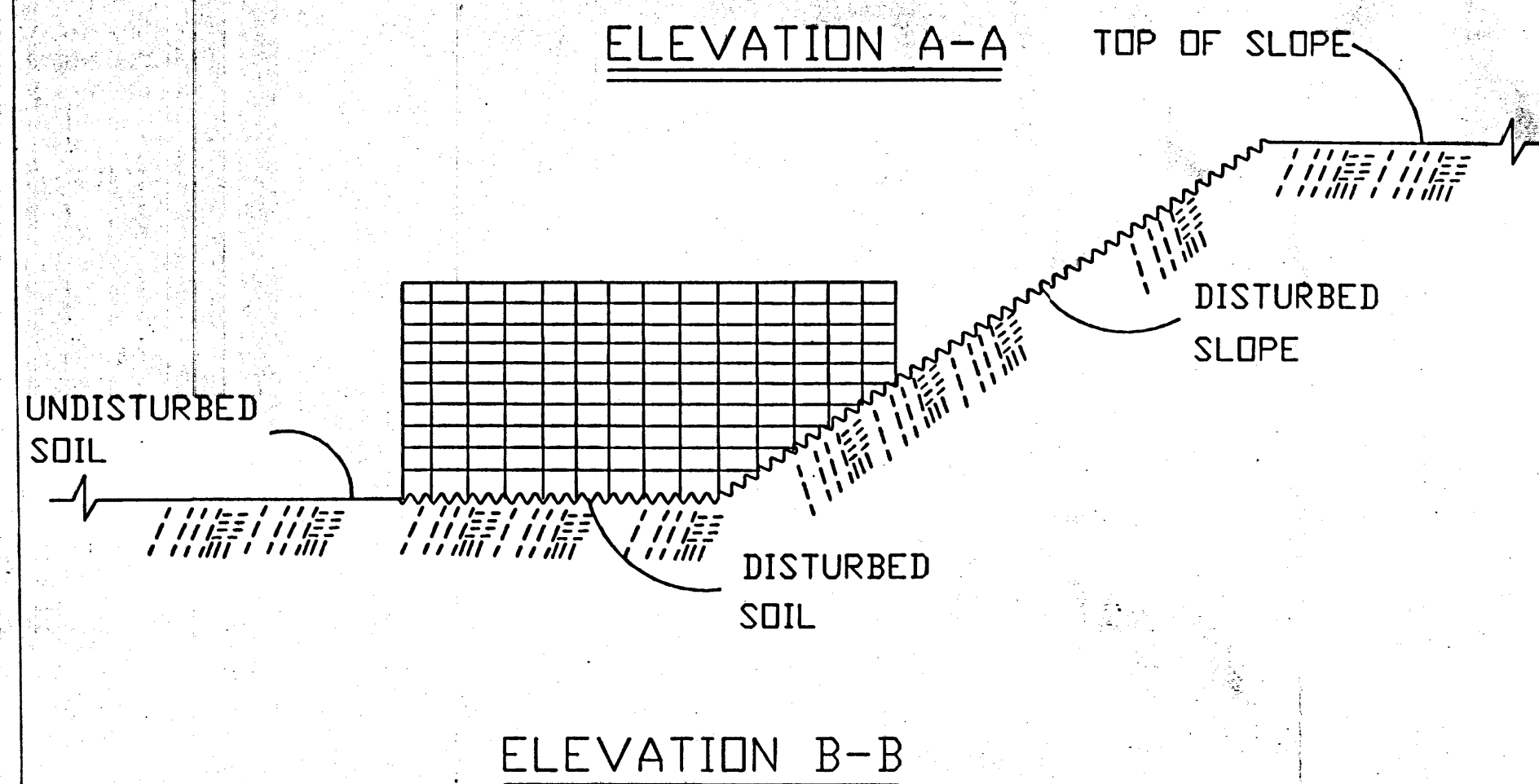
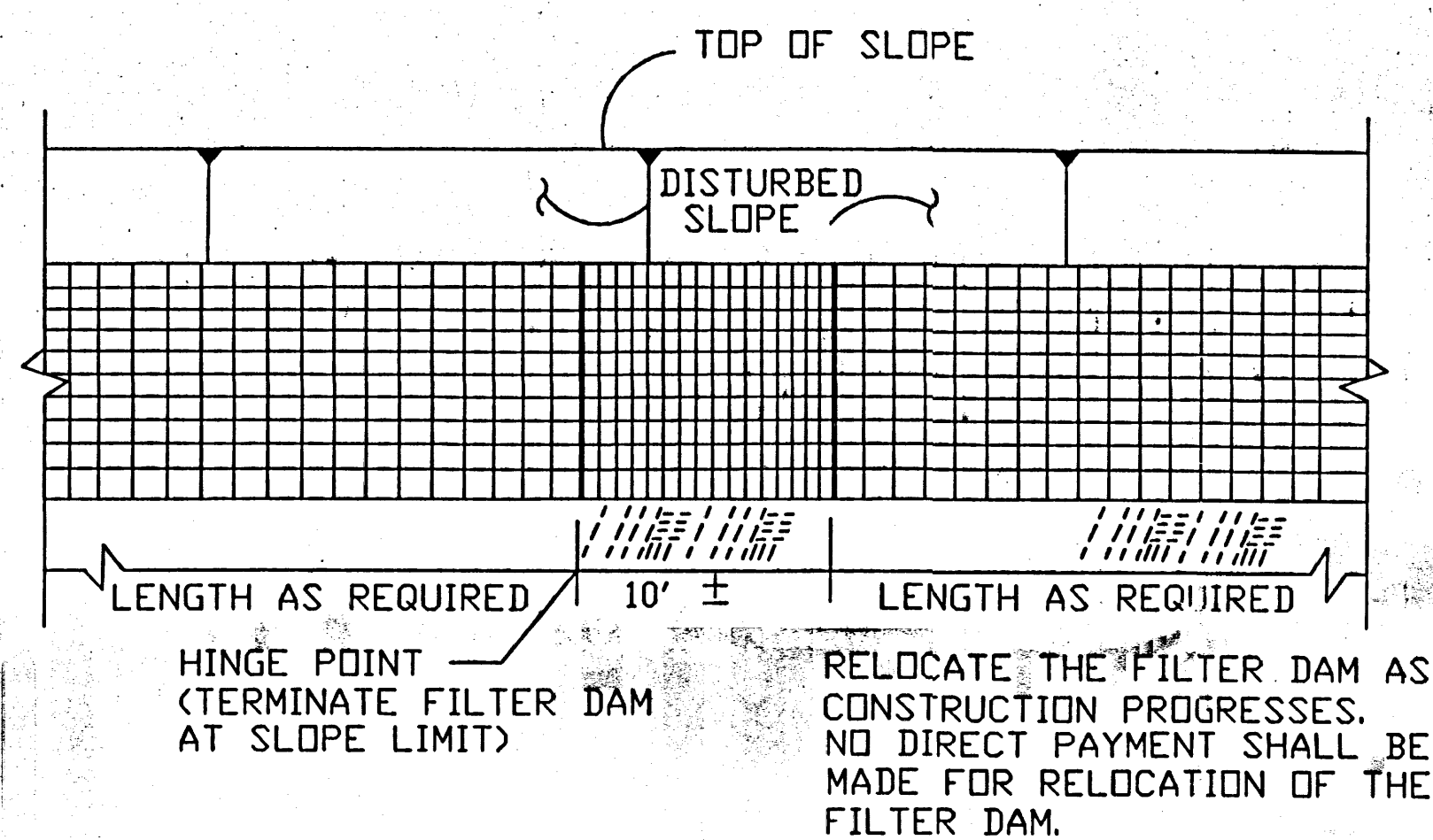
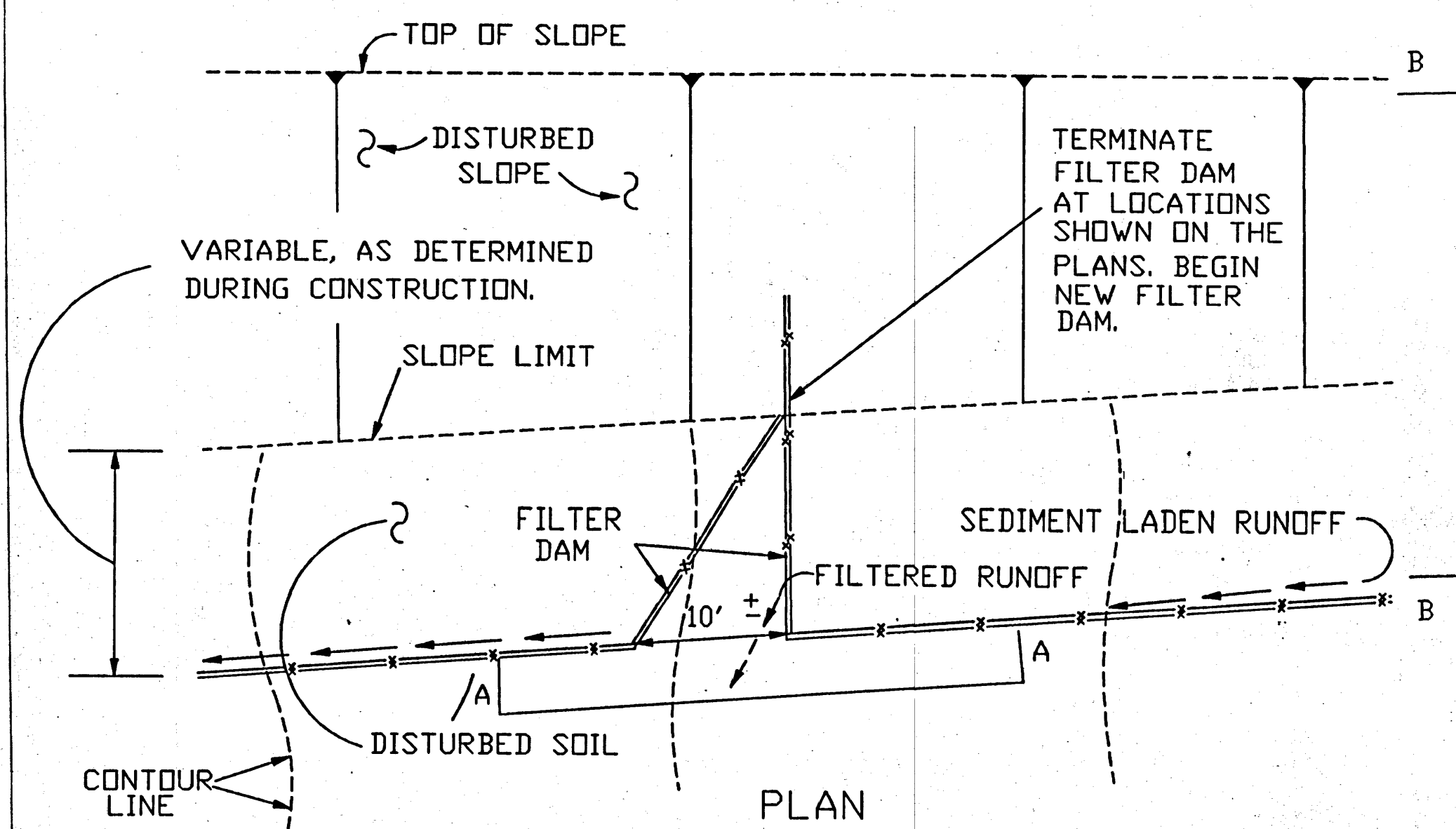
JUL 21 1994

CITY OF ALBUQUERQUE, N.M.

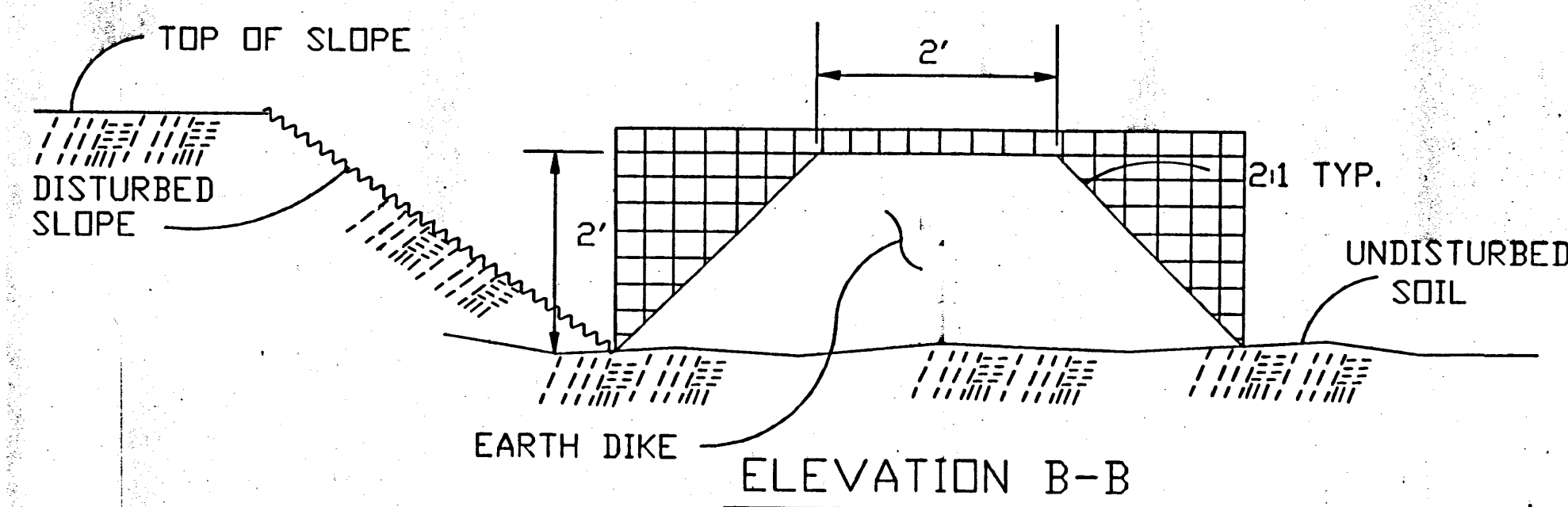
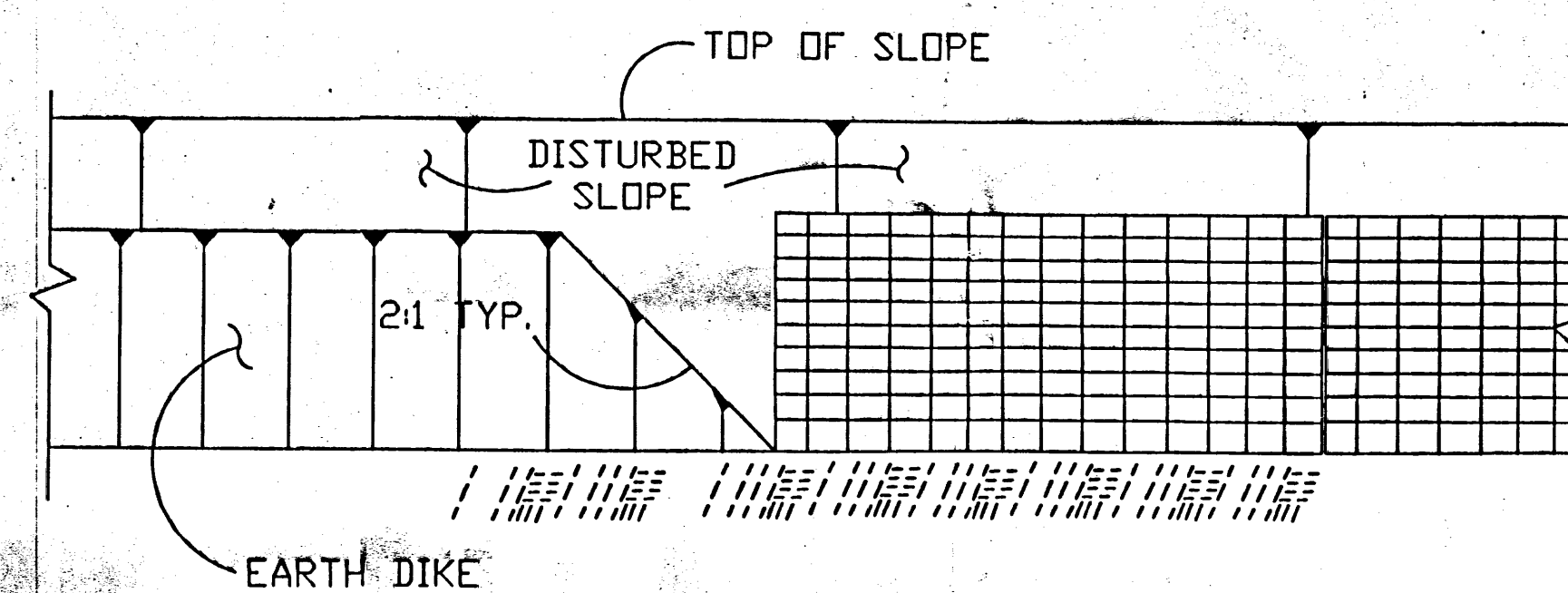
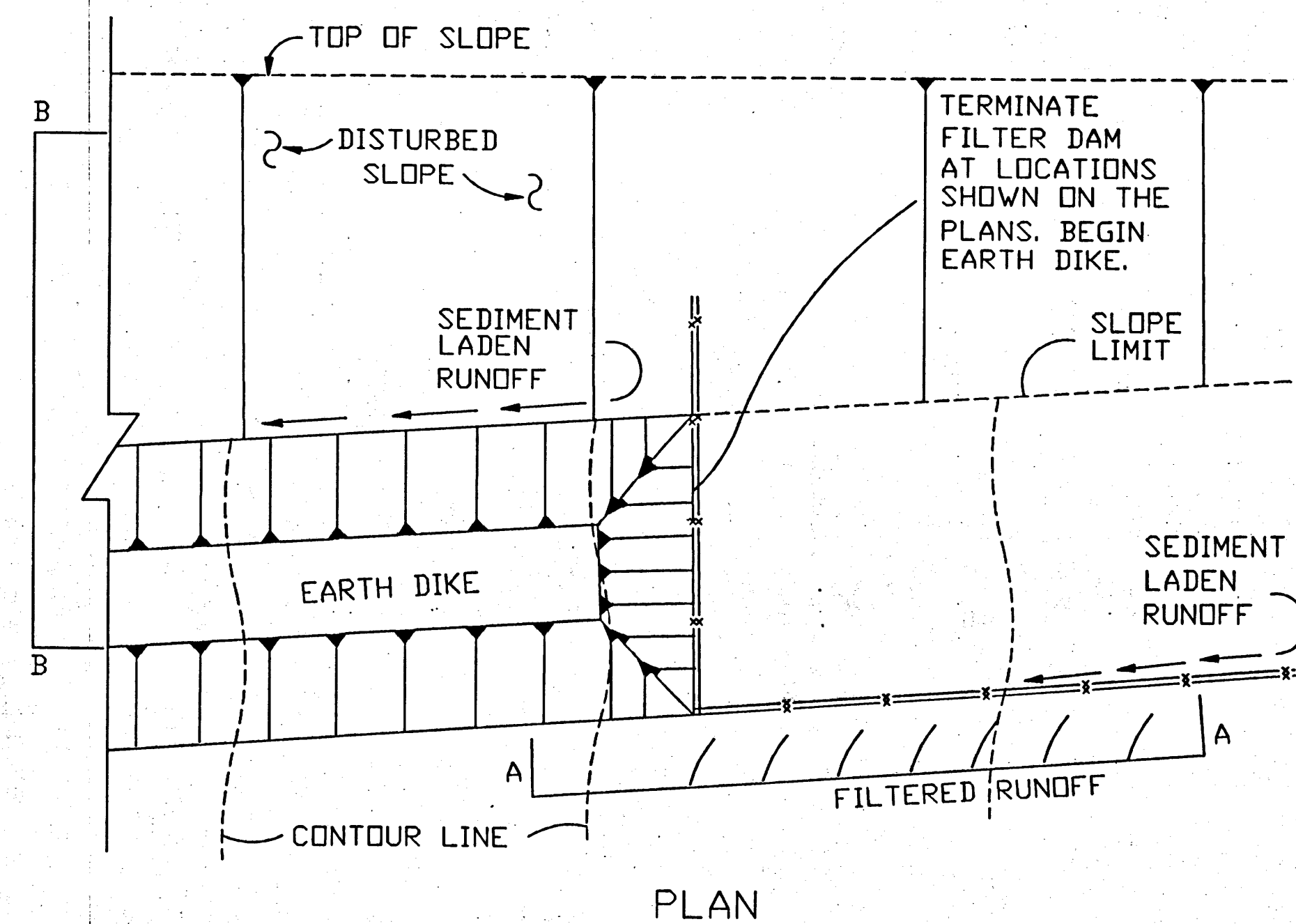
PUBLIC WORKS DEPT.

ENGINEERING GROUP/TRANSPORTATION

REV	SHEETS	CITY	ENGR.	DATE	USER	DEPT.	DATE	USER	DEPT.	DATE
APPROVAL OF REVISIONS										
						MOLZEN-CORBIN & Associates				
PROJECT NO. 6-14-94						C.O.A. 4044-90			SHEET 1-1	



TYPICAL INSTALLATION FOR FILTER DAM ON SLOPES WITH LONGITUDINAL SLOPE *



TYPICAL INSTALLATION FOR FILTER DAM WITH EARTH DIKE ON SLOPES WITH LONGITUDINAL SLOPE *

TEMPORARY EROSION & SEDIMENT CONTROL MEASURES (T.E.S.C.M.)

GENERAL NOTES:

1. THE SOIL RETENTION BLANKET INSTALLATION DETAILS SHOWN FOR DITCH LINERS SHALL BE USED FOR ALL TEMPORARY EROSION AND SEDIMENT CONTROL MEASURES UTILIZING SOIL RETENTION BLANKETS UNLESS OTHERWISE NOTED.
2. ROCK PLATING USED IN THE TEMPORARY EROSION AND SEDIMENT CONTROL MEASURES SHOWN ON THESE SHEETS SHALL HAVE A MINIMUM THICKNESS OF 9 INCHES UNLESS OTHERWISE INDICATED.
3. ALL TEMPORARY EROSION AND SEDIMENT CONTROL MEASURES PLACED WITHIN THE CLEAR ZONE SHALL BE INSTALLED WITH 8:1 SLOPES PARALLEL TO TRAFFIC AND 3:1 SLOPES PERPENDICULAR TO TRAFFIC WHERE APPLICABLE. FOR SEDIMENT TRAPS LOCATED WITHIN THE CLEAR ZONE, THE MAXIMUM HEIGHT OR EXCAVATED DEPTH OF THE TRAP SHALL NOT EXCEED 12 INCHES.
4. SEDIMENT BASINS AND TRAPS SHALL BE CLEANED OF ACCUMULATED SEDIMENT WHEN APPROXIMATELY 50% FILLED.
5. FILTER DAMS SHALL BE CLEANED OF ACCUMULATED SEDIMENT WHEN THE DEPOSITS REACH APPROXIMATELY ONE-HALF THE HEIGHT OF THE FILTER DAM.
6. DITCH LINER SHALL BE INSTALLED UPON INITIATION OF EARTH ACTIVITIES AND MAINTAINED AS PRACTICAL UNTIL STABILIZATION IS COMPLETED AND ACCEPTED. DITCH LINER MAY BE REMOVED FOR PERIODS OF TIME AS REQUIRED DURING CONSTRUCTION TO COMPLETE ADJACENT IMPROVEMENTS.

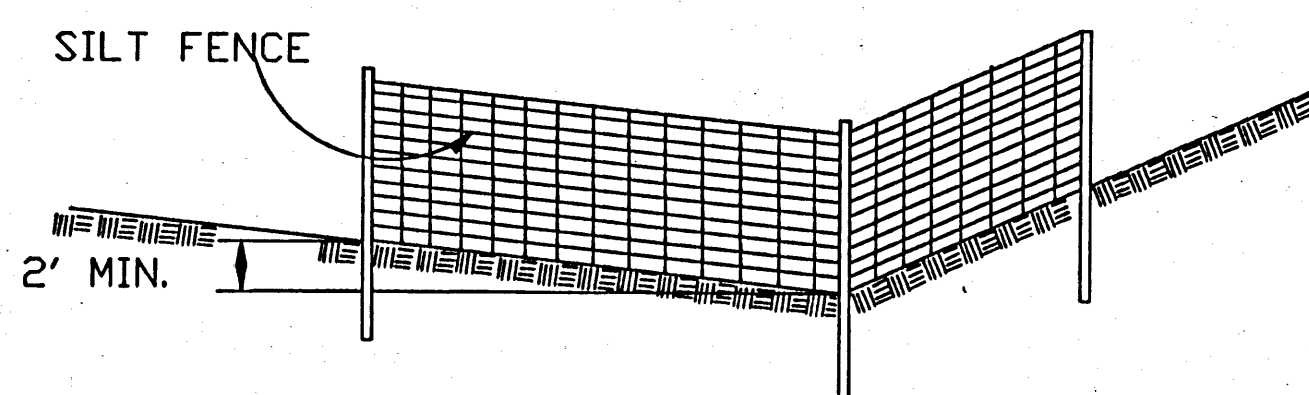
* THE CONTRACTOR MAY CONSTRUCT AN EARTH DIKE, AS SHOWN OR RELOCATE THE FILTER DAM AS CONSTRUCTION PROGRESSES. NO DIRECT PAYMENT SHALL BE MADE FOR RELOCATION OF THE FILTER DAM.

3	REVISED FILTER DAM DRAWINGS	10-6-93	JH/BL
2	MINOR TYPING REVISIONS	8-27-93	BSL
1	DESCRIPTION	DATE	BY
REVISIONS (OR CHANGE NOTICES)			
NEW MEXICO STATE HIGHWAY AND TRANSPORTATION DEPARTMENT			
TEMPORARY EROSION & SEDIMENT CONTROL MEASURES			
LAYOUT BY	APPROVAL	RECOMMENDED	ENGINEER
DRAWN BY	APPROVED	DESIGN BUREAU CHIEF	DATE
CHECKED BY			
DRAWING 050 SHEET 1 OF 4			

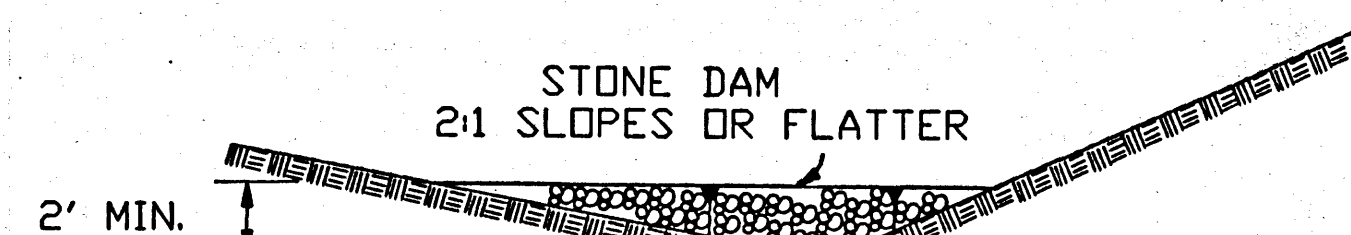
SILT FENCE NOTES:

1. POST SPACING SHALL BE 4 FT. MAXIMUM W/O SUPPORTING FENCE, 10 FT. MAXIMUM WITH SUPPORTING FENCE.
2. POSTS FOR 4 FT. MAXIMUM POST SPACING SHALL BE 2 INCH SQUARE OR HEAVIER WOOD POSTS OR STANDARD T OR U SECTION STEEL POSTS WEIGHING NOT LESS THAN 1.0 LB. PER LINEAR FOOT. POSTS FOR 10 FT. MAXIMUM POST SPACING SHALL BE 4 INCH SQUARE OR HEAVIER WOOD POSTS OR STEEL POSTS AS SPECIFIED ABOVE.
3. SUPPORTING FENCE SHALL BE WIRE MESH (14 GA. MIN., 6 INCH MAX. MESH OPENINGS) OR SNOW FENCE.
4. SUPPORTING FENCE SHALL BE FASTENED SECURELY TO POSTS WITH STAPLES OR WIRE TIES. FILTER FABRIC SHALL BE FASTENED SECURELY TO SUPPORTING FENCE WITH WIRE TIES SPACED AT 24 INCH CENTERS ALONG THE TOP AND MID-SECTION. WHEN A SUPPORTING FENCE IS NOT USED, FILTER FABRIC SHALL BE SECURELY FASTENED TO POSTS WITH STAPLES OR WIRE TIES.

NOTE: WHEN SILT FENCE IS USED FOR FILTER DAM INSTALLED IN DITCHES A SUPPORTING FENCE SHALL BE PROVIDED AND THE POST SPACING SHALL BE 10' MAXIMUM.



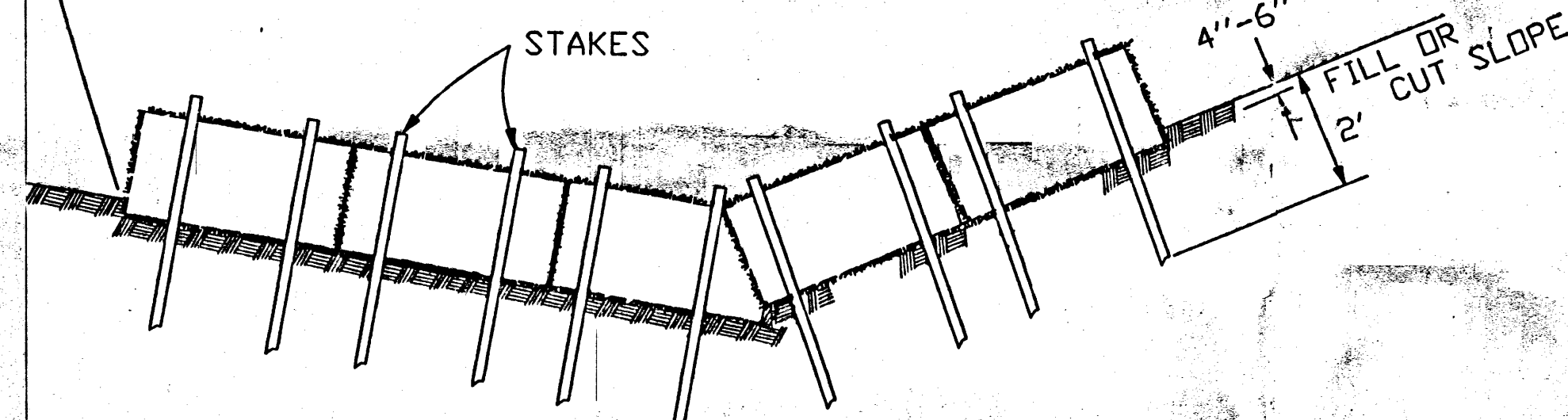
ELEVATION - FILTER DAM
(SILT FENCE OPTION)



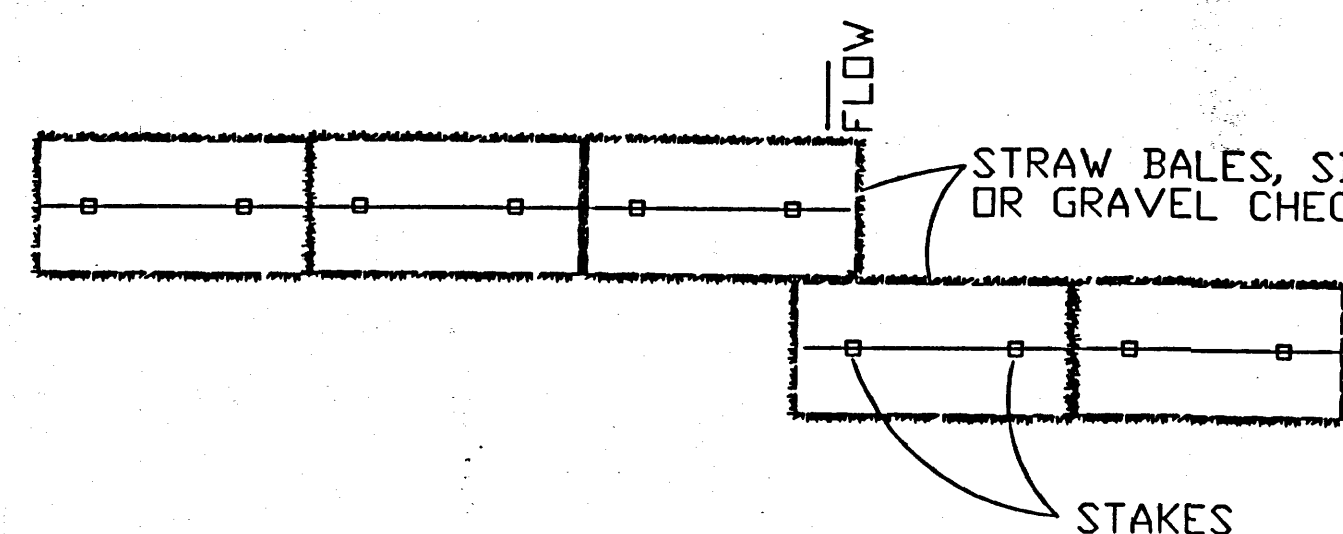
NOTE: STONE SHALL CONSIST OF 1" TO 3" WASHED GRAVEL.

ELEVATION - FILTER DAM
(STONE DAM OPTION)

EXTEND BALES, SILT FENCE OR STONE DAM IN BOTH DIRECTIONS UNTIL INTERCEPT ELEVATION IS A MINIMUM OF TWO FEET (2') ABOVE DITCH LINE ELEVATION.



ELEVATION - FILTER DAM
(STRAW BALES OPTION)



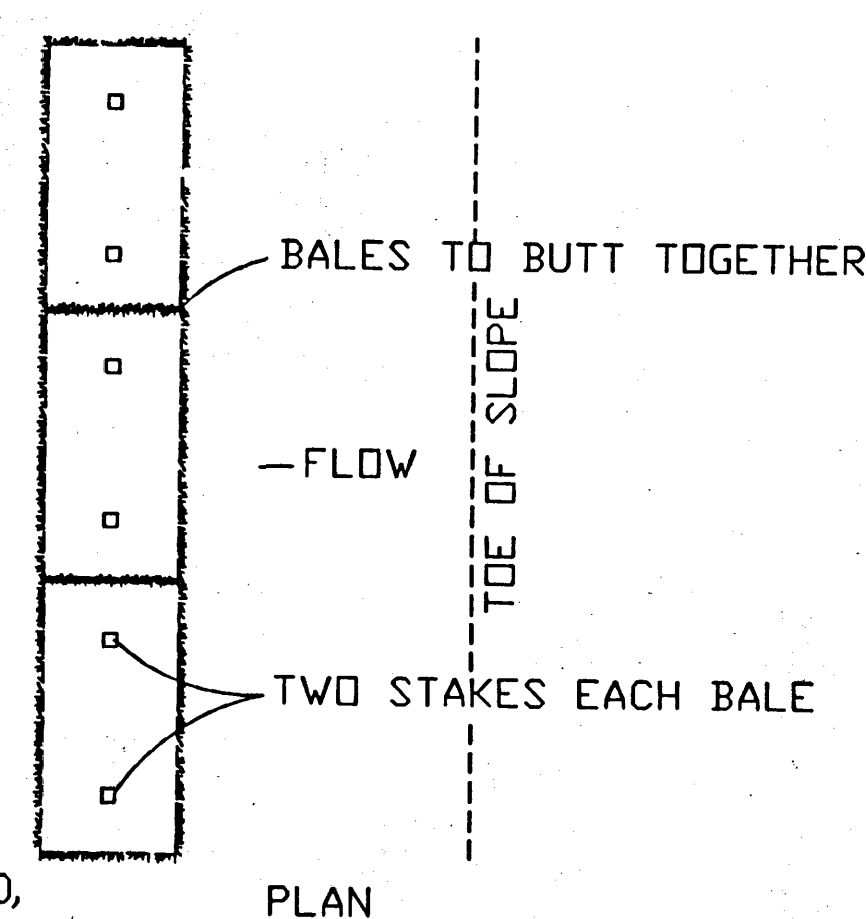
FILTER DAM

(FOR DITCHES)

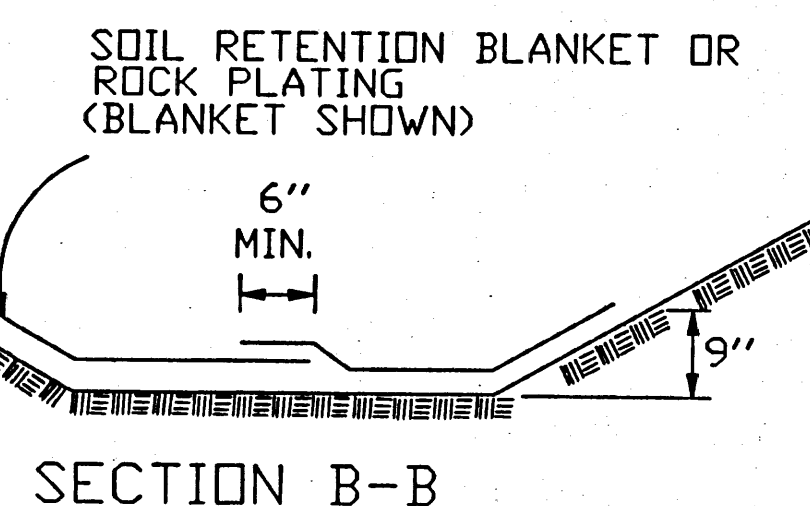
SEE FILTER DAM (FOR SLOPES) FOR ADDITIONAL CONSTRUCTION DETAILS OF SILT FENCE AND STRAW BALES.

STRAW BALES FILTER DAM NOTES:

1. EMBED BALES 4 TO 6 INCHES INTO GROUND.
2. IN AREAS WHERE BALES MAY BE ALLOWED TO REMAIN IN PLACE, WOOD STAKES MUST BE USED. IN OTHER AREAS ALTERNATE STAKES MAY BE USED.
3. LOOSE HAY OR STRAW SHALL BE STUFFED BETWEEN BALES TO FILL VOIDS.
4. STAKES SHALL BE 2"X 2" WOOD, REBAR (#4 MIN.) OR STANDARD STEEL POSTS DRIVEN 2' MIN. INTO GROUND.

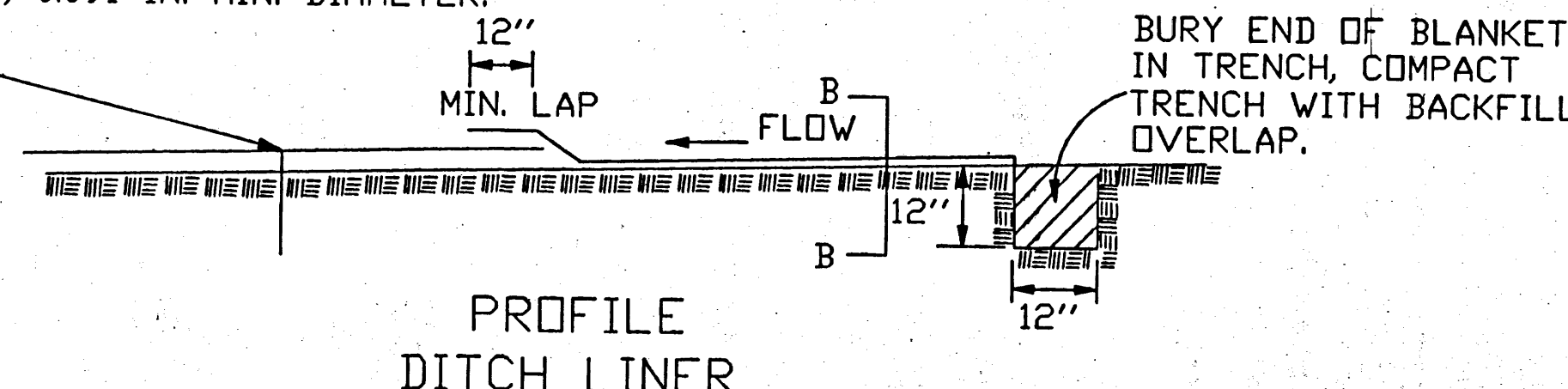


FILTER DAM
(FOR SLOPES)

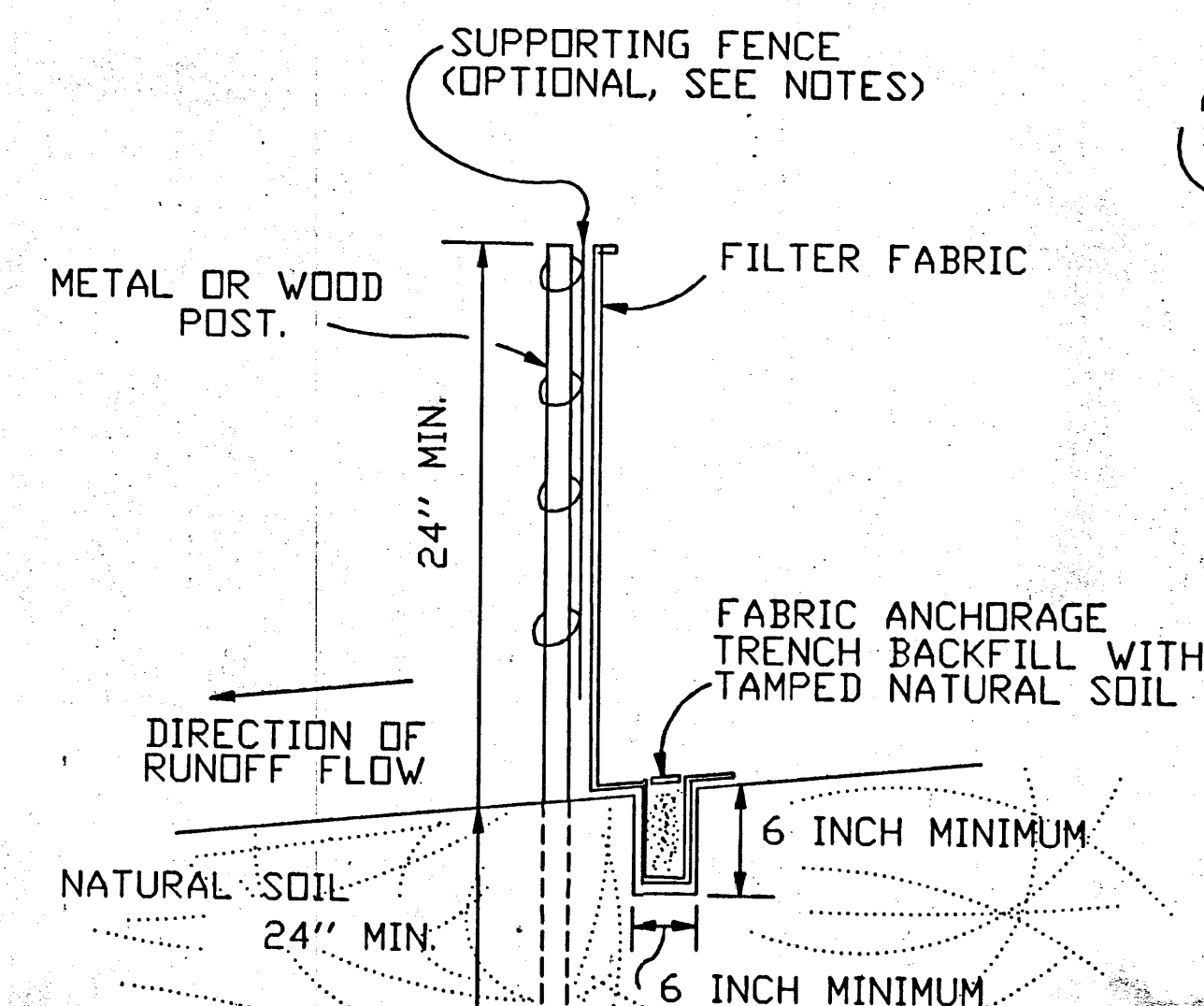


SECTION B-B

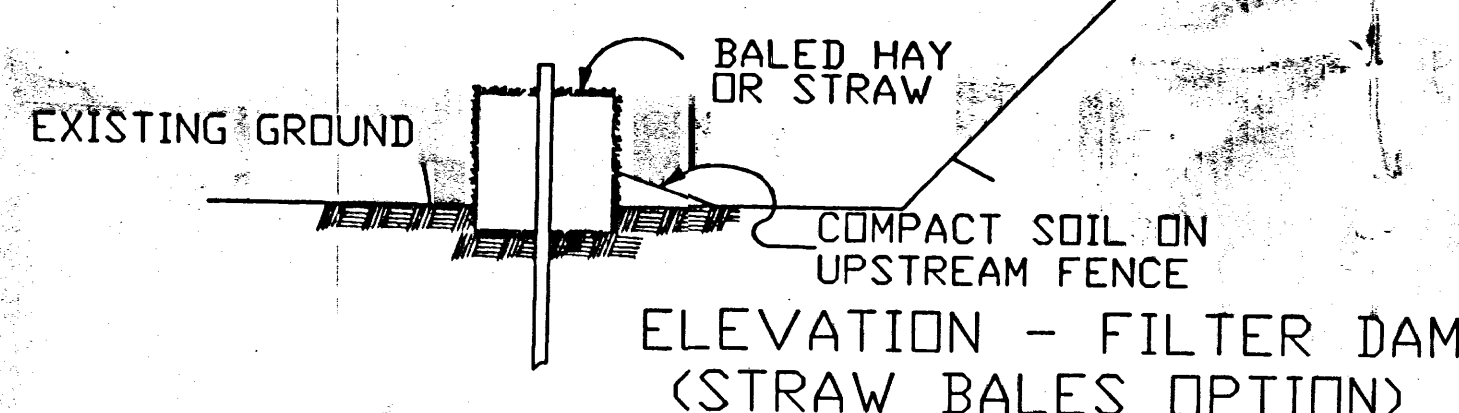
ANCHOR - 8" X 1" X 8" "U" SHAPED STEEL STAPLES, 0.091 IN. MIN. DIAMETER.



PROFILE
DITCH LINER

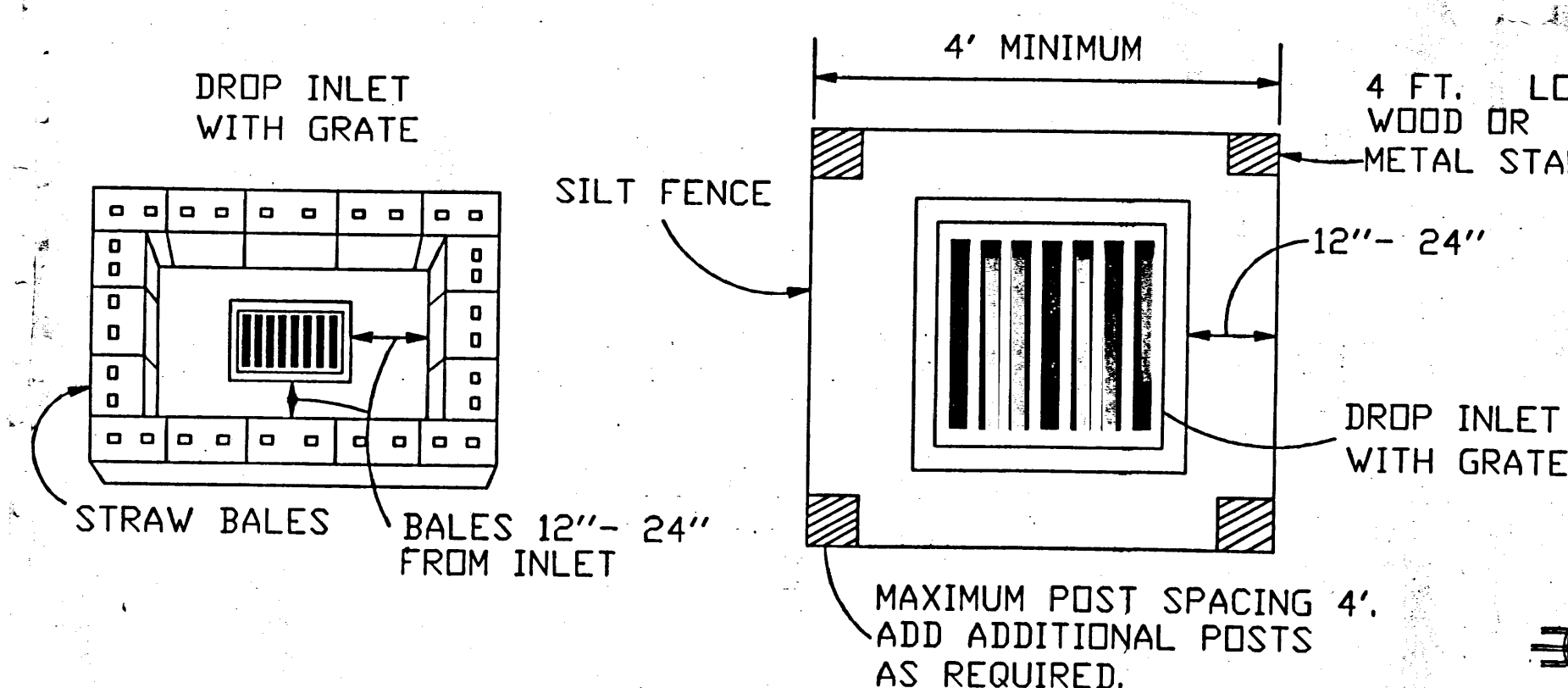


ELEVATION - FILTER DAM
(SILT FENCE OPTION)



ELEVATION - FILTER DAM
(STRAW BALES OPTION)

TYPICAL DITCH LINER INSTALLATIONS AT CULVERTS



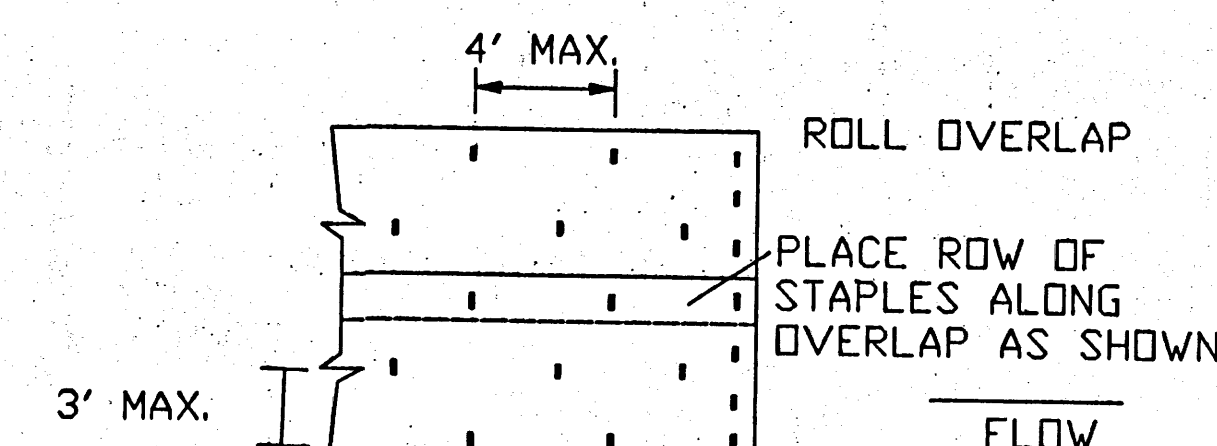
SEE FILTER DAM (FOR SLOPES) FOR CONSTRUCTION DETAILS OF SILT FENCE.

CHECK DAM

CHECK DAM SHOWN FOR DROP INLET, LAYOUT FOR CURB INLETS SIMILAR.

DITCH LINER NOTES:

1. THE DITCH LINER WIDTH REQUIRED SHALL BE IN ACCORDANCE WITH THESE DETAILS UNLESS SPECIFIED OTHERWISE.
2. THE SOIL RETENTION BLANKET INSTALLATION SHOWN OUTLINES MINIMUM REQUIREMENTS. MANUFACTURERS RECOMMENDATIONS SHALL BE USED IF THEY ARE MORE STRINGENT.
3. WHEN DITCH LINER IS SPECIFIED, EITHER SOIL RETENTION BLANKETS OR ROCK PLATING MAY BE PROVIDED.

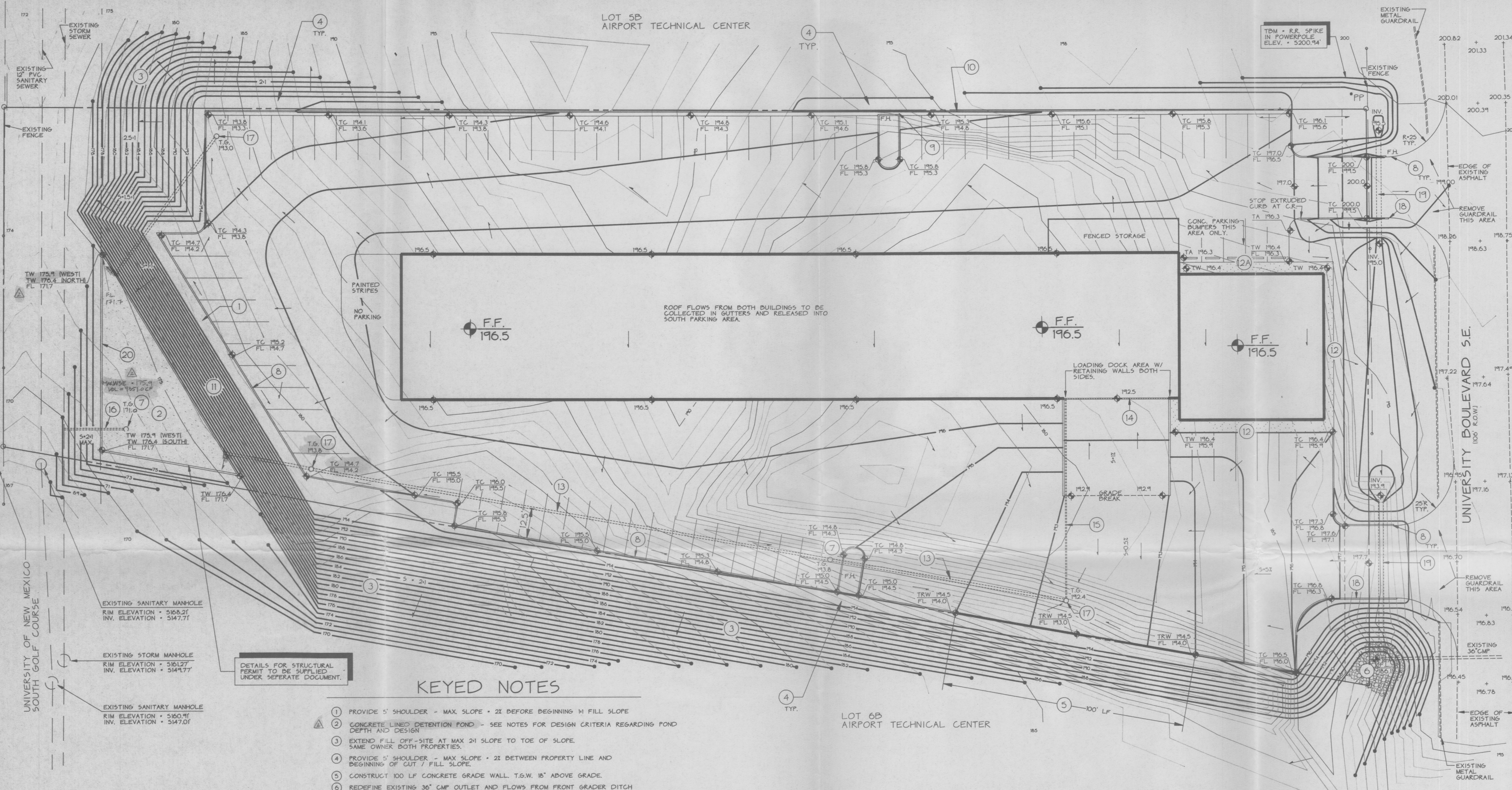


USE 1 FT. SPACING FOR STAPLES AT BEGINNING OF ROLL AND AT TRAVERSE OVERLAP.

SOIL RETENTION BLANKET
STAPLE PATTERN

3			
2			
1	MINOR TYPING REVISIONS	8-27-93	BSL
NO.	DESCRIPTION	DATE	BY
REVISIONS (OR CHANGE NOTICES)			
NEW MEXICO STATE HIGHWAY AND TRANSPORTATION DEPARTMENT			
T.E.S.C.M. FILTER DAM ALTERNATES & RETENTION BLANKET DETAILS			
LAYOUT BY	APPROVAL		
DRAWN BY	RECOMMENDED ENGINEER		DATE
CHECKED BY	APPROVED		DATE
		DESIGN BUREAU CHIEF	
DRAWING 050		SHEET 2 OF 4	

SHT. 2-36

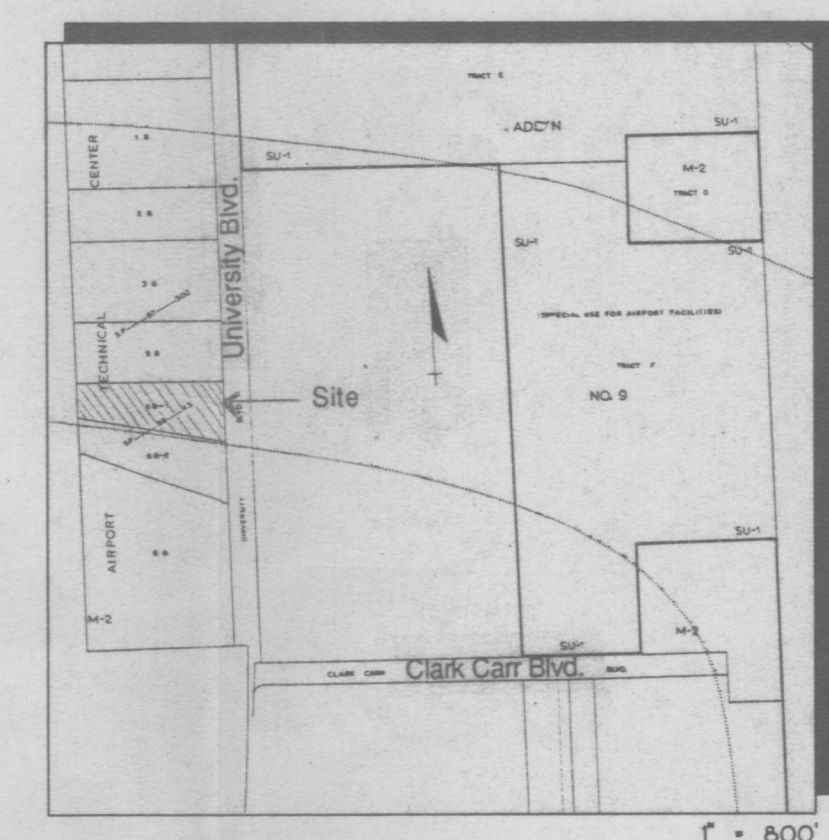


KEYED NOTES

- 1 PROVIDE 5' SHOULDER - MAX SLOPE = 2% BEFORE BEGINNING 1:1 FILL SLOPE
- 2 CONCRETE LINED DETENTION POND - SEE NOTES FOR DESIGN CRITERIA REGARDING POND DEPTH AND DESIGN
- 3 EXTEND FILL OFF-SITE AT MAX 2:1 SLOPE TO TOE OF SLOPE. SAME OWNER BOTH PROPERTIES.
- 4 PROVIDE 5' SHOULDER - MAX SLOPE = 2% BETWEEN PROPERTY LINE AND BEGINNING OF CUT / FILL SLOPE.
- 5 CONSTRUCT 100 LF CONCRETE GRADE WALL T.G.W. 15' ABOVE GRADE.
- 6 REDEFINE EXISTING 36" CMP OUTLET AND FLOWS FROM FRONT GRADER DITCH TO LOT 6B. PROVIDE RIP-RAP AS SHOWN FOR EROSION PROTECTION. SAME OWNER BOTH PROPERTIES. SEE DETAIL 11 - SHEET 2 OF 2.
- 7 INSTALL 16" DIAMETER CONCRETE PIPE DROP INLET WITH BEEHIVE GRATE TOP. SLOPE PAVING TO INLET FROM ALL DIRECTIONS. SEE DETAIL 5 - SHEET 2 OF 2.
- 8 CONSTRUCT 6" HIGH EXTRUDED CONCRETE CURB ON PAVEMENT PARKING AREAS. SEE DETAIL 1 - SHEET 2 OF 2.
- 9 PROVIDE 1' OPENING IN PARKING ISLAND FOR DRAINAGE. CONTINUE CONCRETE GUTTER THROUGH THIS AREA.
- 10 CONSTRUCT 2' WIDE STANDARD CURB AND GUTTER (SLOPE = 0.5%) SEE DETAIL 4 - SHEET 2 OF 2.
- 11 INSTALL TENSAR GEORID PER MANUFACTURER'S SPECIFICATIONS ON SLOPES INDICATED FOR EARTH STABILIZATION. APPLY FROM EDGE OF PAVEMENT TO TOE OF SLOPE. SEED AREA PER C.O.A. STANDARD SPECIFICATION SECTION 1011. CLASS F-1 (NO WATERING). USE #830 DRYLAND BLEND NATIVE SEED. APPLIED AT 2 LBS / 1000 SF. USE 16-8-8 CHEMICAL FERTILIZER APPLIED AT 4 LBS / 1000 SF.
- 12A TURNED DOWN WALK. SEE DETAIL 2 - SHEET 2 OF 2.
- 13 INSTALL NEW 12" DIA. ULTRA-RIB PVC STORM DRAIN BETWEEN DROP INLETS AND DETENTION POND. SEE SHEET 2 OF 2 FOR PROFILES / DETAILS.
- 14 INSTALL 84 LF POLYDRAIN SYSTEM TRENCH DRAIN IN ACCORDANCE WITH MANUFACTURER'S DETAILS. TOP WIDTH = 6.1 INCHES. RADIUS BOTTOMS WITH BUILT-IN SLOPE OF 0.60% GRATE TO BE IN-LAY TYPE. TRENCH SHALL DISCHARGE HORIZONTALLY INTO A 6" PVC STORM DRAIN PIPE.
- 15 6" PVC FROM TRENCH DRAIN TO STORM INLET.
- 16 CONNECT 1-8" ULTRA-RIB PVC OUTLET FROM THE DETENTION POND TO THE EXISTING STORM DRAIN MANHOLE. TAP TO EXISTING LINE AND GROUT FOR WATERTIGHT CONNECTION. SEE PROFILE / DETAILS SHEET 2 OF 2.
- 17 INSTALL 48" DIAMETER CONCRETE PIPE DROP INLET WITH 24" DIA. GRATE TOP. SLOPE PAVING TO INLET FROM ALL DIRECTIONS. SEE DETAIL 5 - SHEET 2 OF 2.
- 18 CONSTRUCT CONCRETE GRADE WALL FROM CURB RETURN TO CURB RETURN ON SOUTH SIDE OF EACH DRIVE ENTRANCE. 36 LF AT NORTH ENTRANCE AND 26 LF AT SOUTH ENTRANCE.
- 19 INSTALL 18" DIA. ULTRA-RIB PVC TO CARRY FLOWS BENEATH EACH DRIVE ENTRANCE. SEE DVG PLAN FOR INVERTS.
- 20 CONSTRUCT 6" HIGH STANDARD CHAIN LINK FENCE AND GATE PER C.O.A. DETAIL #2252. ALONG PERIMETER OF CONCRETE POND.

LEGEND

- SIDEWALK, CURB AND GUTTER (EXISTING, PROPOSED)
- PROPOSED ASPHALT
- BUILDING (EXISTING, PROPOSED)
- PROPERTY LINE
- EXISTING SPOT ELEVATION
- EXISTING CONTOUR
- PROPOSED SPOT ELEVATION
- PROPOSED CONTOUR
- SURFACE FLOW DIRECTION (EXISTING, PROPOSED)
- LANDSCAPED AREA
- TOP OF GRADE WALL (< 15' HIGH)
- TOP OF RETAINING WALL (> 15' HIGH)
- TOP OF ASPHALT
- TOP OF CURB
- FLOW LINE
- FINISHED FLOOR
- RIGHT OF WAY
- PROPERTY LINE
- POWER POLE
- CURB RETURN



VICINITY MAP N-15



FLOOD HAZARD MAP

RESUBMITTAL: 3/10/93

- ▲ REVISE HYDROGRAPH - SHEET 2 OF 2
- ▲ ADD INFO. RE: DETENTION POND
- ▲ PROVIDE FLOW RATE AND VELOCITY INFO. TO STORM DRAIN PROFILES (2 OF 2)
- ▲ ENERGY DISSIPATION NOTES ADDED (2 OF 2)
- ▲ DETENTION POND NOTES MODIFIED (2 OF 2)

Chris Weiss 3/10/93
CHRISTOPHER L. WEISS DATE

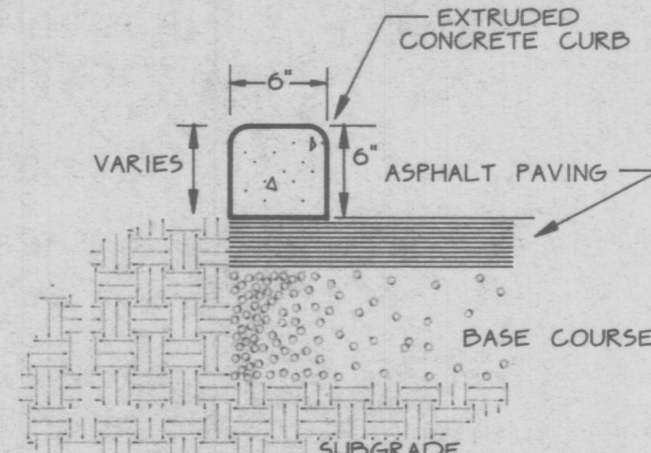


REVISIONS	DATE	BY	CHKD
1	3/10/93		
2			
3			

C.L. WEISS ENGINEERING, INC.
 POST OFFICE BOX 87 SANDIA PARK, N.M. 87047 - (505) 281-8800
 1100 ALVARADO DR NE ALBUQUERQUE, N.M. 87110 - (505) 266-3444



AIRBORNE DRAINAGE / GRADING PLAN

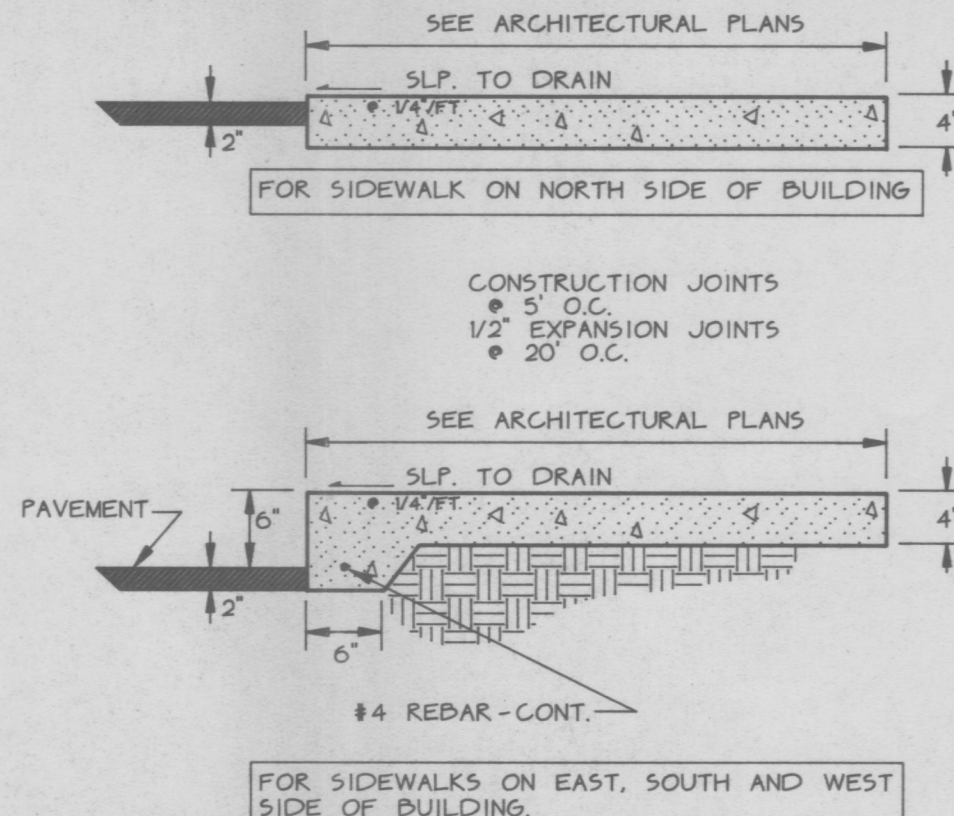


GENERAL NOTES

1. PROVIDE CONTRACTION JOINTS @ 10' O.C. MAX. ADJACENT TO BLDGS, WALLS AND CURB RETURNS
2. EDGES SHOULD BE REMOVED WITH 3/8" EDGING TOOL

1 EXTRUDED CONCRETE CURB

N.T.S.

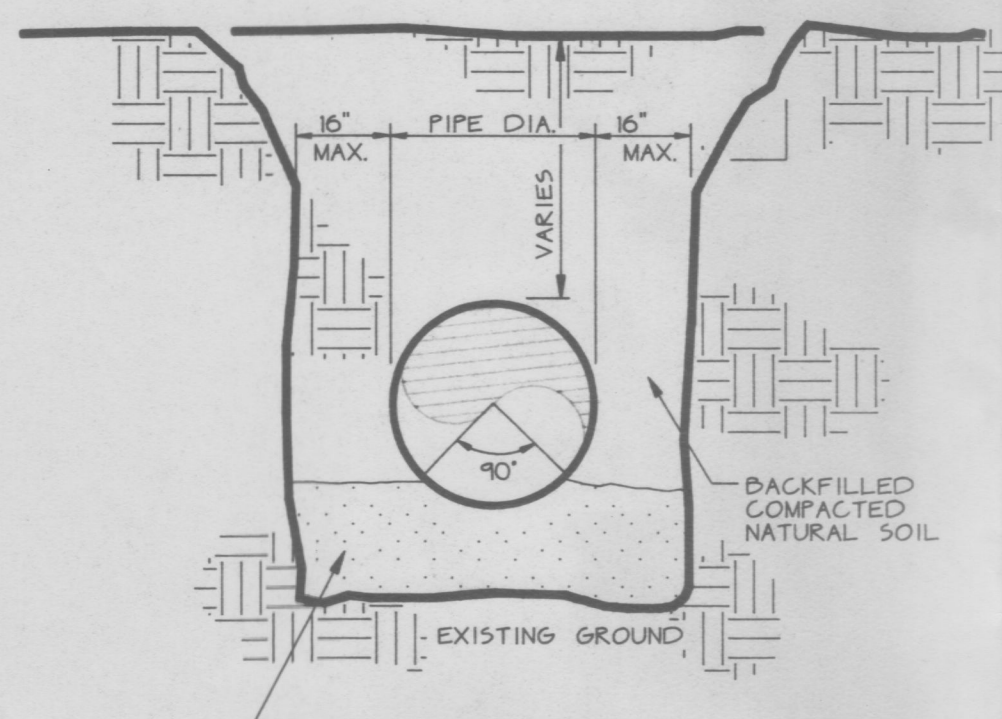


2 CONCRETE WALKS

N.T.S.

NOTES:

1. BACKFILL AREA SURROUNDING PIPE ON SIDES AND TOP 16" MAX WITH NATURAL SOIL MATERIAL. EXCLUDE ROCKS, LUMPS AND DEBRIS FROM BACKFILL MATERIAL.
2. GRANULAR BEDDING MATERIAL SHALL BE WELL GRADED WITH 100% PASSING THE 3/8" SIEVE AND NOT MORE THAN 10% PASSING THE NO. 200 SIEVE. MANY SITE SOILS MEET THIS SPECIFICATION.
3. PONDING OR JETTING PIPE BACKFILL WILL NOT BE PERMITTED.
4. THE PIPE SHALL BE PROTECTED BY A COVER OF AT LEAST 3" BEFORE PERMITTING HEAVY CONSTRUCTION EQUIPMENT TO PASS OVER DURING CONSTRUCTION STAGE.

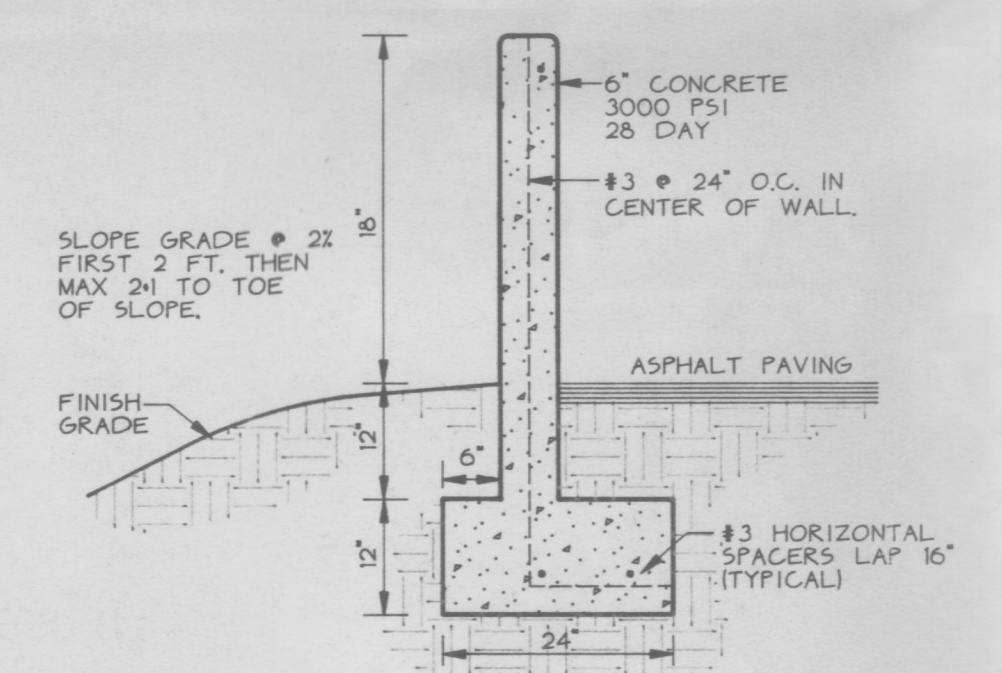


6 PIPE BEDDING + BACKFILL

N.T.S.

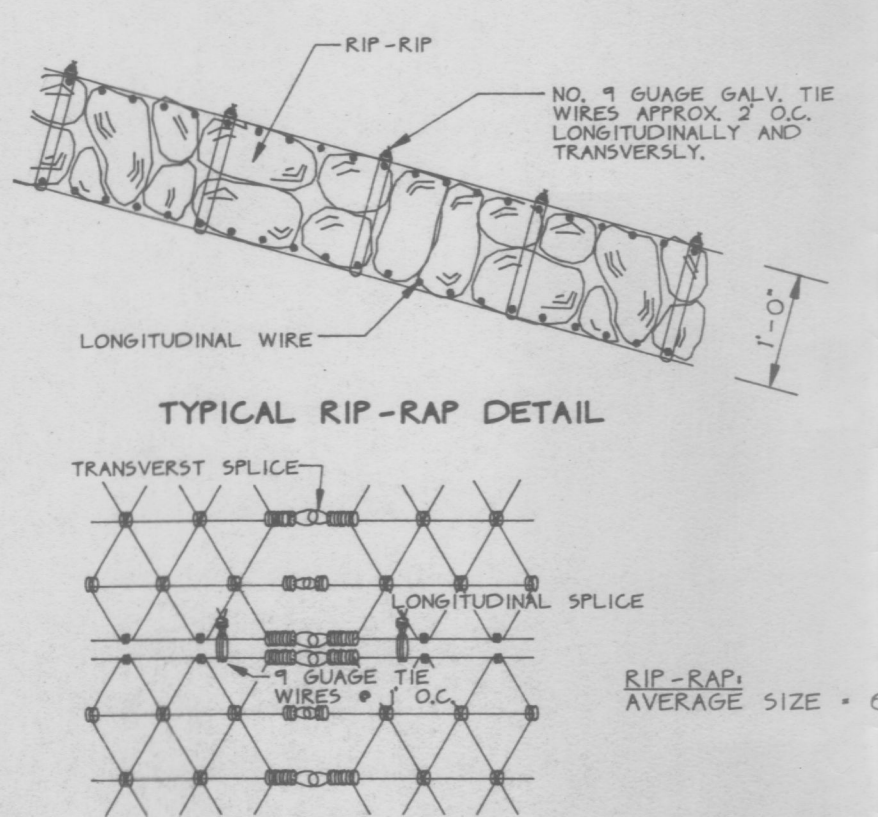
PROVIDE REFLECTIVE MARKERS ON EACH END OF WALL, DRIVEWAY SIDE.

PROVIDE 1" RADIUS EACH END



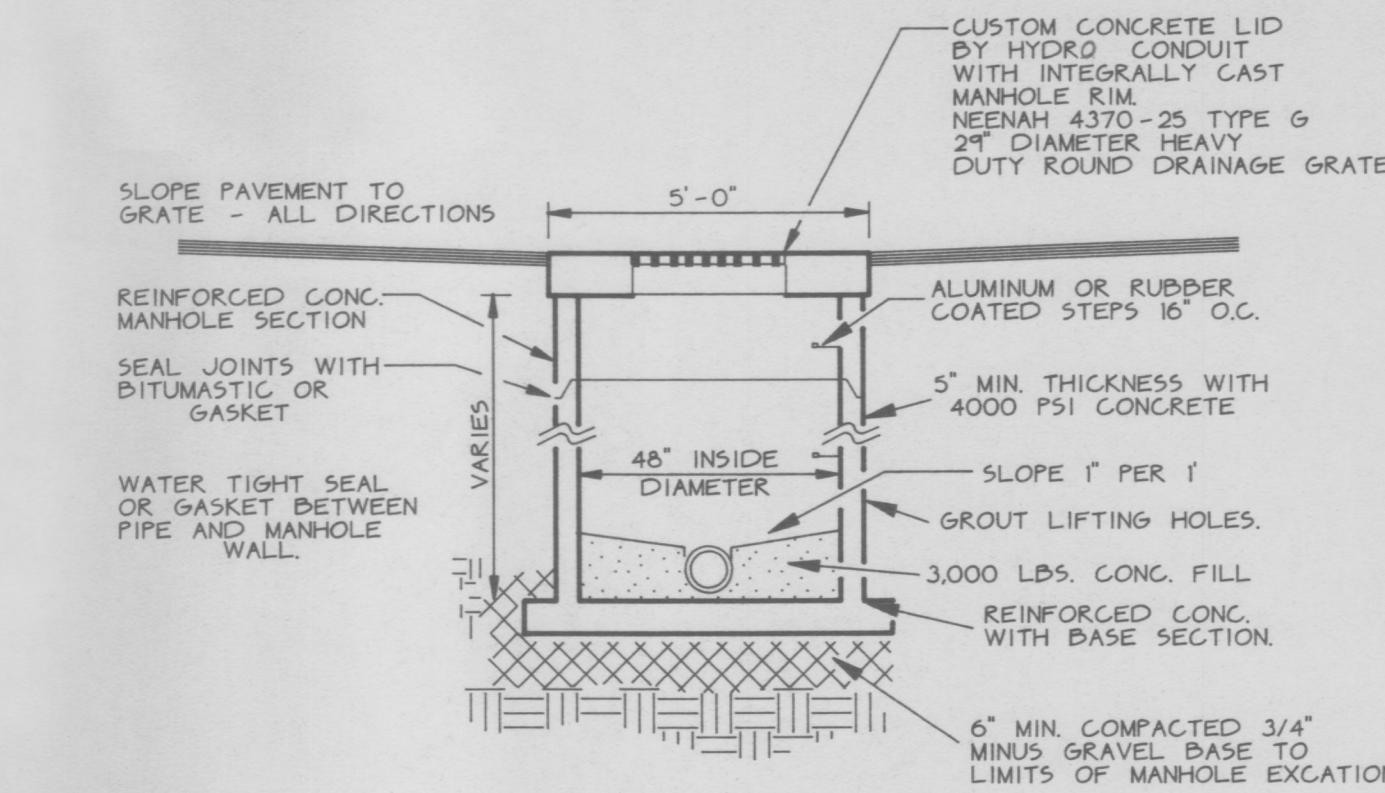
8 CONCRETE GRADE WALL

N.T.S.



11 WIRE ENCLOSED RIP-RAP

N.T.S.



3 DROP INLET

N.T.S.

ONSITE PRIVATE STORM DRAIN SYSTEM

The site drainage patterns are divided into two sub-basins - the north portion (0.71 Ac. - comprised of parking and a small amount of landscaped area) and the south area (1.31 Ac. - comprised of the roof area and the remainder of the parking). The flows from the north area will collect against the north curb bordering the parking area and be routed to the west to be collected by a single storm inlet functioning in a ponding condition. Flows from the south area will collect against the south parking curb and flow short distances to be collected by three storm inlets, all functioning in ponding conditions.

As a function of the percentage of each area, the approximate flows from each sub-basin will be:

North Area
55% of total, or 3.8 cfs, + 0.3 cfs offsite = 4.1 cfs to a single storm inlet

South Area
65% of total, or 7.0 cfs to three storm inlets. The storm inlet nearest the loading dock area will be subjected to at least one half of the total flows of the south sub-basin, or 3.5 cfs.

Grate Capacity
(Neenah Foundry Co. - Cat No. R 4370-25 type G, 29" diameter)

Based on the flow distributions for the site, the largest grate capacity will need to handle a minimum of 4.1 cfs. All the grate sizes will be standardized to facilitate construction of the inlets, with the size/capacity based on the minimum flow requirement.

For flow through a grate under ponding conditions, orifice type flow occurs. If the net open area is used as the orifice area, the discharge can be computed using the orifice equation $Q = CA(2gh)^{1/2}$, where C has a value of 0.60, A = area in sq. ft., g = the constant value 32.2, and h = depth in feet of water over the grate. For the above referenced grate, the clear opening space is 2.0 ft. Maximum depth of ponded water over the grate would be 0.5', which is a function of the curb height. Grate capacity would then equal 6.7 cfs. Reductions in the discharge due to trash accumulation, clogging or design variations could equal 30%, leaving an allowable capacity/grate of 4.7 cfs, which is greater than 4.1 cfs referenced above.

Storm Pipe Capacity

The north storm inlet will be intercepting flows from the south sub-basin, or a total of 7 cfs. Using Kutters Formula for pipes flowing full, an 12" dia Ultra-Rib PVC pipe has the capacity to carry 7 cfs for any slope greater than 1%. A 12" Ultra-Rib PVC installed at a minimum of 2.0% will handle the peak discharge draining directly into the south end of the detention pond. Available slope for the storm drain in this area approaches 25%.

The other three storm inlets will be intercepting flows from the south sub-basin, or a total of 7 cfs. Using Kutters Formula for pipes flowing full, an 12" dia Ultra-Rib PVC pipe has the capacity to carry 7 cfs for any slope greater than 1%. A 12" Ultra-Rib PVC installed at a minimum of 2.0% will handle the peak discharge draining directly into the south end of the detention pond. Available slope for the storm drain in this area approaches 35%.

Energy Dissipation at Detention Pond

Initial energy dissipation will be provided by 90° horizontal bend at pipe outlets (see plan view). When pond begins to fill with water, energy dissipation will be provided by backwater.

Detention Pond Capacity

Using a graphical design to size the detention pond, a simplified synthetic hydrograph for the design storm and site development is plotted, with the undeveloped flow rate (3.8 cfs) serving as the outflow rate from the pond into the existing storm drainage system. The volume of detention is obtained by calculating the area between the hydrograph and the superimposed outflow rate, or 9351 CF (see graphic). Depth of ponded waters will average 4.2' deep for the designated pond area of 2237 SF. The top of the pond wall on the south and east sides should be constructed a minimum of 4.7' high to provide for freeboard, while the west wall should be constructed 0.5' lower to provide for a spillway area.

Grate at outflow pipe to be Neenah Foundry Co. - Cat. No. R 4350 Beehive Grate in a 12" concrete pipe (bell end). The outflow pipe into the existing storm drain will be sized according to the orifice equation, $Q = CA(2gh)^{1/2}$, where C has a value of 0.60, and the head equals 4.2'. Solving for the area, $A = 0.29$ SF. Checking Kutters formula for pipe flowing full for slope greater than 10%, capacity = 10 CFS. Therefore, pipe friction loss is not a controlling factor. Inlet control will govern. Connect 1-8" Ultra-Rib PVC outlet from the detention pond to the existing storm drain. Cap pipe at inlet and drill a 7.8" diameter hole in pipe for orifice control.

TC = 12 MIN

$A_t = 2.7 \text{ ACRES (ON-SITE AND OFF-SITE)} = 117,925 \text{ SF}$

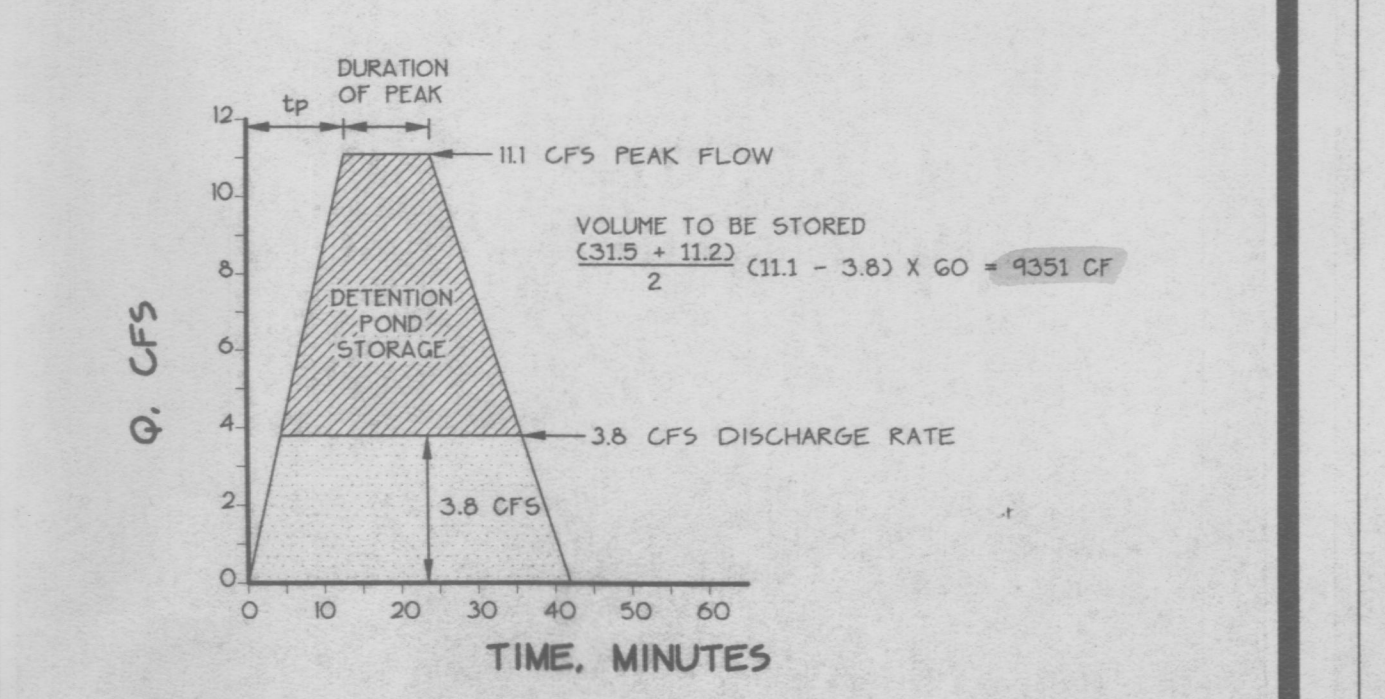
$E = (0.53)(11,325) + (0.78)(4150) + (1.13)(14,500) + (2.12)(87,950) = 1.80$

$117,925$

$tp = (0.7)(12) + 8 - \frac{(5)(2.02)}{2.71} = 12.7 \text{ min.}$

$tb = \frac{(121)(1.80)(2.71)}{11.1} - \frac{(15)(2.02)}{2.71} = 42 \text{ min.}$

$\text{DURATION OF PEAK} = \frac{(15)(2.02)}{2.71} = 11.2 \text{ min.}$



HYDROGRAPH

SCOPE:

The proposed improvements will be the new facilities for Airborne Express and will consist of the administration building and package handling area, employee/customer parking and access drives to University Blvd.

The present site is designated as Lot 6B-2 of the Airport Technical Center and is an undeveloped tract of land consisting of uneven topography with an overall drop to the west toward the University Golf Course. The adjacent lots to the north and south are also part of the subdivision and are presently undeveloped. University Blvd., a paved two-lane street without curb and gutter, borders the east side of the site. Utilities in the area consist of a water main located within the University Blvd. R/W, with a sanitary sewer and storm drain located within a 40 foot wide easement along the west side of the site.

The intent of this plan is to show:

- Grading relationships between the existing ground elevations and proposed finished elevations in order to facilitate positive drainage to designated discharge points.
- The extent of proposed site improvements, including buildings, walks and pavement.
- The flow rate/volume of rainfall runoff across or around these improvements and methods of handling these flows to meet City requirements for drainage management and the previously approved master drainage plan for the Airport Technical Center.
- The relationship of onsite improvements with existing neighboring property to insure an orderly transition between proposed and surrounding grades.

DRAINAGE PLAN CONCEPT:

Runoff within the site will be routed to inlets located within the parking areas for collection by a private storm drainage system. The flows will then be routed to a detention pond situated at the southwest corner of the lot before being released into the existing storm drain, which is located along the west side of the site. The use of a detention pond is necessary to release the developed runoff at the current undeveloped rate to comply with the approved master drainage plan for the Airport Technical Center.

GENERAL NOTES:

LEGAL: Lot 6B-1, Airport Technical Center, Bernalillo County, NM.

SURVEYOR: Jeff Mortensen and Associates

B.M. City of Albuquerque benchmark (2-N16), a standard C.O.A. brass cap set in concrete monument stamped "2-N16" and projecting 0.1 ft. above ground near the SW corner of Albuquerque International Airport in an open prairie. Elev. = 5304.88 ft. (M.S.L.D.)

T.B.M. Railroad spike in power pole. Elev. = 5200.94 ft. (M.S.L.D.)

SOILS: The SCS Soil Survey of Bernalillo County indicates that the soil is (Cu), cut-and-fill land, a sandy loam and very gravelly sand.

FLOOD HAZARD: Per FEMA Floodway maps, the property does not lie within a flood zone.

OFF-SITE DRAINAGE: Approximately 0.26 acres of undeveloped land north of the site drains across the site. These flows will be temporarily routed through the site for discharge via the proposed improvements. Future development of the adjacent area will isolate this site from the effects of these minor flows.

EROSION CONTROL: The contractor is responsible for containing all sediment generated during construction by means of a temporary earthen berm or silt fence located at the lowest point near the southwest corner of the site.

CALCULATIONS:

Calculations are based on the *Development Process Manual, Vol. 2 Design Criteria*, August, 1991. Design based on a 100 year, 6-storm, in Precipitation Zone 2.

AREA OF SITE:

Area of site = 2.4471 Ac.

SITE	
Undeveloped Land Conditions	Developed Land Conditions
$A_t = 106,600 \text{ SF}$	$A_t = 0 \text{ SF}$
$A_g = 0 \text{ SF}$	$A_g = 4,150 \text{ SF}$
$A_c = 0 \text{ SF}$	$A_c = 14,500 \text{ SF}$
$A_d = 0 \text{ SF}$	$A_d = 87,950 \text{ SF}$
TOTAL = 106,600 SF	TOTAL = 106,600 SF

Onsite Weighted Excess Precipitation (100-Year, 6-Hour Storm-Precipitation Zone 2):

Weighted E = $E_{A_t}A_t + E_{A_g}A_g + E_{A_c}A_c + E_{A_d}A_d$

$A_t = 106,600$
 $A_g = 4,150$
 $A_c = 14,500$
 $A_d = 87,950$

Undeveloped = $(0.53)(106,600) + (0.78)(4,150) + (1.13)(14,500) + (2.12)(87,950) = 0.53$

Developed = $(0.53)(0) + (0.78)(4,150) + (1.13)(14,500) + (2.12)(87,950) = 1.93$

Undeveloped Volume of Runoff:

$V_{360} = (0.53)(106,600) = 4,708 \text{ CF}$

Developed Volume of Runoff:

$V_{360} = (1.93)(106,600) = 17,145 \text{ CF}$

Onsite Peak Discharge Rate:

$Q_p = Q_{pA_t} + Q_{pA_g} + Q_{pA_c} + Q_{pA_d}$

Undeveloped = $(1.56)(106,600) + (2.28)(4,150) + (3.14)(14,500) + (4.70)(87,950) = 43,560$

Developed = $(1.56)(0) + (2.28)(4,150) + (3.14)(14,500) + (4.70)(87,950) = 10.8 \text{ CFS}$

Offsite Land Condition

$A_t = 11,325 \text{ SF}$
 $A_g = 0 \text{ SF}$
 $A_c = 0 \text{ SF}$
 $A_d = 0 \text{ SF}$

TOTAL = 11,325 SF

Offsite Peak Discharge Rate:

$Q_p = Q_{pA_t} + Q_{pA_g} + Q_{pA_c} + Q_{pA_d}$

Offsite = $(1.56)(11,325) + (2.28)(0) + (3.14)(0) + (4.70)(0) = 0.3 \text{ CFS}$

TOTAL FLOWS:

Peak Flow To Detention Pond:

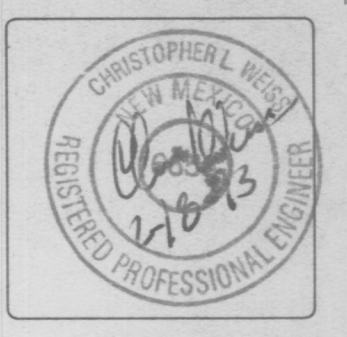
10.8 cfs onsite
0.3 cfs offsite
11.1 cfs total

9 NORTH STORM DRAIN PROFILE

N.T.S.

10 POND STORM DRAIN PROFILE

N.T.S.



REVISIONS	DATE	BY	CHKD
1-5	3/16/93	DJP	DJP
		DJP	CLW

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