359.03 copy 2 Amole Del Norte Storm Drainage Facilities - Tower/Sage Drainage Master Plan (Draft) Andrews, Asbury & Robert, Inc. Andrews, Asbury & Robert, 1995



# CITY OF ALBUQUERQUE NEW MEXICO

# AMOLE DEL NORTE STORM DRAINAGE FACILITIES

TOWER/SAGE
DRAINAGE MASTER PLAN

ANDREWS, ASBURY & ROBERT, INC.
CONSULTING ENGINEERS
ALBUQUERQUE, NEW MEXICO

LIBRARY

Tower Dage - their new AHARO GOT Tiena Bayeta (north 1/3 of ADNC bain) - AAR Tower dage (new upont) - updated topo for T/S from KTi t - small sliver drains to Snow Visto (back to the west) OK?

- 5 are tracts from 1944

Clift OK I - helf of area is in County; they should review and be aware of this \* - need to show any floodplains on mos \* - all areas (FEMA) approard (9x capt for 5 \$ 7 NAA) need to show new revisions X - land treatments are low (30-50% B??) - what about affect @ ADC??

# CITY OF ALBUQUERQUE NEW MEXICO

#### AMOLE DEL NORTE STORM DRAINAGE FACILITIES

### TOWER/SAGE DRAINAGE MASTER PLAN

**APRIL 1995** 

Prepared By

ANDREWS, ASBURY & ROBERT, INC. 149 Jackson Street, N.E. Albuquerque, New Mexico 87108

# City of Albuquerque

## TOWER/SAGE DRAINAGE MASTER PLAN

#### **TABLE OF CONTENTS**

1.0		o. 1, Vicinity Map	
2.0	DRAIN	IAGE AREA BOUNDARIES	4
3.0	3.1 3.2 3.3 3.4	IAGE CHARACTERISTICS Topography Soils and Vegetation Land Use Platting Annexation	6 6 6 7
4.0	EXIST	ING DRAINAGE FACILITY	8
5.0	FLOO	D PLAINS	10
6.0	Table	OLOGY	12
	Table	and Volumes"	
7.0	PROP 7.1 7.2 7.3	OSED STORM DRAINAGE SYSTEM Storm Drains Hydraulics Tower Detention Pond/Neighborhood Park Figure No. 1, "Conceptual Layout, Tower Pond & Neighborhood	23 24
		Park	27
8.0	RIGH 8.1 8.2	T-OF-WAY Tower Detention Pond/Neighborhood Park Sage Road Storm Drain	29
9.0	CONC 9.1 9.2	CLUSIONS	31

#### TABLE OF CONTENTS - CONTINUED

10.0	EXISTING DRAINAGE DATA - REFERENCES	33
11.0	ESTIMATED CONSTRUCTION COSTS	36
APPE	ENDIX A, AHYMO Summary Tables	<b>4-1</b>
APPE	ENDIX B, Parks & General Services Letter	3-1
BACK	K POCKET: Map No. 2, "Drainage Area Map" Map No. 3, "Storm Drain System Map"	

#### City of Albuquerque

#### TOWER/SAGE DRAINAGE MASTER PLAN

#### 1.0 INTRODUCTION

The Tower/Sage Drainage Basin is a sub-basin of an overall drainage area known as the Amole Del Norte Drainage Basin located on the West Mesa in the southwest quadrant of the Albuquerque metropolitan area. (See enclosed Vicinity Map, Map No. 1)

In February 1985, Boyle Engineering, Inc. submitted the Design-Development Report for the Evaluation Study of the Amole Del Norte Diversion Facility and the plan presented in such report was adopted by the City of Albuquerque as the Master Drainage Plan for the Amole Del Norte Drainage Basin.

The Amole Del Norte Drainage Basin, which encompasses an area of approximately 6.6 square miles can be broken down into three sub-basins and are identified as follows:

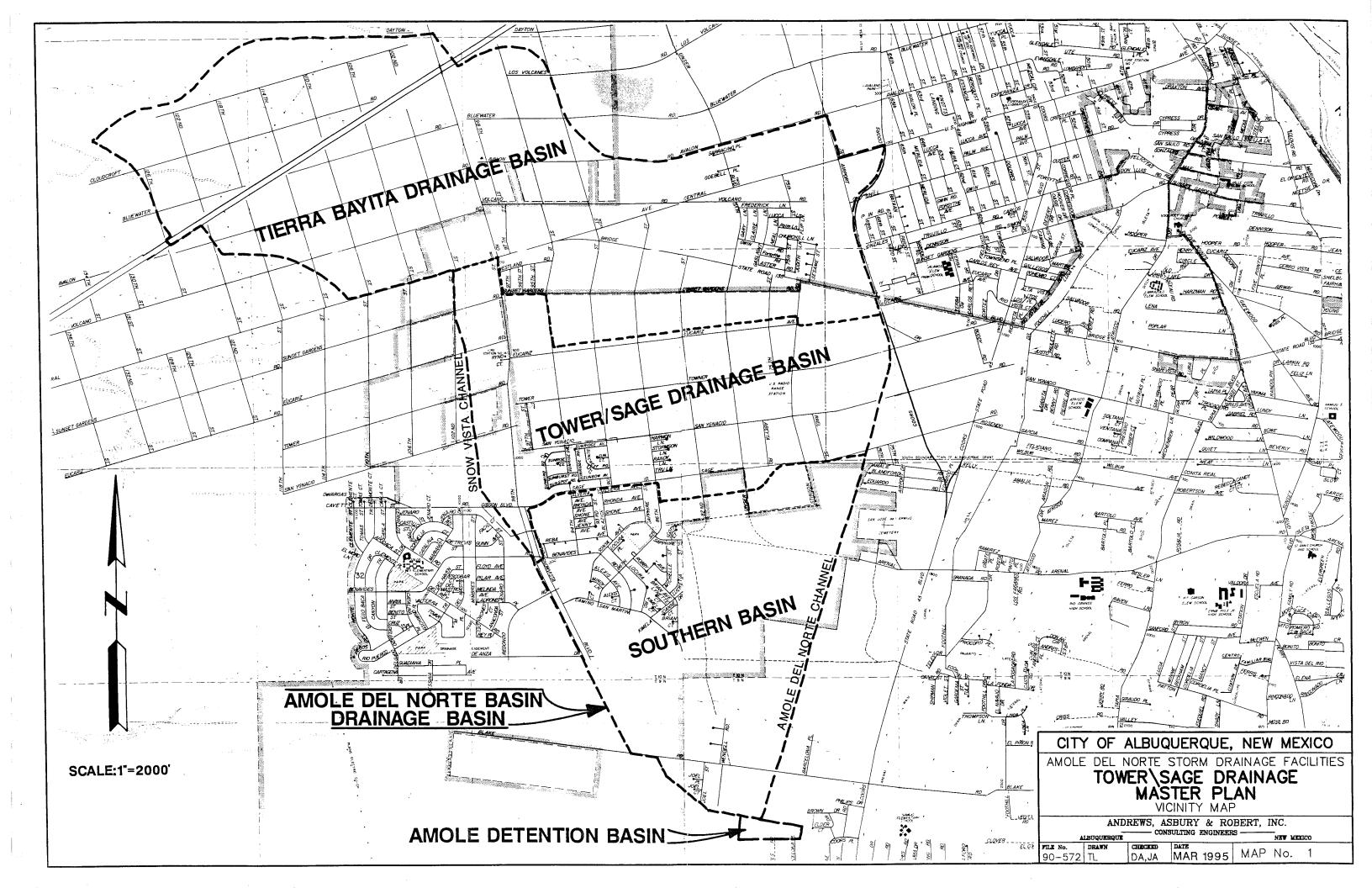
- The Tierra Bayita Drainage Basin The northern sub-basin of the
   Amole Del Norte Basin
- The Tower/Sage Drainage Basin The middle sub-basin of the
   Amole Del Norte Basin
- The Southern Basin
   The southern sub-basin of the
   Amole Del Norte Basin

The analysis presented in the Boyle Engineering report was utilized in the design and construction of the Amole Del Norte Channel. This channel is to carry the storm water runoff from the overall Amole Del Norte Drainage Basin. Subsequent to the Boyle Engineering Report, and the construction of the Amole Del Norte Channel, the City of Albuquerque adopted revised hydrology standards called AHYMO (Albuquerque Hydrologic Model). This AHYMO standard creates substantially more runoff from drainage basins than the standard previously used. It is, therefore, necessary to re-analyze the drainage basins being served by the Amole Del Norte Channel, and to prepare a plan to manage the storm water runoff.

Greiner Inc. has developed a refined drainage plan including proposed drainage facilities for the Tierra Bayita Drainage Basin. The facilities proposed were to be constructed in four phases. Two of these four phases have been constructed, with the remaining two phases planned to be completed by December 1996. The southern basin remains as presented in the Boyle Engineering, Inc. report and has not been refined or updated as of this date.

This Tower/Sage Drainage Master Plan is prepared to re-evaluate the runoff generated by the Tower/Sage Drainage Basin utilizing the current AHYMO hydrology standard and to present proposed facilities, as necessary, to accommodate the rate and volume of runoff, and to deliver the runoff to the Amole Del Norte Channel at an acceptable rate so as not to exceed the channel's capacity.

In addition, the City of Albuquerque presently has a Special Assessment District (SAD-222) project in progress for the construction of infrastructure improvements within the westerly portion of the Tower/Sage Drainage Basin. This master plan of drainage is to provide a method for managing the storm drainage from the City's SAD 222 project that is consistent with an overall drainage plan for the basin.



#### 2.0 DRAINAGE AREA BOUNDARIES

The basin boundaries are generally described as bounded on the east by the Amole Del Norte Channel; on the west by the Snow Vista Channel; on the north by the southerly boundary of the Tierra Bayita Basin; and, on the south, generally by Sage Road. Map No. 2, included in the back pocket of this report, shows the drainage area boundaries of the Tower/Sage Drainage Basin under the proposed, developed conditions.

The limits of the developed Tower/Sage Drainage Basin were determined primarily from information provided in the "Design-Development Report for the Re-evaluation Study of the Amole Del Norte Storm Diversion Facility." The "Improved Conditions Report for Amole Watershed Drainage Management Plan" was also used; however, to a lesser degree.

Updated topography of the Tower/Sage Basin area dated April 1991 was obtained from Resources Technology, Inc., who are currently preparing a restudy report of the area for FEMA. Based on the updated topography along with reviewing the existing platted streets, some adjustments to the previous boundary have been made:

- 2.1 The northwest corner of the boundary was modified by down-sizing sub-basin A1-D. A meeting was held with AMAFCA (Albuquerque Metropolitan Arroyo Flood Control Association) drainage engineer, and it was determined that the area west of 102nd Street could become part of the Amole Drainage Basin and allowed to drain into the Snow Vista Channel without significantly affecting the channel capacity.
- 2.2 Area A8-D, located east of 98th Street between Sunset Gardens Road and Eucariz Avenue, was made a part of the Tower/Sage Basin for practical topographic reasons. This area slopes easterly to 94th Street and then 94th

- Street slopes to Eucariz Avenue which lies within the Tower/Sage Basin. Previously, A8-D was a portion of the Tierra Bayita Basin.
- 2.3 At the northeast corner of the basin, the area between Bridge Boulevard and north of sub-basin A16-D was placed in the Tierra Bayita Basin. This area slopes steeply to the north and presently drains to the Tierra Bayita Channel.
- 2.4 The southern boundary was modified slightly by including a 400-strip south of Sage Road to sub-basins S5-D, S6-D, S7-D, and S8-D. The 400-foot wide strip is relatively flat and, when developed, could drain to Sage Road.

#### 3.0 DRAINAGE BASIN CHARACTERISTICS

#### 3.1 TOPOGRAPHY

The Tower/Sage Drainage Area generally slopes from the northwest to the southeast and has a surface gradient varying from approximately 1.5 percent to 3 percent. The upper northwesterly portions have the steeper slopes. A natural playa currently exists east of Unser Boulevard and west of Stinson Street. Also, fairly steep slopes occur in the far east portion of the drainage basin. The topography of the area is shown on Map No. 2 included in the back pocket of this report.

#### 3.2 SOILS AND VEGETATION

The major portion of the soils within the drainage basin consist of hydrologic Soil Group A and Soil Group B. Generally, Group A soils occur on the westerly portion of the basin in the vicinity of 98th Street and on the far easterly portion of the basin on the steeper slopes directly west of the Amole Del Norte Channel. The remainder of the area consists of Group B soils.

Existing vegetation is relatively sparse throughout the area and consists of an opentype desert grassland. Generally, vegetative coverage is estimated at less than 20 percent. Under developed conditions, it is anticipated that the area will be covered with hard surfaces and various types of landscaping that are consistent with the Land Use proposed in the Tower/Unser Sector Development Plan.

#### 3.3 LAND USE

Under existing conditions, approximately 90 percent of the Tower/Sage Basin area is currently undeveloped. Some development exists adjacent to 98th Street with most of this development near Sage Road at the southwest corner of the basin.

For drainage purposes, developed conditions of the Tower/Sage Drainage Basin assumes development occurring in accordance with zoning and land use presented in the Tower/Unser Sector Development Plan. The majority of the zoning presented in this sector plan provides for residential uses ranging from single family homes to multi-family units up to 20 dwelling units per acre. Proposed commercial and office zoning is minimal within the basin and is limited to areas near the major roadway intersections.

#### 3.4 PLATTING

The major portion of the land in the Tower/Sage Basin area was originally subdivided in 1944, as part of the Town of Atrico Grant. This original subdivision divides the land on a grid into 25-acre blocks separated with public rights-of-way. Each block generally contains five rectangular parcels of approximately five acres, each measuring approximately 204 feet by 1067 feet. Generally, there are separate owners for each five acre parcel, although some individuals own multiple tracts. Replatting in the area is mostly limited to some lands adjacent to 98th Street and at the southwest corner of the basin, east of 98th Street and north of Sage Road.

#### 3.5 ANNEXATION

The westerly portion of the drainage basin consisting of approximately 60 percent of the basin area has been annexed and is currently within the City of Albuquerque municipal limits. The easterly and remaining portion of the basin remains outside the municipal limits. A line designating the municipal limits generally extends north-south through the basin just east of 86th Street.

#### 4.0 EXISTING DRAINAGE FACILITIES

Historically, the drainage areas impacting the Tower/Sage drainage basin from the west were relatively large. However, the construction of the Snow Vista Drainage Channel (concrete-lined) aligned north-south and located approximately 1000 feet west of 98th Street has intercepted and diverted the major historic storm water flows south to the Amole Arroyo and Amole Detention Basin, and away from the Tower/Sage drainage area. This Snow Vista Channel, therefore, determines the west boundary of the basin.

The Amole Del Norte Storm Diversion Facility, located at the east boundary of the drainage basin, consists of a sedimentation basin from Bridge Boulevard to Tower Road, then drains to a concrete-lined channel that begins at Tower Road and Coors Road, then extends southerly varying from approximately 300 feet to 1300 feet west of Coors Road and discharges into the Amole Detention Basin to the south. This facility was installed in 1989 and 1990 and serves as the outlet for the Amole Del Norte Drainage Basin.

Recently, a drainage channel to serve the northerly adjacent Tierra Bayita Drainage Basin was constructed along the southerly side of Bridge Boulevard and extends westerly from the Amole Del Norte Diversion Channel Sedimentation Basin. This channel intercepts flows from the Tierra Bayita Basin and serves as the north boundary of the Tower/Sage Basin along its easterly reaches.

At the present time, no drainage facilities exist within the basin itself. The drainage in the basin is basically natural and follows the terrain which slopes from west to east.

The City's recent adoption of AHYMO (Albuquerque Hydrologic Model) as its hydrology standard has caused many of its existing storm drainage systems to be undersized and the Amole Del Norte Channel is one of these systems. This channel

was designed from hydrology developed as part of the "Design Development Report for the Re-Evaluation Study of the Amole Del Norte Storm Diversion Facility" in 1985. The recently adopted AHYMO computer program, together with smaller sub-basin delineation, produces flows considerably higher than flows generated using the older HYMO computer program. Therefore, a drainage plan is required to be developed to control the flows from the drainage basins that are served by the Amole Del Norte Channel so that the capacity of the channel is not exceeded.

#### 5.0 FLOOD PLAINS

In reviewing the flood boundary and floodway maps for the City of Albuquerque, New Mexico, Bernalillo County (Panel 32 of 50 Community-Panel Number 350002 0032 and Panel 33 of 50 Community-Panel Number 350002 0033) dated October 14, 1983, flood plains are shown to exist on properties in the drainage area. Since the construction of the Snow Vista Channel in 1987, there has been no Letter of Map Revision made for this area. A "Draft-Flood Insurance Restudy Report for Six Areas Within the City of Albuquerque, Bernalillo County, New Mexico Community Number 350002," December 1993 is currently being reviewed by FEMA; however, comments on this restudy report have not been received from FEMA at the time of the writing of this report. The proposed drainage plan, when implemented, will remove the flood plains from the basin.

#### 6.0 HYDROLOGY

Frequency flows were quantified using the latest version of the computer program AHYMO (January 1994) according to "Section 22.2 Hydrology of the Development Process Manual, Volume 2, Design Criteria for the City of Albuquerque, New Mexico," January 1993. For the purpose of this master drainage plan, only fully developed conditions were considered in the computer model.

Rainfall amounts for the frequency events were derived from the NOAA Atlas and as shown in "Section 22.2 Hydrology of the Development Process Manual, Volume 2, Design Criteria for the City of Albuquerque, New Mexico, January 1993," Figures C-1, C-2, and C-3. Sub-basin boundaries were generally broken down into the platted blocks; however, in certain instances, topographic features were considered to determine appropriate boundaries. Sub-basin areas were computed from a 1" = 500' orthophoto topographic map that was produced from April 1991 photography. Land uses were determined from the recommended zoning documented in the "Tower/Unser Sector Development Plan." Time of concentrations were calculated using the SCS Upland Method.

Table 1, included hereinafter, links the recommended zoning provided in the "Tower/Unser Sector Development Plan" to the appropriate land treatments used in the AHYMO computer model. Table 2, herein, contains the AHYMO basin parameter worksheet together with peak flows and volumes for each sub-basin.

Table 3 presents peak flows and volumes at each analysis point as shown on Map No. 2. AHYMO Output Summary Tables are included in Appendix A of this report. Detailed computer printouts of the AHYMO Model are available for observation at the offices of Andrews, Asbury, & Robert, Inc.

TABLE 1
TOWER/SAGE DRAINAGE MASTER PLAN
LAND TREATMENTS

		LAND TRE	ATMENTS	
ZONE DESIGNATION	"A"	"B"	"C"	"D"
RESIDENTIAL				
R-1		50		50
R-T		35		65
R-D (9 UNITS/ACRE)		40		60
R-D (14 UNITS/ACRE)		35		65
R-D (20 UNITS/ACRE)		30		70
R-2		30		70
OFFICE				
0-1		20		80
COMMEDIAL				
COMMERCIAL				
C-1		10		90
C-2		10		90

NOTE: ZONING TAKEN FROM TOWER/UNSER SECTOR DEVELOPMENT PLAN

TABLE 2
TOWER/SAGE DRAINAGE MASTER PLAN
AHYMO BASIN PARAMETER WORKSHEET
PEAK BASIN FLOWS AND VOLUMES

(ALL FLOWS & VOLUMES INCLUDE A 5% BULKING FACTOR)

_									 																			
100 YEAR	RUNOFF	VOLUME	(24hr.)	(ac.ft.)				5.2				4.2				4.3			7	5				4.4				4.0
100	PEAK	FLOW	(6hr.)	(cfs)				112				96				103			5	2				103				92
10 YEAR	RUNOFF	VOLUME	(24hr.)	(ac.ft.)				3.2				2.6				2.6			33	2.0				2.6				2.3
9	PEAK	FLOW	(6hr.)	(cfs)				70				59				62			0	S				61		_	·•!	54
		_		۵				76				70				65			C	3				60				20
		ATMEN	[	٥										<u>-</u>														
		LAND TREATMENT	%	8	-			24				30				35			Ę	2				6				22
		ב		A												-			*						M	•		
			T(p)	(hr.)	0.05	90.0	0.03	0.15	0.03	0.03	0.08	0.14	0.04	900	0.03	0.12	0.03	0.03	0.08	2	0.04	90.0	0.04	0.14	0.04	90.0	0.04	0.14
			T(c)	(hr.)	0.08	0.09	0.05	0.22	0.05	0.05	0.12	0.21	90'0	800	40.0	0.18	0.05	0.05	0.12	0.22	90.0	0.10	90.0	0.21	900	0.10	0.00	0.21
			VEL	(fps)	4.	1.55	5.00		1.21	4.93	2.32		66.0	900	4.65		121	4.24	2.32		66.0	2.75	4.24		66.0	2.75	4.24	
				ᅩ	1.0	2.0	3.0		 0.7	3.0	3.0		2.0	30	3.0		20	3.0	3.0		2.0	3.0	3.0		0.7	3.0	3.0	
			SLOPE	(%)	2.00	09.0	2.78		3.00	2.71	09.0		2.00	6	2.40		3 00	2.00	09:0		2.00	0.84	2.00		2 00	0.84	2.00	
		ELEV.	DIFF.	(#.)	8.0	3.0	25.0		0.9	23.0	6.0		40	6	18.0		6.0	16.0	6.0		4.0	8.0	18.0		40	8.0	18.0	
			LENGTH	(ft.)	400	200	006		200	820	1000		200	0	220		200	800	1000		200	920	06		200	920	006	
			AREA	(sq.mi.)	0.0458			TOTAL =	0.0395			TOTAL =	0.0419			TOTAL =	0.0439		- 14101	200	0.0452			TOTAL =	0.0452			TOTAL =
			AR	(ac.)	29.3				25.3				26.8				28.1		æ		28.9	-			28.9			
				BASIN	A1-D				A2-D				A3-D	!			A4-D				AS-D				A6-D			

SEE MAP NO. 2 FOR BASIN IDENTIFICATION

SEE MAP NO. 2 FOR BASIN IDENTIFICATION

TABLE 2
TOWER/SAGE DRAINAGE MASTER PLAN
AHYMO BASIN PARAMETER WORKSHEET
PEAK BASIN FLOWS AND VOLUMES

(ALL FLOWS & VOLUMES INCLUDE A 5% BULKING FACTOR)

_								1	 			П				T							_							_
100 YEAR	RUNOFF	VOLUME	(24hr.)	(ac.ff.)				1.8				6.1			6	9.0				6.0					1.0					4.4
100	PEAK	FLOW	(6hr.)	(cfs)				\$				119			}	57				23					23					9
10 YEAR	RUNOFF	VOLUME	(24hr.)	(ac.ft.)				1.0				3.7			l (	0.5				0.5					9.0				,	2.5
10	PEAK	FLOW	(6hr.)	(cfs)				22				73			,	13				13					4					26
		L		۵				20				70			í	22				20					76					76
		LAND TREATMENT		٥																	-									
		IND TRE	8	В				20				30				3				22					24					24
		בן		٨																										
			T(p)	(hr.)	0.05	0.05	0.04	0.14	0.04	0.04	0.11	0.19	70.0	5 6	5 :	0.11	0.03	0.04	00.00	0.08	L C	50.0	0.05	0.01	0.12		) (	90.0	0.0	0.14
			T(c)	(hr.)	20.0	0.07	0.06	0.21	90.0	0.05	0.17	0.28	0 11	י ני	20.1	0.17	0.05	90.0	0.01	0.12	6	0.0	0.08	0.02	0.18	80.0		0.08	0.05	0.21
			VEL	(fps)	0.57	1.50	4.24		0.99	4.58	2.08		0 49	9 7	n č		0.81	4.24	4.24		i	C.)	3.42	3.00		0.70	) (	3.3/	3.33	
				¥	0.7	3.0	3.0		0.7	3.0	3.0		0.7	; c	) )		0.7	3.0	3.0			0.	3.0	3.0		0.7	. (	3.0	3.0	
			SLOPE	(%)	19.0	0.25	2.00		2.00	2.33	0.48		0.50	2 6	¥ ;		1.33	2.00	2.00		(	0.50	6. 8.	1.00		5		1.26	1.23	
		ELEV.	DIFF.	(ft.)	1.0	1.0	18.0		4.0	21.0	0.9		<b>C</b>	, ,	0.77		2.0	18.0	2.0			) )	13.0	2.0		2.0	) (	12.0	0.8	
			LENGTH	(ft.)	150	400	006		200	006	1250		2000	8 8	3		150	006	100		9	3	1000	200		000	3 1	920	650	
			AREA	(sq.mi.)	0.0206			TOTAL =	0.0570			TOTAL =	0.0102	10.0		TOTAL =	0.0102			TOTAL =		0.0086			TOTAL =	0.0359	}			TOTAL =
	`		AF	(ac.)	13.2				36.5				5 9	3			6.5					o.0				23.0	2			
				BASIN	A7-D				A8-D				0	2			A10-D					A11-D				A12.D	)			

SEE MAP NO. 2 FOR BASIN IDENTIFICATION

TABLE 2
TOWER/SAGE DRAINAGE MASTER PLAN
AHYMO BASIN PARAMETER WORKSHEET
PEAK BASIN FLOWS AND VOLUMES

(ALL FLOWS & VOLUMES INCLUDE A 5% BULKING FACTOR)

														10)	10 YEAR	100	100 YEAR
														PEAK	RUNOFF	PEAK	RUNOFF
				ELEV.						2	ND TRE	LAND TREATMENT		FLOW	VOLUME	FLOW	VOLUME
	AR	AREA	LENGTH	DIFF.	SLOPE		VEL	T(c)	T(p)		(%)			(6hr.)	(24hr.)	(6hr.)	(24hr.)
BASIN	(ac.)	(sq.mi.)	(ff.)	(ft.)	(%)	¥	(fps)	(hr.)	(hr.)	٨	В	ပ		(cfs)	(ac.ft.)	(cfs)	(ac.ft.)
							3		, 0								
A13-D	28.9	0.0452	500	3.0	1.50	). O	98.0	9 5 5	0.04								
			1000	3.0	0.30	3.0	1.64	0.17	0.11								
101			820	7.0	0.82	3.0	2.72	60.0	90.0			-					
		TOTAL =						0.32	0.21		8	+	93	52	2.8	86	4.6
							;		;								
A14-D	28.9	0.0452	<u>0</u>	0.5	0.17	0.	0.41	0.20	0.14								
			1000	4.0	0.40	3.0	96.	0.15	0.10								
			800	1.0	0.13	3.0	1.06	0.21	0.14								
		TOTAL =						0.56	0.37		8		20	39	2.9	63	4.8
					•			,	!							·	
A15-D	16.2	0.0253	8	0.	0.50	0.7	0.49	0.11	0.07								
			950	4.0	0.42	3.0	1.95	41.0	60.0	•							
			300	1.0	0.33	3.0	1.73	0.05	0.03								
		TOTAL =						0.30	0.20		8	+	8	28	4.1	84	2.5
A16-D	40.8	0.0638	200	0.5	0.25	0.7	0.35	0.16	0.11		J.,240						
			920	1.0	0.11	3.0	0.97	0.27	0.18			<u>_</u>					
-			200	3.0	09:0	3.0	2.32	90.0	0.04								
			1250	56.0	4.48	3.0	6.35	0.05	0.04								
		TOTAL =						0.54	0.36		20		20	£	3.2	92	5.6
						i		,								·	
A17-D	6.9	0.0108	50	3.0	5.00	0.7	0.99	0.0	0.03								
			8	14.0	1.56	3.0	3.74	0.07	0.04				•				
			9	0.	9.	3.0	3.00	0.01	0.01					•	_		
		TOTAL =						0.12	90.0		22		20	4	0.5	24	6.0

SEE MAP NO. 2 FOR BASIN IDENTIFICATION

TABLE 2
TOWER/SAGE DRAINAGE MASTER PLAN
AHYMO BASIN PARAMETER WORKSHEET
PEAK BASIN FLOWS AND VOLUMES

# (ALL FLOWS & VOLUMES INCLUDE A 5% BULKING FACTOR)

100 YEAR	RUNOFF	VOLUME	(24hr.)	(ac.ff.)				0.1					1.1		_			0.7				2.4					3.4					3.8
100	PEAK	FLOW	(6hr.)	(cfs)				24					22			***		16				28			-		83					88
10 YEAR	RUNOFF	VOLUME	(24hr.)	(ac.ft.)				9.0					9.0					0.4				1.5					2.0				1	2.2
10	PEAK	FLOW	(6hr.)	(cfs)				14					13					10				35					64		_			51
		_		D				90					90					8				88					99					22
		LAND TREATMENT	(%)	ပ		·			-																			•				_
		AND TRE	6	В				49					4					8				32					8	· · · ·				က္ခ
		ר		٨																						•						
			T(p)	(hr.)	0.03	90.0	0.01	0.10		0.05	0.12	0.01	0.18	y	3 !	0.07	0.01	0.13	-	0.03	0.05	0.08		0.03	0.05	0.03	0.11	50	) (	0.05	0.05	0.15
			(c)	(hr.)	50.0	60.0	0.01	0.15		0.07	0.18	0.01	0.26	20	5	0.10	0.01	0.19		0.05	0.07	0.12	-	0.05	90.0	0.04	0.17	80	9 6	0.07	0.07	0.22
			VEL	(fps)	0.84	2.83	3.00			0.57	1.4	2.12		1	5	1.3 4.	2.12			1.1	4.45			1.21	3.94	4.39		0.70	) (	3.79	3.61	
				X	0.7	3.0	3.0			0.7	3.0	3.0		7	5	3.0	3.0			0.7	3.0			0.7	3.0	3.0		7.0	. (	3.0	3.0	
			SLOPE	(%)	1 33	0.89	1.00			0.67	0.22	0.50		230	5.0	0.20	0.50			2.50	2.17			3.00	1.73	2.14		5	9 6	99.	<del>1</del> .	
		ELEV.	DIFF.	(ff.)	2.0	8.0	1.0			1.0	2.0	0.5		•	<u>.</u>	0.	0.5			5.0	25.0			0.9	19.0	15.0		0.0	) (	16.0	13.0	
			LENGTH	(H.)	150	8 06	8			150	006	100		450	3	200	100			200	1150			200	18	200		6		98	06	
			AREA	(sq.mi.)	0.0103	2	. "	TOTAL =		0.0108			TOTAL =	0900	6000			TOTAL =		0.0230		TOTAL =		0.0350			TOTAL =	0.0436	2			TOTAL =
			AR	(ac.)	y	3				6.9				,	ţ					14.7				22.4				976	) i			
				BASIN	0 at 4	2				A19-D				000	7-024					B1-D			•	B2-D				R.2.	1			

SEE MAP NO. 2 FOR BASIN IDENTIFICATION

TABLE 2
TOWER/SAGE DRAINAGE MASTER PLAN
AHYMO BASIN PARAMETER WORKSHEET
PEAK BASIN FLOWS AND VOLUMES

(ALL FLOWS & VOLUMES INCLUDE A 5% BULKING FACTOR)

	,								Ţ																
100 YEAR	RUNOFF	VOLUME	(24hr.)	(ac.ft.)				2.0	9	<u>?</u>					4.7				6.2						7.8
100	PEAK	FLOW	(6hr.)	(cfs)				5	55	3					89				97						98
10 YEAR	RUNOFF	VOLUME	(24hr.)	(ac.ft.)				1.	90	) i					2.8				3.7						4.4
\$	PEAK	FLOW	(6hr.)	(cfs)				53	7	i					41				58	·,					49
		Ŧ		D				20	5	)			-		65				29						8
		EATMEN	9	၁					ī,	)	*														
	-	LAND TREATMENT	(%)	В				20	5.0	3					35				33		-				20
		ב		٨					8	3										-	-				
			T(p)	(hr.)	0	200	7 0	0.12	0.13	) ;	-	0.07	0.18	0.07	0.32	0.09	0.11	0.08	0.28	70.0	5 6	0.20	0.14	0.08	0.49
			T(c)	(hr.)	9	200	5 6	0.09	0.20			0.11	0.27	0.10	0.49	0.13	0.17	0.12	0.42	,	- 6	0.29	0.21	0.12	0.74
			VEL	(fps)	111	3 46	F 6	3.21				0.49	0.97	2.30		0.87	79.	2.18		9,	}	2 3	90.1	2.18	
				¥	20		9 0	3.0				0.7	3.0	3.0		1.0	3.0	3.0		7	- (	O.	3.0	3.0	
			SLOPE	(%)	0.50	- 23	3 ;	1.14				0.50	0.11	0.59		0.75	0.30	0.53		C C	9 6	0.10	0.13	0.53	
		ELEV.	DIFF.	(ft.)	5	9 6	3 9	12.0				0.1	0.1	5.0		3.0	3.0	5.0		·	. ·	O	1.0	5.0	
			LENGTH	(ft.)	200	450	2	950				200	950	850		400	1000	920		5	3 5	3	88	920	
			AREA	(sq.mi.)	0.030			TOTAL =	0.0391			0.0459			TOTAL =	0.0591			TOTAL =	1080					TOTAL =
			AF	(ac.)	147	•		_	25.0	}		29.4				37.8				21	9				
				BASIN	84.0	5			R5.D	TOWER	POND	D-98		,		B7-D				۵	2				

SEE MAP NO. 2 FOR BASIN IDENTIFICATION

TABLE 2
TOWER/SAGE DRAINAGE MASTER PLAN
AHYMO BASIN PARAMETER WORKSHEET
PEAK BASIN FLOWS AND VOLUMES

(ALL FLOWS & VOLUMES INCLUDE A 5% BULKING FACTOR)

Colored Fig.   Colo														_	5	10 YEAR	100	100 YEAR
AREA LENGTH DIFF. SLOPE (fps) (hr.) (hr.) A (rt.) (rt.														1	PEAK	RUNOFF	PEAK	RUNOFF
AREA   LENGTH   DIFF. SLOPE   K (Fps)   (hr)   (hr)   A   B					ELEV.						Ž	ND TRE	ATMENT		FLOW	VOLUME	FLOW	VOLUME
(ac)   (sq.mi)   (ft.)   (%)   K   (fps)   (hr.)   A   B		AF	ξEA	LENGTH	DIFF.	SLOPE		VEL	T(c)	T(p)		%)			(ehr.)	(24hr.)	(6hr.)	(24hr.)
20.1 0.0314 100 2.0 2.00 0.7 0.99 0.03 0.02 0.03 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.03 0.02 0.03 0.02 0.03 0.02 0.03 0.02 0.03 0.03	BASIN		(sq.mi.)	(H)	(ff.)	(%)	¥	(fps)	(hr.)	(hr.)	A	В	ပ	۵	(cfs)	(ac.ft.)	(cfs)	(ac.ff.)
20.1 0.0314 100 2.0 2.00 0.7 0.99 0.03 0.02   325 8.0 2.46 3.0 4.71 0.02 0.01   400 8.0 2.46 3.0 4.71 0.02 0.01   526 8.0 2.46 3.0 4.71 0.02 0.01   527.9 0.0436 2.00 9.0 0.7 0.99 0.01 0.01   527.9 0.0436 2.00 9.0 1.00 0.7 0.86 0.06 0.06   528 8.0 2.46 3.0 4.71 0.02 0.01   528 8.0 2.46 3.0 4.71 0.02 0.01   529 8.0 2.46 3.0 4.71 0.02 0.01   520 8.0 2.46 3.0 4.71 0.02 0.01   520 8.0 2.0 3.0 3.0 3.0 0.05 0.03   527.9 0.0436 2.00 3.0 1.50 0.7 0.86 0.06 0.04   527.9 0.0436 2.00 3.0 1.50 0.7 0.86 0.06 0.04   527.9 0.0436 2.00 9.0 1.00 3.0 3.0 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.0 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.0 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.0 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.0 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.0 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.0 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.0 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.0 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.0 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.0 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.00 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.00 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.00 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.00 0.08 0.06   527.9 0.0436 2.00 9.0 1.00 3.0 3.00 0.08 0.06   527.9 0.0436 2.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0																		
TOTAL = 400 1.48 3.0 3.65 0.05 0.03	S1-D	20.1	0.0314	18	2.0	2.00	0.7	66.0	0.03	0.02								
10.4 0.0163 100 2.0 2.00 3.0 4.74 0.02 0.01  10.4 0.0163 100 2.0 2.00 0.7 0.99 0.03 0.02  10.4 0.0163 100 2.0 2.00 0.7 0.99 0.03 0.02  235 8.0 2.46 3.0 4.71 0.02 0.01  235 8.0 2.46 3.0 4.71 0.02 0.01  10.5 0.05 0.01  20.5 0.05 0.01  20.5 0.05 0.01  20.5 0.05 0.01  20.5 0.05 0.01  20.5 0.05 0.01  20.5 0.05 0.01  20.5 0.05 0.03  20.5 0.05 0.03  20.5 0.04  20.6 0.04  20.6 0.04  20.6 0.04  20.7 0.08 0.00  20.8 0.01  20.9 0.01  20.0 0.01				675	10.0	1.48	3.0	3.65	0.05	0.03			-					
10.4 0.0163 100 2.0 2.00 0.7 0.99 0.03 0.02 35 10.04 0.0163 100 2.0 2.00 0.7 0.99 0.03 0.02 0.03 0.03				325	8.0	2.46	3.0	4.71	0.02	0.01								
10.4 0.0163 100 2.0 2.00 0.7 0.99 0.03 0.02 0.03 0.02 0.03 0.02 0.03 0.02 0.03 0.02 0.03 0.02 0.03 0.02 0.03 0.02 0.03 0.02 0.01 0.00 0.03 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.02				400	8.0	2.00	3.0	4.24	0.03	0.02	-			-				
10.4 0.0163 100 2.0 2.00 0.7 0.99 0.03 0.02 0.03 0.05 0.05 0.03 0.05 0.05 0.05 0.05			TOTAL =						0.12	0.08		35		65	9	1.9	4	3.2
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0	9	200	5	Ċ	5	7	000	000									
36.3 0.0567 50 1.00 1.48 3.0 3.65 0.05 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.02	7-7c	<u>.</u>	0.0	3	) i	50.7	. (	3 6	3 6	9 6								
36.3 0.0567 50 1.0 2.46 3.0 4.71 0.02 0.01  TOTAL = 400 8.0 2.46 3.0 4.71 0.02 0.01  36.3 0.0567 50 1.0 2.00 0.7 0.99 0.01 0.01  500 5.0 1.00 3.0 4.50 0.02 0.02  500 5.0 1.00 3.0 4.65 0.01  250 250 0.80 3.0 4.65 0.01  150 1.0 0.67 3.0 2.45 0.02  27.9 0.0436 200 3.0 1.50 0.07  500 0.05 0.09  300 0.05 0.04  500 0.04 50  27.9 0.0436 200 3.0 1.50 0.07  500 0.06 0.04  500 0.06 0.04  500 0.09 0.06 0.04  500 0.09 0.09 0.06  500 0.09 0.09 0.09  500 0.09 0.09 0.09  500 0.09 0.09 0.09  500 0.09 0.09 0.09				675	10.0	<del>6</del> .	3.0	3.65	0.05	0.03								
36.3 0.0567 50 1.0 2.00 3.0 4.71 0.02 0.01 50  36.3 0.0567 50 1.0 2.00 0.7 0.99 0.01 0.01 0.01 0.01 0.01 0.02 0.02 0.02				325	8.0	2.46	3.0	4.71	0.02	0.01								
36.3 0.0567 50 1.0 2.00 0.7 0.99 0.01 0.01 50 50 50.0 50.0 50 0.02 0.02 0.02 0.02				325	8.0	2.46	3.0	4.71	0.02	0.01								
36.3 0.0567 50 1.0 2.00 0.7 0.99 0.01 0.01 50 50 5.0 1.00 2.25 3.0 4.50 0.02 0.02 0.02 5.0 2.25 3.0 4.65 0.03 0.05 0.03 5.0 1.00 3.0 3.00 0.05 0.03 5.0 1.00 0.80 3.0 2.68 0.03 0.02 5.0 14.0 1.65 3.0 3.85 0.06 0.04 5.0 1.00 0.67 3.0 2.45 0.02 0.01 0.01 5.0 1.00 0.67 3.0 2.45 0.02 0.01 0.01 0.01 0.01 0.01 0.02 0.03 0.02 0.03 0.02 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.05				\$	8.0	2.00	3.0	4.24	0.03	0.02					<del></del>			
36.3 0.0567 50 1.0 2.00 0.7 0.99 0.01 0.01 0.01 5.00 5.0 1.00 2.25 3.0 4.50 0.02 0.02 0.02 0.02 5.0 1.00 3.0 3.0 0.05 0.03 0.03 5.0 5.0 1.00 3.0 3.0 2.68 0.03 0.02 0.04 5.0 1.00 0.67 3.0 2.45 0.02 0.04 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.05			TOTAL =						0.14	0.10		22		20	77	8.0	36	1.4
36.3 0.0567 50 1.0 2.00 0.7 0.99 0.01 0.01 0.01 0.01 0.01 0.01 0.01																		-
27.9 0.0436 200 9.0 2.25 3.0 4.50 0.02 0.02 0.02 0.02 0.02 0.03 0.03 0.0	- 23-D	36.3	0.0567	20	0.	2.00	0.7	66.0	0.0	0.01								
250 5.0 1.00 3.0 0.05 0.03 0.03 250 6.0 2.40 3.0 2.68 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.0				400	9.0	2.25	3.0	4.50	0.02	0.02								
250 6.0 2.40 3.0 4.65 0.01 0.01 250 2.0 0.80 3.0 2.68 0.03 0.02 850 14.0 1.65 3.0 3.85 0.06 0.04 150 1.0 0.67 3.0 2.45 0.02 0.0436 200 3.0 1.50 0.7 0.86 0.06 0.04 950 10.0 1.05 3.0 3.08 0.09 0.06 900 9.0 1.00 3.0 3.00 0.08				200	5.0	9.1	3.0	3.00	0.05	0.03								
250 2.0 0.80 3.0 2.68 0.03 0.02 850 14.0 1.65 3.0 3.85 0.06 0.04 150 1.0 0.67 3.0 2.45 0.02 0.01 27.9 0.0436 200 3.0 1.50 0.7 0.86 0.06 0.04 950 10.0 1.05 3.0 3.08 0.09 0.06				250	6.0	2.40	3.0	4.65	0.01	0.01								
27.9 0.0436 200 10.0 1.05 3.0 3.08 0.06 0.04 0.04 0.04 0.04 0.04 0.04 0.04				250	2.0	0.80	3.0	2.68	0.03	0.02								
TOTAL = 150 1.0 0.67 3.0 2.45 0.02 0.01 0.20 0.14 0.20 0.0436 200 3.0 1.50 0.7 0.86 0.06 0.04 0.06 0.00 0.00 0.00 0.00 0.0				850	14.0	1.65	3.0	3.85	90.0	0.04								
27.9     0.0436     200     3.0     1.50     0.7     0.86     0.06     0.04       27.9     0.0436     200     3.0     1.05     3.0     3.08     0.06     0.06       900     9.0     1.00     3.0     3.00     0.08     0.06				150	1.0	29.0	3.0	2.45	0.02	0.01								
27.9         0.0436         200         3.0         1.50         0.7         0.86         0.06         0.04           950         10.0         1.05         3.0         3.08         0.09         0.06           900         9.0         1.00         3.0         3.00         0.08         0.06			TOTAL =						0.20	0.14		20		22	88	2.8	120	5.0
27.9         0.0436         200         3.0         1.50         0.7         0.86         0.06         0.04           950         10.0         1.05         3.0         3.08         0.09         0.06           900         9.0         1.00         3.0         0.08         0.06																		
950         10.0         1.05         3.0         3.08         0.09         0.06           900         9.0         1.00         3.0         3.00         0.08         0.06	S4-D	27.9	0.0436	200	3.0	1.50	0.7	98.0	90.0	0.04								
900 9.0 1.00 3.0 0.08 0.06				950	10.0	1.05	3.0	3.08	60.0	90.0								
				006	0.6	1.8	3.0	3.00	0.08	90.0							*****	
0.23   0.16			TOTAL =						0.23	0.16		40		90	55	2.5	93	4.2

SEE MAP NO. 2 FOR BASIN IDENTIFICATION

TABLE 2
TOWER/SAGE DRAINAGE MASTER PLAN
AHYMO BASIN PARAMETER WORKSHEET
PEAK BASIN FLOWS AND VOLUMES

(ALL FLOWS & VOLUMES INCLUDE A 5% BULKING FACTOR)

100 YEAR	RUNOFF	VOLUME	(24hr.)	(ac.ft.)	-		2.3				7	9.7				6.2				6.8				:	6.5
100	PEAK	FLOW	(6hr.)	(cfs)			26				Ų	ន				2				87					166
10 YEAR	RUNOFF	VOLUME	(24hr.)	(ac.ft.)			1.3				Ċ	2.2				3.7				4.1					3.7
9	PEAK	FLOW	(6hr.)	(cfs)			33				(	35				43				52					94
		Ħ		۵			59				5	9				71				63					20
		LAND TREATMENT	(%)	ပ													 								
		AND TR	9)	В			4					8				62				37					20
				A																					
			T(p)	(hr.)	0.02	0.10	0.12	0.15	0.05	0.01	0.10	0.31	0.10	0.27	0.03	0.46	0.10	0.20	0.09	0.39	0.03	3 6	90.0	0.04	0.13
			T(c)	(hr.)	0.03	0.15	0.18	0.22	0.07	0.02	0.15	0.47	0.16	0.41	0.13	0.70	0.16	0.29	0.14	0.59	ייי	3	0.09	90.0	0.20
			VEL	(fps)	3.67	1.90		0.50	1.50	3.00	2.02		0.71	0.65	1.36		0.71	0.95	2.22		2,00	3 3	2.92	5.08	
				X	3.0	3.0		0.1	3.0	3.0	3.0		1.0	2.0	2.0		1.0	3.0	3.0		,	2 :	3.0	3.0	
			SLOPE	(%)	1.50	0.40		0.25	0.25	1.00	0.45		0.50	0.11	0.46		0.50	0.10	0.55		2 33	5	0.95	2.87	
		ELEV.	DIFF.	(ff.)	6.0	4.0		1.0	1.0	2.0	5.0		2.0	1.0	3.0		2.0	1.0	0.9		ç	2	0.6	33.0	
			LENGTH	(H.)	94	1000		400	400	200	1100		904	920	650		400	1000	1100		Ö	3	920	1150	
			AREA	(sq.mi.)	0.0238		TOTAL =	0.0378				TOTAL =	0.0570			TOTAL =	0.0683			TOTAL =	0.0740	0.0740			TOTAL =
			AR	(ac.)	15.2	!		24.2	!				36.5				43.7				7	<b>4</b> 3			
				BASIN	S5-D	3		G-9S	3				S7-D				S8-D					- - - - - - - -			

SEE MAP NO. 2 FOR BASIN IDENTIFICATION

TABLE 2
TOWER/SAGE DRAINAGE MASTER PLAN
AHYMO BASIN PARAMETER WORKSHEET
PEAK BASIN FLOWS AND VOLUMES

(ALL FLOWS & VOLUMES INCLUDE A 5% BULKING FACTOR)

,																												_
100 YEAR	RUNOFF	VOLUME	(24hr.)	(ac.ff.)						4.0					1.9				3.0						3.4	6:0	25	<u>}</u>
100	PEAK	FLOW	(6hr.)	(cfs)						96					46				29						11	22	55	3
10 YEAR	RUNOFF	VOLUME	(24hr.)	(ac.ft.)						2.4					1.1				1.9						2.1	0.5	r.	?
2	PEAK	FLOW	(6hr.)	(cfs)						28					78				\$						84	13	ç	3
		Ŀ		۵						29				•	65				90						74	55	Ş	3
		EATMEN	(%)	၁	·																					જ		1
		LAND TREATMENT	0	В						33					35				10						56		Ç	2
		]		٨																								
			T(p)	(hr.)	0 03		0.04	0.03	0.01	0.11	C	70.0	0.04	0.02	0.08	0.03	0.01	0.04	0.08	8	20.00	0.03	0.01	0.06	0.14	0.14	0.12	71.0
			T(c)	(hr.)	900		90.0	0.05	0.02	0.17	6	3	0.07	0.03	0.13	0.04	0.02	0.06	0.12	ų o	6.03	0.05	0.05	0.09	0.21	0.20	0.18	2
			VEL	(fps)	1 21	<u> </u>	2.32	4.93	3.79		ç c		3.10	3.67		2.83	3.00	3.82			=	2.68	5.20	3.34		1.70	214	4.1.4
				¥	20	,	3.0	3.0	3.0		20		3.0	3.0		2.0	3.0	3.0		1	). O	3.0	3.0	3.0		3.0	0.0	2.7
			SLOPE	(%)	9	9	0.60	2.71	1.60		000	2.00	1.07	1.50		5.00	1.00	1.63		Ċ	7.20 0.27	0.80	3.00	1.24		0.32	7 1 7	<u>+</u>
		ELEV.	DIFF.	(ff.)	0 8	9	3.0	23.0	4.0			 	8.0	0.9		8.0	2.0	13.0		(	0.0	4.0	9.0	13.0		4.0	76.0	10.01
			LENGTH	(ff.)	500	3	200	820	250		00,	3	750	400		9	200	800		i d	8	200	300	1050		1250	1,400	1400
			AREA	(sq.mi.)	9000	0.000				TOTAL =		0.0188			TOTAL =	0.0234			TOTAL =		9050.0				TOTAL =	0.0091	200	0.0134
			AR	(ac.)	77.7	7.4.7					0	12.0				15.0		-		!	19.7					5.8	, ;	12.4
				BASIN		<u>ڄ</u> د					1	CZ-D				C3-D					C4D					Q-90	G G	-95 -0-95

TABLE 3
TOWER/SAGE DRAINAGE MASTER PLAN
SUMMARY OF PEAK DISCHARGES
AND PEAK VOLUMES

(ALL FLOWS INCLUDE A 5% BULKING FACTOR)

ANALYSIS POINT	Q(10) (6hr.) (cfs)	V(10) (24hr.) (ac.ft.)	Q(100) (6hr.)	V(100) (24hr.)
1	70	3.2	(cfs) 112	(ac.ft.) 5.2
2	126	5.7	204	9.4
3	179	8.3	292	13.7
4	244	11.4	397	18.8
5	298	14.0	490	23.2
6	73	3.7	119	6.1
7	78	4.2	132	7.0
8	86	4.7	147	7.0
9	445	22.0	748	36.8
10	457	22.6	766	37.8
11	35	1.5	58	2.4
12	77	3.5	132	5.8
13	118	5.6	211	9.6
14	142	6.8	252	11.6
15	46	1.9	77	3.2
16	65	2.7	109	4.6
17	132	5.5	228	9.6
18	185	8.0	318	13.8
19	202	9.4	348	16.4
20	345	16.5	599	27.7
21	820	39.3	1414	67.2
22	23	39.3	25	67.2
23	59	42.1	90	71.9
24	111	45.8	178	78.1
25	151	50.2	250	85.9
26	56	2.5	91	4.1
27	104	5.2	170	8.7
28	127	8.2	207	13.5
29	14	0.5	24	0.9
30	22	1.1	39	1.9
31	24	1.7	46	3.0
32	30	2.1	57	3.7
33	180	11.7	303	19.6
34	217	14.9	368	25.2
35	32	2.2	55	3.7
36	71	5.9	118	9.8
37	120	9.9	201	16.7
38	149	13.7	251	23.2
39	58	2.4	96	4.0
40	83	3.6	138	5.9
41	124	5.4	199	8.9
42	48	2.1	77	3.4
43	171	7.5	276	12.3
44	175	8.0	283	13.2
45	36	1.5	55	2.5

NOTE: SEE MAP NO. 2 FOR LOCATION OF ANALYSIS POINTS

#### 7.0 PROPOSED STORM DRAINAGE SYSTEM

The master planned Tower/Sage Storm Drainage System is shown on Map No. 3 included in the back pocket of this report. Pipe sizes shown are preliminary and may vary when the final facility design is performed.

As previously stated in the existing facilities section of this report, the Amole Del Norte Channel does not have the capacity to carry flows originating from the Sage/Tower Drainage Basin under developed conditions when applying the new AHYMO hydrology program. Therefore, a permanent detention facility is required upstream of the Amole Del Norte Channel to collect a portion of the storm water and then provisions for drainage of the pond at a controlled rate. Existing inlet pipes to the Amole Del Norte Channel have been provided at Tower Road and at Sage Road to serve the Tower/Sage Drainage Basin. These two inlets were designed to receive 601 cfs from the Tower Road storm drain line and 211 cfs from the Sage Road storm drain line.

The location of the detention pond is critical, so that the flows generated by the area below and east of the detention pond will be equal to or less than the rate of flow for which the Amole Del Norte Channel is designed to receive from the Tower/Sage Drainage Basin. To meet this criteria, a detention facility designated herein as the "Tower Detention Pond" is proposed to be constructed within the block bounded by Tower Road and San Ygnacio Road on the north and south respectively, and 86th Street and 82nd Street on the west and east respectively.

The pond will be designed to collect and detain the runoff from the upper, western portion of the Tower/Sage Drainage Basin (west of the Tower Detention Pond). The Tower/Unser Sector Development Plan proposes a Neighborhood City Park in the same vicinity as the proposed Tower Detention Pond. In this regard, City Parks and General Services was contacted and, in turn, they have expressed interest in

the concept of a joint-use facility consisting of a neighborhood park and storm water detention facility (see letter enclosed as Appendix B.

#### 7.1 STORM DRAINS

Storm water from the westerly portion of Drainage Basin A (Sub-basins A-1 thru A-11) will be collected and carried to the detention pond by a storm drain located in 98th Street and Tower Road. This storm drain will discharge to the Tower Pond just east of 86th Street.

Storm water from the westerly portion of Drainage Basin S (Sub-basins S-1 thru S-5) will be collected and carried to the detention pond by a storm drain in Sage Road. This storm drain turns north approximately 400 feet east of 86th Street to carry the flows to the detention pond. The northerly alignment of this storm drain was chosen as the farthest east and most feasible location relative to the existing topography as Sage Road ranges from four feet to six feet lower than the southerly side of the detention pond. It is proposed that the storm drain will be located on the easterly portion of the platted subdivision known as South Mesa Patio Townhomes. Although this area is subdivided, no development has occurred as of the date of this report. A 10-foot wide storm drainage easement exists along the easterly side of this subdivision; however, additional right-of-way for an easement of up to approximately 50 feet in width will be needed to accommodate the storm drain installation.

Storm water from the westerly portion of Drainage Basin B (Sub-basins B-1 through B-4) will be collected and carried in San Ygnacio Street until the street capacity is reached; then a combination of street and storm drain will be utilized to carry and discharge the water to the detention pond.

Storm water runoff generated from Drainage Basin C (Sub-basins C-1 through C-6) west of 98th Street and south of Tower Road will be collected and carried south by

a storm drain in 98th Street and Snow Vista Boulevard. This storm drain will discharge into the Snow Vista Channel south of Benavidas Road. The discharge of the storm water from this basin to the Snow Vista Channel was reviewed at a meeting with AMAFCA's drainage engineer and it was determined that the flow from this basin could be drained to the Snow Vista Channel without significantly affecting the channel capacity.

Storm water runoff generated from the easterly portion of the Basin will be collected and carried to the Amole Del Norte Channel by storm drains located in Tower Road, San Ygnacio Road, and Sage Road as shown on Map No. 3

#### 7.2 HYDRAULICS

The hydraulics of the proposed storm drain system are based on utilizing the following three basic system parts:

- Streets which act as open channels to convey storm water runoff to drop inlets.
- 2. Underground piping which convey storm water runoff from the drop inlets to the Tower Detention Pond or to the Amole Del Norte Channel.
- 3. Tower Detention Pond which will detain the storm water runoff and discharge it at a controlled rate to the Amole Del Norte Channel.

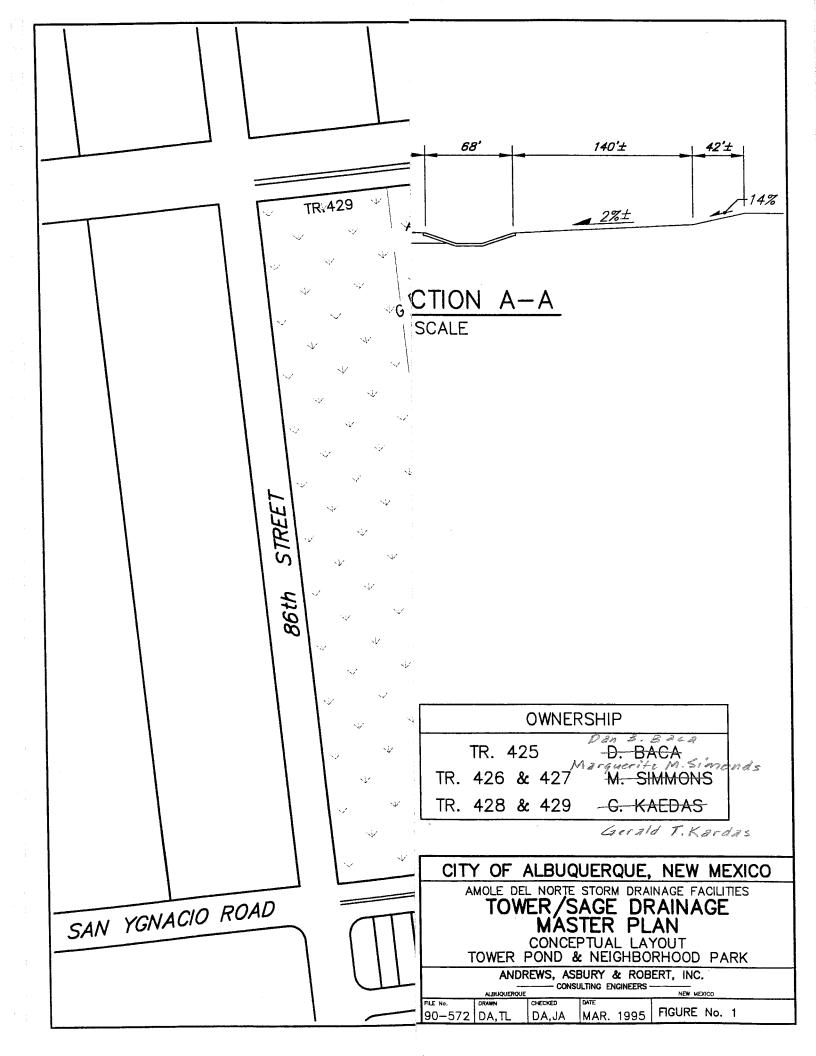
Street capacities were approximated within the Tower/Sage Drainage Area using Manning's Equation for open channel flow, proposed street sections, and existing terrain as street grades. Hydraulic grade lines were calculated for the storm drain pipes, again using Manning's principles for pressure flow and, in some instances, nonpressurized flow. Storm water runoff upstream of the Tower Detention Pond was routed through the pond as part of the AHYMO computer model. Table 4

displays a tabular version of the stage/storage curve and outflow curve for the Tower Detention Pond used in the AHYMO computer model. Section 7.3 below, discusses in more detail the proposed Tower Detention Pond configuration and hydraulic characteristics.

#### 7.3 TOWER DETENTION POND/NEIGHBORHOOD PARK

The Tower Detention Pond is proposed to be constructed south and east of the intersection of Tower Road and 86th Street. Figure 1 shows a conceptual Tower Detention Pond layout for a joint-use facility with a public neighborhood park. It is proposed that the block area outlined by public streets and consisting of 25 acres of land be made available for the City Park and the Tower Detention Pond. Twenty of the twenty-five available acres can be used as a neighborhood park. Six of these 20 acres will be utilized on infrequent occasions as part of the Tower Detention Pond. Approximately four to five acres of the 25 acres available will be used solely for detention pond purposes.

The park, in concept, will consist of grass and trees with slopes averaging two percent. A shallow concrete-lined low flow channel/swale will run through the park. Park patrons will be able to easily walk across the shallow channel/swale. There will be a 40-foot strip within the park, around the perimeter of the pond area, that will slope at 14 percent  $(7:1\pm)$ . This slope is part of the overall detention pond that is required to contain the 100 year storm. The four to five acres to be used solely for detention purposes will be approximately 20 feet deep with three to one, horizontal to vertical, side slopes. This depth is required to receive the storm drain line from Sage Road. This area will be designed to contain a two-year storm and is proposed to be fenced and seeded with a native vegetation. Figure 1 also shows high water levels in the Tower Detention Pond for various 24-hour storm frequencies.



# TABLE 4 TOWER/SAGE MASTER DRAINAGE PLAN TOWER POND

# STORAGE AND OUTFLOW RATING CURVE INFORMATION

ELEVATION (ft.)	INCREMENTAL VOLUME (ac.ft.)	TOTAL VOLUME (ac.ft.)	OUTFLOW (cfs)
			1
5072		0.0	0.0
	5.8		
5076		5.8	11.9
	7.1		
5080		13.0	17.4
	2.2		
5081		15.2	18.5
	2.5		
5082		17.7	19.6
	2.8		
5083		20.5	20.6
	3.3		
5084		23.8	21.5
	4.4		
5085		28.2	22.5
	6.2		
5086		34.4	23.3
	15.4		
5088		49.9	25.0
	8.2		
5089		58.0	25.8
	26.4		
5092		84.4	3000*

TOP OF BERM ELEVATION = 5092.00 FT. EMERGENCY SPILLWAY ELEVATION = 5089.00 FT.

<sup>\*</sup> EMERGENCY SPILLWAY FLOW

TABLE 5
TOWER/SAGE MASTER DRAINAGE PLAN
TOWER POND DATA

	24 - HOUR STORM DURATION				
	2 - YEAR STORM	5 - YEAR STORM	10 - YEAR STORM	100 - YEAR STORM	
TOTAL VOLUME ENTERING TOWER POND	21.8 ac.ft.	31.4 ac.ft.	39.3 ac.ft.	67.2 ac.ft.	
HIGH WATER LEVEL IN TOWER POND	5080.9 ft.	5083.6 ft.	5085.1 ft.	5088.1 ft.	
TIME TO DRAIN TOWER POND	63 hr.*	67 hr.*	70 hr.*	82 hr.*	

TOP OF BERM ELEVATION = 5092.00 FT.
EMERGENCY SPILLWAY ELEVATION = 5089.00 FT.

<sup>\*</sup> TIME TO DRAIN LAST FOOT OF STORM WATER IN POND = 38 HRS.

#### 8.0 RIGHT-OF-WAY

The major portion of the master-planned storm drain lines proposed herein are located within existing street right-of-way.

The City of Albuquerque is currently in the process of obtaining right-of-way for the widening and construction of 98th Street and includes the right-of-way to provide for realignment of the streets intersection 98th Street. The storm drains proposed in 98th Street and in Tower Road can be constructed within the existing right-of-way and/or the street right-of-way being obtained.

#### 8.1 TOWER DETENTION POND/NEIGHBORHOOD PARK

The lands on which the Tower Detention Pond and the Neighborhood Park are proposed to be constructed is presently in private ownership. Therefore, this pond and park area will require acquisition prior to construction of these facilities.

The detention pond and park are proposed for the block area bounded on the north by Tower road, on the east by 82nd Street, on the south by San Ygnacio Road, and on the west by 86th Street, and consists of approximately 25 acres. Based on the conceptual layout plan included in this report, the required area for the detention pond and park area is divided approximately equal (i.e., 12.5 acres for the detention pond and 12.5 acres for the neighborhood park).

#### 8.2 SAGE ROAD STORM DRAIN

To provide for construction of the Sage Road Storm Drain between Sage Road and San Ygnacio Road, additional right-of-way will need to be acquired. An existing 10-foot wide drainage right-of-way exists along the east side of the South Mesa Townhomes Subdivision; however, additional right-of-way varying from 30 feet to

40 feet in width is required for construction of this portion of the Sage Road Storm Drain. The additional right-of-way area to be acquired is estimated at one (1) acre.

#### 9.0 CONCLUSIONS AND RECOMMENDATIONS

This Master Plan of Drainage presents a storm drainage system and plan to manage the storm water generated by the Tower/Sage Drainage Basin using the City's current AHYMO hydrologic model.

Within the designated land uses and the limits established by the hydrologic analysis included herein, the implementation of this plan will allow the areas within the basin to be developed, based on approved drainage plans without restricting runoff.

Flood plains in the area can also be removed by providing proper documentation and application to FEMA when the construction of the facilities has been completed.

The plan provides for a system that can be separated into construction project phases and it is recommended that an initial phase be implemented as follows:

#### 9.1 PHASE I

As mentioned previously in this report, the City of Albuquerque presently has Special Assessment District 222 in progress to provide for improvements in the westerly portion of the Tower/Sage Drainage Basin. It is recommended that the first phase of the planned facilities be constructed as a portion of this Special Assessment District 222. This first phase, Phase I, should include the following:

- 98th Street and Tower Road Storm Drain to Tower Detention Pond.
- San Ygnacio Road Storm Drain to Tower Detention Pond.
- Tower Detention Pond
- 98th Street Storm Drain to Snow Vista Channel

#### 9.2 OTHER PHASES

Other phases, including one or all of the following systems, should be programmed and arrangements made for implementation based on their need and availability of funds. These other phases are:

- Sage Road Storm Drain to Tower Pond.
- Tower Road Storm Drain to Amole Del Norte Channel.
- San Ygnacio Storm Drain to Amole Del Norte Channel.
- Sage Road Storm Drain to Amole Del Norte Channel.

### 10.0 EXISTING DRAINAGE DATA - REFERENCES

Previous drainage reports have been prepared relative to this area. These reports and appropriate criteria were reviewed and used in the preparation of this report. The references used are as follows:

Albuquerque Metropolitan Arroyo Flood Authority, January 1994, "AHYMO Computer Program Users Manual."

Andrews, Asbury & Robert, Inc., December 1990, "Sage Road Improvements Drainage Report."

Boyle Engineering Corp., July 1984, "Investigation Phase Report for the Re-evaluation Study of the Amole Del Norte Storm Diversion Facility."

Boyle Engineering, February 1985, "Design - Development Report for the Re-evaluation Study of the Amole Del Norte Storm Diversion Facility."

City of Albuquerque, January 1982, "Development Process Manual Volume 2, Design Criteria" (Including all revisions).

City of Albuquerque, January 1993, "Section 22.2, Hydrology of the Development Process Manual Volume 2, Design Criteria."

City of Albuquerque Planning Department, September 1989, "Tower/Unser Sector Development Plan."

Gordon Herkenhoff & Associates, Inc., December 1980, "Interim Design Report Westgate Diversion Channels."

Gordon Herkenhoff & Associates, Inc., July 1982, "Phase III Design Guidelines Snow Vista Channel Westgate Diversion Channels."

Greiner, Inc., October 1990, "Preliminary Design Report for Amole Del Norte Diversion Facilities Tierra Bayita Drainage Facilities."

Greiner, Inc., June 1994, "Design Report for Amole Del Norte Diversion Facilities Tierra Bayita Drainage Facilities phase IIIC."

Holmes and Narver Inc., November 1985, "Existing Conditions for Amole Watershed Drainage Management Plan."

Holmes and Narver Inc., April 1986, "Improved Conditions Report for Amole Watershed Drainage Management Plan."

Leedshill-Herkenoff, Inc., April 1994, "Drainage Report for Sunset West Unit 2 Albuquerque, New Mexico."

Resource Technology, Inc., December 1993, "Draft - Flood Insurance Restudy Report for Six Areas Within The City of Albuquerque, Bernalillo County, New Mexico Community Number 350002."

Soil Conservation Service, June 1977, "Soil Survey of Bernalillo County and Parts of Sandoval and Valencia Counties, New Mexico."

# City of Albuquerque TOWER/SAGE DETENTION POND

# SUMMARY Estimated Construction Costs

11.1	PHASE I	Estimated Construction Cost
•	98th Street and Tower Road Storm Drain System to Tower Detention Pond	\$1,512,229.13
•	San Ygnacio Road Storm Drain System to Tower Detention Pond	344,303.03
•	Tower Detention Pond	606,001.00
•	98th Street Storm Drain System to Snow Vista Channel	678,623.00
	TOTAL ESTIMATED CONSTRUCTION COST	\$3,141,216.16

Right-of-Way for Tower Detention Pond/Neighborhood Park

25 acres @ \$28,314.00/Ac =

\$707,850.00

As an interim measure to drain the Tower Detention Pond, prior to the time the easterly portion of the San Ygnacio Storm Drain is constructed, an 18" dia. drain line may need to be installed from the Tower Detention Pond to the Amole Del Norte Channel. The estimated cost of this drain line is \$150,000 to \$200,000.

606 708 1314 941 2255,000 1830

### 11.2 OTHER PHASES

•	Sage Road Storm Drain System to Tower Detention Pond	\$826,115.40
•	Tower Road Storm Drain System to Amole Del Norte Channel	941,204.00
•	San Ygnacio Road Storm Drain System to Amole Del Norte Channel	609,650.00
•	Sage Road Storm Drain System to Amole Del Norte Channel	<u>521,891.15</u>
	TOTAL ESTIMATED CONSTRUCTION COST	\$2,898,8681.35
•	Right-of-Way for Sage Road Storm Drain between Sage Road and San Ygnacio Road	
	1 Acre @ \$43,560/Ac =	\$43,560.00

## 98TH STREET & TOWER ROAD STORM DRAIN SYSTEM TO TOWER DETENTION POND SERVING THE WESTERLY PORTION OF BASIN A

ITEM DESCRIPTION	UNIT	ESTIMATED QUANTITY	UNIT PRICE	AMOUNT
18" RCP, furnish & install in open trench, cip.	LF	1,175	\$20.50	\$24,087.50
Trenching, backfill & compaction for 18" sewer pipe, cip.	LF	1,175	\$11.00	\$12,925.00
24" RCP, furnish & install in open trench, cip.	LF	1,175	\$27.20	\$31,960.00
Trenching, backfill & compaction for 24" sewer pipe, cip.	LF	1,175	\$12.50	\$14,687.50
42" RCP, furnish & install in open trench, cip.	LF	1,375	\$55.00	\$75,625.00
Trenching, backfill & compaction for 42" sewer pipe, cip.	LF	1,375	\$30.75	\$42,281.25
48" RCP, furnish & install in open trench, cip.	LF	900	\$60.00	\$54,000.00
Trenching, backfill & compaction for 48" sewer pipe, cip.	LF	900	\$35.00	\$31,500.00
54" RCP, furnish & install in open trench, cip.	LF	2,400	\$112.00	\$268,800.00
Trenching, backfill & compaction for 54" sewer pipe, cip.	LF	2,400	\$39.50	\$94,800.00
60" RCP, furnish & install in open trench, cip.	LF	2,250	\$104.00	\$234,000.00
Trenching, backfill & compaction for 60" sewer pipe, cip.	LF	2,250	\$43.75	\$98,437.50
84" RCP, furnish & install in open trench, cip.	LF	800	\$150.00	\$120,000.00
Trenching, backfill & compaction for 84" sewer pipe, cip.	LF	800	\$61.25	\$49,000.00
Manhole, 6' diameter Type "C", cip.	EA	3	\$2,300.00	\$6,900.00
4' diam. tee manhole, cip.	EA	18	\$2,000.00	\$36,000.00
Furnish & install RCP Class IV bulkhead, cip.	EA	3	\$1,250.00	\$3,750.00
Furnish & install 54" RCP_bend, cip.	EA	2	\$700.00	\$1,400.00
Furnish & install 84" RCP_bend, cip.	EA	2	\$1,500.00	\$3,000.00
Catch basin, type "A", cip.	EA	78	\$2,200.00	\$171,600.00

**ESTIMATED CONSTRUCTION COST SUBTOTAL** 

\$1,374,753.75

10% CONTINGINCES

\$137,475.38

**ESTIMATED CONSTRUCTION COST** 

\$1,512,229.13

## SAN YGNACIO ROAD STORM DRAIN SYSTEM TO TOWER DETENTION POND SERVING THE WESTERLY PORTION OF BASIN B

ITEM DESCRIPTION	UNIT	ESTIMATED QUANTITY	UNIT PRICE	AMOUNT
18" RCP, furnish & install in open trench, cip.	LF	395	\$20.50	\$8,097.50
Trenching, backfill & compaction for 18" sewer pipe, cip.	LF	395	\$11.00	\$4,345.00
24" RCP, furnish & install in open trench, cip.	LF	395	\$27.20	\$10,744.00
Trenching, backfill & compaction for 24" sewer pipe, cip.	LF	395	\$12.50	\$4,937.50
42" RCP, furnish & install in open trench, cip.	LF	1,075	\$55.00	\$59,125.00
Trenching, backfill & compaction for 42" sewer pipe, cip.	LF	1,075	\$30.75	\$33,056.25
54" RCP, furnish & install in open trench, cip.	LF	450	\$112.00	\$50,400.00
Trenching, backfill & compaction for 54" sewer pipe, cip.	LF	450	\$39.50	\$17,775.00
90" RCP, furnish & install in open trench, cip.	LF	230	\$160.00	\$36,800.00
Trenching, backfill & compaction for 90" sewer pipe, cip.	LF	230	\$65.75	
Manhole, 6' diameter Type "C", cip.	EA	3	\$2,300.00	\$15,122.50
4' diam. tee manhole, cip.	EA	2		\$6,900.00
Furnish & install RCP Class IV bulkhead, cip.	EA		\$2,000.00	\$4,000.00
		2	\$1,250.00	\$2,500.00
Furnish & install 90" RCP_bend, cip.	EA	1	\$2,000.00	\$2,000.00
Catch basin, type "A", cip.	EA	26	\$2,200.00	\$57,200.00

**ESTIMATED CONSTRUCTION COST SUBTOTAL** 

\$313,002.75

10% CONTINGINCES

\$31,300.28

**ESTIMATED CONSTRUCTION COST** 

\$344,303.03

### **TOWER DETENTION POND**

ITEM DESCRIPTION	UNIT	ESTIMATED QUANTITY	UNIT PRICE	AMOUNT
Excavation for detention pond, cip.	CY	110,000	\$3.00	\$330,000.00
Reinforced structural concrete within pond, cip.	LS	Lump Sum	\$200,000.00	\$200,000.00
Chain link fence, inc. posts and hardware, cip.	SF	9,000	\$2.10	\$18,900.00
Gated for chain link fence, inc. all hardware, cip.	SF	300	\$6.70	\$2,010.00

**ESTIMATED CONSTRUCTION COST SUBTOTAL** 

\$550,910.00

**10% CONTINGINCES** 

\$55,091.00

**ESTIMATED CONSTRUCTION COST** 

\$606,001.00

## 98TH STREET STORM DRAIN SYSTEM TO SNOW VISTA CHANNEL SERVING BASIN C

ITEM DESCRIPTION	UNIT	ESTIMATED QUANTITY	UNIT PRICE	AMOUNT
18" RCP, furnish & install in open trench, cip.	LF	525	\$20.50	\$10,762.50
Trenching, backfill & compaction for 18" sewer pipe, cip.	LF	525	\$11.00	\$5,775.00
24" RCP, furnish & install in open trench, cip.	LF	525	\$27.20	\$14,280.00
Trenching, backfill & compaction for 24" sewer pipe, cip.	LF	525	\$12.50	\$6,562.50
36" RCP, furnish & install in open trench, cip.	LF	1,750	\$47.00	\$82,250.00
Trenching, backfill & compaction for 36" sewer pipe, cip.	LF	1,750	\$15.00	\$26,250.00
42" RCP, furnish & install in open trench, cip.	LF	950	\$55.00	\$52,250.00
Trenching, backfill & compaction for 42" sewer pipe, cip.	LF	950	\$30.75	\$29,212.50
72" RCP, furnish & install in open trench, cip.	LF	1,625	\$125.00	\$203,125.00
Trenching, backfill & compaction for 72" sewer pipe, cip.	LF	1,625	\$52.50	\$85,312.50
Manhole, 6' diameter Type "C", cip.	EA	6	\$2,300.00	\$13,800.00
4' diam. tee manhole, cip.	EA	4	\$2,000.00	\$8,000.00
Furnish & install RCP Class IV bulkhead, cip.	EA	1	\$1,250.00	\$1,250.00
Furnish & install 72" RCP_bend, cip.	EA	1	\$1,100.00	\$1,100.00
Catch basin, type "A", cip.	EA	35	\$2,200.00	\$77,000.00

**ESTIMATED CONSTRUCTION COST SUBTOTAL** 

\$616,930.00

**10% CONTINGINCES** 

\$61,693.00

**ESTIMATED CONSTRUCTION COST** 

\$678,623.00

## SAGE ROAD STORM DRAIN SYSTEM TO TOWER DETENTION POND SERVING THE WESTERLY PORTION OF BASIN S

ITEM DESCRIPTION	UNIT	ESTIMATED QUANTITY	UNIT PRICE	AMOUNT
18" RCP, furnish & install in open trench, cip.	LF	545	\$20.50	\$11,172.50
Trenching, backfill & compaction for 18" sewer pipe, cip.	LF	545	\$11.00	\$5,995.00
24" RCP, furnish & install in open trench, cip.	LF	545	\$27.20	\$14,824.00
Trenching, backfill & compaction for 24" sewer pipe, cip.	LF	545	\$12.50	\$6,812.50
36" RCP, furnish & install in open trench, cip.	LF	1,830	\$47.00	\$86,010.00
Trenching, backfill & compaction for 36" sewer pipe, cip.	LF	1,830	\$15.00	\$27,450.00
48" RCP, furnish & install in open trench, cip.	LF	1,080	\$60.00	\$64,800.00
Trenching, backfill & compaction for 48" sewer pipe, cip.	LF	1,080	\$35.00	\$37,800.00
78" RCP, furnish & install in open trench, cip.	LF	1,600	\$140.00	\$224,000.00
Trenching, backfill & compaction for 78" sewer pipe, cip.	LF	1,600	\$57.00	\$91,200.00
Manhole, 6' diameter Type "C", cip.	EA	5	\$2,300.00	\$11,500.00
4' diam. tee manhole, cip.	EA	7	\$2,000.00	\$14,000.00
Furnish & install RCP Class IV bulkhead, cip.	EA	1	\$1,250.00	\$1,250.00
Catch basin, type "A", cip.	EA	36	\$2,200.00	\$79,200.00
Arterial pavement removal & replacement, cip.	LS	LS	\$75,000.00	\$75,000.00

**ESTIMATED CONSTRUCTION COST SUBTOTAL** 

\$751,014.00

10% CONTINGINCES

\$75,101.40

**ESTIMATED CONSTRUCTION COST** 

\$826,115.40

## TOWER ROAD STORM DRAIN SYSTEM TO AMOLE DEL NORTE CHANNEL SERVING THE EASTERLY PORTION OF BASIN A

ITEM DESCRIPTION	UNIT	ESTIMATED QUANTITY	UNIT PRICE	AMOUNT
18" RCP, furnish & install in open trench, cip.	LF	575	\$20.50	\$11,787.50
Trenching, backfill & compaction for 18" sewer pipe, cip.	LF	575	\$11.00	\$6,325.00
24" RCP, furnish & install in open trench, cip.	LF	575	\$27.20	\$15,640.00
Trenching, backfill & compaction for 24" sewer pipe, cip.	LF	575	\$12.50	\$7,187.50
36" RCP, furnish & install in open trench, cip.	LF	1,075	\$47.00	\$50,525.00
Trenching, backfill & compaction for 36" sewer pipe, cip.	LF	1,075	\$15.00	\$16,125.00
42" RCP, furnish & install in open trench, cip.	LF	1,175	\$55.00	\$64,625.00
Trenching, backfill & compaction for 42" sewer pipe, cip.	LF	1,175	\$30.75	\$36,131.25
48" RCP, furnish & install in open trench, cip.	LF	875	\$60.00	\$52,500.00
Trenching, backfill & compaction for 48" sewer pipe, cip.	LF	875	\$35.00	\$30,625.00
60" RCP, furnish & install in open trench, cip.	LF	1,075	\$104.00	\$111,800.00
Trenching, backfill & compaction for 60" sewer pipe, cip.	LF	1,075	\$43.75	\$47,031.25
66" RCP, furnish & install in open trench, cip.	LF	1,750	\$114.00	\$199,500.00
Trenching, backfill & compaction for 66" sewer pipe, cip.	LF	1,750	\$48.25	\$84,437.50
Manhole, 6' diameter Type "C", cip.	EA	6	\$2,300.00	\$13,800.00
4' diam. tee manhole, cip.	EA	9	\$2,000.00	\$18,000.00
Furnish & install RCP Class IV bulkhead, cip.	EA	4	\$1,250.00	\$5,000.00
Furnish & install 66" RCP_bend, cip.	EA	1	\$1,000.00	\$1,000.00
Catch basin, type "A", cip.	EA	38	\$2,200.00	\$83,600.00

**ESTIMATED CONSTRUCTION COST SUBTOTAL** 

\$855,640.00

**10% CONTINGINCES** 

\$85,564.00

**ESTIMATED CONSTRUCTION COST** 

\$941,204.00

### SAN YGNACIO ROAD STORM DRAIN SYSTEM TO AMOLE DEL NORTE CHANNEL SERVING THE EASTERLY PORTION OF BASIN B

ITEM DESCRIPTION	UNIT	ESTIMATED QUANTITY	UNIT PRICE	AMOUNT
18" RCP, furnish & install in open trench, cip.	LF	390	\$20.50	\$7,995.00
Trenching, backfill & compaction for 18" sewer pipe, cip.	LF	390	\$11.00	\$4,290.00
24" RCP, furnish & install in open trench, cip.	LF	390	\$27.20	\$10,608.00
Trenching, backfill & compaction for 24" sewer pipe, cip.	LF	390	\$12.50	\$4,875.00
30" RCP, furnish & install in open trench, cip.	LF	1,300	\$39.20	\$50,960.00
Trenching, backfill & compaction for 30" sewer pipe, cip.	LF	1,300	\$14.00	\$18,200.00
48" RCP, furnish & install in open trench, cip.	LF	3,300	\$60.00	\$198,000.00
Trenching, backfill & compaction for 48" sewer pipe, cip.	LF	3,300	\$35.00	\$115,500.00
60" RCP, furnish & install in open trench, cip.	LF	200	\$104.00	\$20,800.00
Trenching, backfill & compaction for 60" sewer pipe, cip.	LF	200	\$43.75	\$8,750.00
Manhole, 6' diameter Type "C", cip.	EA	3	\$2,300.00	\$6,900.00
4' diam. tee manhole, cip.	EA	9	\$2,000.00	\$18,000.00
Furnish & install RCP Class IV bulkhead, cip.	EA	1	\$1,250.00	\$1,250.00
Furnish & install 60" RCP_bend, cip.	EA	1	\$900.00	\$900.00
Catch basin, type "A", cip.	EA	26	\$2,200.00	\$57,200.00
Connect 60" RCP to Amole Del Norte Channel	LS	1	\$30,000.00	\$30,000.00

**ESTIMATED CONSTRUCTION COST SUBTOTAL** 

\$554,228.00

**10% CONTINGINCES** 

\$55,422.80

**ESTIMATED CONSTRUCTION COST** 

\$609,650.80

## SAGE ROAD STORM DRAIN SYSTEM TO AMOLE DEL NORTE CHANNEL SERVING THE EASTERLY PORTION OF BASIN S

ITEM DESCRIPTION	UNIT	ESTIMATED QUANTITY	UNIT PRICE	AMOUNT
18" RCP, furnish & install in open trench, cip.	LF	395	\$20.50	\$8,097.50
Trenching, backfill & compaction for 18" sewer pipe, cip.	LF	395	\$11.00	\$4,345.00
24" RCP, furnish & install in open trench, cip.	LF	395	\$27.20	\$10,744.00
Trenching, backfill & compaction for 24" sewer pipe, cip.	LF	395	\$12.50	\$4,937.50
30" RCP, furnish & install in open trench, cip.	LF	1,050	\$39.20	\$41,160.00
Trenching, backfill & compaction for 30" sewer pipe, cip.	LF	1,050	\$14.00	\$14,700.00
48" RCP, furnish & install in open trench, cip.	LF	2,700	\$60.00	\$162,000.00
Trenching, backfill & compaction for 48" sewer pipe, cip.	LF	2,700	\$35.00	\$94,500.00
60" RCP, furnish & install in open trench, cip.	LF	350	\$104.00	\$36,400.00
Trenching, backfill & compaction for 60" sewer pipe, cip.	LF	350	\$43.75	\$15,312.50
Manhole, 6' diameter Type "C", cip.	EA	3	\$2,300.00	\$6,900.00
4' diam. tee manhole, cip.	EA	8	\$2,000.00	\$16,000.00
Furnish & install RCP Class IV bulkhead, cip.	EA	1	\$1,250.00	\$1,250.00
Furnish & install 60" RCP_bend, cip.	EA	1	\$900.00	\$900.00
Catch basin, type "A", cip.	EA	26	\$2,200.00	\$57,200.00

**ESTIMATED CONSTRUCTION COST SUBTOTAL** 

\$474,446.50

10% CONTINGINCES

\$47,444.65

**ESTIMATED CONSTRUCTION COST** 

\$521,891.15

### **APPENDIX A**

# AMOLE DEL NORTE STORM DRAINAGE FACILITIES TOWER/SAGE DRAINAGE MASTER PLAN

#### AHYMO SUMMARY TABLE - 2 YEAR - 24 HOUR STORM

AHYMO SUMMARY TABLE (AHYMO194) - AMAFCA Hydrologic Model - January, 1994 INPUT FILE = MASTER2.IN

RUN DATE (MON/DAY/YR) =12/10/1994 USER NO.= ANASRONM.IO1

							TOTAL MOTOR PRINCIPLE OF THE PRINCIPLE O				
	HYDROGRAPH	FROM ID	TO ID	AREA	PEAK DISCHARGE	RUNOFF VOLUME	RUNOFF	TIME TO PEAK	CFS PER	PAGE =	: 1
COMMAND	IDENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATI	ON
START										TIME=	.00
	PE= 2									RAIN24=	1.160
SEDIMENT BUL										PK BF =	1.05
COMPUTE NM H		<b>-</b> _	3	.04580	40.45	1.842	.75409	1.500		PER IMP=	76.00
ROUTE	AP-1R	3	2	-04580	39.97	1.842	.75410	1.550	1.364		
COMPUTE NM H			3	.03950	33.62	1.466	.69579	1.500		PER IMP=	70.00
ADD HYD	AP#2	2& 3	10	.08530	70.50	3.308	.72709	1.550	1.291		
ROUTE	AP#2R	10	2	.08530	70.77	3.308	.72710	1.550	1.296		
COMPUTE NM H		-	3	.04190	34.25	1.446	.64721	1.500			65.00
ADD HYD	AP#3	2& 3	10	.12720	100.19	4.754	.70078	1.550	1.231		
ROUTE	AP#3R	10	2	.12720	101.05	4.754	.70078	1.550	1.241		
COMPUTE NM H		-	3	.04390	40.76	1.857	.79296	1.500			80.00
ADD HYD	AP#4	2& 3	10	.17110	140.05	6.611	.72443	1.550	1.279		
ROUTE	AP#4R	10	2	.17110	140.22	6.611	.72443	1.550	1.280		
COMPUTE NM H			3	.04520	33.17	1.443	.59863	1.500		PER IMP=	60.00
ADD HYD	AP#5	2& 3	10	.21630	170.37	8.054	.69814	1.550	1.231		
ROUTE	AP#5R	10	2	.21630	169.15	8.054	.69814	1.550	1.222		
COMPUTE NM H		-	3	.04520	27.86	1.209	.50146	1.500		PER IMP=	50.00
ADD HYD	PART_AP#9	2& 3	10	.26150	194.52	9.263	.66414	1.550	1.162		
COMPUTE NM H			3	.02060	12.70	.551	.50146	1.500		PER IMP=	50.00
ADD HYD	PART_AP#9		10	.28210	206.09	9.813	.65226	1.550	1.141		
COMPUTE NM H			3	.05700	41.85	2.115	.69579	1.550		PER IMP=	70.00
ROUTE	AP&6R	3	2	.05700	37.67	2.115	.69580	1.600	1.033		
COMPUTE NM H			3	.01020	6.49	.273	.50146	1.500		PER IMP=	50.00
ADD HYD	AP#7		20	.06720	41.94	2.388	.66629	1.600	.975		
ROUTE	AP#7R	20	2	.06720	41.44	2.388	.66630	1.650	.963		
COMPUTE NM H		-	3	.01020	6.49	.273	.50146	1.500		PER IMP=	50.00
ADD HYD	AP#8		20	.07740	45.24	2.661	.64456	1.600	.913		
ROUTE	AP#8R	20	2	.07740	45.07	2.661	.64457	1.650	.910		
ADD HYD		10& 2	10	.35950	238.50	12.474	.65060	1.550	1.037		
ROUTE	AP#9R	10	2	.35950	237.62	12.474	.65060	1.550	1.033		
COMPUTE NM }		-	3	.00860	8.17	.346	.75409	1.500		PER IMP=	76.00
ADD HYD	AP#10	2& 3	20	.36810	244.63	12.820	.65302	1.550	1.038		
COMPUTE NM I		-	3	.02300	19.63	.830	.67636	1.500		PER IMP=	68.00
ROUTE	AP#11R		2	.02300	16.50	.830	.67638	1.550	1.121		
COMPUTE NM I			3	.03500	26.50	1.117	.59863	1.500		PER IMP=	60.00
ADD HYD	AP#12		10	.05800	40.73	1.947	.62944	1.500	1.097		
ROUTE	AP#12R		2	.05800	35.20	1.947	.62946	1.600	-948		
COMPUTE NM			3	.04360	25. <i>7</i> 3	1.166	.50146	1.500	.922	PER IMP=	50.00
ADD HYD	AP#13		10	.10160	58.91	3.113	.57452	1.550	.906	5	
ROUTE	AP#13R	10	2	.10160	57.77	3.113	.57452	1.600	.888	3	
COMPUTE NM I			3	.02300	14.64	.615	.50146	1.500		PER IMP=	50.00
ADD HYD	AP#14		10	.12460	69.46	3.728	.56103	1.550	.87		
ROUTE	AP#14R		12	.12460	69.06	3.728	.56103	1.550	.866	5	
COMPUTE NM I	HYD S1-D&AP#15		3	.03140	25.67	1.084	.64721	1.500	1.277	7 PER IMP=	65.00
ROUTE	AP-15R	3	2	.03140	24.64	1.084	.64723	1.500	1.226	5	
COMPUTE NM	HYD S2-D	-	3	.01630	10.38	.436	.50146	1.500	.995	FER IMP=	50.00
ADD HYD	AP#16			.04770	35.01	1.520	.59739	1.500	1.147	7	
ROUTE	AP#16R	10	2	.04770	34.72	1.520	.59741	1.550	1.137	7	

	FROM	TO		PEAK	RUNOFF		TIME TO		.GE = 2
HYDROGRAPH COMMAND IDENTIFICATION	ID NO.	ID NO.	AREA (SQ MI)	DISCHARGE (CFS)	VOLUME (AC-FT)	RUNOFF (INCHES)	PEAK (HOURS)	PER ACRE NO	TATION
COMPLETE NA HAD CZ-D		7	05470	34.95	1.516	501/4	1 500	047 DED 1	ND- E0 00
COMPUTE NM HYD S3-D ADD HYD AP#17	- 20 7	3 10	.05670 .10440	67.58	3.036	.50146 .54529	1.500 1.500		MP= 50.00
		2	.10440	68.61	3.036	.54529	1.550	1.012 1.027	
ROUTE AP#17R	10	3		29.38	1.392				WD- (0.00
COMPUTE NM HYD S4-D	-		.04360	29.36 97.99		.59862	1.550	1.053 PER I	MP= 60.00
ADD HYD AP#18		10	.14800		4.428	.56100	1.550	1.035	
ROUTE AP#18R	10	2	.14800	90.91	4.428	.56100	1.600	.960	50
COMPUTE NM HYD S5-D		3	.02380	17.73	.748	.58891	1.500	1.164 PER I	MP= 59.00
ADD HYD AP#19		10	.17180	104.08	5.176	.56486	1.550	.947	
ADD HYD AP#20	12&10	10	.29640	173.15	8.904	.56325	1.550	.913	
ADD HYD PART_AP#21		10	.66450	417.78	21.724	.61298	1.550	.982	
COMPUTE NM HYD B5-D_TWRPND	-	3	.03910	2.79	.112	.05389	1.500	.112 PER 1	MP= 5.00
	10& 3	20	.70360	420.24	21.836	.58191	1.550	.933	
ROUTE RESERVOIR AP#22	20	12	.70360	18.44	21.136	.56324	2.550	.041 AC-F1	r= 15.081
ROUTE AP#22R	12	2	.70360	18.44	21.123	.56291	2.600	.041	
COMPUTE NM HYD B6-D	-	3	.04590	23.22	1.584	.64721	1.700	.790 PER 1	MP= 65.00
ADD HYD AP#23	2& 3	10	.74950	36.14	22.708	.56807	1.750	.075	
ROUTE AP#23R	10	2	.74950	35.42	22.689	.56760	1.800	.074	
COMPUTE NM HYD B7-D	-	3	.05910	33.40	2.101	.66664	1.650	.883 PER 1	MP= 67.00
ADD HYD AP#24		10	.80860	64.31	24.790	.57484	1.700	.124	
ROUTE AP#24R		2	.80860	64.24	24.774	.57445	1.750	.124	
COMPUTE NM HYD B8-D		3	.08910	25.88	2.383	.50146	1.900	.454 PER	MP= 50.00
ADD HYD AP#25		30	.89770	86.89	27.156	.56721	1.800	.151	20100
COMPUTE NM HYD A12-D&AP#26		3	.03590	33.09	1.444	.75409	1.500	1.440 PER	IMP= 76 00
ROUTE AP#26R		2	.03590	31.80	1.444	.75411	1.550	1.384	10.00
COMPUTE NM HYD A13-D		3	.04520	28.90	1.560	.64721	1.600		IMP= 65.00
ADD HYD AP#27		10	.08110	60.36	3.004	.69452	1.550	1.163	IMF - 05.00
ROUTE AP#27R		2	.08110	58.12	3.004	.69452	1.600	1.120	
		3	.04520	22.40	1.677	.69579	1.750		IMP= 70.00
		10	.12630	72.95	4.681	.69497	1.600	.903	IMP- 70.00
ADD HYD AP#28 ROUTE AP#28R		2	.12630	72.22	4.681	.69497	1.600	.893	
									(0.00
COMPUTE NM HYD A15-D		3	.02530	15.45	.808	.59863	1.550	.954 PER	IMP= 60.00
ADD HYD PART_AP#33			.15160	87.33	5.489	.67889	1.600	.900	
COMPUTE NM HYD A17-D&AP#29		3	.01080	6.88	.289	.50146	1.500		IMP= 50.00
ROUTE AP&29F		2	.01080	4.23	.289	.50150	1.600	.613	
COMPUTE NM HYD A18-D		3	.01030	7.80	.329	.59863	1.500		IMP= 60.00
ADD HYD AP#30			.02110	10.81	.618	-54886	1.500	.800	
ROUTE AP&30F		2	.02110	6.01	.618	.54885	1.750	.445	
COMPUTE NM HYD A19-E		3	.01080	7.04	.345	.59863	1.550		IMP= 60.00
ADD HYD AP#3*	1 2& 3		.03190	11.70	.962	.56566	1.600	.573	
ROUTE AP#31F	₹ 10	2	.03190	11.43	.962	.56568	1.600	.560	
COMPUTE NM HYD A20-0	) -	3	.00690	5.23	.220	.59863	1.500	1.184 PER	IMP= 60.00
ADD HYD AP#32	2 28 3	10	.03880	14.86	1.183	.57152	1.600	.598	
ROUTE AP#32F	₹ 10	22	.03880	13.79	1.183	.57153	1.650	.555	
ADD HYD AP#33	3 20&22	10	.19040	100.33	6.672	.65701	1.600	.823	
ROUTE AP#331		2	.19040	100.61	6.672	.65701	1.650	.826	
COMPUTE NM HYD A16-1		3	.06380	23.21	1.706	.50146	1.750		IMP= 50.00
ADD HYD AP#34		_	.25420	120.71	8.378	.61796	1.650	.742	22.00
COMPUTE NM HYD S6-D&AP#3		3	.03780	18.01	1.207	.59863	1.700		IMP= 60.00
ROUTE AP#35		2	.03780	17.52	1.207	.59863	1.750	.724	55.00
COMPUTE NM HYD S7-I		3	.05700	24.87	2.145	.70551	1.850		IMP= 71.00
			.09480	40.63	3.351	.66287	1.800	.670	INF - /1.00
		2	.09480	39.76	3.352				
ROUTE AP#36	. 10	2	.07460	37.10	٤٠٠٠	.66288	1.850	.655	

		HYDROGRAPH	FROM ID	TO ID	AREA	PEAK Discharge	RUNOFF VOLUME	RUNOFF	TIME TO PEAK	CFS PER	PAGE =	3
COMMAND	1	DENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATI	ON
COMPUTE	NM HYD	\$8-D	-	3	.06830	29.31	2.287	.62778	1.800	.671 i	PER IMP=	63.00
ADD HYD		AP#37	2& 3	10	.16310	68.00	5.638	.64817	1.850	.651		
ROUTE		AP#37R	10	2	.16310	68.32	5.638	.64817	1.850	.655		
COMPUTE	NM HYD	S9-D	_	3	.07480	47.24	2.000	.50146	1.500	.987	PER IMP=	50.00
ADD HYD		AP#38	2& 3	20	.23790	83.36	7.639	.60204	1.800	.548		
COMPUTE	NM HYD	C1-D&AP#39	-	3	.03860	32.48	1.372	.66664	1.500	1.315	PER IMP=	67.00
ROUTE		AP#39R	3	2	.03860	31.42	1.372	.66666	1.500	1.272		
COMPUTE	NM HYD	C2-D	-	3	.01880	15.37	.649	.64721	1.500	1.277	PER IMP=	65.00
ADD HYD		AP#40	2& 3	10	.05740	46.79	2.021	.66027	1.500	1.274		
ROUTE		AP#40R	10	2	.05740	45.96	2.021	.66028	1.550	1.251		
COMPUTE	NM HYD	C3-D	-	3	.02340	26.19	1.111	.89013	1.500	1.749	PER IMP=	90.00
ADD HYD		AP#41	2& 3	10	.08080	69.84	3.132	.72683	1.500	1.350		
COMPUTE	NM HYD	C4-D&AP#42	-	3	.03080	27.67	1.207	.73466	1.500	1.403	PER IMP=	74.00
ROUTE		AP#42R	3	2	.03080	27.17	1.207	.73468	1.500	1.378		
ADD HYD		AP#43	10& 2	10	.11160	97.00	4.339	.72899	1.500	1.358		
ROUTE		AP#43R	10	2	.11160	94.99	4.339	.72900	1.550	1.330		
COMPUTE	NM HYD	C5-D	-	3	.00910	6.89	.272	.56068	1.500	1.184	PER IMP=	50.00
ADD HYD		AP#44	2& 3	10	.12070	101.40	4.611	.71630	1.550	1.313		
COMPUTE	NM HYD	C6-D&AP#45	•	3	.01940	21.71	.921	.89013	1.500		PER IMP=	90.00

HYDROGRAP	FROM I ID	TO ID	AREA	PEAK Discharge	RUNOFF VOLUME	RUNOFF	TIME TO PEAK	CFS PAGE PER	= 2
COMMAND IDENTIFICATION		NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE NOTAT	ION
COMPUTE NM HYD S3-		3	.05670	52.60	2.222	.73491	1.500	1 //O DED IND-	
ADD HYD AP#1		10	.10440	100.58	4.399	.78997	1.500	1.449 PER IMP= 1.505	50.00
ROUTE AP#17		2	.10440	101.92	4.399	.78998	1.550	1.525	
COMPUTE NM HYD S4-		3	.04360	42.58	1.993	.85698	1.550	1.526 PER IMP=	60.00
ADD HYD AP#1		10	.14800	144.50	6.391	.80971	1.550	1.526	00.00
ROUTE AP#18		2	.14800	135.23	6.391	.80972	1.550	1.428	
COMPUTE NM HYD S5-		3	.02380	25.87	1.072	.84477	1.500	1.698 PER IMP=	: 50 nn
ADD HYD AP#1		10	.17180	157.67	7.464	.81457	1.550	1.434	37.00
	12&10	10	.29640	265.52	12.845	.81254	1.550	1.400	
ADD HYD PART_AP#2		10	.66450	627.13	31.011	.87502	1.550	1.475	
COMPUTE NM HYD B5-D TWRPN		3	.03910	11.33	.343	.16453	1.500	.453 PER IMP=	5.00
	1 10& 3	20	.70360	637.93	31.354	.83553	1.550	1.417	2.00
ROUTE RESERVOIR AP#2	2 20	12	.70360	21.14	30.140	.80320	2.650	.047 AC-FT=	22.490
ROUTE AP#22	12	2	.70360	21.14	30.122	.80271	2.700	.047	
COMPUTE NM HYD B6-	) -	3	.04590	32.98	2.247	.91802	1.700	1.123 PER IMP=	65.00
ADD HYD AP#2	3 2& 3	10	.74950	48.86	32.369	.80977	1.750	.102	
ROUTE AP#23	R 10	2	.74950	47.94	32,343	.80912	1.800	.100	
COMPUTE NM HYD B7-	) -	3	.05910	47.30	2.971	.94243	1.650	1.251 PER IMP	67.00
ADD HYD AP#2	4 2& 3	10	.80860	90.81	35.314	.81886	1.700	.175	
ROUTE AP#24	R 10	2	.80860	90.32	35.289	.81828	1.750	.175	
COMPUTE NM HYD B8-	o -	3	.08910	38.26	3.492	. <i>7</i> 3491	1.900	.671 PER IMP	50.00
ADD HYD AP#2		30	.89770	122.92	38.781	.81001	1.800	.214	
COMPUTE NM HYD A12-D&AP#2		3	.03590	46.03	2.015	1.05230	1.500	2.003 PER IMP	76.00
ROUTE AP#26	R 3	2	.03590	44.24	2.015	1.05231	1.550	1.925	
COMPUTE NM HYD A13-	D -	3	.04520	41.11	2.213	.91802	1.600	1.421 PER IMP	65.00
ADD HYD AP#2		10	.08110	85.04	4.228	.97745	1.550	1.638	
ROUTE AP#27		2	.08110	81.75	4.228	.97746	1.600	1.575	
COMPUTE NM HYD A14-		3	.04520	31.52	2.360	.97905	1.750	1.089 PER IMP	70.00
ADD HYD AP#2		10	.12630	103.43	6.588	.97802	1.600	1.280	
ROUTE AP#28		2	.12630	102.75	6.588	.97803	1.600	1.271	
COMPUTE NM HYD A15-		3	.02530	22.32	1.156	.85698	1.550	1.379 PER IMP	= 60.00
ADD HYD PART_AP#3			.15160	124.54	7.744	.95782	1.600	1.284	
COMPUTE NM HYD A17-D&AP#2		3	.01080	10.40	.423	.73491	1.500	1.505 PER IMP	= 50.00
ROUTE AP&29		2	.01080	6.82	.423	<b>.</b> 73495	1.600	.986	
COMPUTE NM HYD A18-		3	.01030	11.34	.471	.85698	1.500	1.721 PER IMP	= 60.00
ADD HYD AP#3			.02110	16.27	.894	.79446	1.550	1.205	
ROUTE AP&30		2	.02110	9.74	.894	.79445	1.700	.721	
COMPUTE NM HYD A19-		3	.01080	10.18	.494	.85698	1.550	1.473 PER IMP	= 60.00
ADD HYD AP#3			.03190	18.22	1.388	.81559	1.600	.893	
ROUTE AP#3'		2	.03190	17.85	1.388	.81560	1.600	.874	
COMPUTE NM HYD A20-		3	.00690	7.60	.315	.85698	1.500	1.721 PER IMP	= 60.00
ADD HYD AP#3			.03880	22.90	1.703	.82294	1.600	.922	
ROUTE AP#3		22	.03880	21.53	1.703	.82295	1.650	.867	
	3 20&22		.19040	145.20	9.447	.93033	1.600	1.192	
ROUTE AP#33		2	.19040	144.79	9.447	.93033	1.650	1.188	F0 00
COMPUTE NM HYD A16-		3	.06380	34.20 174.00	2.501	.73491	1.750	.838 PER IMP	= 50.00
ADD HYD AP#			.25420	174.99	11.948	.88128	1.650	1.076	/6 55
COMPUTE NM HYD S6-D&AP#3		3	.03780	25.85 25.10	1.728	.85698	1.700	1.068 PER IMP	= 60.00
ROUTE AP#3!		2	.03780	25.19	1.728	.85698	1.750	1.041	74 00
COMPUTE NM HYD S7		3	.05700 .09480	34.90 57.44	3.013	.99126	1.850	.957 PER IMP	= /1.00
ADD HYD AP#3		10		57.66 56.61	4.741	.93770	1.800	.950	
ROUTE AP#3	ık IU	2	.09480	10.01	4.741	.93771	1.850	.933	

	FROM	TO		PEAK	RUNOFF		TIME TO	CFS	PAGE =	: 3
HYDROGRAP	i ID	ID	AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER		
COMMAND IDENTIFICATIO	i NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATI	ON
COMPUTE NM HYD S8-	) -	3	.06830	41.75	3.255	.89360	1.800	.955 P	ER IMP=	63.00
ADD HYD AP#3	7 2& 3	10	.16310	97.31	7.996	.91923	1.800	.932		
ROUTE AP#37	₹ 10	2	.16310	97.38	7.996	.91924	1.850	.933		
COMPUTE NM HYD S9-	) -	3	.07480	71.67	2.932	.73491	1.500	1.497 P	ER IMP=	50.00
ADD HYD AP#3	3 2& 3	20	.23790	120.04	10.928	.86127	1.800	.788		
COMPUTE NM HYD C1-D&AP#3	- (	3	.03860	46.22	1.940	.94243	1.500	1.871 P	ER IMP=	67.00
ROUTE AP#39	₹ 3	2	.03860	44.71	1.940	.94245	1.500	1.810		
COMPUTE NM HYD C2-	) -	3	.01880	22.00	.920	.91802	1.500	1.828 P	ER IMP=	65.00
ADD HYD AP#4	0 2& 3	10	.05740	66.71	2.861	.93443	1.500	1.816		
ROUTE AP#40	R 10	2	.05740	65.45	2.861	.93444	1.550	1.782		
COMPUTE NM HYD C3-	- 0	3	.02340	35.46	1.527	1.22320	1.500	2.368 P	ER IMP=	90.00
ADD HYD AP#4	1 2& 3	10	.08080	98.24	4.387	1.01805	1.500	1.900		
COMPUTE NM HYD C4-D&AP#4	2 -	3	.03080	38.65	1.688	1.02788	1.500	1.961 P	ER IMP=	74.00
ROUTE AP#42	R 3	2	.03080	37.98	1.688	1.02790	1.500	1.927		
ADD HYD AP#4	3 10& 2	10	.11160	136.22	6.076	1.02077	1.500	1.907		
ROUTE AP#43	R 10	2	.11160	133.80	6.076	1.02077	1.550	1.873		
COMPUTE NM HYD C5-	D -	3	.00910	10.46	.403	.82943	1.500	1.795 P	ER IMP≔	50.00
ADD HYD AP#4	4 2& 3	10	.12070	143.51	6.478	1.00634	1.550	1.858		
COMPUTE NM HYD C6-D&AP#4	5 -	3	.01940	29.40	1.266	1.22320	1.500		ER IMP=	90.00
FINISH										

# AMOLE DEL NORTE STORM DRAINAGE FACILITIES TOWER/SAGE DRAINAGE MASTER PLAN

### AHYMO SUMMARY TABLE - 10 YEAR - 6 HOUR STORM

AHYMO SUMMARY TABLE (AHYMO194) - AMAFCA Hydrologic Model - January, 1994
INPUT FILE = MASTER10.IN

RUN DATE (MON/DAY/YR) =12/10/1994 USER NO.= ANASRONM.IO1

01 1122												
	н	YDROGRAPH	FROM ID	TO ID	AREA	PEAK Discharge	RUNOFF VOLUME	RUNOFF	TIME TO PEAK	CFS PER	PAGE =	1
COMMAND		IFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATIO	ON
START											TIME=	.00
	TYPE= 1										RAIN6=	1.470
SEDIMENT B				_	0/500	(0.0)	0 555	4 04407	4 577		PK BF =	1.05
COMPUTE NM	HYD	A1-D&AP#1		3	.04580	69.84	2.555	1.04607	1.533		PER IMP=	76.00
ROUTE		AP-1R	3	2	.04580	68.19	2.555	1.04608	1.533	2.326		
COMPUTE NM	HYD	A2-D		3	.03950	58.73	2.070	.98256	1.500		PER IMP=	70.00
ADD HYD		AP#2	2& 3	10	.08530	126.03	4.625	1.01666	1.533	2.309		
ROUTE		AP#2R	10	2	.08530	121.55	4.625	1.01666	1.567	2.227	D=D	<b>45.00</b>
COMPUTE NM	I HYD	A3-D		-	.04190	62.00 178.95	2.077	.92964	1.500		PER IMP=	65.00
ADD HYD		AP#3	2& 3 10	10 2	.12720 .12720	176.30	6.703 6.703	.98799 .98799	1.533 1.567	2.198 2.166		
ROUTE	LUVO	AP#3R	-	3	.04390	69.37	2.548		1.533		DED IMP-	00.00
COMPUTE NM	ו אזט	A4-D AP#4	2& 3	10	.17110	244.00	9.251	1.08841 1.01375	1.533	2.469	PER IMP=	80.00
ADD HYD ROUTE		AP#4R	10	2	.17110	243.66	9.251	1.01376	1.567	2.225		
	UVO	AF#4K A5-D	-	3	.04520	60.67	2.113	.87671	1.500		DED IND-	40.00
COMPUTE NM	טוח ו	AP#5	2& 3	10	.21630	298.09	11.364	.98511	1.533	2.153	PER IMP=	80.00
ADD HYD ROUTE		AP#5R	10	2	.21630	300.22	11.364	.98512	1.567	2.169		
COMPUTE NM	4 HVD	A6-D	-	3	.04520	54.14	1.858	.77086	1.500		PER IMP=	50.00
ADD HYD	יוווט	PART AP#9	2& 3	10	.26150	348.39	13.223	.94808	1.567	2.082	TER THE	30.00
COMPUTE NM	4 UVD	A7-D		3	.02060	24.68	.847	.77086	1.500		PER IMP=	50.00
ADD HYD	יו וווט	PART AP#9	102 3	10	.28210	370.35	14.069	.93514	1.567	2,051	TER THE	30.00
COMPUTE NM	A HVD	A8-D&AP#6	-	3	.05700	73.08	2.987	.98256	1.567		PER IMP=	70.00
ROUTE	1 1115	AP&6R	3	2	.05700	69.35	2.987	.98256	1.600	1.901	1 EK 1141 -	10.00
COMPUTE NM	M HYD	A9-D	-	3	.01020	12.85	.419	.77086	1.500		PER IMP=	50 00
ADD HYD		AP#7	2& 3	20	.06720	78.19	3.406	.95042	1.600	1.818		30.00
ROUTE		AP#7R	20	2	.06720	77.45	3.406	.95042	1.600	1.801		
COMPUTE NA	HYD	A10-D	-	3	.01020	12.85	.419	.77086	1.500		PER IMP=	50.00
ADD HYD		AP#8	2& 3	20	.07740	86.29	3.826	.92675	1.600	1.742		
ROUTE		AP#8R	20	2	.07740	84.57	3.826	.92676	1.633	1.707		
ADD HYD			10& 2	10	.35950	444.68	17.895	.93333	1.567	1.933		
ROUTE		AP#9R		2	.35950	445.31	17.895	.93333	1.567	1.935		
COMPUTE N	M HYD	A11-D	-	3	.00860	14.12	.480	1.04607	1.500	2.566	PER IMP=	76.00
ADD HYD		AP#10	2& 3	20	.36810	456.74	18.375	.93596	1.567	1.939		
COMPUTE N	M HYD	B1-D&AP#11	-	3	.02300	35.05	1.179	.96139	1.500	2.381	PER IMP=	68.00
ROUTE		AP#11R	3	2	.02300	30.26	1.179	.96140	1.567	2.056		
COMPUTE N	M HYD	82-D	-	3	.03500	49.22	1.637	.87671	1.500	2.197	PER IMP=	60.00
ADD HYD		AP#12	2& 3	10	.05800	76.96	2.816	.91028	1.533	2.073		
ROUTE		AP#12R	10	2	.05800	70.87	2.816	.91029	1.567	1.909		
COMPUTE N	M HYD	B3-D	-	3	.04360	50.81	1.793	.77086	1.533	1.821	PER IMP=	50.00
ADD HYD		AP#13		10	.10160	117.94	4.608	.85045	1.533	1.814		
ROUTE		AP#13R		2	.10160	118.15	4.608	.85045	1.567	1.817		
COMPUTE N	M HYD	B4-D		3	.02300	28.97	.946	.77086	1.500		PER IMP=	50.00
ADD HYD		AP#14		10	.12460	142.09	5.554	.83575	1.567	1.782		
ROUTE		AP#14R		12	.12460	142.64	5.554	.83576	1.567	1.789		
COMPUTE N	M HYD	S1-D&AP#15		3	.03140	46.47	1.557	.92964	1.500		PER IMP=	65.00
ROUTE		AP-15R		2	.03140	45.36	1.557	.92964	1.533	2.257		
COMPUTE N	M HYD	S2-D		3	.01630	20.53	.670	.77086	1.500		PER IMP=	50.00
ADD HYD		AP#16			.04770	64.98	2.227	.87537	1.533	2.129		
ROUTE		AP#16R	10	2	.04770	64.75	2.227	.87538	1.533	2.121		

		FROM	то		PEAK	RUNOFF		TIME TO	CFS	PAGE =	= 2
	HYDROGRAPH	ID	ID	AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER		
COMMAND ID	ENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTAT	ION
COMPUTE NM HYD	s3-D	-	3	.05670	67.91	2.331	.77086	1.500	1 872 5	ER IMP=	50.00
ADD HYD	AP#17		10	.10440	132.26	4.558	.81861	1.533	1.979	LK IMF-	30.00
ROUTE	AP#17R	10	2	.10440	129.72	4.558	.81861	1.533	1.942		
COMPUTE NM HYD	S4-D	•	3	.04360	55.28	2.039	.87671	1.533		ER IMP=	60.00
ADD HYD	AP#18	2& 3	10	.14800	185.00	6.597	.83572	1.533	1.953		00100
ROUTE	AP#18R	10	2	.14800	174.83	6.597	.83572	1.567	1.846		
COMPUTE NM HYD	\$5-D	-	3	.02380	33.12	1.099	.86612	1.500		ER IMP=	59.00
ADD HYD	AP#19	2& 3	10	.17180	201.97	7.696	.83993	1.567	1.837		
ADD HYD	AP#20	12&10	10	.29640	344.61	13.250	.83818	1.567	1.817		
ADD HYD	PART AP#21	20&10	10	.66450	801.35	31.625	.89235	1.567	1.884		
COMPUTE NM HYD	B5-D TWRPND	-	3	.03910	20.97	.559	.26796	1.533		PER IMP=	5.00
ADD HYD		10& 3	20	.70360	820.24	32.184	.85765	1.567	1.822		2100
ROUTE RESERVOIR	AP#22	20	12	.70360	22.56	27.419	.73067	2.733		AC-FT=	28.648
ROUTE	AP#22R	12	2	.70360	22.56	27.370	.72937	2.767	.050		
COMPUTE NM HYD	B6-D	-	3	.04590	40.84	2.276	.92964	1.700		PER IMP=	65.00
ADD HYD	AP#23	2& 3	10	.74950	58.74	29.646	.74163	1.733	.122		
ROUTE	AP#23R	10	2	.74950	57.42	29.578	.73995	1.767	.120		
COMPUTE NM HYD	B7-D	-	3	.05910	58.43	2.997	.95081	1.667		PER IMP=	67.00
ADD HYD	AP#24	2& 3	10	.80860	110.96	32.575	.75537	1.700	.214		
ROUTE	AP#24R	10	2	.80860	110.02	32.517	.75400	1.733	.213		
COMPUTE NM HYD	<b>B8-</b> D	-	3	.08910	48.60	3.663	.77086	1.900		PER IMP=	50.00
ADD HYD	AP#25	2& 3	30	.89770	151.40	36.180	.75568	1.767	.264		
COMPUTE NM HYD	A12-D&AP#26		3	.03590	56.49	2.003	1.04607	1.500		PER IMP=	76.00
ROUTE	AP#26R	3	2	.03590	55.04	2.003	1.04608	1.533	2.395		
COMPUTE NM HYD	A13-D	-	3	.04520	51.60	2.241	.92964	1.567	1.784	PER IMP=	65.00
ADD HYD	AP#27	2& 3	10	.08110	104.41	4.244	.98117	1.567	2.012		
ROUTE	AP#27R	10	2	.08110	100.48	4.244	.98117	1.600	1.936		
COMPUTE NM HYD	A14-D	-	3	.04520	38.70	2.369	.98256	1.767	1.338	PER IMP=	70.00
ADD HYD	AP#28	2& 3	10	.12630	126.50	6.612	.98166	1.600	1.565		
ROUTE	AP#28R	10	2	.12630	125.93	6.612	.98166	1.633	1.558		
COMPUTE NM HYD	A15-D	-	3	.02530	28.32	1.183	.87671	1.567	1.749	PER IMP=	60.00
ADD HYD	PART_AP#33	2& 3	20	.15160	152.70	7.795	.96414	1.600	1.574		
COMPUTE NM HYD	A17-D&AP#29	-	3	.01080	13.61	.444	.77086	1.500		PER IMP=	50.00
ROUTE	AP&29R	3	2	.01080	9.06	.444	.77088	1.600	1.311		
COMPUTE NM HYD	A18-D		3	.01030	14.49	.482	.87671	1.500	2.198	PER IMP=	60.00
ADD HYD	AP#30		10	.02110	21.78	.926	.82249	1.533	1.613		
ROUTE	AP&30R		2	.02110	13.18	.926	.82251	1.667	.976		
COMPUTE NM HYD	A19-D		3	.01080	12.75	.505	.87671	1.567	1.845	PER IMP=	60.00
ADD HYD	AP#31	2& 3	10	.03190	24.19	1.430	.84080	1.600	1.185		
ROUTE	AP#31R	10	2	.03190	23.73	1.431	.84081	1.633	1.162		
COMPUTE NM HYD	A20-D		3	.00690	9.71	.323	.87671	1.500		PER IMP=	60.00
ADD HYD	AP#32		10	.03880	30.03	1.753	.84717	1.600	1.209		
ROUTE	AP#32R		22	.03880	28.02	1.753	.84718	1.633	1.128		
ADD HYD		20&22		.19040	179.65	9.548	.94031	1.600	1.474		
ROUTE	AP#33R		2	.19040	178.37	9.549	.94031	1.633	1.464		
COMPUTE NM HYD	A16-D		3	.06380	43.34	2.623	.77086	1.733		PER IMP=	50.00
ADD HYD	AP#34		10	.25420	216.66	12.171	.89778	1.667	1.332		
COMPUTE NM HYD	S6-D&AP#35		3	.03780	32.34	1.767	.87671	1.700		PER IMP=	60.00
ROUTE	AP#35R		2	.03780	31.61	1.767	.87671	1.733	1.307		
COMPUTE NM HYD	S7-D		3	.05700	42.77	3.019	.99315	1.867	1.173	PER IMP=	71.00
ADD HYD	AP#36			.09480	71.13	4.787	.94670	1.800	1.172		
ROUTE	AP#36R	₹ 10	2	.09480	69.58	4.787	.94671	1.833	1.147		

		FROM	то		PEAK	RUNOFF		TIME TO	CFS PAGE =	2
	HYDROGRAPH	ID	ID	AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER	_
COMMAND ID	ENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE NOTATION	
COMPLIES NW HAD	\$3-D	-	3	.05670	119.63	4.223	1.39652	1.500	3.297 PER IMP= 50	
COMPUTE NM HYD	AP#17	2& 3	10	.10440	227.71	8.117	1.45773	1.533	3.408	
ADD HYD ROUTE	AP#17R	10	2	.10440	224.43	8.117	1.45773	1.533	3.359	
COMPUTE NM HYD	S4-D	-	3	.04360	93.23	3.563	1.53221	1.533		0.00
ADD HYD	AP#18	2& 3	10	.14800	317.66	11.679	1.47967	1.533	3.354	
	AP#18R	10	2	.14800	301.32	11.680	1.47967	1.567	3.181	
ROUTE NM HVD	S5-D	-	3	.02380	56.16	1.928	1.51864	1.500		2.00
COMPUTE NM HYD	AP#19		10	.17180	347.65	13.607	1.48506	1.567	3.162	
ADD HYD	AP#20		10	.29640	599.14	23.440	1.48281	1.567	3.158	
ADD HYD	PART_AP#21	20210	10	.66450	1364.74	55.012	1.55226	1.567	3.209	
ADD HYD	B5-D_TWRPND	-	3	.03910	54.90	1.551	.74390	1.500		5.00
COMPUTE NM HYD	AP#21		20	.70360	1414.13	56.563	1.50734	1.567	3.140	.00
ADD HYD		20	12	.70360	25.11	35.845	.95522	2.967		074
ROUTE RESERVOIR	AP#22			.70360	25.11	35.760	.95294	3.000		.036
ROUTE	AP#22R	12	2	.04590	67.94	3.917	1.60006	1.700	.056	- 00
COMPUTE NM HYD	86-D				89.59	39.676			2.313 PER IMP= 65	0.00
ADD HYD	AP#23	2& 3	10	.74950	87.10		.99257	1.700	.187	
ROUTE	AP#23R	10	2	.74950		39.564	.98976	1.767	.182	7 00
COMPUTE NM HYD	B7-D	-	3	.05910	96.51	5.129	1.62720	1.667	2.552 PER IMP= 67	7.00
ADD HYD	AP#24		10	.80860	178.28	44.693	1.03635	1.700	.345	
ROUTE	AP#24R	10	2	.80860	176.50	44.595	1.03409	1.733	.341	
COMPUTE NM HYD	88-D		3	.08910	85.98	6.636	1.39652	1.900		0.00
ADD HYD	AP#25	2& 3	30	89770	249.59	51.232	1.07006	1.767	.434	
COMPUTE NM HYD	A12-D&AP#26		3	.03590	90.60	3.349	1.74932	1.500		6.00
ROUTE	AP#26R	3	2	.03590	88.53	3.349	1.74933	1.533	3.853	
COMPUTE NM HYD	A13-D	· -	3	.04520	85.68	3.857	1.60006	1.567	2.962 PER IMP= 65	5.00
ADD HYD	AP#27		10	.08110	170.19	7.207	1.66612	1.567	3.279	
ROUTE	AP#27R		2	.08110	163.37	7.207	1.66613	1.567	3.148	
COMPUTE NM HYD	A14-D		3	.04520	63.41	4.021	1.66790	1.767	2.192 PER IMP= 70	0.00
ADD HYD	AP#28		10	.12630	206.62	11.227	1.66675	1.600	2.556	
ROUTE	AP#28R		2	.12630	205.14	11.227	1.66676	1.633	2.538	
COMPUTE NM HYD	A15-D		3	.02530	47.80	2.067	1.53221	1.567		0.00
ADD HYD	PART_AP#33			.15160	250.62	13.295	1.64430	1.600	2.583	
COMPUTE NM HYD	A17-D&AP#29		3	.01080	23.94	.804	1.39652	1.500	3.464 PER IMP= 50	0.00
ROUTE	AP&29R		2	.01080	17.25	.804	1.39654	1.567	2.496	
COMPUTE NM HYD	A18-D		3	.01030	24.48	.842	1.53221	1.500	3.713 PER IMP= 60	0.00
ADD HYD	AP#30			.02110	39.23	1.646	1.46272	1.533	2.905	
ROUTE	AP&30R		2	.02110	27.05	1.646	1.46274	1.633	2.003	
COMPUTE NM HYD	A19-D	-	3	.01080	21.52	.883	1.53221	1.567	3.114 PER IMP= 60	0.00
ADD HYD	AP#31	2& 3		.03190	46.47	2.529	1.48619	1.600	2.276	
ROUTE	AP#31R	10	2	.03190	45.55	2.529	1.48621	1.633	2.231	
COMPUTE NM HYD	A20-D	-	3	.00690	16.40	.564	1.53221	1.500	3.715 PER IMP= 60	0.00
ADD HYD	AP#32	2& 3	10	.03880	56.70	3.092	1.49437	1.600	2.283	
ROUTE	AP#32R	10	22	.03880	53.24	3.092	1.49438	1.633	2.144	
ADD HYD	AP#33	20&22	10	.19040	302.55	16.387	1.61374	1.600	2.483	
ROUTE	AP#33R	10	2	.19040	300.65	16.387	1.61375	1.633	2.467	
COMPUTE NM HYD	A16-D		3	.06380	76.29	4.752	1.39652	1.733	1.868 PER IMP= 50	0.00
ADD HYD	AP#34		10	.25420	368.19	21.139	1.55922	1.667	2.263	
COMPUTE NM HYD	\$6-D&AP#35		3	.03780	54.70	3.089	1.53221	1.700		0.00
ROUTE	AP#35R		2	.03780	53.55	3.089	1.53221	1.733	2.213	
COMPUTE NM HYD	S7-D		3	.05700	69.88	5.112	1.68147		1.915 PER IMP= 7	1.00
ADD HYD	AP#36			.09480	118.32	8.201	1.62194		1.950	
ROUTE	AP#36F		2	.09480	115.67	8.201	1.62195		1.906	
	301		_							

				FROM	TO		PEAK	RUNOFF		TIME TO	CFS	PAGE =	3	
			HYDROGRAPH	ID	ID	AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER			
COMMAND		I	DENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATI	ON	
COMPUTE	NM	HYD	\$8-D	-	3	.06830	51.91	3.309	.90847	1.767	1.187	PER IMP=	63.00	
ADD HYD			AP#37	2& 3	10	.16310	120.45	8.096	.93069	1.833	1.154			
ROUTE			AP#37R	10	2	.16310	120.46	8.096	.93069	1.833	1.154			
COMPUTE	NM	HYD	S9-D	-	3	.07480	93.91	3.075	.77086	1.500	1.962	PER IMP=	50.00	
ADD HYD			AP#38	2& 3	20	.23790	148.71	11.171	.88043	1.800	.977			
COMPUTE	NM	HYD	C1-D&AP#39	_	3	.03860	58.26	1.957	.95081	1.500	2.358	PER IMP=	67.00	
ROUTE			AP#39R	3	2	.03860	56.81	1.957	.95081	1.533	2.300			
COMPUTE	NM	HYD	C2-D	_	3	.01880	27.83	.932	.92964	1.500	2.313	PER IMP=	65.00	
ADD HYD			AP#40	2& 3	10	.05740	83.20	2.889	.94386	1.533	2.265			
ROUTE			AP#40R	10	2	.05740	83.01	2.890	.94387	1.533	2.260			
COMPUTE	NM	HYD	C3-D	-	3	.02340	43.23	1.490	1.19426	1.500	2.887	PER IMP=	90.00	
ADD HYD			AP#41	2& 3	10	.08080	123.65	4.380	1.01638	1.533	2.391			
COMPUTE		HYD	C4-D&AP#42	_	3	.03080	47.58	1.684	1.02490	1.500	2.414	PER IMP=	74.00	
ROUTE			AP#42R	3	2	.03080	47.65	1.684	1.02491	1.533	2.417			
ADD HYD				10& 2	10	.11160	171.29	6.063	1.01873	1.533	2.398			
ROUTE			AP#43R	10	2	.11160	162.28	6.063	1.01873	1.567	2.272			
COMPUTE	NM	HYD	C5-D	-	3	.00910	13.14	.429	.88414	1.500		PER IMP=	50.00	
ADD HYD			AP#44	2& 3	10	.12070	174.80	6.493	1.00858	1.533	2.263			
COMPUTE FINISH		HYD		-	3	.01940	35.85	1.236	1.19426	1.500		PER IMP=	90.00	

### AMOLE DEL NORTE STORM DRAINAGE FACILITIES **TOWER/SAGE DRAINAGE MASTER PLAN**

### AHYMO SUMMARY TABLE - 10 YEAR - 24 HOUR STORM

AHYMO SUMMARY TABLE (AHYMO194) - AMAFCA Hydrologic Model - January, 1994 RUN DATE (MON/DAY/YR) =12/10/1994 INPUT FILE = MAST2410.IN

USER NO. = ANASRONM. IO1

	HYDROGRAPH	FROM ID	TO ID	AREA	PEAK DISCHARGE	RUNOFF VOLUME	RUNOFF	TIME TO PEAK	CFS PER	PAGE =	1
COMMAND	IDENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATIO	ON
START										TIME=	.00
	PE= 2									RA I N24=	1.780
SEDIMENT BUL			7	.04580	68.62	3,162	4 20/75	4 500		PK BF =	1.05
COMPUTE NM H	HYD A1-D&AP#1 AP-1R	- 3	3 2	.04580	67.80	3.162	1.29435 1.29436	1.500 1.550	2.341	PER IMP=	76.00
COMPUTE NM H		-	3	.03950	58.32	2.551	1.21103	1.500		PER IMP=	70.00
ADD HYD	AP#2	2& 3	10	.08530	121.60	5.713	1.25576	1.500	2.227	- LK THE-	70.00
ROUTE	AP#2R	10	2	.08530	122.25	5.713	1.25577	1.550	2.239		
COMPUTE NM F		-	3	.04190	60.91	2.551	1.14160	1.500		PER IMP=	65.00
ADD HYD	AP#3	2& 3	10	.12720	175.06	8.264	1.21816	1.550	2.150		
ROUTE	AP#3R	10	2	.12720	177.74	8.264	1.21816	1.550	2.183		
COMPUTE NM 1	HYD A4-D	-	3	.04390	68.23	3.161	1.34990	1.500	2.429	PER IMP=	80.00
ADD HYD	AP#4	2& 3	10	.17110	242.91	11.425	1.25196	1.550	2.218		
ROUTE	AP#4R	10	2	.17110	244.83	11.425	1.25196	1.550	2.236		
COMPUTE NM I		-	3	.04520	60.28	2.585	1.07217	1.500		PER IMP=	60.00
ADD HYD	AP#5	2& 3	10	.21630	300.08	14.009	1.21439	1.550	2.168		
ROUTE	AP#5R	10	2	.21630	300.55	14.009	1.21439	1.550	2.171	DED 140	F0 00
COMPUTE NM I		- 20.7	3	.04520	53.83 350.21	2.250 16.259	.93330 1.16580	1.500		PER IMP=	50.00
ADD HYD	PART_AP#9 HYD A7-D	2& 3	10 3	.26150 .02060	24.54	1.025	.93330	1.550 1.500	2.093	PER IMP=	E0.00
COMPUTE NM I	PART AP#9	102.3	10	.28210	372.85	17.284	1.14882	1.550	2.065	PER IMP-	30.00
COMPUTE NM	_	1002 3	3	.05700	72.44	3.682	1.21103	1.550		PER IMP=	70.00
ROUTE	AP&6R	3	2	.05700	69.75	3.682	1.21104	1.600	1.912	, ex tra -	,0.00
COMPUTE NM		-	3	.01020	12.64	.508	.93330	1.500		PER IMP=	50.00
ADD HYD	AP#7	2& 3	20	.06720	78.23	4.189	1.16887	1.600	1.819		20100
ROUTE	AP#7R	20	2	.06720	78.03	4.189	1.16888	1.600	1.814		
COMPUTE NM		-	3	.01020	12.64	.508	.93330	1.500	1.936	PER IMP=	50.00
ADD HYD	AP#8	2& 3	20	.07740	86.51	4.697	1.13782	1.600	1.746		
ROUTE	AP#8R	20	2	.07740	84.14	4.697	1.13783	1.650	1.699		
ADD HYD	AP#9	10& 2	10	.35950	443.11	21.981	1.14645	1.550	1.926		
ROUTE	AP#9R	10	2	.35950	442.23	21.981	1.14645	1.550	1.922		
COMPUTE NM		-	3	.00860	13.87	.594	1.29435	1.500		PER IMP=	76.00
ADD HYD	AP#10	2& 3	20	.36810	454.18	22.575	1.14991	1.550	1.928		
COMPUTE NM		-	3	.02300	34.43	1.451	1.18326	1.500		PER IMP=	68.00
ROUTE	AP#11R	3	2	.02300	30.50 48.37	1.451 2.001	1.18328 1.07217	1.550	2.072	DED IND-	(0.00
COMPUTE NM			10	.03500 .05800	46.37 75.46	3.453	1.11621	1.500 1.500	2.139	PER IMP=	60.00
ADD HYD ROUTE	AP#12 AP#12R		2	.05800	70.44	3.453	1.11623	1.550	1.898		
COMPUTE NM	_	-	3	.04360	49.48	2.170	.93330	1.500		PER IMP=	50.00
ADD HYD	AP#13		10	.10160	118.42	5.623	1.03772	1.550	1.821	FER IMF	50.00
ROUTE	AP#13R		2	.10160	116.28	5.623	1.03772	1.550	1.788		
COMPUTE NM			3	.02300	28.48	1.145	.93330	1.500		PER IMP=	50.00
ADD HYD	AP#14			.12460	141.21	6.768	1.01844	1.550	1.771		
ROUTE	AP#14R		12	.12460	140.69	6.768	1.01845	1.550	1.764		
COMPUTE NM	HYD S1-D&AP#15		3	.03140	45.64	1.912	1.14160	1.500	2.271	PER IMP=	65.00
ROUTE	AP-15R		2	.03140	44.09	1.912	1.14162	1.500	2.194		
COMPUTE NM			3	.01630	20.19	.811	.93330	1.500		PER IMP=	50.00
ADD HYD	AP#16			.04770	64.28	2.723	1.07041	1.500	2.106		
ROUTE	AP#16R	10	2	.04770	63.42	2.723	1.07042	1.550	2.077		

HADDOCUAD	FROM	TO	ADEA	PEAK	RUNOFF	DIMOSS	TIME TO	CFS	PAGE =	= 2
HYDROGRAP COMMAND IDENTIFICATIO		ID NO.	AREA (SQ MI)	DISCHARGE (CFS)	VOLUME (AC-FT)	RUNOFF (INCHES)	PEAK (HOURS)	PER ACRE	NOTATI	ION
COMPUTE NM HYD S3-	) -	3	.05670	67.53	2.822	.93330	1.500	1 861 0	ER IMP=	E0 00
ADD HYD AP#1		10	.10440	128.10	5.545	.99594	1.500	1.917	EK IMP-	30.00
ROUTE AP#17		2	.10440	129.55	5.545	.99595	1.550	1.939		
COMPUTE NM HYD S4-		3	.04360	53.32	2.493	1.07217	1.550		ER IMP=	60.00
ADD HYD AP#1		10	.14800	182.86	8.039	1.01840	1.550	1.931		00.00
ROUTE AP#18		2	.14800	173.14	8.039	1.01840	1.550	1.828		
COMPUTE NM HYD S5-		3	.02380	32.55	1.343	1.05828	1.500		ER IMP=	59.00
ADD HYD AP#1	9 2& 3	10	.17180	201.46	9.382	1.02392	1.550	1.832		27100
ADD HYD AP#2	0 12&10	10	.29640	342.15	16.150	1.02162	1.550	1.804		
ADD HYD PART_AP#2		10	.66450	796.34	38.725	1.09268	1.550	1.872		
COMPUTE NM HYD B5-D_TWRPN	o -	3	.03910	20.53	.589	.28248	1.500		ER IMP=	5.00
	1 10& 3	20	.70360	815.60	39.314	1.04766	1.550	1.811		
ROUTE RESERVOIR AP#2	2 20	12	.70360	22.55	37.241	.99242	2.700		C-FT=	28.615
ROUTE AP#22	R 12	2	.70360	22.55	37.214	.99170	2.750	.050		
COMPUTE NM HYD B6-	D -	3	.04590	40.70	2.795	1.14160	1.700		ER IMP=	65.00
ADD HYD AP#2	3 2& 3	10	.74950	58.48	40.009	1.00088	1.700	.122		
ROUTE AP#23	R 10	2	.74950	57.47	39.971	.99994	1.750	.120		
COMPUTE NM HYD B7-	D -	3	.05910	58.27	3.686	1.16937	1.650		ER IMP=	67.00
ADD HYD AP#2	4 2& 3	10	.80860	111.08	43.657	1.01233	1.700	.215		
ROUTE AP#24	R 10	2	.80860	110.07	43.624	1.01156	1.750	.213		
COMPUTE NM HYD B8-		3	.08910	48.46	4.435	.93330	1.900	.850 F	ER IMP=	50.00
ADD HYD AP#2			.89770	151.32	48.059	1.00379	1.750	.263		
COMPUTE NM HYD A12-D&AP#2		3	.03590	56.08	2.478	1.29435	1.500		ER IMP=	76.00
ROUTE AP#26		2	.03590	53.92	2.478	1.29437	1.550	2.347		
COMPUTE NM HYD A13-		3	.04520	50.84	2.752	1.14160	1.600		PER IMP=	65.00
ADD HYD AP#2			.08110	104.48	5.230	1.20921	1.550	2.013		
ROUTE AP#27		2	.08110	100.28	5.230	1.20922	1.600	1.932		
COMPUTE NM HYD A14-		3	.04520	38.63	2.919	1.21103	1.750		PER IMP=	70.00
ADD HYD AP#2			.12630	127.40	8.150	1.20986	1.600	1.576		
ROUTE AP#28		2	.12630	126.72	8.150	1.20986	1.600	1.568		
COMPUTE NM HYD A15-		3	.02530	27.89	1.447	1.07217	1.550		PER IMP=	60.00
ADD HYD PART_AP#3			.15160	153.94	9.596	1.18688	1.600	1.587		
COMPUTE NM HYD A17-D&AP#		3	.01080	13.38	.538	.93330	1.500		PER IMP=	50.00
ROUTE AP&29		2	.01080	9.06	.538	.93334	1.600	1.311		
COMPUTE NM HYD A18		3	.01030	14.24	.589	1.07217	1.500		PER IMP=	60.00
ADD HYD AP#3			.02110	21.01	1.127	1.00106	1.550	1.556		
ROUTE AP&30		2	.02110	13.26	1.126	1.00104	1.650	.982		
COMPUTE NM HYD A19		3	.01080	12.72	.618	1.07217	1.550		PER IMP=	60.00
ADD HYD AP#3			.03190	24.03	1.744	1.02509	1.600	1.177		
ROUTE AP#3		2	.03190	23.54	1.744	1.02510	1.600	1.153		
COMPUTE NM HYD A20		3	.00690	9.54	.395	1.07217	1.500		PER IMP=	60.00
ADD HYD AP#3			.03880	29.89	2.139	1.03345	1.600	1.204		
ROUTE AP#3		22	.03880	28.27	2.139	1.03345	1.650	1.138		
	3 20&22		.19040	181.25	11.735	1.15561	1.600	1.487		
ROUTE AP#3:		2	.19040	180.24	11.735	1.15561	1.650	1.479		FO 00
COMPUTE NM HYD A16		3	.06380 .25420	43.27	3.176	.93330	1.750		PER IMP=	50.00
ADD HYD AP# COMPUTE NM HYD S6-D&AP#			.03780	218.83 32.14	14.910	1.09981	1.650	1.345	DED 1110	(0.00
		3	.03780		2.161	1.07217	1.700		PER IMP=	60.00
ROUTE AP#3 COMPUTE NM HYD S7		2	.05700	31.42 42.70	2.161	1.07217	1.700	1.299	nen	74 00
ADD HYD AP#		3	.09480	71.06	3.724	1.22492	1.850		PER IMP=	71.00
ROUTE AP#3		10	.09480	69.80	5.885	1.16400	1.800	1.171		
ROUTE RPHS	JK 10	2	.07400	07.00	5.885	1.16400	1.850	1.150		

# AMOLE DEL NORTE STORM DRAINAGE FACILITIES TOWER/SAGE DRAINAGE MASTER PLAN

#### AHYMO SUMMARY TABLE - 100 YEAR - 6 HOUR STORM

AHYMO SUMMARY TABLE (AHYMO194) - AMAFCA Hydrologic Model - January, 1994 INPUT FILE = MASTER6.IN

RUN DATE (MON/DAY/YR) =12/10/1994 USER NO.= ANASRONM.IO1

	HYDROGRAPH	FROM ID	TO ID	AREA	PEAK Discharge	RUNOFF VOLUME	RUNOFF	TIME TO PEAK	CFS PER	PAGE =	1
COMMAND	IDENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATI	ON
START										TIME=	.00
RAINFALL TYP										RAIN6=	2.210
SEDIMENT BULK			_	0/500	444.04		4 7/070	4		PK BF =	1.05
COMPUTE NM HY			3	.04580	111.86	4.273	1.74932	1.533		PER IMP=	76.00
ROUTE	AP-1R	3	2	.04580 .03950	109.16 95.91	4.273 3.514	1.74933	1.533	3.724		70.00
COMPUTE NM HY	'D A2-D AP#2	2& 3	10	.08530	203.51	7.787	1.66790 1.71161	1.500 1.533	3.728	PER IMP=	70.00
ROUTE	AP#2R	10	2	.08530	194.79	7.787	1.71162	1.567	3.568		
COMPUTE NM HY		-	3	.04190	102.87	3.576	1.60006	1.500		PER IMP=	<b>65</b> 00
ADD HYD	AP#3	2& 3	10	.12720	291.85	11.362	1.67486	1.533	3.585	CK IMF-	03.00
ROUTE	AP#3R	10	2	.12720	286.92	11.362	1.67487	1.533	3.524		
COMPUTE NM HY		-	3	.04390	109.89	4.223	1.80360	1.533		PER IMP=	80.00
ADD HYD	AP#4	2& 3	10	.17110	396.80	15.585	1.70789	1.533	3.624		
ROUTE	AP#4R	10	2	.17110	392.87	15.585	1.70790	1.567	3.588		
COMPUTE NM HY	rD A5-D	-	3	.04520	102.56	3.694	1.53221	1.500	3.545	PER IMP=	60.00
ADD HYD	AP#5	2& 3	10	.21630	490.46	19.279	1.67118	1.533	3.543		
ROUTE	AP#5R	10	2	.21630	488.61	19.279	1.67118	1.567	3.530		
COMPUTE NM H		-	3	.04520	95.37	3.367	1.39652	1.500		PER IMP=	50.00
ADD HYD	PART_AP#9	2& 3	10	.26150	573.77	22.645	1.62370	1.567	3.428		
COMPUTE NM H			3	.02060	43.47	1.534	1.39651	1.500		PER IMP=	50.00
ADD HYD	PART_AP#9	10& 3	10	.28210	616.11	24.180	1.60711	1.533	3.413		
COMPUTE NM H		٠_	3	.05700	119.28	5.070	1.66790	1.567		PER IMP=	70.00
ROUTE	AP&6R	3	2	.05700	115.76	5.070	1.66791	1.600	3.173		
COMPUTE NM H		-	3	.01020	22.61	.760	1.39652	1.500		PER IMP=	50.00
ADD HYD	AP#7		20	.06720 .06720	131.61 131.12	5.830 5.830	1.62670	1.600	3.060		
ROUTE COMPUTE NM H	AP#7R YD A10-D	20 -	2	.01020	22.61	.760	1.62671 1.39652	1.600 1.500	3.049	PER IMP=	E0 00
ADD HYD	10 A10-D AP#8		20	.07740	146.97	6.590	1.59636	1.600	2.967	PER IMP=	50.00
ROUTE	AP#8R	20	20	.07740	143.44	6.590	1.59637	1.633	2.896		
ADD HYD		10& 2	10	.35950	747.50	30.769	1.60480	1.567	3.249		
ROUTE	AP#9R		2	.35950	747.19	30.769	1.60480	1.567	3.248		
COMPUTE NM H		-	3	.00860	22.64	.802	1.74932	1.500		PER IMP=	76.00
ADD HYD	AP#10	2& 3	20	.36810	765.60	31.572	1.60817	1.567	3.250		
COMPUTE NM H		-	3	.02300	57.58	2.013	1.64077	1.500		PER IMP=	68.00
ROUTE	AP#11R	3	2	.02300	53.26	2.013	1.64077	1.533	3.618		
COMPUTE NM H	YD B2-D	•	3	.03500	83.14	2.860	1.53221	1.500	3.712	PER IMP=	60.00
ADD HYD	AP#12	2& 3	10	.05800	132.29	4.873	1.57525	1.533	3.564		
ROUTE	AP#12R	10	2	.05800	124.14	4.873	1.57526	1.567	3.344		
COMPUTE NM H	YD B3-D	•	3	.04360	89.24	3.247	1.39652	1.533	3.198	PER IMP=	50.00
ADD HYD	AP#13		10	.10160	210.88	8.120	1.49854	1.533	3.243		
ROUTE	AP#13R	10	2	.10160	209.23	8.120	1.49855	1.567	3.218		
COMPUTE NM H			3	.02300	50.97	1.713	1.39652	1.500		PER IMP=	50.00
ADD HYD	AP#14		10	.12460	251.67	9.833	1.47971	1.567	3.156		
ROUTE	AP#14R		12	.12460	251.49	9.833	1.47971	1.567	3.154		
COMPUTE NM H			3	.03140	77.10	2.680	1.60006	1.500		PER IMP=	65.00
ROUTE	AP-15R		2	.03140	75.27	2.680	1.60006	1.533	3.745		F0
COMPUTE NM H			3	.01630	36.13	1.214	1.39652	1.500		PER IMP=	50.00
ADD HYD	AP#16		10	.04770	109.77	3.894	1.53049	1.533	3.596		
ROUTE	AP#16R	10	2	.04770	109.08	3.894	1.53050	1.533	3.573		

	FROM	I TO		PEAK	RUNOFF		TIME TO	CFS	PAGE =	3	
н	YDROGRAPH ID	ID	AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER			
COMMAND IDENT	IFICATION NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	ITATON	ON	
COMPUTE NM HYD	S8-D -	3	.06830	51.63	4.057	1.11383	1.800	1.181 PE	R IMP=	63.00	)
ADD HYD	AP#37 2& 3	3 10	.16310	120.57	9.942	1.14298	1.800	1.155			
ROUTE	AP#37R 10	2	.16310	120.27	9.942	1.14299	1.850	1.152	1		
COMPUTE NM HYD	S9-D -	3	.07480	92.37	3.723	.93330	1.500	1.929 PE	R IMP=	50.00	)
ADD HYD	AP#38 2& 3	3 20	.23790	148.94	13.666	1.07705	1.800	.978			
COMPUTE NM HYD (	:1-D&AP#39 -	3	.03860	57.22	2.407	1.16937	1.500	2.316 PE	R IMP=	67.00	)
ROUTE	AP#39R 3	2	.03860	55.48	2.407	1.16939	1.500	2.246			
COMPUTE NM HYD	C2-D -	3	.01880	27.33	1.145	1.14160	1.500	2.272 PE	R IMP=	65.00	נ
ADD HYD	AP#40 2& 3	3 10	.05740	82.81	3.552	1.16027	1.500	2.254			
ROUTE	AP#40R 10	2	.05740	81.05	3.552	1.16028	1.550	2.206			
COMPUTE NM HYD	C3-D -	3	.02340	42.41	1.858	1.48877	1.500	2.832 PE	R IMP=	90.00	3
ADD HYD	AP#41 2& 3	3 10	.08080	120.53	5.410	1.25540	1.500	2.331			
COMPUTE NM HYD	:4-D&AP#42 -	3	.03080	47.24	2.081	1.26658	1.500	2.396 PE	R IMP=	74.00	3
ROUTE	AP#42R 3	2	.03080	46.52	2.081	1.26660	1.500	2.360			
ADD HYD	AP#43 10& 2	2 10	.11160	167.05	7.490	1.25848	1.500	2.339			
ROUTE	AP#43R 10	2	.11160	164.06	7.491	1.25849	1.550	2.297			
COMPUTE NM HYD	C5-D -	3	.00910	13.07	.508	1.04738	1.500	2.244 PI	R IMP=	50.00	٥
ADD HYD	AP#44 2& 3	3 10	.12070	176.14	7.999	1.24257	1.550	2.280			
COMPUTE NM HYD	C6-D&AP#45 -	3	.01940	35.16	1.540	1.48877	1.500	2.832 PI	ER IMP=	90.00	0
FINISH											

шv	FROM DROGRAPH ID	TO ID	AREA	PEAK Discharge	RUNOFF VOLUME	RUNOFF	TIME TO PEAK	CFS PER	PAGE =	3
COMMAND IDENTI	FICATION NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATI	ON
COMPUTE NM HYD	s8-D -	3	.06830	87.17	5.730	1.57292	1.767	1.994 P	ER IMP=	63.00
ADD HYD	AP#37 2& 3	10	.16310	201.19	13.930	1.60141	1.800	1.927		
ROUTE	AP#37R 10	2	.16310	201.09	13.930	1.60141	1.833	1.926		
COMPUTE NM HYD	S9-D -	3	.07480	165.79	5.571	1.39652	1.500		ER IMP=	50.00
ADD HYD	AP#38 2& 3	20	.23790	251.17	19.501	1.53698	1.767	1.650		20100
	-D&AP#39 -	3	.03860	96.00	3.350	1.62720	1.500		ER IMP=	67.00
ROUTE	AP#39R 3	2	.03860	93.15	3.350	1.62720	1.533	3.771		
COMPUTE NM HYD	C2-D -	3	.01880	46.17	1.604	1.60006	1.500		ER IMP=	6500
ADD HYD	AP#40 2& 3	_	.05740	137.58	4.954	1.61830	1.500	3.745		03.00
ROUTE	AP#40R 10	2	.05740	136.26	4.954	1.61831	1.533	3.709		
COMPUTE NM HYD	C3-D -	3	.02340	66.79	2.420	1,93929	1.500		ER IMP=	90.00
ADD HYD	AP#41 2& 3		.08080	199.05	7.374	1.71126	1.533	3.849		,0.00
	-D&AP#42 -	3	.03080	76.75	2.829	1.72218	1.500		ER IMP=	74.00
ROUTE	AP#42R 3	2	.03080	76.59	2.829	1.72219	1.533	3.885		14.00
ADD HYD	AP#43 10& 2	10	.11160	275.63	10,203	1.71427	1.533	3.859		
ROUTE	AP#43R 10	2	.11160	261.93	10,203	1.71427	1.533	3.667		
COMPUTE NM HYD	C5-D -	3	.00910	21.80	.762	1.57073	1.500		ER IMP=	50.00
ADD HYD	AP#44 2& 3	_	.12070	283.42	10.966	1.70345	1.533	3.669	LK IPF-	20.00
	-D&AP#45 -	3	.01940	55.38	2.007	1.93929	1.500		ER IMP=	90.00
FINISH	DUNI HTJ	,	.01740	33.30	2.007	1.73727	1.500	7.400 F	LK IMF-	70.00

# AMOLE DEL NORTE STORM DRAINAGE FACILITIES TOWER/SAGE DRAINAGE MASTER PLAN

#### AHYMO SUMMARY TABLE - 100 YEAR - 24 HOUR STORM

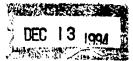
AHYMO SUMMARY TABLE (AHYMO194) - AMAFCA Hydrologic Model - January, 1994
INPUT FILE = MASTER24.IN

RUN DATE (MON/DAY/YR) =12/10/1994 USER NO.= ANASRONM.IO1

	HYDROGRAPH	FROM ID	TO ID	AREA	PEAK Discharge	RUNOFF VOLUME	RUNOFF	TIME TO PEAK	CFS PER	PAGE =	1
COMMAND	IDENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATI	ON
START										TIME=	.00
RAINFALL TY										RAIN24=	2.670
SEDIMENT BUL			_							PK BF =	1.05
COMPUTE NM H			3	.04580	110.15	5.172	2.11755	1.500		PER IMP=	76.00
ROUTE	AP-1R	3	2	.04580	108.15	5.172	2.11756	1.550	3.690		
COMPUTE NM H		- 7	3	.03950	95.25	4.228	2.00697	1.500			70.00
ADD HYD	AP#2	2& 3	10	.08530	197.61	9.400	2.06634	1.500	3.620		
ROUTE	AP#2R	10	2 3	.08530	195.92 101.17	9.401	2.06635	1.550	3.589		<b>(5.00</b>
COMPUTE NM H		- 20 7	_	-04190	284.05	4.279 13.679	1.91483	1.500		PER IMP=	65.00
ADD HYD	AP#3	2& 3 10	10 2	.12720	288.58		2.01643	1.550	3.489		
ROUTE NM H	AP#3R IYD A4-D	-	3	.12720 .04390	108.30	13.679 5.130	2.01643 2.19127	1.550 1.500	3.545		00 00
ADD HYD	AP#4	2& 3	10	.17110	391.99	18.810	2.19127	1.550	3.580	PER IMP=	80.00
ROUTE	AP#4R	10	2	.17110	395.01	18.810	2.06129	1.550	3.607		
COMPUTE NM H		-	3	.04520	101.94	4.394	1.82268	1.500		PER IMP=	60.00
ADD HYD	AP#5	2& 3	10	.21630	488.75	23.204	2.01143	1.550	3.531		00.00
ROUTE	AP#5R	10	2	.21630	489.83	23.204	2.01143	1.550	3.538		
COMPUTE NM H		-	3	.04520	94.89	3.950	1.63839	1.500		PER IMP=	50.00
ADD HYD	PART_AP#9	2& 3	10	.26150	577.67	27.153	1.94694	1.550	3.452		20.00
COMPUTE NM H		-	3	.02060	43.26	1.800	1.63839	1.500			50.00
ADD HYD	PART_AP#9	10& 3	10	.28210	617.72	28.953	1.92441	1.550	3.421		20.00
COMPUTE NM H		-	3	.05700	118.36	6.101	2.00698	1.550		PER IMP=	70.00
ROUTE	AP&6R	3	2	.05700	116.16	6.101	2.00698	1.600	3.184		
COMPUTE NM H		-	3	.01020	22.28	.891	1.63839	1.500	3.412	PER IMP=	50.00
ADD HYD	AP#7	2& 3	20	.06720	131.46	6.992	1.95102	1.600	3.057	,	
ROUTE	AP#7R	20	2	.06720	132.02	6.992	1.95103	1.600	3.070	j	
COMPUTE NM I	HYD A10-D	-	3	.01020	22.28	.891	1.63839	1.500	3.412	PER IMP=	50.00
ADD HYD	AP#8	2& 3	20	.07740	147.32	7.884	1.90982	1.600	2.974	<b>,</b>	
ROUTE	AP#8R	20	2	.07740	145.00	7.884	1.90983	1.600	2.927	,	
ADD HYD	AP#9	10& 2	10	.35950	747.91	36.837	1.92127	1.550	3.251	J	
ROUTE	AP#9R	10	2	.35950	745.86	36.837	1.92127	1.550	3.242	<u>.</u>	
COMPUTE NM I	HYD A11-D	-	3	.00860	22.24	.971	2.11755	1.500	4.040	PER IMP=	76.00
ADD HYD	AP#10	2& 3	20	<b>.</b> 36810	765.11	37.808	1.92586	1.550	3.248		
COMPUTE NM I			3	.02300	56.61	2.417	1.97012	1.500		PER IMP=	68.00
ROUTE	AP#11R		2	.02300	52.84	2.417	1.97014	1.550	3.589		
COMPUTE NM			3	.03500	81.81	3.402	1.82268	1.500		PER IMP	60.00
ADD HYD	AP#12		10	.05800	130.68	5.819	1.88114	1.500	3.521		
ROUTE	AP#12R		2	.05800	125.22	5.819	1.88115	1.550	3.373		
COMPUTE NM			3	.04360	87.28	3.810	1.63839	1.500		B PER IMP=	50.00
ADD HYD	AP#13			.10160	209.92	9.629	1.77697	1.550	3.228		
ROUTE	AP#13R		2	.10160	209.40	9.629	1.77697	1.550	3.220		
COMPUTE NM			3	.02300	50.21	2.010	1.63839	1.500		PER IMP=	50.00
ADD HYD	AP#14			.12460	253.60	11.639	1.75138	1.550	3.180		
ROUTE	AP#14R		12	.12460	250.94 75.82	11.639	1.75139	1.550	3.147		/F 00
COMPUTE NM	HYD S1-D&AP#15 AP-15R		3 2	-03140	73.86	3.207 3.207	1.91483	1.500		3 PER IMP≕	65.00
ROUTE COMPUTE NM			3	.03140 .01630	75.00 35.59	3.207 1.424	1.91484 1.63839	1.500 1.500	3.679		E0 00
ADD HYD	AP#16			.04770	109.45	4.631	1.82035	1.500	3.585	2 PER IMP=	50.00
ROUTE	AP#16R		2	.04770	106.53	4.631	1.82037	1.550	3.489		
K001E	AFHIOR	. 10	~	.04770	100.23	7.031	1.02037	1.550	3.40	,	

HYDROGRAP	FROM I ID	TO ID	AREA	PEAK Discharge	RUNOFF VOLUME	RUNOFF	TIME TO PEAK	CFS PER	PAGE =	= 2
COMMAND IDENTIFICATIO		NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATI	ION
COMPUTE NM HYD S3-	) -	3	.05670	119.03	4.954	1.63839	1.500	7 280 p	ER IMP=	50.00
ADD HYD AP#1		10	.10440	222.73	9.585	1.72153	1.500	3.333	EK IMF-	30.00
ROUTE AP#17		2	.10440	222.44	9.586	1.72153	1.550	3.329		
COMPUTE NM HYD S4-		3	.04360	90.14	4.238	1.82268	1.550		ER IMP=	60.00
ADD HYD AP#1		10	.14800	312.58	13.824	1.75132	1.550	3.300	CK 1111 -	00.00
ROUTE AP#18		2	.14800	300.36	13.824	1.75133	1.550	3.171		
COMPUTE NM HYD S5-		3	.02380	55.26	2.290	1.80425	1.500		ER IMP=	50 00
ADD HYD AP#1		10	.17180	348.69	16.114	1.75866	1.550	3.171	-11 -111 -	37.00
	12&10	10	.29640	599.64	27.753	1.75560	1.550	3.161		
ADD HYD PART AP#2		10	.66450	1364.74	65.561	1.84991	1.550	3.209		
COMPUTE NM HYD B5-D_TWRPN		3	.03910	54.51	1.599	.76663	1.500		ER IMP=	5.00
	1 10& 3	20	.70360	1415.47	67.160	1.78971	1.550	3.143		3.00
ROUTE RESERVOIR AP#2		12	.70360	25.11	53.623	1.42899	2.950	.056 A	C-FT=	51.017
ROUTE AP#22		2	.70360	25.11	53.548	1.42698	3.000	.056	•	
COMPUTE NM HYD B6-		3	.04590	67.74	4.688	1.91483	1.700		ER IMP=	65.00
ADD HYD AP#2	3 2& 3	10	.74950	89.59	58.235	1.45685	1.700	.187		03.00
ROUTE AP#23	R 10	2	.74950	87.30	58.135	1.45433	1.750	.182		
COMPUTE NM HYD B7-	- 0	3	.05910	96.33	6.152	1.95169	1.650		ER IMP=	67.00
ADD HYD AP#2	4 2& 3	10	.80860	178.07	64.286	1.49069	1.700	.344		2
ROUTE AP#24	R 10	2	.80860	176.26	64.199	1.48865	1.700	.341		
COMPUTE NM HYD B8-	D -	3	.08910	85.79	7.786	1.63839	1.900	1.504 P	ER IMP=	50.00
ADD HYD AP#2	5 2& 3	30	.89770	249.51	71.984	1.50352	1.750	.434		
COMPUTE NM HYD A12-D&AP#2	6 -	3	.03590	89.93	4.054	2.11755	1.500		ER IMP=	76.00
ROUTE AP#26		2	.03590	86.27	4.054	2.11756	1.550	3.755		
COMPUTE NM HYD A13-	D -	3	.04520	84.50	4.616	1.91483	1.600	2.921 F	ER IMP=	65.00
ADD HYD AP#2	7 2& 3	10	.08110	170.34	8.670	2.00456	1.550	3.282		
ROUTE AP#27	R 10	2	.08110	161.75	8.670	2.00457	1.600	3.116		
COMPUTE NM HYD A14-	D -	3	.04520	63.35	4.838	2.00697	1.750	2.190 F	ER IMP=	70.00
ADD HYD AP#2	8 2& 3	10	.12630	207.69	13.508	2.00542	1.600	2.569		
ROUTE AP#28	R 10	2	.12630	205.93	13.509	2.00542	1.600	2.548		
COMPUTE NM HYD A15-		3	.02530	47.15	2.459	1.82268	1.550	2.912 F	ER IMP=	60.00
ADD HYD PART_AP#3	32&3	20	.15160	252.00	15.968	1.97492	1.600	2.597		
COMPUTE NM HYD A17-D&AP#2	9 -	3	.01080	23.59	.944	1.63839	1.500	3.412 F	ER IMP=	50.00
ROUTE AP&29	R 3	2	.01080	17.21	.944	1.63844	1.600	2.489		
COMPUTE NM HYD A18-	D -	3	.01030	24.08	1.001	1.82268	1.500	3.654 F	ER IMP=	60.00
ADD HYD AP#3			.02110	37.99	1.945	1.72833	1.550	2.814		
ROUTE AP&30		2	.02110	27.33	1.945	1.72829	1.650	2.024		
COMPUTE NM HYD A19-	D -	3	.01080	21.49	1.050	1.82268	1.550		ER IMP=	60.00
ADD HYD AP#3			.03190	46.33	2.995	1.76023	1.600	2.269		
ROUTE AP#3*		2	.03190	45.57	2.995	1.76023	1.600	2.232		
COMPUTE NM HYD A20-		3	.00690	16.14	.671	1.82268	1.500	3.655 F	ER IMP=	60.00
ADD HYD AP#3			.03880	56.53	3.665	1.77133	1.600	2.276		
ROUTE AP#32		22	.03880	53.38	3.665	1.77131	1.650	2.150		
ADD HYD AP#3	3 20&22		.19040	304.40	19.633	1.93343	1.600	2.498		
ROUTE AP#33		2	.19040	301.70	19.633	1.93343	1.650	2.476		
COMPUTE NM HYD A16		3	.06380	76.21	5.575	1.63839	1. <i>7</i> 50		PER IMP=	50.00
ADD HYD AP#3			.25420	370.33	25.208	1.85938	1.650	2.276		
COMPUTE NM HYD S6-D&AP#		3	.03780	54.41	3.675	1.82268	1.700		PER IMP=	60.00
ROUTE AP#3!		2	.03780	53.37	3.675	1.82269	1.700	2.206		
COMPUTE NM HYD S7		3	.05700	69.82	6.157	2.02540	1.850	1.914	PER IMP=	71.00
ADD HYD AP#			.09480	118.15	9.832	1.94456	1.800	1.947		
ROUTE AP#3	R 10	2	.09480	115.65	9.832	1.94456	1.850	1.906		

### **APPENDIX B**



### CITY OF ALBUQUERQUE

Albuquerque, New Mexico

### INTER-OFFICE MEMORANDUM



December 9, 1994

TO:

Dan Hogan, Division Manager, Hydrology Division

FROM: \ Colleen K. Frenz, Assistant Div. Manager, Design & Dev. Div.

SUBJECT:

POTENTIAL FUTURE PARK SITE - 98TH & TOWER

SAD 222 Master Drainage Plan

A meeting was held on September 23, 1994 regarding the above captioned project. This letter is to inform you that Parks and General Services is interested in pursuing the idea of joint use for a neighborhood park near the detention pond. The Tower/Unser Sector Development Plan identifies two park sites and the Park System Facility Plan supports the need for neighborhood parks in this area, specifically between 98th Street and Unser Boulevard.

Although the planning is in its infancy the opportunity to collocate facilities has proven to be beneficial for both providers of City services and to the public. Once the project progresses, some of the basic design concerns will need to be addressed and notification and approval from the administration will be required.

Thank you for this opportunity. Please continue to keep me informed of project status. My phone number is 857-8636.

cc: Lee Lunsford, SAD Engineer
Douglas L. Andrews
Sandy Zuschlag/Project File
R. J. Herbert/Carmen Chavez

