

P10/D004A

June 14, 2004



Mr. Jonathan Niski
Tierra West, LLC
8509 Jefferson NE
Albuquerque, NM 87113

REF.: DRAINAGE REPORT FOR THE WAL-MART SITE AT
COORS & RIO BRAVO BOULEVARD

Dear Mr. Niski:

The District has reviewed the grading and drainage plan for the above referenced. The following comments must be addressed prior to construction:

1. The District may consider a license to discharge storm water at a rate not to exceed 5 cfs if the Isleta Drain is improved per specifications by AMAFCA & MRGCD under the new drainage study to be completed by AMAFCA & Bernalillo County. Construction plans are required for review and comment.
2. A water quality improvement structure is proposed on the Wal-Mart site prior to discharging into the Isleta Drain. Provide the manufactures information for maintenance of the structure and information for sizing.
3. Who will be responsible for maintaining the water quality structure?
4. A license to replace the existing Rio Bravo Boulevard road culvert crossing is required. Construction plans are required for review and comment.
5. Your plans show the encroachment of a portion of Loris Drive within the Isleta Drain Right-of-Way. A license will be required to allow the encroachment.

If you have any questions please feel free to contact Mr. Ray Gomez for more information at (505) 247-0234.

Sincerely,

P.O. Box 581

87103-0581

1931 Second St SW

Albuquerque, NM

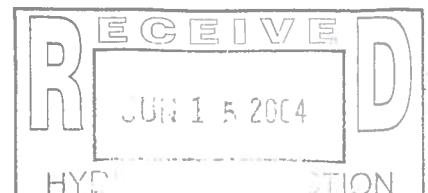
87102-4515

505-247-0234

Fax # 505-243-7308

Subhas K. Shah
Chief Executive Officer

xc: Leonard Utter, Assistant Engineer
Ray Gomez, Engineer I
Lynn Mazur, AMAFCA
File





City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

April 30, 2004

Ron Bohannon, PE
Tierra West LLC
8509 Jefferson NE
Albuquerque, NM 87113

Re: Wal-Mart South Drainage Report
Engineer Stamp date 2-25-04 (P10/D4)

Dear Mr. Bohannon,

Based on information provided in your submittal dated 2-27-04, the above referenced report cannot be approved for Building Permit until the following comments are addressed.

- Please provide written concurrence from MRGCD for the connection to the Isleta Drain. The plan should show the improvements for the channel even though it will be built by Work Order.
- A 0.25" diameter orifice will be incredibly hard to keep from getting clogged. I think these particular inlets should have a detail for removing debris away from the orifice.
- Since the plat is already filed and some of your ponds are accepting public water from the streets, public easements must be provided and an agreement and covenant will be necessary. Since your client is an out-of-town corporation, I would be willing to make this a condition of Certificate of Occupancy but please begin this process as soon as possible.
- Ponds 9, 15 and 19 must have a standpipe outlet with an overflow weir.

If you have any questions, you can contact me at 924-3986.

Sincerely,

Bradley L. Bingham, PE
Principal Engineer, Planning Dept
Development and Building Services

C: file

DRAINAGE AND TRANSPORTATION SHEET

(REV. 1/28/2003rd)

PROJECT TITLE: Wal-Mart South, Store #5430-00 ZONE MAP/DRG. FILE #: P-10
DRB #: _____ EPC #: 03-EPC-01110 WORK ORDER #: _____

LEGAL DESCRIPTION: Tract 1-A-1, Lamonica and Wenk
CITY ADDRESS: Southeast corner of Coors Blvd. and Rio Bravo Blvd.

ENGINEERING FIRM: Tierra West, LLC CONTACT: RONALD R. BOHANNAN OR JON NISKI
ADDRESS: 8509 Jefferson NE PHONE: (505) 858-3100
CITY, STATE: Albuquerque, NM ZIP CODE: 87113

OWNER: _____ CONTACT: _____
ADDRESS: _____ PHONE: _____
CITY, STATE: _____ ZIP CODE: _____

ARCHITECT: Taylor Scott Architects CONTACT: Ryan Wilbanks
ADDRESS: 1437 South Boulder, Suite 800 PHONE: (918) 587-8600
CITY, STATE: Tulsa, OK ZIP CODE: 74119-3609

SURVEYOR: Precision Surveys CONTACT: Larry Medrano
ADDRESS: 8414-D Jefferson Street, NE PHONE: 856-5700
CITY, STATE: Albuquerque, NM ZIP CODE: 87113

CONTRACTOR: _____ CONTACT: _____
ADDRESS: _____ PHONE: _____
CITY, STATE: _____ ZIP CODE: _____

CHECK TYPE OF SUBMITTAL:

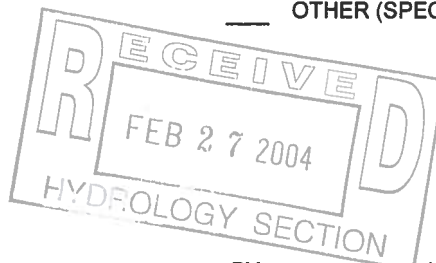
- ☒ DRAINAGE REPORT
☒ DRAINAGE PLAN 1st SUBMITTAL, **REQUIRES TCL or equal**
☐ DRAINAGE PLAN RESUBMITTAL
☐ CONCEPTUAL GRADING & DRAINAGE PLAN
☐ GRADING PLAN
☐ EROSION CONTROL PLAN
☐ ENGINEER'S CERTIFICATION (HYDROLOGY)
☐ CLOMR/LOMR
☐ TRAFFIC CIRCULATION LAYOUT (TCL)
☐ ENGINEERS CERTIFICATION (TCL)
☐ ENGINEERS CERTIFICATION (DRB APPR. SITE PLAN)
☐ OTHER

CHECK TYPE OF APPROVAL SOUGHT:

- ☐ SIA / FINANACIAL GUARANTEE RELEASE
☐ PRELIMINARY PLAT APPROVAL
☐ S. DEV. PLAN FOR SUB'D. APPROVAL
☒ S. DEV. PLAN FOR BLDG. PERMIT APPROVAL
☐ SECTOR PLAN APPROVAL
☐ FINAL PLAT APPROVAL
☐ FOUNDATION PERMIT APPROVAL
☒ BUILDING PERMIT APPROVAL
☐ CERTIFICATE OF OCCUPANCY (PERM.)
☐ CERTIFICATE OF OCCUPANCY (TEMP.)
☒ GRADING PERMIT APPROVAL
☐ PAVING PERMIT APPROVAL
☐ WORK ORDER APPROVAL
☐ OTHER (SPECIFY)

WAS A PRE-DESIGN CONFERENCE ATTENDED:

- ☐ YES
☒ NO
☐ COPY PROVIDED



DATE SUBMITTED: 2/26/2003 BY: Jon Niski

Requests for approvals of Site Development Plans and/or Subdivision Plats shall be accompanied by a drainage submittal. The particular nature, location and scope of the proposed development defines the degree of drainage detail. One or more of the following levels of submittal may be required based on the following:

1. **Conceptual Grading and Drainage Plans:** Required for approval of Site Development Plans greater than five (5) acres and Sector Plans.
2. **Drainage Plans:** Required for building permits, grading permits, paving permits and site plans less than five (5) acres.
3. **Drainage Report:** Required for subdivisions containing more than ten (10) lots or constituting five (5) acres or more.



TIERRA WEST, LLC

8509 Jefferson NE
Albuquerque, NM 87113

(505) 858-3100
fax (505) 858-1118

twllc@tierrawestllc.com
1-800-245-3102

June 17, 2004

File P.10/D4A

Mr. Subhas K. Shah
Chief Executive Officer
Middle Rio Grande Conservancy District
P.O. Box 581
Albuquerque, NM 87103-0581

**RE: DRAINAGE REPORT FOR THE WAL-MART, (ALBUQUERQUE SOUTH),
COORS & RIO BRAVO BOULEVARD, STORE #5430-00**

Dear Mr. Shah:

The following responses are to your comments from your letter dated June 14, 2004.

1. The District may consider a license to discharge storm water at a rate not to exceed 5 cfs if the Isleta Drain is improved per specifications by AMAFCA & MRGCD under the new drainage study to be completed by AMAFCA & Bernalillo County. Construction plans are required for review and comment.

The channel will be designed and constructed based on comments received at the June 17, 2004 meeting with all agencies in attendance. Approval of the plans will be required by AMAFCA and MRGCD prior to the City of Albuquerque issuing a work order for the project.

2. A water quality improvement structure is proposed on the Wal-Mart site prior to discharging into the Isleta Drain. Provide the manufacturers information for maintenance of the structure and information for sizing.

The information you requested is enclosed for your review.

3. Who will be responsible for maintaining the water quality structure?

The Wal-Mart Supercenter will be responsible for the maintenance.

4. A license to replace the existing Rio Bravo Boulevard road culvert crossing is required. Construction plans are required for review and comment.

A license agreement will be submitted once the design of the crossing is agreed upon by AMAFCA and MRGCD.

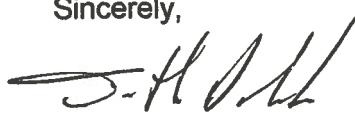
Mr. Subhas K. Shah
June 17, 2004
Page 2

5. Your plans show the encroachment of a portion of Loris Drive within the Isleta Drain Right-of-Way. A license will be required to allow the encroachment.

A license agreement for the roadway encroachment will be submitted within the next week.

If you have any questions or need additional information regarding this matter, please do not hesitate to call me.

Sincerely,



Jonathan D. Niski, E.I.

Enclosure/s

cc: Brad Bingham

JN: 220094
JDR/mjr

2002:220094SubhasShah06162004



TIERRA WEST, LLC

8509 Jefferson NE
Albuquerque, NM 87113

(505) 858-3100
fax (505) 858-1118

twllc@tierrawestllc.com
1-800-245-3102

March 23, 2005

File P10/D4A

Mr. Ray Gomez
MRGCD
1931 Second Street, NW
Albuquerque, NM 87102

**RE: Wal-Mart #5430-00, Coors Boulevard and Rio Bravo Boulevard
Isleta Drain Improvements**

Dear Mr. Gomez:

We are in receipt of the letter from Mr. Shah dated March 16, 2005 informing our office of the request to build a 12'x6' box culvert in light of the recent information that has surfaced regarding the overall South Valley Flood Damage Control project and the discovery of a 16" VHP gas line that is in conflict with a box culvert of that size. We therefore request that the size of the box culvert be revisited by the design engineer for the overall South Valley project. The original design flows that generated the 12'X6' box culvert were 560 cfs. The 12'x6' box culvert had a capacity for 600 cfs. We looked at a couple of alternate sizes based on the new information provided by Resource Technology, Inc. (RTI). The revised design flow is now 429 cfs and we have analyzed a box culvert that is 242 feet in length at a slope of 0.60%. These new criteria allow for either a 10'X4' box culvert or a 6'x6' box culvert to be placed instead of the 12'x6' box culvert originally called for when this project first started. I have enclosed our calculations supporting these alternatives and ask that you have RTI review the information and confirm that these sizes are adequate to handle the design flows for the overall south valley project.

The 10'x4' box culvert allows us to squeeze between the existing 16" VHP gas line and the existing 36" sanitary sewer line. If your agency or AMAFCA require a six foot high box culvert be built we ask that your agency contact PNM and have them relocate the 16" VHP gas line prior to our construction beginning. The cost of this relocation should not be at the expense of Wal-Mart.

We would also like to reiterate that if we build this portion of the channel to the current design being presented by RTI that this stretch of channel will act as a four to five foot deep desilting pond. This portion of the channel will continue to act as a desilting pond until such time the channel down stream is graded to match the design grades for the South Valley project.

Mr. Ray Gomez
March 23, 2005
Page 2

Please review the information we have provided and consult with the South Valley project design engineer to see if one of these alternate box culvert sizes is acceptable. If you have any questions or need additional information regarding this matter, please do not hesitate to contact me

Sincerely,



Jonathan D. Niski, E.I.

Enclosure/s

cc: Lynn Mazur
Brad Bingham
Steve Dyer

JN: 220094
JDN/bgd

2002:22094 Ray Gomez 032205

TIERRA WEST, LLC

8509 Jefferson NE
Albuquerque, NM 87113

(505) 858-3100
fax (505) 858-1118

twllc@tierrawestllc.com
1-800-245-3102

March 2, 2005

File
P10 / D4A

Mr. Subhas K. Shah
Chief Executive Officer
Middle Rio Grande Conservancy District
PO Box 581
Albuquerque, NM 87103-0581
Attention: Ray Gomez

RE: ISLETA DRAIN IMPROVEMENTS

Dear Mr. Shah:

Over the past couple of weeks our office has been working on a redesign of the Rio Bravo Boulevard crossing for the Isleta Drain. This was due to an existing 16-inch, very high pressure, gas line along the north side of Rio Bravo that was previously not marked in the field. The position of the gas line makes it very difficult to construct a 12'x6' box culvert that was agreed to when our project first started. This design, as well as the channel design, was based on preliminary information from Resource Technology, Inc. (RTI) who is working on the South Valley Flood Damage Control project.

Since our initial design RTI has revised some of the design numbers. The design flow has dropped from 560 cfs to 429 cfs. This would allow us to place three 48-inch pipes at the existing 48-inch RCP Rio Bravo crossing to handle the design flows. We understand that MRGCD would like a box culvert placed at the Rio Bravo crossing, however the emergence of the 16-inch very high pressure gas line would prevent a box structure from being constructed in a cost effective and timely manner.

Not only does the 16" very high pressure gas line make it difficult to place a box culvert in the drain, RTI has determined that the channel (at this point) would need to be lowered to an elevation of 4913.30. This elevation is 4.2 feet lower than the existing channel bottom. If we were to construct our portion of the channel at this time the south end would essentially have a 4.2 foot grade break creating a desilting basin. For this portion of the channel to work MRGCD would have to dredge the channel from our southern property line to the outfall of the channel.

We feel this portion of the channel and the crossing should be constructed with the entire South Valley project. The improvements would not work as intended until the rest of the channel construction is complete. Thus, we would like to make a cash contribution in the amount of our portion of the channel improvements (\$661,100.50) toward the overall South Valley project. This would allow the channel to be built in a manner that all of the portions of the channel would operate as intended in the design.

If you have any questions or need additional information regarding this matter, please do not hesitate to call me.

Sincerely,



Ronald R. Bohannon, PE

cc: John Kelly
Brad Bingham
Steve Dyer

JN: 220094
JDN/db



March 16, 2005

Mr. Ronald R. Bohannon, PE
Tierra West, LLC
8509 Jefferson NE
Albuquerque, NM 87113

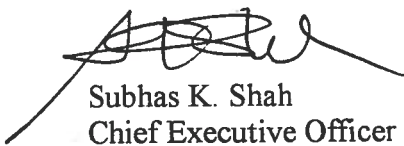
REF.: ISLETA DRAIN IMPROVEMENTS PER THE WAL-MART #5430-00
CONSTRUCTION PLANS

Dear Mr. Bohannon,

This is in response to your letter dated March 2, 2005 regarding the above referenced project. The District prefers that Wal-Mart be responsible for construction of 12' wide x 6' tall concrete box culvert and shotcrete lining. Per latest construction plan we see an existing 16" Ø gas line and 36" Ø sewer line have complicated the installation of the concrete box culvert. Coordination with AMAFCA and Bernalillo County is required to ensure that the concrete box culvert and shotcrete lining is installed correctly and does not interfere with existing utilities. We will review the plans you provided on Monday to us and advise you.

If you have any questions please feel free to contact Mr. Ray Gomez for more information at (505) 247-0234.

Sincerely,



Subhas K. Shah
Chief Executive Officer

xc: Leonard Utter, MRGCD Engineering
Ray Gomez, MRGCD Engineering
John Kelly, AMAFCA
Brad Bingham, City of Albuquerque
Roger Paul, Bernalillo County
File

P.O. Box 581

87103-0581

1931 Second St. SW

Albuquerque, NM

87102-4515

505-247-0234

Fax # 505-243-7308

**DRAINAGE REPORT
FOR**

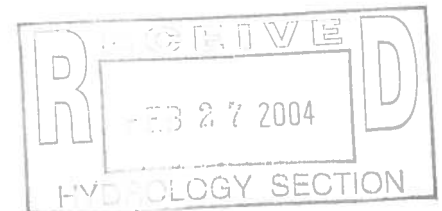
***Tract 1-A-1
Lands of Lamonica and Wenk
Albuquerque, NM***

Prepared by:

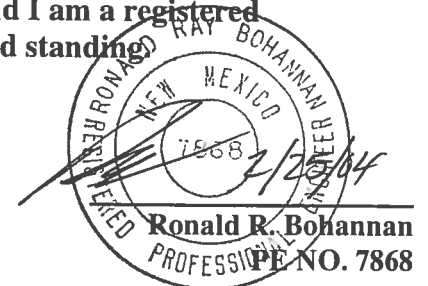
**Tierra West, LLC
8509 Jefferson NE
Albuquerque, New Mexico 87113**

**Prepared for:
Wal-Mart Stores, Inc.
2001 SE 10th Street
Bentonville, AR 72712**

February 2004



I certify that this report was prepared under my supervision, and I am a registered professional engineer in the State of New Mexico in good standing.



Job No 220094

TABLE OF CONTENTS

SECTION I - REPORT

Location	4
Existing Drainage Conditions	4
Flood Plain	4
Vicinity Map	5
Flood Insurance Rate Map	6
Proposed Drainage Management	7
Proposed Basins Map	8
Calculations	9
Summary	9

SECTION II - RUNOFF CALCULATIONS

Runoff Calculations	11
Proposed Pond Exhibit	12
Pond Calculations	13
AHYMO Calculations	32

MAP POCKET

Grading and Drainage Plan

Section I

Report

Prelude

This report is being prepared at the request of the current owner, Wal-Mart Stores, Inc., who proposes to develop a commercial center.

Location

The subject site is located on the southeast corner of Coors Boulevard and Rio Bravo Boulevard and consists of Tract 1-A-1, Lands of Lamonica and Wenk. The exact location of the site is shown highlighted on the enclosed Zone Atlas page number P-10. The site will be built in one phase and contains 27.7381 acres more or less.

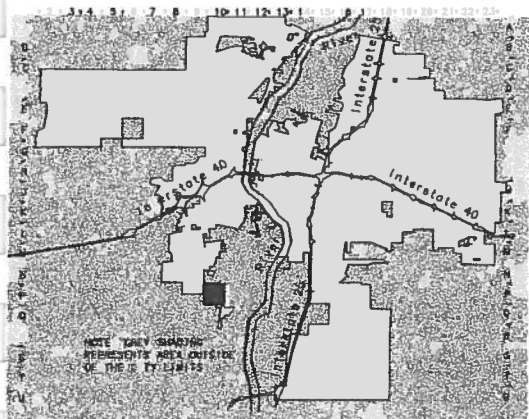
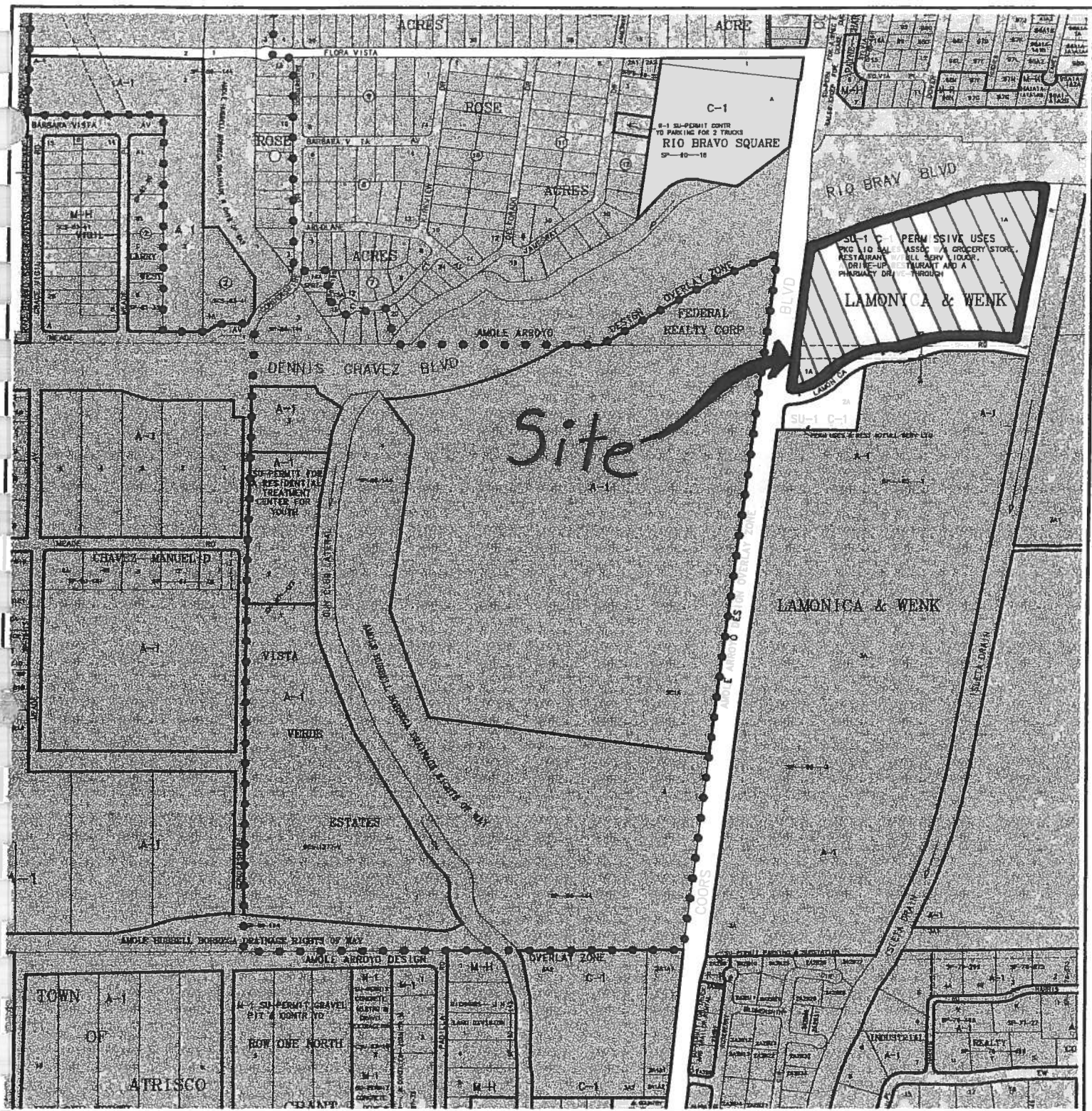
Existing Drainage Conditions

The site is currently undeveloped and is being used as an alfalfa field. It is bordered by Coors Boulevard on the west, Rio Bravo Boulevard on the north, the Isleta Drain on the east and a single residence and farm land on the south.

The site is laser leveled and is currently being irrigated to support the growth of alfalfa. The field is bordered on all sides by berms to facilitate the irrigation of the land. The irrigation is controlled by a culvert and gate under Rio Bravo Boulevard located at the northeast corner of the site. The overflow is controlled via a drain gate and culver located at the midpoint of the sites south property line. During a 100-yr, 6-hour storm event this site generates 33.91 cfs and 0.96 acre feet of potential runoff. Due to the laser leveling and berms surrounding the site, no flows leave the site during this storm event.

Flood Plain

The site is located on FIRM Map 35001C0339 D as shown on the attached excerpt. The map shows that the site lies within flood zone X.



CITY OF
Albuquerque

A G I S
Albuquerque Geographic Information System
PLANNING DEPARTMENT

© Copyright 2001

EXHIBIT A- VICINITY MAP

GRAPHIC SCALE IN FEET

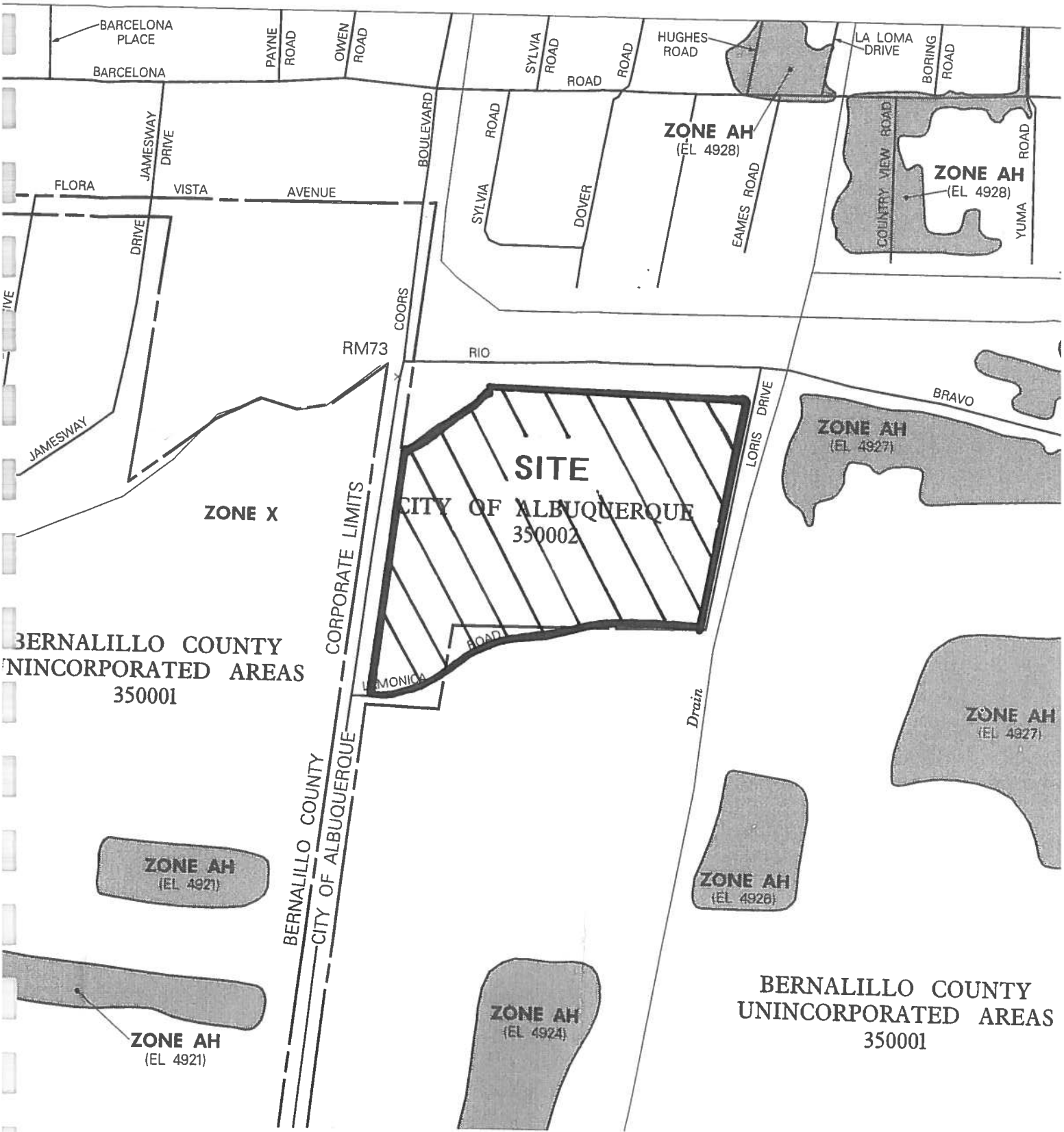


Zone Atlas Page

P-10-Z

Map Amended through July 18, 2001

07"



FIRM MAP 35001C0339 D

Isleta

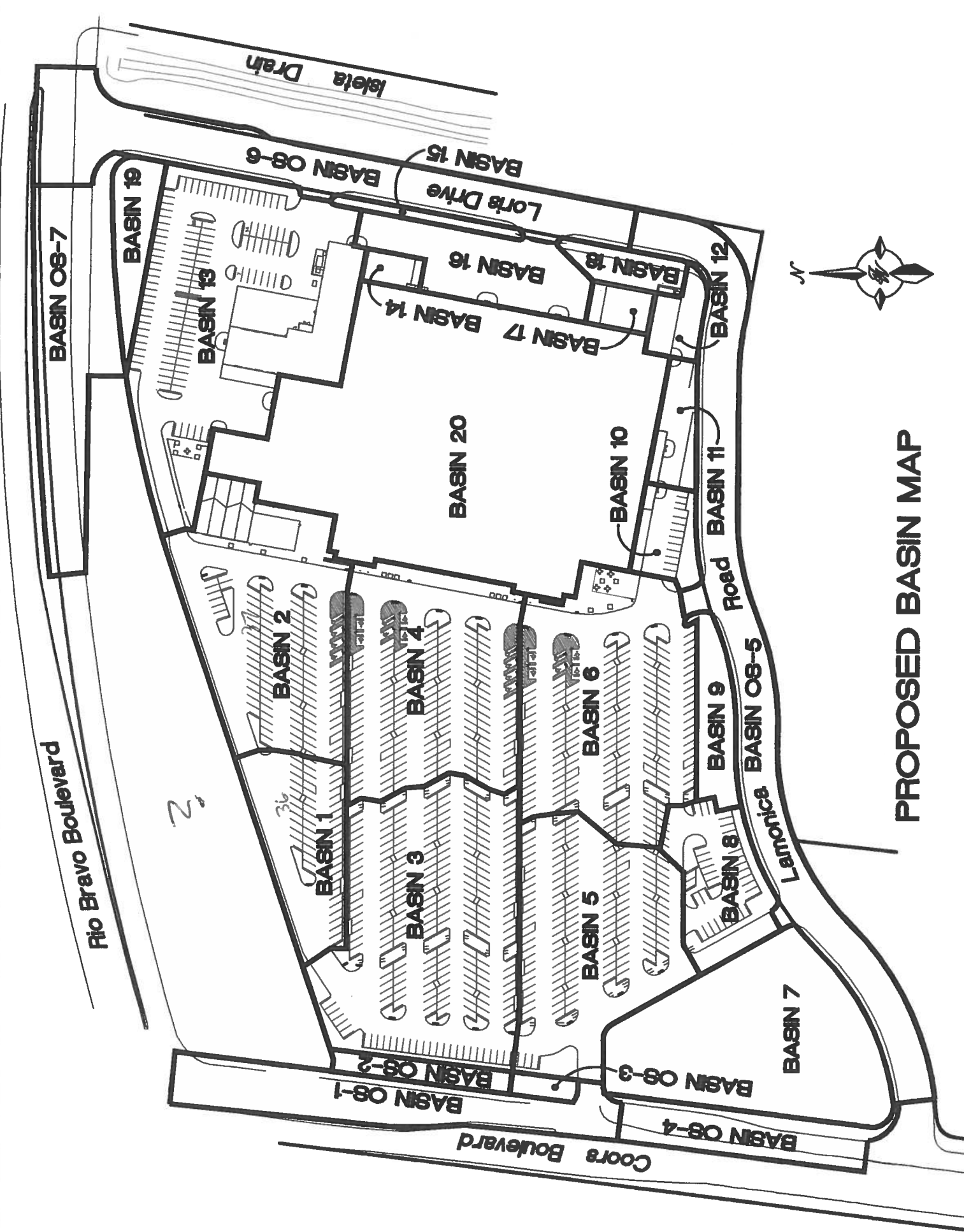
Proposed Drainage Management Plan

As shown on the attached exhibit, the proposed site is divided into 19 basins with the site draining to a number of retention ponds connected to a storm sewer system. The storm sewer system conveys the flows to the southeast corner of the site. At that point the water is discharged into the Isleta Drain via a water quality manhole with a discharge rate of 5.0 cfs.

As shown in Section II, the developed runoff flows for each basin was determined using the Weighted E Method. The site drainage will be controlled by creating 19 individual ponds located on the site. Each pond will drain to either an inlet or discharge pipe with an orifice plate located at each discharge point limiting the amount of flow from the ponds. The Grading and Drainage Plan includes a table of orifice plate sizes for each pond.

The on-site drainage system will accept public water from the adjoining streets and from the outlot located in the southwest corner of the site. The ponds are sized to contain these flows and discharge them at a limited rate.

The storm drain system was modeled using the routing command within AHYMO. The pond volumes and discharge rate calculations as well as the input and output AHYMO files are located in Section II. Based upon the model, the entire site will have a peak discharge of 4.95 cfs, which is below the 5.0 cfs restriction for the site. In the event of inlet clogging or a storm event greater than the predicted 100-year, 6-hour design storm, the site will continue to the pond the water overflowing to the adjacent ponding areas until such time the clog is cleared. At no time will the water pond to a point that it will enter the building.



PROPOSED BASIN MAP

Calculations

The weighted E method from the “City of Albuquerque Development Process Manual Volume 11 – Design Criteria, 1997 Revision” was used to calculate the runoff and volume for the site.

Summary

This site will discharge 4.95 cfs into the Isleta Drain via a water quality manhole as required by AMAFCA. This discharge rate is lower than the 5.0 cfs rate dictated by AMAFCA. The site accepts the offsite flow generated by the surrounding streets and allows the flows to pond onsite and be discharged at a limited rate.

The development of this site is consistent with the DPM, Chapter 22, Hydrology section. Since this site encompasses more than 1 acre, a NPDES permit will be required in addition to a Top Soil Disturbance Permit, prior to any construction activity.

Section II

Runoff Calculations

Weighted E Method

Developed Basins

Basin	Area (sf)	Area (acres)	Area (sq. mi.)	Treatment A			Treatment B			Treatment C			Treatment D			100-Year			10-Year		
				%	(acres)	%	(acres)	%	(acres)	%	(acres)	%	(acres)	%	(acres)	Weighted E (ac-ft)	Volume (ac-ft)	Flow cfs	Weighted E (ac-ft)	Volume (ac-ft)	Flow cfs
1	31,647	0.73	0.00114	0%	0	0	0.07	0%	0.00	0%	0.00	0%	0.65	0%	0.00	1.840	0.111	3.00	1.138	0.069	1.94
2	76,028	1.75	0.00273	0%	0	0	0.10	0%	0.00	0%	0.00	0%	0.94	0%	0.00	1.892	0.275	7.38	1.179	0.171	4.82
3	99,269	2.28	0.00356	0%	0	0	0.23	0%	0.00	0%	0.00	0%	2.05	0%	0.00	1.840	0.349	9.43	1.138	0.216	6.10
4	74,550	1.71	0.00267	0%	0	0	0.03	0%	0.00	0%	0.00	0%	1.68	0%	0.00	1.944	0.277	7.40	1.220	0.174	4.87
5	69,841	1.60	0.00251	0%	0	0	0.11	0%	0.00	0%	0.00	0%	1.49	0%	0.00	1.879	0.251	6.74	1.169	0.156	4.39
6	84,285	1.93	0.00302	0%	0	0	0.08	0%	0.00	0%	0.00	0%	1.86	0%	0.00	1.918	0.309	8.27	1.199	0.193	5.43
7	75,503	1.73	0.00271	0%	0	0	0.35	0%	0.00	0%	0.00	0%	1.39	0%	0.00	1.710	0.247	6.76	1.036	0.150	4.27
8	26,205	0.60	0.00094	0%	0	0	0.15	0%	0.00	0%	0.00	0%	0.45	0%	0.00	1.645	0.082	2.28	0.985	0.049	1.42
9	13,564	0.31	0.00049	0%	0	0	0.31	0%	0.00	0%	0.00	0%	0.00	0%	0.00	0.670	0.017	0.63	0.220	0.006	0.24
10	11,176	0.26	0.00040	0%	0	0	0.06	0%	0.00	0%	0.00	0%	0.20	0%	0.00	1.684	0.036	0.99	1.016	0.022	0.62
11	9,972	0.23	0.00036	0%	0	0	0.05	0%	0.00	0%	0.00	0%	0.18	0%	0.00	1.684	0.032	0.88	1.016	0.019	0.55
12	7,479	0.17	0.00027	0%	0	0	0.01	0%	0.00	0%	0.00	0%	0.16	0%	0.00	1.905	0.027	0.73	1.189	0.017	0.48
13	108,285	2.49	0.00388	0%	0	0	0.20	0%	0.00	0%	0.00	0%	2.29	0%	0.00	1.866	0.387	10.40	1.158	0.240	6.76
14	3,785	0.09	0.00014	0%	0	0	0.00	0%	0.00	0%	0.00	0%	0.00	0%	0.00	1.970	0.014	0.38	1.240	0.009	0.25
15	4,087	0.09	0.00015	0%	0	0	0.09	0%	0.00	0%	0.00	0%	0.00	0%	0.00	0.670	0.005	0.19	0.220	0.002	0.07
16	27,524	0.63	0.00099	0%	0	0	0.00	0%	0.00	0%	0.00	0%	0.63	0%	0.00	1.970	0.104	2.76	1.240	0.065	1.83
17	5,409	0.12	0.00019	0%	0	0	0.00	0%	0.00	0%	0.00	0%	0.12	0%	0.00	1.970	0.020	0.54	1.240	0.013	0.36
18	8,467	0.19	0.00030	0%	0	0	0.06	0%	0.00	0%	0.00	0%	0.13	0%	0.00	1.554	0.025	0.70	0.914	0.015	0.43
19	13,030	0.30	0.00047	0%	0	0	0.30	0%	0.00	0%	0.00	0%	0.00	0%	0.00	0.670	0.017	0.61	0.220	0.005	0.23
20	189,985	4.36	0.00681	0%	0	0	0.00	0%	0.00	0%	0.00	0%	4.36	0%	0.00	1.970	0.716	19.06	1.240	0.451	12.80
OS-1	37,304	0.86	0.00134	0%	0	0	0.00	0%	0.00	0%	0.00	0%	0.86	0%	0.00	1.970	0.141	3.74	1.240	0.088	2.47
OS-2	7,896	0.18	0.00028	0%	0	0	0.16	0%	0.00	0%	0.00	0%	0.02	0%	0.00	0.800	0.012	0.41	0.322	0.005	0.18
OS-3	2,990	0.07	0.00011	0%	0	0	0.06	0%	0.00	0%	0.00	0%	0.01	0%	0.00	0.800	0.005	0.16	0.322	0.002	0.07
OS-4	23,374	0.54	0.00084	0%	0	0	0.09	0%	0.00	0%	0.00	0%	0.45	0%	0.00	1.762	0.079	2.14	1.077	0.048	1.37
OS-5	84,933	1.95	0.00305	0%	0	0	0.00	0%	0.00	0%	0.00	0%	1.95	0%	0.00	1.970	0.320	8.52	1.240	0.201	5.63
OS-6	63,832	1.47	0.00229	0%	0	0	0.00	0%	0.00	0%	0.00	0%	1.47	0%	0.00	1.970	0.241	6.40	1.240	0.151	4.23
OS-7	49,830	1.14	0.00179	0%	0	0	0.25	0%	0.00	0%	0.00	0%	0.89	0%	0.00	1.684	0.161	4.41	1.016	0.097	2.77
Totals	1,210,260	27.78			0	0	2.22	0%	0.00	0%	0.00	0%	0.89	0%	0.00	4.261	114.93		2.636	74.40	

Equations:

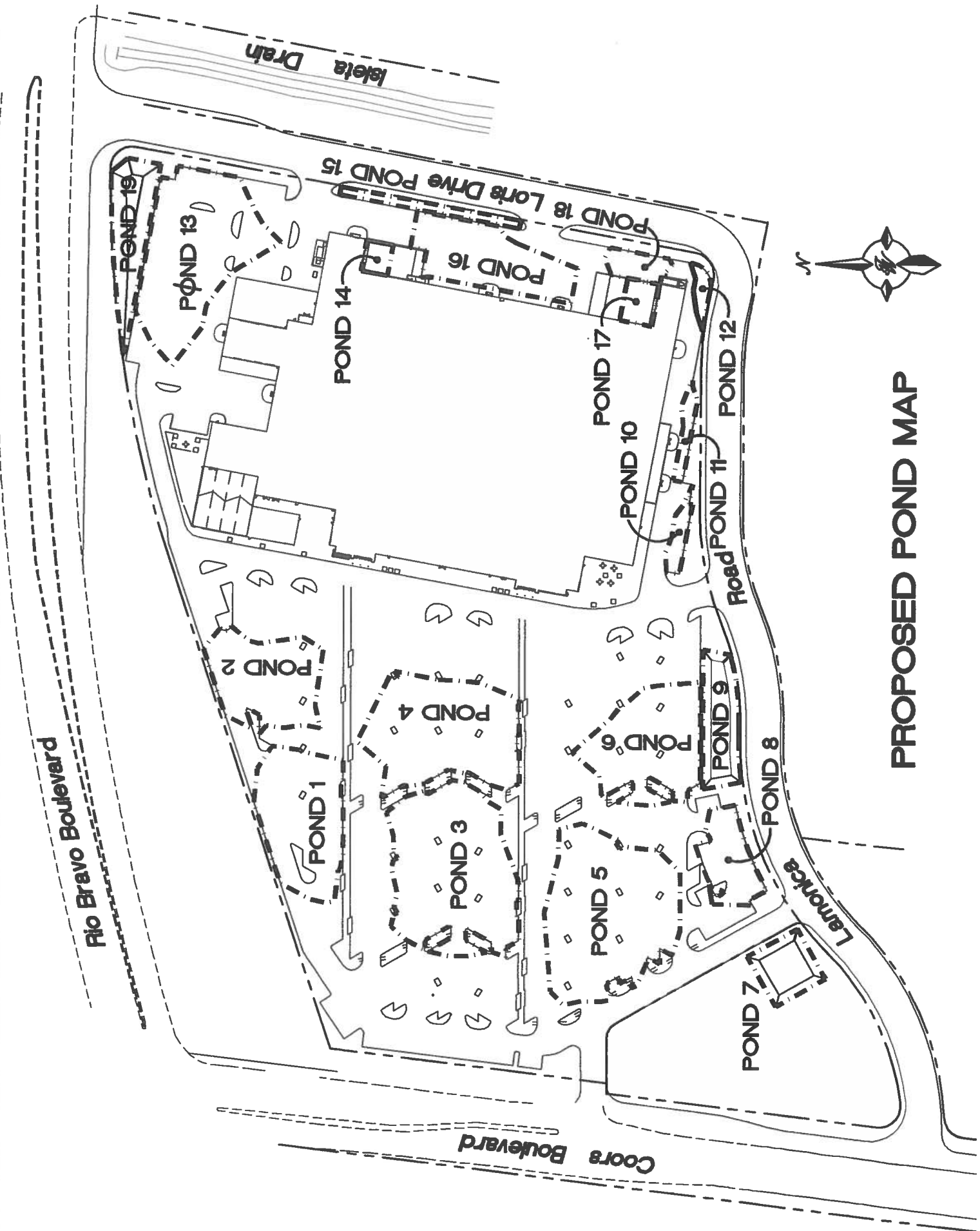
Weighted E = $E_a \cdot A_a + E_b \cdot A_b + E_c \cdot A_c + E_d \cdot A_d$ / (Total Area)

Volume = Weighted D * Total Area

Flow = $Q_a \cdot A_a + Q_b \cdot A_b + Q_c \cdot A_c + Q_d \cdot A_d$

Excess Precipitation, E (inches)			Peak Discharge (cfs/acre)		
Zone 1	100-Year	10 - Year	Zone 1	100-Year	10 - Year
E _a	0.44	0.08	Q _a	1.29	0.24
E _b	0.67	0.22	Q _b	2.03	0.76
E _c	0.99	0.44	Q _c	2.87	1.49
E _d	1.97	1.24	Q _d	4.37	2.89

PROPOSED POND MAP



VOLUME CALCULATIONS

POND 1

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

$$\text{Ab} = 6.80$$

$$\text{At} = 21,297.00$$

$$\text{Dt} = 1.00$$

$$\text{C} = 21290.20$$

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4925.79	0	0	0.0000
4927.96	2.17	0.0003	0.0024
4928.21	2.420	0.0157	0.0025
4928.46	2.670	0.0615	0.0027
4928.71	2.920	0.1379	0.0028
4928.96	3.170	0.2449	0.0029

Orifice Equation

$$Q = \text{CA} \sqrt{2gH}$$

$$\text{C} = 0.6$$

$$\text{Diameter (in)} = \textcircled{0.25}$$

$$\text{Area (ft}^2\text{)} = 0.000 \leftarrow$$

$$g = 32.2$$

$$\text{H (Ft)} = \text{Depth of water above center of orifice}$$

$$\text{Q (CFS)} = \text{Flow}$$

VOLUME CALCULATIONS POND 2

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

$$\text{Ab} = 6.80$$

$$\text{At} = 17,427.00$$

$$\text{Dt} = 1.00$$

$$\text{C} = 17420.20$$

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4925.24	0	0	0.0000
4927.41	2.17	0.0003	0.5241
4927.66	2.420	0.0129	0.5556
4927.91	2.670	0.0504	0.5855
4928.16	2.920	0.1129	0.6140
4928.41	3.170	0.2005	0.6411

Orifice Equation

$$Q = \text{CA} \sqrt{2gH}$$

$$\text{C} = 0.6$$

$$\text{Diameter (in)} = 3.75$$

$$\text{Area (ft}^2\text{)} = 0.077$$

$$g = 32.2$$

$$\text{H (Ft)} = \text{Depth of water above center of orifice}$$

$$\text{Q (CFS)} = \text{Flow}$$

VOLUME CALCULATIONS

POND 3

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

$$\text{Ab} = 6.80$$

$$\text{At} = 34,632.00$$

$$\text{Dt} = 1.00$$

$$\text{C} = 34625.20$$

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4925.04	0	0	0.0000
4927.21	2.17	0.0003	0.0024
4927.46	2.42	0.0252	0.0025
4927.71	2.67	0.0998	0.0027
4927.96	2.92	0.2240	0.0028
4928.21	3.17	0.3979	0.0029

Orifice Equation

$$Q = \text{CA} \text{ SQRT}(2gH)$$

$$\text{C} = 0.6$$

$$\text{Diameter (in)} = 0.25$$

$$\text{Area (ft}^2\text{)} = 0.000$$

$$g = 32.2$$

$$\text{H (Ft)} = \text{Depth of water above center of orifice}$$

$$\text{Q (CFS)} = \text{Flow}$$

VOLUME CALCULATIONS

POND 4

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

$$\text{Ab} = 6.80$$

$$\text{At} = 28,040.00$$

$$\text{Dt} = 1.00$$

$$\text{C} = 28033.20$$

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4923.83	0	0	0.0000
4927.65	3.82	0.0006	0.0032
4927.90	4.070	0.0207	0.0033
4928.15	4.320	0.0811	0.0034
4928.40	4.570	0.1817	0.0035
4928.65	4.820	0.3225	0.0036

Orifice Equation

$$Q = \text{CA} \sqrt{2gH}$$

$$\text{C} = 0.6$$

$$\text{Diameter (in)} = 0.25$$

$$\text{Area (ft}^2\text{)} = 0.000$$

$$g = 32.2$$

$$\text{H (Ft)} = \text{Depth of water above center of orifice}$$

$$\text{Q (CFS)} = \text{Flow}$$

VOLUME CALCULATIONS

POND 5

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

$$\text{Ab} = 6.80$$

$$\text{At} = 35,736.00$$

$$\text{Dt} = 1.00$$

$$\text{C} = 35729.20$$

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4924.20	0	0	0.0000
4926.37	2.17	0.0003	0.0216
4926.62	2.420	0.0260	0.0228
4926.87	2.670	0.1029	0.0240
4927.12	2.920	0.2311	0.0251
4927.37	3.170	0.4106	0.0262

Orifice Equation

$$Q = \text{CA} \sqrt{2gH}$$

$$\text{C} = 0.6$$

$$\text{Diameter (in)} = 0.75$$

$$\text{Area (ft}^2\text{)} = 0.003$$

$$g = 32.2$$

$$\text{H (Ft)} = \text{Depth of water above center of orifice}$$

$$\text{Q (CFS)} = \text{Flow}$$

VOLUME CALCULATIONS

POND 6

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = Ab * D + 0.5 * C * D^2$$

$$C = (At - Ab) / Dt$$

$$Ab = 6.80$$

$$At = 20,894.00$$

$$Dt = 1.00$$

$$C = 20887.20$$

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4922.22	0	0	0.0000
4925.67	3.45	0.0005	0.5050
4925.92	3.700	0.0156	0.5237
4926.17	3.950	0.0606	0.5418
4926.42	4.200	0.1355	0.5592
4926.67	4.450	0.2404	0.5762

Orifice Equation

$$Q = CA \text{ SQRT}(2gH)$$

$$C = 0.6$$

$$\text{Diameter (in)} = 3.25$$

$$\text{Area (ft}^2\text{)} = 0.058$$

$$g = 32.2$$

$$H \text{ (Ft)} = \text{Depth of water above center of orifice}$$

$$Q \text{ (CFS)} = \text{Flow}$$

VOLUME CALCULATIONS

POND 7

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = Ab * D + 0.5 * C * D^2$$

$$C = (At - Ab) / Dt$$

$$Ab = 3,136.00$$

$$At = 6,400.00$$

$$Dt = 3.00$$

$$C = 1088.00$$

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4923.00	0	0	0.0000
4923.60	0.60	0.0432	0.1156
4924.20	1.20	0.0909	0.1718
4924.80	1.80	0.1476	0.2137
4925.40	2.40	0.2132	0.2487
4926.00	3.00	0.2879	0.2793

Orifice Equation

$$Q = CA \text{ SQRT}(2gH)$$

$$C = 0.6$$

$$\text{Diameter (in)} = 2.5$$

$$\text{Area (ft}^2\text{)} = 0.034$$

$$g = 32.2$$

$$H \text{ (Ft)} = \text{Depth of water above center of orifice}$$

$$Q \text{ (CFS)} = \text{Flow}$$

VOLUME CALCULATIONS POND 8

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = Ab * D + 0.5 * C * D^2$$

$$C = (At - Ab) / Dt$$

Ab = 6.80
 At = 8,098.00
 Dt = 1.00
 C = 8091.20

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4922.28	0	0	0.0000
4925.67	3.39	0.0005	0.0030
4925.92	3.64	0.0064	0.0031
4926.17	3.89	0.0238	0.0032
4926.42	4.14	0.0529	0.0033
4926.67	4.39	0.0936	0.0034

Orifice Equation

$$Q = CA \text{ SQRT}(2gH)$$

C = 0.6
 Diameter (in) 0.25
 Area (ft²)= 0.000
 g = 32.2
 H (Ft) = Depth of water above center of orifice
 Q (CFS)= Flow

VOLUME CALCULATIONS

POND 9

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

Ab = 4,001.00
 At = 9,031.00
 Dt = 3.41
 C = 1475.07

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4921.52	0	0	0.0000
4921.93	0.41	0.0377	0.0041
4922.68	1.16	0.1161	0.0070
4923.43	1.91	0.2135	0.0090
4924.18	2.66	0.3300	0.0107
4924.93	3.41	0.4656	0.0121

Orifice Equation

$$Q = \text{CA} \sqrt{2gH}$$

C = 0.6
 Diameter (in) = 0.5
 Area (ft²) = 0.001
 g = 32.2
 H (Ft) = Depth of water above center of orifice
 Q (CFS) = Flow

VOLUME CALCULATIONS

POND 10

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

Ab = 6.80
 At = 2,082.00
 Dt = 0.67
 C = 3097.31

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4925.14	0	0	0.0000
4929.14	4.00	0.0006	0.2628
4929.31	4.17	0.0016	0.2683
4929.48	4.34	0.0047	0.2738
4929.64	4.50	0.0097	0.2792
4929.81	4.67	0.0167	0.2844

Orifice Equation

$$Q = \text{CA} \sqrt{2gH}$$

C = 0.6
 Diameter (in) = 2.25
 Area (ft²) = 0.028
 g = 32.2
 H (Ft) = Depth of water above center of orifice
 Q (CFS) = Flow

VOLUME CALCULATIONS

POND 11

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

Ab = 6.80
 At = 1,924.00
 Dt = 0.62
 C = 3092.26

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4925.62	0	0	0.0000
4929.62	4.00	0.0006	0.2079
4929.78	4.16	0.0015	0.2120
4929.93	4.31	0.0041	0.2160
4930.09	4.47	0.0084	0.2199
4930.24	4.62	0.0144	0.2237

Orifice Equation

$$Q = \text{CA} \sqrt{2gH}$$

C = 0.6
 Diameter (in) 2
 Area (ft²)= 0.022
 g = 32.2
 H (Ft) = Depth of water above center of orifice
 Q (CFS)= Flow

VOLUME CALCULATIONS

POND 12

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = Ab * D + 0.5 * C * D^2$$

$$C = (At - Ab) / Dt$$

Ab = 6.80
 At = 1,444.00
 Dt = 0.67
 C = 2145.07

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4926.00	0	0	0.0000
4930.00	4.00	0.0006	0.2079
4930.17	4.17	0.0013	0.2123
4930.34	4.34	0.0034	0.2166
4930.50	4.50	0.0069	0.2208
4930.67	4.67	0.0118	0.2250

Orifice Equation

$$Q = CA \text{ SQRT}(2gH)$$

C = 0.6
 Diameter (in) 2
 Area (ft²)= 0.022
 g = 32.2
 H (Ft) = Depth of water above center of orifice
 Q (CFS)= Flow

VOLUME CALCULATIONS

POND 13

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

Ab = 6.80
 At = 30,131.00
 Dt = 1.00
 C = 30124.20

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4924.75	0	0	0.0000
4928.75	4.00	0.0006	0.2079
4929.00	4.25	0.0223	0.2144
4929.25	4.50	0.0871	0.2208
4929.50	4.75	0.1952	0.2269
4929.75	5.00	0.3466	0.2329

Orifice Equation

$$Q = \text{CA} \sqrt{2gH}$$

C = 0.6
 Diameter (in) = 2
 Area (ft²) = 0.022
 g = 32.2
 H (Ft) = Depth of water above center of orifice
 Q (CFS) = Flow

VOLUME CALCULATIONS

POND 14

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = Ab * D + 0.5 * C * D^2$$

$$C = (At - Ab) / Dt$$

Ab = 0.00
 At = 1,617.00
 Dt = 1.00
 C = 1617.00

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4926.85	0	0	0.0000
4927.05	0.20	0.0000	0.0028
4927.25	0.40	0.0007	0.0040
4927.45	0.60	0.0030	0.0050
4927.65	0.80	0.0067	0.0058
4927.85	1.00	0.0119	0.0065

Orifice Equation

$$Q = CA \text{ SQRT}(2gH)$$

C = 0.6
 Diameter (in) = 0.5
 Area (ft²) = 0.001
 g = 32.2
 H (Ft) = Depth of water above center of orifice
 Q (CFS) = Flow

VOLUME CALCULATIONS

POND 15

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = Ab * D + 0.5 * C * D^2$$

$$C = (At - Ab) / Dt$$

Ab = 2,625.00
 At = 2,625.00
 Dt = 3.00
 C = 0.00

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4926.75	0	0	0.0000
4927.35	0.60	0.0362	0.2766
4927.95	1.20	0.0723	0.4271
4928.55	1.80	0.1085	0.5370
4929.15	2.40	0.1446	0.6279
4929.75	3.00	0.1808	0.7073

Orifice Equation

$$Q = CA \text{ SQRT}(2gH)$$

C = 0.6
 Diameter (in) 4
 Area (ft^2)= 0.087
 g = 32.2
 H (Ft) = Depth of water above center of orifice
 Q (CFS)= Flow

VOLUME CALCULATIONS

POND 16

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

Ab = 6.80
 At = 16,730.00
 Dt = 1.00
 C = 16723.20

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4925.51	0	0	0.0000
4929.51	4.00	0.0006	0.0033
4929.76	4.25	0.0127	0.0034
4930.01	4.50	0.0487	0.0035
4930.26	4.75	0.1087	0.0036
4930.51	5.00	0.1927	0.0037

Orifice Equation

$$Q = \text{CA} \sqrt{2gH}$$

C = 0.6
 Diameter (in) = 0.25
 Area (ft^2)= 0.000
 g = 32.2
 H (Ft) = Depth of water above center of orifice
 Q (CFS)= Flow

VOLUME CALCULATIONS

POND 17

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

Ab = 0.00
 At = 2,702.00
 Dt = 1.25
 C = 2161.60

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4926.85	0	0	0.0000
4927.10	0.25	0.0000	0.0120
4927.35	0.50	0.0016	0.0178
4927.60	0.75	0.0062	0.0221
4927.85	1.00	0.0140	0.0257
4928.10	1.25	0.0248	0.0289

Orifice Equation

$$Q = \text{CA} \sqrt{2gH}$$

C = 0.6
 Diameter (in) 1
 Area (ft²)= 0.005
 g = 32.2
 H (Ft) = Depth of water above center of orifice
 Q (CFS)= Flow

VOLUME CALCULATIONS POND 18

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

Ab = 6.80
 At = 3,053.00
 Dt = 0.84
 C = 3626.43

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4925.30	0	0	0.00000
4929.30	4.00	0.0006	0.00328
4929.51	4.21	0.0025	0.00336
4929.72	4.42	0.0080	0.00345
4929.93	4.63	0.0172	0.00353
4930.14	4.84	0.0301	0.00361

Orifice Equation

$$Q = \text{CA} \sqrt{2gH}$$

C = 0.6
 Diameter (in) = 0.25
 Area (ft²) = 0.000
 g = 32.2
 H (Ft) = Depth of water above center of orifice
 Q (CFS) = Flow

VOLUME CALCULATIONS

POND 19

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

Ab = 1,399.00
 At = 10,577.00
 Dt = 7.00
 C = 1311.14

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
4923.00	0	0	0.0000
4924.40	1.40	0.0450	0.7167
4925.80	2.80	0.1194	1.0569
4927.20	4.20	0.2529	1.3117
4928.60	5.60	0.4453	1.5245
4930.00	7.00	0.6968	1.7110

Orifice Equation

$$Q = \text{CA} \sqrt{2gH}$$

C = 0.6
 Diameter (in) = 5
 Area (ft²) = 0.136
 g = 32.2
 H (Ft) = Depth of water above center of orifice
 Q (CFS) = Flow

```
TIME= .00
RAIN6= 2.200
```

COMMAND		HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1
NOTATION											
START											
RAINFALL TYPE= 1		TIME= .00 RAIN6= 2.200									
* S BASIN 1											
COMPUTE NM HYD	101.00	-	1		.00114	3.03	.112	1.83567	1.500	4.156 PER IMP=	90.00
* S BASIN 2											
COMPUTE NM HYD	102.00	-	2		.00273	7.40	.275	1.88760	1.500	4.237 PER IMP=	94.00
* S BASIN 3											
COMPUTE NM HYD	103.00	-	3		.00356	9.43	.349	1.83567	1.500	4.140 PER IMP=	90.00
* S BASIN 4											
COMPUTE NM HYD	104.00	-	4		.00267	7.40	.276	1.93952	1.500	4.332 PER IMP=	98.00
* S BASIN 5											
COMPUTE NM HYD	105.00	-	5		.00251	6.77	.251	1.87462	1.500	4.215 PER IMP=	93.00
* S BASIN 6											
COMPUTE NM HYD	106.00	-	6		.00302	8.28	.308	1.91356	1.500	4.283 PER IMP=	96.00
* S BASIN 7											
COMPUTE NM HYD	107.00	-	7		.00271	6.78	.247	1.70586	1.500	3.908 PER IMP=	80.00
* S BASIN 8											
COMPUTE NM HYD	108.00	-	8		.00094	2.29	.082	1.64096	1.500	3.806 PER IMP=	75.00
* S BASIN 9											
COMPUTE NM HYD	109.00	-	9		.00049	.64	.017	.66738	1.533	2.049 PER IMP=	.00
* S BASIN 10											
COMPUTE NM HYD	110.00	-	10		.00040	1.00	.036	1.67990	1.500	3.916 PER IMP=	78.00
* S BASIN 11											
COMPUTE NM HYD	111.00	-	11		.00036	.90	.032	1.67990	1.500	3.919 PER IMP=	78.00
* S BASIN 12											
COMPUTE NM HYD	112.00	-	12		.00027	.75	.027	1.90058	1.500	4.314 PER IMP=	95.00
* S BASIN 13											
COMPUTE NM HYD	113.00	-	13		.00388	10.40	.385	1.86163	1.500	4.187 PER IMP=	92.00
* S BASIN 14											
COMPUTE NM HYD	114.00	-	14		.00010	.29	.010	1.96548	1.500	4.496 PER IMP=	100.00
* S BASIN 15											
COMPUTE NM HYD	115.00	-	15		.00015	.20	.005	.66738	1.533	2.102 PER IMP=	.00
* S BASIN 16											
COMPUTE NM HYD	116.00	-	16		.00099	2.78	.104	1.96548	1.500	4.381 PER IMP=	100.00
* S BASIN 17											
COMPUTE NM HYD	117.00	-	17		.00019	.54	.020	1.96548	1.500	4.437 PER IMP=	100.00
* S BASIN 18											
COMPUTE NM HYD	118.00	-	18		.00030	.71	.025	1.55009	1.500	3.697 PER IMP=	68.00
* S BASIN 19											
COMPUTE NM HYD	119.00	-	19		.00047	.62	.017	.66738	1.533	2.051 PER IMP=	.00
* S BASIN 20											
COMPUTE NM HYD	120.00	-	20		.00681	19.05	.714	1.96548	1.500	4.371 PER IMP=	100.00
* S BASIN OS-1											
COMPUTE NM HYD	121.00	-	21		.00134	3.75	.140	1.96548	1.500	4.378 PER IMP=	100.00
* S BASIN OS-2											
COMPUTE NM HYD	122.00	-	22		.00028	.42	.012	.79719	1.500	2.340 PER IMP=	10.00
* S BASIN OS-3											
COMPUTE NM HYD	123.00	-	23		.00011	.17	.005	.79719	1.500	2.412 PER IMP=	10.00

[illegible]

220094DRAIN.txt

```

*****
*
*           WAL-MART SOUTH #5430-00 DRAINAGE ANALYSIS
*           COORS BLVD. AND RIO BRAVO BLVD. (220094)
*           PROPOSED CONDITIONS (100-YEAR, 6-HR STORM)
*
*****
*
START          TIME=0.0 HR
RAINFALL       TYPE=1 RAIN QUARTER=0.0 IN
               RAIN ONE=1.87 IN RAIN SIX=2.20 IN
               RAIN DAY=2.66 IN DT=0.03333 HR
*
*S BASIN 1
*
COMPUTE NM HYD      ID=1 HYD NO=101 AREA=0.00114 SQ MI
                   PER A=0 PER B=10.00 PER C=0.00 PER D=90.00
                   TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=1 CODE=1
*
*S BASIN 2
*
COMPUTE NM HYD      ID=2 HYD NO=102 AREA=0.00273 SQ MI
                   PER A=0 PER B=6.00 PER C=0.00 PER D=94.00
                   TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=2 CODE=1
*
*S BASIN 3
*
COMPUTE NM HYD      ID=3 HYD NO=103 AREA=0.00356 SQ MI
                   PER A=0 PER B=10.00 PER C=0.00 PER D=90.00
                   TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=3 CODE=1
*
*S BASIN 4
*
COMPUTE NM HYD      ID=4 HYD NO=104 AREA=0.00267 SQ MI
                   PER A=0 PER B=2.00 PER C=0.00 PER D=98.00
                   TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=4 CODE=1
*
*S BASIN 5
*
COMPUTE NM HYD      ID=5 HYD NO=105 AREA=0.00251 SQ MI
                   PER A=0 PER B=7.00 PER C=0.00 PER D=93.00
                   TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=5 CODE=1
*
*S BASIN 6
*
COMPUTE NM HYD      ID=6 HYD NO=106 AREA=0.00302 SQ MI
                   PER A=0 PER B=4.00 PER C=0.00 PER D=96.00
                   TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=6 CODE=1
*
*S BASIN 7
*

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                                220094DRAIN.txt
COMPUTE NM HYD      ID=7 HYD NO=107 AREA=0.00271 SQ MI
                    PER A=0 PER B=20.00 PER C=0.00 PER D=80.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=7 CODE=1

*
*S BASIN 8
*
COMPUTE NM HYD      ID=8 HYD NO=108 AREA=0.00094 SQ MI
                    PER A=0 PER B=25.00 PER C=0.00 PER D=75.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=8 CODE=1

*
*S BASIN 9
*
COMPUTE NM HYD      ID=9 HYD NO=109 AREA=0.00049 SQ MI
                    PER A=0 PER B=100.00 PER C=0.00 PER D=0.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=9 CODE=1

*
*S BASIN 10
*
COMPUTE NM HYD      ID=10 HYD NO=110 AREA=0.00040 SQ MI
                    PER A=0 PER B=22.00 PER C=0.00 PER D=78.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=10 CODE=1

*
*S BASIN 11
*
COMPUTE NM HYD      ID=11 HYD NO=111 AREA=0.00036 SQ MI
                    PER A=0 PER B=22.00 PER C=0.00 PER D=78.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=11 CODE=1

*
*S BASIN 12
*
COMPUTE NM HYD      ID=12 HYD NO=112 AREA=0.00027 SQ MI
                    PER A=0 PER B=5.00 PER C=0.00 PER D=95.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=12 CODE=1

*
*S BASIN 13
*
COMPUTE NM HYD      ID=13 HYD NO=113 AREA=0.00388 SQ MI
                    PER A=0 PER B=8.00 PER C=0.00 PER D=92.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=13 CODE=1

*
*S BASIN 14
*
COMPUTE NM HYD      ID=14 HYD NO=114 AREA=0.00010 SQ MI
                    PER A=0 PER B=0.00 PER C=0.00 PER D=100.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=14 CODE=1

*
*S BASIN 15

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220094DRAIN.txt

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*
COMPUTE NM HYD      ID=15 HYD NO=115 AREA=0.00015 SQ MI
                    PER A=0 PER B=100.00 PER C=0.00 PER D=0.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=15 CODE=1

*
*S BASIN 16
*
COMPUTE NM HYD      ID=16 HYD NO=116 AREA=0.00099 SQ MI
                    PER A=0 PER B=0.00 PER C=0.00 PER D=100.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=16 CODE=1

*
*S BASIN 17
*
COMPUTE NM HYD      ID=17 HYD NO=117 AREA=0.00019 SQ MI
                    PER A=0 PER B=0.00 PER C=0.00 PER D=100.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=17 CODE=1

*
*S BASIN 18
*
COMPUTE NM HYD      ID=18 HYD NO=118 AREA=0.00030 SQ MI
                    PER A=0 PER B=32.00 PER C=0.00 PER D=68.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=18 CODE=1

*
*S BASIN 19
*
COMPUTE NM HYD      ID=19 HYD NO=119 AREA=0.00047 SQ MI
                    PER A=0 PER B=100.00 PER C=0.00 PER D=0.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=19 CODE=1

*
*S BASIN 20
*
COMPUTE NM HYD      ID=20 HYD NO=120 AREA=0.00681 SQ MI
                    PER A=0 PER B=0.00 PER C=0.00 PER D=100.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=20 CODE=1

*
*S BASIN OS-1
*
COMPUTE NM HYD      ID=21 HYD NO=121 AREA=0.00134 SQ MI
                    PER A=0 PER B=0.00 PER C=0.00 PER D=100.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=21 CODE=1

*
*S BASIN OS-2
*
COMPUTE NM HYD      ID=22 HYD NO=122 AREA=0.00028 SQ MI
                    PER A=0 PER B=90.00 PER C=0.00 PER D=10.00
                    TP=0 HR MASS RAINFALL=-1
PRINT HYD           ID=22 CODE=1
*

```

*S BASIN OS-3

*

COMPUTE NM HYD

ID=23 HYD NO=123 AREA=0.00011 SQ MI
PER A=0 PER B=90.00 PER C=0.00 PER D=10.00
TP=0 HR MASS RAINFALL=-1
ID=23 CODE=1

PRINT HYD

*

*S BASIN OS-4

*

COMPUTE NM HYD

ID=24 HYD NO=124 AREA=0.00084 SQ MI
PER A=0 PER B=16.00 PER C=0.00 PER D=84.00
TP=0 HR MASS RAINFALL=-1
ID=24 CODE=1

PRINT HYD

*

*S BASIN OS-5

*

COMPUTE NM HYD

ID=25 HYD NO=125 AREA=0.00305 SQ MI
PER A=0 PER B=0.00 PER C=0.00 PER D=100.00
TP=0 HR MASS RAINFALL=-1
ID=25 CODE=1

PRINT HYD

*

*S BASIN OS-6

*

COMPUTE NM HYD

ID=26 HYD NO=126 AREA=0.00229 SQ MI
PER A=0 PER B=0.00 PER C=0.00 PER D=100.00
TP=0 HR MASS RAINFALL=-1
ID=26 CODE=1

PRINT HYD

*S BASIN OS-7

*

COMPUTE NM HYD

ID=27 HYD NO=127 AREA=0.00179 SQ MI
PER A=0 PER B=22.00 PER C=0.00 PER D=78.00
TP=0 HR MASS RAINFALL=-1
ID=27 CODE=1

PRINT HYD

*

*S ADD BASINS 3 AND OS-2

*

ADD HYD

ID=28 HYD NO=151.00 ID=3 ID=22

PRINT HYD

ID=28 CODE=1

*

*S ADD BASINS 5, OS-1 AND OS-3

*

ADD HYD

ID=29 HYD NO=152.00 ID=5 ID=23

ADD HYD

ID=30 HYD NO=153.00 ID=29 ID=21

PRINT HYD

ID=30 CODE=1

*

*S ADD BASINS 7, AND OS-4

*

ADD HYD

ID=31 HYD NO=154.00 ID=7 ID=24

PRINT HYD

ID=31 CODE=1

*

*S ADD BASINS 9, AND OS-5

*

ADD HYD

ID=32 HYD NO=155.00 ID=9 ID=25

PRINT HYD

ID=32 CODE=1

220094DRAIN.txt

*

*S ADD BASINS 15 AND OS-6

*

ADD HYD ID=33 HYD NO=156.00 ID=15 ID=26
 PRINT HYD ID=33 CODE=1

*

*S ADD BASINS 19, 20 AND OS-7

*

ADD HYD ID=34 HYD NO=157.00 ID=19 ID=20
 ADD HYD ID=35 HYD NO=158.00 ID=34 ID=27
 PRINT HYD ID=35 CODE=1

*

*S POND 1

*

ROUTE RESERVOIR ID=36 HYD NO=201.00 INFLOW ID=1 CODE=24
 OUTFLOW(CFS) STORAGE(AC-FT) ELEVATION(FT)
 0.0000 0.0000 4925.79
 0.0024 0.0003 4927.96
 0.0025 0.0157 4928.21
 0.0027 0.0615 4928.46
 0.0028 0.1379 4928.71
 0.0029 0.2449 4928.96

PRINT HYD ID=36 CODE=1

*

*S POND 2

*

ROUTE RESERVOIR ID=37 HYD NO=202.00 INFLOW ID=2 CODE=25
 OUTFLOW(CFS) STORAGE(AC-FT) ELEVATION(FT)
 0.0000 0.0000 4925.24
 0.5242 0.0003 4927.41
 0.5556 0.0129 4927.66
 0.5855 0.0504 4927.91
 0.6140 0.1129 4928.16
 0.6411 0.2005 4928.41

PRINT HYD ID=37 CODE=1

*

*S POND 3

*

ROUTE RESERVOIR ID=38 HYD NO=203.00 INFLOW ID=28 CODE=24
 OUTFLOW(CFS) STORAGE(AC-FT) ELEVATION(FT)
 0.0000 0.0000 4925.04
 0.0024 0.0003 4927.21
 0.0025 0.0252 4927.46
 0.0027 0.0998 4927.71
 0.0028 0.2240 4927.96
 0.0029 0.3979 4928.21

PRINT HYD ID=38 CODE=1

*

*S POND 4

*

ROUTE RESERVOIR ID=39 HYD NO=204.00 INFLOW ID=4 CODE=24
 OUTFLOW(CFS) STORAGE(AC-FT) ELEVATION(FT)
 0.0000 0.0000 4923.83
 0.0032 0.0006 4927.65
 0.0033 0.0207 4927.90

220094DRAIN.txt

0.0034	0.0811	4928.15
0.0035	0.1817	4928.40
0.0036	0.3225	4928.65

PRINT HYD ID=39 CODE=1
*

*S POND 5
*

ROUTE RESERVOIR	ID=40 HYD NO=205.00 INFLOW ID=30 CODE=24	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
		0.0000	0.0000	4924.20
		0.0216	0.0003	4926.37
		0.0228	0.0260	4926.62
		0.0240	0.1029	4926.87
		0.0251	0.2311	4927.12
		0.0262	0.4106	4927.37

PRINT HYD ID=40 CODE=1
*

*S POND 6
*

ROUTE RESERVOIR	ID=41 HYD NO=206.00 INFLOW ID=6 CODE=24	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
		0.0000	0.0000	4922.22
		0.5050	0.0005	4925.67
		0.5237	0.0156	4925.92
		0.5418	0.0606	4926.17
		0.5592	0.1355	4926.42
		0.5762	0.2404	4926.67

PRINT HYD ID=41 CODE=1
*

*S POND 7
*

ROUTE RESERVOIR	ID=42 HYD NO=207.00 INFLOW ID=31 CODE=24	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
		0.0000	0.0000	4923.00
		0.1156	0.0432	4923.60
		0.1718	0.0909	4924.20
		0.2137	0.1476	4924.80
		0.2487	0.2132	4925.40
		0.2793	0.2879	4926.00

PRINT HYD ID=42 CODE=1
*

*S POND 8
*

ROUTE RESERVOIR	ID=43 HYD NO=208.00 INFLOW ID=8 CODE=24	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
		0.0000	0.0000	4922.28
		0.0030	0.0005	4925.67
		0.0031	0.0064	4925.92
		0.0032	0.0238	4926.17
		0.0033	0.0529	4926.42
		0.0034	0.0936	4926.67

PRINT HYD ID=43 CODE=1
*

*S POND 9

220094DRAIN.txt

*

ROUTE RESERVOIR

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
0.0000	0.0000	4921.52
0.0041	0.0377	4921.93
0.0070	0.1161	4922.68
0.0090	0.2135	4923.43
0.0107	0.3300	4924.18
0.0121	0.4656	4924.93

PRINT HYD

*

ID=44 CODE=1

*S POND 10

*

ROUTE RESERVOIR

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
0.0000	0.0000	4925.14
0.2628	0.0006	4929.14
0.2683	0.0016	4929.31
0.2738	0.0047	4929.48
0.2792	0.0097	4929.64
0.2844	0.0167	4929.81

PRINT HYD

*

ID=45 CODE=1

*S POND 11

*

ROUTE RESERVOIR

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
0.0000	0.0000	4925.62
0.2079	0.0006	4929.62
0.2120	0.0015	4929.78
0.2160	0.0041	4929.93
0.2199	0.0084	4930.09
0.2237	0.0144	4930.24

PRINT HYD

*

ID=46 CODE=1

*S POND 12

*

ROUTE RESERVOIR

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
0.0000	0.0000	4926.00
0.2079	0.0006	4930.00
0.2123	0.0013	4930.17
0.2166	0.0034	4930.34
0.2208	0.0069	4930.50
0.2250	0.0118	4930.67

PRINT HYD

*

ID=47 CODE=1

*S POND 13

*

ROUTE RESERVOIR

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
0.0000	0.0000	4924.75
0.2079	0.0006	4928.75
0.2144	0.0223	4929.00
0.2208	0.0871	4929.25

0.2269	0.1952	4929.50
0.2329	0.3466	4929.75

PRINT HYD ID=48 CODE=1
*

*S POND 14
*

ROUTE RESERVOIR	ID=49 HYD NO=214.00 INFLOW ID=14 CODE=24	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
		0.0000	0.0000	4926.85
		0.0028	0.0000	4927.05
		0.0040	0.0007	4927.25
		0.0050	0.0030	4927.45
		0.0058	0.0067	4927.65
		0.0065	0.0119	4927.85

PRINT HYD ID=49 CODE=1
*

*S POND 15
*

ROUTE RESERVOIR	ID=50 HYD NO=215.00 INFLOW ID=33 CODE=24	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
		0.0000	0.0000	4926.75
		0.2766	0.0362	4927.35
		0.4271	0.0723	4927.95
		0.5370	0.1085	4928.55
		0.6279	0.1446	4929.15
		0.7073	0.1808	4929.75

PRINT HYD ID=50 CODE=1
*

*S POND 16
*

ROUTE RESERVOIR	ID=51 HYD NO=216.00 INFLOW ID=16 CODE=24	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
		0.0000	0.0000	4925.51
		0.0033	0.0006	4929.51
		0.0034	0.0127	4929.76
		0.0035	0.0487	4930.01
		0.0036	0.1087	4930.26
		0.0037	0.1927	4930.51

PRINT HYD ID=51 CODE=1
*

*S POND 17
*

ROUTE RESERVOIR	ID=52 HYD NO=217.00 INFLOW ID=17 CODE=24	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
		0.0000	0.0000	4926.85
		0.0120	0.0000	4927.10
		0.0178	0.0016	4927.35
		0.0221	0.0062	4927.60
		0.0259	0.0140	4927.85
		0.0289	0.0248	4928.10

PRINT HYD ID=52 CODE=1
*

*S POND 18
*

ROUTE RESERVOIR	ID=53 HYD NO=218.00 INFLOW ID=18 CODE=24	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)

220094DRAIN.txt

0.00000	0.0000	4925.30
0.00328	0.0006	4929.30
0.00336	0.0025	4929.51
0.00345	0.0080	4929.72
0.00353	0.0172	4929.93
0.00361	0.0301	4930.14

PRINT HYD ID=53 CODE=1

*

*S POND 19

*

ROUTE RESERVOIR	ID=54 HYD NO=219.00 INFLOW ID=35 CODE=24	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
		0.0000	0.0000	4923.00
		0.7167	0.0450	4924.40
		1.0569	0.1194	4925.80
		1.3117	0.2529	4927.20
		1.5245	0.4453	4928.60
		1.7110	0.6968	4930.00

PRINT HYD ID=54 CODE=1

*

*ADD PONDS 1 THRU 19

*

ADD HYD	ID=55 HYD NO=301.00	ID=36	ID=37
ADD HYD	ID=56 HYD NO=302.00	ID=55	ID=38
ADD HYD	ID=57 HYD NO=303.00	ID=56	ID=39
ADD HYD	ID=58 HYD NO=304.00	ID=57	ID=40
ADD HYD	ID=59 HYD NO=305.00	ID=58	ID=41
ADD HYD	ID=60 HYD NO=306.00	ID=42	ID=43
ADD HYD	ID=61 HYD NO=307.00	ID=60	ID=44
ADD HYD	ID=62 HYD NO=308.00	ID=59	ID=61
ADD HYD	ID=63 HYD NO=309.00	ID=62	ID=45
ADD HYD	ID=64 HYD NO=310.00	ID=63	ID=46
ADD HYD	ID=65 HYD NO=311.00	ID=64	ID=47
ADD HYD	ID=66 HYD NO=312.00	ID=54	ID=48
ADD HYD	ID=67 HYD NO=313.00	ID=66	ID=49
ADD HYD	ID=68 HYD NO=314.00	ID=67	ID=50
ADD HYD	ID=69 HYD NO=315.00	ID=68	ID=51
ADD HYD	ID=70 HYD NO=316.00	ID=69	ID=52
ADD HYD	ID=71 HYD NO=317.00	ID=70	ID=53
ADD HYD	ID=72 HYD NO=317.00	ID=71	ID=65

PRINT HYD ID=72 CODE=1

*

FINISH

AHYMO PROGRAM (AHYMO_97) -

- Version: 1997.02d

RUN DATE (MON/DAY/YR) = 02/12/2004

START TIME (HR:MIN:SEC) = 16:22:03

USER NO.= AHYMO-S-

9702d1TierraW-AH

INPUT FILE = C:\AHYMO\1\220094~1.TXT

```
*****
*
*           WAL-MART SOUTH #5430-00 DRAINAGE ANALYSIS
*           COORS BLVD. AND RIO BRAVO BLVD. (220094)
*           PROPOSED CONDITIONS (100-YEAR, 6-HR STORM)
*
*****
```

```
START           TIME=0.0 HR
RAINFALL        TYPE=1 RAIN QUARTER=0.0 IN
                RAIN ONE=1.87 IN RAIN SIX=2.20 IN
                RAIN DAY=2.66 IN DT=0.03333 HR
```

COMPUTED 6-HOUR RAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2

- PEAK AT 1.40 HR.

DT =	.033330 HOURS	END TIME =	5.999400 HOURS
.0000	.0016	.0033	.0050
.0122	.0141	.0160	.0180
.0266	.0289	.0312	.0337
.0443	.0472	.0502	.0534
.0675	.0715	.0758	.0809
.1334	.1771	.2398	.3254
.9780	1.1804	1.2649	1.3363
1.5600	1.6061	1.6493	1.6900
1.8314	1.8623	1.8915	1.9193
1.9630	1.9682	1.9732	1.9780
1.9953	1.9993	2.0031	2.0068
2.0207	2.0240	2.0272	2.0303
2.0420	2.0448	2.0475	2.0502
2.0605	2.0629	2.0653	2.0677
2.0768	2.0790	2.0812	2.0833
2.0916	2.0936	2.0956	2.0976
2.1051	2.1070	2.1088	2.1106
2.1176	2.1193	2.1210	2.1227
2.1292	2.1308	2.1324	2.1340
2.1401	2.1416	2.1431	2.1446
2.1504	2.1518	2.1532	2.1546
2.1600	2.1614	2.1627	2.1640
2.1692	2.1705	2.1718	2.1731
2.1780	2.1792	2.1804	2.1817
2.1864	2.1876	2.1887	2.1899
2.1944	2.1956	2.1967	2.1978
			2.1989
			2.2000

*

*S BASIN 1

*

COMPUTE NM HYD

ID=1 HYD NO=101 AREA=0.00114 SQ MI

PER A=0 PER B=10.00 PER C=0.00 PER D=90.00

TP=0 HR MASS RAINFALL=-1

*****Warning*****A value for the Time to Peak was not previously computed; use Tp=0.133333 hrs.

TIME TO PEAK (hrs)= .1333

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 4.0497 CFS UNIT VOLUME = .9965 B =
526.28 P60 = 1.8700
AREA = .001026 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = .27966 CFS UNIT VOLUME = .9499 B =
327.09 P60 = 1.8700
AREA = .000114 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 101.00

RUNOFF VOLUME = 1.83567 INCHES = .1116 ACRE-FEET
PEAK DISCHARGE RATE = 3.03 CFS AT 1.500 HOURS BASIN AREA =
.0011 SQ. MI.

*
*S BASIN 2
*

COMPUTE NM HYD ID=2 HYD NO=102 AREA=0.00273 SQ MI
PER A=0 PER B=6.00 PER C=0.00 PER D=94.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 10.129 CFS UNIT VOLUME = .9982 B =
526.28 P60 = 1.8700
AREA = .002566 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
 SHAPE CONSTANT, N = 3.593454
 UNIT PEAK = .40183 CFS UNIT VOLUME = .9673 B =
 327.09 P60 = 1.8700
 AREA = .000164 SQ MI IA = .50000 INCHES INF = 1.25000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
 = .033330

PRINT HYD ID=2 CODE=1

PARTIAL HYDROGRAPH 102.00

RUNOFF VOLUME = 1.88760 INCHES = .2748 ACRE-FEET
 PEAK DISCHARGE RATE = 7.40 CFS AT 1.500 HOURS BASIN AREA =
 .0027 SQ. MI.

*
 *S BASIN 3
 *

COMPUTE NM HYD ID=3 HYD NO=103 AREA=0.00356 SQ MI
 PER A=0 PER B=10.00 PER C=0.00 PER D=90.00
 TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 12.646 CFS UNIT VOLUME = .9985 B =
 526.28 P60 = 1.8700
 AREA = .003204 SQ MI IA = .10000 INCHES INF = .04000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
 = .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
 SHAPE CONSTANT, N = 3.593454
 UNIT PEAK = .87333 CFS UNIT VOLUME = .9849 B =
 327.09 P60 = 1.8700
 AREA = .000356 SQ MI IA = .50000 INCHES INF = 1.25000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
 = .033330

PRINT HYD ID=3 CODE=1

PARTIAL HYDROGRAPH 103.00

RUNOFF VOLUME = 1.83567 INCHES = .3485 ACRE-FEET
PEAK DISCHARGE RATE = 9.43 CFS AT 1.500 HOURS BASIN AREA =
.0036 SQ. MI.

*
*S BASIN 4
*

COMPUTE NM HYD ID=4 HYD NO=104 AREA=0.00267 SQ MI
PER A=0 PER B=2.00 PER C=0.00 PER D=98.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed
hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 10.328 CFS UNIT VOLUME = .9982 B =
526.28 P60 = 1.8700
AREA = .002617 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = .13100 CFS UNIT VOLUME = .8921 B =
327.09 P60 = 1.8700
AREA = .000053 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=4 CODE=1

PARTIAL HYDROGRAPH 104.00

RUNOFF VOLUME = 1.93952 INCHES = .2762 ACRE-FEET
PEAK DISCHARGE RATE = 7.40 CFS AT 1.500 HOURS BASIN AREA =
.0027 SQ. MI.

*
*S BASIN 5
*

COMPUTE NM HYD ID=5 HYD NO=105 AREA=0.00251 SQ MI
PER A=0 PER B=7.00 PER C=0.00 PER D=93.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333
*****Warning*****This Tp value was used for a previously computed hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 9.2137 CFS UNIT VOLUME = .9980 B =
526.28 P60 = 1.8700
AREA = .002334 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = .43102 CFS UNIT VOLUME = .9673 B =
327.09 P60 = 1.8700
AREA = .000176 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=5 CODE=1

PARTIAL HYDROGRAPH 105.00

RUNOFF VOLUME = 1.87462 INCHES = .2509 ACRE-FEET
PEAK DISCHARGE RATE = 6.77 CFS AT 1.500 HOURS BASIN AREA =
.0025 SQ. MI.

*
*S BASIN 6
*

COMPUTE NM HYD ID=6 HYD NO=106 AREA=0.00302 SQ MI
PER A=0 PER B=4.00 PER C=0.00 PER D=96.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333
*****Warning*****This Tp value was used for a previously computed hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 11.443 CFS UNIT VOLUME = .9984 B =
526.28 P60 = 1.8700
AREA = .002899 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = .29634 CFS UNIT VOLUME = .9540 B =
327.09 P60 = 1.8700
AREA = .000121 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=6 CODE=1

PARTIAL HYDROGRAPH 106.00

RUNOFF VOLUME = 1.91356 INCHES = .3082 ACRE-FEET
PEAK DISCHARGE RATE = 8.28 CFS AT 1.500 HOURS BASIN AREA =
.0030 SQ. MI.

*
*S BASIN 7
*

COMPUTE NM HYD ID=7 HYD NO=107 AREA=0.00271 SQ MI
PER A=0 PER B=20.00 PER C=0.00 PER D=80.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed
hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 8.5573 CFS UNIT VOLUME = .9980 B =
526.28 P60 = 1.8700
AREA = .002168 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = 1.3296 CFS UNIT VOLUME = .9903 B =
327.09 P60 = 1.8700
AREA = .000542 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=7 CODE=1

PARTIAL HYDROGRAPH 107.00

RUNOFF VOLUME = 1.70586 INCHES = .2466 ACRE-FEET
PEAK DISCHARGE RATE = 6.78 CFS AT 1.500 HOURS BASIN AREA =
.0027 SQ. MI.

*

*S BASIN 8

*

COMPUTE NM HYD ID=8 HYD NO=108 AREA=0.00094 SQ MI
PER A=0 PER B=25.00 PER C=0.00 PER D=75.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed
hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 2.7827 CFS UNIT VOLUME = .9955 B =
526.28 P60 = 1.8700
AREA = .000705 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = .57649 CFS UNIT VOLUME = .9768 B =
327.09 P60 = 1.8700
AREA = .000235 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=8 CODE=1

PARTIAL HYDROGRAPH 108.00

RUNOFF VOLUME = 1.64096 INCHES = .0823 ACRE-FEET
PEAK DISCHARGE RATE = 2.29 CFS AT 1.500 HOURS BASIN AREA =
.0009 SQ. MI.

*

*S BASIN 9

*

COMPUTE NM HYD ID=9 HYD NO=109 AREA=0.00049 SQ MI
PER A=0 PER B=100.00 PER C=0.00 PER D=0.00

TP=0 HR MASS RAINFALL=-1
TIME TO PEAK (hrs)= .1333
*****Warning*****This Tp value was used for a previously computed hydrograph.

A new Tp value should be computed.

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = 1.2020 CFS UNIT VOLUME = .9894 B =
327.09 P60 = 1.8700
AREA = .000490 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=9 CODE=1

PARTIAL HYDROGRAPH 109.00

RUNOFF VOLUME = .66738 INCHES = .0174 ACRE-FEET
PEAK DISCHARGE RATE = .64 CFS AT 1.533 HOURS BASIN AREA =
.0005 SQ. MI.

*
*S BASIN 10
*

COMPUTE NM HYD ID=10 HYD NO=110 AREA=0.00040 SQ MI
PER A=0 PER B=22.00 PER C=0.00 PER D=78.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333
*****Warning*****This Tp value was used for a previously computed hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 1.2315 CFS UNIT VOLUME = .9897 B =
526.28 P60 = 1.8700
AREA = .000312 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = .21588 CFS UNIT VOLUME = .9353 B =
327.09 P60 = 1.8700
AREA = .000088 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=10 CODE=1

PARTIAL HYDROGRAPH 110.00

RUNOFF VOLUME = 1.67990 INCHES = .0358 ACRE-Feet
PEAK DISCHARGE RATE = 1.00 CFS AT 1.500 HOURS BASIN AREA =
.0004 SQ. MI.

*

*S BASIN 11

*

COMPUTE NM HYD ID=11 HYD NO=111 AREA=0.00036 SQ MI
PER A=0 PER B=22.00 PER C=0.00 PER D=78.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed
hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 1.1083 CFS UNIT VOLUME = .9897 B =
526.28 P60 = 1.8700
AREA = .000281 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = .19429 CFS UNIT VOLUME = .9295 B =
327.09 P60 = 1.8700
AREA = .000079 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=11 CODE=1

PARTIAL HYDROGRAPH 111.00

RUNOFF VOLUME = 1.67990 INCHES = .0323 ACRE-Feet
PEAK DISCHARGE RATE = .90 CFS AT 1.500 HOURS BASIN AREA =
.0004 SQ. MI.

*

*S BASIN 12

*

COMPUTE NM HYD

ID=12 HYD NO=112 AREA=0.00027 SQ MI

PER A=0 PER B=5.00 PER C=0.00 PER D=95.00

TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000

SHAPE CONSTANT, N = 7.106420

UNIT PEAK = 1.0124 CFS UNIT VOLUME = .9881 B =

526.28 P60 = 1.8700

AREA = .000257 SQ MI IA = .10000 INCHES INF = .04000

INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685

SHAPE CONSTANT, N = 3.593454

UNIT PEAK = .33118E-01CFS UNIT VOLUME = .8721 B =

327.09 P60 = 1.8700

AREA = .000014 SQ MI IA = .50000 INCHES INF = 1.25000

INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD

ID=12 CODE=1

PARTIAL HYDROGRAPH 112.00

RUNOFF VOLUME = 1.90058 INCHES = .0274 ACRE-FEET

PEAK DISCHARGE RATE = .75 CFS AT 1.500 HOURS BASIN AREA =
.0003 SQ. MI.

*

*S BASIN 13

*

COMPUTE NM HYD

ID=13 HYD NO=113 AREA=0.00388 SQ MI

PER A=0 PER B=8.00 PER C=0.00 PER D=92.00

TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 14.089 CFS UNIT VOLUME = .9985 B =
 526.28 P60 = 1.8700
 AREA = .003570 SQ MI IA = .10000 INCHES INF = .04000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
 = .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
 SHAPE CONSTANT, N = 3.593454
 UNIT PEAK = .76146 CFS UNIT VOLUME = .9821 B =
 327.09 P60 = 1.8700
 AREA = .000310 SQ MI IA = .50000 INCHES INF = 1.25000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
 = .033330

PRINT HYD ID=13 CODE=1

PARTIAL HYDROGRAPH 113.00

RUNOFF VOLUME = 1.86163 INCHES = .3852 ACRE-FEET
 PEAK DISCHARGE RATE = 10.40 CFS AT 1.500 HOURS BASIN AREA =
 .0039 SQ. MI.

*

*S BASIN 14

*

COMPUTE NM HYD ID=14 HYD NO=114 AREA=0.00010 SQ MI
 PER A=0 PER B=0.00 PER C=0.00 PER D=100.00
 TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = .39471 CFS UNIT VOLUME = .9711 B =
 526.28 P60 = 1.8700
 AREA = .000100 SQ MI IA = .10000 INCHES INF = .04000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
 = .033330

PRINT HYD ID=14 CODE=1

PARTIAL HYDROGRAPH 114.00

RUNOFF VOLUME = 1.96548 INCHES = .0105 ACRE-FEET
PEAK DISCHARGE RATE = .29 CFS AT 1.500 HOURS BASIN AREA =
.0001 SQ. MI.

*

*S BASIN 15

*

COMPUTE NM HYD ID=15 HYD NO=115 AREA=0.00015 SQ MI
PER A=0 PER B=100.00 PER C=0.00 PER D=0.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed
hydrograph.

A new Tp value should be computed.

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = .36797 CFS UNIT VOLUME = .9644 B =
327.09 P60 = 1.8700
AREA = .000150 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=15 CODE=1

PARTIAL HYDROGRAPH 115.00

RUNOFF VOLUME = .66738 INCHES = .0053 ACRE-FEET
PEAK DISCHARGE RATE = .20 CFS AT 1.533 HOURS BASIN AREA =
.0002 SQ. MI.

*

*S BASIN 16

*

COMPUTE NM HYD ID=16 HYD NO=116 AREA=0.00099 SQ MI
PER A=0 PER B=0.00 PER C=0.00 PER D=100.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed
hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 3.9076 CFS UNIT VOLUME = .9965 B =
526.28 P60 = 1.8700

AREA = .000990 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=16 CODE=1

PARTIAL HYDROGRAPH 116.00

RUNOFF VOLUME = 1.96548 INCHES = .1038 ACRE-FEET
PEAK DISCHARGE RATE = 2.78 CFS AT 1.500 HOURS BASIN AREA =
.0010 SQ. MI.

*
*S BASIN 17
*

COMPUTE NM HYD ID=17 HYD NO=117 AREA=0.00019 SQ MI
PER A=0 PER B=0.00 PER C=0.00 PER D=100.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed
hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = .74994 CFS UNIT VOLUME = .9840 B =
526.28 P60 = 1.8700
AREA = .000190 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=17 CODE=1

PARTIAL HYDROGRAPH 117.00

RUNOFF VOLUME = 1.96548 INCHES = .0199 ACRE-FEET
PEAK DISCHARGE RATE = .54 CFS AT 1.500 HOURS BASIN AREA =
.0002 SQ. MI.

*
*S BASIN 18
*

COMPUTE NM HYD ID=18 HYD NO=118 AREA=0.00030 SQ MI
PER A=0 PER B=32.00 PER C=0.00 PER D=68.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = .80520 CFS UNIT VOLUME = .9862 B =
526.28 P60 = 1.8700
AREA = .000204 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = .23550 CFS UNIT VOLUME = .9406 B =
327.09 P60 = 1.8700
AREA = .000096 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=18 CODE=1

PARTIAL HYDROGRAPH 118.00

RUNOFF VOLUME = 1.55009 INCHES = .0248 ACRE-Feet
PEAK DISCHARGE RATE = .71 CFS AT 1.500 HOURS BASIN AREA =
.0003 SQ. MI.

*

*S BASIN 19

*

COMPUTE NM HYD ID=19 HYD NO=119 AREA=0.00047 SQ MI
PER A=0 PER B=100.00 PER C=0.00 PER D=0.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed hydrograph.

A new Tp value should be computed.

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = 1.1530 CFS UNIT VOLUME = .9884 B =
327.09 P60 = 1.8700
AREA = .000470 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD

ID=19 CODE=1

PARTIAL HYDROGRAPH 119.00

RUNOFF VOLUME = .66738 INCHES = .0167 ACRE-Feet
PEAK DISCHARGE RATE = .62 CFS AT 1.533 HOURS BASIN AREA =
.0005 SQ. MI.

*
*S BASIN 20
*

COMPUTE NM HYD ID=20 HYD NO=120 AREA=0.00681 SQ MI
PER A=0 PER B=0.00 PER C=0.00 PER D=100.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed
hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 26.880 CFS UNIT VOLUME = .9989 B =
526.28 P60 = 1.8700
AREA = .006810 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD

ID=20 CODE=1

PARTIAL HYDROGRAPH 120.00

RUNOFF VOLUME = 1.96548 INCHES = .7139 ACRE-Feet
PEAK DISCHARGE RATE = 19.05 CFS AT 1.500 HOURS BASIN AREA =
.0068 SQ. MI.

*
*S BASIN OS-1
*

COMPUTE NM HYD ID=21 HYD NO=121 AREA=0.00134 SQ MI
PER A=0 PER B=0.00 PER C=0.00 PER D=100.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed
hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 5.2891 CFS UNIT VOLUME = .9973 B =
 526.28 P60 = 1.8700
 AREA = .001340 SQ MI IA = .10000 INCHES INF = .04000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
 = .033330

PRINT HYD ID=21 CODE=1

PARTIAL HYDROGRAPH 121.00

RUNOFF VOLUME = 1.96548 INCHES = .1405 ACRE-FEET
 PEAK DISCHARGE RATE = 3.75 CFS AT 1.500 HOURS BASIN AREA =
 .0013 SQ. MI.

*
 *S BASIN OS-2
 *

COMPUTE NM HYD ID=22 HYD NO=122 AREA=0.00028 SQ MI
 PER A=0 PER B=90.00 PER C=0.00 PER D=10.00
 TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = .11052 CFS UNIT VOLUME = .9032 B =
 526.28 P60 = 1.8700
 AREA = .000028 SQ MI IA = .10000 INCHES INF = .04000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
 = .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
 SHAPE CONSTANT, N = 3.593454
 UNIT PEAK = .61820 CFS UNIT VOLUME = .9787 B =
 327.09 P60 = 1.8700
 AREA = .000252 SQ MI IA = .50000 INCHES INF = 1.25000
 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
 = .033330

PRINT HYD ID=22 CODE=1

PARTIAL HYDROGRAPH 122.00

RUNOFF VOLUME = .79719 INCHES = .0119 ACRE-FEET
PEAK DISCHARGE RATE = .42 CFS AT 1.500 HOURS BASIN AREA =
.0003 SQ. MI.

*

*S BASIN OS-3

*

COMPUTE NM HYD ID=23 HYD NO=123 AREA=0.00011 SQ MI
PER A=0 PER B=90.00 PER C=0.00 PER D=10.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed
hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = .43418E-01CFS UNIT VOLUME = .8873 B =
526.28 P60 = 1.8700
AREA = .000011 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = .24286 CFS UNIT VOLUME = .9454 B =
327.09 P60 = 1.8700
AREA = .000099 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=23 CODE=1

PARTIAL HYDROGRAPH 123.00

RUNOFF VOLUME = .79719 INCHES = .0047 ACRE-FEET
PEAK DISCHARGE RATE = .17 CFS AT 1.500 HOURS BASIN AREA =
.0001 SQ. MI.

*

*S BASIN OS-4

*

COMPUTE NM HYD ID=24 HYD NO=124 AREA=0.00084 SQ MI
PER A=0 PER B=16.00 PER C=0.00 PER D=84.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 2.7851 CFS UNIT VOLUME = .9955 B =
526.28 P60 = 1.8700
AREA = .000706 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = .32971 CFS UNIT VOLUME = .9578 B =
327.09 P60 = 1.8700
AREA = .000134 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=24 CODE=1

PARTIAL HYDROGRAPH 124.00

RUNOFF VOLUME = 1.75779 INCHES = .0787 ACRE-FEET
PEAK DISCHARGE RATE = 2.16 CFS AT 1.500 HOURS BASIN AREA =
.0008 SQ. MI.

*
*S BASIN OS-5
*

COMPUTE NM HYD ID=25 HYD NO=125 AREA=0.00305 SQ MI
PER A=0 PER B=0.00 PER C=0.00 PER D=100.00
TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 12.039 CFS UNIT VOLUME = .9984 B =
526.28 P60 = 1.8700
AREA = .003050 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD

ID=25 CODE=1

PARTIAL HYDROGRAPH 125.00

RUNOFF VOLUME = 1.96548 INCHES = .3197 ACRE-FEET
PEAK DISCHARGE RATE = 8.54 CFS AT 1.500 HOURS BASIN AREA =
.0031 SQ. MI.

*

*S BASIN OS-6

*

COMPUTE NM HYD

ID=26 HYD NO=126 AREA=0.00229 SQ MI

PER A=0 PER B=0.00 PER C=0.00 PER D=100.00

TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed
hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420

UNIT PEAK = 9.0388 CFS UNIT VOLUME = .9980 B =
526.28 P60 = 1.8700

AREA = .002290 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD

ID=26 CODE=1

PARTIAL HYDROGRAPH 126.00

RUNOFF VOLUME = 1.96548 INCHES = .2400 ACRE-FEET
PEAK DISCHARGE RATE = 6.41 CFS AT 1.500 HOURS BASIN AREA =
.0023 SQ. MI.

*S BASIN OS-7

*

COMPUTE NM HYD

ID=27 HYD NO=127 AREA=0.00179 SQ MI

PER A=0 PER B=22.00 PER C=0.00 PER D=78.00

TP=0 HR MASS RAINFALL=-1

TIME TO PEAK (hrs)= .1333

*****Warning*****This Tp value was used for a previously computed
hydrograph.

A new Tp value should be computed.

K = .072666HR TP = .133333HR K/TP RATIO = .545000
SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 5.5109 CFS UNIT VOLUME = .9973 B =
526.28 P60 = 1.8700
AREA = .001396 SQ MI IA = .10000 INCHES INF = .04000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

K = .131024HR TP = .133333HR K/TP RATIO = .982685
SHAPE CONSTANT, N = 3.593454
UNIT PEAK = .96606 CFS UNIT VOLUME = .9862 B =
327.09 P60 = 1.8700
AREA = .000394 SQ MI IA = .50000 INCHES INF = 1.25000
INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT
= .033330

PRINT HYD ID=27 CODE=1

PARTIAL HYDROGRAPH 127.00

RUNOFF VOLUME = 1.67990 INCHES = .1604 ACRE-FEET
PEAK DISCHARGE RATE = 4.43 CFS AT 1.500 HOURS BASIN AREA =
.0018 SQ. MI.

*
*S ADD BASINS 3 AND OS-2
*

ADD HYD ID=28 HYD NO=151.00 ID=3 ID=22
PRINT HYD ID=28 CODE=1

PARTIAL HYDROGRAPH 151.00

RUNOFF VOLUME = 1.75916 INCHES = .3603 ACRE-FEET
PEAK DISCHARGE RATE = 9.85 CFS AT 1.500 HOURS BASIN AREA =
.0038 SQ. MI.

*
*S ADD BASINS 5, OS-1 AND OS-3
*

ADD HYD ID=29 HYD NO=152.00 ID=5 ID=23
ADD HYD ID=30 HYD NO=153.00 ID=29 ID=21
PRINT HYD ID=30 CODE=1

PARTIAL HYDROGRAPH 153.00

RUNOFF VOLUME = 1.87493 INCHES = .3960 ACRE-FEET
PEAK DISCHARGE RATE = 10.69 CFS AT 1.500 HOURS BASIN AREA =
.0040 SQ. MI.

*

*S ADD BASINS 7, AND OS-4

*

ADD HYD ID=31 HYD NO=154.00 ID=7 ID=24
PRINT HYD ID=31 CODE=1

PARTIAL HYDROGRAPH 154.00

RUNOFF VOLUME = 1.71799 INCHES = .3253 ACRE-FEET
PEAK DISCHARGE RATE = 8.94 CFS AT 1.500 HOURS BASIN AREA =
.0036 SQ. MI.

*

*S ADD BASINS 9, AND OS-5

*

ADD HYD ID=32 HYD NO=155.00 ID=9 ID=25
PRINT HYD ID=32 CODE=1

PARTIAL HYDROGRAPH 155.00

RUNOFF VOLUME = 1.78569 INCHES = .3371 ACRE-FEET
PEAK DISCHARGE RATE = 9.18 CFS AT 1.500 HOURS BASIN AREA =
.0035 SQ. MI.

*

*S ADD BASINS 15 AND OS-6

*

ADD HYD ID=33 HYD NO=156.00 ID=15 ID=26
PRINT HYD ID=33 CODE=1

PARTIAL HYDROGRAPH 156.00

RUNOFF VOLUME = 1.88553 INCHES = .2454 ACRE-FEET
PEAK DISCHARGE RATE = 6.61 CFS AT 1.500 HOURS BASIN AREA =
.0024 SQ. MI.

*

*S ADD BASINS 19, 20 AND OS-7

*

ADD HYD ID=34 HYD NO=157.00 ID=19 ID=20
ADD HYD ID=35 HYD NO=158.00 ID=34 ID=27
PRINT HYD ID=35 CODE=1

PARTIAL HYDROGRAPH 158.00

RUNOFF VOLUME = 1.84179 INCHES = .8909 ACRE-FEET
PEAK DISCHARGE RATE = 24.09 CFS AT 1.500 HOURS BASIN AREA =
.0091 SQ. MI.

*

*S POND 1

*

ROUTE RESERVOIR ID=36 HYD NO=201.00 INFLOW ID=1 CODE=24
OUTFLOW(CFS) STORAGE(AC-FT) ELEVATION(FT)
0.0000 0.0000 4925.79
0.0024 0.0003 4927.96
0.0025 0.0157 4928.21
0.0027 0.0615 4928.46
0.0028 0.1379 4928.71
0.0029 0.2449 4928.96

* * * * *

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4925.79	.000	.00
.80	.00	4925.79	.000	.00
1.60	2.09	4928.42	.054	.00
2.40	.12	4928.60	.103	.00
3.20	.02	4928.61	.107	.00
4.00	.02	4928.61	.108	.00
4.80	.02	4928.61	.109	.00
5.60	.02	4928.62	.110	.00

PEAK DISCHARGE = .003 CFS - PEAK OCCURS AT HOUR 6.30

MAXIMUM WATER SURFACE ELEVATION = 4928.620

MAXIMUM STORAGE = .1104 AC-FT INCREMENTAL TIME=
.033330HRS

PRINT HYD ID=36 CODE=1

PARTIAL HYDROGRAPH 201.00

RUNOFF VOLUME = .07031 INCHES = .0043 ACRE-FEET
PEAK DISCHARGE RATE = .00 CFS AT 6.299 HOURS BASIN AREA =
.0011 SQ. MI.

*

*S POND 2

*

ROUTE RESERVOIR ID=37 HYD NO=202.00 INFLOW ID=2 CODE=25

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
0.0000	0.0000	4925.24
0.5242	0.0003	4927.41
0.5556	0.0129	4927.66
0.5855	0.0504	4927.91
0.6140	0.1129	4928.16
0.6411	0.2005	4928.41

* * * * *

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4925.24	.000	.00
.80	.00	4925.24	.000	.00
1.60	5.09	4928.16	.114	.61
2.40	.31	4928.39	.195	.64
3.20	.06	4928.30	.162	.63
4.00	.04	4928.19	.124	.62
4.80	.04	4928.05	.086	.60
5.60	.05	4927.91	.050	.59
6.40	.00	4927.67	.015	.56

PEAK DISCHARGE = .640 CFS - PEAK OCCURS AT HOUR 2.20
MAXIMUM WATER SURFACE ELEVATION = 4928.403
MAXIMUM STORAGE = .1981 AC-FT INCREMENTAL TIME=
.033330HRS

PRINT HYD ID=37 CODE=1

PARTIAL HYDROGRAPH 202.00

RUNOFF VOLUME = 1.88900 INCHES = .2750 ACRE-FeET
PEAK DISCHARGE RATE = .64 CFS AT 2.200 HOURS BASIN AREA =
.0027 SQ. MI.

*

*S POND 3

*

ROUTE RESERVOIR ID=38 HYD NO=203.00 INFLOW ID=28 CODE=24

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
0.0000	0.0000	4925.04
0.0024	0.0003	4927.21
0.0025	0.0252	4927.46
0.0027	0.0998	4927.71
0.0028	0.2240	4927.96
0.0029	0.3979	4928.21

* * * * *

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4925.04	.000	.00
.80	.00	4925.04	.000	.00
1.60	6.83	4927.86	.174	.00
2.40	.41	4928.12	.334	.00
3.20	.08	4928.13	.346	.00
4.00	.05	4928.14	.350	.00
4.80	.05	4928.15	.353	.00
5.60	.06	4928.15	.356	.00
6.40	.01	4928.15	.359	.00

PEAK DISCHARGE = .003 CFS - PEAK OCCURS AT HOUR 6.53

MAXIMUM WATER SURFACE ELEVATION = 4928.154

MAXIMUM STORAGE = .3590 AC-FT INCREMENTAL TIME=
.033330HRS

PRINT HYD ID=38 CODE=1

PARTIAL HYDROGRAPH 203.00

RUNOFF VOLUME = .02175 INCHES = .0045 ACRE-FEET

PEAK DISCHARGE RATE = .00 CFS AT 6.533 HOURS BASIN AREA =
.0038 SQ. MI.

*

*S POND 4

*

ROUTE RESERVOIR	ID=39 HYD NO=204.00 INFLOW ID=4 CODE=24
OUTFLOW(CFS)	STORAGE(AC-FT) ELEVATION(FT)
0.0000	0.0000 4923.83
0.0032	0.0006 4927.65
0.0033	0.0207 4927.90
0.0034	0.0811 4928.15
0.0035	0.1817 4928.40
0.0036	0.3225 4928.65

* * * * *

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4923.83	.000	.00
.80	.00	4923.83	.000	.00
1.60	5.07	4928.28	.132	.00
2.40	.31	4928.53	.255	.00
3.20	.06	4928.55	.264	.00
4.00	.04	4928.55	.267	.00
4.80	.04	4928.56	.270	.00

5.60 .05 4928.56 .272 .00
 6.40 .00 4928.56 .275 .00
 PEAK DISCHARGE = .004 CFS - PEAK OCCURS AT HOUR 6.43
 MAXIMUM WATER SURFACE ELEVATION = 4928.565
 MAXIMUM STORAGE = .2746 AC-FT INCREMENTAL TIME=
 .033330HRS

PRINT HYD ID=39 CODE=1

PARTIAL HYDROGRAPH 204.00

RUNOFF VOLUME = .03877 INCHES = .0055 ACRE-FEET
 PEAK DISCHARGE RATE = .00 CFS AT 6.433 HOURS BASIN AREA =
 .0027 SQ. MI.

*

*S POND 5

*

ROUTE RESERVOIR ID=40 HYD NO=205.00 INFLOW ID=30 CODE=24
 OUTFLOW(CFS) STORAGE(AC-FT) ELEVATION(FT)
 0.0000 0.0000 4924.20
 0.0216 0.0003 4926.37
 0.0228 0.0260 4926.62
 0.0240 0.1029 4926.87
 0.0251 0.2311 4927.12
 0.0262 0.4106 4927.37

* * * * *

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4924.20	.000	.00
.80	.00	4924.20	.000	.00
1.60	7.36	4927.04	.190	.02
2.40	.44	4927.31	.365	.03
3.20	.09	4927.32	.376	.03
4.00	.06	4927.33	.378	.03
4.80	.06	4927.33	.381	.03
5.60	.07	4927.33	.383	.03
6.40	.01	4927.33	.385	.03
7.20	.00	4927.33	.383	.03
8.00	.00	4927.33	.381	.03
8.80	.00	4927.33	.380	.03
9.60	.00	4927.32	.378	.03
10.40	.00	4927.32	.376	.03
11.20	.00	4927.32	.375	.03
12.00	.00	4927.32	.373	.03
12.80	.00	4927.31	.371	.03
13.60	.00	4927.31	.369	.03
14.40	.00	4927.31	.368	.03
15.20	.00	4927.31	.366	.03
16.00	.00	4927.31	.364	.03

16.80	.00	4927.30	.363	.03
17.60	.00	4927.30	.361	.03
18.40	.00	4927.30	.359	.03
19.20	.00	4927.30	.357	.03

PEAK DISCHARGE = .026 CFS - PEAK OCCURS AT HOUR 6.17

MAXIMUM WATER SURFACE ELEVATION = 4927.334

MAXIMUM STORAGE = .3851 AC-FT INCREMENTAL TIME=.033330HRS

PRINT HYD ID=40 CODE=1

PARTIAL HYDROGRAPH 205.00

RUNOFF VOLUME = .19043 INCHES = .0402 ACRE-FEET

PEAK DISCHARGE RATE = .03 CFS AT 6.166 HOURS BASIN AREA = .0040 SQ. MI.

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*S POND 6

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ROUTE RESERVOIR	ID=41	HYD NO=206.00	INFLOW ID=6	CODE=24
	OUTFLOW(CFS)		STORAGE(AC-FT)	ELEVATION(FT)
	0.0000		0.0000	4922.22
	0.5050		0.0005	4925.67
	0.5237		0.0156	4925.92
	0.5418		0.0606	4926.17
	0.5592		0.1355	4926.42
	0.5762		0.2404	4926.67

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TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
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.00	.00	4922.22	.000	.00
.80	.00	4922.22	.000	.00
1.60	5.68	4926.41	.131	.56
2.40	.35	4926.65	.231	.57
3.20	.07	4926.58	.203	.57
4.00	.05	4926.50	.169	.56
4.80	.05	4926.42	.135	.56
5.60	.05	4926.31	.102	.55
6.40	.00	4926.20	.068	.54
7.20	.00	4926.02	.033	.53

PEAK DISCHARGE = .575 CFS - PEAK OCCURS AT HOUR 2.27

MAXIMUM WATER SURFACE ELEVATION = 4926.651

MAXIMUM STORAGE = .2325 AC-FT INCREMENTAL TIME=.033330HRS

PRINT HYD ID=41 CODE=1

PARTIAL HYDROGRAPH 206.00

RUNOFF VOLUME = 1.91409 INCHES = .3083 ACRE-FEET
 PEAK DISCHARGE RATE = .57 CFS AT 2.266 HOURS BASIN AREA =
 .0030 SQ. MI.

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*S POND 7

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ROUTE RESERVOIR ID=42 HYD NO=207.00 INFLOW ID=31 CODE=24
 OUTFLOW(CFS) STORAGE(AC-FT) ELEVATION(FT)
 0.0000 0.0000 4923.00
 0.1156 0.0432 4923.60
 0.1718 0.0909 4924.20
 0.2137 0.1476 4924.80
 0.2487 0.2132 4925.40
 0.2793 0.2879 4926.00

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TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4923.00	.000	.00
.80	.00	4923.00	.000	.00
1.60	6.22	4924.86	.154	.22
2.40	.36	4925.95	.282	.28
3.20	.07	4925.89	.274	.27
4.00	.05	4925.77	.260	.27
4.80	.05	4925.66	.245	.26
5.60	.05	4925.55	.231	.26
6.40	.00	4925.43	.217	.25
7.20	.00	4925.29	.201	.24
8.00	.00	4925.15	.185	.23
8.80	.00	4925.01	.170	.23
9.60	.00	4924.87	.155	.22
10.40	.00	4924.73	.141	.21
11.20	.00	4924.59	.128	.20
12.00	.00	4924.46	.115	.19
12.80	.00	4924.33	.103	.18
13.60	.00	4924.20	.091	.17
14.40	.00	4924.07	.080	.16
15.20	.00	4923.94	.070	.15
16.00	.00	4923.82	.061	.14
16.80	.00	4923.71	.052	.13
17.60	.00	4923.61	.044	.12
18.40	.00	4923.51	.037	.10
19.20	.00	4923.43	.031	.08

PEAK DISCHARGE = .277 CFS - PEAK OCCURS AT HOUR 2.50

MAXIMUM WATER SURFACE ELEVATION = 4925.954

MAXIMUM STORAGE = .2821 AC-FT INCREMENTAL TIME=

.033330HRS

PRINT HYD

ID=42 CODE=1

PARTIAL HYDROGRAPH 207.00

RUNOFF VOLUME = 1.58074 INCHES = .2993 ACRE-FEET
PEAK DISCHARGE RATE = .28 CFS AT 2.500 HOURS BASIN AREA =
.0036 SQ. MI.

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*S POND 8

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ROUTE RESERVOIR ID=43 HYD NO=208.00 INFLOW ID=8 CODE=24

OUTFLOW (CFS)	STORAGE (AC-FT)	ELEVATION (FT)
0.0000	0.0000	4922.28
0.0030	0.0005	4925.67
0.0031	0.0064	4925.92
0.0032	0.0238	4926.17
0.0033	0.0529	4926.42
0.0034	0.0936	4926.67

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TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4922.28	.000	.00
.80	.00	4922.28	.000	.00
1.60	1.60	4926.31	.040	.00
2.40	.09	4926.56	.076	.00
3.20	.02	4926.58	.079	.00
4.00	.01	4926.58	.079	.00
4.80	.01	4926.58	.080	.00
5.60	.01	4926.59	.080	.00

PEAK DISCHARGE = .003 CFS - PEAK OCCURS AT HOUR 6.23

MAXIMUM WATER SURFACE ELEVATION = 4926.592

MAXIMUM STORAGE = .0808 AC-FT INCREMENTAL TIME=
.033330HRS

PRINT HYD

ID=43 CODE=1

PARTIAL HYDROGRAPH 208.00

RUNOFF VOLUME = .10381 INCHES = .0052 ACRE-FEET
PEAK DISCHARGE RATE = .00 CFS AT 6.233 HOURS BASIN AREA =
.0009 SQ. MI.

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*S POND 9

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ROUTE RESERVOIR ID=44 HYD NO=209.00 INFLOW ID=32 CODE=24
 OUTFLOW (CFS) STORAGE (AC-FT) ELEVATION (FT)
 0.0000 0.0000 4921.52
 0.0041 0.0377 4921.93
 0.0070 0.1161 4922.68
 0.0090 0.2135 4923.43
 0.0107 0.3300 4924.18
 0.0121 0.4656 4924.93

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TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4921.52	.000	.00
.80	.00	4921.52	.000	.00
1.60	6.35	4923.03	.162	.01
2.40	.38	4924.06	.312	.01
3.20	.07	4924.13	.322	.01
4.00	.05	4924.15	.325	.01
4.80	.05	4924.17	.328	.01
5.60	.06	4924.18	.331	.01
6.40	.01	4924.20	.333	.01
7.20	.00	4924.19	.332	.01
8.00	.00	4924.19	.331	.01
8.80	.00	4924.18	.331	.01
9.60	.00	4924.18	.330	.01
10.40	.00	4924.18	.329	.01
11.20	.00	4924.17	.329	.01
12.00	.00	4924.17	.328	.01
12.80	.00	4924.16	.327	.01
13.60	.00	4924.16	.326	.01
14.40	.00	4924.15	.326	.01
15.20	.00	4924.15	.325	.01
16.00	.00	4924.14	.324	.01
16.80	.00	4924.14	.324	.01
17.60	.00	4924.13	.323	.01
18.40	.00	4924.13	.322	.01
19.20	.00	4924.13	.322	.01

PEAK DISCHARGE = .011 CFS - PEAK OCCURS AT HOUR 6.27

MAXIMUM WATER SURFACE ELEVATION = 4924.196

MAXIMUM STORAGE = .3328 AC-FT INCREMENTAL TIME =
 .033330HRS

PRINT HYD ID=44 CODE=1

PARTIAL HYDROGRAPH 209.00

RUNOFF VOLUME = .08601 INCHES = .0162 ACRE-Feet

PEAK DISCHARGE RATE = .01 CFS AT 6.266 HOURS BASIN AREA =
 .0035 SQ. MI.

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*S POND 10

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ROUTE RESERVOIR ID=45 HYD NO=210.00 INFLOW ID=10 CODE=24

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
0.0000	0.0000	4925.14
0.2628	0.0006	4929.14
0.2683	0.0016	4929.31
0.2738	0.0047	4929.48
0.2792	0.0097	4929.64
0.2844	0.0167	4929.81

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TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4925.14	.000	.00
.80	.00	4925.14	.000	.00
1.60	.70	4929.67	.011	.28
2.40	.03	4929.59	.008	.28
3.20	.01	4925.25	.000	.01
4.00	.01	4925.22	.000	.01
4.80	.01	4925.22	.000	.01
5.60	.01	4925.23	.000	.01

PEAK DISCHARGE = .283 CFS - PEAK OCCURS AT HOUR 1.90
MAXIMUM WATER SURFACE ELEVATION = 4929.749
MAXIMUM STORAGE = .0142 AC-FT INCREMENTAL TIME=
.033330HRS

PRINT HYD

ID=45 CODE=1

PARTIAL HYDROGRAPH 210.00

RUNOFF VOLUME = 1.67920 INCHES = .0358 ACRE-FeET
PEAK DISCHARGE RATE = .28 CFS AT 1.900 HOURS BASIN AREA =
.0004 SQ. MI.

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*S POND 11

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ROUTE RESERVOIR ID=46 HYD NO=211.00 INFLOW ID=11 CODE=24

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
0.0000	0.0000	4925.62
0.2079	0.0006	4929.62
0.2120	0.0015	4929.78
0.2160	0.0041	4929.93
0.2199	0.0084	4930.09
0.2237	0.0144	4930.24

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TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
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.00	.00	4925.62	.000	.00
.80	.00	4925.62	.000	.00
1.60	.63	4930.14	.010	.22
2.40	.03	4930.13	.010	.22
3.20	.01	4925.75	.000	.01
4.00	.00	4925.71	.000	.00

PEAK DISCHARGE = .224 CFS - PEAK OCCURS AT HOUR 1.97

MAXIMUM WATER SURFACE ELEVATION = 4930.238

MAXIMUM STORAGE = .0143 AC-FT INCREMENTAL TIME=
.033330HRS

PRINT HYD ID=46 CODE=1

PARTIAL HYDROGRAPH 211.00

RUNOFF VOLUME = 1.67920 INCHES = .0322 ACRE-FEET

PEAK DISCHARGE RATE = .22 CFS AT 1.966 HOURS BASIN AREA =
.0004 SQ. MI.

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*S POND 12

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ROUTE RESERVOIR	ID=47 HYD NO=212.00	INFLOW ID=12	CODE=24
OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)	
0.0000	0.0000	4926.00	
0.2079	0.0006	4930.00	
0.2123	0.0013	4930.17	
0.2166	0.0034	4930.34	
0.2208	0.0069	4930.50	
0.2250	0.0118	4930.67	

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TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
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.00	.00	4926.00	.000	.00
.80	.00	4926.00	.000	.00
1.60	.51	4930.54	.008	.22
2.40	.03	4930.43	.005	.22
3.20	.01	4926.12	.000	.01
4.00	.00	4926.08	.000	.00

PEAK DISCHARGE = .224 CFS - PEAK OCCURS AT HOUR 1.90

MAXIMUM WATER SURFACE ELEVATION = 4930.616

MAXIMUM STORAGE = .0103 AC-FT INCREMENTAL TIME=
.033330HRS

PRINT HYD

ID=47 CODE=1

PARTIAL HYDROGRAPH 212.00

RUNOFF VOLUME = 1.89975 INCHES = .0274 ACRE-FEET
PEAK DISCHARGE RATE = .22 CFS AT 1.900 HOURS BASIN AREA =
.0003 SQ. MI.

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*S POND 13

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ROUTE RESERVOIR ID=48 HYD NO=213.00 INFLOW ID=13 CODE=24
OUTFLOW(CFS) STORAGE(AC-FT) ELEVATION(FT)
0.0000 0.0000 4924.75
0.2079 0.0006 4928.75
0.2144 0.0223 4929.00
0.2208 0.0871 4929.25
0.2269 0.1952 4929.50
0.2329 0.3466 4929.75

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TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4924.75	.000	.00
.80	.00	4924.75	.000	.00
1.60	7.16	4929.46	.178	.23
2.40	.44	4929.73	.334	.23
3.20	.09	4929.73	.332	.23
4.00	.06	4929.71	.321	.23
4.80	.06	4929.69	.309	.23
5.60	.07	4929.67	.298	.23
6.40	.01	4929.65	.286	.23
7.20	.00	4929.63	.271	.23
8.00	.00	4929.60	.256	.23
8.80	.00	4929.58	.241	.23
9.60	.00	4929.55	.226	.23
10.40	.00	4929.53	.211	.23
11.20	.00	4929.50	.196	.23
12.00	.00	4929.47	.181	.23
12.80	.00	4929.43	.166	.23
13.60	.00	4929.40	.151	.22
14.40	.00	4929.36	.136	.22
15.20	.00	4929.33	.121	.22
16.00	.00	4929.29	.107	.22
16.80	.00	4929.26	.092	.22
17.60	.00	4929.21	.077	.22
18.40	.00	4929.16	.063	.22
19.20	.00	4929.10	.049	.22

PEAK DISCHARGE = .232 CFS - PEAK OCCURS AT HOUR 2.63
MAXIMUM WATER SURFACE ELEVATION = 4929.733

MAXIMUM STORAGE = .3361 AC-FT INCREMENTAL TIME=
.033330HRS

PRINT HYD ID=48 CODE=1

PARTIAL HYDROGRAPH 213.00

RUNOFF VOLUME = 1.69480 INCHES = .3507 ACRE-FEET
PEAK DISCHARGE RATE = .23 CFS AT 2.633 HOURS BASIN AREA =
.0039 SQ. MI.

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*S POND 14

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ROUTE RESERVOIR ID=49 HYD NO=214.00 INFLOW ID=14 CODE=24
OUTFLOW(CFS) STORAGE(AC-FT) ELEVATION(FT)
0.0000 0.0000 4926.85
0.0028 0.0000 4927.05
0.0040 0.0007 4927.25
0.0050 0.0030 4927.45
0.0058 0.0067 4927.65
0.0065 0.0119 4927.85

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TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4926.85	.000	.00
.80	.00	4926.85	.000	.00
1.60	.20	4927.56	.005	.01
2.40	.01	4927.75	.009	.01
3.20	.00	4927.74	.009	.01
4.00	.00	4927.73	.009	.01
4.80	.00	4927.72	.009	.01
5.60	.00	4927.71	.008	.01
6.40	.00	4927.70	.008	.01
7.20	.00	4927.68	.008	.01
8.00	.00	4927.67	.007	.01
8.80	.00	4927.65	.007	.01
9.60	.00	4927.63	.006	.01
10.40	.00	4927.61	.006	.01
11.20	.00	4927.59	.006	.01
12.00	.00	4927.57	.005	.01
12.80	.00	4927.55	.005	.01
13.60	.00	4927.53	.005	.01
14.40	.00	4927.52	.004	.01
15.20	.00	4927.50	.004	.01
16.00	.00	4927.48	.004	.01
16.80	.00	4927.46	.003	.01
17.60	.00	4927.44	.003	.00

PEAK DISCHARGE = .006 CFS - PEAK OCCURS AT HOUR 2.50

MAXIMUM WATER SURFACE ELEVATION = 4927.748
 MAXIMUM STORAGE = .0093 AC-FT INCREMENTAL TIME=
 .033330HRS

PRINT HYD ID=49 CODE=1

PARTIAL HYDROGRAPH 214.00

RUNOFF VOLUME = 1.60356 INCHES = .0086 ACRE-FEET
 PEAK DISCHARGE RATE = .01 CFS AT 2.500 HOURS BASIN AREA =
 .0001 SQ. MI.

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*S POND 15

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ROUTE RESERVOIR ID=50 HYD NO=215.00 INFLOW ID=33 CODE=24

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
0.0000	0.0000	4926.75
0.2766	0.0362	4927.35
0.4271	0.0723	4927.95
0.5370	0.1085	4928.55
0.6279	0.1446	4929.15
0.7073	0.1808	4929.75

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TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4926.75	.000	.00
.80	.00	4926.75	.000	.00
1.60	4.55	4928.58	.110	.54
2.40	.28	4929.66	.176	.70
3.20	.05	4929.07	.140	.62
4.00	.04	4928.50	.105	.53
4.80	.04	4928.01	.076	.44
5.60	.04	4927.62	.053	.34
6.40	.00	4927.32	.034	.26
7.20	.00	4927.10	.021	.16
8.00	.00	4926.96	.013	.10
8.80	.00	4926.88	.008	.06
9.60	.00	4926.83	.005	.03
10.40	.00	4926.80	.003	.02
11.20	.00	4926.78	.002	.01
12.00	.00	4926.77	.001	.01
12.80	.00	4926.76	.001	.00

PEAK DISCHARGE = .707 CFS - PEAK OCCURS AT HOUR 2.17
 MAXIMUM WATER SURFACE ELEVATION = 4929.750
 MAXIMUM STORAGE = .1808 AC-FT INCREMENTAL TIME=
 .033330HRS

PRINT HYD ID=50 CODE=1

PARTIAL HYDROGRAPH 215.00

RUNOFF VOLUME = 1.88549 INCHES = .2454 ACRE-FeET
 PEAK DISCHARGE RATE = .71 CFS AT 2.166 HOURS BASIN AREA =
 .0024 SQ. MI.

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*S POND 16

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ROUTE RESERVOIR	ID=51 HYD NO=216.00 INFLOW ID=16 CODE=24
OUTFLOW(CFS)	STORAGE(AC-FT) ELEVATION(FT)
0.0000	0.0000 4925.51
0.0033	0.0006 4929.51
0.0034	0.0127 4929.76
0.0035	0.0487 4930.01
0.0036	0.1087 4930.26
0.0037	0.1927 4930.51

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TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4925.51	.000	.00
.80	.00	4925.51	.000	.00
1.60	1.90	4930.01	.050	.00
2.40	.12	4930.21	.096	.00
3.20	.02	4930.22	.099	.00
4.00	.02	4930.22	.100	.00
4.80	.02	4930.23	.101	.00
5.60	.02	4930.23	.102	.00

PEAK DISCHARGE = .004 CFS - PEAK OCCURS AT HOUR 6.27
 MAXIMUM WATER SURFACE ELEVATION = 4930.233
 MAXIMUM STORAGE = .1022 AC-FT INCREMENTAL TIME=
 .033330HRS

PRINT HYD ID=51 CODE=1

PARTIAL HYDROGRAPH 216.00

RUNOFF VOLUME = .10513 INCHES = .0056 ACRE-FeET
 PEAK DISCHARGE RATE = .00 CFS AT 6.266 HOURS BASIN AREA =
 .0010 SQ. MI.

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*S POND 17

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ROUTE RESERVOIR	ID=52 HYD NO=217.00 INFLOW ID=17 CODE=24
OUTFLOW(CFS)	STORAGE(AC-FT) ELEVATION(FT)

0.0000	0.0000	4926.85
0.0120	0.0000	4927.10
0.0178	0.0016	4927.35
0.0221	0.0062	4927.60
0.0259	0.0140	4927.85
0.0289	0.0248	4928.10

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TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
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.00	.00	4926.85	.000	.00
.80	.00	4926.85	.000	.00
1.60	.37	4927.69	.009	.02
2.40	.02	4927.90	.016	.03
3.20	.00	4927.87	.015	.03
4.00	.00	4927.84	.014	.03
4.80	.00	4927.79	.012	.02
5.60	.00	4927.74	.011	.02
6.40	.00	4927.70	.009	.02
7.20	.00	4927.65	.008	.02
8.00	.00	4927.60	.006	.02
8.80	.00	4927.52	.005	.02
9.60	.00	4927.45	.003	.02
10.40	.00	4927.38	.002	.02
11.20	.00	4927.27	.001	.02
12.00	.00	4927.12	.000	.01

PEAK DISCHARGE = .027 CFS - PEAK OCCURS AT HOUR 2.30

MAXIMUM WATER SURFACE ELEVATION = 4927.903

MAXIMUM STORAGE = .0163 AC-FT INCREMENTAL TIME = .033330HRS

PRINT HYD

ID=52 CODE=1

PARTIAL HYDROGRAPH 217.00

RUNOFF VOLUME = 1.96553 INCHES = .0199 ACRE-FEET

PEAK DISCHARGE RATE = .03 CFS AT 2.300 HOURS BASIN AREA = .0002 SQ. MI.

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*S POND 18

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ROUTE RESERVOIR

ID=53 HYD NO=218.00 INFLOW ID=18 CODE=24

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
0.00000	0.0000	4925.30
0.00328	0.0006	4929.30
0.00336	0.0025	4929.51
0.00345	0.0080	4929.72
0.00353	0.0172	4929.93
0.00361	0.0301	4930.14

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TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4925.30	.000	.00
.80	.00	4925.30	.000	.00
1.60	.50	4929.82	.012	.00
2.40	.02	4930.02	.023	.00
3.20	.00	4930.03	.023	.00

PEAK DISCHARGE = .004 CFS - PEAK OCCURS AT HOUR 3.73

MAXIMUM WATER SURFACE ELEVATION = 4930.031

MAXIMUM STORAGE = .0234 AC-FT INCREMENTAL TIME = .033330HRS

PRINT HYD

ID=53 CODE=1

PARTIAL HYDROGRAPH 218.00

RUNOFF VOLUME = .34349 INCHES = .0055 ACRE-FEET

PEAK DISCHARGE RATE = .00 CFS AT 3.733 HOURS BASIN AREA = .0003 SQ. MI.

*

*S POND 19

*

ROUTE RESERVOIR	ID=54 HYD NO=219.00	INFLOW ID=35	CODE=24
	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEVATION(FT)
	0.0000	0.0000	4923.00
	0.7167	0.0450	4924.40
	1.0569	0.1194	4925.80
	1.3117	0.2529	4927.20
	1.5245	0.4453	4928.60
	1.7110	0.6968	4930.00

* * * * *

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	4923.00	.000	.00
.80	.00	4923.00	.000	.00
1.60	16.62	4928.28	.401	1.48
2.40	1.01	4929.96	.689	1.71
3.20	.20	4929.50	.608	1.64
4.00	.13	4928.97	.512	1.57
4.80	.13	4928.41	.419	1.50
5.60	.15	4927.78	.332	1.40
6.40	.01	4927.18	.251	1.31
7.20	.00	4926.33	.170	1.15
8.00	.00	4925.41	.099	.96
8.80	.00	4924.36	.044	.70

9.60	.00	4923.47	.015	.24
10.40	.00	4923.17	.005	.08
11.20	.00	4923.06	.002	.03
12.00	.00	4923.02	.001	.01
12.80	.00	4923.01	.000	.00

PEAK DISCHARGE = 1.709 CFS - PEAK OCCURS AT HOUR 2.23
 MAXIMUM WATER SURFACE ELEVATION = 4929.984
 MAXIMUM STORAGE = .6940 AC-FT INCREMENTAL TIME=
 .033330HRS

PRINT HYD ID=54 CODE=1

PARTIAL HYDROGRAPH 219.00

RUNOFF VOLUME = 1.84178 INCHES = .8909 ACRE-FEET
 PEAK DISCHARGE RATE = 1.71 CFS AT 2.233 HOURS BASIN AREA =
 .0091 SQ. MI.

*
 *ADD PONDS 1 THRU 19
 *

ADD HYD	ID=55	HYD NO=301.00	ID=36	ID=37
ADD HYD	ID=56	HYD NO=302.00	ID=55	ID=38
ADD HYD	ID=57	HYD NO=303.00	ID=56	ID=39
ADD HYD	ID=58	HYD NO=304.00	ID=57	ID=40
ADD HYD	ID=59	HYD NO=305.00	ID=58	ID=41
ADD HYD	ID=60	HYD NO=306.00	ID=42	ID=43
ADD HYD	ID=61	HYD NO=307.00	ID=60	ID=44
ADD HYD	ID=62	HYD NO=308.00	ID=59	ID=61
ADD HYD	ID=63	HYD NO=309.00	ID=62	ID=45
ADD HYD	ID=64	HYD NO=310.00	ID=63	ID=46
ADD HYD	ID=65	HYD NO=311.00	ID=64	ID=47
ADD HYD	ID=66	HYD NO=312.00	ID=54	ID=48
ADD HYD	ID=67	HYD NO=313.00	ID=66	ID=49
ADD HYD	ID=68	HYD NO=314.00	ID=67	ID=50
ADD HYD	ID=69	HYD NO=315.00	ID=68	ID=51
ADD HYD	ID=70	HYD NO=316.00	ID=69	ID=52
ADD HYD	ID=71	HYD NO=317.00	ID=70	ID=53
ADD HYD	ID=72	HYD NO=317.00	ID=71	ID=65

PRINT HYD ID=72 CODE=1

HYDROGRAPH FROM AREA 317.00

RUNOFF VOLUME = 1.11501 INCHES = 2.5803 ACRE-FEET
 PEAK DISCHARGE RATE = 4.95 CFS AT 2.200 HOURS BASIN AREA =
 .0434 SQ. MI.

*
 FINISH

NORMAL PROGRAM FINISH

END TIME (HR:MIN:SEC) = 16:22:03

Map Pocket

Grading and Drainage Plan

File

Walmart / Rio Bravo

P-16/D004A

**FEASIBILITY DESIGN
FOR
REPLACEMENT CULVERTS
ARENAL MAIN CANAL/RIO BRAVO BOULEVARD
CROSSING AT ISLETA DRAIN**

Prepared For:



Albuquerque Metropolitan Arroyo
Flood Control Authority
2600 Prospect, NE
Albuquerque, NM 87107

Prepared By:



5501 Jefferson Blvd., NE, Suite 200 Albuquerque, NM 87109
Phone: (505) 243-7300 Fax: (505) 243-7400 E-mail: rti@nm.net

February 2004

INTRODUCTION

This report describes a feasibility design for the proposed replacement culverts which pass under the Arenal Main Canal and Rio Bravo Boulevard (linking drain segments Isleta 15 to Isleta 16) initiated by the Walmart proposal to cover approximately 300 feet of the Isleta Drain downstream (south) of Rio Bravo. See Figure 1. This proposal has significantly altered the recommended improvements for this location in the Southwest Valley Feasibility Study, which were two 6'x10' box culverts approximately 400 feet in length.

HYDRAULIC DESIGN

The recommended improvement to pass the design flow of 560 cfs was based upon the results of K-ROUTE modeling. A number of iterations were performed to determine the water surface elevations within the Isleta Drain and the optimum culverts to pass the required flow without overtopping the drain. The K-ROUTE model input includes a culvert outflow rating curve derived from the New Mexico State Highway and Transportation Department (NMSHTD) nomographs contained within "Drainage Manual-Volume II, Hydraulics, Sedimentation and Erosion." Initial iterations showed that the 6' high culvert outlet would be submerged. Therefore, Chart 15, page A-21 of Volume II, for concrete box culverts flowing full along with a submerged outlet was selected. Using 1-foot of differential head, based upon previous assumptions from the Southwest Valley study, Chart 15 indicated that a minimum of two 6'x10' box culverts would be required, and they will discharge 320 cfs per box, or a total of 640 cfs. See Figure 2.

The Walmart proposal of covering approximately 300 additional feet of the Isleta Drain will extend the required length of the culverts by this same amount. By extending the length of the culverts, the head losses are increased and the recommended improvement of two 6'x10' box culverts is no longer adequate to pass the design flow of 560 cfs.

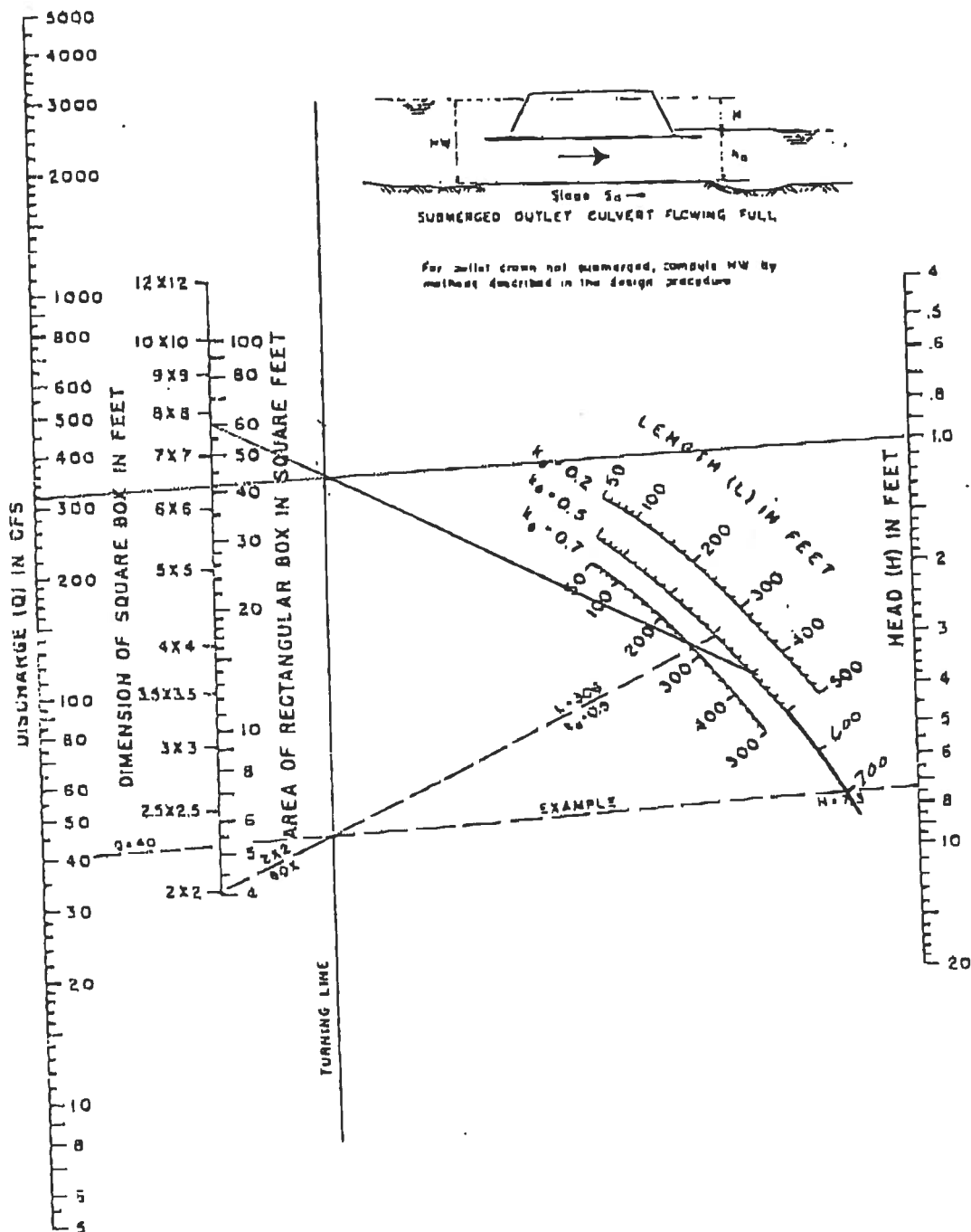
An initial review indicated that increasing the size of the culverts would prove to be very complex and cost prohibitive; therefore, an alternative design was investigated. It was determined that lowering the outlet and thereby increasing the differential head would reduce the size of the culverts. Although this would increase the amount of earthwork needed, a cost savings will be realized by reducing the required amount of concrete.

The Walmart site will replace the existing farm land with their buildings and parking facilities. This will eliminate the need for the lateral crossing that is currently serving this farming operation. Therefore, this portion of the Isleta Drain can be lowered from 4920 feet to 4916 feet, the existing drain bottom elevation downstream of the lateral crossing. This will increase the available differential head to 4 feet. Using 4 feet of differential head, Chart 15 indicated that two 6'x 6' box culverts would be sufficient, and they will discharge 300 cfs each, or a total of 600 cfs. See Figure 3.

COST ESTIMATE

The City of Albuquerque 1998 unit costs were used to determine the total projected cost of the improvements. The amount of concrete required by the box culverts was determined from NMSHID Serial CB-32. See Table 1 for the item numbers and associated cost. Please note that the unit costs are 6 years old now and should be updated as necessary.

CHART 15



HEAD FOR
CONCRETE BOX CULVERTS
FLOWING FULL

$n = 0.012$

FIGURE 2

MO OF PUBLIC ROADS, JAN 1963

**AMAFCA**

2600 Prospect Av. NE
Albuquerque, NM 87107
Ph: (505) 884-2215
Fax: (505) 884-0214

FA

Post-it® Fax Note 7671		Date 3-9	# of pages 9
To BRAD BINGHAM		From LYNN MAZUR	
Co./Dept. HYDROLOGY		Co. AMAFCA	
Phone #		Phone #	
Fax #		Fax #	

To: Jon Niski**Of:** Tierra West, LLC**Fax #:** 858-1118**Pages:** 9, incl. cover sheet**From:** Lynn Mazur, P.E.
Development Review Engineer**Date:** March 8, 2004**Subject:** Wal-Mart @ Rio Bravo/Coors**COMMENTS:**

Here is the report we had RTI prepare for the Rio Bravo crossing of Isleta Drain. You were copied on a letter from MRGCD that stated that they will not approve a double box culvert. Therefore, you need to put a single 12' x 6' CBC on the Infrastructure List. You may come up with an alternate design for final, but we will need to meet with MRGCD to coordinate.



March 8, 2004

Mr. Flvidio Diniz
Resource Technology, Inc.
5501 Jefferson Blvd. NE, Suite 200
Albuquerque, NM 87109

REF.: RIO BRAVO ROAD CULVERT REPLACEMENT ACROSS THE ISLETA
DRAIN RIGHT-OF-WAY

Dear Mr. Diniz:

The District has reviewed your feasibility design for the above referenced. The District recommends the existing road culvert pipe be replaced with a single barrel concrete box culvert or a trapezoidal concrete box culvert.

If you have any questions please feel free to contact Mr. Ray Gomez for more information at (505) 247-0234.

Sincerely,

Subhas K. Shah
Chief Executive Officer

cc: Leonard Utter, Assistant Engineer
Ray Gomez, Engineer I
Lynn Mazur, AMAFCA
Jonathan Niski, Tierra West, LLC
File

P.O. Box 581

87103-0581

1931 Second St. SW

Albuquerque, NM

87102-4515

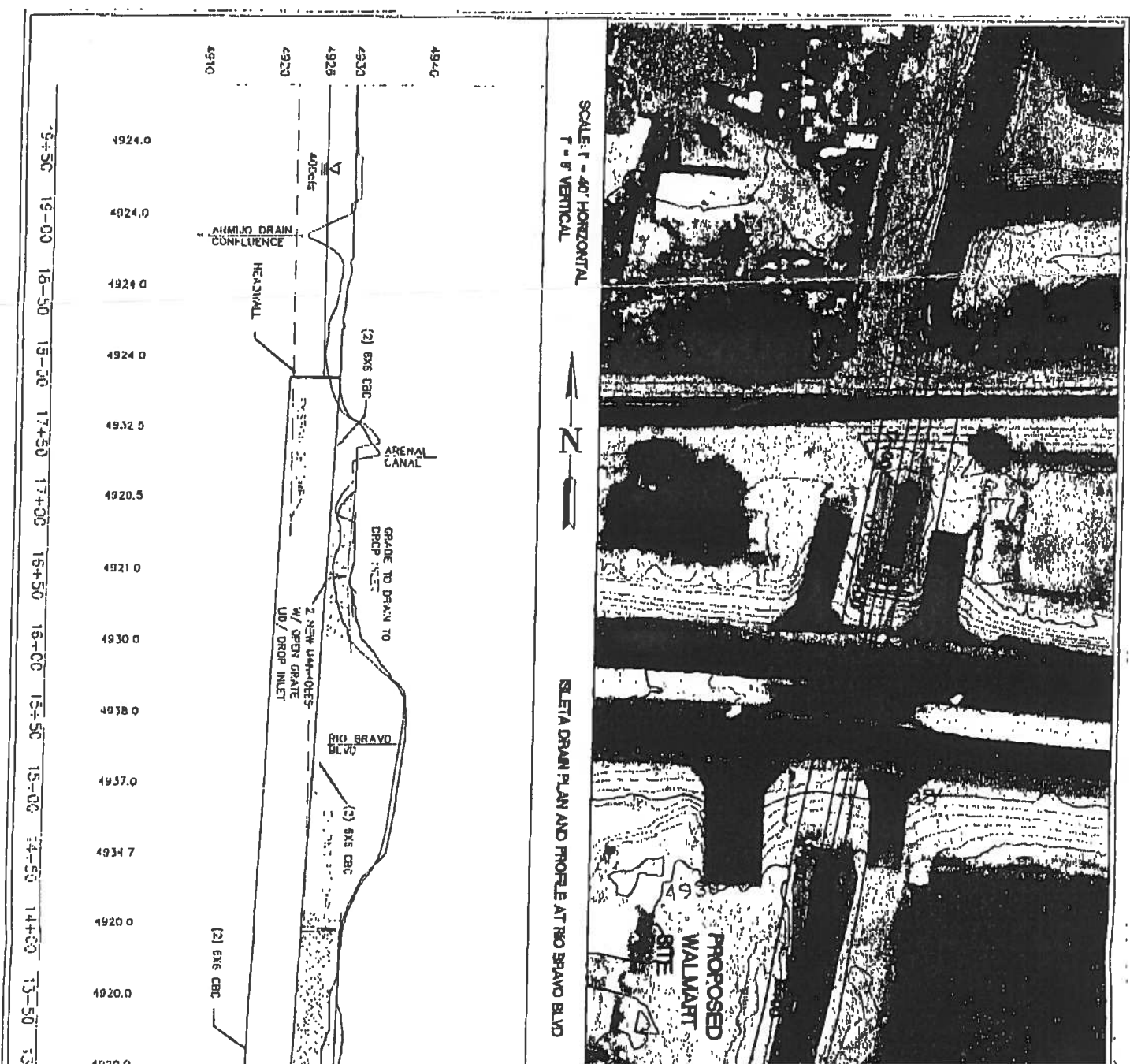
505-247-0234

Fax // 505-243-7308

*Drain needs to be dredged 2' to Lakeview.
1-12' x 6' C.B.C. - or - equivalent*

*** DOC. MEMORY LIST ***

TX/RX NO	MODE	CONNECTION TEL/ID	PGS.	SET TIME	ST. TIME	SENDER NAME
8750	MEMORY RX		3	03/09 08:37	-----	



Current DRC
Project Number: _____

FIGURE 12
INFRASTRUCTURE LIST

Date Submitted: _____
Date Site Plan Approved: _____
Date Preliminary Plat Approved: _____
Date Preliminary Plat Expires: _____
DRB Project No.: _____

EXHIBIT "A"
TO SUBDIVISION IMPROVEMENTS AGREEMENT
DEVELOPMENT REVIEW BOARD (D.R.B.) REQUIRED INFRASTRUCTURE LIST

Wal-Mart #430-00 (Coors Blvd. & Rio Bravo Blvd.)
PROPOSED NAME OF PLAT AND/OR SITE DEVELOPMENT PLAN

Tract 1-A-1, Lamonica and Wenk

EXISTING LEGAL DESCRIPTION PRIOR TO PLATTING ACTION

HYDROLOGY SECTION

Following is a summary of PUBLIC/PRIVATE infrastructure required to be constructed or financially guaranteed for the above development. This Listing is not necessarily a complete listing. During the SIA process and/or in the review of the construction drawings, if the DRC Chair determines that appurtenant items and/or unforeseen items have not been included in the infrastructure listing, the DRC Chair may include those items in the listing and related financial guarantee. Likewise, if the DRC Chair determines that appurtenant or non-essential items can be deleted from the listing, those items may be deleted as well as the related portions of the financial guarantees. All such revisions require approval by the DRC Chair, the User Department and agent/owner. If such approvals are obtained, these revisions to the listing will be incorporated administratively. In addition, any unforeseen items which arise during construction which are necessary to complete the project and which normally are the Subdivider's responsibility will be required as a condition of project acceptance and close out by the City.

SIA Sequence #	COA DRC Project #	Size	Type of Improvement	Location	From	To	Private Inspector	City Inspector	City Cnst Engineer
		48' F-F	Arterial Paving Curb and Gutter 6' Sidewalk (North Side)	Lamonica Road	Coors Blvd.	Loris Drive	/	/	/
		48' F-F	Arterial Paving Curb and Gutter 6' Sidewalk (West Side)	Loris Drive	Lamonica Road	Rio Bravo Blvd.	/	/	/
		12'	Right Turn Lane Curb and Gutter	Rio Bravo Blvd. and Loris Dr. Intersection	Eastbound Rio Bravo Blvd.	Loris Drive	/	/	/
		12'	Dual Left Turn Lanes* Curb and Gutter	Rio Bravo Blvd. and Loris Dr. Intersection	Westbound Rio Bravo Blvd.	Loris Drive	/	/	/
		12'	Acceleration Lane Curb and Gutter	Rio Bravo Blvd	Loris Drive	680' East of Loris Dr.	/	/	/
			Median Improvements for Intersection	Rio Bravo Blvd. and Loris Dr. Intersection	200' West of Loris Dr.	200' East of Loris Dr.	/	/	/
		12'	Right Turn Lane Curb and Gutter	Coors Blvd. and Lamonica Road	Northbound Coors Blvd.	Lamonica Road	/	/	/
		12'	Dual Left Turn Lanes* Curb and Gutter	Coors Blvd. and Lamonica Road	Southbound Coors Blvd.	Lamonica Road	/	/	/
		12'	Right Turn Lane Curb and Gutter	Coors Blvd.	Lamonica Road	Private Entrance	/	/	/
		12'	Right/Thru Lane Curb and Gutter	Rio Bravo Blvd. and Coors Blvd. Intersection	Eastbound Rio Bravo Blvd.	Coors Blvd	/	/	/
		12'	Reshape Additional Left Turn Lane	Rio Bravo Blvd. and Coors Blvd. Intersection	Westbound Rio Bravo Blvd.	Coors Blvd	/	/	/

☐	☐	12"	Restripe Additional Left Turn Lane	Rio Bravo Blvd. and Coors Blvd. Intersection	Southbound Coors Blvd.	Rio Bravo Blvd.	/	/	/
☐	☐		Bus Bay w/ Shelter	Coors Blvd.			/	/	/
☐	☐		Traffic Signal	Lamonica Road and Coors Blvd. Intersection			/	/	/
☐	☐		Traffic Signal	Loris Drive and Rio Bravo Blvd. Intersection			/	/	/
☐	☐	6"	Sidewalk	Rio Bravo Blvd.	Coors Blvd.	Loris Drive	/	/	/
☐	☐	6"	Sidewalk	Coors Blvd.	Rio Bravo Blvd.	Lamonica Road	/	/	/
☐	☐	8"	SAS Gravity Line	Lamonica Road	Coors Blvd.	800' West of Coors	/	/	/
☐	☐	10"	Water PVC Line	Lamonica Road	Coors Blvd.	Loris Drive	/	/	/
☐	☐	10"	Water PVC Line	Loris Drive	Lamonica Road	350' North of Lamonica	/	/	/
☐	☐	2	Sidewalk Culverts	Loris Drive			/	/	/
☐	☐	24"	RCP Storm Sewer	Lamonica Road			/	/	/
☐	☐	8"	PVC Storm Sewer	Loris Drive	Loris Drive	Isiela Drain	/	/	/
☐	☐		Drainage Crossing Structure	Rio Bravo Blvd. and Isiela Drain	North side of Rio Bravo Blvd	South side of Rio Bravo Blvd.	/	/	/
☐	☐		Water Infrastructure to include Valves, Fittings, Valve Boxes, and Fire Hydrants as required.				/	/	/
☐	☐		Sanitary Sewer to include Manholes, and Service Connections as required.				/	/	/
☐	☐		*One Left Turn Lane will be blocked out with striping until needed.				/	/	/
☐	☐		Catch Basins and RCP connections included with Storm Sewer				/	/	/
☐	☐		Residential Street Lights per DPM				/	/	/
☐	☐		Certified Grading and Drainage with Private Walls and Private Drainage (Non- work order item) Required for S/A/Financial Guarantee Release.				/	/	/

NOTES

1 _____

2 _____

3 _____

AGENT / OWNER

DEVELOPMENT REVIEW BOARD MEMBER APPROVALS

NAME (print)

DRB CHAIR - date

PARKS & GENERAL SERVICES - date

FIRM

TRANSPORTATION DEVELOPMENT - date

AMAFCA - date

SIGNATURE - date

UTILITY DEVELOPMENT - date

_____ - date

MAXIMUM TIME ALLOWED TO CONSTRUCT
THE IMPROVEMENTS WITHOUT A DRB
EXTENSION: _____

CITY ENGINEER - date

_____ - date

DESIGN REVIEW COMMITTEE REVISIONS

REVISION	DATE	DRB CHAIR	USER DEPARTMENT	AGENT / OWNER