CITY OF ALBUQUERQUE

Planning Department Alan Varela, Director



Mayor Timothy M. Keller

August 18, 2022

Diego A. Gomez, P.E. Greenbox Architecture 502 Seventh Street, Suite 203 Oregon City, OR 97045

RE: Kairos Power Expansion 5201 Hawking Drive SE Grading Plans and Drainage Calculations Engineer's Stamp Date: 07/20/22 Hydrology File: Q16DA5000A

Dear Mr. Gomez:

PO Box 1293 Based upon the information provided in your submittal received 07/26/2022, the Grading Plans and Drainage Calculations are approved for Building Permit, Grading Permit, and for action by the DRB on Platting and Site Plan for Building Permit. Please attach a copy of this approved plan in the construction sets for Building Permit processing along with a copy of this letter.

Albuquerque

PRIOR TO CERTIFICATE OF OCCUPANCY:

 NM 87103
Engineer's Certification, per the DPM Part 6-14 (F): Engineer's Certification Checklist For Non-Subdivision is required.

www.cabq.gov

2. Please provide the Drainage Covenant with Exhibit A for the Existing Retention Pond per Article 6-15(C) of the DPM prior to Permanent Release of Occupancy. Please submit the original copies along with the \$25.00 recording fee check made payable to Bernalillo County to Carrie Compton (cacompton@cabq.gov) on the 4th floor of Plaza de Sol. Please note that Hydrology will need a pdf copy of the recorded Drainage Covenant prior to Hydrology's approval of Permanent Release of Occupancy.

As a reminder, if the project total area of disturbance (including the staging area and any work within the adjacent Right-of-Way) is 1 acre or more, then an Erosion and Sediment Control (ESC) Plan and Owner's certified Notice of Intent (NOI) is required to be submitted to the Stormwater Quality Engineer (Doug Hughes, PE, <u>jhughes@cabq.gov</u>, 924-3420) 14 days prior to any earth disturbance.

CITY OF ALBUQUERQUE

Planning Department Alan Varela, Director



Mayor Timothy M. Keller

If you have any questions, please contact me at 924-3995 or <u>rbrissette@cabq.gov</u>.

Sincerely,

Renée C. Brissette

Renée C. Brissette, P.E. CFM Senior Engineer, Hydrology Planning Department

PO Box 1293

Albuquerque

NM 87103

www.cabq.gov

| City of Alb Planning De Development & Buildin DRAINAGE AND TRANSPOR | epartment |
|--|---|
| Project Title: Kairos Power Expansion Building Per | mit #: Hydrology File #: |
| | Work Order#: DEL SOL INNOVATIONPARK II (A SUBDIVISION OF TRACT D MESA DEL |
| Legal Description: <u>SOL INNOVATIONPARK II) CONT 16.4161 AC</u> | · |
| City Address: _5201 Hawking Drive SE, Albuquerque, NM 8 | 7106 |
| Applicant: Greenbox Architecture | Contact: Derek Metson |
| Address: 502 Seventh Street, Suite 203 Oregon City, OR | |
| Phone#: (503) 207-5537 Fax#: | E-mail: permits@greenboxpdx.com |
| Other Contact: <u>KAIROS POWER</u> | Contact: Lara Gutierrez |
| Address: 5201 Hawking Drive SE, Albuquerque, NM 87106 | |
| Phone#: (505)702-1128 Fax#: | E-mail: gutierrez@kairospower.com |
| TYPE OF DEVELOPMENT: PLAT (# of lots) | RESIDENCEX DRB SITEADMIN SITE |
| IS THIS A RESUBMITTAL? Yes X No | |
| DEPARTMENT TRANSPORTATION HYD | ROLOGY/DRAINAGE |
| Check all that Apply: | TYPE OF APPROVAL/ACCEPTANCE SOUGHT: BUILDING PERMIT APPROVAL |
| TYPE OF SUBMITTAL: | CERTIFICATE OF OCCUPANCY |
| ENGINEER/ARCHITECT CERTIFICATION | |
| PAD CERTIFICATION | PRELIMINARY PLAT APPROVAL |
| CONCEPTUAL G & D PLAN X GRADING PLAN | SITE PLAN FOR SUB'D APPROVAL |
| X DRAINAGE REPORT | $\underline{\chi}$ SITE PLAN FOR BLDG. PERMIT APPROVAL |
| DRAINAGE MASTER PLAN | \underline{X} FINAL PLAT APPROVAL |
| FLOODPLAIN DEVELOPMENT PERMIT APPLIC | SIA/ RELEASE OF FINANCIAL GUARANTEE |
| ELEVATION CERTIFICATE | |
| ELEVATION CERTIFICATE | FOUNDATION PERMIT APPROVAL |
| CLOMR/LOMR | FOUNDATION PERMIT APPROVAL GRADING PERMIT APPROVAL |
| CLOMR/LOMR TRAFFIC CIRCULATION LAYOUT (TCL) | |
| CLOMR/LOMR TRAFFIC CIRCULATION LAYOUT (TCL) TRAFFIC IMPACT STUDY (TIS) | X GRADING PERMIT APPROVAL SO-19 APPROVAL X PAVING PERMIT APPROVAL |
| CLOMR/LOMR TRAFFIC CIRCULATION LAYOUT (TCL) TRAFFIC IMPACT STUDY (TIS) STREET LIGHT LAYOUT | X GRADING PERMIT APPROVAL SO-19 APPROVAL X PAVING PERMIT APPROVAL GRADING/ PAD CERTIFICATION |
| CLOMR/LOMR TRAFFIC CIRCULATION LAYOUT (TCL) TRAFFIC IMPACT STUDY (TIS) STREET LIGHT LAYOUT OTHER (SPECIFY) | X GRADING PERMIT APPROVAL SO-19 APPROVAL X PAVING PERMIT APPROVAL GRADING/ PAD CERTIFICATION WORK ORDER APPROVAL |
| CLOMR/LOMR TRAFFIC CIRCULATION LAYOUT (TCL) TRAFFIC IMPACT STUDY (TIS) STREET LIGHT LAYOUT | X GRADING PERMIT APPROVAL SO-19 APPROVAL X PAVING PERMIT APPROVAL GRADING/ PAD CERTIFICATION WORK ORDER APPROVAL CLOMR/LOMR |
| CLOMR/LOMR TRAFFIC CIRCULATION LAYOUT (TCL) TRAFFIC IMPACT STUDY (TIS) STREET LIGHT LAYOUT OTHER (SPECIFY) | X GRADING PERMIT APPROVAL SO-19 APPROVAL X PAVING PERMIT APPROVAL GRADING/ PAD CERTIFICATION WORK ORDER APPROVAL CLOMR/LOMR FLOODPLAIN DEVELOPMENT PERMIT |
| CLOMR/LOMR TRAFFIC CIRCULATION LAYOUT (TCL) TRAFFIC IMPACT STUDY (TIS) STREET LIGHT LAYOUT OTHER (SPECIFY) | X GRADING PERMIT APPROVAL SO-19 APPROVAL X PAVING PERMIT APPROVAL GRADING/ PAD CERTIFICATION WORK ORDER APPROVAL CLOMR/LOMR FLOODPLAIN DEVELOPMENT PERMIT X OTHER (SPECIFY) Site Plan - DRB, Major Amendment |

COA STAFF:

ELECTRONIC SUBMITTAL RECEIVED:

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Exp : 12.31.2023

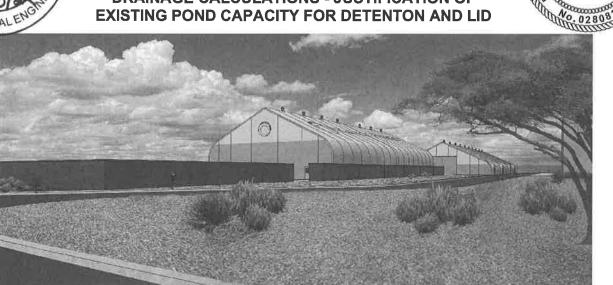
CIVIL

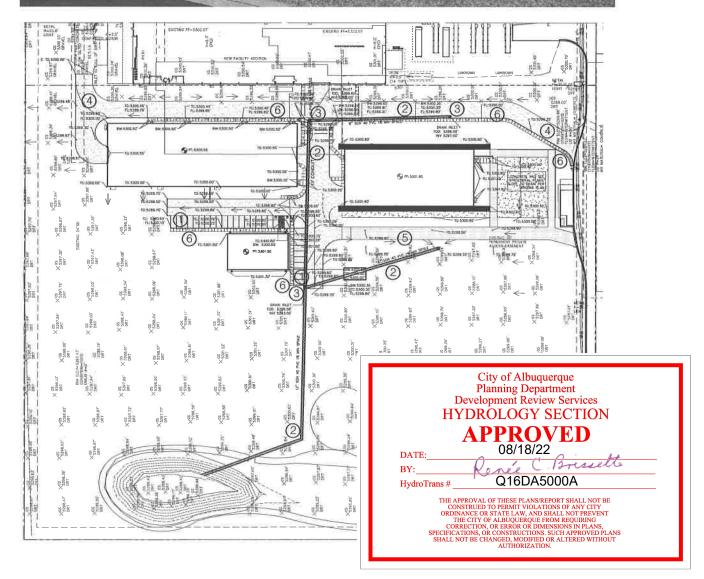
ASHKEVICH

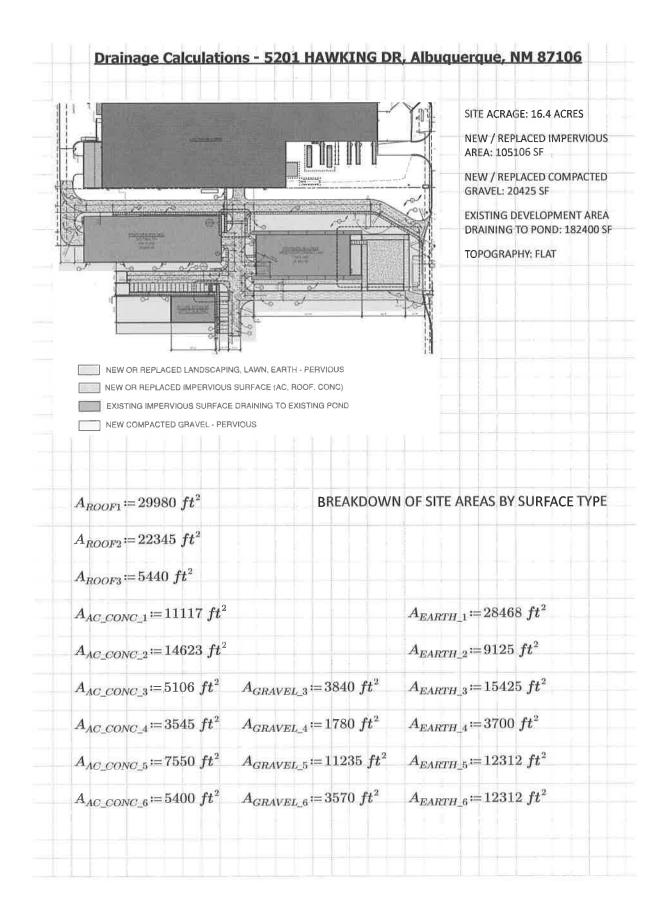


KAIROS POWER FACILITY EXPANSION

DRAINAGE CALCULATIONS - JUSTIFICATION OF EXISTING POND CAPACITY FOR DETENTON AND LID



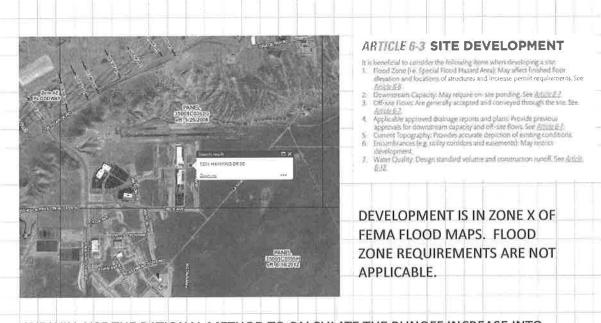




Created with PTC Mathcad Express, See www.mathcad.com for more information.

| $A_{imp_n_r} = 105106 \; ft^2$ | TOTAL NEW/REPLACED DRAINED TO EXISTING I | IMPERVIOUS AREA TO BE POND |
|---|--|---|
| $A_{existing_imp_pond} \!\coloneqq\! 182400 \; ft^2$ | EXISTING IMPERVIOUS EXISTING POND | AREA DRAINWD TO |
| $A_{new_gravel} \coloneqq A_{GRAVEL_3} + A_{GRAVEL}$ | $_4 + A_{GRAVEL_5} + A_{GRAVEL_6}$ | |
| $A_{new_gravel}\!=\!20425\;ft^2$ | TOTAL AREA OF NEW G | RAVEL PARKING / ROAD |
| $A_{n_landscaping} \coloneqq A_{EARTH_1} + A_{EARTH}$ | $A_2 + A_{EARTH_3} + A_{EARTH_4} + A_{EARTH$ | $A_{EARTH_5} + A_{EARTH_6}$ |
| $A_{n_landscaping}\!=\!81342\;ft^2$ | TOTAL AREA OF NEW L | ANDSCAPING AND EARTH |
| METHODOLOGY DRAINAGE AND RETENTION CALC THE DEVELOPMENT PROCESS MA CHAPTER 6 | | |
| FIGURE 6.2.3 Precipitation Zones | CONE 4 58 58 59 59 59 59 59 59 59 59 59 59 | DEVELOPMENT IS IN ZONE 2 OF THE PRECIPITATION ZONES FIG 6.2.3 DPM |
| 6161213131313131313 | | |

Created with PTC Mathcad Express. See www.mathcad.com for more information.



WE WILL USE THE RATIONAL METHOD TO CALCULATE THE RUNOFF INCREASE INTO THE EXISTING DETENTION POND AND VERIFY THAT IT HAS ADEQUATE CAPACITY. WE WILL ALSO VERIFY THAT THE CULVERTS USED TO TRANSMIT THE DRAINAGE TO THE POND ARE ADEQUATELY SIZED.

Part 6-10(A) General Hydraulic Criteria

Closed condust sections (pipe, box or arch sections) will be designed as flowing full and, whenever possible, under pressure except when the following conditions exist:

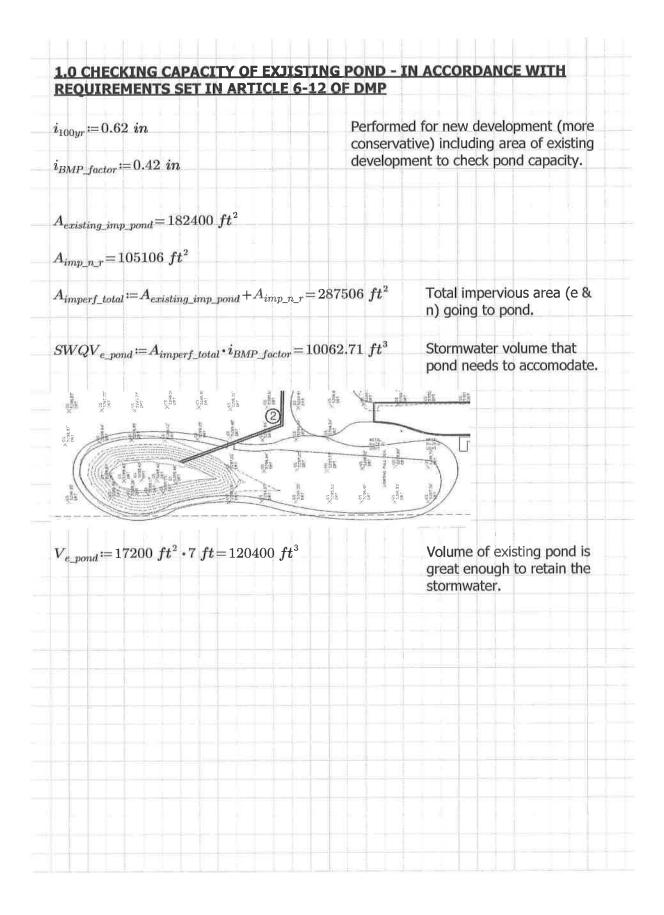
- In some ateas of high sediment potential, there is a possibility of stoppage occurring in drains. In situations where sediment may be expected, the City Engineer must be consulted for a determination of the appropriate builking factor.
- In certain situations, open channel sections upstream of the proposed closed conduit may be adversely affected by backwater.

If the proposed conduit is to be designed for pressure conditions, the HGL shall not be higher than the ground or street surface, or encroach on the same in a reach where interception of surface flow is necessary, however, in those reaches where no surface flow will be intercepted, an HGL that encroaches on or is slightly higher than the ground or street surface will be acceptable provided that pressure manholes east or will be constructed. The stormwater quality volume new development sites are required to manage is the runoff from a 0.62 inch storm. The stormwater quality volume redevelopment sites are required to manage is the runoff from a 0.48 inch storm. A site is defined as a redevelopment site if the land was occupied by an arithficial surface or by any structure intended for human occupation, including structures intended for commercial enterprise.

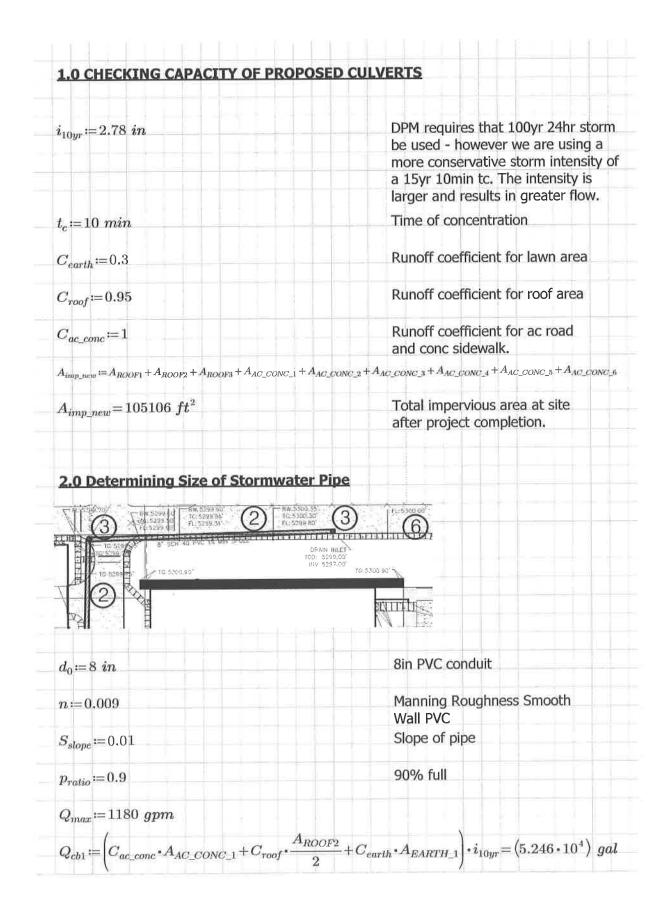
The methodology used in the U.S. Environmental Protection Agency (EPA) Report, <u>Estimating Predevelopment Hydrology in the Middle Rio Grande</u> <u>Watershed</u>, New Mexico, TetraTech, April 2014, EPA Publication Number 832-R: 14-007, yields runoif values of 0.42 inches for the 90th percentile storm and using the same methodology but generated from HEC-HMS, 0.26 inches for the 80th percentile storm.

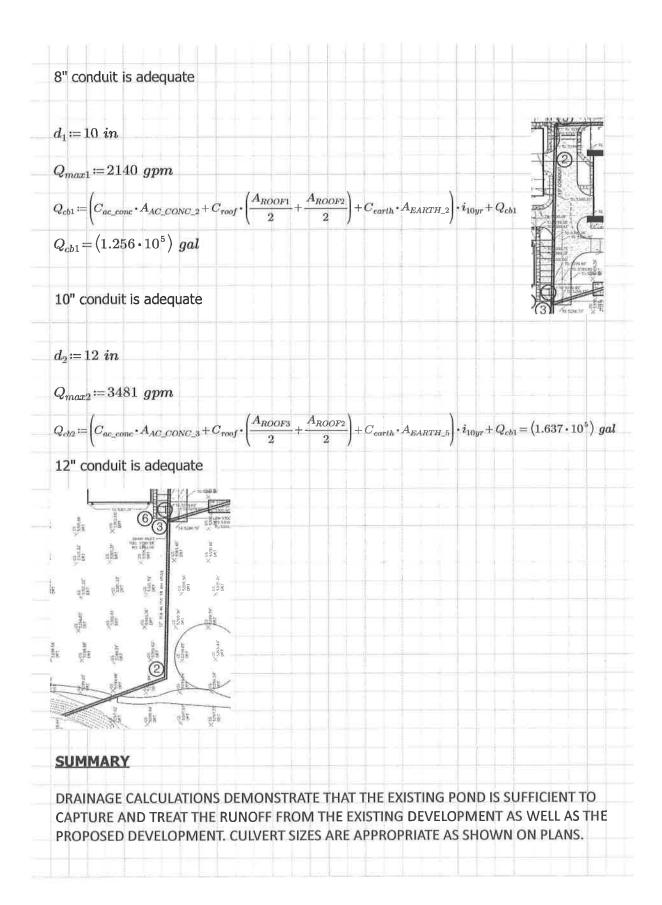
To calculate the required SWDW, multiply the impervious area draining to the BMP by 0.42 inches for new development sites and 0.26 inches for redevelopment sites. The calculations of both the required and the provided volume of each BMP must be shown on the Grading and Drainage Plan. Each BMP should be labeled on the Grading and Drainage Plan. Each BMP should be labeled on the Grading and Drainage Plan with the required SWDV and associated water surface elevation and the 100-year water surface elevation. Landscaping of surface BMPs is also required to be noted on the Grading and Drainage Plan.

| 1 | Grading and Drahvage Plan. | |
|---|--------------------------------|---|
| | | - |
| - | | |
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Manning Formula Uniform Pipe Flow at Given Slope and Depth

| Printable Title | | | | |
|---|----------------|---|-----------|-----------|
| Printable Subtitle | | | | |
| | | Results | | |
| | | Flow, Q (See notes) | 3481.0299 | gpm 🗸 |
| Inputs | | Velocity, v | 10.4178 | ft/sec ∽ |
| Pipe diameter, d ₀ | 12 in 🗸 | Velocity head, h _v | 20.2412 | in H2O 🗸 |
| <u>Manning roughness, n</u> | 0.009 | Flow area | 107.2115 | sq. in. 🛩 |
| | 0.02 | Wetted perimeter | 29.9771 | in 🛩 |
| Pressure slope (possibly $\underline{?}$ equal to pipe slope), S ₀ | rise/run 🛩 | Hydraulic radius | 3.5764 | in 🛩 |
| Percent of (or ratio to) full depth (100% or 1 if flowing | | Top width, T | 7.2000 | in 🛩 |
| full) | 0.9 fraction ~ | Froude number, F | 1.65 | |
| | | Average shear stress (tractive force), tau | 0.3721 | psf 🗸 |



Notes:

This is the flow and depth inside the pipe.

Getting the flow into the pipe may require significantly higher headwater depth. Add at least 1.5 times the velocity head to get the headwater depth or see my 2-minute tutorial for standard culvert headwater calculations using HY-8.

Manning Formula Uniform Pipe Flow at Given Slope and Depth

| Printable Title | | | | |
|---|----------------|---|-----------|-----------|
| Printable Subtitle | | | | |
| | | Results | | |
| Incorporation | | Flow, Q (See notes) | 1180.6769 | gpm 🗸 |
| Inputs | | Velocity, v | 7.9503 | ft/sec ∽ |
| Pipe diameter, d ₀ | 8 in ~ | Velocity head, h _v | 11.7882 | in H2O 🗸 |
| <u>Manning roughness, n</u> | 0.009 | Flow area | 47.6496 | sq. in. 🛩 |
| | 0.02 | Wetted perimeter | 19.9847 | in 🛩 |
| Pressure slope (possibly $\underline{?}$ equal to pipe slope), S ₀ | rise/run ∽ | Hydraulic radius | 2.3843 | in 🛩 |
| Percent of (or ratio to) full depth (100% or 1 if flowing | | Top width, T | 4.8000 | in 🗸 |
| full) | 0.9 fraction V | Froude number, E | 1.54 | |
| | | Average shear stress (tractive force), tau | 0.2481 | psf 🗸 |



Notes:

This is the flow and depth inside the pipe.

Getting the flow into the pipe may require significantly higher headwater depth. Add at least 1.5 times the velocity head to get the headwater depth or see my 2-minute tutorial for standard culvert headwater calculations using HY-8.

Manning Formula Uniform Pipe Flow at Given Slope and Depth

| Printable Title | | | | |
|---|----------------|--|-----------|-----------|
| Printable Subtitle | | | | |
| | | Results | | |
| | | Flow, Q (See notes) | 2140.7097 | gpm 🗸 |
| Inputs | 1 | Velocity, v | 9.2255 | ft/sec 🛩 |
| Pipe diameter, d ₀ | 10 in 🗸 | Velocity head, h _v | 15.8731 | in H2O 🗸 |
| <u>Manning roughness, n</u> | 0.009 | Flow area | 74.4524 | sq. in. 🗸 |
| | 0.02 | Wetted perimeter | 24.9809 | in 🛩 |
| Pressure slope (possibly $\underline{?}$ equal to pipe slope), S ₀ | rise/run ∽ | Hydraulic radius | 2.9804 | in 🛩 |
| Percent of (or ratio to) full depth (100% or 1 if flowing | Indovidin | Top width, T | 6.0000 | in 🗸 |
| full) | 0.9 fraction Y | Froude number, F | 1.60 | |
| | | Average shear stress (tractive force), tau | 0.3101 | psf 🗸 |



Notes:

This is the flow and depth inside the pipe.

Getting the flow into the pipe may require significantly higher headwater depth. Add at least 1.5 times the velocity head to get the headwater depth or see my 2-minute tutorial for standard culvert headwater calculations using HY-8.



NOAA Atlas 14, Volume 1, Version 5 Location name: Albuquerque, New Mexico, USA* Latitude: 35.0051°, Longitude: -106.6109° Elevation: 5293.72 ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dletz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_& aerials

PF tabular

| Duration | | Average recurrence interval (years) | | | | | | | | |
|----------|------------------------|-------------------------------------|---------------------|------------------------|------------------------|------------------------|------------------------|-------------------------------|-------------------------------|-----------------------------|
| Duration | 1 | 2 | 5 | 10 | 25 | 50 | 100 | 200 | 500 | 1000 |
| 5-min | 2.15 | 2.78 | 3.71 | 4.43 | 5.41 | 6.17 | 6.96 | 7.79 | 8.92 | 9.79 |
| | (1.87-2.47) | (2.41-3.20) | (3.20-4.26) | (3.82-5.06) | (4.66-6.19) | (5.27-7.06) | (5.92-7.97) | (6.58-8.90) | (7.44-10.2) | (8.12-11.2) |
| 10-min | 1.63 | 2.11 | 2.82 | 3.37 | 4.12 | 4.69 | 5.30 | 5.93 | 6.78 | 7.45 |
| | (1.42-1.88) | (1.84-2.44) | (2.44-3.25) | (2.90-3.86) | (3.54-4.71) | (4.01-5.37) | (4.50-6.06) | (5.00-6.77) | (5.66-7.77) | (6,18-8.54) |
| 15-min | 1.35 | 1.75 | 2.33 | 2.78 | 3.40 | 3.88 | 4.38 | 4.90 | 5.60 | 6.16 |
| | (1.18-1.55) | (1.52-2.01) | (2.02-2.68) | (2.40-3.19) | (2.92-3.89) | (3.31-4.44) | (3.72-5.01) | (4.13-5.60) | (4.68-6.42) | (5.11-7.06) |
| 30-min | 0.910 | 1.18 | 1.57 | 1.87 | 2.29 | 2.61 | 2.95 | 3.30 | 3.77 | 4.15 |
| | (0.792-1.04) | (1.02-1.35) | (1.36-1.81) | (1.62-2.15) | (1.97-2.62) | (2.23-2.99) | (2.50-3.37) | (2.78-3.77) | (3.15-4.32) | (3.44-4.75) |
| 60-min | 0.563 | 0.728 | 0.971 | 1.16 | 1.42 | 1.62 | 1.82 | 2.04 | 2.34 | 2.57 |
| | (0.490-0.647) | (0.633-0.838) | (0.841-1.12) | (1.00-1.33) | (1.22-1.62) | (1.38-1.85) | (1.55-2.09) | (1.72-2.33) | (1.95-2.68) | (2.13-2.94) |
| 2-hr | 0.320 | 0.410 | 0.539 | 0.644 | 0.788 | 0.904 | 1.03 | 1.15 | 1.33 | 1.47 |
| | (0.278-0.374) | (0.354-0.478) | (0.468-0.630) | (0.556-0.748) | (0.675-0.912) | (0.769-1.04) | (0.865-1.18) | (0.964-1.33) | (1.10-1.53) | (1.21-1.70) |
| 3-hr | 0.226 | 0.287 | 0.375 | 0.445 | 0.542 | 0.619 | 0.702 | 0.789 | 0.908 | 1.01 |
| | (0.198-0.262) | (0.250-0.333) | (0.327-0.436) | (0.386-0.514) | (0.467-0.626) | (0.530-0.713) | (0.597-0.807) | (0.665-0.908) | (0.758-1.05) | (0.830-1.16 |
| 6-hr | 0.132 | 0.165 | 0.212 | 0.249 | 0.300 | 0.339 | 0.381 | 0.423 | 0.482 | 0.530 |
| | (0.116-0.152) | (0.145-0.191) | (0.187-0.245) | (0.219-0.286) | (0.261-0.344) | (0.293-0.388) | (0.327-0.436) | (0.361-0.484) | (0.408-0.553) | (0.444-0.609 |
| 12-hr | 0.073 | 0.091 | 0.115 | 0.134 | 0.160 | 0.179 | 0.200 | 0.220 | 0.249 | 0.271 |
| | (0.064-0.082) | (0.081-0.104) | (0.102-0.130) | (0.118-0.151) | (0.140-0.180) | (0.157-0.202) | (0.173-0.225) | (0.190-0.248) | (0.212-0.281) | (0.230-0.307 |
| 24-hr | 0.041 | 0.052 | 0.064 | 0.075 | 0.088 | 0.099 | 0.110 | 0.121 | 0.136 | 0.147 |
| | (0.037-0.046) | (0.046-0.058) | (0.058-0.072) | (0.067-0.083) | (0.079-0.099) | (0.088-0.110) | (0.097-0.123) | (0.106-0.135) | (0.119-0.151) | (0.128-0.164 |
| 2-day | 0.022 | 0.027 | 0.034 | 0.039 | 0.047 | 0.052 | 0.058 | 0.063 | 0.071 | 0.077 |
| | (0.020-0.024) | (0.025-0.031) | (0.031-0.038) | (0.035-0.044) | (0.042-0.052) | (0.047-0.058) | (0.051-0.064) | (0.056-0.070) | (0.063-0.079) | (0.067-0.085 |
| 3-day | 0.016 | 0.020 | 0.024 | 0.028 | 0.033 | 0.037 | 0.040 | 0.044 | 0.049 | 0.053 |
| | (0.014-0.017) | (0.018-0.022) | (0.022-0.027) | (0.025-0.031) | (0.030-0.036) | (0.033-0.040) | (0.037-0.044) | (0.040-0.048) | (0.044-0.054) | (0.047-0.058 |
| 4-day | 0.013 | 0.016 | 0.019 | 0.022 | 0.026 | 0.029 | 0.032 | 0.035 | 0.038 | 0.041 |
| | (0.012-0.014) | (0.015-0.017) | (0.018-0.021) | (0.020-0.024) | (0.024-0.028) | (0.027-0.031) | (0.029-0.034) | (0.032-0.037) | (0.035-0.042) | (0.038-0.045 |
| 7-day | 0.008 | 0.010 | 0.013 | 0.014 | 0.017 | 0.019 | 0.020 | 0.022 | 0.024 | 0.026 |
| | (0.008-0.009) | (0.010-0.011) | (0.012-0.014) | (0.013-0.016) | (0.016-0.018) | (0.017-0.020) | (0.019-0.022) | (0.020-0.024) | (0.022-0.026) | (0.023-0.028 |
| 10-day | 0.006 | 0.008 | 0.010 | 0.011 | 0.013 | 0.015 | 0.016 | 0.017 | 0.019 | 0.020 |
| | (0.006-0.007) | (0.007-0.009) | (0.009-0.011) | (0.010-0.012) | (0.012-0.014) | (0.013-0.016) | (0.015-0.017) | (0.016-0.019) | (0.017-0.020) | (0.019-0.022 |
| 20-day | 0.004 | 0.005 | 0.006 | 0.007 | 0.008 | 0.009 | 0.010 | 0.010 | 0.011 | 0.012 |
| | (0.004-0.004) | (0.005-0.006) | (0.006-0.007) | (0.007-0.008) | (0.008-0.009) | (0.008-0.010) | (0.009-0.010) | (0.010-0.011) | (0.010-0.012) | (0.011-0.013 |
| 30-day | 0.003 | 0.004 | 0.005 | 0.006 | 0.006 | 0.007 | 0.007 | 0.008 | 0.008 | 0.009 |
| | (0.003-0.004) | (0.004-0.004) | (0.005-0.005) | (0.005-0.006) | (0.006-0.007) | (0.006-0.007) | (0.007-0.008) | (0.007-0.008) | (0.008-0.009) | (0.008-0.009 |
| 45-day | 0.003 (0.002-0.003) | 0.003 (0.003-0.004) | 0.004 (0.004-0.004) | 0.004 (0.004-0.005) | 0.005 (0.005-0.005) | 0.005 (0.005-0.006) | 0.006 (0.005-0.006) | 0.006 (0.006-0.006) | 0.006 (0.006-0.007) | 0.006 (0.006-0.00 |
| 60-day | 0.002 | 0.003 | 0.003 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 |

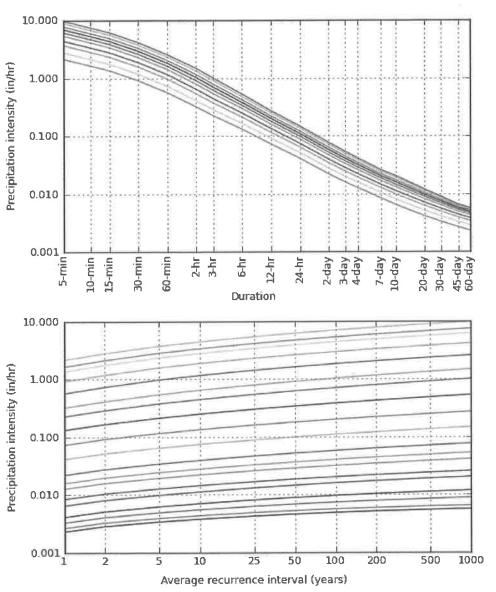
Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

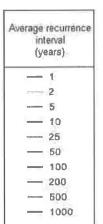
Please refer to NOAA Atlas 14 document for more information.

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PF graphical



PDS-based intensity-duration-frequency (IDF) curves Latitude: 35.0051°, Longitude: -106.6109°



| Dura | ation |
|---------|----------|
| — 5-min | — 2-day |
| 10-min | 3-day |
| 15-min | 4-day |
| 30-min | — 7-day |
| 60-min | — 10-day |
| 2-hr | — 20-day |
| — 3-hr | — 30-day |
| - 6-hr | — 45-day |
| — 12-hr | — 60-day |
| 24-hr | |

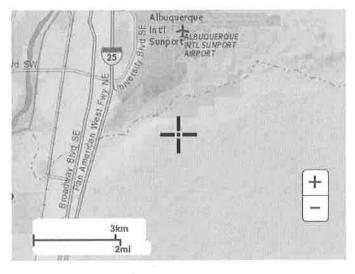
NOAA Atlas 14, Volume 1, Version 5

Created (GMT): Sat Jul 2 14:43:17 2022

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Maps & aerials

Small scale terrain



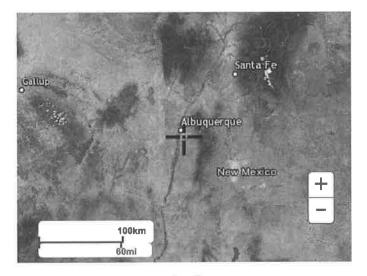
Large scale terrain



Large scale map



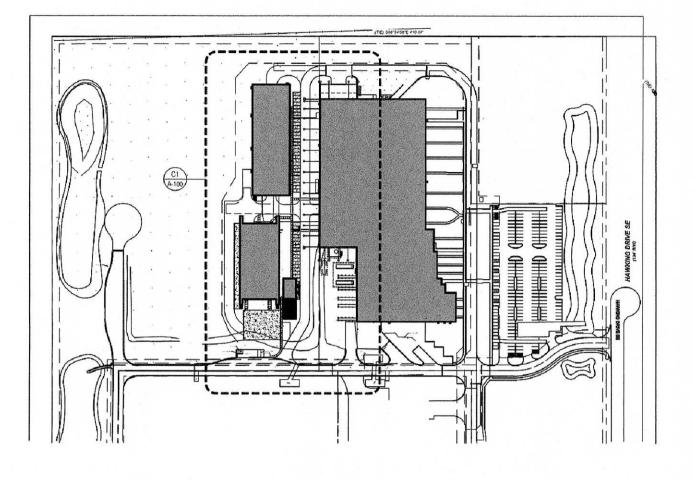
Large scale aerial



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US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

<u>Disclaimer</u>







| (A) | |
|--------------|---|
| LEGEND | |
| • | TOP OF PAVEMENT ELEVATION POINT |
| • BW: NAVD88 | BALK OF WALK ELEVATION POINT |
| • TC: NAVD88 | TOP OF CURB ELEVATION POINT |
| • FL: NAVD88 | FLOW LINE ELEVATION POINT |
| | NEW GRADNIG CONTOUR |
| \times | EXISTING ELEVATION POINT TO REMAIN |
| | EXISTING CONTOUR TO REMAIN |
| | |
| | ELECTRICAL CONDUIT - SEE MEP PLANS FOR SIZES |
| | NEW WATER LINE SEE MEP PLANS FOR ADDITIONAL INFO |
| | NEW SEWER LINE |
| sco | SEWER CLEANOUT |
| | |
| • | LIGHT POLE |
| | |

KAIROS POWER FACILITY CIVIL PLANS 5201 HAWKING DR, ALBUQUERQUE, NM

GENERAL CONTRACTION NOTES

- 1. ALL CONSTRUCTION SHALL BE IN ACCORDANCE WITH THE MOST CURRENT CITY OF ALBUQUERQUE, NEW MEXICO STANDARD PLANS AND SPECIFICATIONS ..
- 2. EXISTING GROUND CONTOURS BASED ON OVERALL GRADING PLAN PREPARED BY MATTHEW F SATCHES DATED SEPTEMBER 2020 NO 24572. CONTRACTOR SHALL VERIFY SITE CONDITIONS.
- 3. LOCATION OF EXISTING UTILITIES ARE APPROXIMATE ONLY. THE CONTRACTOR SHALL VERIFY LOCATION BY OBTAINING UTILITY LOCATE PRIOR TO BEGINNING CONSTRUCTION. EXERCISE CAUTION DURING EXCAVATION.
- 4. VERIFY HORIZONTAL AND VERTICAL LOCATION OF ALL UTILITIES ENCOUNTERED DURING CONTRACTION. RECORD LOCATION AND CHANGES TO UTILITIES IN SURVEY NOTES AND ON AS-BUILD DRAWINGS.
- 5. ELEVATION POINTS SHOWN ARE BASED ON NAVD88 DATUM.
- 6. RESTORE ALL DISTURBED PROPERTY OUTSIDE OF WORK LIMITS TO ORIGINAL CONDITIONS AND/OR IN ACCORDANCE WITH COUNTY OF SACRAMENTO STANDARDS ..
- 7. THE CONTRACTOR SHALL FOLLOW ALL CITY OF ALBUQUERQUE REGULATION FOR NOISE HOURS OF OPERATIONS AND DUST CONTROL.
- 8. WATER RESULTING FROM CONTRACTOR'S DEWATERING EFFORT MAY NOT BE PUMPED OF OTHERWISE DIVERTED INTO EXISTING STORM DRAINS UNLESS PERMITS ARE OBTAINED BY THE CONTRACTOR, INCLUDING, BUT NOT LIMITED TO, THOSE REQUIRED BY COUNTY OF SACRAMENTO STORM WATER PLAN REVIEW OFFICE. UNDER NO CIRCUMSTANCES WILL THE CONTRACTOR BE ALLOWED TO DIVERT WATER FROM AN EXCAVATION ONTO ROADWAYS., CONTRACTOR SHALL PROVIDE A DISPOSAL SITE FOR EXCESS WATER AND SHALL BE RESPONSIBLE FOR SECURING ALL NECESSARY PERMITS AND APPROVALS. CONTRACTOR SHALL PROVIDE COPIES OF NECESSARY PERMITS AND APPROVALS TO THE MOA RIGHT OF WAY PERMIT OFFICE.
- 9. KEEP SITE FREE OF CLUTTER.
- 10. MINIMIZE OFF-SITE VEHICLE TRACKING OF SEDIMENTS. SWEEP SITE ENTRANCE AND EXIT DURING CONSTRUCTION WHEN SOILS ACCUMULATE TO DEPTHS GREATER THAN ONE-FOURTH INCH. WATER EXPOSED SOILS AS NECESSARY TO CONTROL GENERATION OF DUST. CONSTRUCTION ACTIVITIES SHALL BE MONITORED ON A DAILY BASIS TO DETERMINE IF TRACKING OF DIRT AND DEBRIS ONTO THE ADJACENT ROADWAYS HAS OCCURRED. ANY NECESSARY CLEANUP SHALL BE ACCOMPLISHED ON A DAILY BASIS.
- 11. REVISIONS THAT ALTER THE REVIEWED AND APPROVED DESIGN INTENT REFLECTED IN THIS SET OF SIGNED CONSTRUCTION DRAWINGS MUST BE SUBMITTED TO CITY OF SACRAMENTO DEPARTMENT OF PUBLIC WORKS FOR REVIEW AND APPROVAL PRIOR TO CONSTRUCTION. ADJUSTMENTS NECESSARY TO ACCOMMODATE FIELD CONDITIONS MAY BE MADE IF SUCH ADJUSTMENTS ARE WITHIN THE SCOPE OF THE DESIGN INTENT AND ARE APPROVED BY THE ENGINEER OF RECORD.
- 12. CONTRACTOR SHALL REFER TO THE ARCHITECTURAL PLANS FOR PRECISE LOCATIONS OF ALL STRUCTURES AND FURNITURE.
- 13. CONTRACTOR SHALL REFER TO THE MECHANICAL, ELECTRICAL AND PLUMBING PLANS FOR SIZES AND TYPES OF UTILITY CONNECTIONS.
- 14. ALL MEANS AND METHODS OF CONSTRUCTION ARE AT THE DISCRETION OF THE CONTRACTOR AND COUNTY.
- 15. ALL EARTHWORK SHORING AND STRUCTURAL SHORING IS BY CONTRACTOR.

| | SHEET INDEX |
|-----------|---|
| SHEET NO. | SHEET TITLE |
| COVER | COVER |
| C1 | EXISTING SITE CONDITIONS |
| C2 | PROPOSED SITE CONDITIONS / GRADING & DRAINAGE |
| C3 | FINE GRADING PLAN 1 OF 3 |
| C4 | FINE GRADING PLAN 2 OF 3 |
| C5 | FINE GRADING PLAN 3 OF 3 |
| C6 | EROSION AND SEDIMENT CONTROL PLAN / HOUSE KEEPING |
| C7 | CIVIL DETAILS 1 |
| C8 | CIVIL DETAILS 2 |
| C9 | CIVIL DETAILS 3 |
| C10 | UTILITY PLANS |
| | |

Scale: NTS

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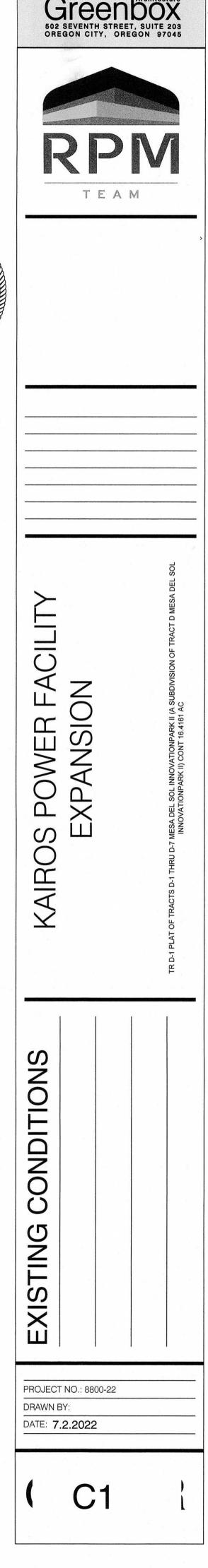


| PRACTICES | |
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