CITY OF ALBUQUERQUE

Planning Department Alan Varela, Director



December 13, 2023

Diego A. Gomez, P.E. Greenbox Architecture 502 Seventh Street, Suite 203 Oregon City, OR 97045

RE: Kairos Power Expansion – Mechanical Room Addition

5201 Hawking Drive SE

Grading Plan

Engineer's Stamp Date: 11/23/23 Hydrology File: Q16DA5000A

Dear Mr. Gomez:

PO Box 1293

Based upon the information provided in your submittal received 11/29/2023, the Grading Plan is approved for Building Permit and Grading Permit. Please attach a copy of this approved plan in the construction sets for Building Permit processing along with a copy of this letter.

Albuquerque

PRIOR TO CERTIFICATE OF OCCUPANCY:

NM 87103

1. Engineer's Certification, per the DPM Part 6-14 (F): *Engineer's Certification Checklist For Non-Subdivision* is required.

www.cabq.gov

As a reminder, if the project total area of disturbance (including the staging area and any work within the adjacent Right-of-Way) is 1 acre or more, then an Erosion and Sediment Control (ESC) Plan and Owner's certified Notice of Intent (NOI) is required to be submitted to the Stormwater Quality Engineer (Doug Hughes, PE, jhughes@cabq.gov, 924-3420) 14 days prior to any earth disturbance.

If you have any questions, please contact me at 924-3995 or <u>rbrissette@cabq.gov</u>.

Sincerely,

Renée C. Brissette, P.E. CFM Senior Engineer, Hydrology

Renée C. Brissette

Planning Department



City of Albuquerque

Planning Department

Development & Building Services Division

DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 6/2018)

BP-2023-35129 &

Project Title: Kairos Power Expansion	Building Permit #: BP-2023-07920	Hydrology File #: Q16DA5000A
DRB#: PR-2020-004448 TR D-1 PLAT OF TRACTS D-1 T	EPC#:	Work Order#:
TR D-1 PLAT OF TRACTS D-1 T Legal Description: SOL INNOVATIONPARK II) CON	HRU D-7 MESA DEL SOL INNOVATIONPARK IT 16.4161 AC	(II (A SUBDIVISION OF TRACT D MESA DEL
City Address: 5201 Hawking Drive SE, Albuqu		
Applicant: Greenbox Architecture		Contact: Derek Metson
Address: 502 Seventh St. Suite 203, Oregon 0	City, OR 97045	
Phone#: 503.207.5537	Fax#:	E-mail: permits@greenboxpdx.com
Other Contact: Kairos Power		
Address: 5201 Hawking Drive SE, Albuquerque		
Phone#: _505.702.1128	Fax#:	E-mail: gutierrez@kairospower.com
TYPE OF DEVELOPMENT: PLAT (#	f of lots)RESIDENCE X	DRB SITE ADMIN SITE
IS THIS A RESUBMITTAL? X Yes	No	
DEPARTMENT TRANSPORTATION	X HYDROLOGY/DRAINAGE	
Check all that Apply:	TYPE OF APPROV. X BUILDING PER	AL/ACCEPTANCE SOUGHT: RMIT APPROVAL
TYPE OF SUBMITTAL: ENGINEER/ARCHITECT CERTIFICATION	CERTIFICATE	OF OCCUPANCY
PAD CERTIFICATION CONCEPTUAL G & D PLAN		PLAT APPROVAL
X GRADING PLAN		R SUB'D APPROVAL
X DRAINAGE REPORT		R BLDG. PERMIT APPROVAL
DRAINAGE MASTER PLAN	FINAL PLAT A	APPROVAL
FLOODPLAIN DEVELOPMENT PERMIT A	PPLIC SIA/ RELEASE	OF FINANCIAL GUARANTEE
ELEVATION CERTIFICATE		PERMIT APPROVAL
CLOMR/LOMR	GRADING PER	RMIT APPROVAL
TRAFFIC CIRCULATION LAYOUT (TCL)	SO-19 APPROV	/AL
TRAFFIC IMPACT STUDY (TIS) STREET LIGHT LAYOUT	PAVING PERM	IIT APPROVAL
OTHER (SPECIFY)		O CERTIFICATION
PRE-DESIGN MEETING?	WORK ORDER .	
	CLOMR/LOMR	
		DEVELOPMENT PERMIT IFY)
	<u> </u>	
DATE SUBMITTED: <u>11/27/2023</u>	,	
COA STAFF:	ELECTRONIC SUBMITTAL RECEIVED:	

FEE PAID:____



Date: 11.02.2023

Site Address: Kairos Power, 5201 Hawking Dr SE, Albuquerque, NM 87106

Subject: - 24in Drainage Culvert Capacity Analysis

19357 19357 19357 19357

To whom this may concern:

I am writing to present the results of our recent engineering analysis, which focused on determining the demand and capacity of the existing 24" drainage culvert situated on the northern portion of the subject property.

Project Objective:

The primary objective of our project was to assess the capability of the 24" drainage culvert, responsible for transferring drainage from the developed sections of the subject property. Specifically, our goal was to evaluate its performance under extreme weather conditions and ascertain the impact of potential modifications, such as the addition of foundation drainage for a new 6000 square foot building.

Methodology:

We initiated our analysis by utilizing Geographic Information System (GIS) tools to calculate the drainage area, which was determined to be 11.86 acres. In our calculations, we adopted a conservative runoff coefficient of 1, effectively modeling the entire area as perfectly impervious. Additionally, we referenced NOAA rain map data to establish the 100-year 24-hour rainfall frequency, employing the Rational Method to compute the maximum flow within the culvert under these extreme conditions.

Findings:

Our findings indicate that, even under the extreme conditions of a 100-year 24-hour rain event, the subject culvert will only be 20% full, demonstrating efficient flow performance. Consequently, the inclusion of foundation drainage for the proposed 6000 square foot building is anticipated to have a negligible impact on the culvert's capacity. Importantly, as the new lateral will solely handle foundation drainage and not roof drainage, we can confidently assert that the overall capacity of the culvert will not be adversely affected.

Integration with Existing Infrastructure:

It is noteworthy that the subject culvert outfalls into an existing drainage basin, the capacity of which has been previously verified in accordance with the City of Albuquerque Development Process Manual. This further strengthens our confidence in the capacity of the entire drainage system.

Sincerely,

Dmitriy Lashkevich PE CTO – RPM Team 415-227-2880

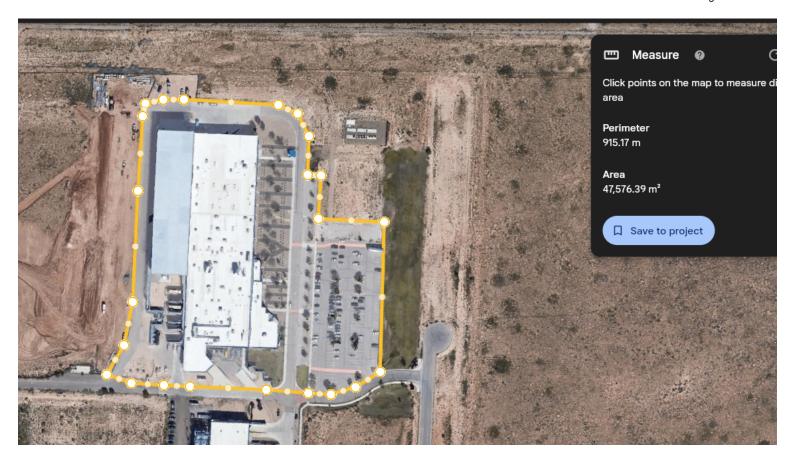
WWW.RPM-TEAM.COM



Img 1: Terrain is largely barren and undeveloped. We analyzed the drainage patterns using available GIS and topographic survey to identify the tributary area to the culvert in question.



Img 2: The image shows the original site conditions and location of the subject culvert (in blue). We identified the southern developed portion drains into a separate retention basin and does not contribute to the subject culvert. Only the developed areas highlighted in red drain into the culvert we are analyzing.



Img 3: We calculated the developed area contributing to the culvert in question.

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ive flow depth, y/d₀ 0.2 fraction ✓ X Velocity head, h₀ 1.5936 in H2O ✓ Froude number, F 0.97	Relative flow depth, y/d₀ 0.2 fraction ✓ X Velocity head, h₀ 1.5936 in H2O ✓ Froude number, F 0.97 Average shear stress (tractive force), tau 4.1810 N/m²2 ✓	Relative flow depth, y/d ₀ 0.2 fraction \(\times \) Velocity head, h _v 1.5936 in H2O \(\times \) Froude number, F 0.97 Average shear stress (tractive force), tau 4.1810 N/m^2 \(\times \) Flow, Q (See notes) 586.8024 gpm \(\times \)	Relative flow depth, y/d₀ 0.2 Ifraction ✓ X Velocity head, h₂ froude number, F 0.97 Average shear stress (tractive force), tau 4.1810 N/m²2 ✓ Flow, Q (See notes) 586.8024 gpm ✓ Full flow, Q0 6700.8520 gpm ✓	Prill Set u	rintable Title ntable Subtitle units: m mm ft in [Hide this line] ts e diameter, d ₀	24		×	Flow depth, y Flow area, a Pipe area, a0 Relative area Wetted perim Hydraulic rad) a, a/a0 neter, P _w			64.4106 452.3902 0.1424 22.2551 2.8942	sq. in. sq. in. fraction in in	~	
Froude number, F 0.97	Froude number, F Average shear stress (tractive force), tau 4.1810 N/m^2 N/m^2	Froude number, F 0.97 Average shear stress (tractive force), tau 4.1810 N/m^2 > Flow, Q (See notes) 586.8024 gpm >	Froude number, F 0.97 Average shear stress (tractive force), tau 4.1810 N/m^2 Flow, Q (See notes) 586.8024 gpm Full flow, Q0 6700.8520 gpm	Prill Set u	rintable Title ntable Subtitle units: m mm ft in [Hide this line] ts e diameter, do	24 0.015	in v	X X	Flow depth, y Flow area, a Pipe area, a0 Relative area Wetted perim Hydraulic rad Top width, T) a, a/a0 neter, P _w			64.4106 452.3902 0.1424 22.2551 2.8942 19.2000	sq. in. sq. in. fraction in in in in	n ~	
A ((() A 4040		Flow, Q (See notes) 586.8024 gpm ✓	Flow, Q (See notes) 586.8024 gpm ✓ Full flow, Q0 6700.8520 gpm ✓	Prill Set u	rintable Title ntable Subtitle units: m mm ft in [Hide this line] ts e diameter, d ₀ nning roughness, n ssure slope (possibly ? equal to pipe slope), S ₀	24 0.015 0.0058	in v		Flow depth, y Flow area, a Pipe area, a0 Relative area Wetted perim Hydraulic rad Top width, T Velocity, v	a, a/a0 neter, P _w dius, R _h			64.4106 452.3902 0.1424 22.2551 2.8942 19.2000 2.9231	sq. in. sq. in. fraction in in in ft/sec	n	
			Full flow, Q0 6700.8520 gpm ✓	Prill Set u	rintable Title ntable Subtitle units: m mm ft in [Hide this line] ts e diameter, d ₀ nning roughness, n ssure slope (possibly ? equal to pipe slope), S ₀	24 0.015 0.0058	in v		Flow depth, y Flow area, a Pipe area, a0 Relative area Wetted perim Hydraulic rad Top width, T Velocity, v Velocity head Froude numb	a, a/a0 neter, P _w dius, R _h			64.4106 452.3902 0.1424 22.2551 2.8942 19.2000 2.9231 1.5936 0.97	sq. in. sq. in. fraction in v in v ft/sec v in H2C		
		Full flow, \(\sqrt{\text{q}}\text{\text{0}} \qqrt{\text{10}7\text{\text{0}}\cdot{\text{\text{6370}\text{\text{l}\text{\text{l}\text{\text{l}\text{\text{l}\text{\text{\text{l}\text{\text{\text{l}\text{\text{\text{\text{l}\text{\tin}\text{\tex{\tex		Printer Printe	rintable Title ntable Subtitle units: m mm ft in [Hide this line] ts e diameter, d ₀ nning roughness, n ssure slope (possibly ? equal to pipe slope), S ₀	24 0.015 0.0058	in v		Flow depth, y Flow area, a Pipe area, a0 Relative area Wetted perim Hydraulic rad Top width, T Velocity, v Velocity head Froude numb Average shea	a, a/a0 neter, P _w dius, R _h d, h _v oer, F ar stress	(tractive fc	orce), tau	64.4106 452.3902 0.1424 22.2551 2.8942 19.2000 2.9231 1.5936 0.97 4.1810	sq. in. sq. in. fractio in in ft/sec in H2C		
	Full flow (1)0			Printer Printe	rintable Title ntable Subtitle units: m mm ft in [Hide this line] ts e diameter, d ₀ nning roughness, n ssure slope (possibly ? equal to pipe slope), S ₀	24 0.015 0.0058	in v		Flow depth, y Flow area, a Pipe area, a0 Relative area Wetted perim Hydraulic rad Top width, T Velocity, v Velocity head Froude numb Average shea	a, a/a0 neter, P _w dius, R _h d, h _v oer, F ar stress	(tractive fo	orce), tau	64.4106 452.3902 0.1424 22.2551 2.8942 19.2000 2.9231 1.5936 0.97 4.1810	sq. in. sq. in. fraction in in ff/sec in H2C N/m^2 gpm	n ~]	
				Pri Prii Set u	rintable Title ntable Subtitle units: m mm ft in [Hide this line]				Flow depth, y Flow area, a Pipe area, a0)			64.4106 452.3902	sq. in.		~
IFIOW. G (See Hotes) 1300 0074 100111 🔻				Printer Printe	rintable Title ntable Subtitle units: m mm ft in [Hide this line] ts e diameter, d ₀ nning roughness, n ssure slope (possibly ? equal to pipe slope), S ₀	24 0.015 0.0058	in v		Flow depth, y Flow area, a Pipe area, a0 Relative area Wetted perim Hydraulic rad Top width, T Velocity, v Velocity head Froude numb Average shea	a, a/a0 neter, P _w dius, R _h d, h _v oer, F ar stress	(tractive fo	orce), tau	64.4106 452.3902 0.1424 22.2551 2.8942 19.2000 2.9231 1.5936 0.97 4.1810	sq. in. sq. in. fractio in in ft/sec in H2C		
	Eull flow CO 6700 0E20 apps 34		Katio to tuli flow. Q/QU U.U8/6 I fraction ✓	Printer Printe	rintable Title ntable Subtitle units: m mm ft in [Hide this line] ts e diameter, d ₀ nning roughness, n ssure slope (possibly ? equal to pipe slope), S ₀	24 0.015 0.0058	in v		Flow depth, y Flow area, a Pipe area, a0 Relative area Wetted perim Hydraulic rad Top width, T Velocity, v Velocity head Froude numb Average shea	a, a/a0 neter, P _w dius, R _h d, h _v oer, F ar stress	(tractive fo	orce), tau	64.4106 452.3902 0.1424 22.2551 2.8942 19.2000 2.9231 1.5936 0.97 4.1810	sq. in. sq. in. fraction in in ff/sec in H2C N/m^2 gpm	n ~]	

We demonstrate that the maximum runoff for 100 year 24 hour storm will result in 20% of pipe capacity being utilized.

In accordance with the soils report ground water was not encountered during testing. If we conservatively assume that 50% of runoff from the roof will contribute to the foundation drainage we show below that the addition is negligible.

$$A_{roof} = 6000 \, \mathbf{ft}^2$$

$$i_{24hr_100yr} = 0.109 \frac{in}{hr}$$

$$C \coloneqq 1$$

$$Q_{additional} \coloneqq 0.5 \cdot C \cdot i_{24hr_100yr} \cdot A_{roof} = 3.397 \ \textit{gpm}$$

We demonstrate that 3.4gpm is added to the culvert and are still at 20% capacity.

Printable Title Printable Subtitle Set units: m mm ft in [Hide this line] Results Flow depth, y 4.8120 in 🕶 64.6411 Flow area, a sq. in. 🗸 Pipe area, a0 452.3902 sq. in. 🗸 Relative area, a/a0 0.1429 Inputs Wetted perimeter, Pv 22.2851 Pipe diameter, do 24 in 🗸 in 🗸 Hydraulic radius, R_h 2.9006 Manning roughness, n 0.015 Top width, T 19.2180 in 🗸 Pressure slope (possibly ? equal to pipe slope), S₀ 0.0058 rise/run Velocity, v 2.9274 ft/sec ➤ 1.5983 in H2O 🗸 Velocity head, h_v Relative flow depth, y/d₀ 0.2005 fraction ~ Froude number, F 0.97 Average shear stress (tractive force), tau 4.1903 N/m^2 ~ Flow, Q (See notes) 589.7770 gpm 🗸 Full flow, Q0 6700.8520 gpm 🕶

Ratio to full flow, Q/Q0

0.0880

fraction ~

Printable version (reload/refresh to restore)





NOAA Atlas 14, Volume 1, Version 5 Location name: Albuquerque, New Mexico, USA* Latitude: 35.0051°, Longitude: -106.6109° Elevation: 5294 ft**

source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-b	DS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) ¹												
Duration	Average recurrence interval (years)												
Duration	1	2	5	10	25	50	100	200	500	1000			
5-min	2.15 (1.87-2.47)	2.78 (2.41-3.20)	3.71 (3.20-4.26)	4.43 (3.82-5.06)	5.41 (4.66-6.19)	6.17 (5.27-7.06)	6.96 (5.92-7.97)	7.79 (6.58-8.90)	8.92 (7.44-10.2)	9.79 (8.12-11.2)			
10-min	1.63 (1.42-1.88)	2.11 (1.84-2.44)	2.82 (2.44-3.25)	3.37 (2.90-3.86)	4.12 (3.54-4.71)	4.69 (4.01-5.37)	5.30 (4.50-6.06)	5.93 (5.00-6.77)	6.78 (5.66-7.77)	7.45 (6.18-8.54)			
15-min	1.35 (1.18-1.55)	1.75 (1.52-2.01)	2.33 (2.02-2.68)	2.78 (2.40-3.19)	3.40 (2.92-3.89)	3.88 (3.31-4.44)	4.38 (3.72-5.01)	4.90 (4.13-5.60)	5.60 (4.68-6.42)	6.16 (5.11-7.06)			
30-min	0.910 (0.792-1.04)	1.18 (1.02-1.35)	1.57 (1.36-1.81)	1.87 (1.62-2.15)	2.29 (1.97-2.62)	2.61 (2.23-2.99)	2.95 (2.50-3.37)	3.30 (2.78-3.77)	3.77 (3.15-4.32)	4.15 (3.44-4.75)			
60-min	0.563 (0.490-0.647)	0.728 (0.633-0.838)	0.971 (0.841-1.12)	1.16 (1.00-1.33)	1.42 (1.22-1.62)	1.62 (1.38-1.85)	1.82 (1.55-2.09)	2.04 (1.72-2.33)	2.34 (1.95-2.68)	2.57 (2.13-2.94)			
2-hr	0.320 (0.278-0.373)	0.409 (0.354-0.478)	0.539 (0.468-0.630)	0.644 (0.555-0.747)	0.788 (0.675-0.912)	0.904 (0.769-1.04)	1.03 (0.865-1.18)	1.15 (0.964-1.33)	1.33 (1.10-1.53)	1.47 (1.21-1.70)			
3-hr	0.225 (0.197-0.262)	0.286 (0.250-0.333)	0.375 (0.327-0.435)	0.444 (0.385-0.513)	0.542 (0.466-0.625)	0.619 (0.530-0.712)	0.701 (0.597-0.807)	0.788 (0.664-0.907)	0.908 (0.757-1.04)	1.00 (0.829-1.16)			
6-hr	0.131 (0.115-0.151)	0.165 (0.145-0.191)	0.212 (0.186-0.244)	0.249 (0.218-0.286)	0.299 (0.260-0.343)	0.339 (0.292-0.388)	0.380 (0.326-0.435)	0.423 (0.361-0.484)	0.482 (0.407-0.552)	0.530 (0.443-0.608)			
12-hr	0.072 (0.064-0.082)	0.091 (0.081-0.103)	0.115 (0.101-0.130)	0.134 (0.118-0.151)	0.159 (0.140-0.179)	0.179 (0.156-0.201)	0.199 (0.173-0.224)	0.220 (0.190-0.248)	0.248 (0.212-0.280)	0.271 (0.229-0.307)			
24-hr	0.041 (0.036-0.046)	0.051 (0.046-0.057)	0.064 (0.057-0.072)	0.074 (0.066-0.083)	0.088 (0.078-0.098)	0.098 (0.087-0.110)	0.109 (0.097-0.122)	0.120 (0.106-0.134)	0.135 (0.118-0.151)	0.147 (0.128-0.164)			
2-day	0.021 (0.019-0.024)	0.027 (0.024-0.030)	0.034 (0.030-0.037)	0.039 (0.035-0.043)	0.046 (0.041-0.051)	0.051 (0.046-0.057)	0.057 (0.051-0.063)	0.063 (0.056-0.070)	0.070 (0.062-0.078)	0.076 (0.067-0.085)			
3-day	0.015 (0.014-0.017)	0.019 (0.017-0.021)	0.024 (0.022-0.026)	0.027 (0.025-0.030)	0.032 (0.029-0.035)	0.036 (0.033-0.039)	0.040 (0.036-0.044)	0.044 (0.039-0.048)	0.049 (0.044-0.053)	0.053 (0.047-0.058)			
4-day	0.012 (0.011-0.013)	0.015 (0.014-0.017)	0.019 (0.017-0.020)	0.022 (0.020-0.023)	0.025 (0.023-0.028)	0.028 (0.026-0.031)	0.031 (0.029-0.034)	0.034 (0.031-0.037)	0.038 (0.035-0.041)	0.041 (0.037-0.044)			
7-day	0.008 (0.007-0.009)	0.010 (0.009-0.011)	0.012 (0.011-0.013)	0.014 (0.013-0.015)	0.016 (0.015-0.018)	0.018 (0.017-0.019)	0.020 (0.018-0.021)	0.021 (0.020-0.023)	0.024 (0.022-0.025)	0.025 (0.023-0.027)			
10-day	0.006 (0.006-0.006)	0.008 (0.007-0.008)	0.009 (0.009-0.010)	0.011 (0.010-0.012)	0.013 (0.012-0.014)	0.014 (0.013-0.015)	0.015 (0.014-0.017)	0.017 (0.015-0.018)	0.019 (0.017-0.020)	0.020 (0.018-0.021)			
20-day	0.004 (0.003-0.004)	0.005 (0.004-0.005)	0.006 (0.005-0.006)	0.007 (0.006-0.007)	0.008 (0.007-0.008)	0.008 (0.008-0.009)	0.009 (0.008-0.010)	0.010 (0.009-0.011)	0.011 (0.010-0.012)	0.011 (0.010-0.012)			
30-day	0.003 (0.003-0.003)	0.004 (0.003-0.004)	0.004 (0.004-0.005)	0.005 (0.005-0.005)	0.006 (0.005-0.006)	0.006 (0.006-0.007)	0.007 (0.006-0.007)	0.007 (0.007-0.008)	0.008 (0.007-0.009)	0.008 (0.008-0.009)			
45-day	0.002 (0.002-0.002)	0.003 (0.003-0.003)	0.003 (0.003-0.004)	0.004 (0.004-0.004)	0.004 (0.004-0.005)	0.005 (0.004-0.005)	0.005 (0.005-0.006)	0.005 (0.005-0.006)	0.006 (0.005-0.006)	0.006 (0.006-0.006)			
60-day	0.002 (0.002-0.002)	0.002 (0.002-0.003)	0.003 (0.003-0.003)	0.003 (0.003-0.004)	0.004 (0.003-0.004)	0.004 (0.004-0.004)	0.004 (0.004-0.005)	0.005 (0.004-0.005)	0.005 (0.005-0.005)	0.005 (0.005-0.006)			

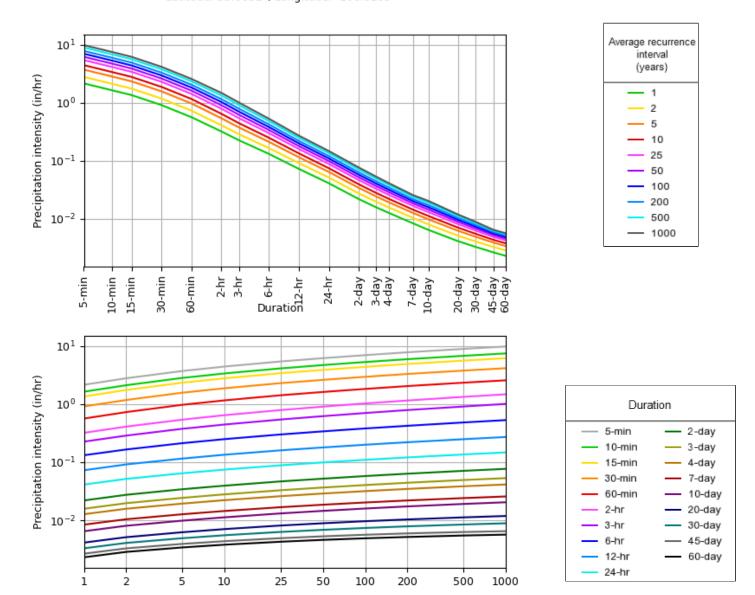
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PDS-based intensity-duration-frequency (IDF) curves Latitude: 35.0051°, Longitude: -106.6109°



NOAA Atlas 14, Volume 1, Version 5

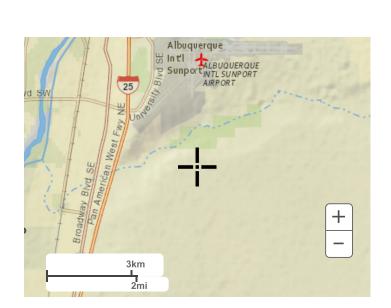
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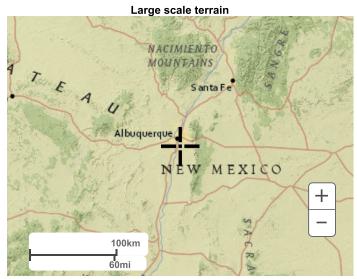
Back to Top

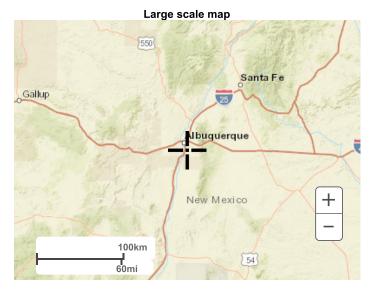
Average recurrence interval (years)

Maps & aerials

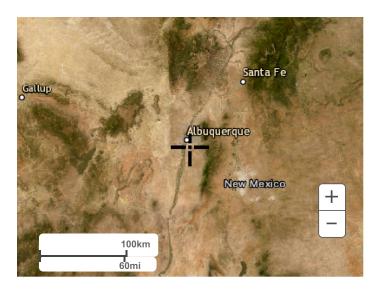
Small scale terrain







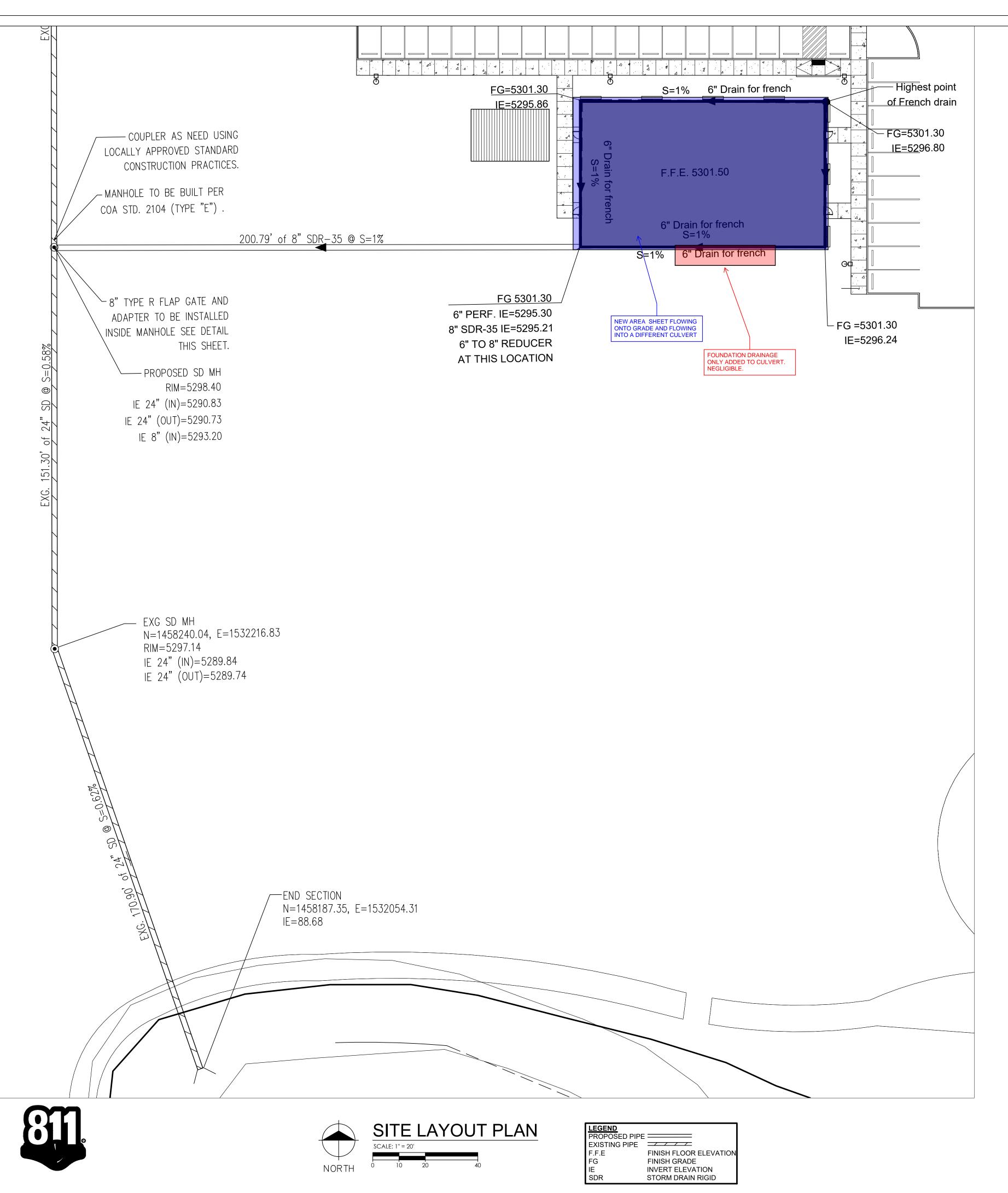
Large scale aerial



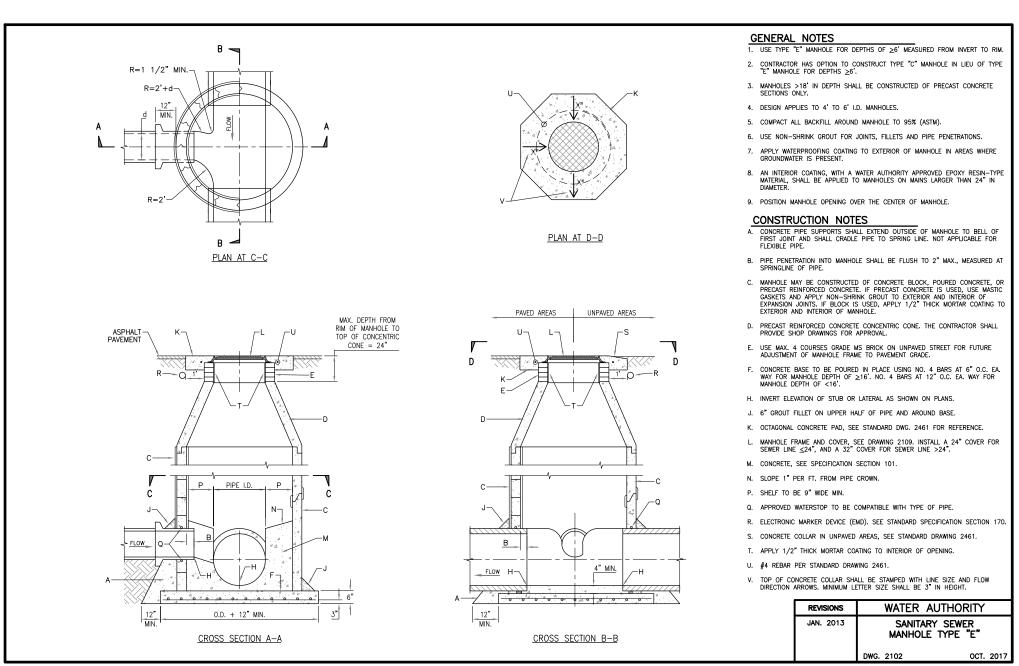
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US Department of Commerce
National Oceanic and Atmospheric Administration
National Weather Service
National Water Center
1325 East West Highway
Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

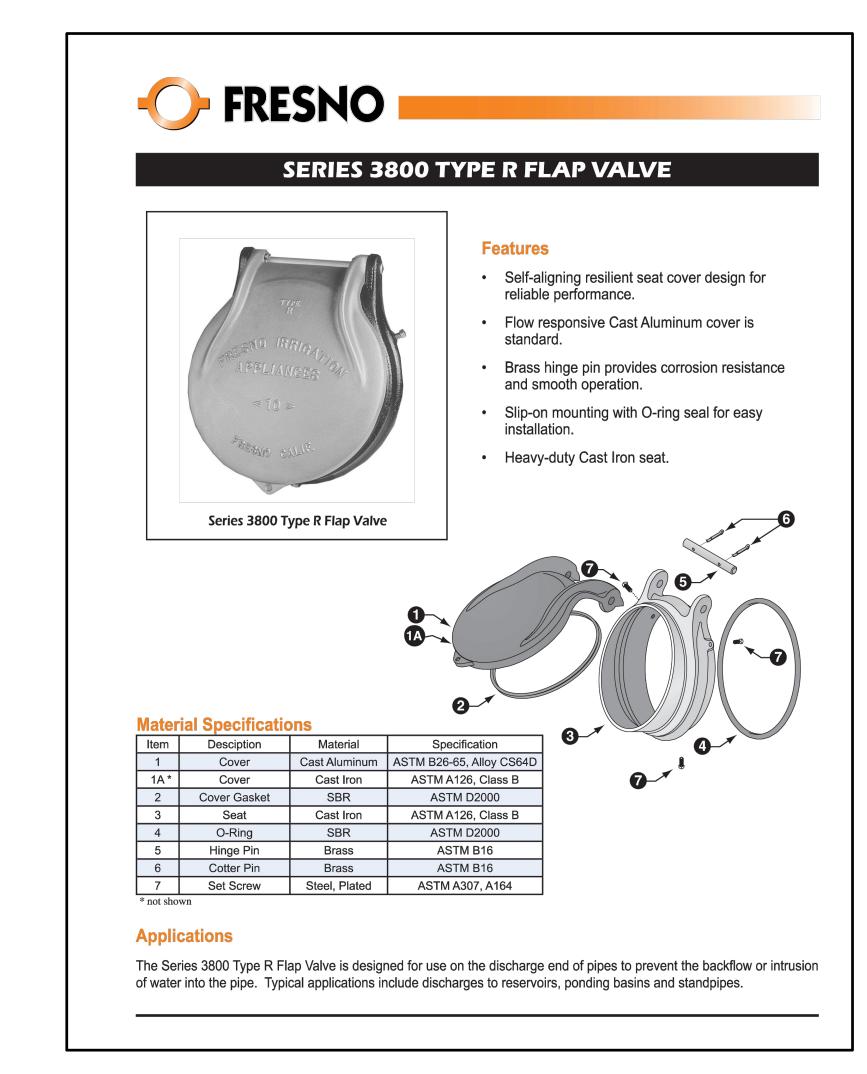
Disclaimer



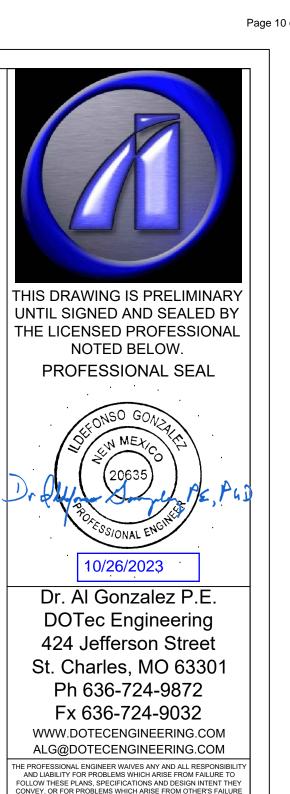
THIS PLAN SHOWS THE PROPOSED 8" DRAINAGE LATERAL THAT WILL TRANSFER FOUNDATION DRAINAGE TO THE 24" CULVERT IN QUESTION. ITS IMPORTANT TO NOTE THAT THE AREA HIGHLIGHTED IN BLUE WILL SHEET FLOW TO A SEPARATE DRAINAGE CULVERT AND WILL NOT CONTRIBUTE TO THE 24" **CULVERT IN QUESTION.**



SANITARY SEWER DETAIL N.T.S.



TYPE R FLAP GATE DETAIL



SHEET NAME:

5201 HAWKING DRIVE S.E. ALBUQUERQUE, NM -KAIR

SHEET NUMBER:

DRAWN BY:

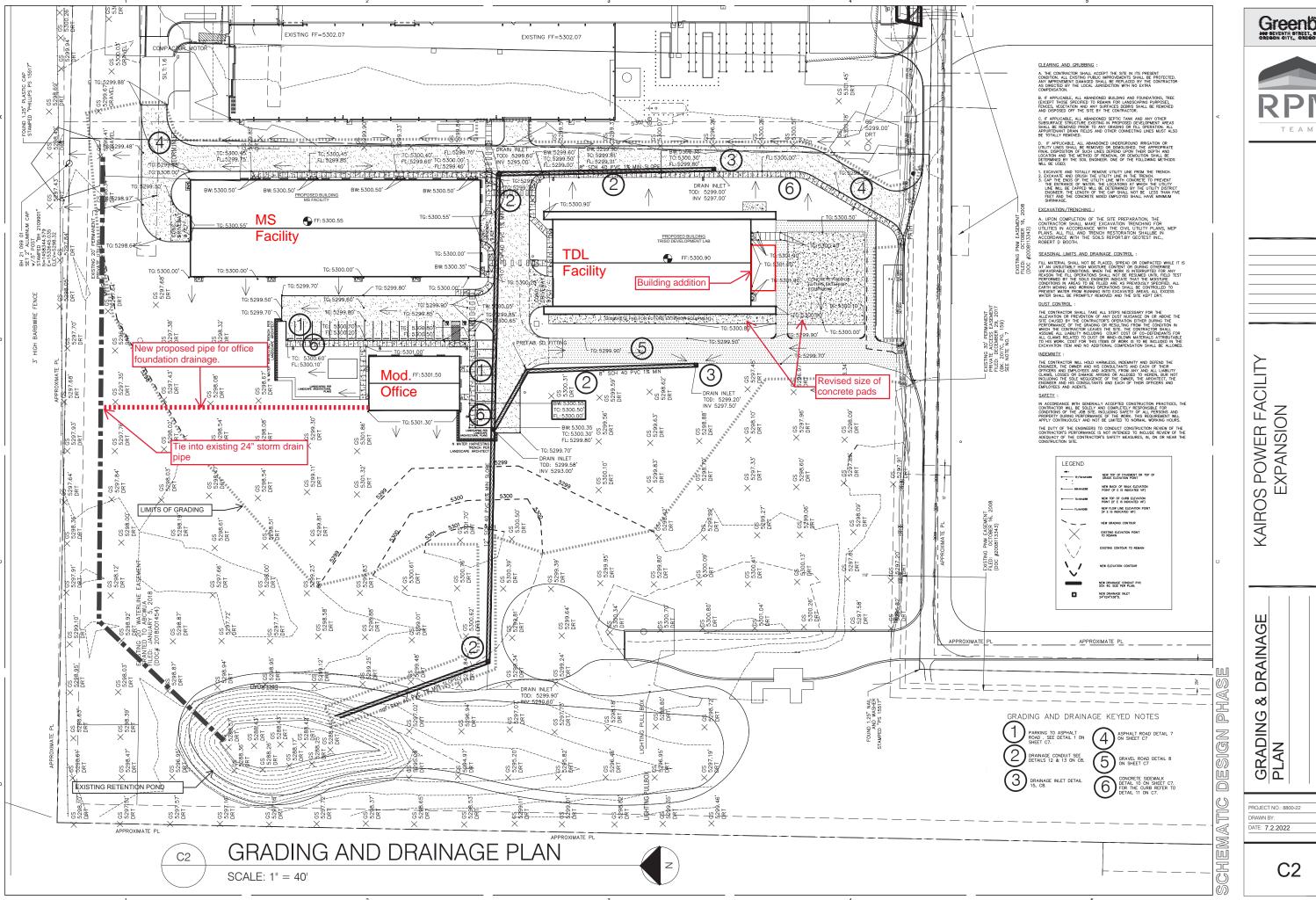
PROJECT NUMBER: 2309077

CHECKED BY: MAD

PRELIMINARY DRAWING

SITE LAYOUT

10/26/2023



Greenbox



